

OBSERVATIONS

MADE AT THE

MAGNETICAL AND METEOROLOGICAL OBSERVATORY

ΑT

TORONTO IN CANADA.

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INTRODUCTION.

It has been suggested to me that the time is arrived when a brief review of what the Colonial Magnetic Observatories have accomplished may be desirable, showing—primarily, how far they have successfully carried out the instructions originally drawn up for their guidance by the Committee of Physics of the Royal Society (and approved by the President and Council of that body); and, collaterally, how a similar organization may be made available for the further prosecution of the objects for which the Colonial Observatories were established.

The magnetic investigations designed to be carried into execution by the Colonial Observatories embraced a much wider scope than had been contemplated by any previous institutions, or than had been provided for by the arrangements or instrumental means of any then existing establishment, whether national or private. Not, as previously, limited to observations of a single element (the Declination), or combining at the most one only of the components of the Magnetic Force, the instructions of the Royal Society, and the instrumental means prepared under its direction, provided for the examination, in every branch of detail, of each of the three elements which, taken in combination, represent, not partially but completely, the whole of the magnetic affections experienced at the surface of the globe, classed under the several heads of absolute values, secular changes, and variations either periodical or occasional,—and proceeding from causes either internal or external. To meet the requirements of inductive reasoning, it was needful that the results to be obtained should comprehend all particulars under these several heads attainable by an experimental inquiry of limited duration. That no uncertainty might exist as to the objects to which, in so novel an undertaking, attention was to be directed, the Report of the Committee, approved and adopted by the President and Council of the Royal Society, conveyed in a very few sentences, remarkable alike for their comprehensiveness and conciseness, the desiderata of magnetical science. It may be convenient to reproduce these, when desiring to show the degree in which the Observatories have fulfilled their contemplated purposes:—"The observations will naturally refer

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"themselves to two chief branches, into which the science of terrestrial magnetism in its present state may be divided. The first comprehends the actual distribution of the magnetic influence over the globe, at the present epoch, in its mean or average state, when the effects of temporary fluctuations are either neglected, or eliminated by extending the observations over a sufficient time to neutralize their effects. The other comprises the history of all that is not permanent in the phenomena, whether it appear in the form of momentary, daily, monthly, or annual change and restoration, or in progressive changes not compensated by counter-changes, but going on continually accumulating in one direction, so as in the course of many years to alter the mean amount of the quantities observed."—(Report of the Committee of Physics, pp. 1 and 2.)

With reference to the first of these two branches, viz. the actual distribution of the magnetic influence over the globe at the present epoch, the Report goes on to state:—"The three elements, viz. the horizontal direction, the dip, and the intensity of the Magnetic Force, require to be precisely ascertained before the magnetic state of any given station on the globe can be said to be fully determined and as all these elements are at each point now ascertained to be in a constant state of fluctuation, and affected by transient and irregular changes, the investigation of the laws, extent, and mutual relations of these changes is now become essential to the successful prosecution of magnetic discovery."

With reference to the second branch, viz. "the secular and periodical variations," it is observed, that "the progressive and periodical being mixed up with the transitory "changes, it is impossible to separate them so as to obtain a correct knowledge and analysis of the former, without taking express account of and eliminating the latter;" and with reference to the secular changes in particular, it is remarked, "These cannot be concluded from comparatively short series of observations, without giving to those observations extreme nicety, so as to determine with perfect precision the mean state of the elements at the two extremes of the period embraced, which, as already observed, presupposes a knowledge of the casual deviations."

It is clear from these extracts, that in the discussion of the observations the first point to be attended to, in the order of time, ought to be an investigation into "the "laws, extent, and mutual relations of the transient and" (as they were called at the time the Report was written) "irregular changes," as a preliminary step to the elimination of their influence on the observations from which a correct knowledge and analysis of the progressive and periodical changes were to be obtained. It will be

proper to show, therefore, in the first place, what the Observatories have accomplished in regard to the so-called casual or transitory variations.

Casual Variations.—All that was known regarding these phenomena at the period when the Report of the Committee of Physics was written, was, that there occurred occasionally, and, as it was supposed, irregularly, disturbances in the horizontal direction of the needle, which were known to prevail, with an accord which it was impossible to ascribe to accident, simultaneously over considerable spaces of the earth's surface. and were believed to be in some unknown manner connected, either as cause or effect, with the appearances of the aurora borealis. The chief feature by which the presence of a disturbance of this class could be recognized at any instant of observation,—or by which its existence might be subsequently inferred independently of concert or comparison with other Observatories,—appeared to be the deflection of the needle from its usual or normal position to an amount much exceeding what might reasonably be attributed to irregularities in the ordinary periodical fluctuations. The observations which had been made on the disturbances anterior to the institution of the Colonial Observatories had been chiefly confined to the Declination. A few of the German Observatories had recently began to note the disturbances of the Horizontal Force, but as yet no conclusions whatsoever as to their laws had been obtained;—in the words of the Committee's Report, the disturbances "apparently observe no law."—(Report, p. 10.) By the instructions cited above, the field of research was enlarged, being made to comprehend the disturbance-phenomena of the three elements; and the importance of their examination was urged, not alone as a means of eliminating their influence on the periodic and progressive changes, but also on the independent ground that "the "theory of the transitory changes might prove itself one of the most interesting and " important points to which the attention of magnetic inquirers can be turned, as "they are no doubt intimately connected with the general causes of terrestrial " magnetism, and will probably lead us to a much more perfect knowledge of those " causes than we now possess."

The feature which has been referred to as furnishing the principal if not the only certain characteristic of a disturbance of this class, namely, the magnitude of the departure from the usual or normal state at the instant of observation, has, in the discussion of the observations, been made available for the object at present under notice; it has afforded the means of recognizing and separating from the entire mass of hourly observations, taken during several years, a sufficient body of observations to furnish the necessary data for investigating at three points of the earth's surface—one in the

temperate zone of the northern hemisphere, a second in the temperate zone of the southern hemisphere, and a third in the tropics—the laws or conditions regulating or determining the occurrence of the magnetic disturbances. The method by which this separation has been effected has been explained on several recent occasions, and will be found fully described in pp. viii, ix, and x of the present volume, when treating of the disturbances of the Horizontal Force at Toronto. By processes of a similar description, the disturbances of principal magnitude in each of the three elements, the Declination, Inclination, and Total Force, have been separated from the other observations at the three Observatories of Toronto, Hobarton, and St. Helena, and submitted to an analysis, of which the full particulars as regards the Toronto observations are contained in the present volume, as those of Hobarton and St. Helena will be in volumes which have yet to appear. By the adoption of a uniform magnitude as constituting a disturbance throughout the whole period comprised by the analysis, the amount of disturbance in the several years, months, and hours is rendered intercomparable. The result of this investigation (which could not be otherwise than a very laborious operation, since the Toronto observations alone, for example, considerably exceeded 100,000 in number, each of which had to be passed through several distinct processes), has made known to us that this class of phenomena, which may with propriety and advantage receive in future the appellation of occasional, are, in their mean or average effects, subject to periodical laws of a very systematic character, placing them, as a first step towards an acquaintance with their physical causes, in immediate connection with the Sun as their primary exciting cause. They have, 1°, a diurnal variation which follows the order of the solar hours, and manifests, therefore, its relation to the sun's position as affected by the earth's rotation on its axis; 2°, an annual variation, connecting itself with the sun's position in regard to the ecliptic; and, 3°, a third variation, which seems to refer still more distinctly to the direct action of the sun, since both in period, and in epochs of maximum and minimum, it coincides with the remarkable solar period of about ten or eleven of our years, the existence of which has been recently made known to us by the phenomena of the solar spots; but which, as far as we yet know, is wholly unconnected with any thermic or physical variation of any description (except magnetic) at the surface of the earth, and equally so with any other cosmical phenomena with which we are acquainted. The discovery of a connection of this remarkable description, giving apparently to magnetism a much higher position in the scale of distinct natural forces than was previously assigned to it, may justly be claimed on the part of the Colonial Observatories, as the result of the system of observation enjoined (and so patiently and carefully maintained), and of the investigation for which it has supplied the data; since it was by means of the

disturbance-variations so determined, that the coincidence between the phenomena of the solar spots and the magnitude and frequency of magnetic disturbances was first perceived and announced.—(Phil. Trans. 1852, Art. viii.)

The extent and mutual relation of the disturbance-variations of the three elements, even at a single station (as is shown in the present volume for Toronto), supply a variety of points of approximation and of difference, which are well suited to elucidate the physical causes of these remarkable phenomena; but valuable as such aids may be when obtained for a single station, their value is greatly augmented when we are enabled to compare and combine the analogous phenomena as they present themselves at different points of the earth's surface. To give but a single example: there are certain variations produced by the mean effects of the disturbances which attain their maximum at Toronto during the hours of the night (pp. lix-lxi of this volume); the corresponding variations attain their maximum, at Hobarton, also during the hours of the night, but with a small systematic difference as to the precise hour, and with this distinguishing peculiarity, that the deflection at Hobarton is of the opposite pole of the needle (or of the same pole in the opposite direction) to the Toronto disturbance; whilst at a third station, St. Helena, which is a tropical one, the hours of principal disturbance are those, not of the night, but of the day. A very superficial examination is sufficient to show that for the generalisation of the facts,—a generalisation which is indispensable for their correct apprehension and employment in the formation of a theory,—the stations at which the phenomena are known must be increased. Those which were chosen for a first experiment were well selected to prove the importance of the investigation, and thus to lead to its extension. It is only at the Colonial Observatories that the disturbance-variations have hitherto been made out; and, guided by experience, we may infer that by adopting a similar organization and similar processes of observation at other stations, similar results may be expected, and the inquiry be further prosecuted.*

^{*}The Colonial Observatories which were under my superintendence were originally four in number; viz. Toronto, St. Helena, Cape of Good Hope, and Hobarton. In July 1846 the detachment of the artillery at the Cape of Good Hope was withdrawn by orders from England, and the charge of the Magnetical and Meteorological Observations transferred to Mr. Maclear, the Government astronomer at that station. The Magnetical Observations made at the Cape, whilst the Magnetic Observatory was one of those which were under my superintendence, were published in 1851 in a volume similar to the present. Since the transfer to Mr. Maclear, Mr. Pierce Morton, a gentleman of considerable mathematical attainments, who has been added as an assistant to take charge, under Mr. Maclear, of that branch of the Cape Observatory, has applied himself to the investigation of the lunar magnetic influence (as derived from the Cape Observations), with a view of presenting the results to the Royal Society. For this and for other investigations into which he may desire to enter, he will have the entire series of observations, viz. those, as above stated, already published, and those which have been made since the transfer of the Observatory up to the present time.

Periodical Variations.—The anticipation expressed in the Report of the Committee of Physics, that, for the purpose of obtaining a correct knowledge of the "regular periodical " variations," it would be found necessary to eliminate the "casual perturbations," has been fully confirmed. Had the latter been strictly "casual," or accidental in a sense contra-distinguished from and opposed to periodical, a sufficiently extended continuance of observation might have occasioned their mutual compensation; but now that we have learned that the mean effects which they produce are governed by periodical laws, and that these laws and those of the regular periodical variations are dissimilar in their epochs, it is manifest that in their joint and undivided effects we have two variations, due to different causes and having distinct laws, superimposed upon each other; to know the one correctly, we must necessarily therefore eliminate the other. A striking illustration of the importance of such elimination is furnished by the solardiurnal variation of the Total Force. It will readily be imagined that the question must be an important one, whether a variation which is supposed to derive its origin from the sun be a single or a double progression; whether it have two maxima and two minima in the 24 hours, or but one maximum and one minimum in that period. When no separation is made of the disturbances, the progression appears to be a double one, having two minima, one occurring in the day and the other in the night. With the removal of the disturbed observations the night-minimum disappears, and we learn that the regular solar-diurnal variation of the Total Force has but one notable inflection in the 24 hours; viz. that which takes place during the hours when the sun is above the horizon. The night-minimum is, in fact, the mean effect of the occasional disturbances (pp. xciii—xcv of this volume). It is probable that the nocturnal inflection of the solar-diurnal variation of the Declination may be ascribed to the same cause, namely, to the superposition of two distinct variations.

A careful analysis of the solar-diurnal variations of the Declination at the Colonial Observatories has brought to light the existence at all these stations of an annual inequality in the direction of the needle, concurrent with changes in the sun's declination, having its maxima (in opposite directions) when the sun is in or near the opposite solstices, and disappearing at or near the epochs of the equinoxes. An intercomparison of the results of the analysis at these stations has shown, that this inequality has the remarkable characteristic of having notably the same direction and amount in the southern as in the northern hemisphere, and in the tropical as in the temperate zones. An ingenious explanation of these phenomena has been suggested by Dr. Langberg of Christiania (Proceedings of the Royal Society, Vol. VII., p. 345); but whether this explanation be or be not the correct one, the

theoretical importance of the facts is considerable, inasmuch as they appear to be wholly irreconcilable with the hypothesis which would attribute the magnetic variations to thermic causation. We may ascribe to the general and almost exclusive prevalence of the thermic hypothesis, and to its influence on magnetic reasonings, that the well-known erroneous opinion was so confidently promulgated by a deservedly high magnetic authority,* that a line must exist surrounding the globe in which the needle would be found to have no diurnal variation. We have now, on the contrary, reason to be assured by the facts above referred to that there is no such line, but that everywhere in the regions of its supposed existence a diurnal variation subsists, having opposite characteristics in opposite parts of the year, as influenced by the sun's position on either side of the equator, and disappearing only at the epochs when the sun passes from south to north or from north to south declination.

Lunar Variation.—But if thermic relations have failed to supply a connecting link between the sun and those magnetic variations which are, without doubt, referable to the sun as their primary cause, the failure of that hypothesis is made still more obvious by the existence of variations governed by the moon's position relatively to the place of observation. We are indebted to Mr. Kreil, now holding the same position in Austria that I have filled in England, for the first suggestion of the existence of a lunardiurnal variation of one of the elements, viz. the Declination, founded on observations at Milan and Prague; and in the present volume, pp. lxxviii-lxxxvi, will be found a complete exposition of the facts of the moon's diurnal influence on all the three magnetic elements at Toronto, viz. on the Declination, Inclination, and Total Force. In the case of this investigation also, notwithstanding the smallness of the values concerned, the instrumental means supplied to the Colonial Observatories have been found competent to determine with an approximation sufficient for present theoretical purposes, the character and amount for each element of the regular daily effect of the moon on the terrestrial magnetic phenomena, the existence of which does not appear to have been even suspected at the time when the Report of the Committee of Physics was drawn up. The discovery of the moon's influence on any of the magnetic elements is due, as already stated, to Mr. Kreil; but Toronto is the first, and as yet the only, station at which the numerical values at every lunar hour of the lunardiurnal variations of the three elements have been published. Corresponding statements to that which has been given for Toronto will be given for St. Helena and Hobarton in the volumes of those Observatories which are now in preparation. All the results

^{*} Arago, Annuaire, 1836, p. 284.

at the three stations present the same general characters. The lunar influence does not appear to partake in the decennial inequality which is found in all the variations depending upon the sun.—(Phil. Trans. 1857, Art. I.) The lunar-diurnal variation of each of the elements is a double progression in the 24 lunar hours, having epochs of maximum and minimum symmetrically disposed. In character, therefore, it differs from what might be expected to take place if the moon were possessed of inherent magnetism—i.e. if she were a magnet, as it is usually termed, per se—and accords with the phenomena which might be expected to follow if she were magnetic only by induction from the earth. On the other hand, it is believed that the amount of the variation, as observed at each of these stations, very far exceeds what can be imagined to proceed from the earth's inductive action reflected from the moon. In this theoretical difficulty, we are naturally thrown back to seek a more extensive knowledge of the phenomena than we have yet obtained, and to the generalisation which will follow when sufficient materials for it have been procured. In subordinate particulars a difference which is apparently systematic is perceived to exist in regard to the hours which constitute the epochs of maxima and minima at the three stations, as well as in regard to the amounts of the respective variations; these differences are no doubt intimately connected with the causes of the phenomena, and are likely to lead to their elucidation. It is therefore greatly to be desired that the number of stations furnishing complete determinations, such as the Colonial Observatories only have hitherto supplied, should be increased.

The domain of periodical variations has thus been considerably enlarged since the Report of the Committee of Physics was drawn up, and must henceforth be understood to comprise, in addition to the variations "whose amount is a function " of the hour-angle of the sun, and of his longitude," [or of his declination] (Report, p. 10)-1°, those variations of the three elements whose amount is a function of the hour-angle of the moon; 2°, those variations which were classed in the Committee's Report as "irregular," or "apparently observing no law," but which are now known to be governed by laws depending on the sun's declination and hour-angle; and 3°, those variations, both "regular" and "occasional," which have their epochs and amounts dependent apparently on a solar period of not yet perfectly ascertained duration, manifesting itself also by periodical changes in the frequency and amount of the solar spots. With the exception of the last-named class, all these variations require for their generalisation that the phenomena should be investigated at several points of the earth's surface widely distant from each other; and we have now the knowledge, grounded on experience, that a very few years are sufficient for the observations at each station,

with the instrumental means and methods recommended by the Royal Society, and when the investigation is made a primary object by those who engage in it.

Absolute Values and Secular Changes.—But interesting and valuable as is the acquisition of a fuller and more precise knowledge of the comparatively small magnetic variations, produced at the surface of the earth by the action or influence of external bodies, even greater importance seems to attach, when terrestrial magnetism is in question, to the purposes of that distinct branch of the duties of a Magnetic Observatory, which consists in the determination of the absolute values and secular changes of the three magnetic elements. By the absolute values we seek to acquire a knowledge of the actual present order and distribution of the terrestrial magnetic influence at the surface of the earth, and to provide the materials by which the constancy, or otherwise, of the earth's magnetic charge may hereafter be examined; and by determinations of the present direction and amount of the secular changes, we seek to become acquainted with the laws, and ultimately with the causes, of that most mysterious change, by which the magnetic condition of the globe at one epoch passes progressively and systematically into that of another. It is specially by determinations of this class, obtained with the necessary precision in different parts of the globe, that (in the words of the Committee's Report) the "patient inductive inquirer " must seek to ascend to the general laws of the earth's magnetism." At the time when the Report of the Committee of Physics was written, doubts were reasonably entertained whether the limited time during which the Colonial Observatories were likely to be maintained in action would be sufficient for the determination of the secular changes; and it was therefore very properly urged, that "these changes " cannot be concluded from comparatively short series of observations without giving " to the observations extreme nicety, so as to determine with perfect precision the " mean state of the elements at the two extremes of the period embraced." It is with much satisfaction, and with a well-deserved recognition of the pains which have been bestowed by the successive Directors of the Toronto Observatory, and their assistants, to this branch of their duties, that I am able to refer to the determinations of the absolute values and secular changes of the three elements contained in this volume, in evidence that the instrumental means which were devised, and the methods which have been adopted, have proved, under all the disadvantages of a first essay, sufficient to determine these data with a precision which is greatly in advance of preceding experience, and, as far as may be judged, equal to the present requirements of theoretical investigation. It should, moreover, be noticed, that Toronto is a station where the casual and periodical variations, which it was apprehended would seriously

interfere with the determination of absolute values, are unusually large. We may derive, therefore, the greatest encouragement from the results thus obtained, to persevere in a line of research which is no longer one of doubtful experiment, and to give it that further extension which the interests of science require.

Amongst the results which have recompensed the labours of the Colonial Observatories in this branch of their inquiries, perhaps there is none of more general theoretical importance than the conclusion which has been established by means of the observations of the Declination at St. Helena, that the current annual amount of secular change takes place by equal aliquot portions in every month, and even in every fortnight, of the year. The magnitude of the annual change of the Declination at St. Helena, 8' (or more precisely 7'·93), in each of the eight years during which the observations were maintained, and the comparative tranquillity of the tropical regions in regard to magnetic disturbances, were circumstances which made St. Helena a particularly eligible locality for this investigation. The result has been to remove secular change conclusively and altogether from the category of atmospheric or thermic relations, with which, in the absence of a correct knowledge of the facts, it has frequently been associated, and to characterize it henceforward as a phenomenon of far more systematic order and regularity than had previously been generally apprehended.—(Proceedings of the Royal Society, vol. VII. pp. 67—75.)

It has thus been shown that in each and all of the branches of inquiry for which the institution of the Colonial Observatories was recommended they have accomplished the objects which were contemplated, and have in many respects exceeded the expectations on which the recommendation was founded. Nor has the scope of their performance been limited to a mere registry of the observations, or to their publication in a crude and undigested form. It was well remarked by an authority of the greatest weight, when addressing the British Association on the occasion of the assembly of the Magnetical and Meteorological Conference at Cambridge in 1845 (Herschel, Address, p. xxxv), that "a man may as well keep a register of his dreams as of the " weather or any other set of daily phenomena, if the spirit of grouping, combining, and " eliciting results be absent." To advance by the simple and straightforward path of inductive inquiry, in a science such as terrestrial magnetism in which a physical theory has yet to be sought, the endeavour must be made "to grapple with the palpable " phenomena, seeking means to reduce their features to measurement, the measure-" ments to laws, the laws to higher generalisations; and so step by step to advance to " causes and theories." The mere observational part is not, and ought never to be, viewed as the fulfilment of the duties of institutions such as Magnetic Observatories;

those duties ought always to be held to include (either on the part of the Directors of the Observatories themselves, or on that of persons who, as Superintendents or otherwise, have constantly watched the progress of the work) "the systematic deduction from " the registered observations of the mean values, and of the local coefficients of diurnal, "annual, and secular change," because "no other class of persons stands in anything like " so favourable a position for working out the first elementary laws of phenomena, and " referring them to their immediate points of dependence," as those who have directed or superintended the processes by which the data required for the knowledge of the phenomena have been obtained. The introductory discussions prefixed to the several volumes which contain the observations of the Colonial Observatories,—and a succession of papers presented to the Royal Society and published in the Philosophical Transactions,—bear testimony to at least unsparing labour on the part of the Superintendent, to give a completeness to the experiment of Colonial Observatories corresponding to its original conception, though this portion of the duty might well have fallen into abler hands. One great advantage in the task has undoubtedly been enjoyed; viz. the union of the detailed knowledge above alluded to with the opportunity of generalisation, and consequent insight, afforded by results admitting of strict comparison and combination, obtained from well-selected stations at such distant points of the globe, and by a uniform system of observation.

It may be useful on the present occasion, that we should recall to more distinct recollection the views and opinions entertained by those who were the principal instigators of the proceedings by which the Royal Society became the responsible advisers,—and Her Majesty's Government the chief supporters,—of measures which have placed this country in the very conspicuous position of taking that lead in the advancement of certain branches of science which other nations were willing and desirous that she should take. These views cannot be better stated than in the words of one to whom all will be willing to concede pre-eminence, as well in counselling the recommendation to Government, as in conducting the several matters connected with it to a successful issue (Herschel, in Quar. Rev., No. CXXXI.):—" Great physical "theories, with their trains of practical consequences, are pre-eminently national " objects, whether for glory or utility. In effect, such they ought to be considered " by every nation calling itself civilized; and if we look to consequences, we have " only to point to the history of science in all its branches to show, that every great " accession to theoretical knowledge has uniformly been followed by a new practice, " and by the abandonment of ancient methods as comparatively inefficient and " uneconomical. This consideration alone we think sufficient to justify, even on

" utilitarian grounds, a large and liberal devotion of the public means to setting on foot " undertakings and maintaining establishments in which the investigation of physical " laws and the determination of exact data should be the avowed and primary object, " and practical application the secondary, incidental, and collateral one. That the "time is now fully arrived when other great branches of physical knowledge must be " considered as entitled to share in that public support and encouragement which has " hitherto fallen to the lot of astronomy alone, will, we think, be granted without " hesitation by all who duly consider the present state and prospects of science. The "great problems which offer themselves on all hands for solution—problems which "the wants of the age force upon us as practically interesting, and with which its "intellect feels itself competent to deal—are far more complex in their conditions, " and depend on data which to be of use must be accumulated in far greater masses, " collected over an infinitely wider field, and worked upon with a greater and more " systematised power, than has sufficed for the necessities of astronomy. The collect-" ing, arranging, and duly combining these data are operations which, to be carried " out to the extent of the requirements of modern science, lie utterly beyond the " reach of all private industry, means, or enterprise. Our demands are not merely for " a slight and casual sprinkling to refresh and invigorate an ornamental or luxurious " product, but for a copious, steady, and well-directed stream, to call forth from a " soil ready to yield it an ample, healthful, and remunerating harvest. There are " secrets of nature we would fain see revealed; resources hidden in her fertile bosom " for the well-being of man upon earth, we would fain see opened up for the use " of the generation to which we belong. But if we would be enlightened by the "one, or benefited by the other, we must lay on power, both moral and physical, " without grudging and without stint."

If at the period when it was still doubtful what the Colonial Observatories, then just established, might be able to accomplish,—and when in effect the expectations from them were little more than the anticipations of what a voyage of discovery upon an unknown ocean might produce,—the propriety of embarking upon such investigations was thus unhesitatingly affirmed, how much more confidently may the duty of perseverance be insisted upon, when the results of the first experiment have already more than realized the expectations which caused it to be undertaken. They have indeed confirmed the belief that "the gigantic problem proposed to be resolved" is of a nature to yield in its full extent only to "continued and persevering inquiry," but at the same time they may be said to have narrowed the field of inquiry, by showing more distinctly than was previously apprehended, both what is desired to be known,

and how and where it is to be sought. If the history of magnetical science is to be something more than a fragment, the researches must be persevered in.

In considering the means by which the researches thus opened out may be most advantageously prosecuted, it is natural that we should look in the first instance to the adoption, at other selected stations, of arrangements similar to those which were instituted at the stations which were chosen for a first, and, as it has proved, successful, experiment; and with this view, I may be permitted to restate the opinions which I submitted to the Magnetical and Meteorological Conference at Cambridge in 1845, as all that has since taken place has served to confirm those opinions:—

"Before I close this communication, I wish to advert to the expediency of extending the system of observation now in operation at Toronto, St. Helena, and the Cape of Good Hope, to other of the British colonies, where the same objects can be accomplished in an equally effective and economical manner.

"In cases where the institution of similar establishments is strongly urged by the Governor of a colony,—where competent persons are present and disposed to superintend the observations,—and where soldiers of the artillery are stationed, whose services may be available, and whose employment has been shown to be economical and effective in a high degree in the execution of a laborious and exact routine of observation,—there is wanting only a supply of instruments, the tempoward allotment of a building to contain them, extra pay such as the individuals at the above-named Observatories receive, and an authorised connexion with a head-quarter establishment, whence they may derive instruction and guidance.

"The cost of one of the Ordnance Observatories (including 100% a year for incidentals of all kinds) is 392% a year, exclusive of publication. It may be assumed that five years of hourly observation is a sufficient time of continuance for obtaining in any particular colony the mean values of the magnetical and meteorological elements, and their diurnal, annual, and secular variations, as well as the peculiarities of climate bearing on the health and industrial occupations of man. If the observations were printed in full detail for the five years, they would occupy two quarto volumes; but if it were thought sufficient hereafter that duplicate or triplicate manuscript copies should be deposited in different public libraries, and that publication should be confined to abstracts and an analysis, the cost of the publication would form but a small addition.

"The colonies of Ceylon, New Brunswick, Bermuda, and Newfoundland are in the described case; their respective Governors are recommending the establishment of Magnetical and Meteorological Observatories in them; competent Directors are on the spot" (this was written in 1845); "and they are all artillery stations."

To the four stations thus named may now be added Mauritius and Demerara, as from both these colonies strong and repeated applications to the same effect have been sent through their respective Governors to the Secretary of State for the Colonies. Both these colonies have offered to bear a portion of the expense of the proposed establishments, and have earnestly solicited to be placed in connexion with a head-quarter establishment, from which they might receive properly constructed instruments, with instructions and guidance in their use. Can it be said that we perform our duty as a mother country when we put such applications on the shelf?—whilst, in the interests of science, it would be difficult to estimate too highly the value of such institutions,—in forming good observers, who might subsequently extend their activity over a wider range,—in affording to travelling observers the opportunity of testing and correcting their instruments, as well as keeping up and perfecting their skill in observation,—and in contributing to arouse, to nourish, and to extend to other parts of natural knowledge that desire for the greatest possible accuracy, which was formerly met with only in astronomy and in geodetical operations of the highest class.

When it was first suggested that the officers and soldiers of the scientific corps of the army (Artillery or Engineers) stationed in the colonies might, both beneficially to themselves and advantageously to the public interests, be made available for the performance of such temporary services, the suggestion, from its novelty, might have been open to many objections. None were, indeed, made by the military authorities of the time, who, on the contrary, approved and encouraged the proposition. There may have been doubts entertained in other quarters whether persons, whose ordinary occupations were so dissimilar, would be found to possess the necessary qualifications for carrying out a scheme of exact and varied observation, in which there was no precedent to guide, and of which the performance would be sure to be extensively and closely scrutinized; but such doubts, if they existed, have probably long since subsided as the successive volumes of the Colonial Observatories have appeared; and if any should yet remain, the contents of the present volume, it is hoped, may entirely remove them.

One great and unquestionable advantage which future institutions of this nature will have over those whose duties are accomplished, will be found in the assistance they will derive from the *Physical Observatory of the British Association* at Kew, as a head-quarter Observatory, in which their instruments can be prepared and verified, the constants, &c. carefully determined, new instruments be devised as occasion may require, and be tested by experiment before they are sent out for use; and to which practical difficulties of all kinds which may present themselves to the Directors

may be referred. The omission of a provision of this kind, when the Observatories were first formed, was undoubtedly a great fault, which has been, and could only be, very imperfectly remedied by the Woolwich establishment, designed for a very different purpose, and of insufficient strength even for the duties for which it was designed.

The colonial establishments were first instituted at the instance of the Royal Society and British Association, with a more general concurrence and approval on the part of the cultivators of science in all parts of the globe than, it is believed, were ever before manifested in regard to any purely scientific undertaking; and with such a cordial and effectual co-operation of the public authorities as is well deserving of being held in remembrance. It is for those two great scientific bodies to consider whether any and what steps should now be taken to procure the continuance of the researches.

EDWARD SABINE.

Woolwich, March 1857.

ADJUSTMENTS, ABSTRACTS, AND COMMENTS.

HORIZONTAL FORCE.

Separation and Analysis of the larger Disturbances.—An important preliminary step in this investigation must be the examination in the most direct and practical manner, i.e., by means of the observations themselves, of the equivalent, in divisions of the scale of the Bifilar Magnetometer, to a change of temperature of 1° Fahrenheit.

From the latter end of 1843 to the termination of the hourly series in June 1848, we have an unbroken series of Bifilar observations particularly suitable for this examination, inasmuch as that interval comprehends the principal part of the observations which it is intended to employ in the purposed investigation. Collecting into one view the mean monthly scale readings and their corresponding temperatures from the general monthly tables of the Horizontal Force in vols. II. and III. of the Toronto Observations, we have as follows:—

TABLE I.

M	Ionth and Year.		Monthly Mean in Scale Divisions.	Temperature of the Magnet.	Quarterly Mean in Scale Divisions.	Quarterly Mean Temperature.	Seasons.
1843. 1844.	December January February March	-	514.94 525.33 519.62 512.61	43°95 37°95 43°28 46°29	} 519·96	4 1 °73	Winter Quarter (1).
	April - May -	-	498·11 500·67	56.65 60.85	503.79	54.60	Spring Quarter (2).
	June - July - August	-	506°31 507°96 516°58	$65.36 \\ 70.32 \\ 68.72$	510.28	68.13	Summer Quarter (3).
	September October November	-	529.07 552.37 565.53	65°33 53°25 46°88	} 548·99	55°15	Autumn Quarter (4).
1845.	December January February	-	577°33 576°39 580°08	42:40 42:52 42:90	} 577.93	42*61	Winter Quarter (5).
	March April - May -	- -	571 ° 22 562 ° 57 558 ° 82	47:97 53:65 59:57	} 564.20	53.73	Spring Quarter (6).
	June - July - August	-	554.14 548.70 552.80	67:38 72:45 73:37	} 551.88	71.07	Summer Quarter (7).
		_	002 00	10 01	,		(Continued on p. ii.)

Vol. III.

Table I.—continued.

						,	· · · · · · · · · · · · · · · · · · ·
M	onth and Year.		Monthly Mean in Scale Divisions.	Temperature of the Magnet.	Quarterly Mean in Scale Divisions.	Quarterly Mean Temperature.	Seasons.
1845.	September	_	570.93	63°24			
(cont.)		_	586.86	57.68	586.61	56.90	Autumn Quarter (8).
(0000)	November	_	602.05	49.79	000 01	00 50	riutumii Quarter (0).
	December	_	617.16	40.61	K	1	
1846.	January	_	611.77	44.84	614.12	42.74	Winter Quarter (9).
1010.	February	-	613.23	42.78	011 10	12 11	William Quarter (9).
	March -	_	601.03	50.25	15	j	
	April -	_	593.09	54.23	591.39	55.99	Spring Quarter (10).
	May -	-	580.05	63.18	1	00 55	Spring Quarter (10).
	June -	_	575.55	69.10	1		
	July -	-	571.16	74.19	573.11	72.51	Summer Quarter (11).
	August -	_	572.61	74.25		01	Cammor Quartor (22).
	September	-	580.78	69.97	1	}	·
	October	-	602.27	56.70	599.28	59.84	Autumn Quarter (12).
	November	-	614.80	52.86)	30 02	220202 (22)
	December	_	635.55	43.25	15		
1847.	January	-	640.48	40.17	636.43	41.93	Winter Quarter (13).
	February	_	633.26	42.37	1	11 00	
	March -	_	627.88	44.70	1		
	April -	_	616.12	51.26	616.78	52.36	Spring Quarter (14).
	May -	_	606:31	60.82		02 00	1-1-8 4-1-1-()
	June -	_	606.21	64.46	5		
	July •	-	590.43	73.64	597.24	69.72	Summer Quarter (15).
	August	_	594.77	71.07			
	September	-	602.76	62.67	1		
	October	-	615.17	56.05	612.76	56.68	Autumn Quarter (16).
	November	-	620.34	51.31	}		
	December	-	636.98	45.17)		
1848.	January	-	636.08	43.31	636.26	44.15	Winter Quarter (17).
	February	-	636.62	43.98			
	March	- 1	633.20	46.86)		
	April -	-	625.18	53.36	625.39	54.06	Spring Quarter (18).
	May -	-	617.48	61.96]		

It is obvious on the first glance that, independently of variations in the scale readings from the influence of temperature, there was a progressive increase in the scale readings (though by no means regular or even uniformly progressive) from the commencement of the series to its close. According to the mode in which the Bifilar was adjusted, an increase in the scale reading should correspond to a decrease of force either in the earth's magnetism or in the magnetism of the Bifilar Magnet. In the latter case, (that of the decrease of the magnetism of the bar,) we have no reason to expect that the decrease should be regular or uniform; viz., of equal amount in equal times. Nor in respect to secular change in the magnetism of the earth could we venture to assume, in the present state of our knowledge, that the progress of such secular change, whether it were an increase or a decrease of the force, should be uniform. If, however, we except the increase in the scale readings between the spring and summer quarters in 1844, when, from some peculiar cause, it was greater than

b 2

ordinary, the departures from a uniformly progressive increase will not appear great, particularly when we take into account the influence of magnetic disturbances, and of the regular periodical variations in the earth's horizontal force in different parts of the year, by which the different quarters may have been influenced. If, therefore, we take the mean between the scale readings, and also between the temperatures in the winter quarters of 1843-1844 and 1844-1845, Nos. (1.) and (5.), and compare these means with those of the intermediate summer quarter in 1844, No. (3.), regarding the difference in the scale divisions $\left(\frac{519 \cdot 96 + 577 \cdot 93}{2} - 510 \cdot 28 = 38 \cdot 67\right)$ as the value in scale divisions corresponding to the differences of the winter and summer temperatures $\left(\frac{41^{\circ}\cdot 73 + 42^{\circ}\cdot 61}{2} - 68^{\circ}\cdot 13 = 25^{\circ}\cdot 96\right)$ we shall have $\frac{38.67}{25.96} = 1.48$ as the scale equivalent to 1° Fahrenheit, a result subject only to inaccuracies which may be due to magnetic disturbances, or to irregularities in the decrease of magnetic force in the bar magnet, or to other causes which we are not able to particularize, which may have influenced the departures from uniformity in the progressive increase in the scale divisions during the period under consideration. In like manner, a combination of the spring and autumn quarters in 1844 with the intermediate summer quarter in the same year (Nos. (2.) and (4.) with No. (3.) will yield a second result, but of comparatively less value than the first, because the differences of temperature between the summer and the mean of the spring and autumn quarters are less than between the summer and winter quarters. The eighteen quarters will thus yield fifteen results, which are as follow:-

		TABLE II.		
		Differences of Temperature.	Differences of Scale readings.	Equivalent of 1° Fahrenheit.
(1) and (5) with (3) (2) and (4) with (3) (3) and (7) with (5) (4) and (6) with (5) (5) and (9) with (7) (6) and (8) with (7) (7) and (11) with (9) (8) and (10) with (9) (9) and (13) with (11) (10) and (12) with (11)		- 25.96 - 13.25 - 27.00 - 11.83 - 28.40 - 15.76 - 29.05 - 13.70 - 30.18 - 14.59	38 · 67 16 · 08 46 · 85 21 · 33 44 · 16 23 · 52 51 · 65 25 · 15 52 · 18 22 · 22	Sc. Div. 1 '48 1 '21 1 '73 1 '80 1 '57 1 '49 1 '78 1 '84 1 '74 1 '74
(11) and (15) with (13) (12) and (14) with (13) (13) and (17) with (15) (14) and (16) with (15) (16) and (18) with (17)		- 29·18 - 14·17 - 26·68 - 15·20 - 11·22	51.25 28.40 39.25 17.53 17.49	= 1.78 = 2.00 = 1.47 = 1.15 = 1.56
	Sums	- 306.17	495.73	= 1.62

Whence $\frac{495 \cdot 73}{306 \cdot 17} = 1.62$ is the equivalent in scale divisions to 1° of temperature.

The quarters into which the year is here divided are those usually called "Meteorological Seasons," December being classed with January and February, and August with June and July. By this division of the year the differences of temperature between the seasons compared are greater than if the more ordinary division had been adopted.

The partial results obtained by the comparison of the summer and winter quarters (which have the largest differences of temperature) exhibit a very satisfactory accord. There are seven such comparisons, and their results are as follow:—

		TABLE III.		
·		Diffe	rences.	Equivalent
		Temperature.	to 1°.	
(1) and (5) with (3) (3) and (7) with (5) (5) and (9) with (7) (7) and (11) with (9) (9) and (13) with (11) (11) and (15) with (13) (13) and (17) with (15)	-	25.96 27.00 28.40 29.05 30.18 29.13 26.63	38.67 46.85 44.16 51.65 52.18 51.25 39.25	Sc. Div. 1 '48 1 '73 1 '57 1 '78 1 '74 1 '78 1 '47
	ľ	196:35	324.01	1:65

Whence $\frac{324 \cdot 01}{196 \cdot 35} = 1 \cdot 65$, the equivalent to 1°. The value which has been adopted in reducing the observations to an uniform temperature during the period under consideration is 1.63.

According to the method prescribed in the Instructions of the Royal Society, the equivalent in scale divisions for 1° of temperature should be obtained by dividing the change corresponding to 1° of temperature found by experiment in the magnetic moment of the Bifilar Magnet, by the scale coefficient or the value of one division of the scale, both being expressed in parts of the Horizontal Force. The first of these values (viz., q, = the change in the magnetic moment of the magnet for 1° of Fahrenheit) was found, by the experiments recorded in vol. II. p. liii, to be '000234 parts of the Horizontal Force; and that of the scale coefficient k = .000087, also in parts of the force (pp. li and lii). The change in the scale-readings corresponding to 1° of temperature should have been, therefore, $\frac{q}{k} = \frac{.000234}{.000087} = 2.69$ scale divisions. This is the value which, in conformity with the instructions under which the colonial observatories have acted, has been employed in the discussion of the Bifilar observations in the preceding Toronto volumes. It is no doubt quite possible that the values of the temperature and

of the scale-coefficients, as determined by the experiments referred to, may have been, either one or both, slightly inaccurate; but it is scarcely possible to imagine inaccuracies, in either or in both, of sufficient importance to account for the difference between $2 \cdot 69$ and $1 \cdot 63$. The existence of a similar discrepancy in the case of the Makerstoun Bifilar has been shown by Mr. Broun in his very valuable discussion of the observations made at that observatory. The experiments by which the change in the magnetic moment of the bar, corresponding to variations of temperature, is determined, are made with the magnet dismounted; and it may be quite possible that the suspension may in some cases (if not in all the Bifilar Magnetometers of the description employed in the colonial observatories) exercise an influence in the changes of direction of the magnet produced by changes of temperature, which was not taken into account in the prescribed Instructions. Whatever may be the cause of the difference, however, there can, I apprehend, be no hesitation in preferring the result which is derived directly from the observations themselves.

The correct amount of this very important element in the reduction of the observations was the subject of earnest and even anxious consideration with Captain Lefroy during the latter part of his stay at Toronto, and led to an endeavour, after the hourly series had terminated, to ascertain the effect of changes of temperature on the readings of the Bifilar scale by a direct experiment with the magnet suspended precisely as when employed in the hourly observations. For this purpose the magnetometer was enclosed by boards extending from the floor to the ceiling, in a space sufficiently large to include also a copper stove. The scale was read by means of an aperture, which could be closed by a slider when not required. The account of this experiment, and its result, cannot be better related than by making the following extract from Captain Lefroy's report:—" The experiments were made by kindling a fire and keeping " up the temperature for three days, then allowing it to go out, and opening the " communication with the external air for the same length of time. There were five " cold and three hot alternations, each of three days. The readings were taken every " half-hour from 6 A.M. to 11 P.M., and at each reading the small Bifilar, which had " been in adjustment since December 1845, was also observed. It was hoped that the " small Bifilar would not show the changes of temperature of the other instrument, but " it was not found practicable to prevent the whole body of air in the room being " affected by these changes to some extent. Instead, therefore, of having a means of " correction independent of the temperature coefficient of the second instrument, we " have to reduce the small Bifilar readings to an uniform temperature by the employ-" ment of its own coefficient: but, in the first place, the value of $\frac{q}{k}$ obtained for this " instrument in the ordinary way is more likely to be practically correct than that of " the other instrument, the suspension of the one being of silk and the other of metal; " and in the second place, the value of k given by adjustment for this instrument

" ('0003551) agrees very nearly with the value found by deflection ('0003644); " lastly, if the correction $\frac{q}{L}$ employed be somewhat in error, the result will be affected " only by the difference between the actual and the assumed value, which cannot be " important upon differences not exceeding 5°, as compared with the correction for " differences averaging 61° with the other instrument. To compute the results two " abstracts are formed, one containing the half-hourly observations on the fifteen cold " days, the other those of the twelve hot days: by these we get two diurnal curves with " both instruments, which must be exactly comparable as diurnal curves, the days being The differences between the corrected mean scale reading of the small " Bifilar for the same hour of observation by the two diurnal curves is therefore the " change of Horizontal Force which we have to eliminate before comparing the corre-" sponding readings of the large Bifilar. Multiplying this difference by the ratio of the " scale coefficients of the two instruments, and applying it as a correction to the second " curve of the large Bifilar, the two curves of the latter instrument are reduced to the " same values of the Horizontal Force, and the difference of scale reading between them " is the residual effect of the change of temperature. We have then from the successive " half-hourly observations a like number of equations; omitting the three first half-" hours on each day, when it may be probable that the magnet may not have taken " up the temperature indicated by the thermometer (the bulb of which was, however, " close to it), we obtain, as the result of the whole, 1.74 as the equivalent in scale " divisions for 1° of Fahrenheit."

"The inner case of gilt wood was removed, and the outer one was slightly raised by wedges to allow the air in the box to acquire the temperature of the rest of the room. There was no reason to suppose that currents of air affected the scale readings: there was no iron whatsoever about the stove, and it was always in the same position, whether heated or otherwise."

That the result of these experiments should exhibit so close an approximation to the value (1.63) which has been found to represent the actual change produced in the readings of the scale by 1° of temperature in the whole body of the observations themselves, is a strong testimony to the care which must have been taken in conducting the experiments under the very difficult condition of regulating artificial temperatures in air heated by a stove.

The separation and analysis of the larger disturbances of the Horizontal Force has been conducted on the principle already described in discussing the larger disturbances of the Declination (Toronto Observations, vol. II. pp. xxii to xxxv). As the first step, the whole of the observations were reduced individually to an uniform temperature of 55°, employing the coefficient named in the preceding pages (1.63); the mean scale division was then computed for every hour in each of the sixty months, and the correctness of the whole work was examined by the comparison of these hourly means with the hourly

means printed in the monthly tables, the latter being reduced to the standard temperature of 55° by the application in each case of the correction due to the difference between the recorded temperature and 55°.

The hourly means thus corrected in each month presented to the eye at the different hours the diurnal variation of the Horizontal Force, cleared from the influence of temperature on the magnetism of the bar, but retaining whatever effects may have been due to disturbances. For the purpose of climinating the disturbances of largest amount, the observations which had been individually corrected for temperature were compared each with the monthly mean, at the same hour and in the same month, and every observation which differed 14.0 scale divisions or more from that mean was provisionally marked as a disturbed observation. Fresh means for each hour in each month were then taken, omitting the observations marked as disturbed, and the means thus obtained were then used as standards of comparison for a second examination. This process was repeated until the hourly means were strictly the means of all the remaining observations, after the separation of those which differed from them respectively by 14.0 scale divisions or more.

The value of 14 scale divisions in parts of the Horizontal Force at Toronto was about '0012. When the larger disturbances are thus separated, the diurnal variation at the same period of the year, in different years, exhibits a very satisfactory accordance; and, by the process of elimination which has been explained, it is probable that the diurnal variation has very little, if any, influence on the determination of the observations separated as disturbed.

A much greater practical difficulty has been occasioned by a circumstance already noticed in discussing the temperature-coefficient, namely, the progressive increase in the scale readings, partly from secular change and partly also from instrumental causes. Whenever the amount of increase in the course of a month was seen to be such as to interfere with the proper comparability of the observations in the carlier or later portions of the month with the means taken in the usual manner, fresh means, more suitable for the comparison, have been formed; thus, for example, for comparison with the observations in the last week of one month and the first week of the next, it has in some instances appeared preferable to form the hourly means from the whole of the observations of the two months united, instead of from each month separately, whereby the advantage is gained, that the period which furnishes the standard of comparison for the fortnight in question extends to a nearly equal distance on either side of the observations compared with it. In a few instances in which the increase was more irregular than was commonly the case, fortnightly means, and even, when absolutely required, weekly means, have been substituted for the monthly or two-monthly means. This part of the process requires in the person who conducts it an attentive preliminary consideration and study of the observations, and it is important that it should be carefully executed, because normal values, correctly obtained, form an essential basis for the study of all the terrestrial magnetic variations. To facilitate researches of this nature in which the observations contained in these volumes may hereafter be employed, as well as to show the steps by which the conclusions now submitted have been arrived at, a table of the hourly means of the readings of the Horizontal Force Magnetometer reduced to 55° Fahrenheit, and omitting the observations in which the amount of disturbance equalled or exceeded 14 scale divisions (or '0012 parts of the whole Horizontal Force,) is subjoined at the close of this discussion (pp. xviii to xxi), specifying in each case the interval to which the normal values correspond, as well as the interval comprehended by the observations from which they have been derived.

The period which the hourly observations included in this investigation comprise is one of five complete years, terminating on the 30th June 1848. It is not, however, an absolutely unbroken period, as in October 1843 the magnet of the Vertical Force Magnetometer was displaced from its mounting, and employed in experiments designed to show the change in its magnetic moment occasioned by changes of temperature. It was remounted in February 1844; consequently the five months from October 1843 to February 1844 that would have made a continuous suite during the five years are deficient. These have been replaced (in the similar investigation to the present, in which the observations of the Vertical Force Magnetometer have been employed) by the observations of the same months of the preceding year, viz., October 1842 to February 1843. And as it is desirable that the five years submitted to this investigation should consist of identical months in the Horizontal and in the Vertical Force, the observations of the Horizontal Force during the months from October 1843 to February 1844 have been replaced by those of October 1842 to February 1843. It will be understood, therefore, that whenever in the subjoined pages the year ending June 30th 1844 is spoken of in reference to the Horizontal and Vertical Forces, (and to their theoretical equivalents, the Inclination and Total Force,) the months which constitute that year consist of July to September 1843 inclusive, October 1842 to February 1843 inclusive, and March 1844 to June 1844 inclusive.

The course that has been followed in working out the several parts of the process by which the larger disturbances of the Horizontal Force have been separated from the other observations, and the laws of their periodical variations shown, has been as follows:—The hourly observations of the Bifilar Magnetometer during the five years terminating June 30, 1848, were received at Woolwich from Toronto precisely in the state in which they appear in the 2d and 3d Toronto volumes; namely, the readings, uncorrected for temperature, at every hour of Göttingen time, arranged in monthly tables, accompanied by corresponding tables of the temperature of the Bifilar Magnet, shown by a thermometer of which the ball was enclosed in the same case with the magnet, and which was read contemporaneously with the Bifilar scale. The monthly tables of the scale readings and of the temperature were summed before their transmission to Woolwich, both in Vertical and Horizontal columns, and means

taken of all the days in the month at the different hours, and of all the hours of the day on the different days, forming "hourly means" and "daily means." In this state the Observations were received at Woolwich and printed; they were, in fact, printed from the original manuscripts.

The first step taken at the Woolwich office was to rewrite the whole of the observations of the five years in scale divisions, corresponding to the respective readings, but reduced to an uniform temperature of 55°, taken as a convenient approximate mean temperature; for this purpose each of the observations had to receive a correction proportioned to the difference between the recorded contemporaneous reading of the thermometer and the standard temperature of 55°, and computed by a coefficient representing the change in the scale reading produced by an alteration of 1° of the thermometer. The mode and process of deriving this coefficient from the observations themselves has been stated in pp. i to vi of this volume. The formation of the monthly tables of the "Scale Readings reduced to an uniform temperature of 55°" from the tables "uncorrected for temperature" was performed, under the superintendence of Mr. Magrath, the principal clerk in this office, by two con-commissioned officers, each working independently of the other, and having the correctness of the work proved by the accordance of the two independent computers; the daily and hourly means were then taken in the same manner by two independent computers, and were additionally checked by comparison with the daily and hourly uncorrected means calculated at Toronto, when these means were also reduced to the standard temperature of 55° [excepting in a very few instances in which the observations on days of excessive disturbance had been omitted in the sums and means of the uncorrected readings computed at Toronto, but were restored in the sums and means of the corrected tables. The new tables thus formed, of the scale readings reduced to 55°, then passed into my hands; and having satisfied myself by a careful examination that a difference of 14 scale divisions above or below what might be taken as a normal value, (viz., the mean value at the same hour during the same month, or for several preceding and several succeeding days,) would constitute a convenient minimum limit for the disturbances of largest amount—being on the one hand a greater departure from the normal value than could reasonably be ascribed to any other cause than that of a disturbance in the earth's magnetism, whilst on the other hand the number of disturbances that would be thereby separated would form a sufficient body to permit their periodical laws (if such existed) to be investigated—I proceeded to mark provisionally with a pencil every observation which differed 14 scale divisions or more from its normal. I then recomputed the normals omitting the observations provisionally marked as disturbed, and compared afresh all the observations, including the provisionally marked ones, with the new normals, altering the markings where required, and continuing this process until the normal in every case included every observation which differed less than 14 scale divisions from itself, and excluded every observation which differed 14 scale divisions or more from itself; the latter were then marked finally with a surrounding ring in ink. In this state the tables were returned to the office, and the correctness of the markings, and of the normals excluding the larger disturbances, was examined by a separate computer.

A table was then formed by two computers working separately, and their work compared, of the marked disturbances during the five years, arranged chronologically, showing the day, the hour, and the amount of disturbance (i.e. the difference from the normal) in scale divisions; and on the receipt of this table from the office I proceeded to distribute the disturbances according to the years, months, and hours of their occurrence, separating them into disturbances increasing and disturbances decreasing the force, and forming the tables contained in the following analysis; the correctness of the distribution and of the calculations in each of the tables being in every case examined by a second person.

In the course of the process of marking the disturbances it became evident, as already remarked, that there were times, occasional but by no means frequent, when the change in the mean monthly scale reading, (i.e. the means of all the hours and all the days in the month from one month to the next,) was so considerable as to cause the regular hourly normals of the month to be inapplicable to the earlier or later portions of the month. In such cases the difficulty was met, and more suitable normals obtained for the earlier or later portions of the month, by taking the hourly means of the last fortnight of the one month and the first fortnight of the next, or by a mean of the normals of the two months combined; or in a very few instances, in which the departure from an uniformly progressive change was greatest, by normals derived from periods of less duration than a month.

The number of the Bifilar observations in which the amount of disturbance equalled or exceeded 14.0 scale divisions in the five years was 2968, being about 1 in between 12 and 13 of the whole body of the observations.

The aggregate values of the disturbed observations of the Horizontal Force in the different years, each ending June 30, are as follow—

									Ratios.
Year ending	June 3	0, 1844	-	-	8618.7 S	c. Div.	-	-	0.49
,,	,,	1845	-	-	8032.4	3 7	_	-	0.45
,,	,,	1846	-	-	$9479^{\circ}2$,,	-	-	0.23
,,	,,	1847	-	-	19700'1	,,	-	-	1.11
"	,,	1848	-	-	$42905 \cdot 3$	"	•	-	2.42
	m . 1		**						
	Total	in the Fiv	ve Years	•	88735.7	27			
					-				

The sum of the disturbances in the five years (88735.7 sc. div.) gives an annual mean of $17747 \cdot 1$ sc. div.; and calling this annual mean = $1 \cdot 00$, we obtain the ratios which the aggregate values in the different years bear to the average annual value. We find in this table a progressive increase in the annual value of the disturbed observations from the years ending in June 1844 and June 1845 to the year ending June 1848. The aggregate value in the year ending June 1844 exceeds by a small amount that of the year ending June 1845; but it will be remembered that the former of these two years included five months taken from the preceding year, namely, October 1842 to February 1843 inclusive, in consequence of the Vertical Force Magnetometer having been dismounted from October 1843 to February 1844 inclusive; and as we learn from the observations of the Declination at Toronto, (Vol. II. p. xxiii) that 1843 was a year of minimum disturbance in comparison with the years which preceded and followed it, it was to be expected that the aggregate value of the disturbed observations which stand in the table as corresponding to the year ending June 1844, should be swelled by the substitution of the disturbances in five months of a preceding year. It will be seen in the sequel, that when the months actually belonging to the year ending June 1844 are employed, the aggregate values, and consequently the ratio in that year, are less than in 1845.

Table V. exhibits the aggregate values in the different years, divided into disturbances increasing the force and disturbances diminishing the force.

T_A	BLE	V
1. 4	7121717	Υ.

						Increasing.	Decreasing	
Year ending	June	1844	-		-	1963.9	6654.8	sc. div.
,,	,,	1845	-		-	1122.5	6909.9	,,
"	,,	1846	-		-	1566.8	7912.4	,,
"	,,	1847	-		-	2385.8	17314.3	,,
>>	,,	1848	-		-	5015.2	37889.8	"
Totals in	the f	ive year	:s	-	-	12054.5	76681.2	

It appears from this table that the effect of the larger disturbances was in each year to diminish the Horizontal Force considerably more than to increase it. The ratio of the value of the disturbances decreasing the force to those which increased it was, on the average of the five years, nearly as 6.4 to 1.

The next table exhibits the aggregate values of the disturbed observations, distributed into the different *months* of their occurrence. The final column expresses the

ratio which the values in the preceding column bears to the mean monthly value or average of all the months:—

TABLE VI.

Months.			Sums in the					
		1844.	1845.	1846.	1847.	1848.	Five Years.	Ratios.
July - August - September October - November - January - February - March - April - May - June -	-	Sc. Div. 1092 6 585 9 300 4 576 4 2004 6 610 2 401 2 139 6 1122 3 1223 9 456 4 105 2	Sc. Div. 190'6 788'7 1266'6 1201'8 1132'9 719'3 702'1 471'0 422'0 611'1 369'8 156'5	Sc. Div. 630°2 740°2 1211°7 575°7 235°3 546°6 598°3 429°9 895°3 1289°5 1241°8 1069°0	Sc. Div. 1218'3 1609'6 3092'7 2637'2 642'9 352'6 452'0 936'3 1741'2 3731'2 2515'7 786'1	Sc. Div. 1383°1 1876°5 6739°9 5931°9 3225°0 7174°8 2112°8 4941°7 2721°0 4187°6 2042°6 568°4	Sc. Div. 4514'8 5600'9 12611'3 10923'0 7240'7 9403'5 4266'4 6918'5 6901'8 11043'3 6626'3 2685'2	0.61 0.75 1.71 1.48 0.98 1.28 0.58 0.94 0.94 0.94 0.90 0.36
		Total in th	ne five years	-	•		88735.7	
	Mean month	ly value	<u> </u>		$\frac{38735\cdot7}{12} =$	7395 = 1	•00	

April and September are the months of maximum disturbance, and January and June of minimum disturbance. The progression from the maxima to the minima and from the minima to the maxima are continuous, with the exception of the month of December; an exception obviously caused by the occurrence of excessive disturbance December 1847. If the year ending June 1848 be omitted, the ratios in December and January of the other four years to the average monthly disturbance in those four years are, of December 0.58 to 1, and of January 0.56 to 1. On the whole, therefore, we may conclude that in the larger disturbances of the Horizontal Force, as in those of the Declination (Toronto Observations, Vol. II. p. xxvi), the greatest amount of disturbance takes place at or about the equinoxes, and the least at or about the solstices. The amount of disturbance at the equinoxes (April and September) is to that at the solstices (January and June) in the proportion of between 3 and 4 to 1.

The next table exhibits the aggregate values of the disturbed observations, distributed into the different *hours* of their occurrence.

Aggregate Values of the Disturbances, distributed into the different Hours of their Occurrence, with the Ratios of the Values at each Hour to the Mean Hourly Value or Average of all the Hours.

Toronto		In the	Sums in the	Daria -	Toronto			
Astronomical Hours.	1844.	1845.	1846.	1847.	1848.	Five Years.	Ratios.	Civil Hours.
18	335.6	201.8	200*8	8791	2263.9	3881 2	1.00	6 a.m.
19	286.3	273.2	210.8	860.6	3507.9	5138.8	1.40	7 a.m.
20	178.6	171.5	297.5	716.0	2953.7	4317.3	1.20	8 a.m.
21	334.5	317.5	463.6	728.5	2203.0	4047'1	1.09	9 a.m.
22	563.3	446.2	411*3	770.2	1515.3	3706.3	1.00	10 a.m.
23	478.0	378.8	399.9	624.8	1570.2	3451.7	0.80	11 a.m.
o	475.9	415.9	386 ·3	606.2	1393.6	3278.2	0.87	Noon.
1	394.0	275.7	470°1	413.7	1249.6	2803'1	0.76	1 p.m.
2	3951	264.7	242.3	540 ·5	1019.2	2461.8	0.66	2 p.m.
3	288.7	231.3	369.0	548.6	1015.8	2453.4	0.66	3 p.m.
4	345 . 5	141.2	327.6	522.7	929.4	2266.7	0.61	4 p.m.
5	421.6	322.6	260.4	629.0	902.1	2535.7	0.66	5 p.m.
6	367.9	187.9	326.4	517.5	774.7	2174.4	0.29	6 p.m.
7	353.7	351.0	259.3	480.5	1355.8	2800.3	0.76	7 p.m.
8	344.6	363.2	433.6	515.3	1111.1	2767.8	0.75	8 p.m.
9	459.0	366.3	504.6	1012.5	966.2	3308.9	0.80	9 p.m.
10	496.7	434.0	622.5	933.5	1324.1	3810.5	1.03	10 p.m.
11	322.3	285.1	556.9	1187.7	1851.7	4203.7	1.14	11 p.m.
12	293.8	537.0	625.3	990*5	2247.5	4694'1	1.22	Midnight.
13	366.1	544.9	544.8	1613.6	2597.8	5667.2	1.53	1 a.m.
14	399.9	458'1	464.5	1463.2	3155.7	5941.4	1.60	2 a.m.
15	248.5	390.3	532.0	1453.3	2427.5	5051.6	1.37	3 a.m.
16	212.8	311.4	317.1	938.6	2430.0	4209'9	1.14	4 a.m:
17	256.3	362.5	252.6	754.0	2139.2	3764.6	1.02	5 a.m.
Total in the five years						88735.7		
Mean hourly value - $\frac{88735\cdot7}{24}$ =					3697 = 1.00			

When we examine the ratios presented in this table we at once perceive that the occurrence of the larger disturbances of the Horizontal Force at Toronto is regulated by periodical laws. The amount of disturbance is systematically greater at all the

hours from 10 p.m. to 10 a.m. inclusive, than at any hour from 11 a.m. to 9 p.m. inclusive. The ratios are equal to or above unity from 10 p.m. to 10 a.m. inclusive, and below unity from 11 a.m. to 9 p.m. inclusive. The maximum is at 2 a.m., and the minimum intermediately between 2 and 6 p.m., during which latter hours there is but little variation in the amount. There is also a secondary maximum about 7 or 8 a.m., preceded by a secondary minimum at 5 or 6 a.m. In the year ending June 1848 (but for that year only,) the secondary maximum at 7 a.m. was greater than at 2 a.m. (the usual hour of the principal maximum,) or than at any other hour in that year; this circumstance is chiefly due to the great disturbances which occurred in December 1847.

Tables VIII. and IX. exhibit the aggregate hourly values in the different years separated into disturbances increasing the force and disturbances decreasing the force; with the ratios at each hour to the respective mean hourly values.

TABLE VIII.

Disturbances increasing the Force.

Toronto Astrono-		In the	Year ending Ju	Sums in the	Ratios.	Toronto Civil		
mical Time.	1844.	1845.	1846.	1847.	1848.	Five Years.		Time.
н. 18	Sc. Div.	Sc. Div.	Sc. Div. 55°9	Sc. Div. 17:3	Sc. Div. 103 1	Sc. Div.	0.38	н. 6 а.т.
19	15°5 45°5		55 9	16.2	54.3	191.8	0.23	7 a.m.
20	18.5	19.1	28.8	37.0	65.4	168.2	0.33	8 a.m.
21	86.6	87.5	118.3	32.6	147.5	472.5	0.94	9 a.m.
$\frac{21}{22}$	231.2	151.7	87.4	80.4	181.7	732.7	1.46	10 a.m.
23	203.9	138.7	89.8	173.9	351.5	957.5	1.90	11 a.m.
ő	185.7	159.9	104.2	125.0	345.0	920.1	1.83	Noon.
ì	158.0	99.1	123.3	74.4	331.4	786.2	1.57	1 p.m.
$ar{2}$	210.6	130.1	171.4	210.0	434.0	1156.1	2.30	2 p.m.
2 3	80.9	52.4	112.2	305.3	448.5	999.3	2.00	3 p.m.
4	189.4	17.6	227.6	292.6	530.4	1257.6	2.20	4 p.m.
5	183.9	53.2	117.8	381.9	374.2	1111.0	2.50	5 p.m.
6	72.5		82.7	150.6	131.7	437.5	0.82	6 p.m.
7	17.3	17.1	70.1	62.2	609.8	776.8	1.55	7 p.m.
8	31.4	50.2	66.2	26.5	362.8	537.4	1.07	8 p.m.
9	51.9	18.2	18.7	104.7	123.2	317.0	0.63	9 p.m.
10	92.8	55`7	J	93.7	101.0	343.2	0.68	10 p.m.
11	14.6	36.2	-	46'1	105.1	202.3	0.40	11 p.m.
12		49.2	30.6	36.3	100.5	216.3	0.43	Midnight
13				66.0	20.8	116.9	0.53	1 a.m.
14			-		17.4	17.4	0.03	2 a.m.
15	28*3			35.0	14.9	78.2	0.16	3 a.m.
16	15.3		15.0			30.3	0.06	4 a.m.
17	30.1		32.2	17.8	31.2	111.9	0.55	5 a.m.
			Total in the	e five years	-	12054.5		
			Mean hourl	y value 1	$\frac{2054}{24} =$	502.2 =	1,00	

Table IX.

Disturbances decreasing the Force.

Toronto Astrono-		In the	Year ending J	Sums in the	Paris	Toronto Civil		
mical Time.	1844.	1845.	1846.	1847.	1848.	Five Years.	Ratios.	Time.
н.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.		II.
18	320.1	201.8	144.9	861.8	2160.8	3689.4	1.12	6 a.m.
19	240.8	273.2	210.8	844.4	3453.6	5022.8	1.57	7 a.m.
20	160.4	152.4	268.7	679.0	2888:3	4148.8	1.30	8 a.m.
21	247.9	230.0	345.3	695.9	2055.5	3574.6	1.15	9 a.m
22	331.8	294.5	323.9	689.8	1333.6	2973.6	0.33	10 a.m
23	274.1	240.1	310.1	450.9	1219:0	2494.2	0.78	11 a.m.
0	290.2	270.0	267.8	481.5	1048.6	2358.1	0.74	Noon.
1	236.0	176.6	346.8	339.3	918:2	2016.9	0.63	1 p.m
2	184.5	134.6	70.9	330.2	585.2	1305.7	0.41	2 p.m
3	207.8	178.9	256.8	243.3	567:3	1454.1	0.46	3 p.m
4	156.1	123.9	100.0	230.1	399.0	1009.1	0.31	4 p.m
5	237.4	269.4	141.6	247.1	527.9	1424.7	0.45	5 p.m.
6	295.4	187.9	243.7	366.9	643.0	1736.9	0.54	6 p.m.
7	336.4	333.9	189.2	418.0	746.0	2023.5	0.63	7 p.m
8	313.2	312.7	367.4	488.8	748:3	2230.4	0.70	8 p.m
9	407.1	348.1	485.9	907.8	843.0	2991.9	0.94	9 p.m
10	403.9	378.3	622.5	839.5	1223.1	3467:3	1.09	10 p.m
11	307.7	248.6	556.9	1141.6	1746.6	4001.4	1.25	11 p.m
12	293.8	487.8	594.7	954.2	2147.3	4477.8	1.40	Midnigh
13	366.1	544.9	544.8	1547.6	2546.9	5550.3	1.73	1 a.m
14	399.9	4581	464.5	1463.2	3138.3	5924.0	1.86	2 a.m
15	220.2	390.3	532.0	1418.3	2412.6	4973.4	1.56	3 a.m
16	197.5	311.4	302.1	938.6	2430.0	4179.6	1.31	4 a.m
17	226.5	362.5	220.1	736.2	2107.7	3652.7	1.14	5 a.m
			Total in the	e five years	- -	76681*2		
			Mean hour	ly value 7	$\frac{76681}{24} =$	3195.0 = 1	1.00	· V

We perceive by these tables that both the disturbances which increase and those which decrease the force are governed in respect to their frequency and amount by periodical laws depending on the solar hours, and that the laws are different in the two cases. The disturbances which increase the force have a maximum at 4 P.M., and a minimum from 2 to 4 A.M. There are also secondary maxima at 11 A.M., at 2 P.M., and at 7 P.M.; and secondary minima at 1, 3, and 6 P.M., unless we may regard these secondary maxima and minima as accidents which would disappear on a longer continuance of the observations.

From 10 A.M. to 8. P.M. inclusive the ratios are with a single exception above unity and from 9 P.M to 9 A.M. inclusive without an exception below unity. It is in the hours

of the day, consequently, that the disturbances which increase the force have their greatest prevalence, whilst the hours of the night are comparatively tranquil. The converse law holds in regard to the disturbances which decrease the force; from 10 p.m. to 9 a.m. the ratios exceed unity at every hour, and from 10 a.m. to 9 p.m. they are uniformly less than unity. The maximum is at 2 a.m. and the minimum at 4 p.m. The continuous progression from the maximum to the minimum, and from the minimum to the maximum, undergoes an interruption of very marked character at 7 and 8 a.m., constituting a very decided secondary maximum in the disturbances which increase the force at those hours, which hours are not distinguished by any peculiarity in the disturbances of opposite character.

The table which follows (Table X., pp. xviii to xxi) shows the normal values finally adopted, the periods for which they have been employed, and the periods from which they have been derived. This table is the result of careful consideration; and is presented, not alone as one of the steps by which the conclusions arrived at in this volume have been obtained, but as a means of rendering the whole body of the Bifilar Observations in the five years more valuable for future enquiries than they would be without a table of this kind. Possessed of a table containing an approximate normal reading for every day and every hour, the inquirer has it in his power, by a simple comparison of the observations in the monthly tables, with the table of normals, to ascertain the state of the Horizontal Force relatively to its mean value on any particular day or hour to which his attention may be directed; he will have in such case only to correct the tabular scale reading in the monthly table to the standard temperature of 55°, by the aid of the coefficient 1.63 as the equivalent of 1° of Fahrenheit.

TABLE X.

Hourly Means of the Readings of the Bifilar Magnetometer, reduced to an uniform Temperature of 55° Fahrenheit; omitting disturbed Observations in which the Amount of Disturbance equalled or exceeded 14 Scale Divisions or about '0012 parts of the whole Horizontal Force at Toronto.

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Table X.

Hourly Means of the Readings of the Bifilar Magnetometer, reduced to an uniform Temperature of exceeded 14 Scale Divisions, or about .0012 parts

Periods					G	ÖTTING	EN HOU	RS.				
to which the	0	1	2	3	4	5	6	7	8	9	10	11
Hourly Means			····································	<u> </u>	3	ORONTO	Hours	3.				
correspond.	18	19	20	21	22	23	0	1	2	3	4	5
1842 :	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
Oct. 1 to 31 -	449'3	446.6	442.8	434.2	429.6	429.3	431.0	435.5	441.7	444.6	446.6	447.2
Nov. 1 to 26 -	457.7	457.2	451.4	445.7	4381	437.7	440.8	444'5	450.4	455.8	456.2	458.4
Nov. 27 to 30 -	462.6	462.1	459.0	454.5	447.6	445'2	447.0	450.4	455.6	460.5	462.6	463.7
Dec. 1 to 31 -	467.6	467.0	466.6	463.4	457.1	452.8	453'1	456.3	460.9	465.3	469.0	469.0
1843:												1
Jan. 1 to 31 -	465.8	466.5	466.2	461.8	456.1	449.2	447.0	451.7	454.6	462.0	466.7	465.2
Feb. 1 to 9 -	469.3	469.9	466.6	464.1	460.1	457.4	457.9	462.1	464.5	470.2	475.5	473.5
July 2 to 15 -	904.6	903.8	902.6	909.0	899.7	899.8	905.6	907.3	912.2	915.2	919.0	916.8
July 16 to 29 -	928'1	927.0	927.8	925.4	922.3	925.4	930.2	934.4	938.2	943.3	940.0	939.3
July 30 to Aug. 12	949.9	948.2	942.1	938.1	940.2	944.6	947.2	953.7	957.1	960.8	960.1	962.5
Aug. 13 to 26 -	967.5	964.2	962.8	960.0	957.6	963.3	966.6	971.2	978.7	981.6	979.6	979.4
Aug. 27 to Sept.16	987.1	986.2	980.8	$975 \cdot 2$	976.5	979.5	980.9	990.7	995.7	999.1	995.4	992.9
Sept. 17 to 20 -	998.9	997.6	992.1	986.8	986.4	987.3	990.5	997.5	1002.2	1006.3	1006.5	1004.1
Sept. 21 to 30 -	1010.6	1008.6	1003.4	998.3	996.2	995.1	999'4	1004.3	1008.7	1013.2	1016.9	1015.2
Oct. 2 to 31 -	490.6	489.7	487.3	483.7	481.3	480.1	482.8	484.8	488.3	490.4	492.2	492.2
Nov. 1 to 30 -	496.8	495 6	492.9	489.5	488.7	488.9	489.1	490.8	493.8	496.3	497.6	498.4
Dec. 1 to 31 -	500.9	500.9	499.7	499.2	495.7	491.5	490.1	491.1	494.4	497.2	500.0	499.7
1844:						'						l
Jan. 1 to 31 -	499.8	500.2	498.6	496.9	494.3	492.0	491.5	494.4	496.6	499.3	502.0	501.9
Feb. 9 to 29 -	503.2	502.7	500.7	499.5	499.7	499.4	500.3	501.7	504.1	506.4	506.7	505.9
March 1 to 31 -	504.2	501.2	498.0	496.9	494.2	492.1	491.6	494.0	498.8	504.4	504.2	504.1
April 1 to 30 -	503.1	503.7	501.2	497.6	494.8	495.6	494.5	499.3	505.0	508.2	508.0	518.8
May 1 to 11 -	506.7	506.7	504.2	500.0	497.6	498.6	500.3	505.4	510.3	513.6	513.6	514.5
May 12 to 25 -	510.3	509.6	507.1	502.2	500.4	501.6	506.1	511.2	515.6	518.6	519.2	518.1
May 26 to June 8	515.8	515.2	513.0	509.6	508.2	509.9	513.6	518.3	523.7	524.8	525.0	524.5
June 9 to 22 -	521.3	520.8	518.8	516.6	515.9	518.2	521.2	525.0	529.7	531.0	530.9	531.0
June 23 to July 6	527.4	527.3	523.9	520.3	517.3	520.3	525.2	529.3	534.5	536.6	537.1	536.2
July 7 to 27 -	533.5	533.8	528.9	523.9	518.8	522.4	529.1	533.6	538.7	542.3	543.3	541.4
July 28 to Aug. 3	537.2	536.0	531.3	525.4	521.2	524.8	530.9	536.5	541.5	546.4	546.4	544.5
Aug. 4 to 24 -	540.9	5 38 .3	533.6	526.9	523.6	527.2	532.7	539.4	544.3	550.5	549.6	547.5
Aug. 25 to Sept. 7	545.1	542.5	537.4	531.4	528.3	531.5	537.0	544.0	549'3	552.8	553.1	551'4
Sept. 8 to 28 -	549.3	546.7	541.2	535.8	532.9	535.7	541.4	548.6	554.3	5551	556.6	555.3
Sept. 29 to Oct. 5	551.7	549.6	544.6	539'4	536.2	538.4	542.8	548.4	553.6	555.3	556.8	556.7
Oct. 6 to 26 -	554.1	552.4	548.0	543.0	539.5	541.0	544.2	548'1	553.9	555.5	557.1	558.0
Oct. 27 to Nov. 2	555.5	554'3	551.0	547.0	544.0	543.5	546.0	549.0	554.4	556.6	557.6	558.2
Nov. 3 to 30 -	556.9	557.2	554.0	551.0	548.5	545.9	547.7	550.0	554.9	557.7	558.2	558.3
Dec. 1 to 31 -	561.4	560.4	560.2	559.1	556'4	550.7	552.4	555.1	556'7	559.9	563.0	561.8
1845 :				1				1]			
Jan. 1 to 31.	560.3	560.4	556.9	551.3	546.0	546.9	548.4	552.3	555.2	557.8	560.2	560.1
Feb. 1 to 28 •	564.1	563.9	560.6	558.2	555.8	553.9	554.3	556.4	560.6	565.1	564.8	565.7
March 1 to 31 -	564.2	562.1	558.8	554.9	551.4	548.6	550.7	554.7	558.9	563.8	565.9	566.8
April 1 to 26	563.6	562.6	559'6	551.5	546.9	547.0	550.0	555.7	562.7	564.0	569.4	568.3
April 27 to May 10	565.1	564.2	561.1	554.6	551.6	552.2	555.6	561.0	567.1	569.3	572.9	572.2
May 11 to 24 -	566.7	566.4	562.6	557.8	556.3	557.5	561.2	566.4	571.5	574.6	576.4	576.1
May 25 to June 7	571.4	570.8	567.4	562.5	559.6	561.0	564.7	569.7	575.4	578.5	580.3	580.0

TABLE X.
55° Fahrenheit; omitting disturbed Observations in which the Amount of Disturbance equalled or of the whole Horizontal Force at Toronto.

				G	ÖTTING	EN HOU	RS.					Periods
12	13	14	15	16	17	18	19	20	21	22	23	from which the
		·			roront) HOURS	3.					Hourly Means
6	7	8	9	10	11	12	13	14	15	16	17	are derived.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	1842 :
446.6	446.6	444'3	443'9	445.2	444.9	445.5	445.4	447.0	446.1	449'4	448.7	Oct. 1 to 31.
459.1	4581	456.8	455.6	454.8	454.2	454.5	455.8	454.0	455.7	457.0	458.4	Nov. 1 to 26.
463.4	462.5	461.0	459.8	459.4	458.5	458.6	459.0	460.0	460.0	461.7	463.4	Nov. and Dec.
467.7	467'0	465.2	464.1	464.0	462.8	462.7	463.0	465.2	464.2	466'4	468.3	Dec. 1 to 31.
								ļ				1843:
464.4	463.4	462.9	461.5	461.2	461.1	461'1	461.7	462.3	463.3	464'8	465.9	Jan. 1 to 31.
471'3	465.8	465.7	466.7	466.7	465.4	467.6	467.3	466.6	466.8	469'1	468.2	Feb. 1 to 9.
916.9	914.7	910.2	911.0	909.0	907.5	905.8	906.9	906.7	906.8	904.7	902.2	July 2 to 15. July 16 to 29.
936.7	936.4	933.2	931.5	929.2	930.5	929.6	928.3	929.2	929.2	928.0	928.0 947.0	July 30 to Aug. 12.
958.8	957.6	954.6	953.6	952.6	951.4 971.1	950.8	949.9	951.8	950.2	966.7	967.1	Aug. 13 to 26.
976.4	973.9	973.6	989.0	987.7	986.8	986.2	986.9	986.2	984.6	986.2	985.2	Aug. 27 to Sept. 16.
1001.6	1000.1	997.6	997.8	997.2	997.0	997.6	998.0	997.5	996.6	998.5	998.7	Sept. 1 to 30.
1012.5	1009'4	1004.7	1006.6	1006.6	1007.2	1009.0	1009.2	1008.5	1008.2	1010.2	1011.9	Sept. 21 to 30.
490.3	490.1	489 4	488.7	487.4	486.0	485.6	488.0	487.5	487.9	489.0	489.8	Oct. 2 to 31.
497.5	496.5	494.7	494'9	493.1	492.7	493.5	492.9	494.0	493.3	494'3	495.8	Nov. 1 to 30.
499.8	498.0	497.7	497.5	496.5	496.3	496.6	497.4	497.6	497.8	498'9	499.6	Dec. 1 to 31.
				ł	1							1844:
500.7	500.2	500.2	498.6	497.9	497.8	497.1	497.3	497.4	498.3	499'1	499.6	Jan. 1 to 31.
505.8	505.2	504.1	504.3	502.8	502.8	502.7	500.8	500.6	501.3	502.0	503.0	Feb. 9 to 29.
503.9	503.4	502.4	502.8	501.2	500.7	500.3	500.2	500.3	500.4	501.5	502 9	March 1 to 31.
507.6	505.3	501.9	501.5	502.0	500.5	501.1	501.0	501.0	501.1	503.7	504.2	April 1 to 30.
511.1	508.3	506.7	505.9	507.1	504.9	504.9	504.8	505.3	505.4	507.0	507.4	April and May. May 1 so 31.
514.5 521.3	511.3	511.6	510.3	512°2 517°2	509.3	508.7	508.5	509.6 515.4	509'6	510.2	510.5 515.6	May and June.
528.2	518'9 526'5	518.4	523.3	52 2 ·1	521.8	522.0	522.1	521.3	520.5	519.8	520.7	June 1 to 30.
533.2	331.2	529.8	528.3	527.1	527.3	527.3	527.3	525.9	525.9	525.4	526.3	June and July.
538.8	536.4	534.4	533.4	532.1	532.9	532.7	532.2	530.2	531.2	531.1	532.0	July 1 to 31.
541.5	538.9	537.2	537.3	537.0	537.8	536.3	536.5	535.6	535'4	535.0	536.0	July and Aug.
544.2	541.4	540.0	541'1	541.8	542.6	539.9	540.6	540.7	539.2	538.9	540.0	Aug. 1 to 31.
549.1	547.4	544.6	545.2	545.7	545.7	544.0	544.2	544.5	543.9	543.6	544.6	Aug. and Sept.
554.0	553.4	549.2	549.3	549.6	548.7	548.2	548.3	548.4	548'6	548.4	549.2	Sept. 1 to 30.
554.3	553'8	551.2	551.5	551.2	550.6	550.2	550.7	549.1	550.8	551.3	551.5	Sept. and Oct. Oct. 1 to 31.
554.6 556.0	554.2	553.1	553.7	552.8 554.0	552.4	552.3	553°0 553°3	549.8	552.9	554.1	553°8 555°4	Oct. and Nov.
557.5	555°8 555°8	554.7 556.2	554.2	555.2	552.9	552.4	553.6	553.4	553.6	554.2	557.0	Nov. 1 to 30.
561.1	561.2	559.4	556.2	555.5	556.7	555.1	555.2	556.2	556.7	558.1	559.9	Dec. 1 to 31.
		000 F	0000	555 5								1845:
557.4	550.7	FE0.7	557.7	558.7	557.8	557*2	556.7	556.8	556.5	558.1	557.4	Jan. 1 to 31.
564.0	558.7 563.5	558.7 561.6	557.7 561.3	561.8	561.0	561.4	561.0	560.8	560.6	562.7	562.8	Feb. 1 to 28
564.0	563.7	564.7	563.7	562.4	561.4	561.9	561.3	561.0	560.9	562.5	563.1	March 1 to 31.
566.9	564.7	563.7	563.4	563.5	562.9	562.4	561.2	562.5	562.6	564.7	563.8	April 1 to 30.
$^{\scriptscriptstyle 1}$ $569\cdot_3$	567.7	565.8	564.5	564.3	564.1	563.8	562.9	563.9	563.8	565.4	564.8	April 1 to May. 31.
571.8	570.8	568.0	565.2	565.2	566 6	565.2	564 7	565.3	565.1	566.1	565.8	May 1 to 31.
576.4	574.4	572.1	570.2	570.0	570.1	568.9	568.4	568.8	568.6	569.5	570.0	May 1 to June 30.
	1					1	(1	-	(Continued on p. xx.)

TABLE X.—continued.

					G	ÖTTING	EN HOU	RS.				
Periods	О	1	2	3	4	5	6	7	8	9	10	11
to which the												
Hourly Means						TORONT	O HOURS					
correspond.	I	,										
	18	19	20	21	22	23	0	1	2	3	4	5
1045	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
1845: June 8 to 28 -	576.1	575.3	572.3	567.2	562.9	564.6	568.2	573.1	579.3	582.2	584.2	583'7
June 29 to July 5	577.3	576.6	574.2	568.8	565.3	565.9	570.0	575.0	580.5	583.8	585.0	584.2
July 6 to 26	578.5	578.0	575.9	570.4	567.8	567.3	571.9	577.0	581.2	585.1	585.8	584.8
July 27 to Aug. 2	581.4	578.6	576.3	571.6	569.3	570.3	575.2	580.1	585.3	586.5	589.5	587.5
Aug. 3 to 23 -	584.3	580.7	576.7	572.8	570.8	573.3	578.5	583.2	589.4	591.8	593.8	590.3
Aug. 24 to Sept. 6	585.9	582.7	578.3	574.6	572.2	574.6	580.3	584.9	590.6	591.8	5 93 · 2	591.0
Sept. 7 to 27 -	587.5	584.7	580.0	576.4	573.7	575.9	582.1	586.6	591.8	591.8	5 92.6	591.7
Sept. 28 to Oct. 4	589.0	588.9	585.2	582.2	580.7	581.6	586.0	588.9	592.7	594.0	594.5	593 2
Oct. 5 to 25	593.9	593.0	590.5	588.0	587.7	587.4	589.9	591.2	593.6	596.1	596.4	594
Oct. 26 to Nov. 8	596.0	595.4	591.5	588.5	586.9	586.2	588.2	590'6	593.7	595.8	596.5	595.5
Nov. 9 to 30	598.1	597.8	592.5	588.9	586.1	584.9	586.6	590.1	593.8	595.5	596.6	596.3
Dec. 1 to 31 -	596.7	597.2	597.0	593.9	591.4	589.8	587.5	589.2	591.5	596.3	598.3	598.5
1846:	1				j							
Jan. 1 to 31 -	597.7	597.9	596.7	594.4	589 1	586.5	586.9	591.7	595.9	601.1	602.5	602.0
Feb. 1 to 29 -	596.5	595.4	593.3	590.7	589.1	588.6	589.6	591.9	593.7	597.5	596.5	596.7
March 2 to 31 -	598.7	596.0	592.6	589.0	585.2	582.0	582.9	586.2	589.2	595.1	598.1	599.3
April 1 to 30 -	595°3 593°4	$\begin{vmatrix} 595.2 \\ 593.8 \end{vmatrix}$	590.7	584.7 581.7	582.4 581.8	581.8 584.5	584.7 588.1	588.0 594.0	592.6 602.4	603.3	600.9	601.3
May 1 to 31 - June 1 to 30 -	597.6	596.7	593.7	591.9	588.3	591.2	595.4	597.5	603.6	608.9	605.7	610.8
July 1 to 31 -	602.4	602.2	599.4	597.3	591.5	595.3	600.2	605.8	609.8	610.8	615.5	614.7
Aug. 1 to 31 -	605.6	604.4	597.7	592.3	593.7	594.4	602.3	610.2	615.0	618.1	618.1	616.2
Sept. 1 to 39	610.6	606.8	601.2	596.4	592.1	594.2	600.5	608.7	615.6	619.6	616.4	612.7
Oct. 1 to Nov. 1 -	613.7	610.0	605.2	600.9	598.8	597.5	600.2	604.7	608.3	611.6	614.0	613'4
Nov. 2 to 30 -	617.8	616.6	611.9	606.8	605.0	601.2	603.3	605.5	609.3	613.4	614.7	615.3
Dec. 1 to 31 -	620.6	620.1	617.1	614.8	610.7	607.0	607.0	609.8	614.8	619.4	621.2	620.6
1847:		0.0.0		27.7.0	21010	207.0						
Jan. 1 to 31 -	619.2	619.2	618.8	615 6	610.8	607.3	607.7	611.0	614.9	620.5	621.1	622.1
Feb. 1 to 28 -	615.8	613.0	609.4	608.4	607.2	606.2	606.8	611.1	614.3	615.7	617.9	616.9
March 1 to 31 -	615.6	$\begin{vmatrix} 614.1 \\ 611.7 \end{vmatrix}$	606.0	606.7	598.5	598.7 595.0	599 . 1	603.9	608.9	614.6	619.2	620°1
April 1 to 30 - May 1 to 31 -	615.3	613.8	612.6	607.1	602.6	605.6	612.0	619.5	623.5	626.0	625.8	625.4
June 1 to 30 -	623.3	622.7	619.2	615.7	610.2	611.7	616.0	624.5	632.0	635.6	636.6	632.5
July 1 to 31 -	621.9	618.5		611.1	609.0	610.2	616.4	621.2	627.3	633.6	633.2	630.4
Aug. 1 to 31 -	623.1	621.9	615.5	610.1	607.0	606.1	611.5	617.8	627.7	632.0	632.6	632.8
Sept. 3 to 30 -	621.8	618.1	613.7	604.5	599.3	600.8	606.7	612.6	621.2	628.2	631.6	630.5
Oct. 1 to 31 -	620.1	618.9	610.9	607.9	603.4	602.5	606.9	611.2	615.0	619.1	621.9	624.5
Nov. 1 to 30 -	624.1	620.6	615.4	609.6	604.7	600.7	598.9	605.1	611.8	8.919	620.4	620.8
Dec. 1 to 31 -	629.7	628.8	627.6	623.2	617.9	614.2	614.7	616.1	617.2	618.3	622.9	624.7
1848:	20	20017	00110	00010	600.0	203.5	000:-	coo: -	611.5	000:0	000.5	002.5
Jan. 1 to 31 -	624.4	623.5	624.8	622.0	608.2	601.7	602.7	608.5	611.5	620.3	626.7	625.9
Feb. 1 to 29	628.4	626.3	625.5	621.7	617.6	611.5	607.1	609.8	617.3	620.7	625.7	629.4
March 1 to 31 -	629.9	626.8	623.6	616.0	612.6	607.5	605.5	613.5	619.3 621.5	624'3	628.6	631'7
April 1 to 30 - May 1 to 31 -	624.4	626.6	622.8	617.5	$612.1 \\ 616.2$	$609.4 \\ 617.2$	620.4	632.1	636.1	630.1	634.4	635.3
	635.7	634.7	630.7	625.8	619.8	620.6	629.0	636.4	643.0	645.0	647.3	647.0
- COURT 10 00	1 000	004 /	000 1	10-00	013 0	0200	023 0	000 r	010 0	010	0110	011

Table X.—continued.

-					G	ÖTTINGI	EN HOUI	RS.					
	12	13	14	15	16	17	18	19	20	21	22	23	Periods from which the
					ŗ	roront) HOURS	3.	,		<u>.</u>		Hourly Means are derived.
	6	7	8	9	10	11	12	13	14	15	16	17	are derived.
	\$c. Div. 581.0 582.0 582.9 586.1 589.3 589.8 590.2 591.6 593.0 594.7 596.8 600.5 600.6 600.6 600.6 600.6 600.6 600.6 601.2 601.3 601.5 621.8 617.1 617.2 617.2 617.2 617.2 617.3 631.1 629.0 631.5	5c. Div. 577 '9 579 '5 581 '1 583 '6 586 '1 586 '4 586 '7 589 '4 592 '1 594 '6 597 '1 595 '9 598 '0 596 '5 599 '7 597 '2 598 '6 606 '6 607 '5 604 '3 612 '0 613 '2 614 '3 619 '0 619 '2 617 '6 617 '0 613 '2 617 '8 626 '3 625 '1 627 '4 627 '8	se. Div. 576:3 577:9 579:5 582:5 585:4 586:0 586:7 589:3 591:9 594:5 597:7 596:2 598:5 596:5 596:5 596:5 600:8 600:9 604:1 612:7 611:4 613:2 619:1 619:2 616:4 616:9 623:1 625:2 626:7	sc. Div. 575:3 577:0 578:7 582:3 585:9 586:7 589:1 590:7 593:2 595:6 595:5 596:8 595:6 597:5 595:3 593:2 597:0 603:2 605:0 614:5 612:3 614:4 619:4 618:3 617:6 6611:4 618:2 621:1 623:2 625:7	\$c. Div. 574.6 575.6 576.7 581.2 585.7 587.0 588.2 590.3 592.4 594.2 596.0 596.9 594.8 598.1 593.9 598.6 602.4 602.1 612.2 610.9 613.8 619.7 617.9 616.4 614.8 610.5 617.0 622.1 621.8 625.2	sc. Div. 573 · 7 575 · 0 576 · 4 580 · 8 585 · 1 586 · 8 588 · 4 589 · 6 591 · 0 592 · 3 593 · 7 594 · 8 596 · 0 597 · 8 602 · 8 611 · 7 608 · 8 612 · 9 618 · 0 617 · 3 615 · 4 614 · 7 611 · 6 617 · 3 621 · 1 622 · 6 626 · 1 623 · 9	sc. Div. 572.6 575.8 576.9 580.3 583.7 585.2 586.8 588.7 590.7 592.5 594.3 594.1 594.9 594.6 596.5 593.4 593.2 596.0 599.3 606.5 612.0 608.3 612.3 616.6 617.1 615.6 615.7 613.4 615.7 613.4 615.6 620.3 625.5 622.3	sc. Div. 572·2 574·6 577·1 580·5 583·9 585·0 586·1 589·5 593·2 593·6 594·6 596·5 593·9 601·5 605·9 614·1 617·8 617·9 615·2 612·8 613·1 616·4 619·0 621·0 621·0 624·2 621·2	sc. Div. 572·4 575·1 577·9 580·8 583·6 585·3 586·9 589·8 593·4 594·0 594·6 595·6 595·0 597·2 593·5 594·0 614·6 618·6 618·0 614·9 612·3 610·7 614·4 620·8 619·8 622·6	sc. Div. 572 1 574 5 577 0 580 5 583 9 585 5 587 1 589 6 592 1 593 8 595 5 594 6 596 3 595 3 597 2 596 0 600 1 605 9 606 2 612 2 614 7 618 1 618 7 616 1 613 1 611 8 614 2 620 7 619 8 623 5 622 8	se. Div. 573.0 575.1 577.3 579.7 582.1 584.8 587.5 590.7 595.1 596.7 595.1 596.8 600.1 604.6 612.2 612.8 615.4 618.7 619.8 616.1 613.8 613.2 614.2 620.8 619.3 623.9 625.2	sc. Div. 574 '2 576 ' 0 577 ' 9 581 ' 0 584 ' 2 586 '2 588 '2 591 ' 5 594 ' 7 595 ' 7 595 ' 7 595 ' 1 596 ' 9 594 ' 4 597 ' 9 594 ' 4 597 ' 9 595 ' 8 593 ' 7 595 ' 1 600 ' 0 605 ' 4 612 ' 7 613 ' 4 617 ' 0 619 ' 3 618 ' 1 617 ' 0 614 ' 0 614 ' 2 614 ' 4 621 ' 4 621 ' 4 621 ' 4 621 ' 4 621 ' 4 621 ' 4 621 ' 4 621 ' 4 622 ' 4 624 ' 4	1845: June 1 to 30. June 1 to July 31. July 1 to 31. July 1 to Aug. 31. Aug. 1 to Sept. 30. Sept. 1 to 30. Sept. 1 to Oct. 31. Oct. 1 to Nov. 30. Nov. 1 to 30. Dec. 1 to 31. 1846: Jan. 1 to 31. Feb. 1 to 29. March 1 to 31. April 1 to 30. July 1 to 31. Aug. 1 to 31. Sept. 1 to 30. July 1 to 31. Sept. 1 to 30. Dec. 1 to 31. Aug. 1 to 31. Sept. 1 to 30. Dec. 1 to 31. Nov. 1 to 30. Dec. 1 to 31. Aug. 1 to 31. April 1 to 30. Dec. 1 to 31. June 1 to 30. Dec. 1 to 31. April 1 to 30. July 1 to 31. April 1 to 30. May 1 to 31. April 1 to 30. May 1 to 31. April 1 to 30. July 1 to 31. Aug. 1 to 31. Sept. 3 to 30.
	625 · 9 620 · 8 627 · 0	$ \begin{array}{c c} 624.4 \\ 622.1 \\ 625.7 \end{array} $	625.5 621.9 621.0 624.8	623.8 620.9 620.9 626.5	624.9 621.0 621.7 625.3	$\begin{bmatrix} 620.7 \\ 620.2 \\ 625.3 \end{bmatrix}$	619.9 620.1 624.2	619.5 619.9 624.8	620.8 622.6 625.4	620 · 9 621 · 4 626 · 0	620.9 622.7 626.6	621.5 623.2 626.6	Oct. 1 to 31. Nov. 1 to 30. Dec. 1 to 31.
	624.6 628.6 630.4 633.8 640.1 642.7	621'9 628'9 628'8 630'5 634'6 639'4	621.6 628.2 627.3 628.9 633.2 637.8	621'9 628'4 625'1 628'0 633'4 637'4	622.7 627.0 625.9 627.1 631.9 634.1	621.0 625.3 626.2 626.6 631.7 632.1	619.5 624.7 626.0 627.2 631.8 633.4	621.6 623.2 625.7 628.6 630.1 632.0	619'8 626'0 627'8 627'2 630'6 632'8	621.6 626.5 627.4 629.1 629.8 631.5	622 · 2 626 · 9 626 · 8 627 · 6 628 · 6 632 · 8	623°0 628°4 627°9 629°1 630°0 632°6	1848: Jan. 1 to 31. Feb. 1 to 29. March 1 to 31. April 1 to 30. May 1 to 31. June 1 to 30.

VERTICAL FORCE.

Separation and Analysis of the larger Disturbances.—In preparing the observations of the Vertical Force Magnetometer for the various deductions that can be made from them, the first step must be to ascertain in the most direct and practical manner, from the observations themselves, the equivalent in divisions of the Magnetometer scale to a variation of 1° of temperature. Commencing with February 1844, in the middle of which month the Magnetometer was adjusted, an unbroken series continued until the end of May in the following year, when a re-adjustment took place. From March 1844 to May 1845 inclusive, we have consequently an unbroken series of fifteen months, in which the mean monthly scale readings, with the corresponding temperatures, were as follows:—

TABLE XI.

		Sc. Divisions.	Temperature.	Sc. Divisions.	Temperature.	
1844.	March April May	121°8 99°0 88°0	46°5 56°5 60°5	} 102.93	° 54°5	Spring (1).
	June July August	75°1 60°2 58°5	64.8 69.7 68.3	} 64.60	67.6	Summer (2).
	September - October - November -	61'4 83'6 95'1	65°1 53°4 47°1	80.03	55*2	Autumn (3).
1845.	February	101°1 99°5 93°3 82°9	42.7 42.7 42.9 48.0	97.97	42.77	Winter (4).
	April May	72·1 58·6	53.6 59.4	} 71.20	53.67	Spring (5).

From the difference in the mean scale reading in the spring quarters of 1844 and 1845 (102.93 - 71.20 = 31.73) in which quarters the temperatures were nearly the same, we may infer that a considerable change took place in the scale readings during this interval from other causes than changes in the earth's magnetism; variations depending on particular periods of the year can have no place, since the seasons compared are the same, and any secular change which could be reasonably imagined must have been far less considerable. We must, therefore, attribute this decrease of 31.73 scale divisions occurring in one year principally, if not wholly, to instrumental causes.

On a comparison of the *monthly* scale readings each with the others we further find reason to believe that the decrease thus occasioned was progressive during the whole interval, though not always to an uniform amount. Under these circumstances, perhaps the best mode of combining these five quarterly results with the view of

eliminating periodical and secular variations, and, as far as may be, instrumental error, and of thereby obtaining the effect of temperature, is to mean the results in the spring and autumn of 1844 (Nos. 1 and 3), and compare their mean with the intermediate summer (No. 2); and in like manner to mean the results of the autumn of 1844 and spring of 1845 (Nos. 3 and 5), and compare their mean with the intermediate winter (No. 4); and then to take a mean of the results of these two comparisons: these are stated in the following table:

TABLE XII.

	-	Difference of Temperature.	Difference of Scale Readings.	Equivalent to a Variation of 1° Fah [*] .
From (1) and (3) compared with (2) we have	-	12°75	26°85	2·10
From (3) and (5) compared with (4) we have		11°65	22°40	1·92

If we could regard these comparisons as sufficient of themselves to give a final result, we should only have to take the mean between them, 2.01, in which we might consider that any subsisting periodical and secular variations were eliminated. But the shortness of the period during which the series was unbroken, together with the magnitude and irregularity of the change from instrumental causes, will not permit us to rest in this as a final result, and we are led to seek for further evidence.

In examining the monthly tables in which the Vertical Force Observations from March 1844 to May 1845 inclusive are contained (Toronto Observations, vol. 2, pp. 224-243, 404-413), we find several instances in which the temperature of days very near to each other differed very considerably, and when consequently the effect of a change of temperature on the indications of the magnetometer can be examined with advantage. In choosing amongst these, it is obvious that the shorter the interval between the observations compared, the less the result is likely to be affected by the instrumental change which has been adverted to; and those instances are to be preferred in which a high temperature may be found between two nearly equidistant low temperatures, or a low temperature between two nearly equidistant high ones; provided that the condition of proximity be tolerably preserved, and that care be taken to avoid times of considerable magnetic disturbance. The following table presents a selection of instances made on these principles, with the results which they give individually and collectively:—

TABLE XIII.

					,	,	· · · · · · · · · · · · · · · · · · ·	
	Дат	Trs.		Mean	Mean	Differe	nces.	Equivalent to a
	17111	201		Temperature.	Scale Readings.	Temperature.	Readings.	Variation of 1° Faht.
1844.	March	12 and 13 18 and 19 25 and 26		50.77 39.46 49.50	Sc. Div. 116°13 133°64 115°72	} 10.67	Sc. Div. 17°72	Sc. Div. 1 '66
1844.	May June	20 to 22 27 to 28 10 and 11	-	56.63 66.55 58.80	94.47 95.58 87.75	8.84	15.23	1.79
1844.	September	16 to 20 23 to 27	-	71.47 55.95	48 · 92 77 · 94	} 15.2	29.02	1.87
1844.	October	21 and 22 24 and 25 28 to 31	-	50.80 57.21 45.05	87°33 76°00 98°16	9.29	16.74	1.80
1844.	October November	28 to 31 4 to 8 25 to 28	-	45.05 50.69 39.25	98.16 89.48 108.83	8.24	14.02	1.64
1844.	November December		-	39·25 46·30 38·52	108.83 95.74 108.00	} 7.41	12.68	1.70
1845.	January February	23 to 25 1 to 7	-	47 · 29 34 · 44	89 · 91 109 · 50	14.39	25.09	1.74
1845.	March	21 to 26 11 to 13 17 to 19		50°37 48°54 41°38	78.92 80.36 95.03	9.50	17.68	1.86
1845.	May	26 to 28 7 and 8 12 and 13 15 and 16		53°22 54°10 68°67 56°70	74°34 69°53 40°93 63°42	} 13·27	25*55	1.83
				Colle	ectively -	97.43	174.03	1.78

From this table we have 1.78 as the equivalent in scale divisions to a variation of 1° temperature: or if we combine this with the result previously obtained from the five quarterly means (page xxiii), we have $\frac{174.03 + 49.25}{97.43 + 24.38} = \frac{223.28}{121.81} = 1.83$ sc. divisions, as the equivalent of 1°. The value adopted for the portion of the observations from March 1844 to May 1845 inclusive has been 1.80.

From June 1845 to August 1845 inclusive, and from September 1845 to March 1846, the Vertical Force Observations form two series, the break between them occurring at the end of August; each series is therefore of only a few months' duration. At the end of March 1846, the magnet was removed from the Magnetometer, remagnetised, and mounted afresh. The time of Horizontal Vibration, which had been previously 11^s·50, was reduced by the stronger magnetic charge imparted to the needle to 10^s·29 observed on 1st of April 1846; which was only increased to 10^s·36 when again observed on February 28th, 1849. The series of observations which was commenced in April 1846 continued without interruption to the close of the hourly observations in

June 1848, forming an unbroken series of twenty-seven months; and for this period it will be necessary to examine afresh the equivalent in scale divisions to a change of 1° of temperature, inasmuch as the equivalent must be expected to be slightly modified by the increased magnetism of the needle.

The mean monthly scale readings, with the corresponding temperatures, are as follow, and are collected in quarterly values:—

TABLE XIV.

	T		a i b i		Quarter	ly Means.	C
	Dates.		Scale Readings.	Temperature.	Readings.	Temperature.	Seasons.
1846.	April -	_	214.0	54·7)		
	May -	-	198.3	62.8	7 199.3	62.0	Spring (1).
	June -	-	185.7	68.6	J	1	
	July -	-	173.7	73.6			
	August	-	170.8	73.7	73.2	72.3	Summer (2).
	September	-	175.9	69.5)		
	October	-	197.1	56.6)		
	${f November}$	-	200.6	52.8	202.6	50.8	Autumn (3).
	$\mathbf{December}$	-	210.2	43.0	J		
1847.	January	-	209.0	40°3)		
	Februar y	-	203.4	42.3	204.4	42.4	Winter (4).
	March -	-	200.7	44.6	J		
	April -	-	188.9	51.4)		
	May -	-	171.8	60.3	7 174.2	58.2	Spring (5).
	June -	-	161.9	63.9	J		
	July -	-	143.1	73.0)		G (0)
	\mathbf{A} ugust	-	145.4	70.4	149.8	68.6	Summer (6).
	September	-	160.8	62.4)		1
	October	-	172.5	56.1)		
	November	-	179.8	51.6	} 180.5	51.0	Autumn (7).
	${f D}$ ecember	-	188.3	45.2	J		
1848.	January	-	187.2	43.4)		7777 (0)
	February	-	182.5	43.9	} 182.5	44.3	Winter (8).
	March -	-	177.7	46.7	J		
	April -	-	165.9	53.3	1)		G . (0)
	May -	٠.	148.9	61.5	149.5	61.0	Spring (9).
	June -	-	133.7	68.2	J		

By comparing with each other similar seasons in different years, and thus eliminating periodical variations, whilst, at the same time, we have the temperatures approximately the same, we find that during this period, independently of changes from other causes, a progressive decrease took place in the scale readings which did not greatly differ from an uniform decrease. Without entering at present into the question of the cause of this decrease, let x = its amount taken from quarter to quarter, assumed to be uniform, and counted from the middle quarter (April, May, and June, 1847), and let y = the equivalent in scale readings for a change of temperature of 1°. Then each quarter will furnish an equation towards the values of x and y; and by least squares we find the most probable value of x to be 6·43, and of y 1·64, the coefficient of x being positive in the quarters antecedent to April, May, and June, 1847, and negative in the

subsequent quarters; and the coefficient of y positive when the temperature is above $56^{\circ} \cdot 7$ (the arithmetical mean of the temperatures of the nine quarters), and negative when it is less than $56^{\circ} \cdot 7$.

Comparing the summer and winter quarters, or the quarters in which the differences of temperature are greatest, we have as follows:—

			Differ	ences.	Equivalent of 1°.
			Scale Readings.	Temperature.	Equivalent of 1.
Summer and Winter	-{ (2) and (6) with (4) (4) and (8) with (6)	-	42.75 43.65	$2\overset{\circ}{8} \cdot 05 \\ 25 \cdot 25$	$\left. \left. \right\} \frac{86.4}{53.3} = 1.62 \right.$

Comparing also the spring and autumn quarters alternately with summer and with winter, we have as follows:—

					Differ	ences.	Forizalent of 10.
					Scale Readings.	Temperature.	Equivalent of 1°.
Spring and A	utumn wi	Winter,	(1) and (3) with ((3) and (5) with ((5) and (7) with ((7) and (9) with (4) - 6) -	27.45 16.00 27.40 17.65	15.90 12.25 13.85 11.70	$\begin{cases} 88.5 \\ 53.7 \end{cases} = 1.65$

The equivalent to 1° of temperature appears, therefore, to have been somewhat less in the period from April 1846 to June 1848 than in the period from March 1844 to May 1845; between these periods the needle had been re-magnetized, and its magnetic force increased, the times of Horizontal and Vertical vibration being slightly affected thereby (Toronto, vol. II. p. lxi). The ratio of the times of Horizontal and Vertical vibration being one of the elements upon which the change in the scale readings, corresponding to changes of temperature, depends, we should be prepared to expect that the amount of the equivalent to 1° of temperature would not be exactly the same before and after the re-magnetization, but that the equivalent would be slightly diminished in amount when the magnetic charge of the needle was increased. The two values, 1·80 and 1·64, differ from each other in the direction, and very nearly to the amount which might be expected from the change effected in the times of Horizontal and Vertical vibration. The results may be considered, therefore, as being each approximately corroborative of the other.

The value of the Scale-coefficient, k, computed according to the Instructions of the Royal Society, varied in different months between March 1844 and May 1845 from $\cdot 000060$ to $\cdot 000065$ parts of the Vertical Force, the mean being $\cdot 0000628$; and between April 1846

Thence we should and June 1848 from '000065 to '000067, the mean being '0000658. have, theoretically, the change in the magnetic moment of the needle corresponding to 1° of Fahrenheit, $.0000628 \times 1.80 = .000113$ for the first period, and .0000658× 1.64 = .000108 for the second period. There were two attempts made to obtain the change in the magnetic moment by direct experiment, one at the end of 1843 and beginning of 1844, of which the particulars are related in the Toronto Observations, vol. I. pp. liii-lvii, the result being '000112; and a second in March and April 1846, of which the particulars are given in vol. II, pp. lxii-lxiii, and of which the result was '00007. The result of the experiments in 1843 and 1844 (000112) is in remarkable accord with the deduction obtained by the present investigation, 0001105 (mean of 000113 and 000108). The partial results in the second series, viz., in March and April 1846, accord better with each other than do those of 1843–1844; but it is possible that there may have been some accidental oversight causing an error which may have pervaded the whole. The needle itself has been since transferred, by direction of Her Majesty's Government, to the provincial authorities of Canada, and remains at Toronto in what is now a provincial observatory; it has not been possible, therefore, to repeat the direct experiments on its magnetic moment at Woolwich, which would otherwise have been done. It would have been satisfactory to have *proved* by this means, what is, however, extremely probable, that in the case of the Vertical Force needle the method of determining the temperature equivalent prescribed in the Instructions, and that which has been here adopted, of deriving it from the observations themselves, lead to an identical conclusion.

The separation and analysis of the larger disturbances of the Vertical Force has been conducted on the same principle as in the case of the larger disturbances of the Horizontal Force. As the first step, the whole of the observations were reduced individually to an uniform temperature of 55°, employing the coefficients named in the preceding pages. The mean scale division was then computed for every hour in each of the sixty months; and the correctness of the whole work was examined by the correspondence of two computers, and by the agreement of these hourly means with the hourly means printed in the monthly tables, when the latter were reduced to the standard temperature of 55° by the application in each case of the correction due to the difference between the recorded temperature and 55°. The hourly means thus corrected in each month presented to the eye at the different hours the diurnal variation of the Vertical Force, cleared from the influence of temperature on the magnetism of the bar, but retaining whatever effects may have been due to disturbances. For the purpose of eliminating the disturbances of largest amount, the observations which had been individually corrected for temperature were compared each with the monthly mean, at the same temperature, hour, and month, and every observation which differed 4.0 scale divisions or more from that mean was provisionally marked as a disturbed observation.

Fresh means for each hour in each month were then taken omitting the observations marked as disturbed, and the means thus obtained were then used as standards of comparison for a second examination. This process was repeated until the "hourly means" were strictly the means of all the remaining observations, after the separation of those which differed from them respectively by four scale divisions or more. (The value of four scale divisions in parts of the Vertical Force at Toronto was '00026.)

When the larger disturbances are thus separated, the diurnal variation at the same period of the year, in different years, exhibits a very satisfactory accordance; and, by the process of elimination which has been explained, it is probable that the diurnal variation has very little, if any, influence in the determination of the observations separated as disturbed.

A much greater practical difficulty was occasioned by a circumstance already noticed in discussing the temperature coefficient; namely, the progressive decrease in the scale readings from instrumental causes, and possibly also in part from secular change. Whenever the amount of decrease in the course of a month was seen to be such as to interfere with the proper comparability of the observations in any part of the month with the means taken in the usual manner, fresh means more suitable for the comparison were formed; thus, for example, for the observations in the last week of one month, and the first week of the next, it has in some instances appeared preferable to form the hourly means for comparison from the whole of the observations of the two months united, instead of from each month separately, whereby the advantage is gained that the period which furnishes the standard of comparison for the fortnight in question extends to a nearly equal distance on either side of the observations compared with it. In a few instances in which the decrease was more irregular than was commonly the case, fortnightly means, and even, when absolutely required, weekly means, were substituted for the monthly or two-monthly means. This part of the process requires an attentive preliminary consideration and study of the observations, and it is important that it should be carefully executed, because normal values, however obtained, form an essential basis for the study of all the terrestrial magnetic variations. To facilitate researches of this nature, in which the observations contained in these volumes may hereafter be employed, as well as to show the steps by which the conclusions now submitted have been arrived at, a table of the hourly means of the readings of the Vertical Force Magnetometer reduced to 55° Fahrenheit, and omitting the observations in which the amount of disturbance equalled or exceeded four scale divisions (or '00026 parts of the whole Vertical Force at Toronto), is subjoined, (pp. xxxviii to xli) specifying in each case the interval to which the normal values correspond, as well as the interval comprehended by the observations from which they are derived.

The period which these normal values comprise is one of five complete years, terminating on the 30th June 1848. It is not, however, an absolutely unbroken period, as in October 1843 the magnet of the Vertical Force Magnetometer was displaced from

its mounting, and employed in experiments designed to show the change in its magnetic moment occasioned by changes of temperature. It was remounted in February 1844; consequently the five months from October 1843 to February 1844 that should have formed a continuous suite are deficient. These have been replaced by the observations of the same months of the year preceding, viz., October 1842 to February 1843.

It will be understood, therefore, that, throughout the discussion of the Vertical Force disturbances, whenever the year ending June 30th 1844 is named, the months which constitute it consist of July to September 1843 inclusive, October 1842 to February 1843 inclusive, and March 1844 to June 1844 inclusive.

The number of the Vertical Force observations in which the amount of disturbance equalled or exceeded 4.0 scale divisions in the five years was 5220, being about 1 in 7 of the whole number of observations.

The aggregate values of the disturbed observations of the Vertical Force in the different years, each ending June 30th, are as follow:—

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Table XV.

Year ending June 30, 1844 - - - 7008 5 Scale Divisions.

" " 1845 - - 6201 1 ",

" 1846 - - - 7839 1 ",

" 1847 - - 13055 7 ",

" 1848 - - 19161 5 ",

Total in the five years - 53265 9
```

Table XV. shows a progressive increase in the annual value of the disturbed observations from the years ending in June 1844 and 1845 to the year ending June 1848. The aggregate value in the year ending in June 1844 exceeds by a small amount that of the year ending June 1845; but it must be remembered that these two years do not admit of strict comparison with each other, because the first included five months taken from a preceding year, in consequence of the magnetometer being dismounted from October 1843 to February 1844 inclusive. If, as there is reason to believe, 1843 was a year of minimum disturbance (as was certainly the case in the Declination and Horizontal Force), it becomes probable that the amount of disturbance in the Vertical Force in the year ending June 1844 may have been swelled by this substitution of five months from the preceding year.

The sum of the disturbances in the five years (53265 · 9 scale divisions) gives an annual mean of 10653 · 2, and hence we obtain the ratios which the aggregate values in the different years bear to the average annual value, as shown in the following table:—

Table XVI. Year ending June, 1844 - - 0.65 to 1. ,,, 1845 - - - 0.58 to 1. ,,, 1846 - - 0.73 to 1. ,,, 1847 - - - 1.23 to 1. ,,, 1848 - - 1.80 to 1.

Table XVII. exhibits the aggregate values in the different years, divided into disturbances increasing the force and disturbances diminishing the force.

r	Гλ	723	T	Y	V	T

					Increasing.		Decreasing	:
Year ending	June,	1844	-	-	3174.2	-	3834.3	Scale Divisions.
,,	,,	1845	-	-	2061.2	-	4139.9	**
, ,	22	1846	-	-	3356.1	-	4483.0	**
»	"	1847	-	-	4372.9	-	8682.8	**
,,	,,	1848	-	-	9298 ·3	-	$9863^{\circ}2$,,
Sui	ns in	the five	years	-	22262.7	-	31003.2	"

It appears from this table that the average operation of the disturbances of larger amount at Toronto is to diminish the Vertical Force more than to increase it. The ratio of the disturbances diminishing the force to those which increased it, on the average of the five years, was nearly as 1 · 4 to 1.

The next table exhibits the aggregate values of the disturbed observations, distributed into the several *months* of their occurrence, with the ratios which the values in the preceding columns bear to the mean monthly value or average of all the months.

TABLE XVIII.

Trans.			In the	Year ending	June 30,		Sums in the	Ratios.	Months.
Months.		1844.	1845.	1846.	1847.	1848.	Five Years.	Ratios.	Months.
July - August - September October November December January February March - April - May - June -	-	Sc. Div. 527 '3 281 '5 536 '9 489 '9 589 '7 794 '7 384 '3 72 '8 1283 '7 1374 '4 490 '5 182 '8	sc. Div. 351'1 760'1 1115'0 1017'1 666'1 198'6 652'2 346'8 345'1 249'5 382'7 116'8	sc. Div. 562·3 808·1 625·2 463·3 524·8 659·4 301·7 266·7 374·3 1048·3 1347·2 857·8	sc. Div. 1406 '8 2075 '1 2369 '5 1125 '7 408 '3 149 '3 313 '0 508 '0 1163 '2 2034 '5 1081 '9 420 '4	sc. Div. 637·5 880·8 2434·4 2663·6 1138·2 2611·3 841·1 2093·0 1619·6 1901·7 1683·1 657·2	sc. Div. 3485 ° 0 4805 ° 6 7081 ° 0 5759 ° 6 3327 ° 1 4413 ° 3 2492 ° 3 3287 ° 3 4785 ° 9 6608 ° 4 4985 ° 4 2235 ° 0	0.71 1.08 1.60 1.29 0.75 1.00 0.56 0.74 1.08 1.49 1.12 0.50	July. August. September. October. November. January. February. March. April. May. June.
	-		Total	in the five	e years		53265.9		
AND A STATE OF THE			Mean	monthly v	aiue. —	$\frac{65.9}{12} =$	4438*8	= 1.00	

April and September are the months of maximum disturbance, and January and June the months of minimum disturbance. The progression from the maxima to the minima, and vice versā, is continuous with the exception of December, an exception manifestly caused by the occurrence of excessive disturbance in December 1847. If the year ending June 30, 1848, be omitted, the ratios of the disturbances in the months of December and January respectively, to the mean monthly disturbance in the remaining four years are, December 0.63 and January 0.58. On the whole, therefore, we may conclude, that in the disturbances of the Vertical Force, as in the Declination and Horizontal Force, the maxima occur at or about the equinoxes, and the minima at or about the solstices. The values of the disturbances at the equinoxes are to those at the solstices in the ratio of nearly 3 to 1.

Tables XIX. and XX. exhibit the aggregate monthly values in the different years, separated into disturbances increasing the force, and disturbances decreasing the force.

TABLE XIX.

Disturbances increasing the Force.

35 17			In the	Year ending J	June 30,		Sums in the	D.	36.11
Months.		1844.	1845.	1846.	1847.	1848.	Five Years.	Ratios.	Months.
		Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.		
July -	-	214.0	25.7	153.3	362.3	279.5	1034.8	0.22	July.
August	-	83.2	2 84 .3	236.1	442'0	363.1	1408.7	0.76	August.
September	-	309.2	149.1	133.1	779.5	1395.5	2766.4	1.49	September.
October	-	256.5	278.5	278.7	344.0	1151.2	2308.9	1.25	October.
November	-	245.8	250.2	63.2	137.7	828'4	1525.3	0.85	November.
$\mathbf{December}$	-	685.3	126.7	454.2	117.2	1356.1	2739.5	1.48	December.
January	-	144.9	460.4	110.3	232.5	368.3	1316.4	0.71	January.
February	-	58.1	88.0	60.2	268.8	958'1	1433.5	0.77	February.
March -	-	506.8	159°9	208.1	587.9	782.1	2244.8	1.21	March.
April -	-	95.9	109 . 9	679.2	637.6	790.1	2712.7	1.46	April.
May -	-	128.2	95.1	656'1	227.6	722.4	1829 4	0.99	May.
June -	-	46.3	33.4	323.3	235.8	303.2	942.3	0.21	June.
			Total	in the five	years		22262.7		
			Mean	monthly v	alue, $\frac{222}{12}$		1855.2 =	= 1.00	

Table XX.

Disturbances decreasing the Force.

75 .1		In the	Year ending .	June 30,		Sums in the	Ratios.	35-0-
Months.	1844.	1845.	1846.	1847.	1848.	Five Years.	Ratios.	Months.
July - August September October November December January February March - April - May - June -	Sc. Div. 313 '3 198 '3 227 '7 233 '4 343 '9 109 '4 239 '4 14 '7 776 '9 878 '5 362 '3 136 '5	sc. Div. 325*4 475*8 965*9 738*6 415*9 71*9 191*8 258*8 185*2 139*6 287*6 83*4	sc. Div. 409'0 572'0 492'1 184'6 461'6 205'2 191'4 206'2 166'2 369'1 691'1 534'5	sc. Div. 1044'5 1633'1 1590'0 781'7 270'6 32'1 80'5 239'2 575'3 1396'9 854'3 184'6	\$6. Div. \$58.0 \$17.7 \$1038.9 \$1512.4 \$309.8 \$1255.2 \$472.8 \$1134.9 \$837.5 \$1111.6 \$960.7 \$353.7	Sc. Div. 2450'2 3396'9 4314'6 3450'7 1801'8 1673'8 1175'9 1853'8 2541'1 3895'7 3156'0 1292'7	0°95 1°31 1°65 1°33 0°68 0°63 0°45 0°69 0°98 1°55 1°22 0°50	July. August. September. October. November. December. January. February. March. April. May. June.
		Total	in the five	years		31003.2		
		Mean	monthly v	alue, 3100	$\frac{03.5}{2} =$	2583.6 =	: 1.00	

It is seen by Tables XIX. and XX. that the values of the disturbances which increase the force, and of those which decrease the force, follow, in their ratios to their respective mean monthly values, the same general law as that obtained from their conjoint consideration in the remarks on Table XVIII. The equinoxes are the epochs of maxima, and the solstices of minima.

It has been seen in page xxx. that, on the average of the whole year, the disturbances which decrease the force preponderate in value over those which increase the force in the ratio of 1.4 to 1.0. This preponderance, however, appears to be subject to a periodical variation, and to have a maximum about the time of the northern solstice, and a minimum at the opposite period of the year. This variation is of considerable amount; and though the number of years (five) over which the series of observations extends is insufficient to give its progression with great regularity, it is still quite sufficient to indicate the general fact of the existence of such a variation, and to point it out as worthy of a more extensive examination. Table XXI. exhibits the ratios in the different months of the values of the disturbances decreasing the force to those which increase it, the latter being taken throughout as the units.

TABLE XXI.

Ratios of the Values of the Disturbances decreasing the Vertical Force in the different Months to the Value of those which increase it.

Months.	Ratios.	Months.	Ratios.
July	2·41 1·56 1·49	January February March April May June	0.89 1.29 1.13 1.43 1.72 1.37

In December and January the preponderance of the decreasing values ceases, and increasing values preponderate. If we combine in one view the north-solstitial months of May, June, and July, the mean ratio is 1.8 to 1.0. In the opposite part of the year (combining November, December, and January in one view,) the preponderance is reversed, the mean ratio being as 0.83 to 1.0. In the comparison of the values of the easterly and westerly disturbances of the Declination at Toronto (Toronto Observations, vol. II. p. xxvii), we have the evidence of an analogous periodical variation existing in that element. In the north-solstitial months, easterly disturbances preponderate, and in the south-solstitial months westerly predominate. In the analogy thus traced the predominance of easterly disturbances of the Declination ranges itself with the predominance of disturbances which decrease the Vertical Force, and the predominance of westerly disturbances of the Declination with that of disturbances which increase the Vertical Force.

On comparing with each other the periodical affections of the Vertical Force in the different months which have been thus brought into notice, we find that in the sums of the values of the whole disturbances (when those which decrease are combined with those which increase the force) the equinoctial months are the epochs of maximum disturbance, and the solstitial months epochs of minimum disturbance; whilst in the periodical variation of the ratios of the disturbances of opposite character to each other (viz., those which decrease and those which increase the force,) the extreme dissimilarity takes place at or near the solstitial epochs, whilst the equinoctial epochs hold a middle place. In both these respects the analogy holds in respect to the disturbances of the Declination.

Table XXII. exhibits the aggregate values of the disturbed observations, distributed into the several *hours* of their occurrence, together with the ratios of the values at the different hours to the mean hourly value or average of all the hours.

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TABLE XXII.

Toronto		In the	Year ending J	une 30,		Sums in the	Ratios.	Toronto Civil
Astronomical Time.	1844.	1845.	1846.	1847.	1848.	Five Years.	matios.	Time.
н.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	1.01	н.
18	398 .3	363.5	306.8	633.0	994.9	2696.5	1.21	6 a.m.
19	365.7	241.9	245.3	563.7	1149.8	2566.4	1.15	7 a.m.
20	273.7	188.6	262.5	455.4	598.4	1778.6	0.80	8 a.m.
21	207.8	109.3	129.7	261.4	483.4	1191.6	0.54	9 a.m.
22	183.6	57.3	111.7	131.5	329.0	813.2	0.36	10 a.m.
23	112.8	65.3	102.0	120.0	355.8	755.9	0.34	11 a.m.
0	145.1	58.2	188.1	191.3	454.6	1037.3	0.46	Noon.
1	207.7	106.6	219.4	305.6	555.1	1400.1	0.63	1 p.m.
2	213.1	159.0	260.6	342.9	720.8	1704.4	0.77	2 p.m.
3	221.1	160.6	317.2	512.1	716.3	1944.1	0.87	3 p.m.
4	290.4	200.7	439.0	510.9	884.4	2325.4	1'04	4 p.m.
5	342.4	260'4	397 .2	522.2	864.6	2387.1	1.07	5 p.m.
6	329.0	228.8	369.1	556.5	757.2	2240.6	1.01	6 p.m.
7	319.6	244.6	302.0	517.5	885.3	2339.0	1.02	7 p.m.
8	274.7	2 23 · 2	256.6	433.8	789.2	1977.5	0.89	8 p.m.
9	204.2	196.7	291.5	361.6	602.4	1656.4	0.74	9 p.m.
10	245.4	181.0	283.9	645.9	5 39.6	1895.8	0.82	10 p.m.
11	277.7	227.9	314.9	585.0	660.2	2065.7	0.93	11 p.m.
12	401.0	484'1	467.5	784.0	957.6	3094.2	1.39	Midnight.
13	366.5	469.5	486.2	1032.1	1161.9	3516.2	1.28	1 a.m.
14	373.3	520.4	537.5	961.5	1171.4	3564.1	1.61	2 a.m.
15	421.0	566.2	591.1	994.7	1273 1	3846.1	1.73	3 a.m.
16	294.8	458.4	5551	934.9	1099.6	3342.8	1.21	4 a.m.
17	439.4	428.9	403.9	697.9	1156.2	3012.6	1.41	5 a.m.
		Total	in the five y	years		53265.9		1
		Mean	hourly valu	e - <u>5</u> 8	$\frac{3265.9}{24} =$	2219.4 =	1.00	

When we examine the values presented in this table, we at once perceive that the occurrence of the larger disturbances of the Vertical Force at Toronto is governed by periodical laws depending on the hours of solar time. The aggregate value of the disturbances in the five years is a maximum at 3 p.m. and a minimum at 11 a.m.; there is also a secondary maximum at 5 p.m. and a secondary minimum at 9 p.m. There is, therefore, a double progression, and between the successive maxima and minima the progression is everywhere continuous. During the hours of the day, i. e. from 8 a.m. to 11 p.m., the ratios are less than unity, except from 4 to 7 p.m. inclusive, when the secondary maximum takes place. From midnight to 7 a.m. the ratios at every hour exceed unity.

Tables XXII. and XXIII. exhibit the aggregate values at the different hours, separated into disturbances increasing the force and disturbances decreasing the force, and the ratios of the values at each hour of both kinds of disturbance to their respective mean hourly values.

Table XXIII.

Disturbances increasing the Force.

Toronto Astronomical		In the	Year ending	June 30,		Sums in the	Ratios.	Toronto Civil
Time.	1844.	1845.	1846.	1847.	1848.	Five Years.	Tatios.	Time.
н.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.		н.
18	63.3	14.8	48.7	17.9	113'1	257.8	0.58	6 a.m.
19	74.9	4.7	47.4	21.0	148.2	296*2	0.35	7 a.m.
20	72.2	27.5	78.8	31.3	177.9	387.7	0.42	8 a.m.
21	62.6	8.8	29.5	22.6	139'9	263.5	0.29	9 a.m.
22	65.8	14.3	80.4	34.5	178.1	373.1	0.40	10 a.m.
23	67.6	29.9	52.3	77.1	262*2	489'1	0.52	11 a.m.
0	86.6	39.8	127.8	149.9	396.7	800.8	0.86	Noon.
1	162.0	80°2	141'3	265.5	495.7	1144.7	1.23	1 p.m.
2	163.6	144.6	194.2	303.6	684.9	1491.2	1.61	2 p.m.
3	203.6	151.9	275.9	469.7	691.4	1792.5	1.93	3 p.m.
4	249.5	185.7	387.6	451.8	870.6	2145.2	2.31	4 p.m.
5	290.1	260.4	350.9	450.2	841.1	2192.7	2.36	5 p.m.
6	278.0	215.7	324.8	5 18 · 6	733.2	2070.6	2.23	6 p.m.
7	333.7	221.9	251.3	471.2	857.2	2135.3	2.30	7 p.m.
8	236'4	208.4	200.2	370.2	766.2	1781.4	1.92	8 p.m.
9	146.3	122.7	238.5	223.7	521.1	1250.3	1.35	9 p.m.
10	127.3	87.5	107.7	131.2	397.1	851.1	0.92	10 p.m.
11	110.9	72.8	68.1	80.8	219.2	551.8	0.59	11 p.m.
12	87.3	55.3	74.5	42.0	216.7	475.8	0.21	Midnight.
13	64.2	31.6	45.8	45.0	139.3	326.2	0.35	1 a.m.
14	60.7	24.6	62'1	47.3	130'1	324.8	0.35	2 a.m.
15	60.3	22.7	63.7	42.1	111.1	303.9	0.33	3 a.m.
16	34.2	21.6	50.4	58.2	91.4	256.1	0.28	4 a.m.
17	72.5	13.4	51.9	47.2	115.6	300.8	0.32	5 a.m.
· · · · · · · · · · · · · · · · · · ·	<u> </u>	Total	in the five y	ears		22262.7		<u>'</u>
-		Mean	hourly value) •	$\frac{22263}{24} =$	927.6 = 1	1.00	

Table XXIV.

Disturbances decreasing the Force.

Toronto		In the	Year ending Ju	ine 30,		Sums in the	Ratios.	Toronto Civil
Astronomical Time.	1844.	1845.	1846.	1847.	1848.	Five Years.	Ttatios.	Time.
н.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.		H.
18	335.0	348.7	2581	615.1	881.8	2438.7	1.30	6 a.m.
19	290.8	237.2	197'9	542.7	1001.6	2270.2	1.76	7 a.m.
20	201.5	161.1	183.7	424'1	420.5	1390.9	1.04	8 a.m.
21	145.2	100.4	100.2	238.8	343.2	928.1	0.72	9 a.m.
22	117.8	43.0	31.3	97.0	151.3	440.4	0.34	10 a.m.
23	45.2	35.4	49.7	42.9	93.6	266.8	0.20	11 a.m.
0	58.5	18.4	60.3	41.4	57.9	236.2	0.18	Noon.
1	51.1	26.4	78.1	40°	59*4	255.4	0.19	1 p.m.
2	57.5	14.4	66.1	39.3	35.9	213.2	0.16	2 p.m.
3	34.3	8.7	41.3	42'4	24.9	151.6	0.11	3 p.m.
4	40.9	15.0	51.4	59.1	13.8	180.2	0.14	4 p.m.
5	52.3	_	46.6	72.0	23.2	194.4	0.12	5 p.m.
6	51.0	13.1	44'3	37.9	23.7	170.0	0.13	6 p.m.
7	55.9	22.7	50.7	46'3	28.1	203.7	0.12	7 p.m.
8	38 ·3	14'8	56.4	63.6	23.0	196.1	0.12	8 p.m.
9	57*9	74.0	55.0	137.9	81.3	406.1	0.31	9 p.m.
10	118'1	93.2	176.2	514.4	142.5	1044.7	0.80	10 p.m.
11	166'8	155.1	246.8	504.2	441.0	1513.9	1.17	11 p.m.
12	313.7	428'8	393.0	742.0	740.9	2618.4	2.02	Midnigh
13	302.0	437.9	440.4	987.1	1022.6	3190.0	2.47	1 a.m.
14	312.6	495.8	475.4	914.2	1041.3	3239.3	2.20	2 a.m.
15	360.7	543.5	523.4	952.6	1162.0	3542.2	2.74	3 a.m.
16	260.3	436.8	504.7	876.7	1008.2	3086.7	2.39	4 a.m.
17	366.9	415.2	352.0	650.7	1040.9	2825.7	2.19	5 a.m.
<u> </u>	<u> </u>	Total	in the five y	ears		31003.5		!
		Mean	hourly value	31	$\frac{003.5}{24} =$	1291.8 =	1.00	

When we examine the ratios presented in these tables, it is at once seen that both the disturbances which increase the force and those which decrease it are regulated by periodical laws. In the disturbances increasing the force, the values are highest from noon to 10 p.m. inclusive; they exceed the mean hourly value from 1 to 9 p.m., and exceed twice that value from 4 to 7 p.m. The hours of maximum and minimum are approximately, the maximum about 5 p.m., and the minimum about 5 a.m., though (in the latter case particularly) the precise hour is not very distinctly marked. In the disturbances decreasing the force, the values are least from 10 a.m. to 9 p.m. inclusive; they are less than the mean hourly value from 9 a m. to 10 p.m. inclusive, and greater from 11 p.m. to 8 a.m. inclusive: from midnight to 5 a.m. the values exceed at each hour twice the mean hourly value. The maximum is well marked at 3 a.m.; the minimum less distinctly marked takes place during the hours of the afternoon. When the ratios are highest in the disturbances increasing the force they are generally lowest in those decreasing the force, and vice versâ; but the periodical laws in the two cases are not strictly the converse of each other.

The account given in pp. viii to x of the operations by which the successive steps were accomplished in the investigation of which the disturbances of the Horizontal Force were the subject, applies equally to the present investigation into the periodical laws of the disturbances of the Vertical Force; and in Table XXV. will be found the successive normal values which have been employed of the Vertical Force at the standard temperature of 55° at the different hours, corresponding to Table X in the case of the Horizontal Force.

Table XXV.

Hourly Means of the Readings of the Vertical Force Magnetometer, reduced to an uniform Temperature or exceeded 4.0 Scale Divisions or .00026 parts

					G	OTTINGE	N HOUF	RS.				
Periods to which the	0	1	2	3	4	5	6	7	8	9	10	11
Hourly Means correspond.					T	CORONTO	Hours	.				
1	18	19	20	21	22	23	0	1	2	3	4	5
1842 :	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
Oct. 1 to 31 - Nov. 1 to 18 -	67.6	68.1	67.5	66.7	66.7	66.8	67.7	68.2	69.0	69.8	69.9	70.0
Nov. 1 to 18 - Nov. 19 to 30 -	64.6 57.3	64.9	65°1 57°7	64.5	63.9	64.0	64.4	65.6	59.6	66.0	66.5	66.9
Dec. 1 to 31 -	57.6	57.4	57.7	57.1	58°1 56°3	56.5	58.9 57.0	57.4	58.6	59°9 58°5	60°5 58°5	61°1 58°6
1	0.0	0. 1	0, 1	0, 1	000	00 0	", "	0, 4	00 0	000	000	000
1843: fan. 1 to 31 -	F7.0		50.0	FF.0	50.0	50.5		50.0	5010	5047	50.3	70.0
Seb. 1 to 31 -	57.9	57:5	56.9	57.0	56.6	56.5	57.5	58.0	58.0	58.1	58.1	58.3
uly 2 to 29	53°1 58°8	53°3 58°9	54.0 58.9	51.7 58.8	51.3	51.9 58.7	52.4 59.2	53.1	53.9	54.3	54.6	54.6
uly and August	57.3	56.8	56.7	56.7	56.7	57.0	57.5	58.2	59.1	61.8	62.7	63.6
lug. 1 to 31 -	55.8	54.8	54.6	54.7	54.7	55.4	55.8	56.6	57.5	58.2	58.8	61.0 58.2
lept. 1 to 9 -	51'2	50.7	50.7	50.7	20.8	21.0	51.2	52.3	53.0	53.7	54.0	53.8
Sept. 10 to 30 -	46.7	46.6	46.9	46.8	46.9	46.7	47.3	48.1	48.4	49'3	49.2	49.2
1844:						'						-0 -
Feb. 9 to 29	105.4	105.6	106.5	104.9	104.0	104.3	104.8	105.0	105.7	105.7	105.6	105.2
March 1 to 23 -	107.8	107.6	107.8	107.3	106.0	105.2	105.8	106.5	106.9	108.0	108.1	108.5
Mar. 24 to April 6	105.0	104.8	105.1	104.8	103.8	103.3	103.7	104.3	105.1	105.6	105.7	106.3
April 7 to 23 -	102.2	102.0	102.2	102.4	101.7	101.3	102.1	102.2	103.4	103.5	103.2	103.9
April 24 to May 11	100.1	100.3	100.4	99.9	99.2	98.7	99.4	99.6	100.1	100.8	101.2	102.0
May 12 to 25 -	98.3	98.6	98.3	97.4	96.7	96.3	96.9	96.7	97.8	98.7	99.8	100.1
May 26 to June 8	95.5	95.2	95.2	94.6	94.3	94'1	94.6	94.5	95.2	96.1	97.0	97.3
une 9 to 22 -	92.8	92.5	92.2	91.9	91.9	92.0	92.4	92.2	92.9	93.6	94.3	94.2
Tune 23 to 30 -	90.6	90.0	89.6	89.5	90.0	90.3	90.2	90.7	92.2	91.7	92.6	92.9
[uly 1 to 6 -]	90.8	91.4	91.0	90.0	88.9	88'4	88.6	89.5	90.8	91.8	92.2	93.6
[uly 7 to 13 •	88.7	89.1	89.0	88.8	87.9	87.9	88.1	88.2	88.9	90.1	91.2	91.1
[uly 14 to 20 -	86.2	86.2	86.6	86.4	85.7	84.2	84.4	85.0	85.6	87.0	88.9	88.8
[uly 21 to 31 -	84*4	84.1	83.4	83.0	82.8	82.9	83.2	83.0	83.6	85.1	85.4	86.2
Aug. 1 to 31 -	82.0	82.4	82.4	81.8	81.8	82.0	81.2	82.8	84.3	85.1	85.2	85.1
Sept. 1 to 30 -	80.6	80.6	79.6	79.1	79'4	80.0	80.6	81.9	82.3	82.8	82.3	82.0
Oct. 1 to 31 - Nov. 1 to 30 -	81.0	81.2	80.9	80.4	79.9	79.9	80.7	81.7	82.0	82.7	82.6	82.4
Nov. 1 to 30 - Dec. 1 to 31 -	79 · 9	80.6	81.0 77.8	79.6 77.8	79.8	80.4	80.6 78.5	81.4	81.9 79.7	82 . 4	82.8	82.7
1845 :	,,,,	'' "				""	100	13 5	13 1	30 0	80.2	80.0
an. 1 to 15 -	78.2	77.8	78.2	77.8	77.8	78.2	78.2	77.6	78.5	70.0	70.7	F0.0
an. 16 to 31 -	75.1	75.1	74.7	74.6	74.4	74.2	75.1	75.9	77.4	78 · 9	78'5	78.6
Feb. 1 to 28 -	70.9	70.7	71.0	70.8	70.2	70.0	70.8	71.6	72.8	73.1	77.5 72.9	77.5
March 1 to 31 -	70.4	70.6	70.4	69.5	68.6	68.0	68.6	69.2	70.1	70.9	71.1	73°3 71°5
April 1 to 30	69.9	69.8	68.9	68.7	68.2	68.1	68.2	69.2	70.1	70.8	70.9	
May 1 to 31 -	67.8	67.3	66.5	65.2	64.2	64.2	65.0	66.2	67.3	68.5	68.6	71.2 69.0
une 11 to 21 -	108.7	109.0	108.2	107.5	106.8	107.1	107.0	107.0	108.2	109.4	110.3	110.2
une 22 to 30 -	105.2	105.8	104.5	102.7	101.8	102.2	103.1	103.4	104.9	106.5	107.5	107.2
uly 1 to 12 🕒	103.3	102.9	102.3	102.1	101.2	101.7	101.2	102.0	102.2	104.1	106.0	107.7
uly 13 to 31 -	98.8	98.3	97.8	97.5	96.6	95.9	95.2	96.7	97.4	98.1	98.7	99.3
ug. 1 to 16 -	167.2	166.8	166.6	165.8	165.4	165.6	165.4	166.0	167.5	167.8	167.9	168.3
lug. 17 to 31 -	163.8	162.7	162.7	161.8	161.4	162.2	162.6	163.7	164.7	164.6	165.0	165.6

TABLE XXV.

of 55° Fahrenheit, and omitting disturbed Observations in which the Amount of Disturbance equalled of the whole Vertical Force at Toronto.

				GC	TTINGE	n HOUR	s.					
12	13	14	15	16	17	18	19	20	21	22	23	Periods from which the
				Т	ORONTO	HOURS	•					Hourly Means are derived.
6	7	8	9	10	11	12	13	14	15	16	17	
Sc. Div. 69 9 66 6 61 7 58 1	sc. Div. 69 9 66 9 61 1 58 1	Sc. Div. 69.6 66.7 60.8 58.0	sc. Div. 69 * 5 66 * 3 60 * 5 58 * 3	Sc. Div. 69°1 66°4 61°0 57°9	Sc. Div. 68.6 65.4 59.7 57.7	Sc. Div. 67.9 64.8 58.9 57.5	Sc. Div. 67 5 64 7 60 6 57 3	sc. Div. 67 ' 7 64 ' 2 60 ' 9 57 ' 2	Sc. Div. 68°1 64°6 59°3 57°2	Sc. Div. 67.9 64.4 59.1 56.8	Sc. Div. 67.5 64.9 58.9 57.5	1842: Oct. 1 to 31. Nov. 1 to 18. Nov. 19 to 30. Dec. 1 to 31. 1843: Jan. 1 to 31.
58.9 55.0 63.6 60.9 58.2 53.7	59°1 55°0 62°4 60°1 57°8 53°5	58.8 54.8 61.6 59.6 57.6 53.3	59.0 54.8 61.3 59.2 57.1 52.8	58°9 54°4 60°5 58°4 56°4 52°1	58.6 53.9 59.7 57.7 55.7 51.7	57°5 53°2 59°4 57°4 55°4 51°1	57.5 52.8 59.2 57.1 55.1	57.5 53.0 57.9 56.2 54.4 49.9	57°2 53°0 58°0 56°1 54°2 50°3	57°1 53°2 58°4 56°2 54°1 50°0	57°3 53°6 58°4 56°8 55°2 50°8	Feb. 1 to 28. July 2 to 29. July and August. Aug. 1 to 31. Aug. 1 to 31 and
49.2	49.2	49.1	48.2	47.9	47.7	46.9	46.3	45.4	46.5	46.0	46.2	Sept. 10 to 30.
105.6 108.3 106.0 103.5 101.6 99.8 97.0 94.1 91.9 92.6 91.3 88.4 86.4 85.1 81.7 82.3 82.2 80.0	106°0 108°0 105°9 102°8 101°4 100°1 97°1 94°1 91°5 92°1 90°8 87°7 86°0 84°3 81°4 82°8 82°3 79°8	106'2 107'8 105'4 102'7 101'1 99'6 96'7 93'9 91'6 91'7 90'6 87'8 84'8 84'8 81'6 82'3 79'7	105.7 108.0 105.1 102.0 100.7 99.5 96.7 93.9 91.5 91.7 90.4 87.0 84.4 81.7 81.8 82.2 79.8	105.7 107.7 104.4 101.1 99.8 98.6 96.0 93.3 91.0 91.1 89.9 86.6 84.0 82.8 81.6 81.4 82.5 79.6	105'8 107'0 104'2 101'3 99'6 98'0 95'5 93'0 90'8 91'0 89'5 86'4 84'0 82'2 80'7 81'1 81'4 79'0	106.0 107.0 104.5 102.1 99.8 97.7 95.2 92.8 91.3 90.7 89.6 84.9 83.7 82.1 80.1 81.2 81.1 78.9	105.6 106.5 104.4 102.3 99.8 97.2 94.7 92.2 90.6 90.2 89.1 86.3 83.3 81.5 80.9 80.3	105:3 106:8 104:5 102:2 99:5 96:7 94:5 92:2 90:3 90:0 89:0 86:6 84:2 80:7 80:7 80:7	105:3 106:5 104:2 101:9 99:7 97:5 94:8 92:1 89:9 90:1 89:6 86:7 84:4 81:1 80:1 81:2 80:1 78:6	105.6 107.1 104.2 101.4 99.4 97.5 95.0 92.4 89.8 90.6 89.0 86.3 84.3 82.2 80.0 80.8 80.1 78.2	105.6 106.9 104.4 102.0 100.0 98.1 95.5 93.0 90.6 91.2 88.0 86.4 82.4 80.2 80.4 80.3 78.3	1844: Feb. 9 to 29. March 1 to 23. March and April. April 7 to 23. April and May. May 12 to 25. May and June. June 9 to 22. June 23 to 30. July 1 to 6. July 7 to 13. July 14 to 20. July 21 to 31. Aug. 1 to 31. Sept. 1 to 30. Oct. 1 to 31. Nov. 1 to 30. Dec. 1 to 31.
78.7 77.5 73.1 71.6 71.1 68.8 110.5 106.9 106.3 99.2 168.4 164.9	78.4 77.7 72.9 71.5 70.8 68.3 109.8 106.9 105.7 98.4 167.4 164.2	78'4 77'4 72'8 71'4 71'0 67'8 109'7 106'1 105'2 97'6 167'3 164'4	78.6 76.7 72.6 71.3 70.7 67.2 109.2 106.4 105.1 97.5 166.3 163.5	78'4 75'6 72'4 71'0 70'0 67'4 109'5 105'8 104'2 97'7 166'5 163'3	77'9 75'9 72'5 71'2 70'0 66'7 109'2 105'6 103'9 97'3 165'3 163'1	78°1 75°7 71°3 70°5 69°5 66°5 108°6 105°9 103°5 97°0 165°3 162°7	77'8 75'7 71'6 70'3 69'2 66'6 108'9 105'5 103'6 96'4 164'4	77'7 75'6 71'4 69'9 68'8 66'8 109'0 105'1 103'7 95'7 165'4 162'1	77'4 75'1 71'6 70'5 69'1 66'8 109'5 105'1 104'1 96'3 165'9 162'3	78.8 75.1 71.0 70.7 69.3 66.7 109.4 105.6 103.7 96.6 165.4 162.6	76.8 75.1 71.3 70.5 70.0 67.2 109.8 106.4 103.9 98.0 165.9 163.3	Jan. 1 to 15. Jan. 16 to 31. Feb. 1 to 28. March 1 to 31. April 1 to 30. May 1 to 31. June 11 to 21. June 22 to 30. July 1 to 12. July 13 to 31. Aug. 1 to 16. Aug. 17 to 31. (Continued on p. xl.)

Table XXV.—continued.

					G	ÖTTING	EN HOU	RS.				
Periods	0	1	2	3	4	5	6	7	8	9	10	11
to which the Hourly Means			I	<u>'</u>	<u>'</u>	TORONT	o Hour	S.	<u> </u>			
correspond.	18	19	20	21	22	23	0	1	2	3	4	5
1845 (cont.): Sept. 1 to 13 - Sept. 14 to 30 - Oct. 1 to 18 - Oct. 19 to 31 - Nov. 1 to 15 - Nov. 16 to 30 - Dec. 1 to 31 -	Sc. Div. 161'0 164'1 162'9 158'8 159'6 158'1 155'5	Sc. Div. 160'8 163'5 163'0 159'1 159'8 158'1 155'2	Sc. Div. 161'2 163'0 163'0 159'5 159'2 157'5 155'2	sc. Div. 160°2 162°1 161°6 159°9 158°5 157°1 155°4	Sc. Div. 160'9 162'0 161'5 158'9 158'4 156'6 155'5	Sc. Div. 161'4 162'6 161'7 158'3 158'6 157'3 155'6	Sc. Div. 162°2 163°1 162°1 158°3 159°4 158°7 155°7	Sc. Div. 163°5 164°2 162°6 159°5 160°2 159°0 156°4	Sc. Div. 165 ' 4 165 ' 1 163 ' 4 160 ' 6 161 ' 4 159 ' 7 157 ' 1	Sc. Div. 165 '4 164 '9 164 '0 160 '8 161 '2 159 '0 157 '6	Sc. Div. 165'1 165'3 163'9 160'0 160'7 158'8 157'5	Sc. Div. 164.9 165.2 164.2 160.6 160.4 158.9 157.1
1846: Jan. 1 to 31 Feb. 1 to 28 March 1 to 24 April 3 to 25 April 26 to May 9 May 10 to 23 May 24 to June 6 June 7 to 24 June 25 to July 4 July 5 to 25 July 26 to Aug. 8 Aug. 9 to 22 Aug. 23 to 31 Sept. 1 to 30 Oct. 1 to Nov. 1 Nov. 2 to 7 Nov. 8 to 28 Nov. 29 to Dec. 12 Dec. 13 to 16	154'9 155'0 154'5 213'7 212'3 210'9 209'3 207'8 206'7 205'6 204'4 203'3 201'8 200'4 200'3 198'3 196'3 193'3	154'9 155'1 154'5 213'5 211'9 210'3 208'6 206'9 206'0 205'1 204'4 203'6 201'8 200'0 200'2 198'4 196'6 193'6 190'6 187'0	155 · 2 155 · 1 154 · 6 213 · 2 211 · 6 210 · 1 208 · 7 207 · 3 206 · 0 204 · 6 203 · 8 202 · 9 201 · 4 199 · 9 200 · 3 198 · 5 196 · 6 193 · 5 190 · 2 187 · 7	154'4 154'1 153'8 212'2 210'6 209'1 208'4 207'8 206'1 204'3 203'3 202'4 200'5 198'6 200'2 198'3 196'4 193'0 189'9 187'1	154'3 153'3 152'7 211'2 210'0 208'7 207'9 207'1 205'7 204'3 202'8 201'4 200'0 198'6 199'6 197'9 196'2 192'6 189'4 186'8	154·4 153·4 152·2 211·9 210·6 209·1 207·6 206·0 204·3 203·1 201·9 201·1 200·4 199·7 197·8 195·9 193·0 189·5 186·8	154.7 154.3 152.7 211.2 211.0 210.9 209.5 208.0 206.4 204.7 203.5 202.4 201.3 200.2 200.0 198.3 196.6 193.5 190.3 187.5	155.9 154.4 153.6 211.8 212.0 212.3 210.4 208.5 206.6 204.8 204.1 203.4 202.3 201.2 201.0 199.1 197.2 194.2 190.7	156.5 155.1 154.4 213.2 213.4 213.6 211.5 209.4 207.8 206.1 205.2 204.4 202.8 202.5 201.9 200.0 195.0 195.0 191.1 188.0	156.7 155.6 155.5 214.0 213.5 213.0 211.0 209.0 207.1 206.2 205.3 203.9 202.3 202.1 198.0 194.8 191.1 188.0	156.4 155.8 155.4 213.6 213.5 213.5 212.7 211.9 210.3 208.8 207.6 206.4 204.5 202.7 202.1 199.8 197.5 195.0 191.0	156.4 155.8 155.5 213.4 213.9 214.0 212.5 210.6 209.8 208.6 207.1 204.8 202.6 202.0 199.8 197.3 191.2 188.2
Dec. 17 to 31 1847: Jan. 1 to 15 Jan. 16 to 31 Feb. 1 to 28 March 1 to 31 April 1 to 30 May 1 to 31 June 1 to 15 June 16 to 30 July 1 to 31 Aug. 1 to 31 Sept. 1 to 30 Oct. 1 to 31 Nov. 1 to 30 Dec. 1 to 31 1848: Jan. 1 to 31 Feb. 1 to 29 March 1 to 31 April 1 to 30 April 1 to 30	187.6 185.7 183.1 182.0 182.7 183.5 181.0 178.4 175.4 173.3 171.8 172.7 172.9 172.6 171.1	186°0 183°1 182°9 183°6 183°3 180°4 176°8 175°2 173°3 171°0 172°8 173°7 173°7 173°3 170°8	185 · 5 183 · 0 183 · 4 184 · 2 182 · 8 179 · 8 176 · 5 174 · 6 173 · 0 170 · 3 172 · 5 173 · 7 172 · 3 170 · 7	184'7 182'9 181'8 183'3 182'1 179'1 176'5 174'4 172'5 169'8 171'3 173'2 170'9	184.5 183.2 181.6 182.5 181.3 176.8 174.1 171.7 170.9 170.7 173.0 171.9 170.6	185°3 182°5 181°6 182°2 181°1 178°3 177°1 173°2 171°7 170°9 171°5 172°2 172°6 171°0	186 · 4 183 · 1 182 · 2 183 · 1 181 · 5 178 · 2 177 · 4 173 · 2 171 · 6 170 · 9 171 · 9 172 · 8 173 · 4 171 · 0 168 · 6 164 · 7 163 · 3 162 · 1	186°2 183°2 182°7 183°2 182°1 179°0 177°8 173°6 172°0 171°1 173°0 174°2 174°2 174°1 171°9 168°9 165°3 164°0 163°2	186.5 183.3 183.1 184.0 183.1 179.7 178.2 174.2 172.5 171.5 173.0 174.4 175.4 172.4	186 8 183 3 183 3 183 0 184 4 184 2 180 8 180 0 175 6 173 9 171 9 173 3 174 7 175 3 173 1	186 '7 182 '7 183 '1 184 '6 184 '7 181 '6 179 '5 177 '0 174 '2 172 '6 173 '6 174 '9 175 '5 172 '2 169 '8 165 '7 165 '0 165 '4	186'8 183'8 183'2 184'8 184'9 182'3

Table XXV.—continued.

				G	ÖTTING	EN HOU	RS.					
12	13	14	15	16	17	18	19	20	21	22	23	Periods from which the
		_			TORONT	o Hour	S.					Hourly Means are derived.
6	7	8	9	10	11	12	13	14	15	16	17	
Sc. Div. 164'9 164'5 164'0 160'6 160'6 158'8 157'1	Sc. Div. 164.5 164.3 164.2 160.5 159.8 158.6 157.5	sc. Div. 163 '8 164 '7 164 '1 161 '0 159 '9 157 '8 157 '3	Sc. Div. 163'4 164'5 164'0 162'3 159'9 158'9 157'0	sc. Div. 163 ' 4 163 ' 4 163 ' 2 161 ' 3 159 ' 4 157 ' 4 157 ' 2	sc. Div. 162'8 162'7 163'4 161'2 159'0 158'1 157'2	Sc. Div. 162'1 162'9 162'9 160'6 159'0 157'5 156'4	Sc. Div. 160'9 163'2 162'3 160'0 159'3 156'9 155'8	Sc. Dv. 160°2 163°0 162°4 159°5 158°9 156°8 155°9	Sc. Div. 160'9 161'7 162'4 159'7 159'2 157'6 155'8	Sc. Div. 160'2 162'0 162'3 159'4 159'1 157'6 155'3	Sc. Div. 161'3 162'9 162'5 159'6 159'4 157'5 155'4	1845: Sept. 1 to 13. Sept. 14 to 30. Oct. 1 to 18. Oct. 19 to 31. Nov. 1 to 15. Nov. 16 to 30. Dec. 1 to 31.
156 1 156 1 155 5 213 1 213 6 214 2 212 4 210 6 209 9 209 2 207 7 206 3 204 2 202 2 202 0 199 9 197 7 194 7 191 1 188 2	156.5 156.4 155.5 215.4 213.8 212.2 211.4 210.6 207.6 206.0 204.1 202.3 202.1 200.1 198.2 198.7	156.6 155.9 154.8 214.9 213.4 211.9 210.7 209.5 208.5 207.5 206.4 205.3 203.5 201.8 200.1 198.5 194.8 191.4	156.2 155.8 154.7 213.5 212.3 211.1 210.2 209.2 207.9 206.6 204.7 202.8 202.0 201.2 201.0 199.5 197.5 197.5 198.4	156'4 156'1 154'8 213'4 212'4 211'4 209'7 208'0 206'6 205'2 204'4 203'7 202'5 201'4 201'1 199'6 199'6 199'9 187'8	156.0 155.7 155.4 213.3 211.6 209.9 209.0 208.1 206.7 205.4 203.9 202.5 201.5 200.4 200.0 199.0 199.0 199.7 187.7	155.7 155.4 154.6 212.0 210.9 209.8 208.5 207.3 206.0 204.8 203.8 201.5 200.2 200.0 198.4 196.7 193.8 190.0 187.6	154.8 154.9 154.2 212.3 210.7 209.1 208.3 207.5 205.2 202.8 202.5 202.3 201.5 200.7 199.6 198.2 196.8 193.4 189.6 187.6	155.2 154.8 154.1 212.7 210.9 209.2 208.0 206.7 200.3 201.0 201.7 201.4 201.1 200.0 198.5 197.1 192.7 190.0 187.2	154.6 154.7 154.1 212.6 210.7 208.8 206.9 205.0 203.6 200.2 200.8 201.5 201.1 200.7 199.9 198.4 196.9 192.3 189.8 187.7	154.9 154.3 154.0 213.2 212.0 210.7 208.6 206.5 203.6 200.9 200.5 201.2 200.6 200.0 199.1 197.9 196.7 192.8 189.4 187.1	154.7 154.5 153.8 213.3 211.7 210.0 208.7 207.5 205.1 202.8 202.1 201.5 200.1 198.8 199.0 197.8 196.6 193.1 189.6 187.4	1846: Jan. 1 to 31. Feb. 1 to 28. March 1 to 31. April 1 to 30. April 1 to May 31. May 1 to 31. May 1 to 30. June 1 to 30. June 1 to 30. June 1 to July 31. July 1 to 31. July 1 to 31. Aug. 1 to 31. Aug. 1 to Sept. 30. Sept. 1 to 30. Oct. 1 to 31. Oct. 1 to Nov. 30. Nov. 1 to 30. Nov. 29 to Dec. 12. Dec. 17 to 31.
187.0 184.2 183.3 181.2 184.3 182.3 179.6 177.3 174.7 172.4 174.0	186.7 183.8 183.3 183.9 184.5 182.2 179.1 176.8 174.2 172.0 172.2 175.3 175.2 172.4	186.7 184.0 183.3 184.6 184.2 182.1 179.4 176.1 173.3 172.0 172.5 175.2 175.4 172.5	186°2 183°5 183°0 184°5 183°6 181°8 179°3 175°5 173°6 171°2 172°6 175°0 174°9 172°5	185·7 183·7 182·8 184·4 183·6 181·5 178·7 174·7 171·1 172·4 175·1 174·3 172·4	185'9 183'6 182'7 183'9 183'3 180'8 178'1 174'5 171'1 172'0 174'7 174'4 171'8	185.5 183.7 182.6 183.5 183.3 180.4 176.8 173.8 172.6 169.6 170.8 173.6 173.9 170.4 168.1 165.8 164.4 161.7 158.6	185'3 183'4 182'6 183'3 182'4 180'3 176'1 174'4 171'7 170'5 170'5 173'1 172'9 171'2	185°3 183°3 182°1 182°6 182°4 180°2 177°2 174°2 171°6 170°0 171°0 171°0 172°7 170°8	185.7 183.3 182.2 183.4 182.9 180.1 177.2 174.4 171.5 170.3 171.6 173.5 172.6 171.1	185°5 182°9 182°2 183°7 179°8 177°8 175°8 172°1 169°7 170°6 173°1 172°6 170°6	185°2 182°9 181°7 183°2 183°1 180°9 178°2 175°4 172°6 170°2 171°6 172°9 172°4 170°0	1847: Jan. 1 to 15. Jan. 16 to 31. Feb. 1 to 28. March 1 to 30. May 1 to 31. June 1 to 15. June 16 to 30. July 1 to 31. Aug. 1 to 31. Sept. 1 to 30. Oct. 1 to 31. Nov. 1 to 30. Dec. 1 to 31. 1848: Jan. 1 to 31. Feb. 1 to 29. March 1 to 31. April 1 to 30. May 1 to 31.

Vol. III.

INCLINATION AND TOTAL FORCE.

Analysis of the larger Disturbances.—The disturbances of the Inclination which equalled or exceeded 1'·0, and of the total force which equalled or exceeded 0004 of the whole force, both measured from the respective normals at the same hour and in the same month, were obtained from the observed disturbances of the Horizontal and Vertical Forces in the following manner: Tables were formed, in the first column of which were placed in chronological order the larger disturbances of the Vertical Force, separated as already described, and in the second column those of the Horizontal Force, each expressed in terms of the respective forces, by the conversion of the scale divisions in which the disturbances were observed into parts of the respective forces by means of the scale coefficient.

At a large proportion of the hours of contemporaneous observation, when one of the two components of the force exhibited a disturbance which by its amount was brought into the category of the larger disturbances, the other component was also disturbed. In such cases there were contemporaneous entries in both columns; but when one of the components only was so affected, the entry in the corresponding column of the other component was blank. These blanks were all filled up by inserting for the component which did not exhibit a disturbance of sufficiently large amount to have been classed as a large disturbance and separated accordingly, the difference, whatever that might be, between the observation at that hour and its proper normal. These two columns then exhibited all the larger disturbances of both the horizontal and vertical components whenever either component was disturbed, with the contemporaneous difference of the other component from its mean or normal value in the cases when one only of the two components exhibited a large disturbance. The entries in the two columns had each their proper signs prefixed, + if the disturbance or difference from the normal were in augmentation of the force, and - if in diminution of the force. These two columns then expressed the values of $\frac{\Delta Y}{Y}$ for the Vertical Force, and $\frac{\Delta X}{X}$ for the Horizontal Force, for every hour at which either $\frac{\Delta Y}{Y}$ equalled or exceeded 00026 parts of the Vertical Force, or $\frac{\Delta X}{X}$ equalled or exceeded 0012 parts of the Horizontal Force. fourth column were then filled in, the third expressing the values of $\Delta\theta$, or the disturbances of the Inclination, and the fourth the values of $\frac{\Delta \Phi}{\Phi}$, or the disturbances of the Total Force (in parts of ϕ , the total force at Toronto), corresponding to

$$\Delta\theta = \sin\theta \cos\theta \left(\frac{\Delta Y}{Y} - \frac{\Delta X}{X}\right);$$

$$\frac{\Delta\phi}{\Phi} = \cos^2\theta \frac{\Delta X}{X} + \sin^2\theta \frac{\Delta Y}{Y}$$

the entries in the first and second columns, and computed by the formulæ—

From the third and fourth columns all the disturbances of the Inclination $(\Delta\theta)$ which equalled or exceeded 1'0 in amount, and all the disturbances of the total force $\left(\frac{\Delta\phi}{\phi}\right)$ equalling or exceeding 0004 in amount, were taken, as forming respectively a sufficient body of the larger disturbances of each element to permit their periodical laws to be investigated and shown. These disturbances were then dealt with, in regard to classification and tabular arrangement, in the same manner that has been already explained in treating of the disturbances of the horizontal and vertical components of the force.

In deriving the disturbances of the Inclination and Total Force from those of the Horizontal and Vertical Forces, all the calculations and arrangement in tables have been prepared, under the superintendence of Mr. Magrath, by the Non-Commissioned Officers of the Royal Artillery employed in the Woolwich Office; every part of the process having had the advantage of two independent computers.

Inclination.—The aggregate values of the disturbed observations of the Inclination in the different years, each ending June 30th, are as follows:—

TABLE XXVI.

Year ending	June 30	th 1844*	_		-	•	684°3
,,	,,	1845 -	-	•	•		613.9
,,	"	1846	-	•	-	-	753.7
,,	"	1847 -		-	-	-	1399.0
**	"	1848	•	•	•	-	3139.8
Tot	tal in the	five years		-	-	-	6590'7
	Mean	annual valu	ле <u>6</u>	$\frac{590.7}{5} =$	1318.1.	•	

The ratios in each year to the mean annual value are as follows:—

TABLE XXVII.

Year ending	June 30	th 1844	•		-	-	-	0.52
"	,,	1845		-		-	-	0.47
,,	,,	1846	-		•	-	-	0.57
,,	,,	1847		-		•	-	1.06
**	**	1848	•		•	•		2.40

Table XXVIII. exhibits the aggregate values in the different years divided into disturbances increasing the Inclination and disturbances decreasing the Inclination.

^{*} Having five months of the preceding year (October 1842 to February 1843) substituted for five of its own months (see page xi).

TABLE XXVIII.

					Increasing.	Decreasing.
Year ending	June 30th	1844	-	-	498.8	185'.5
,,	,,	1845	-	-	510.5	103.4
,,	,,	1846	-	-	612.7	141.0
"	,,	1847	-	-	1165.8	233.2
,,	,,	1848	-	-	2809.8	330.1
	Total in	th e five	years	-	5597.5	993.5
				=		

The effect of the larger disturbances is, therefore, to increase the Inclination considerably more than to decrease it. The ratios of the values of the disturbances increasing the Inclination to those which decrease it, on the average of the five years is 5.6 to 1. In the several years the ratios are as follows:—

TABLE XXIX.

Year ending June 30th 1844: As 2°7 to 1.

"" 1845: As 5°0 to 1.

"" 1846: As 4°3 to 1.

"" 1847: As 5°0 to 1.

"" 1848: As 8°5 to 1.

The augmentation of the ratio in the year ending June 30th, 1848, was occasioned by the excessive amount of disturbance in December 1847, which in the case of the Inclination was chiefly in disturbances increasing its value.

Table XXX. exhibits the aggregate values of the disturbances, distributed into the different *months* of their occurrence, and the ratios which the values in the different months bear to the mean monthly value or average of all the months.

TABLE XXX.

Months.			In the Y	ear ending J	une 30th,		Sums in	D-4'	2541-		
Months.		1844.	1845.	1846.	1847.	1848.	the Five Years.	Ratios.	Months		
July - August - September October - November December January - February March -		69.7 53.5 30.0 59.5 138.7 53.6 33.8 24.9 98.1 83.8	16·1 62·5 73·8 73·4 86·7 61·4 72·5 38·3 35·5 49·8	38'·4 45'·4 83'·0 50'·4 25'·2 73'·9 41'·4 32'·1 63'·9 114'·2	95.2 100.5 200.5 182.6 54.4 32.6 46.1 78.2 149.4 236.6	89.5 143.4 531.3 429.7 253.4 527.8 161.3 340.8 184.6 288.2	308.9 405.3 918.6 795.6 558.4 749.3 355.1 514.3 531.5 772.6	0.56 0.74 1.67 1.45 1.02 1.37 0.64 0.94 0.97 1.41	July. August. September. October. November. December. January. February. March. April.		
May - June -	-	30.2 8.5	33.1 10.8	85.8 82.8	60.8	140 · 9 48 · 9	466.5 214.6	$\begin{array}{c} \textbf{0.39} \\ \textbf{0.82} \end{array}$	May. June.		
Total in the five years 6590.7											
Mean monthly values - $\frac{6590.7}{12} = 549.2 = 1.00$											

December is the only exception to a periodical variation, having its maxima at the epochs of the equinoxes, and its minima at those of the solstices. This apparent anomaly was occasioned by the excessive and unusual disturbances in December 1847. The ratio for the month of December taken from a comparison of the disturbances in that month in the first four years, with the mean monthly value in the same years, is 0.77.

Table XXXI. exhibits the aggregate values of the disturbances of the Inclination distributed into the different *hours* of their occurrence, together with the ratios of the values at each hour to the mean hourly value or average of all the hours.

TABLE XXXI.

Toronto		In the Y	ear ending Ju	ne 30th,		Sums	D. di	Toronto Civil
Astronomical Time.	1844.	1845.	1846.	1847.	1848.	in the Five Years.	Ratios.	Time.
Hours.	,	,	,	,				
18	19.4	12.4	13.0	4ó·1	139.0	223.9	0.81	6 a.m.
19	16.5	16.6	17.7	47.0	224.8	322.6	1.12	7 a.m.
20	10.0	15.0	17.2	38.9	211'2	292.3	1.07	8 a.m.
21	20.6	20.1	35.9	51.6	160'4	288.6	1.00	9 a.m.
22	36.8	34.1	31.4	60.4	122'1	284.8	1.00	10 a.m.
23	36.2	29.7	31.9	51.0	130.2	279.6	1.00	11 a.m.
o	38.8	35.2	34.8	55.3	125.0	289.4	1.00	Noon.
1	34.4	25.2	41.8	42.8	126.8	271.0	0.99	1 p.m.
2	33.2	23.1	23.7	48.8	101'5	230.6	0.84	2 p.m.
3	21.9	26.4	32.9	48.4	95.6	225.2	0.85	3 p.nı.
4	35.7	18.8	30.0	40.0	77.5	202.0	0.73	4 p.m.
5	40.5	32.2	30.2	56.7	77.7	237.6	0.86	5 p.m.
6	43.2	28.0	44.9	61.0	93.8	270.9	0.99	6 p.m.
7	45:1	40.6	33.9	66.8	121.4	307.8	1.12	7 p.m.
8	37.0	40.1	44.5	66.2	94.8	282.6	1.03	8 p.m.
9	42.4	34.6	50.9	88.8	82.1	298.8	1.09	9 p.m.
10	36.2	35.4	48.9	83.0	113.5	317.7	1.16	10 p.m.
11	31.9	21.6	45.1	74.0	141.3	313.9	1.14	11 p.m.
12	19.7	33.3	42.2	52.6	146.3	294'1	1.07	Midnight.
13	20.9	28.4	27.9	100.0	160.7	337.9	1.23	1 a.m.
14	22.1	19.0	22.4	70.4	189.5	323.4	1.18	2 a.m.
15	13.8	15.7	20.8	79.2	133'4	262.9	0.96	3 a.m.
16	9.1	14.3	19.2	41.5	146.4	230.5	0.84	4 a.m.
17	18.0	13.8	12.2	34.5	124.1	202.6	0.74	5 a.m.
	·	Total in	the five year	rs -		6590.7		1
		Mean ho	urly value		$\frac{6590.7}{24} =$	274.6 = 1	.00	

The hourly disturbances of the Inclination arrange themselves in four groups, exhibiting a double progression. From 7 A.M. to noon, and again from 7 P.M. to 2 A.M. inclusive, the values equal or exceed the mean hourly value; and from 1 P.M.

to 6 P.M. inclusive, and again from 3 A.M. to 6 A.M. inclusive, they fall short of the mean hourly value.

Table XXXII. shows, in columns 2 and 3, the values at the different hours separated into disturbances which increase the Inclination and disturbances which decrease it.

The disturbances which increase the Inclination have two epochs of maxima, and two of minima; the principal maximum is at 1 A.M., and the secondary maximum at 7 A.M.; the principal minimum at 4 P.M., and the secondary at 5 A.M. The progression from the afternoon minimum to the maximum twelve hours later, may be regarded as continuous, with slight and possibly accidental interruptions at 8 P.M. and midnight; from the maximum at 1 A.M. to the minimum at 5 A.M., and thence to the secondary maximum at 7 A.M., the progressions are continuous and uninterrupted; and from the maximum at 7 A.M. to the afternoon minimum it is also continuous, with slight and possibly accidental interruptions at noon and 3 P.M.

The disturbances which decrease the Inclination are comparatively small at all the hours; they exhibit, however, a systematic tendency to be greater during the hours of the day than during those of the night; their actual maximum is at 2 p.m., and their minimum at 2 a.m.

The disturbances which increase the Inclination preponderate greatly at all the hours. In the Declination, there are certain hours in which the easterly deflections preponderate, and others in which the westerly deflections preponderate; and in the total force there are certain hours in which the general effect of the disturbances is to increase the force, and other hours in which their general effect is to decrease it. The Inclination differs in this respect from either of the other two magnetic elements; inasmuch as its disturbances have a uniform character in increasing the Inclination at all the hours. The greater or less degree in which this effect is produced is shown in column 4, which contains the differences between the two preceding columns (or their sums when the signs prefixed are regarded). This column therefore exhibits at the different hours the accumulated effect in five years of the disturbances of 1'·0, and upwards. The least amount of disturbance occurs at 2, 3, and 4 in the afternoon; at 6 p.m. it becomes considerable, and continues so till 3 A.M. inclusive, showing a decided maximum at 1 and 2 A.M. There is a second increase in the amount of disturbance at 7, 8, and 9 A.M., with a secondary maximum at 7 A.M., not much inferior in amount to the principal maximum at 2 A.M. In column 5 is shown the average daily effect of the disturbances of 1.0 and upwards, at the different hours of the 24; this is obtained by dividing the accumulated effect at the different hours in five years by 1550, being the number of days in the five years on which the observations were made.

TABLE XXXII.

Toronto	Aggregate Values	of the Disturbances	Excess of the Increasing	Mean Diurnal Effect	Toronto
Astronomical Time.	Increasing the Inclination.	Decreasing the Inclination.	Disturbances in Five Years.	of the larger Disturbances.	Civil Time.
(1.)	(2.)	(3.)	(4.)	(5.)	(6.)
H.	,	,	1	,	
18	+189.7	-34.2	+155.5	+0.10	6 a.m.
19	+301.7	-20.9	+280.8	+0.18	7 a.m.
20	+266.8	-25.5	+241.3	+0.19	8 a.m.
21	+245.1	- 42.5	+201.6	+0.13	9 a.m.
22	+224.4	-60.4	+164.0	+0.10	10 a.m.
23	+205.8	- 73.8	+132.0	+0.09	11 a.m.
0	+216.6	—72 '8	+143.8	+0.09	Noon.
1	+201.4	-69.6	+131.8	+0.09	1 p.m.
2	+150.8	- 79'8	+ 71.0	+0.02	2 p.m.
3	+168.2	-57.0	+111.2	+0.07	3 p.m.
4	+142.2	-59°8	+ 82.4	+0.02	4 p.m.
5	+183.1	-54.5	+128.4	+0.08	5 p.m.
6	+241.3	-29.6	+211.7	+0.14	6 p.m.
7	+265.8	-42.0	+223.8	+0.14	7 p.m.
8	+260.2	-22.4	+237.8	+0.16	8 p.m.
9	+275.1	-23.7	+251.4	+0.16	9 p.m.
10	+275.2	-42.5	+232.7	+0.12	10 p.m.
11	+279.3	-34.6	+244.7	+0.19	11 p.m.
12	+256.6	- 37.5	+219.1	+0.14	${f Midnight.}$
13	+309.4	-28.5	+280.9	+0.18	1 a.m.
14	+308.2	-15.2	+293.0	+0.19	2 a.m.
15	+243.3	-19.6	+223.7	+0.14	3 a.m.
16	+209'4	-21.1	+188.3	+0.15	4 a.m.
17	+177.9	-24.7	+153.2	+0.10	5 a.m.

Total Force.—The aggregate values of the disturbed observations of the Total Force in the different years, each ending June 30th, are as follows:—

TABLE XXXIII.

C	oune 30	th 1844*	-	-	*4491 pa	rts of th	e total force.
,,	,,	1845	-	-	•2775	,,	,,
,,	,,	1846	•	-	*3809	,,	,,
,,	,,	1847	-	-	•7293	,,	,,
"	,,	1848	-	-	1.0747	,,	,,
Total	in the fi	ve years	•	-	2.9112		

^{*} Having five months of the preceding year (October 1842 to February 1843) substituted for five of its own months (see page xxix).

The ratios in each year to the mean annual value are as follows:—

TABLE XXXIV.

Year ending	June 30th,	1844*	-	-	•	0.77
,,	,,	1845	•	-	-	0.48
3)	"	1846	-	•	-	0.65
,,	,,	1847	-	-	-	1.25
••		1848	-	_	-	1.84

Table XXXV. exhibits the aggregate values in the different years divided into Disturbances increasing the force, and Disturbances decreasing the force.

TABLE XXXV.

					Increasing.	Decreasing.		
Year ending	June 30	th, 1844	•	-	•2011	·2480 par	ts of the	Total Force.
,,	,,	1845	-	•	.0616	·2159	,,	,,
,,	,,	1846	-	-	•1363	·24 46	**	,,
,,	,,	1847	-	-	1839	•5454	,,	,,
"	,,	1848	•	•	4067	·6680	,,	,,
Tota	l in the	live years		-	·9896	1.9219		

The general effect of the larger disturbances of the Total Force is to decrease the total magnetic force more than to increase it.

The ratio of the values of the disturbances decreasing the Total Force to those which increase it, on the average of the five years, is 1.94 to 1. The ratios in the several years are as follows:—

TABLE XXXVI.

Year ending J	Tune 30t	h, 1844	-	•	- ,	-	as 1.23 to 1
,,	"	1845	-	•	-	-	as 3.51 to 1
,,	,,	1846	•	-	-	-	as 1'79 to 1
2)	"	1847	•	•	-	-	as 2.96 to 1
1>	,,	1848	•	-	-	-	as 1.64 to 1

^{*} Including five months (October to February) substituted from the preceding year (see page xxix).

Table XXXVII. exhibits the aggregate values of the disturbances distributed into the different *months* of their occurrence; with the ratios which the values in the different months bear to the mean monthly value or average of all the months.

TABLE XXXVII.

36			In the Y	ear ending	June 30,		Sums in		25	
Months.		1844.	1845.	1846.	1847.	1848.	the Five Years.	Ratios.	Months.	
July - August - September October - November - December - January - February - March - April - May - June -	-	*0447 *0244 *0457 *0415 *0515 *0677 *0296 *0026 *0605 *0633 *0164 *0012	*0151 *0349 *0587 *0524 *0317 *0033 *0260 *0144 *0136 *0074 *0144 *0056	· 0294 · 0437 · 0292 · 0205 · 0257 · 0265 · 0128 · 0132 · 0169 · 0551 · 0675 · 0404	*0668 *1161 *1339 *0688 *0170 *0047 *0120 *0256 *0625 *1332 *0711 *0176	*0338 *0384 *1302 *1464 *0604 *1538 *0476 *1237 *1012 *1163 *0929 *0300	1898 2575 3977 3296 1863 2560 1280 1795 2547 3753 2623	0.78 1.06 1.64 1.36 0.77 1.05 0.52 0.74 1.05 1.55 1.08 0.39	July. August. September. October. November. December. January. February. March. April. May. June.	
			Total	in the five	years		2.9112	parts of	the Total Force.	
Mean monthly value $\frac{2.9115}{12} = .2426 = 1.00$										

The anomaly in the, month of December, which is the only exception to a periodical variation having its maxima at the epochs of the equinoxes and its minima at those of the solstices, was occasioned by the excessive and unusual disturbances in December 1847. If the ratio for December be taken from the value of the disturbances in that month in the four years ending respectively June 30th, 1844, 1845, 1846, and 1847, compared with the mean monthly value in the same years, it is found to be 0.66, which would place it in its natural order in the progression. We may, therefore, regard the general progression of the annual variation of the Total Force depending on the larger disturbances to be from a maximum at each of the equinoxes to a minimum at each of the solstices, and vice versa; and the month of December 1847 as forming an accidental exception, presenting a decided anomaly in that particular year, but which might possibly disappear if the month were comprehended in observations continued through a longer series of years than are here combined.

Tables XXXVIII. and XXXIX. exhibit the aggregate monthly values in the different years separated into disturbances increasing and disturbances decreasing the force.

Table XXXVIII.

Disturbances increasing the Total Force.

36 0			In the Y	ear ending	June 30,		Sums in		36.3	
Months.		1844.	1845.	1846.	1847.	1848.	the Five Years.	Ratios.	Months.	
July August September October November December January February March April -	-	*0154 *0078 *0258 *0215 *0201 *0580 *0106 *0016 *0175 *0186	*0004 *0107 *0044 *0084 *0080 	*0062 *0087 *0016 *0105 	*0115 *0174 *0329 *0142 *0039 *0041 *0095 *0100 *0262 *0350	*0152 *0091 *0554 *0367 *0414 *0581 *0181 *0426 *0413 *0370	*0487 *0537 *1201 *0913 *0734 *1378 *0594 *0576 *0964 *1247	0.59 0.65 1.45 1.10 0.89 1.67 0.72 0.70 1.17	July. August. September. October. November. December. January. February. March. April.	
May - June -	-	·0042	.0020 .0009	.0367 .0117	.0100 .0092	.0363 .0155	.0892 .0373	1.08 0.45	May. June.	
			Total i	in the five	years		'9896 pa	rts of th	e Total Force	
Mean monthly value $\frac{.9896}{12} = .0825 = 1.00$										

Table XXXIX.

Disturbances decreasing the Total Force.

			In the Ye	ears ending	June 30,		Sums in			
Months.		1844.	1845.	1846.	1847.	1848.	the Five Years.	Ratios.	Months.	
July - August - September October - November - December - January - February - March - April	-	*0293 *0166 *0199 *0200 *0314 *0097 *0190 *0010 *0430 *0447 *0122	*0147 *0242 *0543 *0440 *0237 *0033 *0072 *0135 *0090 *0049 *0124	'0232 '0350 '0276 '0100 '0257 '0089 '0104 '0107 '0101 '0235 '0308	· 0553 · 0987 · 1010 · 0546 · 0131 · 0006 · 0025 · 0156 · 0363 · 0982 · 0611	*0186 *0293 *0748 *1097 *0190 *0957 *0295 *0811 *0599 *0793	'1411 '2038 '2776 '2383 '1129 '1182 '0686 '1219 '1583 '2506	0.88 1.27 1.73 1.49 0.70 0.74 0.43 0.76 0.99 1.56	July. August. September. October. November. December. January. February. March. April.	
May - June -	-	.0012	.0047	0308	*0084	.0566 .0145	·1731 ·0575	0.36	May. June.	
	·		Total i	n the five	years		-1.9219 I	parts of t	he Total Force.	
Mean monthly value $\frac{1.9219}{12} = .1602 = 1.00$										

Both the disturbances which increase the Total Force and those which decrease it show the same periodical law of monthly variation which has been pointed out in the remarks on Table XXXVII., in which they were exhibited conjointly. In both, the equinoxes are epochs of maxima and the solstices of minima. In the disturbances decreasing the force, the progression from the minima to the maxima and from the maxima to the minima is continuous and uninterrupted. In those increasing the force, December is the only interruption, and ceases to be so if the ratio be taken from the four years ending June 30th, 1844, 1845, 1846, and 1847; omitting the year ending June 30th, 1848. The excessive disturbances in December 1847 are seen by Tables XXXVIII. and XXXIX. to have been chiefly disturbances increasing the Total Force.

Table XL. exhibits the aggregate values of the disturbances distributed into the different hours of their occurrence; together with the ratios of the values at the different hours to the mean hourly value or average of all the hours.

TABLE XL.

Toronto Astrono- mical Time.	In the Year ending June 30,					Sums in the	Ratios.	Toronto Civil
	1844.	1845.	1846.	1847.	1848.	Five Years.		Time.
н.					-			п.
18	.0257	.0185	.0136	.0409	.0655	1642	1.35	6 a.m.
19	.0267	.0127	.0102	.0371	.0759	1629	1.34	7 a.m.
20	.0190	.0064	.0123	.0281	.0381	1039	0.86	8 a.m.
21	.0139	.0045	.0060	·0157	.0268	.0669	0.52	9 a.m.
22	.0099	.0012	.0033	.0020	.0123	.0320	0.26	10 a.m.
23	.0028	.0013	.0024	.0012	.0107	0214	0.17	11 a.m.
0	.0066	.0002	.0054	.0046	.0130	.0301	0.22	Noon.
1	.0135	.0024	.0076	.0120	.0228	.0583	0.48	1 p.m.
$\begin{bmatrix} 2 \\ 3 \end{bmatrix}$.0123	.0039	·0108	.0169	.0337	0776	0.64	2 p.m.
3	·0143	.0040	·0141	0252	.0353	0929	0.76	3 p.m.
4	.0171	.0063	.0225	.0229	.0474	1162	0.96	4 p.m.
5	.0224	.0117	. 0191	.0277	·0434	1243	1.05	5 p.m.
6 7	'0181	'0082	.0148	.0251	.0357	.1019	0.84	6 p.m.
7	. 0235	.0072	.0134	0205	.0458	1104	0.91	7 p.m.
8	.0165	.0063	.0080	. 0176	$\cdot 0395$	*0879	0.72	8 p.m.
9	.0150	.0075	'0104	.0164	0285	0748	0.65	9 p.m.
10	'0141	.0078	'0144	.0364	.0268	0995	0.85	10 p.m.
11	.0191	.0094	.0128	.0359	.0370	1172	0.97	11 p.m.
12	.0261	.0270	.0272	.0488	.0610	1901	1.57	Midnight
13	.0244	.0254	.0267	·0661	.0743	2169	1.78	l a.m.
14	*0257	.0292	.0300	.0634	.0767	2250	1.85	2 a.m.
15	.0292	.0309	.0339	`0625	0821	2386	1.97	3 a.m.
16	.0207	0245	0321	.0578	•0708	2059	1.70	4 a.m.
17	'0325	.0230	.0240	'0415	.0716	1926	1.59	5 a.m.

Total in the five years - - 2.9115 parts of the Total Force.

Mean hourly value $\frac{2.9115}{24} = .1213 = 1.00$

The law which regulates the occurrence in the diurnal period of the disturbances of larger amount of the Total Force is here in its principal features sufficiently distinct and obvious. From 8 a.m. to 11 p.m. inclusive the disturbance at every hour is less than at any hour from midnight to 7 a.m. inclusive. It is a minimum at 11 a.m., and a maximum at 3 a.m., the disturbance at the hour of maximum being about eleven times greater than at the minimum hour. From the maximum at 3 a.m. to the minimum at 11 a.m. the progression is continuous and uninterrupted: from the minimum at 11 a.m. to the maximum at 3 a.m. the progression is interrupted in the afternoon by secondary small maxima at 5 and 7 p.m., with corresponding secondary minima at 6 p.m. and 9 p.m., but from the secondary minimum at 9 p.m. to the principal maximum at 3 a.m. the progression is continuous and uninterrupted.

Tables XLI. and XLII. show the aggregate hourly values in the different years, separated into disturbances increasing and disturbances decreasing the force; with the ratio of the values at each hour to the respective mean hourly values.

TABLE XLI.

Disturbances increasing the Force.

Toronto Astrono-		In the	Year ending Ju	ine 30,		Sums in the Five	Ratios.	Toronto
mical Time.	1844.	1845.	1846.	1847.	1848.	Years.	ranos.	Civil Time.
11. 18 19 20 21 22 23 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	*0045 *0060 *0058 *0055 *0038 *0040 *0056 *0100 *0105 *0122 *0149 *0196 *0150 *0192 *0139 *0079 *0062 *0069 *0061 *0054 *0046 *0048 *0023 *0064	·0004 — ·0009 — ·0005 ·0005 ·0024 ·0039 ·0040 ·0063 ·0117 ·0078 ·0068 ·0055 ·0037 ·0028 ·0022 ·0012 ·0010 — — — —	*0022 *0012 *0026 *0004 *0009 *0016 *0040 *0044 *0085 *0137 *0211 *0177 *0126 *0119 *0064 *0080 *0041 *0028 *0035 *0015 *0012 *0020 *0016 *0024		· 0042 · 0029 · 0043 · 0025 · 0049 · 0088 · 0122 · 0216 · 0325 · 0353 · 0474 · 0434 · 0357 · 0454 · 0386 · 0228 · 0159 · 0074 · 0080 · 0030 · 0025 · 0033 · 0013 · 0028	*0113 *0105 *0147 *0088 *0100 *0157 *0269 *0500 *0715 *0883 *1107 *1184 *0958 *1025 *0796 *0493 *0326 *0211 *0192 *0113 *0099 *0122 *0073 *0120	0·27 0·25 0·36 0·21 0·24 0·38 0·65 1·21 1·73 2·14 2·69 2·87 2·32 2·49 1·93 1·19 0·79 0·51 0·46 0·27 0·24 0·30 0·18 0·29	H. 6 a.m. 7 a.m. 8 a.m. 9 a.m. 10 a.m. 11 a.m. Noon. 1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 6 p.m. 7 p.m. 9 p.m. 11 p.m. Midnight. 1 a.m. 2 a.m. 3 a.m. 4 a.m. 5 a.m.
	1		otal in the	five years		*9896 par	rts of the f	orce.
· · · · · · · · · · · · · · · · · · ·		N	Iean hourly		896 =	·0412 = 1	.00	

Table XLII.

Disturbances decreasing the Force.

Toronto Astrono-		In the	Year ending Ju	ine 30,		Sums in the	Deden	Toronto Civil
mical Time.	1844.	1845.	1846.	1847.	1848.	Five Years.	Ratios.	Time.
н.								11.
18	.0212	.0181	.0114	·0409	.0613	1529	1.91	6 a.m.
19	.0207	.0127	.0093	.0367	.0730	1524	1.30	7 a.m.
20	.0132	0055	.0097	.0270	. 0338	.0892	1.11	8 a.m.
21	.0084	.0045	*0056	.0123	.0243	*0581	0.73	9 a.m.
22	.0061	.0015	.0024	.0046	0074	.0220	0.27	10 a.m.
23	.0018	.0008	.0008	.0004	.0019	.0057	0.07	11 a.m.
0	.0010		.0014		.0008	0032	0.04	Noon.
1	.0035		.0035	.0004	.0012	.0083	0.10	1 p.m.
2	.0018		.0023	.0008	.0012	.0061	0.08	2 p.m.
3	.0021		.0004	.0021	-	.0046	0.06	3 p.m.
4	.0022		.0014	. 0019		.0055	0.07	4 p.m.
5	.0028		*0014	.0012		.0059	0.04	5 p.m.
6	.0031		. 00 2 6	*0004		.0061	0.08	6 p.m.
7	.0043		·0019	.0013	*0004	.0079	0.10	7 p.m.
8	.0026	.0004	.0050	.0024	.0009	.0083	0.10	8 p.m.
9	.0041	.0033	.0029	.0095	.0057	*0255	0.35	9 p.m.
10	.0079	.0046	.0104	0328	.0109	.0669	0.84	10 p.m.
11	.0122	.0067	.0135	.0341	.0296	. 0961	1.50	11 p.m.
12	.0200	.0258	.0237	.0484	.0230	1709	2.13	Midnight.
13	.0190	.0244	.0252	.0657	.0713	2056	2.57	1 a.m.
14	·0211	.0292	·0288	.0618	$\cdot 0742$	2151	2.69	2 a.m.
15	.0244	.0309	·0319	. 0604	$\cdot 0788$	2264	2.83	3 a.m.
16	·0184	0245	.0302	.0557	. 0695	1986	2.48	4 a.m.
17	. 0261	•0230	.0216	•0411	. 0688	1806	2.25	5 a.m.
,		Total in	the five year	ars -		1.9219 pa	rts of the	Total Force.
		Mean ho	urly value		$\frac{9219}{24} =$	·0801 =	1.00	

When Tables XLI. and XLII. are examined, it is seen that the disturbances increasing the force and those decreasing it, may be generally viewed as parts of one and the same phenomenon, subject to one and the same law, expressed by ratios which in the two cases are approximately the complement of each other, viz., at the hours when the one augments in value, the other diminishes, and vice versa; and that the two classes of disturbances, distinguished from each other by the opposite effects which each produces on the mean or normal state of the magnetic force, do in fact constitute when viewed together a diurnal variation of very striking order and regularity, having a maximum of increased force at a certain hour, and a maximum of diminished force at another hour distant nearly twelve hours from the preceding, and forming a regular progression from the hour of the greatest increased force to that of greatest diminished force, and vice versa. To see this in its just light, and to obtain the true

proportions in which the magnetic force is increased or diminished at the different hours by the effects of the disturbances, it is necessary to combine the values in Tables XLI. and XLII. somewhat differently from what is done in Table XL., by taking the differences instead of the sums of the increasing and decreasing values. When we take the sums we investigate the proportion which the whole amount of disturbance, whether its effect be to increase or to decrease the force, bears at each hour to the mean hourly value or average of all the hours: the ratios in this case are shown in Table XL. When, on the other hand, we take the differences, we exhibit the amount by which the magnetic force of the earth is either increased or decreased at the several hours by the influence of the disturbances of '0004 and upwards during five years. This is shown in column 4 of Table XLIII.; the values are in parts of the Total Force at Toronto.

TABLE XLIII.

Hours.			Disturt	oances	General Effect, or accumulated influence at each of	Average Daily Effect at the
			Increasing.	Decreasing.	the 24 hours in 5 Years.	different hours.
(1.) 18; or 6 A.M. 19; or 7 A.M. 20; or 8 A.M. 21; or 9 A.M. 22; or 10 A.M. 23; or 11 A.M. 0; or Noon 1; or 1 P.M. 2; or 2 P.M. 3; or 3 P.M. 4; or 4 P.M. 5; or 5 P.M. 6; or 6 P.M. 7; or 7 P.M. 8; or 8 P.M. 9; or 9 P.M.			(2.) + `0113 + `0105 + `0147 + `0088 + `0100 + `0157 + `0269 + `0500 + `0715 + `0883 + `1107 + `1184 + `0958 + `0796 + `0493 + `0326	(3.)15291524089205810220005700320083006100460055005900610079008300830069	(4.) -:1416 -:1419 -:0745 -:0493 -:0120 +:0100 +:0237 +:0417 +:0654 +:0837 +:1052 +:1125 +:0897 +:0946 +:0713 +:0238 -:0343	(5.) '000092 '000092 '000047 '000032 '00008 +- '000015 +- '000027 +- '000054 +- '000068 +- '000073 +- '000068 +- '000062 +- '000047 +- '000016 '000022
11; or 11 P.M. 12; or Midnight 13; or 1 A.M. 14; or 2 A.M. 15; or 3 A.M. 16; or 4 A.M. 17; or 5 A.M.	-	-	+ '0211 + '0192 + '0113 + '0099 + '0122 + '0073 + '0120	- '0961 - '1709 - '2056 - '2151 - '2264 - '1986 - '1806	- `0750 - `1517 - `1943 - `2052 - `2142 - `1913 - `1686	- '000047 - '000098 - '000125 - '000132 - '000138 - '000123 - '000109

We learn from this table that the law of the diurnal variation due to the disturbances of the Total Force at Toronto is as follows:—From 11 A.M. to 9 P.M. inclusive they augment the force; from 10 P.M. to 10 A.M. inclusive they diminish it. The hour of greatest augmentation is 5 P.M.; of greatest diminution 3 A.M. The decreasing effect changes to an increasing effect about midway between 10 and 11 A.M.; the increasing

to a decreasing between 9 and 10 p.m., nearer to 9 than to 10. The greatest diminution is nearly twice as great as the greatest augmentation. The hours of most rapid change are from 7 to 8 a.m., and from 11 p.m. to midnight. From the greatest diminution at 3 a.m. to the greatest increase at 5 p.m. the progression is continuous and uninterrupted, and from the greatest increase at 5 p.m. to the greatest decrease at 3 a.m. it is also continuous, except in a small and apparently accidental interruption at 7 p.m. As the values in column 4 of Table XLIII. are the accumulated values in five years, and as each year comprised about 310 days of observation (or 1,550 days in the five years) we may take an approximate view of the mean diurnal variation due to the disturbances equalling or exceeding '0004 in amount. An increase of force at 5 p.m. of '1125 divided by 1,550 days = '000073; and a decrease of force at 3 a.m. of '2142 divided by 1550 = '000138; making together an average diurnal range of '000211 parts of the force, changing progressively from + '000073 at 5 p.m. to - '000138 at 3 a.m.

As it is not probable, on the one hand, that the disturbances of $\cdot 0004$ and upwards comprehend all the disturbances of the class to which they belong, we may regard the preceding range as expressing the minimum limit of the true average daily range of variation due to the disturbances of occasional occurrence; whilst, on the other hand, it appears extremely improbable that the minor effects of the causes which produce the larger disturbances should equal in aggregate value those which exceed $\cdot 0004$. We have, then, the same degree of improbability that the range of the diurnal variation due to all the disturbances of this class should amount to twice the value which has been obtained by this analysis, or to $\cdot 000211 \times 2 = \cdot 000422$. The diurnal range may be regarded as something between $\cdot 000211$ and $\cdot 000422$, but probably nearer to the first than to the last. The final column of Table XLIII. (column 5) shows the average daily effect of the disturbances of $\cdot 0004$ and upwards at every hour of the day and night.

DECLINATION.

Analysis of the larger Disturbances.—To complete the view of the magnetic disturbances at Toronto in the five years ending June 30th 1848, a second and a more perfect analysis has been made of the disturbances of the Declination during that period than that which is contained in the second volume of the Toronto Observations (pp. xxvii—l), which was deemed sufficient for a first approximation when other duties pressed heavily on the time at command.

The disturbances which were then subjected to analysis, were those which differed five scale divisions (3'·6 in arc) or upwards from the mean or normal positions of the magnet in the same month and at the same hour, the normal positions being derived from the whole body of the observations, excluding only some very extreme disturbances. The more perfect mode of proceeding is that which has been stated in describing the process adopted in the cases of the Horizontal and Vertical Forces; viz. the subsequent correction of the normal positions by a recalculation in which the whole of the disturbances are excluded, and a revision of the disturbances in conformity with the new normals; both processes being repeated until the normals finally adopted are derived from a body of observations including all which differ less, and excluding all which differ more, than a certain fixed value from themselves. the same time this fixed value has itself been altered by raising the standard considered to constitute a disturbed observation from five scale divisions to seven (i.e. from 3'·6 to 5'·0 of arc), the experience gained in the former investigation having led to the belief that the higher value would constitute in some respects a preferable standard. The number of observations thus separated amounted to 2,172 in the five years of hourly observations ending June 30th 1848, averaging about 1 in 17 of the whole

The aggregate values of the disturbed observations in the different years are shown in the following table:—

Table XLIV. Year ending June 30th 1844 - - 2053'2 minutes of arc. """ 1845 - - 2521'8 "" """ 1846 - - 3246'6 "" """ 1847 - - 5478'7 "" """ 1848 - - 6422'0 "" Total in the five years - 19722'3 Mean annual value - - 19722'3 = 3944'5

The ratios in each year to the mean annual value are as follow:—

				LABL	E	ALV.					
Year	ending	June 30th	1844	_		-	-		-	-	0.52
	,,	,,	1845		-	-		-		-	0.64
•	,,	,,	1846	-		- '	-		-	-	0.85
	,,	,,	1847		-	-		-		-	1.39
	"	,,	1848	-		•	-		-	-	1.63

The observations of the Declination were not interrupted in the months from October 1843 to February 1844; consequently the years ending June 30th 1844, 1845, 1846, 1847, and 1848 are here strictly what they profess to be, and the ratios show a continuous progression from a minimum in the first year to a maximum in the last.

Table XLVI. shows the aggregate values in the different years, divided into easterly and westerly disturbances.

		7	ABLE	XLVI			
						Easterly.	Westerly
Year ending	June 30th	1844	-	-	-	$1235^{\prime}\cdot8$	817.4
,,	,,	1845	-	-	-	1325.4	1196.4
"	,,	1846	-	-	-	1973.3	1273.3
,,	,,	1847	-	-	-	2958.9	2519.8
,,	,,	1848	-	-	-	3573.5	2848.5
	Total in	the five	e years	-	-	11066.9	8655.4

The general effect of the larger disturbances is therefore to decrease the westerly Declination at Toronto. The easterly values preponderate in the ratio of 1.28 to 1.

Table XLVII. exhibits the aggregate values of the disturbances distributed into the different *months* of their occurrence, with the ratios which the values in each of the months bear to the mean monthly value or average of all the months.

TABLE XLVII.

•		Year	s ending June	e 3 0,		Sums in the		
Months.	1844.	1845.	1846.	1847.	1848.	Five Years.	Ratios.	Months.
July - August September October November December January february March - April - May - June -	 327.9 131.1 164.6 122.7 30.9 50.2 65.5 119.4 403.8 389.5 193.1 54.5	160'8 280'5 450'1 341'4 305'6 197'0 250'9 132'6 106'5 151'0 65'0 80'4	159'3 355'4 371'5 263'9 161'8 181'7 142'1 125'6 308'5 312'3 349'7 514'8	565 1 885 3 828 4 608 5 314 1 124 5 89 6 259 8 481 7 750 2 408 5 163 0	329'·5 242·7 848·9 808·2 469·6 691·4 387·9 746·4 524·2 726·0 587·5 59·7	1542.6 1895.0 2663.5 2144.7 1282.0 1244.8 936.0 1383.8 1824.7 2329.0 1603.8 872.4	0°94 1°15 1°62 1°31 0°78 0°76 0°57 0°84 1°11 1°42 0°98 0°53	July. August. September. October. November. December. January. February. March. April. May. June.
	 	Total	in the five	years		19722:3		<u> </u>
		Mean	monthly v	alue, 1972:	$\frac{2\cdot 3}{2} =$	1643.5 =	= 1.00	

September and April are the months of greatest disturbance, and January and June the months of least disturbance. The progression from the maxima to the minima, and from the minima to the maxima, is continuous and uninterrupted.

Table XLVIII. exhibits the aggregate monthly values in the five years separated into easterly and westerly values, with the ratios in each case to the respective mean monthly values, and also the ratios in the different months of the easterly to the westerly values.

TABLE XLVIII.

		Easterly	Values.	Westerly	Values.	Ratios of the	
Months.		Sums in the Five Years.	Ratios to the Mean Monthly Values.	Sums in the Five Years.	Ratios to the Mean Monthly Values.	Easterly to the Westerly Values.	Months.
July - August - September - October - November - January - February - March - April - May - June -	-	903 ² 2 1255·2 1504·8 1174·0 556·6 527·4 527·0 772·9 1062·9 1187·5 904·3 691·1	0'98 1'36 1'63 1'28 0'60 0'57 0'57 0'84 1'15 1'29 0'98	639'4 639'8 1158'7 970'7 725'4 717'4 409'0 610'9 761'8 1141'5 699'5 181'3	0.89 0.89 1.61 1.35 1.06 0.99 0.57 0.84 1.06 1.59 0.98	1 '41 1 '96 1 '29 1 '21 0 '77 0 '74 1 '29 1 '27 1 '40 1 '04 1 '29 3 '82	July. August. September. October. November. December. January. February. March. April. May. June.
Total in the five y	ears,	11066'9		8655 ·3	<u> </u>		
Mean monthly val	ues	- 922·2 = 1	.00 -	721:3 =	1.00		

The same general law is seen to prevail in both easterly and westerly disturbances when separately viewed as when they are viewed conjointly; the equinoxes are the epochs of maximum and the solstices of minimum.

The ratios which indicate the proportion in which the easterly disturbances preponderate over the westerly exhibit, on the other hand, a tendency towards a maximum at the June solstice and a minimum at the December solstice. The mean ratio in the months of November, December, and January is 0.93, and in the months of May, June, and July 2.17.

The next table exhibits the aggregate values of the disturbed observations distributed into the different *hours* of their occurrence, with the ratios which the values at each hour bear to the mean hourly value or average of all the hours.

TABLE XLIX.

Toronto Astrono-		Year	s ending June	30,		Sums in the	Ratios.	Toronto Civil
mical Time.	1844.	1845.	1846.	1847.	1848.	Five Years.	natios.	Time.
н.			,	,	,			
18	93.4	145.3	122.7	206.7	295'-6	863.7	1.02	6 a.m.
19	70.7	98.8	139.8	269.0	383.6	961.9	1.17	7 a.m.
20	67.6	122.2	136.4	297.0	423.5	1046.7	1.27	8 a.m.
21	59 · 1	84.0	129.7	210.5	427.9	910.9	1.11	9 a.m.
22	50.6	89.0	112.2	148.6	311.8	712.2	0.87	10 a.m.
23	37.5	100.5	83.8	119.4	197:3	538.2	0.66	11 a.m.
0	26.2	75.4	57.5	56.2	186.1	401.4	0.49	Noon.
1	29.3	28.8	31.2	42.7	112.6	244.6	0.30	1 p.m.
2	26.8	63.4	23.0	67.7	146.1	327.0	0.40	2 p.m.
3	28.1	57.9		105.1	134.9	326.0	0.40	3 p.m.
4	47.9	52.7	40.2	150.9	140.1	431.8	0.23	4 p.m.
5	66.9	54.7	59.3	159.0	114.4	454.3	0.56	5 p.m.
6	97.3	38.2	70.8	262.3	217.9	686.2	0.84	6 p.m.
7	62.8	101.1	225.9	257.4	156.9	804.1	0.98	7 p.m.
8	139.5	186.3	152.5	295.0	228.4	1001.4	1.22	8 p.m.
9	176.3	243.3	254.8	387.1	$433^{\circ}2$	1494.7	1.82	9 p.m.
10	220.5	178.9	254.9	380.2	232.2	1267.0	1.55	10 p.m
11	109.3	97.0	173.5	329.8	314.5	1024.1	1.25	11 p.m
12	158.2	139.1	193.7	270.5	344.8	1106.3	1.35	Midnigl
13	119.2	118.0	254.1	369.9	389.4	1250.6	1.52	l a.m
14	86.7	127.0	176.3	289.5	308.9	988.4	1.21	2 a.m
15	110.8	74.6	185.0	248.6	307.0	926.0	1.13	3 a.m
16	69.4	163.1	186.1	329.6	348.3	1096.5	1.34	4 a.m
17	99.7	82.3	183.2	225.9	266.6	858.0	1.02	5 a.m
		To	otal in the fi	ve years		19722:3		
		M	ean hourly v	alue, 1972		821.8 =	1.00	

From 10 A.M. to 7 P.M. inclusive the ratios are invariably below unity, and from 8 P.M. to 9 A.M. inclusive as invariably above unity. The hour of least disturbance is 1 P.M., and of greatest 9 P.M., both being well-marked features. The progression during the hours of the day from 8 A.M. to 9 P.M. is uninterrupted to and from the minimum at 1 P.M., but is much less regular during the hours of the night.

Table L. exhibits the aggregate values separated into their easterly and westerly constituents, with the ratios at each hour to the mean hourly value or average of all the hours.

TABLE L.

Toronto Astronomical	Disturb	ances.	Rati	os.	m
Time.	Easterly.	Westerly.	Easterly.	Westerly.	Toronto Civil Time
н.					
18	207.8	655.9	0.45	1.85	6 a.m.
19	160.2	801.7	0.32	2.53	7 a.m.
20	118.1	928.6	0.26	2.58	8 a.m.
21	99.5	811.8	0.21	2.25	9 a.m.
22	128.0	584.2	0.28	1.62	10 a.m.
23	$179 \cdot 9$	358.3	0.39	1.00	11 a.m.
0	111.8	289.6	0 24	0.80	Noon.
1	97.7	146.9	0.21	0.41	1 p.m.
2 3 4 5 6 7 8	93.2	233.8	0.50	0.65	2 p.m.
3	102.6	223.4	0.22	0.62	3 p.m.
4	145.1	286.7	0.35	0.80	4 p.m.
5	200.1	254.2	0.44	0.71	5 p.m.
6	481.5	205.0	1.02	0.57	6 p.m.
7	664.9	139.2	1.44	0.39	7 p.m.
8	899.6	101.8	1.95	0.58	8 p.m.
9	1417.1	77.6	3.09	0.55	9 p.m.
10	1104.7	162.2	2.41	0.45	10 p.m.
îĭ	925.4	98.7	$\frac{5.02}{2}$	0.27	11 p.m.
12	808.9	297.4	1.76	0.82	Midnight.
13	824.2	426.1	1.79	1.19	1 a.m.
14	627.6	360.8	1.37	1.00	2 a.m.
15	589.5	336.2	1.28	0.94	3 a.m.
16	662.5	434.0	1.45	1.51	4 a.m.
17	417.0	441.0	0.81	1.23	5 a.m.
1.	111 0	1110		1 20	0 a.m.
otal in the five years.	11066.9	8655*4			
[ean hourly }	461.1	360.6			

The easterly disturbances are below the average during the hours of the day, or from 5 a.m. to 5 p.m. inclusive, and above the average during the hours of the night, or from 6 p.m. to 4 a.m. inclusive; the westerly disturbances are below the average from noon to midnight inclusive, and above the average, with a single exception at 3 a.m., from 1 a.m. to 11 a.m. inclusive. The easterly have a maximum and the westerly a minimum, both decided features, at 9 p.m.; the westerly have a well-marked maximum at 8 a.m., and the easterly have minima scarcely differing from each other at 9 a.m. and at 1, 2, and 3 p.m. From noon to 5 p.m. both easterly and westerly disturbances are below their respective averages, consequently these are the hours of least general disturbance. From 6 p.m. to 11 p.m. the easterly are so much above their average that they more than compensate for the deficiency of the westerly; from midnight to 5 a.m. both easterly and westerly are above their respective averages (with the slight and apparently accidental exception already noticed at 3 a.m.), and from 6 a.m. to 10 a.m. the high values of the westerly more than compensate for the low values of the easterly disturbances. Excepting at the hours from noon to 5 p.m. inclusive,

when both easterly and westerly disturbances are small, and from 1 A.M. to 5 A.M., when they are both large, there is a systematic tendency to a diminution of easterly disturbance at the hours when large westerly disturbance prevails, and to a diminution of westerly disturbance when large easterly disturbance prevails.

In the following table is shown for each hour (in column 2) the excess of easterly disturbance over westerly, or of westerly over easterly, in the aggregate values of the five years; and in column 3 the mean effect at each hour, or a daily average, obtained by dividing the accumulated excess in five years shown in column 2 by 1,552, the number of days of observation in the five years. Column 3, therefore, exhibits the mean diurnal variation produced on a general average by the disturbances amounting to or exceeding 5'·0 of arc, and which, as a general and systematic effect, is superimposed upon the more regularly occurring diurnal variation derivable from the great body of the observations after the disturbed observations have been individually abstracted.

TABLE LI.

Toronto Astro- nomical Time.	Excess of Easterly or Westerly Values at the different Hours.	Mean Diurnal Variation occasioned by the disturbed Observations.	Toronto Civil Time.	Toronto Astro- nomical Time.	Excess of Easterly or Westerly Values at the different Hours.	Diurnal Variation	Toronto Civil Time.
	(2.)	(3.)			(2.)	(3.)	
H.	, ,					1	
18	448 1 W.	0.29 W.	6 a.m.	6	276.5 E.	0.18 E.	6 p.m.
19	641°5 W.	0'41 W.	7 a.m.	7	525 7 E.	0.34 E.	7 p.m.
20	810.5 W.	0°52 W.	8 a.m.	8	797.8 E.	0.52 E.	8 p.m.
21	712.6 W.	0'46 W.	9 a.m.	9	1339°5 E.	0.87 E.	9 p.m.
22	456°2 W.	0.30 W.	10 a.m.	10	942°5 E.	0.61 E.	10 p.m.
23	178°4 W.	0°11 W.	11 a.m.	11	826 7 E.	0.53 E.	11 p.m.
0	177'8 W.	0°11 W.	Noon.	12	511.5 E.	0.33 E.	Midnight.
1	49°2 W.	0°03 W.	1 p.m.	13	398 4 E.	0.26 E.	1 a.m.
2	140.6 W.	0.09 W.	2 p.m.	14	266.8 E.	0°17 E.	2 a.m.
3	120°8 W.	0.08 M.	3 p.m.	15	253 °O E.	0.16 E	3 a.m.
4	141 6 W.	0.09 M.	4 p.m.	16	228.5 E.	0°15 E.	4 a.m.
5	54°1 W.	0.04 W.	5 p.m.	17	24'0 W.	0.05 M	5 a.m.
	}			l			

It is seen by this table that when a daily average is derived from all the disturbances of larger amount (5'·0 and upwards) occurring in five years at Toronto they are found to produce a maximum easterly deflection of the Declination magnet of 0'·87 at 9 P.M., and a maximum westerly deflection of 0'·52 at 8 A.M., the intermediate progression either way being continuous, and only interrupted by a few slight irregularities occurring in the hours of the afternoon when the disturbances are fewest and of least amount. The range is 0.87 + 0.52 = 1.39, which might possibly be increased to 2'·0 if the disturbances of the same class which are less than 5'·0 could be separated and included in the analysis.

Table LII. contains the hourly normals of the Declination for each month from July 1843 to June 1848 inclusive, omitting disturbed observations in which the amount of disturbance equalled or exceeded 7.0 scale divisions or 5.0 of arc.

TABLE LII.

Hourly Means of the Readings of the Declinometer; omitting disturbed Observations in which

						GÖTT	INGEN H	OURS.				
Periods to which the		0	1	2	3	4	5	6	7	8	9	10
Hourly Means						TOR)NTO HO	ours.				
correspond.		18	19	20	21	22	23	0	1	2	3	4
1843:		Sc. Div.										
uly - Lugust - eptember letober - Vovember December		131.8 131.1 129.4 126.8 127.8 127.4	133.7 133.7 131.7 128.1 128.3 127.7	133.0 133.2 130.7 129.4 129.0 127.6	131.1 130.3 127.8 129.2 128.7 128.4	126.8 125.0 123.4 126.7 126.5 127.7	122.9 121.0 119.8 123.2 123.4 125.8	119°3 117°0 116°7 120°8 122°1 123°6	117.2 116.2 116.5 120.1 121.3 122.5	117.7 117.3 118.1 120.3 122.2 122.0	118.8 119.5 119.9 121.4 123.3 123.6	120.7 122.5 122.4 122.5 124.5 124.6
1844 :												
anuary - Cebruary - March - May - May - Muly - Mugust - Ceptember October - Vovember	-	127'1 128'2 129'1 129'1 130'4 130'3 129'1 130'1 123'9 120'8 118'5 118'7	127.5 129.0 129.8 130.1 131.4 131.5 132.3 131.5 125.0 122.1 119.3 118.6	128'7 129'2 131'0 130'9 131'2 131'3 132'2 131'6 123'9 122'4 120'5 119'0	129'6 128'8 130'3 129'3 129'6 129'0 129'8 127'9 121'1 121'4 120'5 119'8	127.7 126.5 127.8 126.2 125.5 124.4 125.3 122.8 116.3 118.4 118.5 119.5	125.7 124.0 124.0 121.7 121.4 119.6 120.5 117.2 111.5 114.6 115.1 116.9	123'4 121'8 120'5 119'1 118'2 116'1 118'0 115'0 108'4 112'3 113'2 114'6	122.2 121.3 119.5 118.0 116.5 114.6 115.7 112.8 109.9 112.1 112.0 113.6	122.3 122.3 119.5 118.0 116.2 115.3 115.0 114.9 110.8 112.7 113.6 113.5	123·3 123·8 120·5 119·3 117·3 116·7 116·8 115·6 114·1 115·1 114·7 115·5	124·3 125·2 121·7 120·7 119·8 118·8 119·0 119·5 117·5 116·2 115·6 116·0
1845: anuary - cebruary - Iarch - Iay - Iuy - Lugust - Geptember October - Vovember		117.7 119.6 119.7 121.0 122.9 123.3 121.4 121.5 118.2 115.5 114.8 114.9	119'8 120'2 121'6 122'3 124'3 124'3 123'7 123'8 119'2 116'1 116'4 115'3	120°8 120°5 122°8 123°3 124°0 124°4 123°6 118°9 116°8 117°2 116°3	119'9 120'4 122'5 122'6 121'2 122'1 123'0 120'7 115'7 115'6 116'4 116'4	117.8 118.7 120.1 118.5 115.8 118.7 114.8 111.1 113.4 114.0 116.3	115·2 116·0 116·1 115·0 110·4 112·5 113·1 109·1 107·2 110·6 110·2 114·3	113 2 113 3 112 7 110 2 107 6 108 5 108 6 105 1 104 7 108 4 107 6 111 9	113 1 112 3 110 4 107 6 107 4 107 1 106 1 103 8 105 0 108 2 108 0 110 5	113.5 113.0 110.5 107.6 108.1 107.2 105.9 105.2 106.7 108.9 108.8 110.4	115'3 114'7 111'3 108'7 110'4 108'4 107'0 107'8 108'8 110'3 110'1 111'5	116°2 116°5 112°5 111°5 111°8 109°1 111°2 111°5 110°8 111°8 111°8

DECLINATION: TABLE OF NORMALS.

Table LII. the Amount of Disturbance equalled or exceeded 7.0 Scale Divisions or 5.0 Minutes of Arc.

					GÖTTI	NGEN H	ours.					
11	12	13	14	15	16	17	18	19	20	21	22	23
	1	<u>'</u>			TOR	ONTO HO	ours.					
5	6	7	8	9	10	11	12	13	14	15	16	17
sc. Div. 123 ' 4 124 ' 3 123 ' 6 123 ' 9 125 ' 2 126 ' 0	sc. Div. 125°0 124°8 124°2 124°7 126°6 126°9	Sc. Div. 124'9 125'0 124'2 125'4 127'5 127'1	Sc. Div. 124.5 124.6 125.4 125.5 127.3 127.6	sc. Div. 125 '4 125 '2 127 '2 126 '1 127 '1 127 '9	sc. Div. 125 * 2 124 * 9 125 * 4 125 * 9 127 * 2 127 * 7	sc. Div. 125 * 2 125 * 0 124 * 5 126 * 5 127 * 3 127 * 1	sc. Div. 127 1 124 8 126 0 125 2 126 1 126 7	sc. Div. 126.7 124.7 126.0 126.0 125.8 126.1	sc. Div. 126.0 126.4 126.0 125.8 125.5 125.5	sc. Div. 126.0 125.8 126.1 125.6 126.0 126.0	sc. Div. 127 1 126 2 125 6 126 5 126 9 126 4	128° 128° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 126° 1
125°5 125°5 123°8 122°5 121°8 121°0 120°9 121°9 118°4 116°5 116°8	126°2 125°7 124°6 123°8 122°9 122°1 122°6 123°3 118°7 117°4 117°9 117°9	127'3 126'3 126'0 123'5 124'0 122'6 123'3 123'5 118'3 117'9 118'9 118'3	127'4 127'4 126'2 125'7 123'5 122'7 122'7 123'3 119'0 119'0 118'3 118'8	127.9 127.6 125.9 125.2 124.7 122.6 123.1 123.0 118.7 118.2 119.0 119.6	128 * 2 127 * 7 127 * 1 126 * 4 124 * 7 123 * 4 124 * 1 123 * 7 119 * 7 119 * 3 119 * 4 118 * 8	127'2 127'0 127'4 127'6 125'2 124'4 124'4 123'9 118'2 118'3 118'9 119'8	126.6 126.3 127.5 126.0 124.0 123.4 124.6 124.2 120.2 118.7 118.5	126.5 126.5 127.0 126.0 125.4 124.1 125.1 123.9 119.0 118.1 117.4 117.9	126.5 126.3 127.2 126.4 125.4 124.7 124.0 123.5 120.0 118.7 117.0 116.9	126'9 127'2 126'6 126'3 125'3 124'3 124'2 123'0 119'8 118'1 118'1 117'3	127'4 127'4 127'7 126'7 125'7 126'0 125'0 124'5 121'9 119'2 117'7 117'6	126 128 128 127 128 127 126 122 119 118
117·2 116·5 114·7 114·7 115·6 113·7 111·6 113·2 113·4 111·7 112·4	118'4 117'8 116'4 116'3 115'3 114'0 115'0 114'0 112'1 113'4	118.5 117.6 117.7 117.1 116.1 115.5 114.9 114.3 112.9 114.7 116.0	119.0 118.3 117.5 117.0 116.3 115.1 114.4 114.0 114.1 112.8 114.6 116.6	119'4 120'0 117'7 117'0 115'7 115'2 114'8 114'9 114'2 113'7 114'6	119.0 118.6 118.6 117.2 115.9 115.1 116.1 115.2 114.2 113.7 114.6 116.3	118'3 118'1 118'7 118'0 116'3 115'9 116'3 115'7 113'1 113'8 114'1 116'3	117:3 118:9 118:3 117:4 116:1 115:6 115:3 114:8 113:7 114:2 113:6 116:5	117.6 117.3 118.4 117.8 116.8 116.3 115.9 115.0 114.0 114.0 113.4 115.3	117.9 117.5 118.7 117.2 116.8 116.4 115.7 114.5 114.0 115.0 113.2 114.5	117'9 118'1 118'5 118'2 117'6 115'1 115'1 115'7 113'9 115'8	119°3 118°6 118°7 118°5 118°4 117°8 116°2 115°0 116°8 115°6 113°1 115°4	118 118 119 120 120 118 117 117 116 114 115

Table LII.—continued.

					GÖTT	INGEN H	IOURS.				
Periods to which the	О	1	2	3	4	5	6	7	8	9	10
Hourly Means		'			TOR	ONTO HO	OURS.			`	
correspond.	18	19	20	21	22	23	0	1	2	3	4
1846:	Sc. Div.	Sc, Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
anuary -	115.2	116.4	118.3	118.6	116.6	114.2	111.5	109.6	110.3	111.1	112.9
February -	115.6	116.4	117.8	117.1	115.2	112.9	110.6	109.3	109.3	110.4	111.8
larch		117.6	120.1	119.5	116.8	112.1	108.7	106.4	106.1	106.4	109.2
April		119.4	119.4	117.7	114.4	109.5	106.7 104.5	104.4	104.7 103.5	105°0	107.4 107.7
May		120.0	120.1	117.7	115.8	111.4	104.3	102 3	103.3	105.3	106.3
fune	11	122.4	120 7	119.9	116.9	111.8	109.0	106.3	105.9	105.7	106.9
Lugust	1	122.0	121.8	119.8	113.9	109.3	105.0	103.7	103.0	104.4	107.2
eptember -	- H .	119'4	118.5	116.4	111.4	107.0	103.8	103.4	104.4	108.2	111.7
October	11	116.2	118.0	117.0	114.8	110.7	107.6	106.4	106.4	108.6	110.3
November -		114.7	117.0	118.4	115.8	113.1	109.8	108.2	108.1	108.9	109.9
December -	114.9	115.2	116.2	117.7	116.2	113.9	110.7	109.4	109.0	109.7	110.7
1847:											
January	115.5	115.7	117.6	117.8	115.7	113.2	110.6	109.2	109.7	111.0	112.3
February	114.4	115.2	115.9	114.0	112.4	109.6	107.1	106.9	107.4	108.4	109.2
March		115.2	117.5	117.3	114.2	109.5	105.0	102.3	102.9	103.6	105.2
April		117.9	117.6	115.7	112.2	106.1	102.3	101.0	101.7	103.9	106.6
May	1	118.7	118.4	116.6	111.2	106.0	104°2 104°1	102.8	102.5	104.3	106.4 105.6
June July		119.0	118.9	118.0	$ \frac{112}{112}.\frac{4}{7}$	107.6	103.8	102.0	102 1	103.4	106.7
Tuly August	11	122.2	120.0	119.3	112.4	106.8	101.4	98.4	99.4	102.7	105.7
September -	15	119.3	120.5	118.4	112.4	107.3	101.2	99.2	100.9	104.1	107.2
October		116.4	118.8	117.9	114.2	109.5	105.1	104.1	104.5	106.2	107.6
November -	113.5	113.9	116.9	115.5	114.3	110.8	106.7	104.5	104.7	105.8	106.5
December •	112.1	113.3	114°7	116.0	115.1	111'4	109.8	107.1	105.7	107.2	107.7
1848:								-			
anuary -	112.9	112.9	116.2	117.7	116.1	112.7	108.3	106.2	105.9	105.9	106.2
Sebruary	H	119.1	122.8	124.9	123.1	119.9	116.5	113.1	111.5	110.8	111.2
March	- 11	123.6	124.9	125.4	121.8	116.6	110.6	108.6	107.2	108.4	110.8
April	11 -	123'1	123.6	122.7	118.3	114'1	110.7	108.0	107.9	109.0	111.1
May	11	125.9	125.1	122.8	116.8	111.3	107.5 108.5	105.8	105.8	107°5 107°7	109.7
une	123.8	125.7	125.6	123.8	118.9	112.6	109.9	106.6	105.7	10/ /	110 4

DECLINATION: TABLE OF NORMALS.

TABLE LII.—continued.

	GÖTTINGEN HOURS.												
11	12	13	14	15	16	17	18	19	20	21	22	23	
	TORONTO HOURS.												
5	6	7	8	9	10	11	12	13	14	15	16	17	
8c. Div. 114'1 112'1 111'0 109'2 109'5 109'5 110'1 110'2 111'2 111'2	sc. Div. 114'3 112'2 112'1 111'2 111'3 111'1 110'3 112'4 112'6 111'4 113'2	sc. Div. 114'9 113'1 112'7 112'0 111'5 111'2 112'4 111'3 111'6 112'9 113'4 114'1	sc. Div. 115 '9 114 '5 112 '8 112 '2 112 '3 112 '8 112 '4 111 '9 113 '9 114 '2 115 '4	Sc. Div. 116 '2 115 '4 113 '7 113 '9 113 '6 112 '7 113 '6 114 '4 111 '4 115 '2 114 '3 115 '7	Sc. Div. 116.4 114.5 114.5 114.6 114.1 114.2 113.8 113.7 113.7 114.2 115.4	sc. Div. 115'4 114'4 114'8 114'7 114'9 114'6 115'4 112'7 112'1 114'8 113'9 115'2	Sc. Div. 115 '2 113 '8 114 '7 114 '8 113 '3 113 '8 115 '0 114 '3 112 '1 114 '2 114 '0 114 '8	sc. Div. 114'2 113'7 114'1 115'5 114'1 112'6 114'4 115'2 112'7 113'5 111'9 113'7	sc. Div. 114'4 114'1 114'8 113'0 111'6 114'3 112'4 114'2 113'9 112'6 114'1	sc. Div. 114'4 114'4 114'8 115'3 113'0 111'6 112'1 113'8 114'5 113'6 113'8 114'3	sc. Div. 115 '6 114 '9 115 '5 112 '8 113 '7 114 '1 112 '1 115 '3 114 '2 113 '9 115 '1	Sc. Div 115 : 3 115 : 5 116 : 5 116 : 6 117 : 1 119 : 3 113 : 9 116 : 5 114 : 9 114 : 3 114 : 4	
113.0 110.4 106.7 109.3 108.1 109.4 108.3 109.8 108.1 107.8	113'6 111'6 108'6 109'7 110'4 109'4 110'5 110'2 110'4 108'4 110'1 111'0	114'0 112'1 109'6 110'4 110'6 109'8 110'0 109'9 109'6 109'3 110'3 111'1	115.2 111.7 110.4 111.4 110.2 109.1 109.8 109.7 110.4 111.9	115.6 112.8 111.1 111.6 110.1 109.8 110.1 111.0 111.5 110.7 112.0 112.8	115'1 112'4 112'0 111'8 109'9 110'0 111'0 110'7 111'0 110'6 113'1 113'3	115.0 112.4 112.0 111.6 110.0 111.4 111.0 111.2 111.0 110.9 114.2 112.7	114.2 111.7 111.8 111.7 111.2 111.3 111.5 110.8 111.9 111.7 111.8 112.4	114'1 112'1 112'0 111'4 111'0 110'0 111'8 112'0 112'5 111'0 112'1	115.0 111.9 111.5 111.3 110.5 109.7 111.4 111.8 111.7 113.1 112.0 112.7	114.8 112.8 112.7 112.6 110.8 110.3 111.4 112.5 112.2 113.4 112.8 112.6	115.0 113.1 112.4 112.8 113.4 112.5 112.0 113.7 112.4 113.0 112.4 112.8	115.1 114.1 113.7 114.2 115.1 114.0 114.1 116.3 114.2 112.2 113.1	
107.4 111.9 112.0 112.9 113.1 113.9	108'9 112'8 114'1 113'8 114'6 115'5	109'3 114'0 113'4 115'2 114'6 116'7	111'3 116'1 114'5 116'9 115'0 116'5	111.6 116.5 116.4 115.8 115.5 116.0	112°2 118°7 117°5 116°7 115°9 115°6	112.2 118.1 117.6 116.4 115.5 116.1	113°3 118°2 119°0 116°8 116°3 116°7	111.9 118.6 118.4 117.8 116.7 116.2	111.8 117.0 119.7 118.4 117.1 115.4	112.4 117.8 119.7 118.3 116.5 115.9	112.2 117.0 119.6 118.0 117.8 117.5	112°2 118°3 118°2 119°4 121°3 119°3	

preceding pages of this volume: it now remains to bring together in one view the evidence which the three observational and the two derived elements furnish of the periodical laws—decennial, annual, and diurnal—which regulate the occurrence of the larger disturbances.

Decennial Period.—In respect to the decennial period, it must be regarded as a fortunate circumstance that the five years of hourly observation, which were commenced before the existence of any inequality of longer duration than a year was suspected, began with 1843, the year of minimum, and closed with 1848, the year of maximum disturbance, so that the variation has been followed through a complete phase. This has been strictly the case in the Declination and Horizontal Forces, and with a single exception in the Vertical Force also, the exception being caused by the interruption of the observations of that element, (for purposes explained elsewhere,) during the months of October, November, and December 1843, January and February 1844. These months have been supplied, in the year ending June 1844, from hourly observations made with the same apparatus in the preceding year, viz. in the months of October, November, and December 1842, January and February 1843, thus rendering the five years of the Vertical Force complete for the investigation of the annual and diurnal variations; but, of course, in regard to the decennial period the months taken from a different year, even though it be the adjacent one, are an imperfect substitute. The effect of this substitution has been in fact, as shown in p. xxix, to swell the aggregate value of the disturbances of the Vertical Force in the year nominally ending June 30, 1844, but really comprising five months taken from a preceding year, so as to make them slightly exceed the aggregate value in the year ending June 30, 1845. A similar slight excess in the aggregate value of the disturbances of the Horizontal Force in the year ending June 1844, over the aggregate value in the year ending June 1845, is shown (p. ix) when the same five months of the preceding year are substituted for its own months; but when, in the case of the Horizontal Force (the observations of which were not suspended, as were those of the Vertical Force), the actual observations throughout the year ending June 1844 are taken, the true progression is restored, and the apparent anomaly disappears.*

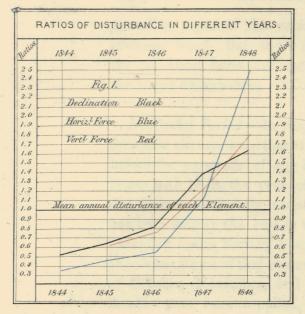
^{*} When the disturbances are taken from the observations of the months actually belonging to the year ending June 1844, the aggregate values of the disturbed observations of the Horizontal Force in the different years are as follow:—

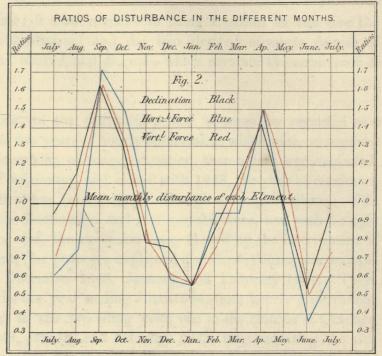
Ratios.

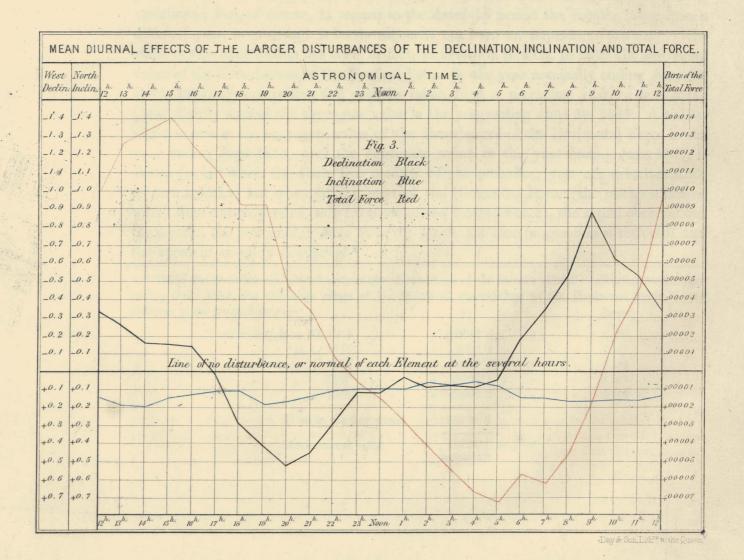
Year ending	June 3	0, 1844	-	-	6016.5	•	-	0.32
,,	,,	1845	•	-	8032.4	-	-	0.47
,,	,,	1846	•	-	$9479 \cdot 2$	•	-	0.55
"	,,	1847	-	-	19700.1	•	-	1.14
,,	,,	1848	-	-	42905.3	•	•	2.49
	Total	in the five	years	-	86133.5			
	Mean	annual va	lue	-	17226.7 =	1.00		

			1
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	-		
•			

ILLUSTRATIONS OF THE MEAN EFFECTS OF THE LARGER DISTURBANCES.







The variations of the three magnetic elements being measured by instruments wholly distinct and unconnected with each other, each element affords an independent evidence of the progressive increase in the aggregate values of the larger disturbances during the period under examination. The sum of the aggregate values of each element in the five years, divided by 5, gives the mean annual value of that element, which we may take in each case as equal to 1.00, for the purpose of comparison with the actual aggregate values in the different years. We have then the ratios of the disturbances of the different elements in the different years as follows:—

					TABLE LII	I.		
			٠		Declination.	Horizontal Force.	Vertical Force.	Mean.
								
Year ending J	une 30), 1844	•		0.25	0.32	0.65*	0.44
"	,,	1845	•	-	0.64	0.47	0.28	0.57
,,	,,	1846	-	•	0.82	0.55	0.73	0.70
,,	,,	1847	-	-	1.39	1.14	1.23	1.25
"	,,	1848	•	-	1.63	2 .49	1.80	1.97

The final column has been added to show the mean ratio of disturbance in each year as derived from the three elements, measured by the aggregate value in each year of all the disturbances which exceeded a certain definite magnitude in each element, the same magnitude being taken throughout the five years.

It is seen by this table that in the year ending June 1847 the ratio of disturbance is above twice as great, and in the year ending June 1848 nearly four times as great, as in either of the years ending June 1844 or June 1845. In the year ending June 1848, which is the year of maximum, the proportion is nearly five times as great as in the year ending June 1844, which is the year of minimum. The evidence of the existence of a decennial period borne by the disturbances of the Declination receives the fullest confirmation from the variations in different years of the disturbances of the Horizontal and Vertical Forces.

Fig. 1. pl. 1. has been drawn in illustration of the progressive increase of disturbance in each of the three elements between the year ending June 1844 and the year ending June 1848. The dotted horizontal line represents the *mean* or *average* annual disturbance in each element, and is the zero line, or unit, with which the *actual* aggregate values of the disturbance of each element in each year are compared: the Declination is represented by a black line, the Horizontal Force by a blue line, and the Vertical Force by a red line. The rate of increase of disturbance is seen to be much slower in the first half than in the second half of the five years.

Annual Period.—The sum of the aggregate values of the disturbances of each element in the five years, divided by 12, gives the average monthly disturbance-value

^{*} In the deduction of this number, five months of the preceding year have been substituted for five months of the year ending June 1844; it has not been included, therefore, in the final column which shows the mean ratios in each year.

for that element, which being taken as = 1.00, and compared with the *actual* monthly disturbance-values, gives the ratios in the following table:—

		${f T}$	ABLE LIV.	•	
Months.]	Declination.	Horizontal Force.	Vertical Force.	Mean.
July -	_	0.94	0.61	0.71	0.75
August -	-	1.16	0.75	1.08	0.99
September	-	1.62	1.71	1.61	1.64
October -	-	1.31	1.48	1.29	1.36
November -		0.78	0.88	0.75	0.84
December -	-	0.76	0.28	0.61	0.65
January -	-	0.57	0.26	0.57	0.57
February -	-	0.84	0.94	0.74	0.84
March -	-	1.11	0.94	1.08	1.04
April	-	1.42	1.20	1.49	1.47
May -	-	0.88	0.80	1.12	1.00
June	-	0.23	0.36	0.20	0.46

The evidence afforded by each of the three observational elements in regard to annual variation is to one and the same effect. January and June are the months of minimum disturbance, September and April the months of maximum disturbance. The aggregate value of the disturbances in the equinoctial months is about three times as great as in the solstitial months. Of the two equinoctial months the value is somewhat higher in each element in September than in April; and of the two solstitial months December is higher than June, also in each of the three elements.

Fig. 2. pl. 1. has been drawn in illustration of the annual variation which has been thus described. The dotted horizontal line is the *mean* monthly disturbance of each element (*i.e.* the sum of the disturbance in the twelve months, divided by 12). The black line for the Declination, the blue line for the Horizontal Force, and the red line for the Vertical Force, show in each case the variation in the proportion which the actual disturbances in each month bear to the *mean* monthly disturbance in the same element. The correspondence of the three elements could scarcely be more perfect.

The annual variation which has been thus deduced has reference exclusively to the variable amount in the different months of the sums of the aggregate values of the disturbances of each element, without distinguishing apart or separating the disturbances which cause easterly deflections and those which cause westerly deflections; or those which increase and those which decrease the Horizontal and Vertical Forces. When this separation is made, we continue to find that each of the two portions into which the disturbances of each element are divided, exhibits distinctly and notably the same general features which have been derived from their conjoint consideration. The equinoxes are in all cases the epochs of maxima and the solstices of minima. But when we study more carefully the relative prevalence of disturbances of particular

character at different periods of the year,—which we may do by forming tables of the relative proportion which the aggregate values in the different months of the easterly disturbances bear to the aggregate values in the same months of the westerly disturbances, and the disturbances which decrease the force bear to those which increase it,—we find that indications present themselves of an annual variation of a different kind from that which has been hitherto described, namely, an annual variation in the character of the disturbances of two at least of the elements which have been observed; and although a greater length of time and a greater amount or continuance of observation may be required for the satisfactory establishment of such a periodical variation, its present indications ought not to be overlooked, since the range of the variation is of considerable magnitude, and its systematic character as distinctly marked as could well be expected in an annual variation derived from not more than five years of repetition. The elements in which these phenomena are most distinctly noticeable are the Declination and the Vertical Force, and the correspondence between the indications of these two elements is in many respects very remarkable. In both elements, when the relative proportions are taken,—in the Declination, of the aggregate values in the different months of easterly and of westerly disturbances; and in the Vertical Force, of disturbances which decrease and disturbances which increase the force,—we find that in both cases the proportions vary from a minimum at the southern solstice to a maximum at the northern solstice, the equinoxes being intermediate. At the northern solstice easterly disturbances are in considerable excess, as are disturbances which decrease the Vertical Force; at the southern solstice, the excess is on the other side; westerly disturbances then predominate, as do the disturbances which increase the Vertical Force. The relative proportion of the aggregate values of easterly to westerly disturbances of the Declination, and of disturbances which decrease the Vertical Force to those which increase it, varies from the one solstice to the other, approximately, as three to one, and in both elements nearly alike.

In the Horizontal Force the disproportion between the values of the disturbances which increase the force and those which decrease it is so great (decreasing disturbances greatly preponderating at all periods of the year) that a variation corresponding to that of the two other elements is not so simply arrived at; but it may be stated generally that the proportion of decreasing disturbances is greater at the epoch of the southern solstice than at that of the northern solstice.

Diurnal Variation.—Before we proceed to examine the diurnal variation of the Declination, Inclination, and Total Force which it is the average effect of the larger disturbances to produce, it may be desirable to show the proportions in which the disturbances of the three observed elements occur at the different hours. This is expressed in the following table by the ratio which the aggregate values in the five years of the disturbances at each particular hour bear to the mean or average disturbance at all the hours in the same five years taken as the unit.

TABLE LV.

Toronto Astronomical		Toronto		
Hours.	Declination.	Horizontal Force.	Vertical Force.	Civil Hours
18	1.02	1.00	1.51	6 a.m.
19	1.12	1.40	1.12	7 a.m.
20	1.27	1.50	0.80	8 a.m.
21	1'11	1.00	0.54	9 a.m.
22	0.87	1.00	0.36	10 a.m.
23	0.66	0.00	0.34	11 a.m.
0	0.49	0.87	0.46	Noon.
1	0.30	0.76	0.63	1 p.m.
2 3	0.40	0.66	0.77	2 p.m.
3	0.40	0.66	0.87	3 p.m.
4	0.23	0.61	1.04	4 p.m.
5	0.26	0.66	1.07	5 p.m.
4 5 6 7	0.84	0.29	1.01	6 p.m.
7	0.98	0.76	1.02	7 p.m.
8 9	1.25	0.75	0.89	8 p.m.
9	1.85	0.90	0.74	9 p.m.
10	1.55	1.03	0.82	10 p.m.
11	1.25	1.14	0.93	11 p.m.
12	1.35	1.22	1.39	Midnight.
13	1.52	1.28	1.28	1 a.m.
14	1.21	1.60	1.61	2 a.m.
15	1.13	1.37	1.73	3 a.m.
16	1.34	1.14	1.21	4 a.m.
17	1.02	1.02	1.41	5 a.m.

From the systematic increase and decrease of the ratios at the different hours, it is obvious that the disturbances of each element, when viewed on the average of a sufficient body of observations, are regulated by laws which have a diurnal period. The diurnal variation thus presented is far, however, from being identical in each of the three elements. The maximum disturbance takes place, indeed, in all the elements during the hours of the night, and the minimum disturbance during the hours of the day; but the particular hours of maximum and minimum are different in the three The hour of maximum in the Declination, for example, is 9 P.M., when the disturbances of the Horizontal and Vertical Forces are both even less than the hourly average: and the Horizontal and Vertical Forces do not reach their hours of maximum until, respectively, 2 and 3 A.M., when the disturbances of the Declination have notably declined. So in respect to the hour of minimum: that of the Declination, 1 P.M., is nearly midway between that of the Vertical Force at 11 A.M. and that of the Horizontal Force at 4 P.M., the disturbance of the Horizontal Force being still high when that of the Vertical is a minimum, and the disturbance of the Vertical Force being still high when that of the Horizontal Force is a minimum. Speaking generally, the disturbances of the three elements are above the average in the hours of the night and early morning, and below the average during the hours of the day; to the latter, however, there is an exception in the Vertical Force, which is above the average from 4 to 7 P.M. In the Declination the aggregate value of the disturbances at the hour of

maximum is about six times as great as at the hour of minimum; in the Horizontal Force, about 2.7 as great; and in the Vertical Force, about five times as great.

In the ratios of the Declination-disturbances at the different hours shown in the preceding table we have the joint effects of two classes of disturbances, those which produce easterly and those which produce westerly deflections; and in the ratios of the disturbances of the Horizontal and Vertical Forces at the different hours, we have the further complication that the variations of the Horizontal and Vertical Forces do not bear a simple relation to those of the theoretical equivalents to which they are due,—viz. the Inclination and the Total Force,—but involve quantities dependent on the resolution of forces, which, when the Inclination is great, as it is at Toronto, have a tendency to mask the simplicity of the variations of the Inclination and of the Total Force, as they would appear if they were the subjects of direct observation. In the following table, therefore, are placed the proportions at the different hours in which the six classes of phenomena respectively vary, viz. the disturbances which produce easterly and those which produce westerly deflections, those which increase and those which decrease the Inclination, and those which increase and those which decrease the Total Force.

TABLE LVI.

			LADILE	14 1 1 .			
Toronto			RATIOS OF I	ISTURBANCE.			
Astrono-	Of the D produ	eclination acing	Of the In	nclinatio n acing	Of the T	Toronto	
Hours.	Easterly Westerly Increase of Inclination.		Decrease of Inclination.	Increase of Force.	Decrease of Force.	Hours.	
18	0.45	1.82	0.85	0.83	0.27	1.91	6 a.m.
19	0.32	2.53	1.29	0.21	0.26	1.91	7 a.m.
20	0.56	2.28	1.14	0.65	0.37	1,15	8 a.m.
21	0.51	2.25	1.02	1.37	0.55	0.65	9 a.m.
22	0.58	1.62	0.96	1.47	0.52	0.58	10 a.m.
23	0.38	1.01	0.89	1.80	0.39	0.07	11 a.m.
0	0.54	0.80	0.83	1.75	0.67	0.04	Noon.
1	0.21	0.41	0.87	1.40	1.25	0.10	1 p.m.
2	0.50	0.65	0.65	1.95	1.79	0.08	2 p.m.
3	0.55	0.65	0.41	1.36	2.21	0.06	3 p.m.
4	0.35	0.80	0.61	1.46	2.77	0.07	4 p.m.
5	0.44	0.71	0.79	1.32	2.96	0.04	5 p.m.
6	1.02	0.22	1.04	0.45	2.39	0.04	6 p.m.
7	1.44	0.39	1.14	1.05	2.56	0.09	7 p.m.
8	1.95	0.58	1.12	0.22	1.99	0.09	8 p.m.
9	3.09	0.55	1.12	0.28	1.53	0.31	9 p.m.
10	2.41	0.45	1.18	1.39	0.81	0.83	10 p.m.
11	2.02	0.27	1.19	0.84	0.23	1.19	11 p.m.
12	1.76	0.85	1.10	0.82	0.46	2.14	Midnight.
13	1.79	1.18	1.32	0.70	0.26	2.57	1 a.m.
14	1.37	1.00	1.33	0.34	0.55	2.40	2 a.m.
15	1.28	0.94	1.05	0.48	0.58	2.81	3 a.m.
16	1.48	1.21	0.90	0.48	0.18	2.48	4 a.m.
17	0.91	1.23	0.76	0.22	0*28	2.24	5 a.m.

We learn from this table that the laws which regulate the occurrence of easterly and westerly disturbances of the Declination are not on the one hand similar, nor on the other hand are they always complementary to each other. Thus from 1 p.m. to 5 P.M. both classes are considerably below the average, and from 1 A.M. to 5 A.M. both classes, with a slight exception, are above the average; whilst from 6 P.M. to 11 P.M. easterly disturbances greatly exceed, and westerly fall greatly short, of the average; and from 6 a.m. to 11 a.m. westerly exceed and easterly fall short of the average. In the Inclination and Total Force the complementary character of the opposite affections of each element is somewhat more extensively manifested: thus, the disturbances which increase the Inclination are below the average from about noon and the early hours after noon, when those which decrease it are above the average; and are below the average from about midnight and the early hours after midnight, when those which increase the same element are above the average. In the Total Force, from 1 A.M. to 8 A.M. the disturbances which increase the force are greatly above, as those which decrease the force are greatly below, the average,—a contrast which is reversed from 1 A.M. to 8 A.M., the disturbances which decrease the force being then greatly above, whilst those which increase it are greatly below, the average. In neither of the two elements, however, does the complementary character exclusively prevail. It may be remarked, that in all the instances which have been thus brought into view, treating successively the diurnal variations of the disturbances of each of the three elements, the parallel cases which have been cited, whether of identity or of contrast, fall, without exception, on homonymous hours—a circumstance which affords additional evidence of the systematic character of the affections of which we are treating.

There does not appear to be any uniform cotemporaneous connection between the prevalence of either easterly or westerly Declination-disturbance, and that of disturbances which either increase or decrease the Inclination or the Total Force. Thus, for example, the hours at which the disturbances which increase the Total Force are most notably above the average occur from 1 p.m. to 9 p.m.; whilst we find that for half that period, or from 1 p.m. to 5 p.m., the Declination-disturbances are characterised by a very low proportion of easterly disturbances, and for the other half of the period, or from 6 p.m. to 9 p.m., by a very high proportion of easterly disturbances; and, without multiplying instances of dissimilarity, it may be remarked generally, that the more the six classes of disturbance are examined and compared with each other, the less reason does there appear to conclude that there is any uniform interaccompaniment of the variations of different elements.

As the instrument by which the variations of the Declination are observed is more simple in construction than those required for the variations of the Inclination and Total Force, and the disturbances of the Declination are therefore more easily observed and more generally known, a somewhat disproportionate consideration has been frequently given to them in the discussion of these phenomena, which it may be

desirable briefly to remark upon. Thus the knowledge of the magnetic disturbances having been chiefly drawn hitherto from those of the Declination, it has been very generally and very naturally imagined that the early hours of the night, or from 8 p.m. to 11 P.M., are those at which magnetic disturbances principally take place; that about 11 p.m., or a little after, they begin to subside, disappearing almost wholly in the daytime, and reappearing again possibly the following evening, at the same hour as on the preceding evening, in supposed analogy with certain peculiar atmospheric disturbances, which manifest a tendency to recur at the same hours on successive days. It is in this supposed analogy that the term of magnetic storms appears to have originated. An examination of the observations of the three elements at but a single station, as Toronto for example, teaches us that this view requires to be considerably modified. The disturbances of the Declination, which reach a maximum at 9 r.m., have indeed already subsided considerably at 11 p.m., but those of the Inclination show no abatement until about 2 A.M., whilst those of the Total Force, which are much below their average at 9 p.m., increase progressively to their maximum, which is only reached at 3 A.M., or nearly six hours after the maximum of the Declination disturbances has taken place. In like manner the hours of the afternoon, in which the Declination is but little disturbed, and which have been supposed in consequence to be hours in which an intermission of disturbance takes place, are seen by the table to be precisely those hours at which the disturbances which increase the Total Force have their principal development, being then in the proportion of nearly ten to one when compared with the homonymous hours after midnight. When these remarkable phenomena are more fully studied, the aspect they present is that of a disturbance continued frequently through several successive days, changing from one element to another, and affecting each at different hours and in different modes, in conformity with laws the average operation of which it has been the object of this investigation to ascertain; and wearing the appearance consequently, when only a single element is regarded, of a limitation to those hours when that element in particular is affected, but which appearance ceases when the phenomena are more generally apprehended.

It was the supposed analogy between magnetical and atmospherical disturbances which led, in the commencement of the British colonial observatories, to the *simultaneous* observation and record of these two great and, as we have now reason to believe, distinct branches of natural phenomena; and as the inquiry advances we are continually becoming acquainted with additional circumstances to strengthen the persuasion, that the causes of these occasional and previously supposed "irregular" manifestations of disturbing magnetical influence are to be sought in more distant sources than in variations of the meteorological phenomena.

There is another misapprehension in regard to the nature of the occasional disturbances, which has followed very naturally from the limitation of the view to the disturbances of a single element. An inference has sometimes been drawn in favour of a local origin of a particular disturbance (in contradistinction to the general fact of

their simultaneous occurrence at extremely distant parts of the globe), from the circumstance that though the disturbance was manifested by the Declination at one station, no indication of it was shown by the cotemporaneous observations of the Declination at another and a distant station. Now, simultaneity at stations separated by considerable intervals of longitude implies a difference in the solar time; and the observations at Toronto show that a difference in the solar time may determine the question whether a disturbance, which may nevertheless be common to both stations. may or may not be traceable by simultaneous observations of a single element only. Towards the attainment of a just conclusion, therefore, in regard to a possible local origin, it is indispensable that a more extensive generalization should be made, and that cotemporaneous affections of the three elements should be brought into the comparison. Nor can this condition of the inquiry be dispensed with even in comparing the phenomena at stations under the same meridian, but separated by large intervals of latitude, unless it be first shown that the same law of solar hours prevails at both stations in regard to the occurrence of the disturbances of each particular element. It need scarcely be said that the general simultaneity of the disturbances has a very important bearing upon their theory, inasmuch as it militates decidedly against the supposition of their originating in atmospherical peculiarities, and tends to assign them, with far greater probability, to a cosmical source. That some disturbances may have a local origin is undoubtedly possible, but no such case has yet, I believe, been established on adequate evidence.

For the purpose of viewing in its simplest form, and expressed in numerical value, the influence which, on a daily average, the larger disturbances exercise on the Declination, Inclination, and Total Force, we must revert to the aggregate values in the five years which supplied the ratios of disturbance at the different hours in each of the six classes of phenomena contained in Table LVI. From these values we obtain readily and immediately for each hour the excess in the aggregate amount of easterly over westerly, or of westerly over easterly, deflection, and of disturbances which increase or decrease the Inclination or the Total Force over those which respectively decrease or increase those elements. Hence we can easily form a table containing, for each of the elements at every hour, the numerical excess in the aggregate values of whichever kind of disturbance predominates at that hour; and dividing the excess by 1550, which is the number of days of observation in the five years, we have the mean effect corresponding to the larger disturbances of each of the elements at the different hours, or the average diurnal variation of each element due to the larger disturbances. This is shown in the following table, illustrated by Fig. 3. pl. 1., in which the diurnal variations of Declination and Inclination are expressed in decimals of a minute of arc, and that of the Total Force in parts of the Total Force at Toronto, which in absolute value and employing British units may be taken with sufficient approximation at 13.9.

TABLE LVII.

Toronto	Mean Diurnal Va	riation occasioned by th	e larger Disturbances.	Toronto	
Astronomical Time.	Declination.	Inclination.	Total Force.	Civil Time.	
н.	,	,	Parts of the Total Force.		
18	0°29 W.	+0.10	- 000092	6 a.m.	
19	0.41 W.	+0.18	- 0000092	7 a.m.	
20	0.52 W.	+0.16	- 000047	8 a.m.	
21	0.46 W.	+0.13	- 000032	9 a.m.	
22	0.30 W.	+0.10	000008	10 a.m.	
23	0°11 W.	+0.09	+ .0000004	11 a.m.	
0	0°11 W.	+0.09	+.000012	${f Noon}.$	
1	0.03 M.	+0.09	+ 000027	1 p.m.	
2	0.09 M.	+0.02	+ 000042	2 p.m.	
$\frac{2}{3}$	0.08 W.	+0.07	+ .000024	3 p.m.	
4 5 6 7 8	0.09 M.	+0.02	+ .000068	4 p.m.	
5	0.04 W.	+0.08	+ .000073	5 p.m.	
6	0.18 E	+0.14	+ .000028	6 p.m.	
7	0°34 E.	+0.14	+ '000062	7 p.m.	
8	0.52 E.	+0.16	+ '000047	8 p.m.	
9	0.87 E.	+0.16	+.000016	9 p.m.	
10	0.61 E.	+0.12	- 000022	10 p.m.	
11	0.53 E.	+0.19	000047	11 p.m.	
12	0.33 E.	+0.14	- 000098	Midnight	
13	0.26 E.	+0.18	- 000125	1 a.m.	
14	0°17 E.	+0.19	- 000132	2 a.m.	
15	0.16 E.	+0.14	-:000138	3 a.m.	
16	0.15 E.	+0.15	- 000123	4 a.m.	

From this table we find that the range of the diurnal variation of the Declination representing the influence of the larger disturbances is from 0'.52 W. at 8 A.M. to 0'.87 E. at 9 P.M. (or the whole range has an extent of 1'.39); that of the Inclination, from a minimum increase of 0'.05 at 2 P.M. to a maximum increase of 0'.19 at 2 A.M. (or a total extent of 0'.14); and that of the Total Force, from a maximum decrease of .000138 at 3 A.M. to a maximum increase of .000073 at 5 P.M. (or a total extent of range of .000211 parts of the Total Force at Toronto).

As the larger disturbances of each element which have been separated by the processes and subjected to the analysis described in this communication, can by no means be supposed to include the whole of the disturbances of the class to which they belong, we can only regard the extent of the diurnal variation as stated above to be in each case a minimum limit, which would be certainly somewhat exceeded if by any mode of proceeding we could succeed in separating the minor effects of the same causes; but we have no reason to suppose that the epochs of maxima and minima or the laws of intermediate progression would sustain any material alteration thereby.

As the aggregate values of the disturbances are taken from the five years which include a complete quinquennial or semi-decennial period, the mean diurnal variation

deduced from them must be considered as also subject to a small decennial variation, analogous to that which has been found to exist in the ordinary solar-diurnal variation. And as the sums of the variation-values at the different hours, taken with their proper signs, in no case equal zero, but have a sensible magnitude in each element, the absolute values of the three elements must also be affected with a very small cyclical variation due to the disturbances, of which the period will also be decennial.

LUNAR-DIURNAL VARIATION.

The observations employed in the investigation on which we now enter are the six years of hourly observations of the Declination from July 1st, 1842, to June 30th, 1848, and the five years of hourly observations of the Horizontal and Vertical Forces commencing July 1st, 1843, and ending June 30th, 1848, but having in the first year of the Horizontal and Vertical Forces the months of October, November, December 1842, January and February 1843, substituted for the same months in the subsequent year, during which the observations of the Vertical Force were suspended.

The larger disturbances of each element having been marked for omission, and the hourly normals (excluding the observations so marked) computed as already described, the retained observations were then characterised in reference to their lunar relation by small figures signifying the lunar hour to which each observation most nearly corresponded. For this purpose the time of the moon's meridian passage at Greenwich was taken from the Nautical Almanac, and corrected for the difference of longitude, so as to give the time of the moon's passage of the astronomical meridian at Toronto in the mean solar time of the station. The difference of time corresponding to the difference between the meridians of Toronto and Göttingen was then applied, so as to give the mean Göttingen time of the moon's passage of the astronomical meridian at Toronto. The observation at the Göttingen hour nearest to the time thus computed was then marked with 0^{π} , signifying that it was the nearest observation to the moon's upper culmination, and from which its distance could not exceed half an hour. The time of the moon's inferior passage was then computed in a similar manner, and the observation at the Göttingen hour nearest to it was marked 12ⁿ. The intermediate hours received corresponding markings, except that when thirteen solar hours, and consequently thirteen observations, were comprised within twelve lunar hours, that observation was omitted which fell most nearly equidistant between the epochs of two exact lunar hours. The monthly tables were thus marked for the lunar hours before they were returned from myself to the office, and were considered to be prepared for re-arrangement in tables conforming to lunar time; but instead of the observations themselves, the differences at each hour between the scale readings observed and the normals at the same hour (Tables X., XXV., and

LII.) were entered in the lunar tables, by which process the diurnal and other variations depending on the period of the year and the hour of the solar day were, in great part at least, eliminated. The differences were marked with a + or - sign according as the scale reading at the time of observation was greater or less than the normal, the entries having a + sign implying in the case of the Declination a westerly deflection of the north end of the magnet, and those having a - sign implying the converse.

The means were then taken in every month, at every lunar hour, the signs being regarded; the monthly means were then collected into yearly means; and finally, the means at each lunar hour in the six years of observation were collected as shown in the subjoined table, in which the entries are expressed in scale divisions, one scale division equalling 0'·721 of arc.

TABLE LVIII.

Lunar			Year endin	g June 30,			Means.	Lunar
Hours.	1843.	1844.	1845.	1846.	1847.	1848.	arcans.	Hours.
н. О	Sc. Div. -0°20	Sc. Div. -0'42	Sc. Div. -0'45	Sc. Div. -0.40	Sc. Div. -0.46	Sc. Div. -0.37	Sc. Div. -0.38	н.
1	-0.11	-0.31	-0.18	-0.37	-0.64	-0.59	-0.35	1
2	-0.08	-0.58	+0.04	-0.58	-0.39	-0.31	-0.22	2
3	-0.09	-0.08	-0.07	0.00	-0.36	-0.13	-0.12	3
4	+0.26	+0.09	+0.31	+0.08	+0.13	+0.58	+0.19	4
5	+0.39	+0.09	+0.42	+0.52	+0.20	+0.45	+0.35	5
6	+0.66	+0.40	+0.23	+0.77	+0.12	+0.48	+0.45	6
7	+0.21	+0.29	+0.47	+0.26	+0.31	+0.29	+0.40	7
8	+0.17	+0.26	+0.08	+0.50	+0.09	+0.10	+0.50	8
9	-0.14	+0.21	-0.31	+0.31	-0.23	+0.35	+0.03	9
10	-0.36	-0.24	-0.57	-0.22	-0.40	+0.04	-0.29	10 11
11	-0.51 -0.59	-0.33	-0.66	-0.54	-0.24 -0.52	-0.49	-0.46	12
12	-0.39 -0.37	$ \begin{array}{c c} -0.48 \\ -0.27 \end{array} $	-0.51 -0.45	-0.51 -0.34	-0.32 -0.29	$-0.22 \\ -0.44$	$\begin{array}{c c} -0.47 \\ -0.36 \end{array}$	13
13 14	-0.37	-0.27 -0.31	-0.45 -0.24	-0.34 -0.32	$-0.29 \\ +0.07$	-0.44	-0.36	14
	+0.07	-0.31 -0.14	+0.04	-0.32 -0.12	$+0.07 \\ +0.52$	-0.10	+0.04	15
15 16	+0.15	+0.22	+0.31	+0.14	+0.32 +0.43	+0.20	+0.04	16
17	+0.37	+0.45	+0.21	+0.19	+0.22	+0.49	+0.42	17
18	+0.43	+0.74	+0.65	+0.39	+0.47	+0.28	+0.54	18
19	+0.56	+0.25	+0.25	+0.51	+0.22	+0.39	+0.36	19
20	+0.59	+0.12	+0.35	+0.20	+0.52	+0.02	$+0.30 \\ +0.21$	20
20	+0.08	+0.12	+0.10	-0.15	-0.51	-0.30	-0.06	$\frac{20}{21}$
$\frac{21}{22}$	-0.56	-0.05	-0.04	-0.53	-0.42	-0.42	-0.24	$\frac{22}{22}$
23	-0.59	-0.37	-0.33	-0.25	-0.31	-0.34	-0.32	23
-3					- 0-			

Representing the mean of the six years by the usual formula of sines and cosines, we have the coefficients of the several terms as follows, expressed in seconds of arc, a being counted in hours (multiplied by 15°) from the time of the moon's upper culmination.

TABLE	LIA.

Arguments.	Constant.	cos a.	sin a.	$\cos 2 a$.	$\sin 2 a$.	$\cos 3 a$.	sin 3 a.	$\cos 4 a$.	sin 4 a.	cos 5 a.	sin 5 a.	cos 6 a.
Coefficients	$\Lambda_0 =$	$\Lambda_1 =$	$B_1 \equiv$	$\Lambda_2 =$	$B_2 =$	Λ_3 $=$	$B_3 =$	$A_i =$	$B_4 =$	$A_5 =$	$B_5 =$	$A_6 =$
Coefficients	0. 0	+0.50	_″ _″*03		+0.45	+1*84	-0.35	+1.51	+0.29	+0.61		-0.22
Arguments.	$\sin 6 a$.	cos 7 a.	sin 7 a.	cos 8 a.	sin 8 a.	cos 9 a.	sin 9 a.	cos 10 a.	sin 10 a.	cos 11 a.	sin 11 a.	sin 12 a.
Coefficients	$B_6 =$	$\Lambda_7 =$	$B_7 =$	$\Lambda_{ m s}$ $=$	$B_8 =$	$\Lambda_{\scriptscriptstyle 9} =$	$B_9 =$	$A_{10} =$	$B_{10} =$	\mathbf{A}_{11} =	$B_{ii} =$	$A_{12} =$
	+0.24		+0.08	+0.16						+0.49	+0.28	

The coefficient of principal magnitude is $A_2 = -19'' \cdot 18$, whose argument is $\cos 2 a$. The same coefficient calculated for the different years is as follows:—

TABLE LX.

								"
Year end	ling June	30th,	1843	-	•1		•	-19.35
2:	,	,,	1844	-	•	-	-	-17.61
,	,	,,	1845	-	-		-	-21.05
,	,	,,	1846	-	-		-	-20.22
,	,	,,	1847	-	-		-	-19.04
,	,	,,	1848	-	-		-	-18.53
And from the mea	n of the s	ix yea	ırs	-	-		-	-19.18

Whence we obtain the probable error of -19.18 (the value of A_2 from the mean of the six years) = ± 0 "·34.

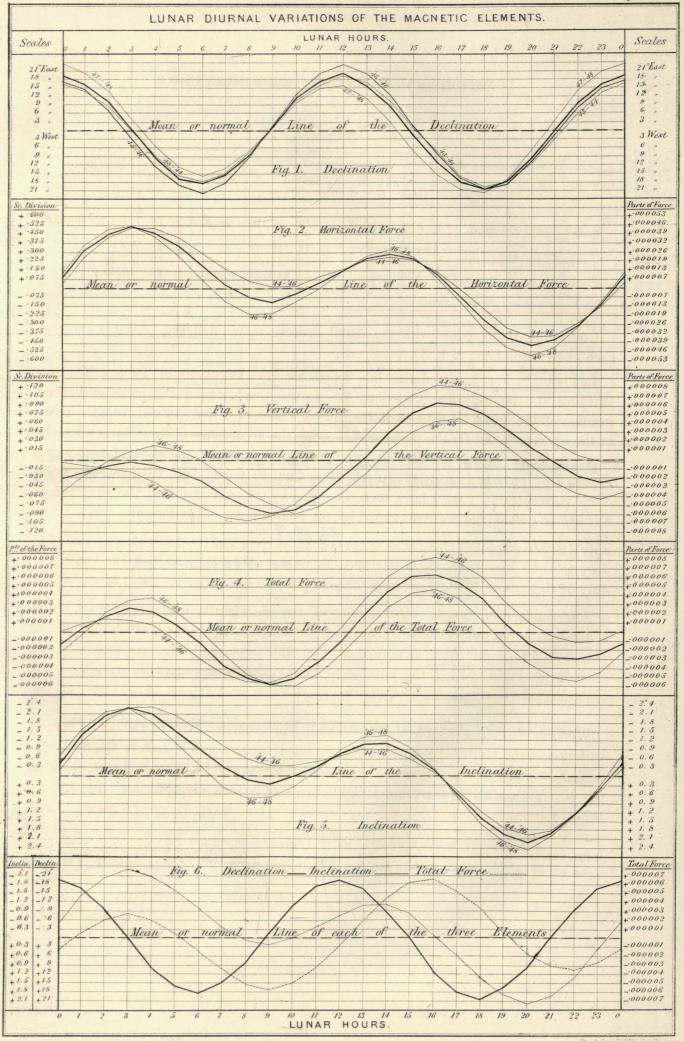
With the two first terms of this formula, viz.—

 $\Delta_x = 0'' \cdot 0 + 0'' \cdot 20 \cos a - 1'' \cdot 03 \sin a - 19'' \cdot 18 \cos 2a + 0'' \cdot 45 \sin 2a$ or its more convenient equivalent,

$$\Delta_x = 0^{"\cdot}0 - 1^{"\cdot}05 \sin(a + 348^{\circ}52') + 19^{"\cdot}186 \sin(2a + 271^{\circ}21')$$

we obtain the deflections of the north end of the magnet at the several lunar hours as follows:—

	•		



Lunar Hours,			Deflections.	Lunar Hours. Deflections.		Lunar Hours. Deflections.	
22 23 0 1 2 3	9.29 to the East. 15.92	4 5 6 7 8 9	9°19 to the West. 15°89 ,, 18°14 ,, 15°34 ,, 8°20 ,, 0°42 to the East.	10 11 12 13 14 15	" 10.67 to the East. 17.30	17 18 19 20	10.77 to the West. 17.78

TABLE LXI.

Comparing these values with the actual deflections, we find the probable error at each observation hour $\pm 1^{\prime\prime}.37$.

In Plate II., Fig. 1., the darker line represents the deflections in Table LXI. constituting the lunar-diurnal variation, the dotted line showing the mean or normal position of the magnet. The variation thus represented is that derived from the mean of the six years; and for the purpose of showing the accordance of the results when the whole period of six years is divided into three portions, each consisting of two years,—viz., July 1842 to June 1844, July 1844 to June 1846, and July 1846 to June 1848,—the corresponding curves have been computed by the subjoined formulæ, obtained as already described, and are represented by the fainter lines. The formulæ are—

```
July 1842 to June 1844, \Delta_x = +0^{"\cdot}41 - 2^{'\cdot}09 \sin(a + 291^{\circ}) - 18^{"\cdot}1 \sin(2a + 87^{\circ}\cdot7)

July 1844 to June 1846, \Delta_x = +0^{"\cdot}30 + 3^{"\cdot}04 \sin(a + 78^{\circ}7') + 20^{"\cdot}6\sin(2a + 270^{\circ}\cdot1)

July 1846 to June 1848, \Delta_x = -0^{"\cdot}58 - 5^{"\cdot}23\sin(a + 53^{\circ}5') + 18^{"\cdot}9\sin(2a + 276^{\circ}\cdot1)
```

The number of hourly observations of the Declination made in the six years amounted to 42,888; of these, 2,345 were disturbed to an amount which equalled or exceeded 5'0 of arc from the normal at the same hour, and were consequently excluded; leaving 40,543 as the number of observations from which the results of the lunar-diurnal variation have been derived.

Horizontal Force.—Table LXII. exhibits, in columns 2 to 6, the mean hourly variation of the Horizontal Force at the different lunar hours in each of the five years ending June 30, and in column 7 the mean of the five years. The lunar influence at the several lunar hours is shown in decimals of a scale division, one such division being approximately 000087 parts of the whole Horizontal Force at Toronto. The sign + implies that the force is increased, and — that it is decreased, by the lunar influence.

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In the Year ending June 30, Lunar Mean of the Lunar Hours. Five Years. Hours. 1844. 1848. 1845. 1846. 1847. (2) (3) (6)(1)(4) (5)(7) (8)Sc. Div. -0'05 Sc. Div. -0'07 Sc. Div. +0'44 sc. Div. +0'10 Sc. Div. +0.70 $^{\text{Sc. Div.}}_{+0.22}$ 0 0 +0.48 +0.70+0.01+0.09+0.68+0.39+0.42 2 +0.68+0.59+0.11+0.29+0.422 3 +0.42+0.48 +0.083 +0.71+0.50+0.444 +0.58+0.28+0.22+0.00+0.19+0.274 +0.16+0.68+0.21+0.43+0.745 6 7 +0.44+0.09 +0.43 6 7 -0.23-0.03+1.11+0.27-0.13-0.20 +0.72-0.25+0.21+0.078 -0.16+0.59-0.31-0.24-0.19-0.06 +0.28 9 -0.23+0.24-0.12-0.79-0.129 -0.10 -0.4310 -0.62+0.23-0.14+0.2010 +0.1711 -0.02+0.32+0.36+0.39-0.2211 12 -0.28+0.37+0.12 -0.02-0.31 -0.02 12 +0.23+0.4713 +0.11+0.11+0.64+0.3113 +0.06+0.84+0.18-0.09+0.40+0.2814 14 +0.06 +0.04+0.20 +0.23-0.06+0.7315 15 +0.32 0.00 +0.13+0.2816 -0.01+0.1416 +0.48 -0.17-0.470.00 +0.33+0.0317 17 -0.08-0.18 -0.13-0.24-0.47-0.2218 18 -0.24 -0.13 -0.80-0.21-0.33-0.40 19 19 20 -0.19-0.70 -0.11-0.55-1:33 -0.5820 -0.8221 -0.19-0.31-0.09-1.07-0.5021 -0.22+0.09 -0.6522 -0.28-0.3022 -0.44-0.08-0.46-0.12+0.34-0.18-0.11

TABLE LXII.

We may represent the values in column 7 of Table LXII. (or the variation of the Horizontal Force at the several lunar hours on the average of the five years of observation) by the first terms of the usual formulæ for periodical functions; viz.,

$$\Delta_x = A_0 + A_1 \cos a + B_1 \sin a + A_2 \cos 2a + B_2 \sin 2a$$
;

and by substituting in this formula the numerical values of the coefficients obtained from the numbers in column 7, it becomes

 $\Delta_x = +.05 - .024 \cos a + .214 \sin a + .0775 \cos 2a + .323 \sin 2a$, or its more convenient equivalent,

$$\Delta_x = +.05 + .215 \sin(a + .353^{\circ}.6) + .3324 \sin(2a + .13^{\circ}.5)$$

the coefficients being decimals of a scale division, and a reckoned in hours (multiplied by 15°) from the time of the moon's superior culmination. By this formula we obtain the curve which is shown by the stronger line in Plate II., Fig. 2.; and for the purpose of showing the degree of confidence to which this curve is entitled as an approximate representation of the variation produced in the Horizontal Force by the moon in the course of a lunar day, the variation in the different years in columns 2 to 6 of Table LXII. have been so combined as to form two separate means, one representing the columns headed 1844, 1845, and 1846, and a second representing

the columns headed 1846, 1847, and 1848,—the years 1844 and 1845 having double weight assigned to them in the first mean, and those in the columns headed 1847 and 1848 double weight in the second mean. The formulæ representing these separate means are—

For 1844 to 1846, $\Delta_x = +.088 + .243 \sin (a + 347^{\circ}.6) + .277 \sin (2a + 4^{\circ}.6)$ For 1846 to 1848, $\Delta_x = +.013 + .192 \sin (a + 355^{\circ}.0) + .395 \sin (2a + 19^{\circ}.2)$

The curves respectively computed by these formulæ are shown by the fainter lines in Fig. 2., in which the stronger line has been already noticed as being derived from the mean of the five years.

The number of hourly observations of the Bifilar Magnetometer employed in this investigation is 34,303.

Vertical Force.—Table LXIII. exhibits, in columns 2 to 6, the mean hourly variation of the Vertical Force at the different lunar hours in each of the five years ending June 30, and in column 7 the mean variation in the five years. The lunar influence at the several lunar hours is expressed in decimals of a scale division, one scale division being approximately '000065 parts of the whole Vertical Force at Toronto. The sign + implies an increase, and — a decrease, of the force from the lunar influence.

TABLE LXIII.

Lunar		In the Year ending June 30,							
Hours.	1844.	1845.	1846.	1847.	1848.	Five Years.	Hours		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)		
^	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.			
0	+0.08	+0.02	-0.05	-0.03	+0.03	+0.05	0		
1	+0.09	-0.03	+0.06	0.00	+0.02	+0.03	1		
2	+0.05	-0.07	-0.16	-0.09	-0.18	-0.10	2		
3	-0.11	0.00	-0.07	+0.18	-0.06	-0.01	3		
4	-0.09	-0.01	-0.01	+0.13	+0.08	+0.02	4		
5	+0.01	-0.05	-0.00	+0.04	+0.05	0.00	5		
6	-0.12	-0.15	+0.00	+0.01	-0.02	-0.04	6 7		
7 8	-0.06	-0.24	+0.08	-0.18	-0.05	-0.08	7		
	+0.03	-0.22	+0.03	-0.12	-0.17	-0.10	8		
9	-0.04	-0.10	-0.10	+0.05	-0.07	-0.06	9		
10	-0.13	-0.10	-0.10	+0.08	-0.11	-0.07	10		
11	-0.14	+0.03	-0.03	+0.05	-0'14	-0.02	11		
12	-0.08	+0.15	-0.10	+0.01	-0.50	-0.02	12		
13	+0.14	+0.03	+0.08	+0.10	-0.16	+0.04	13		
14	+0.03	+0.10	+0.04	+0.03	-0.09	+0.03	14		
15	+0.08	+0.12	+0.06	+0.05	+0.04	+0.07	15		
16	+0.11	+0.18	+0.08	+0.15	+0.06	+0.11	16		
17	+0.12	+0.09	+0.04	+0.04	+0.15	+0.09	17		
18	+0.19	+0.09	+0.18	-0.03	+0.05	+0.09	18		
19	+0.11	+0.02	0.00	0.00	+0.15	+0.06	19		
20	+0.14	+0.01	+0.01	-0.14	+0.08	+0.02	20		
21	+0.11	-0.07	-0.17	-0.13	+0.02	-0.04	21		
22	+0.08	+0.04	-0.51	-0.07	+0.07	-0.03	22		
23	+0.11	+0.04	-0.18	-0.13	-0.03	-9.06	23		

The curves obtained from the values comprised in this table are represented to the eye in Plate II., Fig. 3., the fainter lines corresponding to the variations in the separate periods, 1844 to 1846, and 1846 to 1848, and the stronger line to the mean of the whole period of five years. The formulæ by which these curves have been computed are as follow:—

1844 to 1846,
$$\Delta_x = +.006 - .092 \sin(a + 0.5) + .036 \sin(2a + 345.1)$$

1846 to 1848, $\Delta_x = -.014 - .028 \sin(a + 355.5) + .058 \sin(2a + 316.7)$
1844 to 1848, $\Delta_x = +.005 - .058 \sin(a + 2.0) + .048 \sin(2a + 330.0)$

The coefficients are decimals of a scale division, and a is reckoned in hours (multiplied by 15°) from the time of the moon's superior culmination. The number of hourly observations of the Vertical Force Magnetometer employed in this investigation is 31,773.

Inclination and Total Force.—The variations of the Inclination and Total Force in a lunar day are derived from those of the horizontal and vertical components of the force by the formulæ—

$$\Delta \theta = \sin \theta \cos \theta \left(\frac{\Delta Y}{Y} - \frac{\Delta X}{X} \right);$$
 $\frac{\Delta \phi}{\phi} = \cos^2 \theta \frac{\Delta X}{X} + \sin^2 \theta \frac{\Delta Y}{Y};$

in which θ is the inclination, ϕ the total force, X its horizontal, and Y its vertical component. They are shown for the whole period of the five years in Table LXIV., computed from the values of the Horizontal and Vertical Forces in columns 7 of Tables LXII. and LXIII. The variation of the Inclination is expressed in seconds of arc, the sign + signifying an increase of the dip of the north end of the magnet; and that of the Total Force in parts of the Total Force at Toronto, of which the approximate absolute value is 13:9 in British units.

TABLE LXIV.

Lunar	Lunar-di	Lunar-diurnal Variation		Lunar-dit	ırnal Variation	Lunar	Lunar-diurnal Variation		
	of the Inclination.	of the Total Force.	Hours.	of the Inclination.	of the Total Force.	Hours.	of the Inclination.	of the Total Force.	
0 1 2 3 4 5 6 7	" -0.56 -1.44 -2.07 -2.26 -2.05 -1.61 -0.97 -0.33	Parts of the Force '0000013 + '0006004 + '0000019 + '0000026 + '0000021 + '0000008 - '0000012 - '0000034	8 9 10 11 12 13 14 15	" +0.05 +0.17 0.00 -0.32 -0.75 -1.07 -1.08 -0.76	Parts of the Force '0000051 - '0000058 - '0000050 - '0000034 - '0000010 + '0000021 + '0000044 + '0000060	16 17 18 19 20 21 22 23	" -0.22 +0.57 +1.31 +1.92 +2.14 +1.93 +1.33 +0.42	Parts of the Force, + '0000063 + '0000053 + '0000033 + '0000006 - '0000020 - '0000031 - '0000035 - '0000026	

These variations are represented to the eye by the stronger lines in Figs. 4. and 5. of Plate II.; in which also the fainter lines show the variations derived respectively from the half periods constituted as previously described. In Fig. 6., of Plate II. are collected in one view the lunar-diurnal variations of the Declination, Inclination, and Total Force, as they are separately represented in other figures of the same plate.

General Conclusions.—The three magnetic elements concur in showing that the moon exercises a sensible magnetic influence at the surface of the earth, producing in every lunar day a variation in each of the three elements, which is distinctly appreciable by the instruments employed in the observatories established to carry out the system of observation recommended by the Royal Society, when due care has been taken in conducting the observations, and suitable methods are adopted for elaborating the results.

The lunar-diurnal variation consists in a double progression in each lunar day in each of the three elements: the Declination has two easterly and two westerly maxima, and the Inclination and Total Force each two maxima and two minima in each interval between two successive passages of the moon over the astronomical meridian; the variation passing in every case four times through zero in the course of the lunar day. The easterly maxima of the horizontal deflection of the north end of the magnet synchronise with the moon's superior and inferior passages of the meridian, the westerly maxima with the lunar hours of 6 and 18. The maxima of the increased magnetic force due to the moon's action occur about the lunar hours of 3 and 16, and the minima about the hours of 9 and 20. The maxima of the Inclination, i.e. of the dip of the north end of the magnet, occur about the lunar hours of 3 and 14, and the minima about 9 and 20. The extent of the variation in the lunar day, or the range between the extremes that are widest apart, is in the Declination 38".33, in the Inclination 4".4, and in the Total Force .000012 parts of the whole terrestrial magnetic force at Toronto. These are the values derived from the whole period of observation, i. e. from six years of the Declination, and from five years of the Inclination and Total Force. When the whole period is subdivided into two half-periods, the hours of maxima and minima and the extent of the range accord with the results of the whole period in each of the three elements, with slight and wholly insignificant exceptions. The reality of the variations is thus attested no less by the accordance of the results when the whole period during which the phenomena were observed is subdivided into separate and independent portions, than by the systematic character which the variation is seen to possess, when the strictly independent results at the several lunar hours are brought together and exhibited continuously.

As it happens that in the Declination the variation resulting from the moon's action is greater, relatively to the instrumental means for measuring it, than either in the Inclination or in the Total Force, it is reasonable to conclude that we have a better

opportunity of judging of the particular nature and character of the moon's magnetic influence by studying the effects produced on the Declination than by studying those produced on either of the other elements.

Referring to Table LIX., p. lxxx, which exhibits the coefficients of all the twelve terms in the formula of sines and cosines by which the results of observation are strictly represented, we perceive that the coefficient of the cosine of twice the hour angle is not only the one of greatest amount, but is, in fact, the only one which we can with confidence regard as possessing a substantial value. All the other coefficients are, without exception, not only extremely small in comparison with the one above noticed, but are so small that they may well be supposed to represent the small deviations from a natural law ascribable to errors which cannot wholly be extinguished in averages derived from not more than six years of observation. On the other hand, the coefficient in the second term has a value far beyond any explanation resting on the supposition of errors of observation. The probable error of any single hour is 1".37, whilst the range of the variation is not less than 38". Whilst, therefore, the general result of this investigation is to establish conclusively the existence of a lunar-magnetic influence sensible at the surface of the earth, the lunardiurnal variation which is thus manifested appears to be consistent with the hypothesis that the moon's magnetism may be, in great part at least, if not wholly, derived by induction from the magnetism of the earth.

It is further observable, that in the lunar-diurnal variation there is no appearance of the *decennial* period which constitutes so marked a feature in the solar-diurnal variations.

SOLAR-DIURNAL VARIATION.

Declination.—In the first volume of the Toronto Observations, published in 1845, an inference was drawn from the examination of the observations in 1841 and 1842 printed in that volume, that the double progression which showed itself in the diurnal variation, (produced by a small westerly retrogression of the north end of the magnet occurring between the hours of 10 and 14), might be an effect of the superposition of two distinct diurnal variations, each proceeding from a distinct class of phenomena; one class being the regular solar-diurnal variation corresponding to the sun's daily (apparent) revolution round the earth; and the other class produced by causes, not indeed of daily, but of occasional occurrence, the diurnal variation being in the latter case the representative of the mean effect of the occasional causes: and it was suggested, that if by any process the whole effect of the occasional disturbances could be eliminated, it might be very possible that the residual variation, or that portion which might be regarded as more strictly deserving the name of "diurnal variation," might prove to be "a single progression with but one maximum and one minimum in the 24 hours." It was at the same time further suggested, that though it might be

difficult, and perhaps impossible, to eliminate from the observations the whole effect of the disturbances referred to, it might be very possible, by a partial separation of those of largest amount, to examine whether their influence on the diurnal variation was or was not of a systematic character, and such as might produce the supposed effects.

The Toronto observations from 1843 to 1848 have since been received and printed, and have been treated according to the suggestion above noticed. The result has been to establish the fact, that the occasional and previously called "irregular" disturbances are phenomena subject to periodical laws; and that amongst these there is one which regulates their occurrence in the diurnal period, causing them to constitute in their mean effect a diurnal variation wholly distinct from the regular daily solar-diurnal variation, and having different hours of maxima and minima. (Phil. Trans. 1851, Art. V.; 1852, Art. VIII.; 1856, Art. XV.; and pp. lxxvi and lxxvii of this volume.)

The disturbed observations which have been separated from the great body of the observations for the purpose of this investigation are all those which differ from the normal position of the magnet, at the same hour and in the same month, by a quantity equalling or exceeding 5'·0 of arc. These have sufficed to establish the systematic characters and distinctive features of the diurnal variation which the disturbances occasion, but we are sure that they do not give its full numerical amount; for it cannot be doubted that there must be minor disturbances of the same class,—minor effects proceeding from the same causes,—which remain in the body of the observations when those of 5'·0 and upwards have been removed; and which must still continue to exercise an influence similar in kind, and possibly (as being more numerous) not less in degree, on the residual diurnal curve, modifying the pure result which would be obtained if the whole influence of the disturbances could by any process be separated. The question, then, which now remains to be considered is, whether, and with what degree of probability, we may infer, by means of a comparison of the diurnal variation with and without the disturbances of 5'·0 and upwards, that if their whole influence were eliminated the residual diurnal variation would show itself as a single instead of a double progression.

This question is of some theoretical importance; for since the publication of the first volume of this work, in 1845, the physical explanation of the diurnal variation has occupied the attention of eminent physicists, two of whom in particular, Faraday and Secchi, have propounded physical therories, which, however dissimilar they may be in other respects, concur in regarding the diurnal variation derived from the whole of the observations including the disturbances, as phenomena of one and the same class, and the double progression as an integral part of the same, and a necessary consequence of the physical theory adopted for their explanation. An additional importance is therefore given to the inquiry whether, after the deduction of that portion of the diurnal variation which has now been ascertained to proceed from a distinct class of

phenomena, not of daily but of occasional occurrence, the residual variation, or that due to the regular daily course of the sun round the earth, may not be regarded with greater probability as a "single progression with but one maximum and one minimum," rather than as a "double progression with two maxima and two minima."

In column 2 of the subjoined table (Table LXV.) is shown the mean diurnal variation derived from the whole of the observations, including the disturbances; in column 3 the mean diurnal variation derived from the disturbances which equal or exceed 5'·0 (from Table LI., p. lxi); in column 4 we have the residual diurnal variation when the values in column 3 are deducted from those in column 2; and in column 5 we have the diurnal variation such as it would be found if we permitted ourselves to suppose that by abstracting the disturbances equalling or exceeding 5'·0 we had eliminated half the influence of the disturbances of the class to which they belong.

TABLE LXV.

Toronto		Diurnal Variati	on, as derived from		Toronto
Astronomical Time.	the whole of the Observations.	the larger Disturbances.	the Values in Column 2 — the Values in Column 3.	the Values in Column 2 — twice the Values in Column 3.	Astronomical Time.
(1.)	(2.)	(3.)	(4.)	(5.)	(6.)
n. i	,	,	,	1	н.
12	0.96 E.	0.33 E.	0.63 E.	0.30 E	12
$\overline{13}$	0.80 E.	0.26 E.	0.24 E.	0.58 E.	13
14	0.69 E.	0.14 E.	0.52 E.	0.35 E.	14
15	0.87 E.	0.16 E.	0.71 E.	0.55 E.	15
16	1.27 E.	0.15 E.	1.12 E.	0.94 E.	16
17	1.91 E.	0.05 M	1.93 E.	1.95 E.	17
18	2.69 E.	0.29 W.	2.98 E.	3 · 27 E.	18
19	3.28 E.	0.41 W.	3.99 E.	4.40 E.	19
20	3.95 E.	0.52 W.	4.44 E.	4.96 E.	20
21	3°17 E.	0°46 W.	3.63 E.	4.09 E.	21
22	0.94 E	0.30 M·	1.24 E.	1.54 E.	22
23	1.80 W.	0'11 W.	1.69 W.	1.58 W.	23
0	4°13 W.	0'11 W.	4 ° 02 W.	3.91 W.	0
1	5°10 W.	0.03 M.	5.07 W.	5.04 W.	1
2	4.96 W.	0.09 M.	4.87 W.	4.78 W.	2
3	3.91 W.	0.08 W.	3.83 W.	3.75 W.	3
4	2.57 W.	0.09 W.	2.48 W.	2.39 W.	4 5
5	1:33 W.	0.04 W.	1.29 W.	1.25 W.	5
6	0.30 W.	0.18 E.	0.48 W.	0.66 W.	6
7	0.55 E.	0.34 E.	0.15 W.	0.46 W.	7
8	0.70 E.	0.25 E.	0.18 E.	0.34 W.	8
9	1.39 E.	0.87 E.	0.52 E.	0.32 M.	9
10 ·	1.31 E.	0.61 E.	0.70 E.	0.09 E. 0.18 E.	10
11	1.24 E.	0.23 E.	0.71 E.	0 18 E.	11

From this table we perceive, 1st, that when the diurnal variation is derived from the whole body of the observations including the disturbances as in column 2, the march of the north end of the magnet towards the east, which is otherwise continuous from

the extreme westerly direction between 1 and 2 p.m. to the extreme easterly direction between 7 and 8 the following morning, is interrupted by a small westerly retrogression between 9 p.m. and 4 a.m.; 2d, that when the larger disturbances, or those which equal or exceed 5'·0 in amount, and produce as their mean effect the diurnal variation in column 3, are eliminated, the westerly retrogression previously noticed is reduced very considerably both in amount and continuance, as is seen in column 4; and 3d, that if we assume that, by abstracting the disturbances equalling or exceeding 5'·0, we may have eliminated half of the whole influence of the causes to which the larger disturbances are due (which is certainly no unreasonable supposition), we have the residual diurnal variation as in column 5, in which the westerly retrogression is almost wholly obliterated, and the variation has become virtually a single progression, with but one maximum and one minimum.

Viewing, then, the residual variation after the elimination of the influence of the disturbances as the best approximation we can obtain towards a representation of the phenomena of the regular solar-diurnal variation, and regarding this representation as corresponding to a mean state of the phenomena, or to that which would belong to all the days in the year if the sun's path were always in the plane of the equator, we find the mean solar-diurnal variation at Toronto to be approximately as follows:—The chief variation takes place during the hours when the sun is above the horizon; the motion of the north end of the magnet towards the east, which during the hours of the night is extremely slow, quickens between 4 and 5 A.M., and continues at a nearly uniform rate, exceeding 1' an hour, from 5 A.M. to a few minutes before 8 A.M., when the easterly extreme is reached. The north end then returns rapidly towards the west, attaining the westerly extreme of its daily progress about 20 minutes past 1 P.M. This interval is the time of most rapid motion, the whole amplitude or extent of the diurnal variation, amounting to about 10' of arc, being passed through in about 5½ hours. The motion is most rapid between 10 and 11 A.M., when the change of direction in one hour is very nearly $4' \cdot 0$. After reaching the westerly extreme, at or about 1h. 20m., the north end returns again towards the east, at a nearly uniform rate a little exceeding 1'·0 per hour, until near 6 P.M., at which time the night phase of the variation may be said to commence. This, apart from the disturbances, is a continuation of the easterly motion, but at a comparatively very slow rate, which, on the average of the 10 hours from 6 p.m. to 4 a.m., scarcely exceeds 0'·16 per hour.

Table LXVI. exhibits the solar-diurnal variation of the Declination in the different months of the year after the separation and omission of the larger disturbances. This table is similar in form to Table VII. in vol. II. (p. xv), but differs from it inasmuch as the latter is derived from all the observations, including the disturbances, and in this the disturbances are excluded. The sign + implies that the north end of the magnet is to the east, and — to the west, of the mean position in the month.

Vol. III.

TABLE LXVI.

				,	TORONT	O ASTRO	NOMICA	L HOUR	s.			
Months.	Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .	10h.	11 ^h .
January February March April June July September October November	-	-3·34 -3·30 -5·22 -5·98 -6·20 -5·86 -7·22 -6·38 -4·20 -3·80 -3·02	-3·14 -3·26 -5·36 -5·84 -6·10 -6·26 -5·96 -6·52 -5·40 -3·94 -3·30 -3·36	-2·44 -2·54 -4·78 -4·98 -4·84 -5·26 -5·12 -5·04 -3·36 -2·66 -2·52 -2·38	-1.64 -1.66 -3.42 -3.30 -3.12 -3.76 -3.68 -2.74 -1.16 -1.80 -1.78 -1.70	-0°92 -1°36 -2°18 -1°66 -1°26 -1°68 -1°02 -0°42 -1°24 -1°10 -0°80	-0°32 -0°84 -1°12 -0°80 -0°44 -0°62 -0°70 -0°18 +0°12 -0°70 -0°12 0°00	+0.06 -0.38 -0.56 -0.32 -0.22 -0.36 -0.12 -0.06 -0.22 +0.64 +0.36	+0.76 +0.32 -0.30 +0.44 -0.18 -0.32 -0.66 -0.10 +0.24 +0.24 +0.84 +0.88	+1'02 +0'92 +0'22 +0'44 +0'16 -0'22 -0'16 +0'48 +0'64 +0'58 +0'96 +1'24	+1.08 +0.88 +0.90 +0.82 +0.38 +0.04 +0.36 +0.46 +0.78 +0.48 +1.16 +1.10	+0.66 +0.60 +1.02 +1.12 +0.50 +0.66 +0.58 +0.52 +0.06 +0.62 +1.16 +1.02
Semi- annual Means Oet. to March	$- \begin{vmatrix} -5.17 \\ -2.88 \end{vmatrix}$	$\begin{vmatrix} -6.32 \\ -3.81 \end{vmatrix}$	$\begin{vmatrix} -6.01 \\ -3.73 \end{vmatrix}$	$\begin{vmatrix} -4.77 \\ -2.89 \end{vmatrix}$	$\begin{vmatrix} -2.96 \\ -2.00 \end{vmatrix}$	-1:32 -1:27	-0.44 -0.52	-0.53 -0.05	-0.10 +0.46	+0.22 +0.82	+0.47 +0.93	+0.57 +0.85
Annual Means -		-5.07	-4.87	-3.83	-2.48	-1.59	-0:48	-0.15	+0.18	+0.25	+0.40	+0.41
(continued)												
Months.	12 ^h .	13 ^h .	14 ^h .	15h.	16 ^h .	17 ^h .	18h.,	19 ^h .	20h.	21h.	22 ^h .	23 ^h .
January February - March April May - June July September - October November - December Seiniannual Means April to Sept. Means	- +0.44 - +0.44 - +1.12 - +0.88 - +0.36 - +0.42 - +0.76 - +0.54 - +0.56 - +0.66 - +0.66 - +0.66 - +0.66 - +0.66 - +0.66		-0.04	+0.42 +0.62 +1.28 +1.48 +0.68 +0.02 +0.12 +0.72 +1.40 +0.92 +0.62 +0.30	+1.37	, +0.50 +1.34 +1.56 +2.36 +3.18 +3.04 +2.78 +2.52 +2.64 +1.70 +0.92 +0.58	+0.74 +1.64 +2.26 +3.40 +5.16 +5.28 +4.52 +5.22 +3.90 +1.84 +1.28 +0.58	+1·28 +2·00 +3·52 +4·64 +6·36 +6·50 +6·94 +5·22 +2·74 +1·78 +0·92	+1.46 +5.82	+2·90 +2·78 +4·54 +3·96 +4·18 +4·76 +3·00 +3·04 +2·76 +2·04 +4·25 +3·01	+0.90	-0'38 -0'50 -0'74 -2'02 -3'06 -1'76 -3'12 -3'70 -1'66 -1'12 -0'26 -2'61 -0'78
Annual Means -	- +0.63	1	1	<u> </u>		+1.83		+3.59	<u> </u>	+3.63		

Table LXVII. exhibits the solar-diurnal variation of the Horizontal Force in the different months of the year, after the separation and omission of the larger disturbances. This table is similar in form to Table XXXIII. in vol. II., p. lix.

TABLE LXVII.

					———							
				r	CORONTO) ASTRO	NOMICA	L HOURS	S.			
Months.	0 ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .	10h.	11h.
	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
April	$ \begin{array}{c c} -108 \\ -086 \\ -052 \\ -042 \\ -032 \end{array} $	$\begin{array}{c c} -060 \\ -043 \\ -070 \\ -042 \\ +010 \\ +004 \\ +007 \\ +003 \\ -009 \\ -038 \\ -060 \\ -052 \\ \end{array}$	$\begin{array}{c} -030 \\ -010 \\ -030 \\ +005 \\ +054 \\ +058 \\ +049 \\ +057 \\ +045 \\ -001 \\ -017 \\ -027 \\ \end{array}$	+021 +017 +017 +056 +081 +085 +081 +090 +072 +024 +016 +005	+048 +028 +041 +074 +085 +095 +092 +091 +076 +040 +028 +031	+045 +033 +051 +074 +081 +089 +078 +080 +061 +043 +033 +031	+033 +027 +040 +056 +059 +067 +055 +048 +053 +034 +032 +027	+020 +028 +035 +030 +030 +039 +037 +023 +036 +031 +031 +021	+018 +019 +030 +012 +013 +015 +013 +015 +021 +021 +021 +025 +013	+012 +020 +021 +011 +005 000 +009 +015 +023 +015 +019 +010	$\begin{array}{c} +014 \\ +012 \\ +017 \\ +008 \\ +004 \\ -004 \\ +008 \\ +022 \\ +016 \\ +020 \\ +007 \end{array}$	+008 +008 +014 +005 +001 -015 +005 +011 +018 +008 +007 +002
Semi- annual Means Oct. to March	$\begin{array}{c c} - & -056 \\ -085 \end{array}$	-004 -054	+045 -019	+078 +016	+085 +037	+077 +039	+056 +032	+032 +028	+015 +020	+010 +016	+006 +013	+004 +008
Annual Means -	- 070	-029	+013	+047	+061	+058	+044	+030	+017	+013	+010	+006
(continued)												
	12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18h.	19 ^h .	20h.	21 ^h .	22 ^h .	23 ^h .
Months.	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
January - February - April - April - June July - August - September - October - November December - Semiannual April to Sept. Means Oct. to March	+006 +014 +007 -005 -018 -013 +007 +013 +006 +006	+006 -001 +007 +008 -012 -019 -008 +003 +013 +011 -002	+005 +003 +011 +003 -006 -014 -013 +009 +011 +015 +016 +007	+012 -007 +011 +013 -012 -023 -014 +001 +003 +020 +019 +005	+022 +012 +019 +021 -009 -018 -007 +021 +032 +028 +015	+020 +017 +023 +024 -005 -012 -017 -003 +024 +033 +039 +022 +026	+031 +021 +035 +014 +001 000 -003 +001 +015 +032 +043 +034	+031 +010 +013 +011 -007 -007 -011 -017 -009 +014 +034 +030	+024 -011 -016 -023 -036 -033 -035 -062 -054 -027 -008 +021	-008 -030 -050 -070 -085 -064 -067 -105 -103 -068 -048 -004	-051 -046 -085 -102 -105 -098 -098 -118 -130 -094 -083 -040	-101 -063 -111 -112 -089 -082 -081 -099 -115 -096 -103 -072 -097 -092
Annual Means	+001	+001	+004	+002	+010	+014	+019	+008	-022	-058	-087	-094

Table LXVIII. exhibits a corresponding table of the Vertical Force, similar in form to Table XXXIX. in vol. II., p. lxix, but with omission of the larger disturbances.

TABLE LXVIII.

The Paragraph of the Control of the					TORONT	O ASTRO	ONOMICA	L HOUR	:S.			
Months.	Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .	10 ^h .	11 ^h .
	•00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
January	0013	+0014	+0042	+0058	+0047	+0056	+0070	+0070	+0064	+0050	+0033	+0022
February	- -0068	-0024	+0042	+0087	+0084	+0086	+0081	+0074	+0055	+0055	+0033	+0027
2/2/11/012	- -0081	-0046	0001	+0042	+0056	+0070	+0067	+0061	+0055	+0050	+0041	+0036
2.1/4.12	0077	-0033	+0031	+0068	+0082	+0077	+0063	+0090	+0068	+0027	+0004	-0013
2.2.0	0095	-0041	+0029	+0067	+0110	+0133	+0137	+0093	+0069	+0043	+0035	-0018
	- 0075	-0067	-0005	+0077	+0116	+0131	+0106	+0111	+0074	+0055	+0017	+0000
oury	- 0077 - 0047	-0047 + 0005	+0004	+0081 + 0007	+0141 + 0143	+0184 + 0159	+0174 + 0133	+0145	+0081	$+0064 \\ +0014$	+0010	-0003 -0033
August September -	-0023	+0046	+0070 + 0090	+0109	+0110	+0110	+0095	+0097 +0065	+0081 + 0061	+0014 +0045	+0008 + 0029	-0011
October	-0055	+0005	+0046	+0077	+0074	+0073	+0075	+0086	+0073	+0043	+0023 + 0041	+0013
November -	- 0024	+0020	+0074	+0070	+0073	+0072	+0065	+0068	+0065	+0056	+0042	+0022
December	- 0028	+0013	+0054	+0072	+0060	+0054	+0043	+0055	+0054	+0056	+0042	+0022
Semi- April to Sept.		-0023	+0036	+0085	+0117	+0132	+0118	+0100	+0072	+0041	+0017	-0013
means Oct. to March	- -0045	-0003	+0043	+0068	+0066	+0068	+0067	+0069	+0061		+0039	+0024
Annual Means -		-0013	+0040	+0076	+0091	+0100	+0092	+0084	+0067	+0048	+0028	+0005
(continued)				<u>, </u>					1	1	1	
	12 ^h .	13h.	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18h.	19h.	20h.	21h.	22h.	23 ^h .
Months.	.00	.00	.00	.00	.00	.00	.00	•00	.00	•00	.00	.00
	1		<u> </u>	<u> </u>		1]	1
January	- 0004	-0022	-0028	-0041	-0047	-0045	-0027	-0027	-0036	-0068	-0072	-0064
February -	+0003	-0033	-0045	-0036	-0038	0026	-0022	-0010	-0011	-0082	-0119	-0124
March	+0003	-0023	-0036	-0020	-0003	-0020	-0011	+0017	+0018	-0038	-0101	-0128
April May	+0036 -0045	-0041 -0063	-0038 -0056	-0029 -0043	-0031	+0004	+0027	+0015	-0004	-0042	-0088	-0105
June	-0045	-0003 -0043	-0050	-0045 -0065	-0026 -0009	-0003 + 0020	$+0019 \\ +0004$	$+0001 \\ -0022$	-0027 -0054	-0074 -0079	-0125 -0099	-0124
July	-0030	-0074	-0119	-0116	-0093	-0052	+0004	-0022 -0005	-0028	-0079	-0099 -0078	-0095 -0087
August	- 0056	0069	-0100	-0091	-0091	-0002	+0001	-0023	-0045	-0074	-0078	-0054
September	- 0050	0050	0059	-0054	-0086	-0067	-0019	-0028	-0043	-0095	-0095	-0049
October	-0017	0051	-6041	0026	-0051	-0063	-0040	-0019	-0027	-0056	-0081	-0091
November December	- 0009 - 0019	$-0033 \\ -0027$	$-0046 \\ -0027$	$-0050 \\ -0028$	-0050 - 0056	-0049 -0050	-0061 -0022	-0033 -0037	-0046 -0040	-0077 -0046	$-0090 \\ -0068$	$-0070 \\ -0059$
annual > \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	- 0030 - 0007	-0057 -0031	-0070 -0037	-0066 -0033	- 0056 - 0041	0017 0042	+0006 -0030	-0010 -0018	$-0033 \\ -0024$	-0069 -0060	-0094 -0089	-0086 -0089
Annual Means		-0044	-0054	-0050	-0048	-0030	-0012	—0014	0029	0065	-0091	-0087

From the diurnal variations of the Horizontal and Vertical Forces we obtain those of the Inclination and Total Force, as follows:—

TABLE LXIX.

Diurnal Variation of the Inclination and Total Force, omitting the larger Disturbances.—(The sign + signifies an Augmentation of the North Dip and of the Total Force; the sign - the converse.)

Toronto	IN	CLINATION	•		TOTAL FORCE.		Toronto	
Astrono-	Semi-annı	ual Means.	Annual	Semi-ann	ual Means.	Annual	Civil	
Hours.	April to September.	October to M arch.	Means.	April to September.			Hours.	
и. 12 13 14 15 16 17 18 19 20 21 22 23 0 1 22 23 6		$ \begin{array}{c} $	" - 1.5 - 2.8 - 4.8 - 3.5 - 7.5 - 8.7 - 10.3 - 4.8 + 9.7 + 26.2 + 39.5 + 43.4 + 32.8 + 14.0 - 4.7 - 20.0 - 26.2 - 24.4 - 17.7	Parts of Force. - '000029 - '000055 - '000067 - '000066 - '000015 + '00009 - '00013 - '00019 - '000144 - '000097 - '000024 + '000064 + '000165 + '000173 + '000146	Parts of Force '000003 - '000025 - '000028 - '000024 - '000022 - '000006 - '000024 - '000024 - '000078 - '000127 - '000143 - '000098 - '000028 + '000075 + '000089 + '000085	Parts of Force '000017 - '000040 - '000048 - '000039 - '000019 + '000001 - '000008 - '000041 - '000098 - '000142 - '000143 - '000097 - '000031 + '000046 + '000102 + '000125 + '000131 + '000115	n. Midnight. 1 a.m. 2 a.m. 3 a.m. 4 a.m. 5 a.m. 6 a.m. 7 a.m. 8 a.m. 9 a.m. 10 a.m. 11 a.m. Noon. 1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 6 p.m.	
7 8 9 10	$ \begin{array}{c c} -11 \cdot 2 \\ -3 \cdot 9 \\ -3 \cdot 1 \\ -2 \cdot 2 \\ -2 \cdot 8 \end{array} $	$ \begin{array}{c} -12.3 \\ -10.7 \\ -6.9 \\ -5.6 \\ -4.6 \\ -2.8 \end{array} $	$ \begin{array}{c c} -10.9 \\ -5.4 \\ -4.3 \\ -3.5 \\ -2.8 \end{array} $	+ '000143 + '000113 + '000078 + '000044 + '000020 - '000009	+ '000083 + '000071 + '000062 + '000045 + '000028	+ '000098 + '000074 + '000053 + '000032 + '000009	7 p.m. 8 p.m. 9 p.m. 10 p.m. 11 p.m.	

In the case of the Total Force, the diurnal variation due to the mean effect of the larger disturbances bears so large a proportion to the regular solar-diurnal variation, that when one is superimposed upon the other, and they are viewed in combination,—as is the case when the diurnal variation is obtained from the whole of the observations including the disturbances,—the true character of the regular ordinary solar-variation is altogether masked, and we are in danger of drawing erroneous conclusions in regard to it. Thus, in Vol. I. of the Toronto Observations, pp. lxx, lxxi, the

diurnal variation being there derived from the whole of the observations, the principal features appeared to be, and were stated as follows:—

A principal maximum at 5 hours.

A principal minimum at 15 hours.

A secondary maximum at 18 to 20 hours.

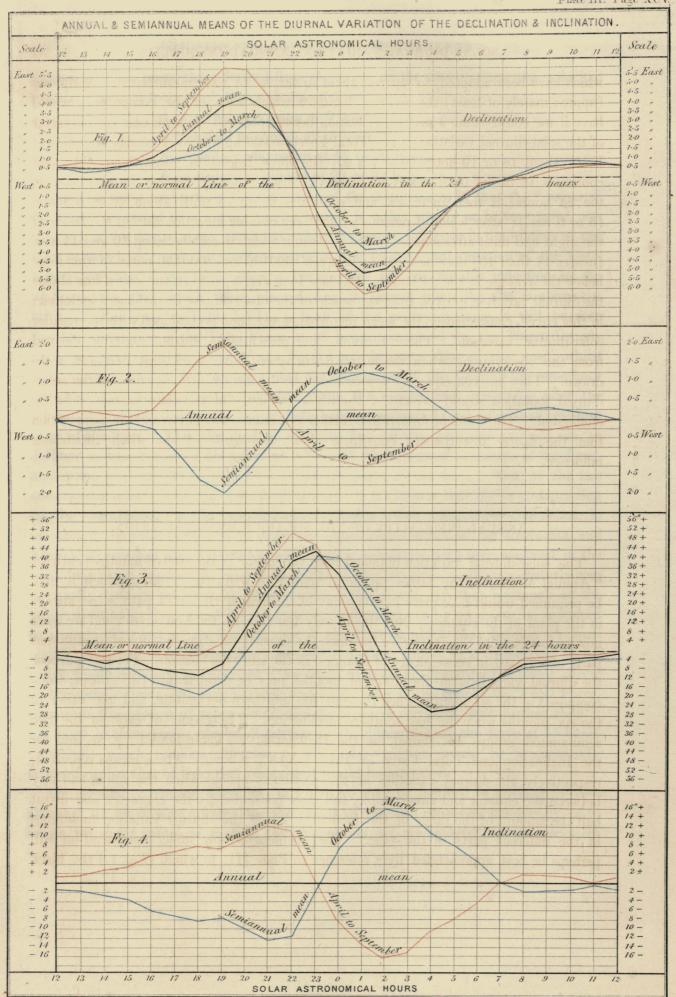
A secondary minimum at 22 or 23 hours.

The first thing we learn by the separation of the disturbances is, that the "principal minimum" so stated as occurring "at 15 hours" is either wholly or in very great part an effect of the disturbances which have their maximum influence in diminution of the force at that hour; and that the true curve of the solar-diurnal variation of the Total Force (like that of the Declination, p. lxxxix) has but one notable inflection in the 24 hours, viz. that which takes place during the hours when the sun is above the horizon. Referring to Table LVII., p. lxxii of the present volume, it will be seen that the diminution of the Total Force at 15 hours occasioned by the larger disturbances averages 000138 parts of the Total Force in every day of the year; whilst from Table LXX., p. xcii, we learn that the diminution of the force at the same hour from the solar-diurnal variation obtained from the observations remaining after the separation and omission of the larger disturbances amounts to not more than '000045 parts of the force. The combination of these two effects, referable as they are to different causes, produced therefore at 15 hours the apparent minimum of the force, amounting to (.000138 + .000045 =) .000183 parts of the force. Now of the two components which form the combined amount, it is obvious that the one depending on the disturbances would be increased, and the other component diminished, in amount, if the values assumed to constitute large disturbances of the Horizontal and Vertical Forces had been taken somewhat smaller than they have been assumed in the preceding pages: and as the remark in p. lxxvii regarding the declination-disturbances is equally true in reference to those of the Total Force, viz. that inasmuch as the larger disturbances separated by the processes described can by no means be supposed to include the whole of the disturbances of the class to which they belong, we must regard the mean diurnal variation obtained from them simply as a "minimum limit," which would certainly be exceeded if we could succeed in separating the minor effects of the same causes;—we may likewise reasonably infer in the case of the Total Force, that were the process of separation of the disturbances carried a little further than it has been in these pages, the small portion of the diminution of the force at 15 hours ('000045) which remains referable to the solar-variation would be progressively reduced, whilst that of the other component would be increased.

The general conclusion, therefore, to which we may be justified in arriving, is, that although we are unable to separate the effects of the two causes so completely as to assign the exact values of each of the components, we are enabled, by the processes

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	V.			

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which have been adopted, to separate them so far, as to have no difficulty in assigning (approximately at least) the general character which each of the components would have if we could make a perfect separation between them. In such case the character of the solar-diurnal variation of the Total Force would appear to be nearly as follows: From about 18 or 19 hours (6 or 7 A.M.) the force begins to diminish sensibly, and continues to do so until nearly 23 hours (11 A.M.), when it reaches its minimum in the 24 hours; it then increases, and continues to do so until about 5 or 6 hours (5 or 6 P.M.); after which it remains without any notable inflection during the hours of the night and until after sunrise. The minimum which occurs between 10 and 11 A.M. (nearer 11 than 10) may be taken at between '000140 and '000150 parts of the force below the average in the 24 hours. In Plate IV., Fig. 3., p. xevi, the dotted line shows the diurnal variation derived from the whole of the observations, disturbances included; in this curve, consequently, the mean disturbance-variation is combined with the regular solar-diurnal variation. The continuous line presents the diurnal variation derived from the observations when the larger disturbances have been separated and withdrawn. This line consequently approximates to the form which the curve of the solardiurnal variation would present if the whole influence of the disturbances could be eliminated. The third or broken line further represents this curve on the supposition that the *larger* disturbances constitute about *two-thirds* of the whole disturbing influence.

ANNUAL INEQUALITY OF THE SOLAR-DIURNAL VARIATION.

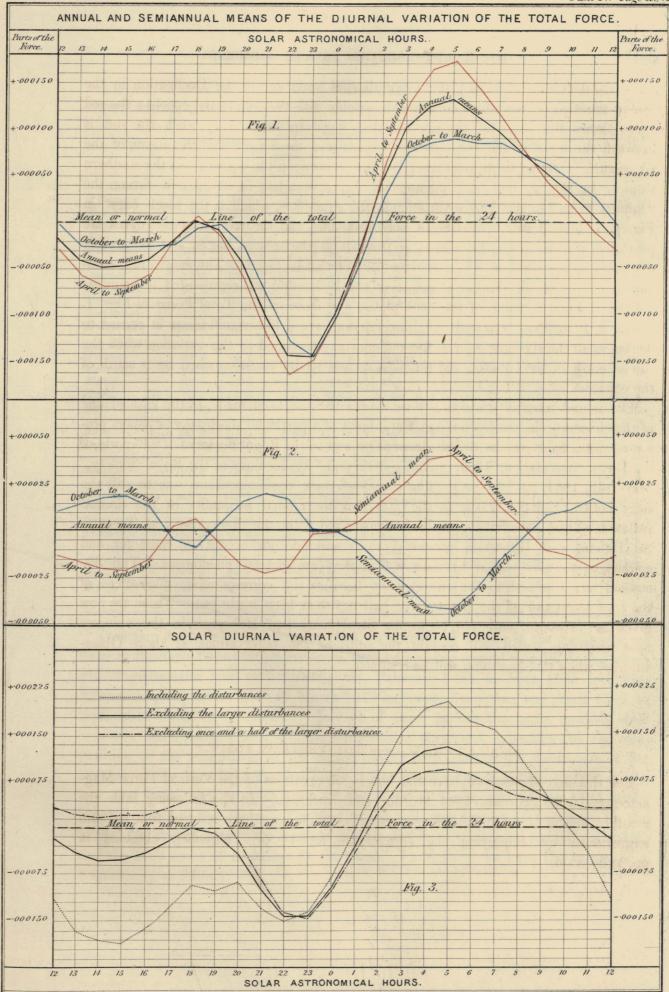
The solar-diurnal variation obtained from the mean of the twelve months (entitled "Annual Means," in the tables pp. xc to xciii) represents the variation which it may be presumed would take place in every day of the year if the sun's path were always in the plane of the equator. But this is only the case at the equinoxes; and we have now to inquire into the *inequality* to which the diurnal variation is subject in different parts of the year in consequence of changes in the sun's declination. For this purpose the diurnal variations in the different months may be divided into two groups,—one composed of the six months when the sun has northern declination, and the other of the six months when he has southern declination. The means of each of the two semi-annual groups are shown, for the Declination in Table LXVI., p. xc, and for the Inclination and Total Force in Table LXIX., p. xciii. These means represent, respectively, the diurnal variation at the particular epochs when the sun is half way between the equator and either tropic, and show consequently the character and about half the amount of the range of the inequality which the diurnal variation undergoes in the different parts of the year. The phenomena now under consideration will perhaps be best apprehended by a reference to Plate III., in which (Fig. 1.) the black

curve exhibits (in arc-value) the mean diurnal variation of the Declination in the twelve months, or that which corresponds strictly with the equinoctial epochs; the red curve shows the mean of the six months (April to September) when the sun is between the equator and the northern tropic; and the blue curve the mean of the six months (October to March) when the sun is between the equator and the southern tropic. In Fig. 2, the same phenomena are represented in a different form: the "annual mean," or the diurnal variation at the equinoxes, which is the black curve in Fig. 1., is here drawn as a straight horizontal line, and the red and blue curves are projected at their respective distances from it at the several hours, and for greater distinctness on a scale of twice the magnitude of that in Fig. 1. The annual and semiannual curves of the diurnal variation of the Inclination are represented in a similar manner in Figs. 3. and 4. of the same plate; and those of the Total Force in Figs. 1. and 2. of Plate IV. The red and blue curves have a like signification in regard to season in all the six figures; viz. the red curves correspond to the variation when the sun is north of the equator, and the blue curves to the variation when he is south of the equator.

The annual inequality which is thus manifested has been made, in the case of one of the elements, viz. the Declination, the subject of a particular discussion in papers presented respectively to the British Association and to the Royal Society.—("Reports of the British Association," 1854, pp. 355—368; and "Proceedings of the Royal Society," May 18th, 1854, pp. 67—82.) The object of these communications was to call the early notice of magneticians to the fact that the annual inequality of the diurnal variation of the Declination, as severally derived from the observations at Toronto, St. Helena, and Hobarton, presented so remarkable an accord in character and amount as to give reason to believe that they are general phenomena. The discussion was confined to the one element because the corresponding phenomena of the Inclination and of the Total Force had not then been made out. These are now given for Toronto, and will be so for St. Helena and Hobarton in the volumes now preparing, which will contain the suite of the observations at those Observatories, when the discussion will be resumed.

SECULAR CHANGE OF THE VERTICAL FORCE.

For this investigation we have the hourly observations of the Vertical Force Magnetometer from February 1844 to June 1848 inclusive. In the following table the monthly means of those observations are collected, having been reduced to a uniform temperature by employing the equivalents for 1° of Fahrenheit obtained in pp. xxii—xxvi.



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TABLE LXX.

Months.	Monthly M	cans. Te	o 1° empe-	Reduced to 55°.	Months.	Monthly Means. Temperature. to 55°. Months.		Means.	Equivalent to 1° Tempe- rature.	Reduced to 55°.
1844: February - March - April - June - July - August - September - October - November - December - 1845: January - February - March - April - June - July June - July June - July Left and the september - October - November - December - October - November - December - Tebruary - Left and the september - October - November - December - December - December - December - Tebruary - February - March -	121.8 99.0 88.0 75.1 60.2 58.5 61.4 83.6 95.1 101.1 99.5 93.3 82.9 72.1 58.6 90.8 68.9 197.9 148.0 157.1 167.1 182.3	44°3 46°5 56°5 60°5 64°8 69°7 68°3 65°1 53°4 47°1 42°7 42°7 42°9 48°0 53°6 59°4 67°1 72°0	Div. 1'80	Sc. Div. 105 6 106 5 101 7 97 9 92 7 86 7 82 4 79 6 80 7 80 9 79 0 77 4 71 5 70 3 69 6 66 5 112 6 99 5 230 1 162 6 161 8 158 1 156 7 154 9 154 4	1846: April - May June - July August September October November December 1847: January February March April - May June - July August September October November December 1848: January February March April - May June - July August September October November December 1848: January February March April - May June -		Se. Div. 214 '0 198 '3 185 '7 173 '7 170 '8 175 '9 197 '1 200 '6 210 '2 209 '0 203 '4 200 '7 188 '9 171 '8 161 '9 143 '1 145 '4 160 '8 172 '5 179 '8 188 '3 187 '2 182 '5 177 '7 165 '9 148 '9 133 '7	\$\frac{\circ}{54\cdot 7}\$ 62\cdot 8 68\cdot 6 73\cdot 6 73\cdot 7 69\cdot 5 56\cdot 6 52\cdot 8 43\cdot 0 40\cdot 3 44\cdot 6 51\cdot 4 60\cdot 3 63\cdot 9 73\cdot 0 70\cdot 4 56\cdot 1 51\cdot 6 45\cdot 2 43\cdot 4 43\cdot 9 46\cdot 7 53\cdot 3 61\cdot 5 68\cdot 2	Sc. Div. 1 '64 "" "" "" "" "" "" "" "" "" "" "" "" "	sc. Div. 213 · 5 211 · 1 208 · 0 204 · 2 201 · 5 199 · 7 199 · 7 197 · 0 190 · 5 184 · 9 182 · 6 183 · 6 183 · 0 180 · 5 176 · 5 172 · 6 170 · 7 172 · 9 174 · 3 174 · 2 172 · 2 164 · 3 164 · 1 159 · 6 155 · 3

Omitting June, July, and August 1845, on account of breaks in the continuity, we have in this table three continuous series, each comprising several months, during which the Magnetometer was undisturbed; viz. February 1844 to May 1845 inclusive, 16 months; September 1845 to March 1846 inclusive, 7 months; and April 1846 to June 1848 inclusive, 27 months. In each of these periods the mean monthly scale readings, when reduced to a uniform temperature, decreased, indicating (on the supposition of the magnetism of the needle having been constant) a diminution in the amount of the terrestrial Vertical Force. The mean value of a scale division in the two first series was 000063 parts of the Vertical Force, and in the third series 000066 parts of the force. The first series will then furnish 16 equations for the value of x, the mean monthly decrease in scale divisions; the second series 7 equations, and the third series 27 equations for the same. From these we have the values of x respectively as follows:—

For the first period of 16 months, x=2.64 scale divisions. For the second period of 7 months, x=1.47 ,, ,, For the third period of 27 months, x=2.06 ,, ,,

The mean of the 23 months composing the first and second periods, allowing weight proportioned to the number of months in each, is 2.28 scale divisions per month, = .000143 parts of the force. The mean of the 27 months composing the third period is 2.06 scale divisions, = .0001365 parts of the force. Hence, on the aforesaid supposition that the magnetism of the needle was constant, we may take the mean between two results which differ so little from each other, viz. .00014, as the approximate monthly diminution of the Vertical Force from February 1844 to June 1848 inclusive, corresponding to an annual decrease of .0017 parts of the force.

The degree of regularity with which the Vertical Force Magnetometer indicated this decrease may be estimated by the probable error of the monthly decrease in the mean scale readings during the third and longest period, which was of 27 months' duration. The monthly decrease was 2.06 scale divisions; the probable error of 2.06 is \pm 0.44, which includes the irregularities occasioned by the disturbances. Judging from the very satisfactory performance of the Toronto instrument which is here indicated, it would appear that the capabilities of the Vertical Force Magnetometer, when used with due precaution and care, have been generally very much underrated.

It may be desirable to show how little the question, so important in many other investigations, of the omission or retention of the larger disturbances of the Vertical Force, affects the indication of the amount of the secular change of that element, derived from an unbroken series of observations of the Vertical Force of many months' continuance. The monthly means reduced to 55° Fahrenheit, from April 1846 to June 1848, in page xcvii, were taken from the whole of the observations of that period, and consequently included the disturbances; but when the larger disturbances, or all those which exceed 4.0 scale divisions from the respective normals, are withdrawn, the monthly means for the same period, also at 55° Fahrenheit, become as follows:—

TABLE LXXI.

Months. Scale Divisions.		Months.	Scale Divisions.	Months.	Scale Divisions.
1846: April	213'0 211'1 208'4 205'2 203'4 200'8 200'6 197'2 190'4	1847: January	184.6 182.6 183.6 183.1 180.5 176.5 172.8 171.1 172.2	1847: October November December 1848: January February March April May June	173 · 9 173 · 8 171 · 5 168 · 3 165 · 4 164 · 2 163 · 3 159 · 9 155 · 6

From these we obtain by least squares, as the most probable value of the monthly decrease, 2.08 scale divisions, with a probable error of ± 0.44 , both being almost identical with the results stated in p. xcviii as obtained from the monthly means of the observations when the disturbances were retained.

We are naturally led by the satisfactory performance of the Vertical Force Magnetometer between the years 1844 and 1848 to examine the observations made with it at an earlier period, which did not receive perhaps their due consideration at the time, from the belief, which appears to have been pretty general, that this instrument was "unavailable for the determination of changes of long period;" and from the circumstance that the Bifilar Magnetometer, from which so much more was expected, did not yield at Toronto results from which any satisfactory conclusion whatever could be arrived at in regard to the secular change of the other component of the Total Force, viz. the Horizontal Force; for which a distinct instrument, the Unifilar, was in consequence supplied. Reverting to Vol. I. of the Toronto Observations, pp. liii to lyii, we find the following to be the history of the early observations of the Vertical Force Magnetometer:—During the first year, viz. September 1840 to September 1841, the magnet was occasionally (six times in the twelve months) dismounted, for the purpose of having its time of vibration in the horizontal plane ascertained. On each of these occasions, consequently, the readings were disconnected, and the continuity of the series interrupted. From October 1841 to October 1843, (at which latter date the magnet was again dismounted to examine the effect of changes of temperature on its magnetic moment,) the magnet was undisturbed, except by its being made to vibrate from time to time in small arcs, in order to ascertain its time of vibration in the vertical plane. For this purpose it was not necessary to touch the magnet, as it was put in vibration by another magnet, and was brought back by the Y's to its proper position on the supports. The frequency with which this examination was made and the times of vibration severally deduced therefrom, are shown in Vol. I., Table XXXVIII., pp. liv and lv, and in Vol. II., Table XXXV., p. lxi. We have here, therefore, another period of 25 months (October 1841 to October 1843 inclusive) in which, assuming, as before, the constancy of the magnetism of the Vertical Force needle, we know of no cause (excepting variations of temperature) to interfere with the indications of the instrument as a true measure of the variations of the Vertical force. The monthly means of the observations, and of the corresponding temperatures, are contained in the following table. They were taken two-hourly from October 1841 to June 1842, and hourly from July 1842 to October 1843.

Months.

1841:

November -

1842:

41.1 41.7

47.9

54.4

57.0

61.9

December -

1843:

January

March

February

107.1

106.1

97.0

86.6

81.8

72.5

October

December

January

February

April -

March

May -

June -

Scale Tempe-Scale Tempe-Scale Tempe-Months. Months. Divisions rature. Divisions rature. Divisions. rature. 1842:1843: 96.7 54.3 69.3 July -57.8 Λ pril 63.2 53.0 102.7 48.6 53.9 69:3 55.4 57.3 August May 109.5 42.3 September -58.0 63.0 June 43.9 63.7 56.7 October 65.4 July -32.8 70.1 November -76.3 August 47.8 26.5 71.3

42.0

45'1

39.4

41.5

29.9

39.2

65.6

57.1

September -

October

TABLE LXXII.

Putting Y' for the most probable monthly mean-reading in October 1842, x for the monthly change, y the equivalent in scale divisions for 1° of temperature, and a and b coefficients respectively of x and y, a being reckoned in months from the mean epoch, — if earlier and + if later, and b reckoned in degrees of Fahrenheit from a standard temperature of 55°, — if lower and + if higher, we have 25 equations, from which by least squares we obtain Y' = 70.6 scale divisions, x = -2.19 scale divisions, and y = -1.32 scale divisions.

75.6

81.2

78.6

From the contents of Table XXXVIII., Vol. I. pp. liv and lv, we find the scale coefficient (k) during this period to have averaged, with slight and apparently accidental variations, '0000935; the magnetic force of the needle having been stronger than in the subsequent period from February 1844 to May 1845, the experiments between October and February 1844 to ascertain the temperature correction having had the effect, as is frequently the case, of sensibly weakening the magnet. The value just found for $y \, (-1.32)$, multiplied by k, gives .000123 as the variation, in parts of the force, of the magnetic moment of the needle by a change of 1° of Fahrenheit. This is a somewhat higher value than '000110, found by subjecting the later observations to a similar process (see ante, p. xxvii), but the difference is small, and quite unimportant in the present investigation. The mean monthly decrease of the Vertical Force is $2.19 \times .0000935 = .00020$; or the annual decrease = .0024. This is also a somewhat larger annual decrease than was found by the later observations, but for this there may be an assignable reason. A secular change of the Vertical Force may proceed from either of two sources (or from both conjointly); viz. a secular change in the Earth's Total Force, or a secular change of the Inclination. Whilst whatever secular change may exist in either or both these elements preserves

a uniform rate, the secular change of the Vertical Force will be uniform also; but if the secular change of either varies, that of the Vertical Force will vary also. Now we have reason to know from the monthly observations of the Inclination between January 1841 and December 1855, discussed in the sequel of this volume, that about the beginning of 1844 the secular change of the Inclination altered from a previously existing annual decrease, to an annual increase. Assuming, therefore, the secular change of the Earth's Total Force, whatever it may have been, to have had the same value in 1841—1843 as in 1844—1848, then, in consequence of the alteration in the secular change of the Inclination, the Vertical Force if losing must have lost more (or if gaining must have gained less) in 1841—1843 than in 1844—1848. The observations of the Inclination would therefore lead us to expect what we have found, viz. that the apparent loss of the Vertical Force, as it may be inferred from the Magnetometer observations in 1841—1843 (assuming the constancy of the magnetism of the needle), should be greater than in 1844—1848.

Thus far in the discussion it has been assumed that the magnetism of the Vertical Force needle was constant; we have now to examine, as far as the materials which have been furnished for the purpose will permit, how far this was the case. The data which we possess are the times of vibration in the horizontal or in the vertical planes observed at particular epochs in the course of the Magnetometer observations. We will commence with the times of horizontal vibration, as being those best suited at Toronto to give a satisfactory result. Now, to ascertain whether a change may have taken place in the magnetic moment of a needle during a certain period from the times of horizontal vibration at its commencement and close, and what that change may have been, it is necessary to know by some independent mode the alteration which may have taken place in the interval in the terrestrial Horizontal Force itself. When the Observatories were first instituted, it was hoped that the secular changes of the Horizontal Force might have been derived from the observations made with the Bifilar magnet; but the experience of the two or three first years led to the substitution for that purpose of a distinct apparatus and a special course of observation. It was not until January 1845 that the series of determinations of the absolute Horizontal Force were commenced with the Unifilar Magnetometer, which had been sent from Woolwich to Toronto for the purpose of supplying this failure in The observations with the Unifilar, discussed in the sequel of this volume, show that from January 1845 to December 1852 inclusive the mean annual decrease of the terrestrial Horizontal Force was '00371 in absolute measure; or $\frac{\Delta X}{X} = -\frac{.00371}{3.53} = -.00105$; and as it further appears by the monthly determinations of the Inclination, also discussed in the sequel of this volume, that we may assume the annual increase of the Inclination from the commencement of 1844 to the

end of 1855 to have been approximately uniform, and to have averaged 0'.8, we may perhaps venture to extend the estimate of the annual decrease of the Horizontal Force $\left(\frac{\Delta X}{X} = -0.00105\right)$ from January 1845 to December 1852 to one year beyond those limits—namely, 1844; whereby we may obtain a standard of comparison for the times of horizontal vibration of the Vertical Force needle observed between February 1844 and June 1848, applicable to the whole of the Magnetometer observations in Table LXX.

(It will be seen by the observations of the Inclination that we should not be justified in extending the same annual increase of the Inclination to the years preceding 1844; and since the annual change of the Horizontal Force is in part dependent on that of the Inclination, we are not possessed of sufficient data to permit a satisfactory deduction of the rate of change of the magnetism of the needle to be derived from its horizontal vibrations from an earlier date than February 1844.)

In November 1843, and to the beginning of February 1844, the Vertical Force needle was dismounted for the purpose of having experiments made on its temperature correction. By these experiments the magnetism of the needle was considerably weakened: its time of vertical vibration, which had been 10°·31 in October 1843, was found in February 1844, 12^s · 79 (Vol. II., Table XXXV., p. lxi). It happened accidentally that at the time when the second Toronto volume was published, it was not known at Woolwich that any observations had been made on the time of horizontal vibration between September 30, 1841, and March 26, 1846 (as stated in Vol. II., p. lxi). It was obvious, however, from the difference in the times of vertical vibration referred to above, that the needle had sustained a considerable loss of force during the temperature experiments (October 1843 to February 1844), and that this must have been known to Captain Younghusband, who was then Director of the Observatory. Believing, from the usual careful habits of that officer, that it was very unlikely that he should have remounted the needle for a fresh series of Magnetometer observations without previously observing its time of horizontal vibration, I had the "Miscellaneous Register Book" examined, in which a record of the observations, if made, would probably be found, and which book had been sent home to Woolwich when the Observatory was transferred to the provincial authorities. I have thus ascertained that the time of horizontal vibration was observed, as I had expected, on the 5th and 6th of February 1844, before the needle was remounted, and again in the beginning of June 1845, when the first of the continuous series in Table LXX. was completed. The time of horizontal vibration was again observed on the 26th of March 1846, when the second continuous series terminated. The needle was then remagnetized; its time of horizontal vibration observed before it was remounted, in the

beginning of April 1846, for the third series; and again observed on the 28th of February 1849. The times of vibration at these several dates were as follow:—

For the change in the magnetic moment of the needle in the first of the three continuous series in Table LXX. (viz. of 16 months, from February 1844 to May 1845 inclusive) we have consequently an increase in the time of the needle's horizontal vibration of $(11^s \cdot 490 - 11^s \cdot 460 =) 0^s \cdot 030$ in 16 months, or $\cdot 0223$ in a year, corresponding to a proportionate decrease of $\cdot 00389$ in parts of the force. But the Horizontal Force itself decreased during the same period at the average rate of $\cdot 00105$ in a year (p. ci). We find, therefore, the proportionate loss of force of the needle between February 1844 and June 1845 to have been at the mean annual rate of $(\cdot 00389 - \cdot 00105 =) \cdot 00284$. Now it has been shown (p. xcviii) that in the same period the monthly scale-readings of the Vertical Force Magnetometer diminished at the average rate of $2 \cdot 64$ scale divisions in a month, or $31 \cdot 68$ in a year, corresponding to $(31 \cdot 68 \times \cdot 0000628 =) \cdot 00199$ parts of the force; therefore the true secular change of the Vertical Force in those 16 months, allowing for the change in the magnetism of the needle, was an *increase* at the mean rate of $(\cdot 00284 - \cdot 00199 =) \cdot 00085$ in a year.

For a similar deduction during the second continuous series in Table LXX. (seven months, from September 1845 to March 1846) we have an increase in the time of horizontal vibration of $(11^s \cdot 4695 - 11^s \cdot 460 =) 0^s \cdot 0095$ in seven months, or $\cdot 0163$ in a year, corresponding to a proportionate decrease of $\cdot 00284$ in parts of the force; we have, therefore, a proportionate loss of force of the needle between September 1845 and March 1846 of $(\cdot 00284 - \cdot 00105 =) \cdot 00179$. The mean monthly decrease in the scale-readings of the Magnetometer (p. xcviii) was 1.47 scale divisions, or 17.64 in a year, corresponding to $(17.64 \times \cdot 0000628 =) \cdot 00111$ parts of the force. Therefore the secular change of the Vertical Force in these seven months was an increase at the mean rate of $(\cdot 00179 - \cdot 00111 =) \cdot 00068$ in a year.

For the third and longest series in Table LXX. (27 months, April 1846 to June 1848 inclusive) we have a mean rate of increase in the time of the needle's horizontal vibration, derived from the observations of the 1st of April 1846 and the 28th of February 1849, of $(10^{\circ} \cdot 3649 - 10^{\circ} \cdot 2879 =) 0^{\circ} \cdot 077$ in 35 months, or $\cdot 0264$ in a year, corresponding to a proportionate decrease of $\cdot 00513$ in parts of the force; and therefore an annual diminution of the magnetic moment of the needle of $(\cdot 00513 - \cdot 00105 =)$ $\cdot 00408$ in a year. The mean monthly decrease in the scale-readings of the Mag.

netometer between April 1, 1846, and June 30, 1848, was $2 \cdot 08$, or $24 \cdot 96$ in a year; and the corresponding decrease in parts of the force $(24 \cdot 96 \times \cdot 0000662 =) \cdot 00165$; therefore the secular change of the Vertical Force in this period, allowing for the change in the magnetism of the needle, was an increase at the mean annual rate of $(\cdot 00408 - \cdot 00165 =) \cdot 00243$ parts of the force.

Between February 1844 and June 1848 we have, therefore, three continuous series with the Vertical Force Magnetometer, by each of which we find the secular change of the Vertical Force at Toronto to have been an increase. The results collected are as follow:—

Giving each of these results weight proportioned to the time it represents, we have a mean annual increase of the Vertical Force derived from 50 months of Magnetometer observations of .00168 parts of the force.

Secular Change of the Total Force.—We have thus the mean annual secular change of the Vertical Force between February 1844 and June 1848, $\frac{\Delta Y}{Y} = + \cdot 00168$; and from the monthly determinations of the absolute Horizontal Force, discussed in the sequel of this volume, $\frac{\Delta X}{X}$ at the same period = $-\cdot 00105$; and as $\frac{\Delta \phi}{\phi} = \cos^2 \theta \cdot \frac{\Delta X}{X} + \sin^2 \theta \cdot \frac{\Delta Y}{Y}$, and θ at the mean epoch = 75° 16′, we have—

$$- \cdot 00105 \cdot \cos^2 75^\circ 16' + \cdot 00168 \cdot \sin^2 75^\circ 16' = + \cdot 0015 = \frac{\Delta \phi}{\phi}$$

or $\Delta \phi = + .0015 \times 13.9 = + .0208$, the annual increase of the Total Force in absolute measure.

The conclusions to be drawn from the times of vertical vibration, in regard to the loss of magnetic force which the needle sustained during the Magnetometer observations (and, correlatively, to the increase of the Earth's Vertical Force during the same period), must necessarily be less satisfactory than those derived from the times of horizontal vibration, because we have no independent measure, by a distinct apparatus (as we have in the case of the Horizontal Force), of the change which the Vertical Force underwent in the interval during which the vertical vibrations measured the constant or varying product of the Earth's Vertical Force into the force of the needle. In referring to Vol. II., Table XXXV., p. lxi, it will be seen that the monthly series of observations of

the times of vertical vibration between February 1844 and June 1848 may be divided into two distinct portions; the first comprising from February 1844 to March 1846 (the needle having been remagnetized on the 28th of March 1846), and the second portion comprising from April 1846 to June 1848. In the first interval the small decrease which will be seen to have taken place in the times of vibration indicates an increase,—and on the other hand the small increase in the times of vibration in the second interval indicates a decrease,—in the product of the magnetic force of the needle into the Earth's Vertical Force. The increase in the one interval and the decrease in the other are both extremely small, and, when the two intervals are taken together, in great measure counterbalance each other. We may therefore regard the times of vertical vibration as indicating a very near approach to constancy in the conjoint forces of the earth and of the needle. But the combined evidence of the Magnetometer observations and of the times of horizontal vibration has shown, that throughout this whole period the needle was losing force, and therefore the earth must have gained the force which the needle lost,—or the times of vertical vibration would not have approached so nearly to constancy. The times of vertical vibration are therefore in accordance with those of horizontal vibration, in manifesting that the Vertical Force of the earth was increasing from 1844 to 1848; though, for many reasons, they are less suited than the times of horizontal vibration to give, by their combination with the Magnetometer observations, a satisfactory result in regard to the rate of increase.

It is much to be desired that the subject which has been here considered should receive a further elucidation by the continuance of observations of the same kind at the Toronto Observatory, which has now passed into the hands of a provincial administration, and retains the instruments with which the valuable observations which have now been discussed were made. To these the method since devised by Dr. Lloyd for the absolute determination of the Vertical Force and of its variations from time to time,—and of the Total Force and its variations,—by direct observation, would be an important auxiliary. It is a research which might also well repay the Directors of the Harvard College Observatory in Cambridge, in the United States, should they think fit to resume their magnetical observations, which commenced with such good promise, but were too soon abandoned.

It has been conceived that the progressive approach of the minor maximum of the force, now in the eastern part of Siberia and moving towards America, should augment the force at the American maximum, and that consequently the force at the American maximum ought at the present epoch to be increasing. If this supposition be correct, the observed increase of the total force at Toronto may be a consequence of the general increase of the total force in the vicinity of the American maximum, from the nearer approach of the two points of maxima to each other; or it may be a consequence of a systematic movement of translation of the isodynamic lines in the same vicinity;

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or it may be due in part to each of these causes. The solution of such questions, which are of the first importance in relation to the secular change which the general magnetic condition of the earth is undergoing, seems imperatively to require the employment of cotemporaneous or nearly cotemporaneous observations at more than one locality in the region surrounding the maximum. In this respect Toronto is at present unaided: there is, indeed, a Magnetic Observatory at Sitka, on the north-west side of the American continent; but, unfortunately, we are not supplied by it with corresponding observations to those which have been here discussed, as the central Observatory at St. Petersburg did not succeed in constructing a Vertical Force Magnetometer. Amongst the British possessions in that quarter of the globe, perhaps Newfoundland presents practically the most eligible site for a Magnetic Observatory to be maintained in action for at least five or six years.

HORIZONTAL FORCE IN ABSOLUTE MEASURE.

The second volume of the Toronto Observations contains, in pp. 595—633, a detailed statement of the monthly observations made with the Unifilar Magnetometer to determine the value of the Horizontal Force in absolute measure, and its annual and secular variations. In the reference made to those observations in the early part of the same volume, pp. lxxxix and xc, it is stated that "as absolute determinations the "results can only yet be considered as provisional, as the exact values of the distances between the centres of the suspended and deflecting magnets, and of the constants of inertia and of induction, will have to be finally determined with the new standard "scale and weights on the return of the Unifilar to England."

Since the publication of that volume, the Unifilar has been brought back to Woolwich, and the graduation of its scale has been compared by Mr. Welsh, of the Kew Observatory of the British Association, with a certified copy of the British standard scale belonging to that observatory. The weight and dimensions of the two rings, employed at Toronto to determine the moment of inertia of the deflecting magnet and the stirrup in which it was suspended during the vibration-observations, have also been examined by Mr. Welsh, and their values assigned in terms of authenticated copies of the British standards of weight and measure.

Mr. Welsh's memorandum of the result of his measurements is as follows:—

Measurement of the Distance-arms of the Unifilar of the Toronto Observatory, and of the Half-length of the Magnet.

Distance of the point, 1 foot, on the one arm, to the point, 1 foot, on the other arm, = 23.960 inches at 62° .

The two arms are not in this instrument of one continuous piece of metal; it is therefore necessary in this case to consider the error of the distance as a constant error at all distances. It appears, therefore, that all the observed distances should be corrected by -0.001666 foot.

The half-length of the magnet I. 18 = 0.1526 of a foot, with a probable error arising from irregularity of figure of $\pm .0001$ foot.

Dimensions of the Inertia Rings employed at the Toronto Observatory.

Ring No. 1.

Weight, 288.900 grains; external diameter, 2.9886 inches at 62°; internal diameter, 2.6097 inches at 62°.

Ring No. 3.

Weight, 358.462 grains; external diameter, 3.6472 inches at 62°; internal diameter, 3.2626 inches at 62°.

Kew Observatory, May 1856.

J. Welsh.

1. In respect to the deflection distances. In different experiments the near end of the deflecting magnet was placed at $1\cdot 0$ ft., $1\cdot 1$ ft., $1\cdot 2$ ft., and occasionally at $1\cdot 3$ ft. from the centre of the suspended magnet, as measured on the graduated arms of the Unifilar; corresponding by Mr. Welsh's memorandum to $0\cdot 9983$ ft., $1\cdot 0983$ ft., $1\cdot 1983$ ft., and $1\cdot 2983$ ft. of British measure at 62° Fahrenheit. To these must be added in each case half the length of the deflecting magnet, making the deflection distances in the different experiments respectively $1\cdot 1509$ ft., $1\cdot 2509$ ft., $1\cdot 3509$ ft., and $1\cdot 4509$ ft. On reference to Vol. II. p. 634, it will be seen that these differ only $\cdot 0001$ in each case from the distances as measured by Captain Lefroy at Toronto in 1851, and employed by Captain Younghusband in computing the values of $\frac{m}{X}$ in pp. 593-633, except that the temperature of the scale on which the measurements were made by Captain Lefroy at Toronto was 50° Fahrenheit, and in Mr. Welsh's measurements 62° Fahrenheit. These differences are so minute, that it has not been considered expedient to make any alterations in the values of $\frac{m}{X}$ as computed by Captain Younghusband.

2. The weight and dimensions of the inertia rings as determined by Mr. Welsh, do not harmonize quite so well with the memorandum which accompanied the rings when sent to Toronto by their maker, Mr. William Jones, of Rupert Street; and it has therefore been necessary to recompute the moment of inertia of the deflecting magnet with the stirrup in which it was placed for the experiments of vibration. Employing Mr. Welsh's measurements, K', the moment of inertia of the ring, = 3.94785 for ring 1, and 7.45135 for ring 3. Substituting these values for 3.93024 and 7.43213, derived from previous measures, and employed by Captain Younghusband in calculating the log. value of $\pi^2 = 1.6558266$ as given in the memorandum in Vol. II. p. 634, we obtain the corrected log. values, viz. 1.65724 by ring 1, and 1.65748 by ring 3; and by the mean of the two rings, 1.65736. The values of T^2 and T^1 (the times of vibration of the magnet with and without the rings) employed by Captain Younghusband were obtained by three experiments of vibration with the large ring, three with the small ring, and three with the magnet alone, made in the autumn of 1845.

The results of the whole series, thus finally computed, are given in the following table:—

TABLE LXXIII.

Abstract of the Monthly Determinations of the Horizontal Force in absolute Measure.—The "Times of Vibration" are corrected for the Torsion of the Suspension Thread and the Rate of the Chronometer, and are reduced to an uniform Temperature of 50°, and to the Mean Bifilar Reading on the Day of Observation. The Values of $\frac{m}{X}$ are obtained from the Distances and from the Angles of Deflection stated in detail in Vol. II. pp. 596—632. The Angles of Deflection are reduced to the same uniform Temperature as the Times of Vibration, and to the Mean Bifilar Reading on the Day of Observation.

	70-4-		Time	No. of	Logarithm	Horizontal Force	
Date.	of Vibration.	Experiments of Vibration.	m X.	$\frac{m}{X}$	in absolute Measure (British Units).		
1845:			8.				
January	15	-	4.8132	1	0.29249	9.19304	3.2460)
,,	16	-	4.8126	1	0.29260	9.19230	3.5494 >3.5472
"	17	-	4.8176	1 1	0.29170	9.19216	3.2463)
February	14	-	4.8182	1	0.29154	9.19245	3.5444)
,,	15	-	4.8138	1	0.29239	9.19292	3.5459 > 3.5471
"	17	-	4.8112	1	0.29286	9.19217	3.2210)
March	14	- 1	4.8163	1	0.29194	9.19243	$\frac{3.5462}{3.5400}$ 3.5471
,,	15	-	4.8176	1	0.29171	9.19174	3.2480 } 3.2411
April	14	-	4.8461	1	0.28658	9.18782	3.2431)
,,	15	- 1	4.8467	1	0.28646	9.18755	3.5437 > 3.5446
"	16	- 1	4.8449	1	0.28680	9.18702	3.2471

TABLE LXXIII.—continued.

			Time	No. of Experiments	Logarithn	nic Values.	Horizontal F orc e
Date				of			in absolute Measure
			of Vibration.	Vibration.	m X.	\tilde{X}	(British Units.)
1845:			8.				
	13	-	4.8485	1	0.28612	9.18692	3.2450)
,,	14	_	4.8469	1	0.28644	9.18578	3.2509 > 3.2481
,,	15	-	4.8501	1	0.28587	9.18578	3.24827
June	14	-	4.8489	1	0.28608	9.18619	3.2477
,,	16	-	4.8501	1	0.28587	9.18504	3.5515 3.5514
- "	17	-	4.8486	1 1	0.28613	9.18444	3.5550)
	14	-	4.8553	1	0.28493	$9.18431 \\ 9.18283$	$\left\{\begin{array}{c} 3.5507 \\ 3.5511 \end{array}\right\}$ 3.5508
"	15 16	-	4.8631 4.8654	1 1	$0.28354 \\ 0.28313$	9:18255	3.2202 }
August	15		4.8671	i	0.28283	9.18287	3.2480
	16		4.8722	i	0.58195	9.18213	3.5473 3.5473
" "	18		4.8750	1	0.28142	9.18182	3.5465
September	16	•	4.9164	2	0.27407	9.17412	3.2479
	17	•	4.9194	2	0.27354	9.17408	3.2460 3.2466
,,,_	18	-	4.9199	1	0.27345	9.17422	3:5452)
October	14	-	4.9027	1	0.27650	9:17740	$3.5445 \ 3.5467 \ 3.5466$
99	15	-	4.0000	1.	0.27623	9°17657 9°17653	$\begin{pmatrix} 3.5467 \\ 3.5485 \end{pmatrix}$
November	16	-	4 ' 9020 4' 9053	1 1	$0.27662 \\ 0.27604$	9.17598	3.2484)
	14		4.9118	1 1	0.27489	9.17490	3.2481 > 3.2471
"	15	-	4.9141	i	0.27448	9.17530	3.2448
December	15	-	4.9427	ī	0.26943	9.16995	3.5461
	16	-	4.9488	1	0.26836	9.16974	3.5425 3.5479
"	17	-	5.0321	1	0.25386	9 .1 5418	3 5468 (
"	18	-	5.0141	1	0.25645	9.15450	3.227
1846:	1.4		5:00 00	2	0.25798	9.15778	3.2490)
	14 15	-	5.0083 5.0145	$\frac{2}{2}$	0 25798	9:15656	3.2490
"	16	-	5.0227	1	0.25548	9.15614	3.5454 >3.5475
"	17	-	5.0204	î	0.25588	9.15692	3.2439
,,	$\overline{22}$	-	5.0215	1	0.25569	9.15623	3.2460
February	14	-	5 0145	2	0.25691	9.15898	3.2399
,,	16	-	5.0123	2	0.25675	9.15842	3.2414 3.2413
, ",	17	-	5.0172	2	0.25644	9.15780	3:5426)
March	14	-	5°0498	2	0.25081	9 · 1527 5 9 · 15297	3.5403
,,	16 17	-	5*0454 5*0530	$\begin{bmatrix} 2 \\ 2 \end{bmatrix}$	$0.25158 \\ 0.25026$	9 13297	$\frac{3.5424}{3.5493}$ 3.5441
,,	18	_	5.0602	$\frac{2}{2}$	0.54905	9.14994	3.5444
$\mathbf{A}^{"}_{\mathrm{pril}}$	15	_	5.0795	$\tilde{2}$	0.24572	9.14702	3.5428)
Mpm "	17	_	5.0805	2	0.24560	9.14706	3.5422 > 3.5414
"	18	-	5.0824	$\frac{2}{2}$	0.24525	9.14742	3.5392)
May	13	-	5.0825	2	0.24520	9:14668	3.5421
	14	-	5.0840	2	0.24495	9.14687	3.5403 3.5414
т "	16	-	5.0827	2	0.24517	9°14670 9°14536	3·5419 <i>)</i> 3·5455)
June	16	-	5.0854 5.0856	$\begin{vmatrix} 2\\2 \end{vmatrix}$	0°24471 0°24467	9 14556	3.5452 > 3.5458
"	$\frac{17}{18}$	-	5.0856 5.0859	$\frac{2}{2}$	0.24462	9.14498	3.5467
July,	14	-	5.0910	2	0.24375	9.14448	3.2425
•	15	_	5.0922	$\begin{bmatrix} 2\\2\\2\\2\\2 \end{bmatrix}$	0.24355	9.14483	3.2429 > 3.2446
	16	_	5.0918	2	0.24362	9.14420	3.2428)
"						į.	

TABLE LXXIII.—continued.

		Time	No. of	Logarithn	nic Values.	Horizontal Force
Date,		of Vibration.	Experiments of Vibration.	m X	$\frac{m}{X}$	in absolute Measure (British Units).
1846:		8.				
August 13	-	5.1016	2	0.24194	9.14382	3.2402)
,, 14	-	5.1030	2	0.24171	9'14366	3.5401 > 3.5397
" 15	-	5.1040	2	0.24154	9.14392	3.5384
September 14	-	5.1144	2 2 2 2 2 2 2 2	0.23977	9.14246	3.5372)
,, 15	-	5.1112	2	0.24026	914234	3.5397 >3.5390
" 16	-	5.1110	2	0.24035	9.14228	3.2402)
October 12	-	5.1170	2	0.23933	9°14165	3.5387
,, 13	-	5 1169	2	0.23934	9°14197	3.5374 >3.5386
,, 14	-	5.1163		0.23945	9.14149	3.2398
November 16	-	5.1177	1	0.23921	9.14028	3.2438
" 17	- 1	5.1180	2 2 2 2	0.23916	9.14229	3.5354 > 3.5360
, 18	-	5.1209		0.23866	9.14245	3.5327)
December 15	-	5.1196	2	0.23889	9.14058	3.5412
, 16	-	5.1182		0.23914	9.14006	3.5444 >3.5433
" 17	-	5.1174	2	0.23926	9.14021	3.2443)
1847:		#41001		0.00		
January 18	-	5.1261	2	0.23778	9.13899	3.2432
, 19	-	5.1240	2	0.23814	9.13881	3.5454 3.5435
" 20	-	5.1266	2	0.23770	9'13916	3 3422
,, 21	-	5.1234	2	0.23824	9.13943	3.2432
February 15	-	5.1283	1	0.23741	9.13888	3:5422
" 16 " 17		5°1293 5°1280	1 1	0.23724	9.13892	3.2413
″ 10	- 1	5 1230 5 1237	1	$0.23746 \\ 0.23819$	9.13920	3.5410 3.5426
,, 18 ,, 19		5.1281	1 1	0.23744	9.13865	3.5463
March 15	- 1	5.1323	l i l	0.23673	9·13884 9·13993	3 · 5424 J 3 · 5352 \
16	-	5.1286	1	0.23736	9.13903	1 2.2412
7 17	-	5.1315	l î	0.23692	9.13919	3.5389 3.5386
" 19		5*1305	i	0.23704	9.13926	3.5391
April 14	-	5.1331	2	0.23660	9.13927	3.5373
., 15	-	5.1338	$\overline{2}$	0.23648	9.13935	2.5265
" 16	-	5.1344	2	0.23638	9.14041	$\frac{3.5318}{3.5318}$ 3.5348
,, 19	-	5.1345	1	0.23636	9.13995	3.5335)
May 15	-	51312	$\frac{2}{2}$	0.23692	9.13870	3.5409
,, 17	-	51358	2	0.23614	9.13939	3.2349
" 19	-	5.1312	2	0.23687	9.13906	3.5392
,, 20	-	51329	2	0.23663	9.13879	3.2394)
June 15	-	5.1306	1	0.23702	9.13911	3.2396
,, 16	-	5 1341	2	0°23643	9.13857	3.2392 (3.2300
,, 17	-	5 1328	2	0.23665	9.13894	0 0000
,, 18	-	5.1298	2	0.23716	9.13875	3.24177
July 14	-	5.1388	3	0.23563	9.13886	3.2320
,, 15	-	5.1387	3	0.23565	9.13816	3.5379 3.5366
,, 16	-	5'1412	2	0.23523	9.13803	3.2368 J
August 17	-	5.1413	2 2	0.33521	9.13646	3.2431
,, 18	-	5.1413	2	0.23521	9.13675	3.5419 3.5424
,, 19	-	5.1438	2	0.23480	9.13624	3.5423)
September 15	-	5.1516	2	0.23347	9.13607	3.5335
,, 16	•	5°1550	$\begin{vmatrix} 2 \\ 0 \end{vmatrix}$	0.23290	9.13644	3.5337 3.5338
,, 17	-	5 1529	2	0.23325	9.13653	3.5348)

TABLE LXXIII.—continued.

		Time	No. of Experiments	Logarithn	nic Values.	Horizontal Force
Date.		of Vibration.	of Vibration.	<i>m</i> X.	$\frac{m}{X}$.	in absolute Measure (British Units).
1847 :		s.				
October 16	-	5.1544	2	0.23300	9.13573	3.2370
" 18	-	5.1572	2	0.23255	9.13591	3.5344 3.5345
,, 19	-	5.1578	2	0.23243	9.13622	3 3327
" 20 November 16	-	5°1580	2	0.23249	9.13587	3·5340J 3·5357)
177		5°1576 5°1576	2 9	0°23246 0°23246	9·13550 9·13540	3.2365
,, 17	-	5.1566	2	0.23263	9.13518	3.5378
December 16	-	5.1587	2 2 2 2	0.23228	9.13469	3.2384
" 18	-	5.1649	2	0.23123	9.13539	3.5313 3.5347
,, 21	-	5.1708	2	0.23025	9.13573	3 3238
" 24	-	5.1636	2	0.23145	9.13263	3.24347
1848:						
January 17	-	5.1687	2	0.23060	9.13488	3.5307
,, 18	-	5.1 661	2 2	0.23103	9.13505	3:5320 3:5329
" 19 February 16	-	5·1 638 5·1 653	1	0°2314 2 0°23117	9°13443 9°13438	3'5359 <i>)</i> 3'53507
17	_	5°1653	2	0.23117	9.13427	9.5955
,, 17 ,, 18	-	5.1655	2	0.23113	9.13405	3.5363 3.5352
, , 19	- [5.1662	2	0.23102	9.13453	3.2339
March 13	-	5.1623	$\begin{bmatrix} 2 \\ 2 \end{bmatrix}$	0.23167	9.13387	3.5392
,, 14	-	5.1617	2	0.23177	9.13433	3:5378 3:5372
,, 15 April 17		5°1654 5°1658	2	$0.23115 \\ 0.23108$	9°13450 9°13424	3.5345) 3.5352)
10		5.1662	2 2	0.23103	9.13392	3.2363 > 3.2361
", 18 ", 19	-	5.1639	$\frac{1}{2}$	0.23140	9.13418	3.5368
May 15	-	5.1638	2 2 2 2	0.23142	9.13361	3.5392
" 16	-	5.1626	2	0.23165	9.13383	3.5391 3.5386
,, 17	-	5.1613		0.23184	9.13448	3.5374)
June 15	-	5°1668 5°1653	$\begin{vmatrix} 2 \\ 9 \end{vmatrix}$	0°23091 0°23117	9°13379 9°1341 5	$\left(\begin{array}{c} 3.5365 \\ 3.5360 \end{array}\right) 3.5366$
17		5 1648	$egin{bmatrix} 2 \ 2 \ 2 \end{bmatrix}$	0.23125	9.13394	3.5372
July 18	-	5.1687	2	0.23060	9.13305	3.5382)
" 19	- 1	5.1653	2	0.23117	9.13318	3.5399 3.5376
" 20	-	5.1711	2	0.23020	9.13348	3.5348
August 15	-	5.1892	2	0.22716	9.13062	3:5340
,, 16	-	5°1839	2 2	0.22804	9.13056	3:5379 3:5360
,, 17 ,, 18		5°1877 5°1865	$\frac{2}{2}$	$0.22741 \\ 0.22761$	9°13026 9°13073	$\begin{bmatrix} 3.5366 \\ 3.5355 \end{bmatrix}$
September 15	-	5 1952	1	0.22612	9.12982	3.2335
" 16	-	5.1929	2	0.22654	9.12989	3.2342 3.2332
" 19	-	5.1958	2	0.22605	9.13004	3.2319)
October 17	-	5.2011	2	0.22517	9.12909	3:5321
,, 19	-	5.2089	$\begin{vmatrix} 2 \\ 0 \end{vmatrix}$	0.22387	9.13024	$\begin{vmatrix} 3.5222 \\ 2.5212 \\ 3.5263 \end{vmatrix}$
" 20 " 21	-	5°2128 5°2010	$\begin{vmatrix} 2\\2 \end{vmatrix}$	$0.22322 \\ 0.22518$	9°12982 9°12972	$\begin{bmatrix} 3.5213 \\ 3.5296 \end{bmatrix}$
November 21		5 2010 5 2088	$\begin{vmatrix} 2\\2 \end{vmatrix}$	0.22388	9 12972	3.5260
00		5·2112	$\frac{2}{2}$	0.22348	9.12915	3.5251 3.5249
,, 22 ,, 23	-	5.2133	2	0.22313	9.12921	3.232
December 19	-	5.2019	2	0.22503	9.12896	3.2325
December 13						
,, 20 ,, 21	-	5 · 2022 5 · 2044	$\begin{bmatrix} 2 \\ 2 \end{bmatrix}$	0°22498 0 °22462	9°12904 9°12869	$\begin{vmatrix} 3.5316 \\ 3.5316 \end{vmatrix}$ 3.5318

Table LXXIII.—continued

	Time	No. of	Logarithmic Values.		Horizontal Force
Date.	of Vibration.	Experiments of Vibration.	$m \mathbf{X}$	$rac{m}{\widetilde{\mathbf{X}}}$	in absolute Measure (British Units).
				<u> </u>	
1849:					
	s.		0.000	0.10077	0.5050.
January 15 -	5:2095	$\frac{2}{2}$	0.22377	$9.12877 \\ 9.12784$	$\left\{\begin{array}{c} 3.5278 \\ 3.5340 \\ \end{array}\right\}$ 3.5319
,, 16 -	5.2058	$\begin{vmatrix} 2\\2 \end{vmatrix}$	$0.22438 \\ 0.22445$	9.12784 9.12798	3.5338
" 17 - February 17 -	5°2054 5°2071	$\frac{2}{2}$	$0.22445 \\ 0.22417$	9.12798	3.2334
10 -	5.2106	$\frac{2}{2}$	0.22358	9.12761	3.5317 3.5312
" 20 -	5.2127	2	0.52323	9.12802	3.5286
March 19 -	5.2065	2	0.22427	9.12747	3.5351)
90 -	5.2089	$\frac{1}{2}$	0.22387	9.12764	3.5328 > 3.5339
" 91 -	5.2067	2	0.22423	9.12769	3.2341)
April 19 -	5.1998	2	0.22537	9.12721	3.2407)
,, 20 -	5.2013	2	0.22513	9.12691	3.5410 3.5378
, 21 •	5.2153	2	0.22280	9.12678	3.2319)
May 16 -	5.2052	2	0.22448	9.12587	3.2425
,, 17 -	5.2036	2	0.22475	9.12690	3.5394 >3.5413
,, 18 -	5.2036	2	0.22475	9.12622	3.5422
June 18 -	5.2102	2	0.22360	9.12541	3.5407
" 19 -	5.2058	2	0.22438	9.12551	3.5436 3.5389
,, 20 -	5.2187	2	0.22223	9.12608	3.5325
July 17 -	5:2040	$\frac{2}{2}$	0.22468	9.12470	3.5480
,, 18 -	5:2116	$\begin{array}{c c} 2 \\ 2 \end{array}$	0°22342 0°22290	$9.12486 \\ 9.12538$	$\begin{pmatrix} 3.5423 \\ 3.5380 \end{pmatrix}$ 3.5428
,, 19 - August 16 -	5·2147 5·2218	$\begin{vmatrix} z \\ 2 \end{vmatrix}$	0.22172	9 12378	3.5397
August 16 - 17 -	5.2193	$\begin{vmatrix} \frac{2}{2} \end{vmatrix}$	0.22213	9.12386	3.2411 >3.2394
" 18 -	5 2224	$\frac{2}{2}$	0.55165	9.12424	3.5375
September 19 -	5.2285	$\frac{2}{2}$	0.55060	9.12375	3.2323)
- 90 -	5.2282	$\frac{1}{2}$	0.22062	9.12319	3.5378 > 3.5382
" 20 - 21 -	5.2242	$\frac{1}{2}$	0.22132	9.12293	3.5416
October 15 -	5.2349	2	0.21954	9.12332	3.5328)
" 17 -	5.2329	2	0.21987	9.12341	3.5338 > 3.5343
,, 18 -	5.2315	$\begin{array}{ c c c }\hline 2\\2\\ \end{array}$	0.22010	9.12294	3.2366)
November 16 -	5.2343	2	0.21964	9.12270	3:5357)
,, 17 -	5.2319	2	0.22004	9.12267	3.5374 > 3.5366
" 19 -	5.2316	2	0.22009	9.12295	3.5365)
December 18 -	5.2396	$\frac{2}{2}$	0.21876	9.12223	3.5340
,, 19 -	5.2370	$\begin{bmatrix} 2\\2\\2\\2\\2 \end{bmatrix}$	0.21919	9.12203	3.5366 > 3.5351
" 20 -	5.2388		0.21890	9.12215	3·5349 J
1850:					
January 16 -	5.2390	2	0.21886	9.12222	3.5344)
17 -	5.2388	$\frac{1}{2}$	0.51890	9.12159	3.5372 > 3.5344
" 18 -	5.2423	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.51831	9.12236	3.5317
February 16 -	5.2430	$\overline{2}$	0.51850	9.12197	3.5328)
10	5.2383	2	0.21898	9.12200	3.5358 > 3.5354
" 19 -	5.2402	2	0.21861	9.12119	3.5377)
March 18 -	5.2379	2	0.21904	9.15181	3.2369
" 19 -	5.2337	2	0.21974	9.15115	3.5425 > 3.5387
,, 20 -	5.2407	2	0.21858	9.12136	3.5368
April 17 •	5.2400	2	0.21870	9.12121	3.5379
,, 18 -	5.2407	$\begin{vmatrix} 2\\2 \end{vmatrix}$	0.21858	9.12141	$\begin{vmatrix} 3.5366 \\ 3.5380 \end{vmatrix}$ 3.5373
,, 19 -	5.2397	1 1	0.21875	9.12122	1 3 538D L

TABLE LXXIII.—continued.

		Time	No. of Experiments	Logarithmic Values.		Horizontal Force
Date.	1		of			in absolute Measure
		of Vibration.	Vibration.	m X	$\frac{m}{X}$	(British Units).
					X	
1250						
1850: May 18		s. 5°2396	2	0.21876	9.12159	3.2366)
20		5 2 2 3 9 0	$\frac{2}{2}$	0.51843	9.12122	3.5368 3.5366
91	-	5.2410	$\frac{2}{2}$	0.51823	9.12140	3.2362
June 17	_	5.2454	2	0.21780	9.12093	3.5354
19	i	5.2425	$\frac{1}{2}$	0.51858	9.11995	3.2414 3.2380
" 10	1	5.2491	$\begin{bmatrix} 2 \\ 2 \end{bmatrix}$	0.21720	9.11981	3.5375)
July 16	,	5.4446	$\frac{1}{2}$	0.18542	9.09060	3.270
" 17		5.4443	$\begin{vmatrix} 2\\2 \end{vmatrix}$	0.18547	9.09043	3.280 3.2584
,, 18		5.4479	2	0.18490	9:08928	3.2303)
August 16	-	5.4543	2	0.18388	9.09097	3.21937
,, 17		5.4531	2	0.18407	9.09101	3.5200 > 3.2199
,, 19		5^*4492	$\begin{bmatrix} 2\\2\\2\\2\\2\\2 \end{bmatrix}$	0.18470	9.09149	3.205
September 16		5.4540	2	0.18393	9.09037	3.220
,, 17		5.4522	$\begin{bmatrix} 2 \\ 2 \end{bmatrix}$	0.18421	9.09051	3.5226 3.5217
,, 18		5.4534	$\frac{2}{2}$	0.18402	9:09077	3.5207
October 15		5.4554	2	0.18370	9.08771	3.5317
,, 16		5.4553	2	0.18372	9.08790	$\left\{\begin{array}{c} 3.5311 \\ 3.5343 \end{array}\right\} 3.5320$
, 17		5.4508	1	0.18444	9:08782	3.2326)
November 19		5.4569	$\frac{2}{9}$	0.18347	9°08654 9°08664	3.5378 3.5361
,, 20		5.4529	$\begin{vmatrix} 2\\2 \end{vmatrix}$	0°18410 0°18409	9.08734	3.5348
" 21 December 16		5.4530 5.4606	$\frac{2}{2}$	0.18288	9.08722	3.5305)
December 10		5 4630	$\begin{vmatrix} 2 \\ 2 \end{vmatrix}$	0.18250	9.08740	3.5282 3.5283
" 18		5.4667	$\frac{2}{2}$	0.18181	9.08733	3.5262
			4			
1851:						
January 15	-	5.4622	2	0.18262	9.08684	3.2310
,, 16		5.4772	2	0.18024	9.08748	3.5187 3.5249
,, 17		5*4693	$egin{bmatrix} 2 \\ 2 \\ 2 \\ 2 \end{bmatrix}$	0.18120	9.08721	3.5249
February 17		5. 4639	2	0.18232	9.08608	3.5330
,, 18		5.4768	2	0.18030	9.08751	3.5188 3.5243
,, 19		5.4760	2 2	0.18043	9.08711	3 · 5210) 3 · 5322)
March 17		5.4643	2	0.18229	9.08620 9.08697	3.5302 3.5321
" 18 " 19		$5^{\boldsymbol{\cdot}}4626 \ 5^{\boldsymbol{\cdot}}4622$	$\begin{vmatrix} 2\\2 \end{vmatrix}$	$0.18256 \\ 0.18262$	9.08609	3.5340
,, 19 April 15		5 4622 5 4650	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.18218	9.08606	3.2331
16		5.4652	$\frac{2}{2}$	0.18212	9.08593	3.5327 3.5311
7 17		5.4691	$\frac{2}{2}$	0.18123	9.08636	3.5284
May 15		5.4638	$\frac{1}{2}$	0.18237	9.08570	3.5345)
16		5.4627	2	0.18224	9.08596	3.5342 3.5328
17		5.4692	$egin{bmatrix} 2 \ 2 \ 2 \ 2 \ 2 \ \end{bmatrix}$	0.18121	9.08605	3.5297)
June 17		5.4444	2	0.18546	9.08912	3.2331 A
" 18		5.4501	2	0.18455	9.08868	3.2313 3.2311
" 19		5.4506	2	0.18447	9.08922	3.5288)
July 15		5.4515	2 2	0.18433	9.08897	3:5292
,, 16		5.4490	2	0.18472	9.08838	3.5332 >3.5317
,, 17		5.4518	2	0.18428	9.08802	3.5329
August 15		5.4561	2	0.18359	9.08786	3.5308
,, 16		5.4547	2	0.18385	9.08851	3.5291 3.5318
" 18	-	5 °4535	2	0.18401	9.08706	3.2322)
			1		1	1

TABLE LXXIII.—continued.

		m:	No. of	Logarithmic Values.		Horizontal Force
Date.		Time	Experiments			in absolute Measure
Date.		of Vibration.	of Vibration.	m X	$rac{m}{\mathbf{X}}$	(British Units).
					Λ	
1851:		8.				
September 16	; -	5.4611	2	0.18280	9.08730	3 5298
" 17		5.4638	2	0.18237	9.08749	3.5274 3.5286
,, 18		5.4632	2	0.18246	9.08725	3.5287
October 16		5.4660	2	0.18202	9.08640	3.5303
,, 17		5.4632	2	0.18246	9.08636	3.5322 3.5311
,, 18		5.4644	2	0.18227	9.08650	3.5309
November 17		5.4864	2	0.17878	9.08352	$\left(\begin{array}{c} 3.5288 \\ 3.5311 \end{array}\right) 3.5304$
, 18		5.4843	2	0.17912	9.08331	
,, 19		5.4820	$\frac{2}{2}$	0.17948	9.08362 9.08340	3.2313) 3.296)
December 15		5.4860	$\frac{2}{2}$	0°17885 0°17880	9.08346	3.5292 > 3.5286
,, 16 18		5.4863	2 2	0.17832	9.08351	3.5292 3.5280
,, 18	•	5.4893	2	0 17852	9 00001	3 3270)
1852 : January 16	;	5.4886	2	0.17844	9.08271	3.5307
17		5.4812	2	0.17960	9.08329	3.5332 > 3.5305
″ 10		5.4911	$\frac{1}{2}$	0.17804	9.08293	3.5276
February 17		5.5062	$\frac{1}{2}$	0.17565	9.08146	3.5246
10		5.5074	1	0.17546	9.08184	3:5222 3:5231
", 13 ", 23		5.5106	2	0.17496	9.08127	3 3223 (
,, 24		5.2102	2	0.17498	9.08127	3.226
March 15	-	5.2125	2	0.17466	9.08116	3.217
,, 16	-	5.2120	2	0.17474	9.08066	3.5240 3.5237
,, 17		5.5097	$\begin{bmatrix} 2 \\ 2 \end{bmatrix}$	0.17510	9.08095	3.5244)
April 16		5.22	2	0.17628	9.08763	3.5021
,, 17		5.4969	$egin{bmatrix} 2 \ 2 \ 2 \end{bmatrix}$	0.17712	9.08716	3:5074 > 3:5054
,, 19		5'5005	2	0.17655	9.08676	3:5067
May 17		5.4956	2	0.17733	9.08534	$\left \begin{array}{c} 3.5156 \\ 3.5148 \end{array}\right> 3.5142$
,, 18		5.4955	2	0.17734	9.08556	$\left(\begin{array}{c} 3.5148 \\ 3.5112 \end{array}\right)$
,, 19		5.5003	2	0.17658	9.08566	3.5058
June 16		5.2038	$\frac{2}{2}$	0°17603 0°17651	$9.08647 \\ 9.08628$	3.5084 3.5083
,, 17		5.5008 5.5023	$\frac{2}{2}$	0.17627	9.08551	3.2107
" 18 July 16		5.233	$\frac{2}{2}$	0.17611	9.08505	3.2120)
July 16		5.2021	2	0.17630	9.08488	3.2133 > 3.2138
19		5.252	2	0.17628	9.08462	3.5142
August 16		5.2022	2	0.17540	9.08463	3.5107)
17		5.2044	2	0.17594	9.08422	3.5145 3.5138
″ 19		5.2018	2	0.17635	9.08463	3.2165
September 16		5.251		0.17268	9.08116	3.5137)
" 17	7 -	5.5267	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.17243	9.08140	3.2117 >3.2118
,, 18		5.5262	2	0.17250	9.08182	3.2102)
October 16		5.5282	2	0.17219	9.08114	3.2118)
,, 18		5.5287	2	0.17211	9.08164	3.2092 3.2110
,, 19	-	5.5283	2	0.17218	9.08118	3.2116
November 18	3 -	5.5306	2	0.12181	9.08058	3.5125
" 19		5.5262	2	0.17250	9.08057	3:5154 >3:5140
,, 20		5.5286	2	0.17213	9.08046	3.2142
December 16	6 -	5.5270	2	0.17238	9.08020	3:5163
,, 17		5.5322	2	0.17156	9.07999	3.2139 3.2149
,, 18	3 -	5.2303	2	0.17186	9.08016	3.2144)

There is still another correction to be applied to these results, which could not be determined until the return of the Unifilar, at the close of the series, to Woolwich, where in the meantime an apparatus had been prepared for the purpose of ascertaining its amount. The necessity for this correction was first pointed out by Dr. Lamont in Dove's Repertorium, Band 7 (1846). In the experiments for measuring the absolute values of the Horizontal Force two operations are required; viz., experiments of vibration, and experiments of deflection: in the experiments of vibration the magnet is in the magnetic meridian; in those of deflection it forms with that meridian an angle which is in all cases considerable. But as it has been found that the earth elicits a sensible degree of magnetism by induction in hardened and magnetized iron or steel, it follows that when placed in the magnetic meridian a magnet is stronger than when it is perpendicular to or forms an angle with the meridian. In the usual mode of computing the results deducible from the combination of the vibration and deflection experiments, the strength of the magnet which is vibrated in the one case and used as a deflector in the other, is assumed to be the same, which, however, is not strictly true, for the reason which has been assigned; hence the necessity of the correction to which has been given, not inappropriately, the name of the inductioncorrection. As its value depends on the capacity of the individual magnet to receive a greater or less inductive charge, it requires, like the temperature-correction, to be determined for the particular magnet which has been employed, which in this case was I. 18 throughout the whole series. The apparatus made for this purpose at Woolwich was similar in principle to Dr. Lamont's, described in Dove's Repertorium, Band 7, and was adapted to one of the ordinary portable Unifilars: it has now been transferred to the Kew Observatory, where it will in future be employed to determine this amongst the other constants of the magnetic instruments supplied through that observatory. I am indebted to Mr. Welsh for the following memorandum of the correction to be applied to the Toronto results, which he has determined by using I. 18 in this apparatus.

Determination of the Induction Coefficient for the Deflecting Magnet I. 18 employed at the Toronto Observatory, 1845—1852.

The experiments have been made with the Woolwich induction apparatus by the method of Dr. Lamont.

Let μ = the magnetic moment induced in the bar by the action of a magnetic force equal to unity of the English measure.

 M_e = moment of permanent magnetism of the bar at the time of making the experiments for the induction coefficient.

 X_e = horizontal component of the earth's magnetic force at the time and place of the experiments.

i = magnetic dip at the same time and place.

 φ = angle of deflection produced upon the freely suspended needle, the deflecting bar being placed vertical with the north end *downwards*.

 φ' = angle of deflection, north end *upwards*.

Then-

$$rac{\mu}{\mathrm{M}_e} = rac{ anrac{1}{2}(arphi-arphi')}{\mathrm{X}_e \; an \; i \; anrac{1}{2}(arphi+arphi')}; \; or, \mu = rac{\mathrm{M}_e}{\mathrm{X}_e} \cdot rac{ anrac{1}{2}(arphi-arphi')}{ an \; i \; anrac{1}{2}(arphi+arphi')}$$

The effect (in parts of the whole magnetic moment of the bar) of the inducing action of the Horizontal Force at any time and place is obtained from the equation,

$$\frac{\Delta m}{m} = \mu \cdot \frac{X}{m}$$

The following are the results of experiments made at the Kew Observatory, January 17 and 19, 1857:—

January 17.	January 19.			
			-	
0 / //	0	,	"	
$\frac{1}{2}(\varphi - \varphi') = 0 24 38.5$	0	31	8.5	
$\frac{1}{2}(\varphi + \varphi') = 46\ 50\ 6.0$	52	39	2.0	
$i = 68 \ 25 \ 0.0$	68	25	0.0	
$\text{Log } \frac{\mathbf{M}_e}{\mathbf{X}_e} = 8.99790$	8	9979	90	
$\mu = 0.0002647$	0	.000	2722	
Mean value of $\mu = 0.00020$	685			

Hence we have for the different values of $\frac{m}{X}$ in Table LXXIII., values of $\frac{\Delta m}{m}$ ranging from 0.00173 to 0.00223; and taking the mean angle of deflection in the Table of the Toronto Observations, Vol. II. pp. 596—633, at 7°.5, the induction-correction applicable to X varies from -.0035 in the experiments of 1845 to -.0044 in those of 1852.

Kew Observatory, January 20, 1857.

J. Welsh.

We obtain, therefore, from Table LXXIII. the following finally corrected values of the absolute Horizontal Force in the several years from 1845 to 1852:—

TABLE LXXIV.

Years	Annual Means from Table LXXIII.	Annual Means corrected for Induction,	Years.	Annual Means from Table LXXIII.	Annual Means corrected for Induction.
1845	3.5478	3.5443	1849	3.5368	3.5328
1846	3.2419	3.2381	1850	3.2322	3.280
1847	3.2381	3.5342	1851	3.5299	3.255
1848	3.2339	3.299	1852	3.2124	3.2110

From the annual means corrected for induction we obtain 3.5305 as the absolute Horizontal Force corresponding to the mean epoch of the table, January 1st 1849; and $-.00371 \pm .00091$ as the mean annual secular change between 1845 and 1852 inclusive. The probable error of a single annual mean is $\pm .0026$; a large proportion of which is due to the observations of 1852, which I have not felt at liberty wholly to omit, as no accidental cause has been stated to be known for their apparent irregularity.

MAGNETIC INCLINATION.

The first volume of the Toronto Observations contained, in pp. 328—332, a detailed statement of the observations of the Inclination made monthly from January 1841 to December 1842 inclusive; the second volume contained, in pp. 559—594, a similar record of the continuation of the series from January 1843 to December 1852 inclusive. The second volume contained also, in pp. lxxxv—lxxxix, a discussion of the results obtained during those years. I have since been favoured by Mr. Kingston, Director of the Toronto Observatory since it has become a provincial establishment, with a continuation of the series during the years 1853, 1854, and 1855, conducted upon the previous model, of which the following is an abstract:—

Table LXXV.

Observations of Inclination continued from Vol. II., page 594. Needle employed, Gambey, No. 1.

				P	oles.			Po	oles.	
1853.	75°+	Monthly Means.	1854.	Direct, 75°+	Reversed,	Monthly Means.	1855.	Direct,	Reversed,	Monthly Means.
Jan. 17	22'-1	, ,	Jan. 1	$6 \mid 25^{'} \cdot 5$	17'1) ° ′	Jan. 15	30.8	16.4	۱ ، ، ،
,,	22.0	li 1	,	, 25.0	18.7			32.2	15.8	
,,	20.4		1		16.6	75 21.4	16	29.0	18.6	>75 24.0
"	20.3		i	, 25.2	16.6	1	17	28.4	20.4	
18	22.2		1	96.1	17.1		()	29.0	19.5	
"	22.4	75 22.06	Feb. 1	, .	15.2)	Feb. 15	29.1	17.6	\prec
"	22.4		,	20.0	17.6		,,	29.7	19.2	
" 19	22.2			6 29.8	16.6	75 00:4	16	27.6	20.1	77 00:0
,,	22.7		,	, 29.3	17.5	75 23.4	,,	27.2	20.4	275 23.8
,,	22.4		i		18.7	[]	17	28.4	20.0	
,,,	22.5	ا لاا	1 30	, 28.5	19.1	[]	Mr. 10	27.0	18.9	1
Feb. 16	$\begin{vmatrix} 23.0 \\ 22.1 \end{vmatrix}$]]	Mar. 1	95.0	18.3		Mar. 19	30.9	18.8 18.1	, }
. **	22.6]	,		17.4		20	29.4	17.7	
"	$\frac{22.8}{22.8}$		ľ	97.9	19.6	>75 23.1	11	28.8	18.2	} 75 23 ` 8
" 7	23.4		1	7 27.9	18.8		21	29.3	17.4	
,,	23.1	75 22.6	,	27.6	18.2	}	,,	29.7	17.4	J
"	22.0	13 22 0	April 1	7 27.8	19.5)	April 16	28.4	18.2)
,,	22.6		,	28.0	18.6		,,	28.7	17.8	
18	21.8] }	1	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	16.4	75 23.0	17	28.2	18°2 18°5	>75 23.0
"	22.8		i		18.8	j	18	27.2	17.9	-
"	$\frac{22.6}{22.6}$		1	27.0	17.2]]	,,	28.1	17.7	
March -		servations.	May 1		18.2	1	May 15	28.5	20.4	าั
April 8	23.0	ו ו	,	, 27.3	18.8	1	,,	26.6	20.9	
- ,,	22.5	75 22.6	i		18.7	>75 23.0	16	29.4	17.0	75 23.5
,,	22.6	IJ .	,	28.3	18.1	, , , , ,	;;	28.8	19.4	(10 20 0
May -	No of 23.2	servations.	1	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	17.7		11	28.7	16.8 16.6	
June 15 16	$\frac{23}{22} \cdot \frac{2}{1}$		June 1	, , -	18.6	15	June 18	$\frac{29}{27} \cdot 3$	17.3	\langle
-	$\frac{22}{22} \cdot \frac{1}{7}$	75 22.5	Joune 1	97.6	19.2	11	ounc 10	29.4	16.7	1
"7	22.0		ĺ		19.1	75 22.9	19	27.1	17.9	75 22.9
,,	22.2]	,	, 26.8	19.1	10 22 9	,,	26.7	17.7	710 22 9
July 18	21.6	1	1		20.3		20	28.1	19.7	
"	21.6		July 1	$\begin{array}{c c} , & 28.3 \\ 7 & 29.4 \end{array}$	18.3]	July 16	27.7 28.4	19°3 17°9	$ \downarrow $
19	$\begin{vmatrix} 21.5 \\ 21.0 \end{vmatrix}$	75 21.5		93.0	23.1		11	25.6	20.4	.
20	$\frac{21}{21.7}$		i		19.9		"7	27.5	18.1	
	21.5		,	90.3	19.8	75 24.3	,,	27.5	19.1	75 23.1
Aug. 16	21.0	1		9 28.0	20.6		18	27.6	18.9	
,,	20.1		,	, 27.6	23.4	J	,,,	27.3	19.1	لِ
17	20.0	75 20.25	Aug. 1		21.4] .	Aug. 15	27.4	19.6	7
"	20.1	1 20 20 1	,	$\frac{26.7}{26.8}$	22.4		16	26.6 27.5	19.8	
18	19.9		1	26.8	18.6	>75 23.2	[]	26.7	20.8	75 23.8
Sept. 16	20.4		i		17.6		17	28.6	19.0	. [
Schr. 10	20.8		1	25.8	19.9		,,	28.6	21.1	

TABLE LXXV.—continued.

		36 (1)		P	oles.	Manall		Po	oles.	March la
1853.	75°+	Monthly Means.	1854.	Direct, 75°+	Reversed, 75°+	Monthly Means.	1855.	Direct, 75°+	Reversed, 75°+	Monthly Means.
Sept. 17 18 Oct. 17 18 19 *Nov. 16 17 18 Dec. 15 16 17 17	22·1 21·7 21·7 22·5 22·9 22·5 21·6 22·9 22·1 22·7 22·2 23·2 23·2 23·2 23·2 23·2 23·2	\begin{cases} \cdot 75 & 21.7 \\ \cdot 75 & 22.4 \\ \cdot 75 & 23.0 \\ \cdot 75 & 22.3 \end{cases} \end{cases}	Sept. 18 19 20 Oct. 16 17 18 Nov. 16 17 18 Dec. 18 20 "	28·3 28·2 27·8 27·2 25·9 27·0 26·1 25·4 26·0 25·2 26·0 26·3 24·1 28·0 26·9 28·4 26·9 27·1 31·0 30·8 28·3 33·1 28·7 30·0	18 9 19 0 20 9 20 3 18 9 18 4 19 2 18 7 17 7 20 0 16 0 16 9 17 9 16 1 17 6 17 4 17 3 18 2 15 4 16 1 19 4 17 7 18 3 17 9	75 23·4 75 22·0 75 22·2 75 23·9	Sept. 17 18 19 Oct. 15 16 17 Nov. 13 16 17 Dec. 18 19 20 "	28.4 29.4 27.6 26.9 26.1 27.5 26.9 27.6 26.7 27.9 27.2 28.7 26.3 26.3 26.5 26.5 26.2 26.8 27.4 27.9 27.5 26.9 27.5	19'8 19'6 21'3 23'9 22'2 21'0 19'2 15'4 19'5 22'0 19'7 19'8 18'9 19'8 20'7 19'4 19'3 19'9 19'9 20'9 17'3 18'9 20'0 19'5	75 24·5 75 23·5 75 23·3

The annual means are 75° 22'·17, 75° 23'·0, and 75° 23'·55. Collecting the several annual means into one view, we have the following table:—

TABLE LXXVI.

Years.	Observed Inclination.	Years.	Observed Inclination.	Years.	Observed Inclination.
1841	75° 16' 6	1846	75 15 1	1851	75 20.4
1842	75 16.4	1847	75 15.3	1852	75 20.5
1843	75 14.7	1848	75 18'3	1853	75 22.2
1844	75 14.8	1849	75 18.8	1854	75 23.0
1845	75 15.5	1850	75 20.0	1855	75 23.6

^{*} Previous to the observations of November 1853 a new stone pillar was substituted for the original wooden one.

From these observations the Inclination appears to have reached an epoch of minimum between the years 1843 and 1844, or about the commencement of 1844; and from 1844 to 1855 to have increased at an average rate of $\frac{75^{\circ} \ 23' \cdot 6 - 75^{\circ} \ 14' \cdot 8}{11} = 0' \cdot 8$. On this supposition we have the computed Inclination in each of the twelve years, with the deviations from the observed values, as follows:—

Years.	Computed Inclination.	Computed— observed.	Years.	Computed Inclination.	Computed— observed.
1844	75 14.8	ó·o	1850	75° 19'·6	-ó·4
1845	75 15.6	+0.1	1851	75 20.4	-0.0
1846	75 16.4	+1.3	1852	75 21.2	+0.7
1847	75 17.2	+1.9	1853	75 22.0	-0.5
1848	75 18.0	-0.3	1854	75 22.8	-0.5
1849	75 18.8	-0.0	1855	75 23.6	-0.0

TABLE LXXVII.

The probable error of a single annual determination computed from these twelve years is $\pm 0' \cdot 5$.

If we further suppose the epoch of minimum to have synchronized with the commencement of 1844, and that the same rate of secular change, but with an opposite sign, existed previously, we shall have the annual means for the three preceding years, with their deviations from the observed values, as follows:—

This last supposition must of course be viewed as merely approximate in regard to the rate of the secular change before 1843; but on any other supposition than that of an epoch of minimum having occurred somewhere about the years 1843 and 1844, the probable error would greatly exceed that which is stated above. The value of the Inclination at the epoch of its supposed minimum is about 75° 14'·4. In the years immediately following the minimum, the annual increase was probably less, and in the latter portion of the twelve years greater, than the average rate of 0'·8 derived as above.

The Gambey's Inclinometer which has been used at Toronto since 1853 is rather a remarkable instrument, on account of the services it has rendered. It

is the property of Admiral Robert FitzRoy, who, when about to be employed on a voyage of survey and circumnavigation in H.M.S. "Beagle," purchased it from the maker. During that voyage, i.e. from 1831 to 1836 inclusive, it served for the determination of the Inclination at above 30 stations in different parts of the globe, the results of which were published in Vol. I. of the "Voyage of the 'Adventure' and 'Beagle,'" pp. 495—499. In 1837 it was lent by Captain FitzRoy to the writer of these pages, to be employed in determining the position and direction of the isoclinal lines in the magnetic survey of Great Britain, the report of which survey is published in the Transactions of the British Association for 1839. In 1842 it was again lent by Captain FitzRoy to Lieutenant (since Lieutenant-Colonel) Lefroy of the Royal Artillery, to be used in the magnetic survey of the British Possessions in North America, and served to determine the Inclination at above 100 stations between Canada and the Polar Sea. Since the completion of the North American Survey the Inclinometer has remained, with Captain FitzRoy's permission, at the Toronto Observatory, and was occasionally used, in conjunction with Robinson's Inclinometer belonging to the Observatory, in the observations previous to 1853; since 1853 it has been used uninterruptedly. It had originally two needles made by Gambey, and has since had two others, made by the late Mr. Robinson, whose dipping needles were scarcely, if at all, inferior to Gambey's. It has thus been, with few intermissions, in constant work for above a quarter of a century, during which time it has been exposed to travelling of all descriptions, and to climates of the most opposite character; and of its four needles one only is known to have suffered a slight deterioration. This speaks well both for the original instrument and for the care with which it has been treated. The observations in 1853, 1854, and 1855, of which the results only are given in Table LXXV., were all made on the same systematic plan as those of the preceding years, detailed in Vol. II., pp. 560-594, and may be referred to as a fair example of the precision which is attainable in such observations.

Solar-diurnal Variation.—In the early stage of the observations, and before experience had been obtained of the reliance to be placed on the conclusions from the combined Horizontal and Vertical Force observations, it was thought that some light might be thrown upon the solar-diurnal variation of the Inclination by dividing the direct observations of this element into two portions, one to be made in the forenoon and the other in the afternoon. We have since become aware that the solar-diurnal variation of the Inclination is deducible by the Horizontal Force and Vertical Force Magnetometer with much greater precision than it can be by direct observation with the Inclinometer, and that the variation is thereby obtained not merely for two epochs in the 24 hours, such as the forenoon and afternoon, but for every hour of the 24. (See ante, p. xciii.) Still, as direct observations were made in the forenoons and Vol. III.

afternoons, agreeably to the directions issued, and were continued from the commencement of 1841 to the end of 1852, it may be proper to show the comparative results which were thus obtained in each year. They are as follow:—

TABLE LXXVIII.

Years.	A.M.	P.M.	Years.	A.M.	P.M.
1841	% / 75 16 68	° ' 75 17:20	1847	。 , 75 15*43	° ', 75 15:27
1842	75 16.94	75 15.69	1848	75 18:23	75 18:44
1843	75 15 15	75 14.35	1849	75 19:14	75 18:70
1844	75 15.33	75 14°31	1850	75 19:90	75 20:09
1845	75 15:31	75 15.76	1851	75 20.27	75 20.44
1846	75 15.21	75 15:09	1852	75 20.56	75 20:47

The mean of the A.M. results is 75° 17′·35, and of the P.M. results 75° 17′·15. On the average of the 12 years the A.M. results exceed the P.M. by 0′·2. This is in the same direction as, but somewhat less in amount than, the difference more satisfactorily shown by the combination of the Horizontal and Vertical Force observations. If we suppose 9 A.M. and 3 P.M. to be about the mean times corresponding to the A.M. and P.M. direct observations, the difference between them should have been nearer 0′·5 than 0′·2; but a discrepancy of this small amount is within the limits of the errors of observation by the direct method.

Annual Variation.—Table L. in Vol. II., p. lxxxvii, contains the several monthly values of the Inclination from 1841 to 1852 inclusive, arranged according to the respective months. The following Table (LXXIX.) contains the continuation of the aforesaid Table in Vol. II., for the subsequent years 1853, 1854, and 1855: the final column exhibits for each month a value which is the arithmetical mean of the results in that month in the 15 years.

Monthly Means of the Observations of the Inclination from January 1841 to December 1855 inclusive, continued from Table L., Vol. II., p. lxxxvii.

Months.			1853.	1854.	1855.	Means for each Month, 1841 to 1855 inclusive.
			75° +	75° +	75 +	
January -		-	22'-1	21'•4	24.0	75 18.78
February	-	-	22.6	23.4	23.8	75 18:43
March -	-	-	22.6*	23.1	23.8	75 18:17
April -	-	- 1	22.6	23.0	23.0	75 18:33
May -	-	-	22.5*	23.0	23.5	75 18.08
June -	-	-	22.5	25.9	22.9	75 17:38
July -	-	-	21.2	24.3	23.1	75 17:13
August -	-	-	20.3	23.2	23.8	75 17:33
September	-	- [21.7	23.4	24.2	75 19:09
October	•	-	22.5	22.0	23.5	75 19.09
November	-	-	23.0	22.5	23.3	75 19.53
Decembe r	-	-	22.3	23.9	23.3	75 19.15
Means for ea	ich vear	_	75 22.2	75 23 0	75 23 6	75 18:38

^{*} The months of March and May of 1853 are interpolated values, as no observations were made in those months. For March, a mean has been taken between the results in February and April of the same year; and for May, a mean between the results in April and June.

On examining the final column, the existence of annual variation is very perceptible: the Inclination is considerably less in the middle months of the year than at its beginning or ending. But these results involve the effects of the secular change which takes place during the year, as well as those of annual variation. To eliminate the influence of secular change, perhaps the least exceptionable process is to take the arithmetical means, respectively, of January and December, February and November, March and October, April and September, May and August, June and July, of all which couples, or bi-monthly means, the 1st of July is the common mean epoch; if, therefore, there were no annual variation, these six means should be all alike. They are as follow:—

January and December	-	-	-	75	18.96
February and November	-	-	-	75	18.98
March and October		-	-	75	18.63
April and September	-	-	-	75	18.71
May and August -	-	-	-	75	17.70
June and July -		-	-	75	17.25

It appears therefore, as the result of fifteen years of careful observations, made throughout at the same spot, and according to the same systematic method, and comprising no less than 1,920 distinct absolute determinations, nearly equally distributed, and averaging, therefore, 128 for each of the twelve months,—and after the elimination of secular change,—that the Inclination is lower at Toronto in June and July than in the previous January and the succeeding December, by an amount which may be taken approximately at 1'·71.

Annual Variation, Absolute Value, and Secular Change of the Total Force.—The mean values of the absolute Horizontal Force in the different months obtained in the eight years (1845 to 1852 inclusive, pp. cvi—cxv) are as follow:—

```
January 3 '5326; December 3 '5291; Mean, January and December 3 '5309. February 3 '5310; November 3 '5287; Mean, February and November 3 '5299. March - 3 '5329; October - 3 '5278; Mean, March and October - 3 '5303. April - 3 '5296; September 3 '5276; Mean, April and September - 3 '5286. May - 3 '5324; August - 3 '5298; Mean, May and August - 3 '5311. June - 3 '5323; July - 3 '5318; Mean, June and July - 3 '5321.
```

Combining these with the mean values of the Inclination in the different months in the preceding page, we have the values of the Total Force as follow:—

```
January and December 3.5309 \times \sec 75^{\circ} 18.96 = 13.9133 February and November 3.5299 \times \sec 75 18.98 = 13.9254 March and October -3.5303 \times \sec 75 18.63 = 13.9218 April and September -3.5286 \times \sec 75 18.71 = 13.9164 May and August -3.5311 \times \sec 75 17.70 = 13.9106 June and July -3.5321 \times \sec 75 17.25 = 13.9076 13.9091
```

It appears therefore, as the result of 96 monthly determinations of the absolute Horizontal Force, and 180 monthly determinations of the Inclination, that the Total Magnetic Force is less at Toronto on the average of the months of June, July, August, and September, than on the average of the months of November, December, January, and February, by 0.01 in absolute measure, or about $\frac{1}{1400}$ of its whole amount.

The mean of the eight years of observation of the absolute Horizontal Force (p. cxvii) is 3.53045, corresponding to the mean epoch of January 1, 1849; the contemporaneous value of the Inclination is 75° 18'.4; whence we have 13.9188 as the absolute value of the Total Force at the same mean epoch. Or if, as some may deem preferable, we omit the observations of the Horizontal Force in 1852, which, from some unexplained cause, differ from the results of the preceding seven years by an amount which greatly exceeds the probable error of a single year as derived from those results, we have, at the mean epoch July 1, 1848,—for the absolute Horizontal Force 3.5332; for the Inclination (the mean of the same seven years) 75° 17'.63; and for the Total Force 13.9178. With the data furnished by the observations of those seven years, we have

the annual secular decrease of the Horizontal Force $\cdot 0026 \pm \cdot 0006$; and the secular increase of the Inclination $1'\cdot 0 \pm 0'\cdot 19$; the probable error of a single annual determination of the absolute Horizontal Force $\pm \cdot 0015$, and of the Inclination $0'\cdot 51$; and with the same data we obtain the absolute values of the Total Force, corresponding to July 1, 1845, 13·9023, and corresponding to July 1, 1851, 13·9334; showing intermediately an increase of $0\cdot 0311$ in six years, or $\cdot 0052$ in one year. Both combinations, therefore, *i.e.* the Horizontal and Vertical Forces examined in pp. ciii—civ, and the Horizontal Force and Inclination examined here, concur in showing an annual increase as the secular change of the Total Force; and we may view the two combinations as being in effect very nearly equivalent to two independent determinations; because, although it is true that the secular change of the Horizontal Force enters into both, yet in its combination with that of the Vertical Force, no variation in its amount which can be regarded as in any degree probable would be otherwise than insignificant in the deduction of the resulting secular change of the Total Force.

SECULAR CHANGE OF THE MAGNETIC DECLINATION.

Volume II. of the Toronto Observations contains, in pp. 635—639, the particulars of the monthly observations, made from 1845 to 1851 inclusive, to determine the absolute values of the Declination by means of a Declinometer placed in a detached building appropriated to that object only. An abstract of these observations, with a statement of their results, is given in Table I. at the commencement of the same volume (pp. iii, iv); and the conclusion from the results in p. vi. The value of the Declination at the mean epoch July 1, 1848, is stated to have been 1° 34′·91 West; and the mean annual increase of West Declination between 1845 and 1851, 1′·952.

I have since received, through the kindness of Mr. Kingston, the present Director of the Toronto Observatory, a continuation of the series made at intervals in the years 1853 and 1854, with the same instrument in the same locality; and the commencement of a new series in 1855, with the Declinometer placed in a new building. The results are contained in the following table.

TABLE LXXX.

Dates.	Mean Observed Declination.	Mean Reading of the Observatory	Mean Monthly Reading of the Observatory	,	ences. -β.	Observed Declination reduced to the Mean Monthly Reading of the Observatory
	Decimation.		Declinometer.	Sc. Div.	Arc.	Declinometer.
o all 20, 20, and 00	0 , 1 48.6 1 51.1	α Sc. Div. 349 1 350 0	β sc. Div. 355.7 355.3	-6.6 -5.3	-4.7 -3.8	o , 1 43.8 W. 1 47.3
March 24 to 30 - April 25 to 27 -	1 52.0 1 46.6 1 51.7 1 52.4 1 51.5	350°4 348°9 345°9 342°8 344°6	351'9 351'1 350'2 350'1 350'2	-1.5 -2.1 -4.3 -7.2 -5.6	-1·1 -1·5 -3·1 -5·2 -4·0	1 50.9 1 45.0 1 48.6 1 47.3 1 47.5

New Series commenced after rebuilding the Observatory.

The annual secular change from 1845 to 1851 inclusive was an increase of 1''95 West Declination; from July 1851 to April 1854 (two years and nine months), an increase of 2'.54; and, assuming the circumstances of the new series to be strictly comparable with those of the old series, the increase from April 1854 to October 1855 is at the mean annual rate of 3'.4. It seems probable, therefore, that the rate of the secular increase of West Declination at Toronto is augmenting.

Captain Younghusband, R.A., who had been Director of the Toronto Observatory from 1841 to 1844 inclusive, and who had subsequently held the appointment of my Assistant at Woolwich, was recalled in January 1854 to regimental duty, from which he had been detached for more than twelve years. Since that date I have had no other assistance than that which I have received from Mr. Magrath, Principal Clerk, and

four non-commissioned officers of the Royal Artillery, acting as Assistant Clerks, who are changed occasionally as military convenience requires.

The long experience which Mr. Magrath has had in the office in which he has served since its commencement in 1840, and his unwearied assiduity and devotion, together with the uniform good conduct of the non-commissioned officers, have enabled me to carry on the duties since December 1853 without requiring the assistance of an officer.

EDWARD SABINE,
Major-General.

Woolwich, March 1857.

TORONTO, 1846 to 1848.

MAGNETICAL OBSERVATIONS.

	Angu	ılar Value o	f one Scale	Division of	he Declinon		NATION. 21. Increa	sing Numbe	ers denote de	ecreasing W	esterly Decl	ination.	
Mean G Tir	öttingen }	Oh.	1h.	2h.	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8h.	9 ^h .	10h.	11h.
	$\left(\begin{array}{c}1\\2\\3\\4\end{array}\right)$	Sc. Div. 115.7 114.5 114.8	Sc. Div. 114.6 114.8 114.0	Sc. Div. 118*8 114*8 115*8	Sc. Div. 119°0 118°0 116°0	Sc. Div. 119°0 116°1 116°6	Sc, Div. 116°2 113°2 114°9	Sc. Div. 112 4 111 0 113 6	Sc. Div. 109 ° 0 110 ° 8 111 ° 0	Sc. Div. 109'4 112'0 110'8	Sc. Div. 111 0 112 4 108 5	Sc. Div. 112.7 112.6 112.5	Sc. Di 113 4 114 1 114 2
	4 5 6 7 8 9 10	114.0 115.6 111.8 117.8 115.7 116.0	114.1 115.8 116.7 114.0 116.2 116.1	117.8 117.0 117.0 114.8 118.0 117.3	118.7 119.2 117.3 117.0 117.4 118.4	117.0 117.7 113.2 116.2 116.5 115.6	114.8 110.3 113.8 115.0 113.8 113.0	111.6 111.0 104.8 111.4 111.4 111.8	110°0 109°0 105°2 109°8 110°4 112°0	111.1 110.0 111.2 111.4 111.6 112.1	111.0 111.2 109.7 112.2 112.2 113.0	111.4 112.4 114.0 113.5 113.2 112.9	110°3 114°0 113°3 115°0 114°0 118°3
JANUARY.	12 13 14 15 16 17 18	112.2 114.3 110.4 113.8 111.0 119.0	114·1 116·3 102·9 114·5 115·4 117·7	110.0 118.0 115.1 114.4 120.8 120.4	109.4 117.4 119.1 118.8 120.7 119.4	116.0 116.6 118.0 115.9 116.9 115.4	115.0 114.9 115.0 113.2 115.8 115.2	113.0 114.4 114.2 112.1 114.0 110.4	111.2 113.5 114.0 113.2 112.2 108.4	109.7 113.6 111.3 113.0 110.0 107.5	110.0 110.4 111.2 112.1 109.0 107.6	111.9 110.5 118.3 112.4 112.0 112.7	117: 111: 114: 112: 111: 117:
J.	19 20 21 22 23 24 25	115.7 116.8 116.0 118.3 116.2 116.8	116.2 117.8 116.4 119.6 117.2 121.7	118.0 118.2 119.2 120.2 119.8 121.2	119.0 119.8 120.8 120.0 119.0	118.8 116.4 118.8 119.1 118.7 118.4	115°1 113°2 116°2 116°2 116°0 114°1	112.0 110.2 110.1 112.7 111.7 110.0	109°2 110°5 107°0 108°8 107°9 104°5	112.0 111.4 105.9 108.0 109.4 109.5	112·2 114·7 109·5 110·4 112·1 112·0	113.0 114.1 113.0 113.2 112.3 111.2	114° 114° 118° 112° 115°
Februa	26 27 28 29 30 31	117.0 115.2 119.8 117.0 116.3 116.0	116.8 115.4 117.0 117.3 117.7 118.8	119.0 119.0 120.4 119.5 120.0 120.8	120°0 116°8 113°8 119°0 118°7 120°2	117.2 112.9 110.6 117.6 117.0 116.8	113.4 108.8 106.2 113.8 113.0 114.1	111.0 108.9 109.0 111.8 108.7 110.0	108'3 107'2 109'4 110'2 107'2 108'0	109.4 109.0 110.2 111.1 107.2 109.2	111.0 112.4 111.6 111.8 109.0 110.8	112.3 114.2 114.0 112.8 110.7 113.2	112: 114: 114: 113: 112: 114:
	Means	115.46	115.89	117.97	118.22	116.63	113.86	111.53	109.22	110.56	111.07	112.85	114.
FEBRUARY.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	117·2 113·2 115·2 114·9 115·0 116·4 118·4 114·2 114·0 114·1 116·0 120·3 109·8 115·0 114·3	111'2 117'4 117'8 114'4 115'6 115'0 	117.0 120.4 117.8 116.8 117.0 116.0 	115.4 120.8 118.2 115.8 117.0 117.2 	117.0 117.3 113.9 116.2 117.0 114.8 	115'1 117'6 113'5 113'0 115'0 110'0 	112'2 113'8 112'0 111'8 113'0 108'0	109'9 109'2 109'8 110'2 111'8 108'2 110'0 107'8 110'2 108'8 108'5 107'0 108'6 109'2 111'4	109'4 109'6 107'8 110'0 111'2 109'5 110'7 109'7 110'4 110'0 109'0 108'0 110'8 108'0 108'8	109'0 110'0 108'0 111'4 112'0 110'4 112'2 112'6 112'0 110'2 109'8 108'2 114'2 111'0 109'0	111'0 111'7 110'3 112'0 112'2 112'7 113'1 113'6 114'0 111'1 111'8 110'0 110'0 112'4 113'8	116: 112: 112: 112: 112: 112: 113: 114: 114: 113: 111: 109: 115: 110: 110: 110:
March	10 19 20 21 22 23 24 25 26 27 28	114.5 115.0 115.3 115.2 	116 2 115 8 116 2 116 2 116 0 117 0 116 8 119 8 118 8 119 0	117.0 117.0 117.0 117.0 	117.0 117.0 116.0 115.0 118.0 117.1 117.2 118.8 120.6	115.6 115.1 114.1 114.0 114.8 116.2 110.3 118.1 117.2	114'9 112'2 110'3	114.2 110.0 110.0 110.0 	112.4 110.0 111.0 	112.0 110.2 111.0 111.2 109.8 104.8 106.0 108.1 107.5	113.0 110.0 110.0 110.0 110.0 110.0 110.0 100.3	113°2 112°0 110°8 112°0 104°0 112°4 110°8 112°0	111 '3 110 '6 109 '6 111 '6 111 '3 102 '3 113 '6 112 '3
	Means	115.60	116.32	117.77	115.22	114.85	112.82	110.55	109.30	109.31	110.38	111.24	111'

	Angula	ar Value of	one Scale D	ivision of th	e Declinome	DECLIN. eter = $0' \cdot 72$		ng Number	s denote dec	reasing Wes	sterl y Declin	ation.
12 ^h .	13h.	14 ^h .	15h.	16 ^h .	17հ.	18h.	19հ.	20h.	21h.	22h.	23h.	Means.
Sc. Div. 115 1 115 0	Sc. Div. 115 4 115 0	Sc. Div. 117 2 116 0	Sc. Div. 116 2 115 7	Sc. Div. 118.8 117.0	Sc. Div. 114°3 116°3	Sc. Div. 114'4 114'2	Sc. Div. 114'0 113'4	Sc. Div. 113 2 114 2	Sc. Div. 112.8 114.2	Sc. Div. 114'4 114'0	Sc. Div. 114*8 110*0	Sc. Div. 114 66 7 114 14
113.5	111.9	117.0	116.2	116 ·2 117·2	116.8	115.0 115.0	114.2 115.0	117.0 114.4	114·2 113·9	114.7 115.0	$\left \begin{array}{c} - \\ 114.4 \\ 114.8 \end{array} \right $	114.49
115.2 113.6 115.0 115.9	112.7 116.2 114.8 115.2	115.0 116.0 115.0 115.3	116.8 114.0 115.4 115.3	116.2 115.0 115.2 115.3	115°3 117°0 115°2 115°3	117'0 116'5 116'1 115'3	104.2 110.2 115.5 115.0	115.5 108.3 115.2 115.4	116.0 112.6 109.0 114.6	121.0 118.6 115.8 113.8	115.8 111.0 115.4 115.4	$oxed{114.27}{113.08}{114.68}{114.73}$
114.5	115.2	116.0	115.8	115 .4	115.0	116.5	130.2	116.2	121.1	117.0	120.0}	116.51
114.2 114.1 113.4 114.1	115.0 115.4 124.4 115.2	115.8 140.4 118.1 116.0	116.2 114.5 116.0 117.4	115.8 119.0 116.1	115.0 122.9 111.0 115.0	114.1 119.0 114.2 115.8	114.2 114.3 113.8 117.0	114.0 111.6 111.6 116.9	114.0 113.0 120.2 114.7 123.5	114.2 113.4 116.4 116.4 113.5	113.5 118.8 114.0 115.5 113.5	113*60 116*23 114*70 114*94 115*51
113.0 112.6	114.3	117.0 115.8	115.9 121.0 —	113.0 113.0	118.5 118.0	121.6	115.9 112.0	116.2	116.2	118.5	117.3	115.43
114.6 114.0 114.2 114.5 117.2	116.0 115.1 115.8 115.7 118.4	115°1 116°0 116°2 115°4 120°0	117.8 115.4 115.8 115.0 115.4	120.8 117.0 117.8 115.2 113.9	115.1 115.7 113.8 115.3 114.0	115.2 115.1 115.0 115.0	115.0 115.0 115.7 115.4 120.0	115°2 120°0 116°2 115°0 149°4	116.8 116.0 116.0 115.0 129.5	115°9 116°0 116°6 114°6 134°6	116°3 116°2 117°0 115°8 125°8	115°39 115°33 114°85 115°32 118°60
114.8 112.0 114.4 114.8	117.7 	115.8 	115.7 ————————————————————————————————————	114.2 113.0 120.2 123.0	114.0 	113°2 112°0 112°8 116°0	113.8 113.0 113.0 110.6	114.0 112.8 113.2 110.6	114.0 112.4 115.2 111.1	114'8 114'0 118'0 117'0	116.0 115.2 114.2 118.0	114.66 113.42 113.82 114.95
113.8 113.8 114.0	113.6 114.6 111.4	115.0 116.4 112.0	114.4 114.8 151.0	114.8 114.8 114.0	120°5 117°6 113°5	112.0 112.0 117.2	114.0 	111.7	111.4	110°2 117°2 114°7	115·4 115·0 115·0	114·11 113·69 114·49
114:31	115.59	117.15	116.12	116.39	115.99	115.18	114.45	115.74	115:30	116:30	115.71	114.80
113.9	115.7	117.0	116.9	116.9	116.0	115.3	113.0	116.0	110.4	109.2	116.5	114.05
113.5 113.6 111.6	113.9 114.0 113.8 112.0	114'1 114'2 114'0 115'2	115'8 118'4 114'2 115'6	115.2 115.0 114.0 116.3	115'0 114'2 114'0 116'1	113.2 113.8 113.8 115.4	113.4 113.6 113.7 116.2	113.2 113.6 116.8	106.4 113.4 113.0 113.0	114.4 113.7 113.8 113.1	113.0 113.0 113.0	113.92 >113.89 113.62 113.48 114.56
113.3	114.0	115.0 - 114.1	115.0 112.8	113.8	113.3 113.3	122.7 114.8	123.0 114.2	123.6 114.8	123.0 114.2	123·2 115·0	$\begin{bmatrix} -121.0 \\ 114.8 \end{bmatrix}$	115°47 112°17
114.5 113.8 112.0 111.0	114.5 114.5 113.0 110.3	114.0 115.4 115.0 113.4	114.0 114.0 114.3 118.5	114.2 113.5 114.2 113.9	112.8 113.2 114.4 115.8	112.8 113.6 114.0 111.8	113.4 113.6 113.8 113.2	113.0 113.8 114.0 114.2	114.8 115.0 114.8 114.0	115.0 115.0 115.2 111.2	114.2 115.8 115.8 121.0	113·42 113·68 113·52 113·34
107.0	113.8	115.0	113'8 — 116'2	113.8	116'2 — 115'0	117:0 111:8	97·2 111·0	128.0 113.8	117.6 116.0	118·2 117·5	116.0 116.0	113.80 113.65
111.8 109.7 112.2 111.1	116.4 111.8 112.4 110.6	113.6 113.0 114.0 113.2	114.6 114.8 114.8	114.8 113.0 114.0 114.5	115.0 113.7 114.0 114.0	112°1 114°5 113°3 113°6	112.7 114.8 114.7 116.2	112.2 111.0 113.8 118.2	115.0 115.0 114.2 115.4	114.0 115.0 114.8 115.8	114.0 115.2 114.6 113.8	113 · 29 113 · 53 114 · 08 113 · 70
110·4 	112.8	112.4	113.4	114.0 114.0	113.8	114.0 112.0	114.4 114.0	116.0 114.5	115.2 112.2	115.6 115.6		113·20 113·51
103.7 114.2 113.0	112.4 104.0 116.0	113.0 114.3 124.2 117.4	118.7 112.8 122.0 113.8	114.0 112.6 119.0 114.0	114.0 112.0 117.0 114.4	114'1 112'0 112'8 113'7	114.8 112.7 113.2 112.4	115.0 113.0 116.4 112.0	115.4 114.2 122.4 115.4	115.6 118.2 117.0 114.2	118.6 112.0 114.0	114.00 111.31 115.09 114.18
115.8	112.6	113.5	116.0	113.9	114.5	114.5	111.2	112.0	111.0	114.7	114.7}	113.43
111.85	112.69	114.91	115.44	114.24	114.43	114.14	113.36	115.09	114.75	115.18	115.87	113.67

I	ingular Value	of one Scale I	Division of t	he Declinom		NATION. 21. Increas	sing Numbe	rs denote de	creasing We	esterl y Decli	nation.	
Mean Göttinge Time.	en } Oh.	1h.	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6h.	7h.	8h.	9 ^h .	10h.	11h.
$\left(egin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \end{array} \right)$	sc. Div. 115 ° 0 116 ° 0 115 ° 4 116 ° 2 116 ° 1 116 ° 0	Sc. Div. 117 6 118 2 116 2 116 0 118 7 119 2	Sc. Div. 121 ° 0 120 ° 0 118 ° 4 118 ° 8 119 ° 0 121 ° 2	Sc. Div. 118 °0 117 °8 117 °5 113 °9 119 °0 121 °4	Sc. Div. 114°0 116°2 116°4 116°4 118°0 119°0	Sc. Div. 112 °6 109 °4 109 °5 116 °3 114 °8 115 °8	Sc. Div. 110°2 108°5 108°6 114°0 111°8 111°8	sc. Div. 107'8 109'6 107'2 112'0 110'0 109'2	Sc. Div. 107'8 109'0 107'1 111'6 109'4 107'8	Sc. Div. 108 '4 108 '8 108 '2 111 '2 110 '8 108 '0	Sc. Div. 109 2 111 0 110 1 111 5 112 2 108 8	Sc. Div. 111.7 112.5 110.5 112.0 113.0 110.8
9 10 11 12 13 14	115.0 116.0 116.2 118.2 118.0 124.2	118'2 117'2 118'8 121'4 112'2 120'8	118.6 119.7 118.7 122.4 101.2 111.0	120°0 119°7 119°7 118°4 106°2 111°4	118°1 117°4 115°6 116°1 99°0 112°9	114.4 111.3 111.9 110.2 97.4 105.5	109°8 106°4 109°1 107°0 101°2 103°9	108.8 104.0 108.3 106.0 104.4 100.6	108.6 105.1 106.3 105.8 105.4 106.8	109.0 106.8 101.9 108.4 105.0 106.0	110.9 109.0 107.8 111.6 105.1 113.2	112.0 112.0 110.6 112.6 98.8 119.0
MARCH 15 16 16 17 18 19 20 21 22	116.8 116.2 102.2 115.0 116.0 116.4	118·2 100·4 114·0 117·6 117·0 118·8	119:2 105:2 118:8 120:2 121:2 118:8	120°2 115°6 121°3 118°2 123°8 120°2	116.8 119.4 117.0 118.1 120.9 114.2	110.8 112.3 113.5 114.0 115.1 110.7	105.2 106.9 110.9 110.4 110.7 107.7	103°8 105°0 107°4 108°2 106°0 105°0	103°0 105°0 107°4 107°0 104°7 103°0	100.0 106.2 108.2 107.3 104.3 102.2	112.4 120.0 108.9 109.6 105.8 105.2	102.1 111.2 111.2 113.0 108.0 108.9
23 24 25 26 27 28 29	116.5 118.5 115.2 97.4 119.2 116.3	119.0 119.2 116.8 116.2 119.2 115.2	120°2 120°8 119°1 123°4 120°6 120°6	119.8 122.6 118.8 116.4 121.0 122.3	115.5 116.9 119.0 116.3 113.6 116.2	110.8 108.4 114.0 110.4 111.2 114.4	108.0 103.2 108.8 108.2 109.8 110.2	104.0 101.0 106.2 104.9 106.0 107.6	106.0 102.2 104.4 105.1 106.2 105.3	107.2 104.4 106.2 105.9 107.5 105.7	109.8 108.8 109.6 110.0 108.9 107.3	111.0 110.4 110.7 110.4 111.4 109.2
30	114.8 117.4	115·2 119·4	122.4 119.6	124·1 119·0	118.4 116.8	113.6 110.4	109.6 107.4	105°2 105°0	103.8	104.4 102.4	107°0 106°8	110°4 110°2
Hourly Mea	ns 115°39	116.95	118.47	118.70	116.08	111.49	108.43	106.35	106.12	106.44	109.63	110.2
$\left(egin{array}{c}1\\2\\3\\4\\5\end{array} ight)$	112.6 117.4 118.7 118.0	115°8 117°6 121°2 121°0	119.4 114.4 122.8 122.8	120°4 114°2 122°0 121°3	117.6 117.3 117.2 118.8	111.8 113.6 112.8 114.5	107°2 110°4 108°0 102°0	105.6 107.0 105.0 100.0	106.6 107.2 102.8 103.0	106.1 107.0 105.7 104.0	106°6 107°5 107°3 105°2	107.6 109.0 110.4 109.2
6 7 8 9	117.0	97.0 117.4 117.2 119.0	81.0 117.2 114.1 119.8	92.7 119.2 116.2 117.8	115.0 113.0 112.2 113.4	115.0 108.8 107.1 107.8	108.4 107.2 105.0 104.5	107.9 105.0 104.1 102.5	105°2 106°9 106°4 103°0	102.0 105.2 106.9 105.3	110.5 106.2 109.8 107.2	95.0 111.0 111.0
APRIL. 11 12 13 14 15 16 17 18	119.8 	118.0 118.6 107.0 123.2 117.2 120.2 118.8	117.2 	118.8 	114·1 112·0 116·2 113·1 106·4 114·3 114·7	108.0 	110.6 	105.4 100.0 103.2 106.8 104.0 105.1 105.0	105.6 	106.8 	109.9 107.0 102.2 102.2 116.6 108.6 105.7	114.9 105.2 103.0 103.0 108.0 107.0 107.5
$\begin{array}{c c} & 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \\ 26 \end{array}$	114.0 119.0 119.6 118.8 116.4 118.2	117'0 121'0 121'0 119'4 118'6 123'0	117.0 122.2 122.7 120.8 118.4 122.2	116.9 120.0 119.0 116.8 117.0 118.3	114.0 116.0 115.2 111.7 115.7 113.2	110.0 109.2 108.0 105.8 107.4 109.0	107.8 106.9 b 111.2 102.3 106.2 107.0	107.0 103.2 c 102.4 101.2 105.2 103.0	105.7 103.7 100.8 103.2 104.0 104.0	106.5 105.0 103.8 104.9 106.2 102.0	106.1 107.7 108.9 106.8 109.5 108.0	108.3 110.0 111.9 109.0 113.0
27 28 29 30	117.8 119.0 118.7 121.4	119.0 120.0 121.6 120.8	118°2 119°2 120°8 119°7	117°2 114°2 121°4 114°4	106.7 110.2 115.6 110.9	107.0 106.4 111.4 107.4	105°2 106°0 106°0 103°0	106'4 106'4 106'0 102'8	106.2 106.2 106.2 105.0	108.0 107.0 106.4 108.0	109.8 107.9 107.2 109.7	112.0 110.0 109.8 109.8
Hourly Mea	ns 117°15	118.02	117:38	116.32	113.80	109.23	106.32	104.41	104.67	104.98	107.76	108.28

^a Good Friday.

b Two minutes late.

c Three minutes late.

112-8 112-8 113-9 113-8 113-8 113-9 114-0 113-9 114-1 115-4 116-0 114-17 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113-1 113		Angula	r Value of	one Scale D	Division of th	ne Declinom	DECLIN teter = 0'.7		sing Numbe	rs denote de	creasing W	esterly Decli	nation.
	12 ^h •	13 ^h .	14 ^h .	15h.	16 ^h .	17h.	18h.	19h.	20h.	21 ^h .	22h.	23h.	Means.
112-2 113-1 113-9 113-9 114-0 114-4 114-0 116-0 116-2 115-7 115-0 115-9 112-8 113-0 113-8 113-1 113-9 114-0 116-0 116-2 115-7 115-0 115-8 113-1 113-8 115-0 114-8 116-8 119-8 117-2 115-0 114-8 114-6 115-8 115-8 115-8 115-0 114-8 114-9 114-9 114-9 112-1 115-8 115-8 115-8 115-9 117-2 115-0 114-8 114-9 114-9 112-2 118-2 116-8 115-8 115-9 117-1 111-5 115-2 115-3 115-8 115-8 115-9 117-1 115-5 115-1 115-8 115-1 115-8 115-9 115-1 115-8 115-9 115-1 115-8 115-9 115-9 115-1 115-8 115-9 115-1 115-8 115-9 115-1 115-1 115-8 115-9 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-	111'4 112'2 112'1 112'0 112'8	111.9 112.8 112.2 112.2 112.8	113.0 113.0 113.0	113.0 113.3 113.4 113.3	113.8 113.0 113.8	113.7 114.0 119.8 115.2 114.0	114.2 118.2 116.0 114.8	113.8 114.2 115.2 115.2	113.8 112.6 113.2 115.0	114.0 116.2 112.8 110.0	114.8 116.4 112.0 117.0	114.2 116.8 116.4 116.0 116.0	113°13 113°76 113°12 114°03 >113°7 114°17
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	112.2 112.8 112.2 110.6 104.0	113·1 113·0 113·8 111·4 111·1	113.9 114.3 113.6 113.8 111.5	113.9 113.2 115.0 115.0 117.1	114.0 114.0 114.8 117.2 117.5	114.4 112.7 116.8 115.0 116.2	114.0 113.0 119.8 114.8 116.4	116.0 114.0 117.2 114.9 124.7	116·2 114·2 115·3 114·9 126·0	115.7 114.6 115.8 112.2 118.1	115.0 115.0 116.2 118.2 116.0	115.8 116.8 119.3 115.5	113·99 112·97 113·84 113·98 110·33
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	112.0 112.2 112.0 110.8	120°2 126°6 113°0 111°8	130.0 110.1 112.8 113.0	126.8 112.8 114.9 113.0	120·2 113·0 113·4 113·0	118.8 113.2 114.0 113.9	122°2 123°5 113°9 114°0 113°4	113°2 116°4 114°0 114°0 115°2	121.8 117.0 114.0 114.6 114.6	115.2 118.0 114.8 114.3 118.2	113.0 118.2 115.0 114.0 117.3	116.8 109.5 114.2 115.6 116.0	114.75 113.11 113.55 113.45
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	111.0 111.4 113.0 114.4	112°1 110°6 113°6 112°8	112.1 112.0 113.7 118.3	112.0 111.9 114.4 116.0	112.3 112.8 114.2 113.6	112.8 113.0 123.3 112.6	113·4 113·1 117·6 112·4 113·4	115.7 113.7 108.3 112.2 114.2	114.8 114.0 124.5 110.4 113.8	115°3 114°4 119°4 115°2 115°4	116.6 115.1 115.5 115.6 114.0	118.7 114.4 115.2 116.2 108.2	112.22 113.38 112.45 113.39
11100	113.0	112.2	112.8	116.8	112.4	113.1	114.9 114.1	113.9 p	113.9 114.8	114.0	113.2 114.6	114.4	113.19
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	110.0 110.3 112.0	111.6 111.3 112.2	112°3 111°8 113°0	114°1 112°2 112°2	112.8 113.5 112.8	121.6 113.4 113.4	114.2 114.0	114.6 114.6 —	111.4 115.3	120.8	121·2 114·2	112.0 112.0	112.88 113.27
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	113.0 112.0 113.4	111.7 116.6 112.3	114'0 114'0	113°2 123°5	107°2 114°4	113·3 114·0 113·2	111.0 118.0 107.4	116.9 107.7 115.4	115.8 112.2 114.8	106.0 114.6 106.0	110.5 106.6 114.5	117.8 113.8 114.0 — 119.7	108.90 111.57 112.45 113.37
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	106.4 107.2 103.8 107.4 109.8	108.0 110.8 133.0 136.8 111.2	110°5 112°0 105°6 124°8	129.5 112.6 112.7 119.4 111.8	119.2 112.4 118.0 140.0 112.2	114.8 114.5 114.0 120.5 113.2	111.0 113.0 117.4 124.0 114.0	116.5 119.8 100.5	112.8 119.1 115.0	116.4 118.7 105.2 125.5	116.4 116.0 114.8 116.4 120.0	117.2 115.9 117.2 118.7 117.0	111.44 111.15 113.42 114.51
113.6 113.8 113.0 115.9 115.0 114.5 114.2 115.5 110.5 113.0 116.0 115.9 112.68 111.9 112.0 114.8 120.3 116.0 115.8 111.8 111.0 114.4 115.1 115.3 116.2 113.83 113.2 113.0 111.0 118.0 118.0 114.5 112.5 116.2 116.2 117.0 115.0 116.2 113.83 113.2 113.0 114.0 114.5 112.5 116.2 116.2 117.0 115.0 116.2 113.83	108.0 113.2 111.9 110.0 113.2	107 · 2 113 · 4 113 · 0 110 · 4 113 · 0	110.0 112.8 110.7 112.9 112.5	112.4 112.8 112.6 110.5 113.2	112.6 114.4 112.8 113.0 129.0	113.8 114.0 111.9 113.8 129.4	114.0 114.7 113.0 113.0 120.0	114.5 117.2 113.6 115.0	115.2 117.2 114.0 114.4 110.2	114.7 115.0 115.0 115.5	115.0 115.8 115.2 115.4	115.0 117.7 116.2 115.4 114.4	111.78 113.42 112.68 111.67 114.46
111.30 113.86 112.89 114.89 115.24 115.32 114.89 114.49 114.80 114.96 115.58 116.20 112.65	113.6 111.8 111.8	113.0 113.0 113.0	113.0 114.8 111.0 111.0	115'9 120'3 118'0 112'0	113.6 118.0 118.0	114.5 115.8 114.5 114.8	110°2 114°2 111°8 112°5 114°0	115.2 111.0 116.2 113.8	118.6 110.5 114.4 116.2 109.2	113.0 112.1 110.0	116.0 112.3 112.0 115.5	115.9 116.2 116.2 117.7	112.68 112.80 113.83 112.03

^a Three minutes late.

b Seven minutes late.

	Angu	ılar Value of	one Scale I	Division of t	he Declinom		NATION. 21. Increa	sing Numbe	ers denote de	ecreasing W	esterly Decl	ination.	
Mean G		0 ^h .	1 ^h .	2h.	3h.	4h.	5 ^h •	6 ^h •	7 ^h .	8 ^h •	9 ^h .	10 ^h .	11 ^h .
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	Sc. Div. 118°4 117°0	Sc. Div. 120°7 119°4	Sc. Div. 118'2 118'0	sc. Div. 116.4 116.0	sc. Div. 110.9 112.0	Sc. Div. 107 8 106 2	sc. Div. 103°1 102°6	Sc. Div. 103°0 103°0	Sc. Div. 105°2 103°0	Sc. Div. 108°3 107°2	Sc. Div. 111'0 109'4	Sc. Div. 113 ° 0 110 ° 0
	3 4 5 6 7 8 9	124.0 118.6 117.4 119.8 118.0 118.0	126.7 119.0 122.5 119.4 120.5 121.8	125'1 117'0 121'2 119'5 119'0 121'3	123.8 113.8 118.0 117.4 116.6 117.0	120.0 111.0 113.9 114.1 114.1 109.0	98.2 106.4 108.7 109.0 110.0 104.2	101.2 101.5 105.4 102.0 104.0 101.8	102.8 101.4 104.0 100.0 102.0 105.0	101 · 2 102 · 0 105 · 0 100 · 5 104 · 2 105 · 0	102.4 103.2 110.2 102.4 102.7 104.2	105.7 103.4 109.7 104.0 103.2 102.3	101.0 103.9 111.0 106.0 107.0 107.0
MAY.	11 12 13 14 15 16	116.2 118.2 114.8 117.0 119.0 118.6	116.0 120.2 116.4 116.2 121.0 119.8	116.4 126.4 116.5 116.4 118.8 121.0	118.5 121.0 116.2 115.6 118.2 119.2	114.6 107.0 118.5 109.5 118.2 115.0	112.2 107.2 115.5 111.3 111.2 110.8	108.8 106.1 111.2 108.0 107.8 109.8	105.0 109.2 112.0 104.0 106.8 106.4	104.8 111.1 106.2 103.2 105.4 104.8	103.6 105.0 109.0 107.0 106.4 106.0	103°3 113°2 108°3 107°0 108°6 107°4	105.8 107.7 108.0 109.2 110.2 107.7
Ä	17 18 19 20 21 22 23	121.4 120.4 105.0 113.2 118.0 124.6	120.0 122.8 121.4 121.2 117.4 127.2	124.2 113.4 117.8 120.7 124.0 126.8	120.0 117.1 107.3 112.8 116.4 115.0	114.3 112.1 102.2 106.2 111.5 116.2	107'4 106'2 98'2 102'2 108'2 103'2	106.0 106.5 103.2 100.0 100.0 103.2	99.2 103.0 104.0 100.0 98.5 101.0	100.0 100.0 108.8 104.6 103.0 102.0	101.7 104.0 107.0 106.0 107.5 104.7	106.1 108.4 112.8 110.3 111.6 109.2	108'3 109'5 116'2 113'8 113'9 112'8
	24 25 26 27 28 29 30 31	108.8 115.0 115.0 120.0 119.2 125.0	109.6 118.8 116.0 120.0 121.8 130.0	113'4 120'0 117'0 122'2 121'4 126'0	107.0 120.0 114.2 121.2 121.0 120.2	109°5 114°2 111°2 115°0 115°3 117°0	108.0 107.8 104.8 109.6 109.0 109.2	105.0 104.4 102.0 104.2 102.0 106.2	104.2 104.4 100.0 102.6 100.3 97.6	103.8 104.6 101.8 103.0 104.0 100.6	104.8 105.0 104.8 105.2 104.8 104.2	106.8 109.8 106.5 109.0 106.8 105.8	107.2 110.4 111.0 112.0 109.2 115.4
Hourly	Means	117.72	120.52	120.07	116.92	112.79	107.40	104.46	103.02	103.76	105.58	107.68	109.2
	1 2 3 4 5 6	120°0 125°8 120°1 118°2 117°0 119°0	115°5 127°7 122°2 120°4 118°4 120°0	113.9 126.2 121.0 117.8 121.5 119.2	115.8 118.4 120.2 115.8 121.2 115.0	112.3 114.2 119.3 111.2 119.9 113.2	114'0 112'0 112'8 106'6 114'3 109'7	106.2 109.6 113.8 101.0 111.0 106.7	107.4 100.0 110.0 100.0 105.3 103.0	108.0 103.8 111.4 107.0 105.0 102.2	106.2 105.0 108.7 108.0 104.0 100.0	107.8 105.9 108.1 108.8 107.0 106.2	109.2 108.0 115.1 111.0 113.2 108.4
	7 8 9 10 11 12 13	120°0 124°6 120°0 120°2 117°8 131°6	121.4 125.0 122.6 122.4 118.2 131.8	121°0 126°0 123°0 123°0 118°0	120°2 118°2 125°4 121°8 120°0 119°0	117.0 115.0 124.6 117.3 117.8 116.2	112.0 109.2 116.2 112.3 111.5 109.6	110°2 107°0 111°8 108°8 113°0 106°0	105.6 102.3 110.0 105.0 107.8 105.6	103.0 102.5 106.6 101.8 106.0 103.2	102.8 101.8 105.0 100.9 105.8 104.6	103.2 105.6 105.0 101.7 106.4 105.7	106.8 107.0 109.0 105.6 108.8 110.1
JUNE.	14 15 16 17 18 19 20 21	118.0 115.2 119.8 115.8 117.8	113.7 109.4 124.2 120.0 118.2 120.2	117.2 122.6 123.7 121.3 120.0 119.2	118.6 118.2 123.0 116.8 114.0 119.8	117.0 121.0 116.8 111.8 109.6 113.8	114.8 109.2 111.3 111.0 107.3 109.8	115.6 107.0 106.3 106.6 107.7 107.0	101.3 109.2 104.8 105.0 103.8 107.0	100°0 105°0 107°8 104°2 103°8 105°6	106.0 110.0 108.0 110.8 106.2 107.0	103.5 110.9 112.0 110.4 108.5 108.4	109.7 111.0 113.7 112.0 110.2 111.0
	22 23 24 25 26 27 28	129.6 119.2 117.0 121.0 118.0 120.6	128°4 120°4 122°3 121°3 119°2 121°0	126.2 119.2 114.8 120.0 119.8 119.4	121 '8 117 '0 113 '0 118 '4 120 '4 117 '7	114.3 115.2 111.3 116.0 119.2 115.2	108.8 108.8 109.3 114.2 113.8 112.8	105.6 108.0 103.8 107.4 108.0 106.8	105.1 102.8 105.0 105.0 105.8 100.0	102°3 105°2 106°3 102°2 105°0 100°0	105·1 109·2 109·2 103·0 105·2 99·0	107.2 106.3 110.2 105.3 105.2 99.8	110.0 111.0 113.2 109.4 106.9 103.1
	29 30	119°8 123°6	121°9 124°2	123°0 123°1	119.6 125.5	117:9 121:3	110 · 9 114 · 2	108'4 108'4	102.8 106.4	100.3	100.0 104.8	100.0 102.5	104.8 107.9
Hourly	Means	120.33	121.12	120.70	119.02	116.09	111.40	108.14	104.85	104.37	105.24	106:32	109.47

	,		I Source 191	VISION OF THE	Decimome	$ter = 0^{7}.721$	N. Increasi	ng Numbers	denote decr	reasing Wes	terly Declin	ation.	
12h.	13 ^h .	14 ^h .	15h.	16 ^h .	17h.	18h.	19 ^h .	20h.	21h.	22h.	23h.	Means.	
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 113°2	Sc. Div. 112'9	Sc. Div. 114.7	Sc. Div.	Sc. Div.	Sc. Div. 112 20	
110.0	112.4	115.2	119.7	117.4	117.8	123.2	119.4	117.8	117.0	121.2	$\left \frac{-}{124\cdot0}\right\}$	114.13	
08.2	106.3	118.8	108.4	98.0	119.2	115.4	111.3	115.9	109.0	115.0	116.2	111.41	
06.0	102.2	113.2	113.2	115.0	112.8	110.0	117.0	117.4	117.0	115.6	116.4	110.73	
11.2	117.6	111.3	111.8	111.8	111.0	112.2	111.8	110.5	114.0	117.8	118.6	112.76) 111.92)	
07.2 11.2	114.0 111.8	112.4 110.6	117'0 111'2	119 . 5	121.0 118.5	110°2 116°3	118 ·2 114 · 0	108'4 112'0	114'2 112'4	114.8 113.3	115°5 115°6	111 70	
11.0	110.6	110.7	111.5	112.2	112.8	—	-			-		111.37	
_						112.8	113.3	114.1	115.0	116.0	116.4	ļ j	
13.3	100.0	107.0	110.5	138.2	112.0	114.2	120.0	114'4	107.0	105.2	107.5 102.8	111.81	
05°0 17°0	106°2 126°2	104°2 114°0	119'8 113'4	116.0 113.0	115 ·2 116 ·4	106 . 4	110°2 107°8	113.4 113.0	115 . 5	114.8 112.2	115.9	114.94	
10.4	119.4	115.6	117.8	119.5	115.5	115.0	114.0	113.8	111.8	109.0	117.0	112.61 >11	2:3
11.0	110.8	111.1	110.5	111'2	112.0	111.0	113.3	112.0	112.1	113.2	116.5	112.33	
09.8	110.5	110.5	112.0	111.0	111.0					— 114·4	115.0}	111.98	
07:3	108.0	115.5	115.0	118.0	118.2	112.4 125.0	112.6 126.2	112.0 111.2	110 . 4	114.4	118.8	113.20	
11.2	111.0	112.5	114.2	117.8	125.2	138.4	123.0	115.6	113.8	106.0	116.0	113.68	
14.8	113.5	111.0	110.0	118.0	117.7	116.0	114'0	112.0	113.8	113.2	116'3	111.41	
14.3	113.2	111.8	115.8	114.0	113.8	111.2	114.0	105.0	103.8	106.3	114.0	110.35	
15°4 13°8	113.0	112.2	111.9	115.8	114.0	114.0	115.0	114.5	113.0	110.8	129.2	112.90	
	112 0	111.8	115.0	130.5	118.3	126.0	106.0	109.5	112.4	113.5	110.2	113.20	
14.6	113.7	111.2	111'2	113.8	120.8	113.0	113.0	112.1	113.0	110.8	113.0	110.36	
12.4	114.2	113.8	117.6	110.8	111.0	111.0	112.5	112.4	112.4	113.7	112.0	112.00	
13.5	111.4	112.2	111.0	112.8	111.3	112.2	111.7	110.7	109.3	112.0	117.8 116.6	110.41	
13.8 08.2	114.0	112.4 109.8	111 · 9	112 ° 0 125 ° 6	111'3 126'0	111'3 117'0	$\frac{111.8}{115.2}$	112 . 4 115 . 4	113 · 2	114°0 109°2	115.9	112.25	9.5
08.0	108.2	107.8	119.8	101.4	126.6		— — —				1 . 1	113.76	4 1
	_		-			128.0	121.0	112.8	111.8	110.8	116.9}		
11.55	111.88	111.90	113.29	115.69	116.50	115.88	114.58	112.21	112.23	112.81	115.66	112.53	
10.4	109.2	140.4	191.3	191 • 4	193.9	190.5	19518	194.3	123.6	122.8	116.0	116.95	
	109 ·2 109 ·4	140°4 109°0	124°3 116°9	121 . 4	123 ·2 115·3	129°2	125°8	124°3 120°0	123.6 110.8	12 2 .8	118.0	116°95 113°82	
26.0 13.5	109 ·2 109 ·4 114·0	140°4 109°0 110°0	124.3 116.9 110.0	121.4 106.0 117.2	123°2 115°3 118°0	129°2 115°8 112°5	111'9 112'2	124°3 120°0 107°8	110°8 109°2	116°1 107°4	118.0 115.2	$\begin{bmatrix} 113.82 \\ 113.72 \end{bmatrix}$	
26'0 13'2 12'0	109 . 4 114.0 111.8	111.0 110.0 109.0	116.0 110.0 115.0	106.0 117.2 110.2	115.3 118.0 110.8	115.8 112.5 107.8	111.0 112.5 110.0	120°0 107°8 119°4	110.8 109.2 117.6	116'1 107'4 117'0	118.0 118.0	113.82 113.72 111.81	
26.0 13.5 12.0 13.0	109.4 114.0 111.8 111.2	110.6 111.0 110.0 109.0	116.9 110.0 112.0 110.2	106.0 117.2 110.2 118.0	115.3 118.0 110.8 120.8	115.8 112.5 107.8 120.2	111'9 112'2	120°0 107°8	110°8 109°2	116°1 107°4	118.0 115.2 118.0 117.8	$\begin{bmatrix} 113.82 \\ 113.72 \end{bmatrix}$ $\begin{bmatrix} 111.81 \\ 113.61 \end{bmatrix}$	
26.0 13.2 12.0 13.0 07.6	109 . 4 114.0 111.8	111.0 110.0 109.0	116.0 110.0 115.0	106.0 117.2 110.2	115.3 118.0 110.8	115.8 112.5 107.8 120.2	111.9 112.2 110.0 104.6	120.0 107.8 119.4 113.2	110°8 109°2 117°6 114°8	116'1 107'4 117'0	118.0 115.2 118.0 117.8	113.82 113.72 111.81 113.61 112.00	
26.0 13.2 12.0 13.0 07.6 —	109.4 114.0 111.8 111.2	110.6 111.0 110.0 109.0	116.9 110.0 112.0 110.2	106.0 117.2 110.2 118.0	115.3 118.0 110.8 120.8	115.8 112.5 107.8 120.2	111.9 112.5 110.0	120°0 107°8 119°4	110.8 109.2 117.6 114.8 — 113.8 129.0	116°1 107°4 117°0 114°4 — 114°4 122°8	118.0 115.2 118.0 117.8 	113.82 113.72 111.81 113.61 112.00 115.96	
26.0 13.2 12.0 13.0 07.6 — 11.0	109.4 114.0 111.8 111.2 108.4 	109.0 110.0 111.0 110.6 108.2 	116.9 110.0 112.0 110.2 121.2 — 111.5 119.1	106.0 117.2 110.2 118.0 115.2 — 124.0 121.2	115·3 118·0 110·8 120·8 113·8 — 119·2 119·2	115.8 112.5 107.8 120.2 — 115.4 123.7 119.3	111.9 112.2 110.0 104.6 — 115.4 137.0 111.8	120°0 107°8 119°4 113°2 ————————————————————————————————————	110.8 109.2 117.6 114.8 — 113.8 129.0 110.2	116·1 107·4 117·0 114·4 —————————————————————————————————	118.0 115.2 118.0 117.8 	113.82 113.72 111.81 113.61 112.00 115.96 113.57	
26.0 13.2 12.0 13.0 07.6 — 11.0 10.4 12.8	109.4 114.0 111.8 111.2 108.4 	109.0 110.0 111.0 110.6 108.2 	116.9 110.0 112.0 110.2 121.2 111.5 119.1 111.2	106.0 117.2 110.2 118.0 115.2 — 124.0 121.2 116.0	115°3 118°0 110°8 120°8 113°8 — 119°2 119°2 117°2	115.8 112.5 107.8 120.2 — 115.4 123.7 119.3 117.0	111.9 112.2 110.0 104.6 — 115.4 137.0 111.8 112.8	120.0 107.8 119.4 113.2 — 113.0 123.0 110.0 112.0	110.8 109.2 117.6 114.8 — 113.8 129.0 110.2 112.5	116°1 107°4 117°0 114°4 —————————————————————————————————	118.0 115.2 118.0 117.8 	113.82 113.72 111.81 113.61 112.00 115.96 113.57 114.51	3*:
26.0 13.2 12.0 13.0 07.6 — 11.0 10.4 12.8	109'4 114'0 111'8 111'2 108'4 108'0 114'0 112'2 110'0	109'0 110'0 111'0 110'6 108'2 107'8 117'0 115'0 110'4	116.9 110.0 112.0 110.2 121.2 ———————————————————————————————	106.0 117.2 110.2 118.0 115.2 	115°3 118°0 110°8 120°8 113°8 — 119°2 119°2 117°2 111°4	115.8 112.5 107.8 120.2 — 115.4 123.7 119.3 117.0 112.5	111.9 112.2 110.0 104.6 — 115.4 137.0 111.8 112.8 113.0	120°0 107°8 119°4 113°2 ————————————————————————————————————	110.8 109.2 117.6 114.8 — 113.8 129.0 110.2 112.5 115.0	116'1 107'4 117'0 114'4 —————————————————————————————————	118.0 115.2 118.0 117.8 	113.82 113.72 111.81 113.61 112.00 115.96 113.57	3 •8
26.0 13.2 12.0 13.0 07.6 - 11.0 10.4 12.8 09.8	109.4 114.0 111.8 111.2 108.4 	109.0 110.0 111.0 110.6 108.2 	116.9 110.0 112.0 110.2 121.2 111.5 119.1 111.2	106.0 117.2 110.2 118.0 115.2 — 124.0 121.2 116.0	115°3 118°0 110°8 120°8 113°8 — 119°2 119°2 117°2	115.8 112.5 107.8 120.2 — 115.4 123.7 119.3 117.0	111.9 112.2 110.0 104.6 — 115.4 137.0 111.8 112.8	120°0 107°8 119°4 113°2 — 113°0 123°0 110°0 112°0 115°8 114°0	110.8 109.2 117.6 114.8 — 113.8 129.0 110.2 112.5 115.0 116.1	116'1 107'4 117'0 114'4 —————————————————————————————————	118.0 115.2 118.0 117.8 	113.82 113.72 111.81 113.61 112.00 115.96 113.57 114.51 112.05 113.15	3:
26.0 13.2 12.0 13.0 07.6 	109'4 114'0 111'8 111'2 108'4 108'0 114'0 112'2 110'0 110'6 113'0	109'0 110'0 111'0 110'6 108'2 107'8 117'0 115'0 110'4 110'4 113'6	116'9 110'0 112'0 110'2 121'2 111'5 119'1 111'2 110'4 111'1 122'2	106°0 117°2 110°2 118°0 115°2 124°0 121°2 116°0 111°2 112°0 114°2	115°3 118°0 110°8 120°8 113°8 — 119°2 119°2 111°4 113°7 113°8 —	115'8 112'5 107'8 120'2 — 115'4 123'7 119'3 117'0 112'5 113'0 — 113'3	111'9 112'2 110'0 104'6 115'4 137'0 111'8 112'8 112'1 110'3	120°0 107°8 119°4 113°2 — 113°0 123°0 110°0 112°0 115°8 114°0 — 110°8	110.8 109.2 117.6 114.8 — 113.8 129.0 110.2 112.5 115.0 116.1 — 106.9	116'1 107'4 117'0 114'4 —————————————————————————————————	118.0 115.2 118.0 117.8 — 119.0 122.8 116.2 116.2 116.8 113.0 123.2 — 109.6	113.82 113.72 111.81 113.61 112.00 115.96 113.57 114.51 112.05 113.15 112.95	3.8
26.0 13.2 12.0 13.0 07.6 	109'4 114'0 111'8 111'2 108'4 108'0 114'0 112'2 110'0 110'6 113'0 119'2	109'0 110'0 111'0 110'6 108'2 107'8 117'0 115'0 110'4 110'4 113'6 114'7	116'9 110'0 112'0 110'2 121'2 111'5 119'1 111'2 110'4 111'1 122'2 124'0	106°0 117°2 110°2 118°0 115°2 124°0 121°2 116°0 111°2 112°0 114°2 121°2	115°3 118°0 110°8 120°8 113°8 — 119°2 119°2 111°4 113°7 113°8 — 122°2	115'8 112'5 107'8 120'2 — 115'4 123'7 119'3 117'0 112'5 113'3 113'8	111'9 112'2 110'0 104'6 115'4 137'0 111'8 112'8 113'0 112'1 110'3 104'2	120°0 107°8 119°4 113°2 — 113°0 123°0 110°0 115°8 114°0 — 110°8 104°1	110.8 109.2 117.6 114.8 — 113.8 129.0 110.2 112.5 115.0 116.1 — 106.9 107.4	116'1 107'4 117'0 114'4 	118.0 115.2 118.0 117.8 	113.82 113.72 111.81 113.61 112.00 115.96 113.57 114.51 112.05 113.15 112.95 112.68	3*8
26.0 13.2 12.0 13.0 07.6 	109'4 114'0 111'8 111'2 108'4 108'0 114'0 112'2 110'0 110'6 113'0 119'2 130'5	109'0 110'0 111'0 110'6 108'2 107'8 117'0 110'4 110'4 110'4 113'6 114'7 117'3	116.9 110.0 112.0 110.2 121.2 111.5 119.1 111.2 110.4 111.1 122.2 124.0 114.0	106°0 117°2 110°2 118°0 115°2 124°0 121°2 116°0 111°2 112°0 114°2 121°2 126°2	115'3 118'0 110'8 120'8 113'8	115.8 112.5 107.8 120.2 — 115.4 123.7 119.3 117.0 112.5 113.0 — 113.3 113.8 114.2	111'9 112'2 110'0 104'6 115'4 137'0 111'8 112'8 113'0 112'1 110'3 104'2 110'2	120°0 107°8 119°4 113°2 — 113°0 123°0 110°0 115°8 114°0 — 110°8 104°1 109°0	110.8 109.2 117.6 114.8 — 113.8 129.0 110.2 112.5 115.0 116.1 — 106.9 107.4 108.0	116'1 107'4 117'0 114'4 	118.0 115.2 118.0 117.8 — 119.0 122.8 116.2 116.2 116.8 113.0 123.2 — 109.6	113.82 113.72 111.81 113.61 112.00 115.96 113.57 114.51 112.05 113.15 112.95 112.68 113.90 113.40	3*:
26.0 13.2 12.0 13.0 10.4 12.8 10.4 12.8 10.4 12.8 11.8 12.8 13.0 12.8 13.0 14.0 15.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0 16.0	109'4 114'0 111'8 111'2 108'4 108'0 114'0 112'2 110'0 110'6 113'0 119'2 130'5 114'0 111'0	109'0 110'0 111'0 110'6 108'2 107'8 117'0 115'0 110'4 110'4 113'6 114'7	116'9 110'0 112'0 110'2 121'2 111'5 119'1 111'2 110'4 111'1 122'2 124'0	106°0 117°2 110°2 118°0 115°2 124°0 121°2 116°0 111°2 112°0 114°2 121°2	115°3 118°0 110°8 120°8 113°8 — 119°2 119°2 111°4 113°7 113°8 — 122°2	115'8 112'5 107'8 120'2 — 115'4 123'7 119'3 117'0 112'5 113'3 113'8	111'9 112'2 110'0 104'6 115'4 137'0 111'8 112'8 113'0 112'1 110'3 104'2	120°0 107°8 119°4 113°2 — 113°0 123°0 110°0 115°8 114°0 — 110°8 104°1	110.8 109.2 117.6 114.8 — 113.8 129.0 110.2 112.5 115.0 116.1 — 106.9 107.4	116'1 107'4 117'0 114'4 	118.0 115.2 118.0 117.8 — 119.0 122.8 116.2 116.8 113.0 123.2 — 109.6 117.0 118.4 113.0 113.2	113.82 113.72 111.81 113.61 112.00 115.96 113.57 114.51 112.05 113.15 112.95 112.68 113.90 113.40 114.69	3.8
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26.0 13.2 12.0 13.0 07.6 	109'4 114'0 111'8 111'2 108'4 108'0 114'0 112'2 110'0 110'6 113'0 119'2 130'5 114'0 111'0	109.0 110.0 111.0 110.6 108.2 107.8 117.0 115.0 110.4 110.4 113.6 114.7 117.3 112.0 115.0	116.9 110.0 112.0 110.2 121.2 111.5 119.1 111.2 110.4 111.1 122.2 124.0 114.0 111.0 136.2	106.0 117.2 110.2 118.0 115.2 	115'3 118'0 110'8 120'8 113'8 — 119'2 119'2 117'2 111'4 113'7 113'8 — 122'2 114'0 113'2 112'1	115.8 112.5 107.8 120.2 — 115.4 123.7 119.3 117.0 112.5 113.0 — 113.3 113.8 114.2 112.5 117.0 111.0 —	111.9 112.2 110.0 104.6	120°0 107°8 119°4 113°2 — 113°0 123°0 110°0 112°0 115°8 114°0 — 110°8 104°1 109°0 112°0 119°2 108°8 —	110.8 109.2 117.6 114.8 — 113.8 129.0 110.2 112.5 115.0 116.1 — 106.9 107.4 108.0 110.0 113.8 109.1 —	116'1 107'4 117'0 114'4 112'8 113'0 113'6 116'0 118'4 110'0 112'3 100'2 116'4 114'9 113'2	118.0 115.2 118.0 117.8 — 119.0 122.8 116.2 116.2 116.8 113.0 123.2 — 109.6 117.0 118.4 113.0 113.2 117.0	113.82 113.72 111.81 113.61 112.00 115.96 113.57 114.51 112.05 113.15 112.95 112.68 113.90 113.40 114.69	3·8
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17:3 13:2 14:4 11:8 07:0 07:2	109'4 114'0 111'8 111'2 108'4	109'0 110'0 111'0 110'6 108'2	116.9 110.0 112.0 110.2 121.2	106.0 117.2 110.2 118.0 115.2	115'3 118'0 110'8 120'8 113'8	115'8 112'5 107'8 120'2 — 115'4 123'7 119'3 117'0 112'5 113'0 — 113'3 114'2 112'5 117'0 111'0 — 113'2 110'7 110'2 111'9 112'8	111'9 112'2 110'0 104'6 115'4 137'0 111'8 112'8 113'0 112'1 110'3 104'2 110'2 111'8 125'0 110'3 108'5 112'0 112'6 111'0	120°0 107°8 119°4 113°2 — 113°0 123°0 110°0 112°0 115°8 114°0 — 110°8 104°1 109°0 112°0 119°2 108°8 — 108°0 108°9 112°8 111°2 108°7	110 · 8 109 · 2 117 · 6 114 · 8 — 113 · 8 129 · 0 110 · 2 112 · 5 115 · 0 116 · 1 — 106 · 9 107 · 4 108 · 0 107 · 0 113 · 8 109 · 1 — 107 · 4 113 · 0 111 · 6 111 · 0	116'1 107'4 117'0 114'4 1122'8 113'0 113'6 116'0 118'4 110'0 112'3 100'2 116'4 114'9 113'2 105'0 111'2 103'0 101'6 111'0 116'2 108'6	118.0 115.2 118.0 117.8	113 *82 113 *72 111 *81 113 *61 112 *00 115 *96 113 *57 114 *51 112 *05 113 *15 112 *95 112 *68 113 *90 113 *40 114 *69 110 *93 112 *12 114 *97 111 *90 111 *77 112 *84 113 *10 110 *45	
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26.0 13.2 12.0 13.0 07.6 11.0 10.4 12.8 09.8 09.8 09.8 12.6 15.4 11.2 13.0 17.3 13.2 14.4 11.8 07.0 07.2	109'4 114'0 111'8 111'2 108'4	109'0 110'0 111'0 110'6 108'2	116.9 110.0 112.0 110.2 121.2	106.0 117.2 110.2 118.0 115.2	115'3 118'0 110'8 120'8 113'8	115'8 112'5 107'8 120'2 — 115'4 123'7 119'3 117'0 112'5 113'0 — 113'3 113'8 114'2 112'5 117'0 111'0 — 113'2 110'7 110'2 111'9 112'8 110'3 — 112'0	111.9 112.2 110.0 104.6 115.4 137.0 111.8 112.8 113.0 112.1 110.3 104.2 110.2 111.8 125.0 110.3 108.5 112.0 112.0 112.6 111.0 116.0 116.4	120°0 107°8 119°4 113°2 — 113°0 123°0 110°0 112°0 115°8 114°0 — 110°8 104°1 109°0 112°0 119°2 108°8 — 108°0 108°9 112°8 111°2 108°7 116°2 — 113°4	110 · 8 109 · 2 117 · 6 114 · 8 — 113 · 8 129 · 0 110 · 2 112 · 5 115 · 0 116 · 1 — 106 · 9 107 · 4 108 · 0 107 · 4 108 · 0 107 · 4 113 · 8 109 · 1 — 107 · 4 113 · 8 109 · 1 — 107 · 4 113 · 8 111 · 6 111 · 0 115 · 8 — 112 · 8	116'1 107'4 117'0 114'4 1122'8 113'0 113'6 116'0 118'4 110'0 112'3 100'2 116'4 114'9 113'2 105'0 111'2 103'0 101'6 111'0 116'2 108'6	118.0 115.2 118.0 117.8	113 *82 113 *72 111 *81 113 *61 112 *00 115 *96 113 *57 114 *51 112 *05 113 *15 112 *95 112 *68 113 *90 113 *40 114 *69 110 *93 112 *12 114 *97 111 *90 111 *77 112 *84 113 *10 110 *45	

Αn	gular Value of	one Scale I	Division of th	ie Declinom		NATION. 21. Increas	sing Number	rs denote de	creasing We	esterly Decli	nation.	
Mean Göttingen Time.	} Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8h.	9h.	10h.	11h.
$\begin{pmatrix} 1\\2\\3\\4\\5\end{pmatrix}$	Sc. Div. 119 ° 0 112 ° 0 118 ° 2 130 ° 4	Sc. Div. 121 ° 0 128 ° 2 117 ° 4 115 ° 2	Sc. Div. 121°1 123°0 119°4 115°0	Sc. Div. 123°0 123°8 116°4 117°4	Sc. Div. 120°0 118°0 113°8 115°5	Sc. Div. 111 6 114 8 115 7 112 8	sc. Div. 111 2 114 6 114 5 108 8	sc. Div. 108 2 109 2 111 4 108 5	sc. Div. 105 *8 106 *7 109 *9 106 *2	Sc. Div. 103 '8 104 '5 107 '1 105 '0	sc. Div. 104.4 104.8 107.7 107.0	sc. Di 108'' 105'' 109''
5 6 7 8 9 10	114.0 121.0 117.0 116.0 122.0 132.8	123.0 126.0 118.4 121.8 123.1 123.6	123 · 5 130 · 0 122 · 4 125 · 0 123 · 0 117 · 0	125°0 119°8 118°0 124°2 119°8 108°0	116.0 120.0 118.0 121.2 119.8 110.6	109.9 115.0 114.2 112.2 114.2 117.0	99.2 107.2 108.0 111.3 111.4 114.2	104.0 106.8 106.2 108.8 104.8 108.6	103°2 113°2 104°2 110°0 102°0 98°0	104.0 106.8 104.6 102.2 106.2 103.8	107.0 105.0 105.5 104.4 106.0 108.8	116° 108° 110° 107° 107° 112°
HTDF 12 13 14 15 16 17 18 19	114.0 117.4 115.0 115.5 121.0 115.7	120.0 119.0 124.2 112.5 124.0 123.0	124.4 118.2 124.4 120.0 123.4 117.3	122·2 118·4 124·8 117·4 120·4 116·4	119.0 116.0 118.6 116.5 115.0 114.0	110.8 110.8 118.2 108.0 a 110.0 106.6	106.8 107.0 109.2 105.0 109.0 103.8	104.0 104.8 109.4 106.7 105.4 101.2	109.2 107.4 106.9 109.0 107.0 104.6	109.8 106.9 109.6 107.0 107.8 108.0	108.0 105.8 108.8 110.0 108.0 114.9	113: 105: 109: 111: 112: 115:
20 21 22 23 24 25 26	117.0 119.2 120.8 120.2 121.0 119.2	121.0 121.0 120.0 124.4 124.2 124.4	120·2 122·8 119·0 123·5 124·8 122·2	118.6 123.8 118.8 116.4 121.8 118.8	114.9 118.5 114.8 114.1 120.5 122.5	110.5 117.0 109.5 106.9 109.8 117.8	109.2 114.0 106.2 107.0 110.9 111.8	109.4 109.0 100.9 105.2 106.2 111.8	108.8 107.0 105.3 104.0 95.4 105.3	107.0 107.5 107.5 105.5 97.0 105.5	108.0 107.1 108.2 109.0 99.4 112.0	110° 109° 111° 101° 108°
27 28 29 30 31	123°3 119°8 127°0 111°2 119°8	124'4 123'2 128'0 111'0 122'4	125.6 124.1 119.2 119.8 117.8	121.3 120.7 118.0 120.4 113.0	118.5 113.1 108.8 117.0 114.5	111.4 106.4 103.6 108.2 107.8	107.2 103.7 95.2 107.4 105.2	102.0 102.0 105.0 110.0 101.8	103.0 103.9 102.2 103.8 105.4	100.0 104.2 108.6 99.6 106.0	103.0 105.0 106.6 97.8 105.0	109° 110° 110° 107°
Hourly Means	119.24	121.64	121.70	119.20	116.64	111.21	108.11	106.34	105.46	105.40	106.26	109
1 2 3 4 5 6 7 8 9 10 11 12	119°2	124.0	115.8 — 119.2 122.7 121.8 124.8 123.2 122.2 — 120.4 123.0 119.0	111.0 — 119.9 121.3 117.0 118.0 123.7 120.9 — 122.7 126.0 112.2	111.0 — 117.2 116.0 108.8 110.2 117.2 122.5 — 118.3 120.8 107.0	109.2 109.2 111.0 111.0 114.2 118.0 	107.4 	103.0	102°2	105.9 	104.1 —110.2 107.0 108.8 104.8 112.0 108.8 —106.0 104.2 107.6	107:2 114:4 109:8 110:8 109:8 108:2 109:2 109:3 114:8
TSDBOY 13 14 15 16 17 18 19 20 21 22	114.2 118.2 104.8 ————————————————————————————————————	100°2 129°0 115°8 ————————————————————————————————————	103.8 119.0 116.9 ————————————————————————————————————	106'0 106'7 113'0 — 122'0 122'0 120'4 114'0 120'6 122'4	107.6 100.6 113.0 116.0 111.0 108.2 110.3 114.2	105.5 98.2 c 109.8 — 114.0 113.4 106.0 106.2 106.8 103.0	107.2 106.0 105.3 — 106.0 103.0 100.4 101.8 104.3 103.0	104.8 105.5 104.8 	105'4 102'0 104'0 — 104'2 103'5 100'0 100'9 103'8 98'6	109'8 102'0 108'0 ———————————————————————————————————	110.0 102.9 110.0 — 106.0 110.2 107.3 108.0 105.0 101.8	112.0 109.0 109.0 112.0 112.0 110.0
23 24 25 26 27 28 29 30	120°2 119°2 119°5 113°0 121°8 117°2	125.0 116.5 123.0 119.4 124.5 124.2	128.0 119.8 127.2 122.0 125.5 121.4	130°2 123°3 124°8 118°2 123°4 116°0	118·1 113·6 115·8 112·8 117·0 116·0	119°2 107°8 109°4 106°8 103°0 113°5	108.8 104.6 104.0 103.0 100.0 113.3	105 · 2 101 · 8 103 · 0 104 · 0 98 · 8 107 · 0	100°0 105°4 102°2 100°4 99°2 102°8	99°3 105°0 104°3 100°0 102°2 104°0	104'0 106'2 107'2 109'6 119'0 107'4	101 °C 108 °C 112 °2 109 °C 118 °3 106 °S
31	118.4	120.0	118.4	116.2	115.6	109.7	104.2	102.8	104.2	106.0	110.0	109

^a Four minutes late.

^b Fourteen minutes late.

c Ten minutes late.

⁴ Five minutes late.

	Angular	· Value of o	one Scale Di	vision of th	e Declinome	DECLIN		sing Number	rs denote de	creasing We	esterly Decli	nation.
12h.	13 ^h .	14 ^h .	15h.	16 ^h •	17h.	18h.	19 ^h .	20h.	21h.	22h.	23h.	Means.
Sc. Div. 111'8 114'8 110'9 109'0	Sc. Div. 109'4 112'0 113'0 111'2	Sc. Div. 121°7 111°2 114°9 107°8	Sc. Div. 114°0 118°8 126°0 107°2	Sc. Div. 111°2 121°9 128°6 117°4	Sc. Div. 111'9 122'0 132'6 117'6	Sc. Div. 109°5 120°2 117°0	Sc. Div. 118°2 123°3 115°8	Sc. Div. 119°0 123°0 117°0	sc. Div. 113 2 124 4 121 8	sc. Div. 125 * 3 131 * 2 123 * 0	sc. Div. 118'6 119'2 123'8 — }	Sc. Div. 114 23 J 116 98) 116 90 111 89
112.2 111.0 112.0 111.0 108.4 114.8	112.6 119.8 111.0 112.2 109.8 109.8	123°8 115°0 110°7 110°4 118°8 114°2	105.7 111.2 117.0 112.2 114.0 126.6	113.9 112.0 116.8 111.6 112.2 126.5	122.0 107.0 115.2 112.2 111.5 127.0	111.0 121.9 121.8 116.2 115.0 112.0	109°1 117°0 114°0 116°6 117°4 110°6	101.8 116.8 113.7 112.2 115.3 114.4	109.0 115.4 113.9 110.0 116.2 120.2	112.8 113.1 113.2 114.6 110.5 131.0	119.6 } 119.0 110.4 117.0 120.8 141.8	114·11 114·26 113·19 113·70 115·17
114'2 112'8 112'4 113'7 113'0 112'6	119'1 107'4 112'5 116'0 113'0 116'8	119.0 115.8 113.4 114.8 111.6 123.6	112.5 118.2 112.4 116.4 111.7 119.0	114.1 115.2 119.0 112.0 112.1 114.8	113.0 118.7 117.2 112.8 119.2 111.2	112.2 116.0 138.0 115.2 112.0 113.0	113.0 115.8 137.0 112.0 114.8 112.0	110.8 113.0 120.2 114.4 116.8 110.8	104.2 105.0 114.0 106.0 110.0	113.8 92.3 111.4 114.0 104.0 110.0	119.8 } 100.0 107.4 116.0 119.8 115.0	114.47 112.33 114.70 114.61 112.40 113.11
111.0 111.0 110.2 113.8 104.8 105.0	112.0 111.0 110.4 114.2 104.0 118.5	123 ° 0 111 ° 8 111 ° 4 113 ° 0 111 ° 2 112 ° 0	117.0 112.0 111.7 112.8 108.2 116.2	115.0 114.0 112.4 115.2a 111.5 114.2	112.0 121.0 112.0 112.7 118.0 114.0	112.5 121.6 130.2 113.2 112.0 117.2	116.0 107.0 125.4 116.0 112.0 111.4	106.0 107.4 114.4 118.0 113.0 111.0	117.6 108.2 113.2 115.0 113.6 109.8	115.7 109.0 111.4 107.6 115.0 105.0	118.7 108.4 114.0 115.4 118.0 116.4	113·54 112·77 115·25 112·23 113·02 110·85
110.0 107.2 110.2 103.0 110.0	112.2 109.2 122.2 110.6 112.8	119.0 111.2 109.4 108.0 109.8	114.7 112.0 110.5 132.7 104.2	117 · 4 113 · 2 112 · 2 117 · 3 115 · 2	110.0 114.0 111.6 121.6 118.0	113.2 120.2 111.2 114.8 110.2 104.6	115.4 117.4 112.5 117.0 107.0 113.0	116.0 112.5 115.0 112.5 114.3 105.8	112.7 108.4 116.6 108.8 115.5 100.0	112.0 114.2 118.8 112.0 113.5 109.8	119.2 } 116.4 118.0 115.0 116.2 118.0	114'49 113'38 112'30 112'03 111'39 110'32
110.77	112.69	114.31	114.62	115.44	116.12	115.99	115.43	113.52	112.47	113.49	117:11	113.47
114.8 	122.2 	115.5 	109.2 116.2 112.0 110.8 170.0 113.0	111.0 	107.2 110.8 111.8 111.1 131.4 114.2	105 · 2 111 · 0 111 · 8 109 · 2 122 · 2 122 · 0	112.0 111.0 112.5 112.3 110.2 79.4	110.4 112.2 114.0 117.2 104.2 121.8	112.8 113.2 117.2 122.8 94.3 117.8	113.4 114.5 114.0 122.0 106.7 113.0	115.0 113.0 118.2 122.4 108.2 99.5	111.20 113.74 113.15 >113.22 112.97 116.17 113.52
112.0 109.2 117.2 112.0 113.6 109.8 142.8	130°0 	120.0 	114.8 	117.6 	124.2 	115.8 116.2 113.7 120.6 129.0 88.6	125.5 113.8 109.8 120.0 123.0 105.5	122.5 120.4 111.4 120.2 127.2 92.0	100.6 114.0 118.8 119.3	112.0 112.0 112.8 114.0 107.0 109.6	109.8 115.7 112.0 113.4 111.2 100.8	115.59 112.56 114.34 113.64 112.66 110.42
111.2 113.8 111.8 113.2 111.8 108.2	113.2 115.9 110.0 111.2 110.0 110.9	122.2 126.9 112.8 111.0 108.8 112.2	128.0 120.8 120.2 110.0 109.0 108.2	117 · 9 116 · 0 112 · 6 111 · 2 117 · 0 110 · 0	111.0 119.0 111.3 109.8 113.3 115.8	125.0 112.8 112.8 111.0 110.6 112.6	122.0 112.0 111.6 101.2 111.2 115.2	116.5 112.2 111.4 113.8 110.2 112.8	110.5 111.0 111.0 113.4 114.0 114.8	110.0 109.0 114.0 115.0 109.8 116.8		114.25 113.69 113.83 111.01 110.53 112.21 111.81
120.0 122.8 113.0 116.0 105.2 109.1	107.0 111.3 111.2 108.1 107.0 107.5	114·1 116·0 111·2 109·2 109·9 106·4	130.0 115.2 112.0 112.0 120.0 109.7	123°3 113°2 113°5 111°0 135°4 109°8	118.0 114.6 127.3 118.5 112.2 113.0	111.2 134.5 116.0 121.8 108.8 111.0	114.0 114.3 111.2 116.8 102.0 108.9	112.0 111.7 111.0 112.1 112.0 106.6	114.0 113.0 108.0 113.1 120.0 110.2	116.0 113.4 103.2 114.3 109.0 104.2	111.5 115.0 114.0 110.0 110.0	115·41 112·03 113·87 110·99 112·22
109.0	111.3	123*4	120.5	114.8	111.0	123.4	111.5 150.0	116.4 111.2	110.0	113.0 100.0	113.8	112.27
112.44	113.24	115.45	119.78	117:34	116.07	115.91	113.09	113.55	112.91	111.83	113.14	112.94

	Ang	ılar Value of	one Scale 1	Division of t	he Declinom		NATION. 21. Increa	sing Numbe	rs denote de	creasing W	esterly Decl	ination.	
	Föttingen }	Oh.	1h.	2 ^h •	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8h.	9 ^h .	10h.	11 ^h .
	$ \begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{pmatrix} $	Sc. Div. 116°9 119°0 120°0 98°0 129°0	Sc. Div. 121 · 2 120 · 5 123 · 0 117 · 0 111 · 4	Sc. Div. 120°3 120°3 122°7 111°0 116°0	Sc. Div. 114'8 116'2 118'0 121'2 113'1	Sc. Div. 111 6 109 8 111 0 108 9 105 8	Sc. Div. 105 ° 0 105 ° 0 104 ° 0 101 ° 4 99 ° 1	sc. Div. 101'9 102'2 100'2 99'0 104'6	Sc. Div. 101 ° 0 102 ° 2 100 ° 2 99 ° 8 102 ° 0	Sc. Div. 103 * 8 103 * 8 102 * 6 102 * 0 101 * 0	Sc. Div. 104.8 107.2 106.4 104.8 110.7	Sc. Div. 108 5 109 2 110 0 108 1 114 9	Sc. Div. 110'4 111'4 111'1 120'6 105'0
.;	6 7 8 9 10 11 12	116.6 116.8 119.0 116.0 83.4 112.7	121 ° 0 115 ° 0 124 ° 0 118 ° 6 111 ° 5 115 ° 4	118.4 110.8 120.3 120.0 111.6 115.1	116.8 111.3 114.7 118.2 108.8 111.9	113 · 2 113 · 0 110 · 2 110 · 2 101 · 0 104 · 0	108.1 109.0 107.0 100.8 104.3 100.0	104.1 105.3 102.8 98.6 100.0 102.8	109°2 105°0 102°0 103°4 100°7 105°0	107.2 111.0 104.0 98.8 103.4 112.8	111.1 114.8 109.6 98.8 108.9 110.0	114.1 111.8 113.5 101.8 117.5 117.0	115°1 111°0 116°2 108°0 121°0 118°0
SEPTEMBER.	13 14 15 16 17 18 19	122'8 112'0 118'2 125'2 116'4 118'0	119.9 109.6 120.2 124.8 119.6 116.0	112.2 119.0 115.5 122.0 119.1 118.8	113.0 115.4 113.8 116.5 118.0 116.0	106.0 106.9 112.0 111.5 113.1 115.0	101.2 b 103.2 108.7 108.3 108.0 108.9	101.0 102.8 107.8 104.2 103.2 104.0	100°0 103°0 107°6 102°3 102°8 102°2	104.8 107.2 109.2 104.8 104.1 101.0	109.0 113.0 111.2 108.8 107.8 100.2	114.0 115.2 112.4 114.8 111.3 102.0	111.8 119.1 112.1 113.0 108.2
	20 21 22 23 24 25 26	123:0 87:2 115:4 116:8 117:0 118:2	126.0 90.2 113.5 121.0 120.5 121.0	123°0 73°0 119°0 118°9 119°6	121 '4 82 '4 116 '7 116 '3 123 '0 118 '0	117.0 99.2 112.2 111.0 111.8 115.2	112·2 96·7 109·9 106·2 109·0 111·0	107.4 109.5 104.0 103.8 106.0 107.0	103 ° 0 117 ° 1 103 ° 0 101 ° 5 102 ° 2 105 ° 0	104.2 106.6 102.9 101.2 102.0 104.4	99.6 110.8 103.5 106.5 105.0 106.4	95.5 99.3 103.5 104.6 107.2 109.2	105.8 116.0 104.6 106.0 110.5
	27 28 29 30	118.5 115.4 114.6	117.8 117.2 115.0	116.6 116.8 116.5	117.6 114.1 119.0	113.0 111.8 113.4	108'4 110'1 111'2	104.0 106.8 104.2	109 '8 106 '7 105 '0	107°2 106°0 106°0	107.2 105.8 105.4	109°1 107°8 103°0	110°0 108°5 106°4
Hourly	Means	114.85	117:34	115.97	114.82	110.30	106.03	103.75	103.91	104.69	107.20	109.05	111.6
	$\left[egin{array}{c} 1 \ 2 \ 3 \end{array} ight]$	116.2 104.8 121.0	120.0 113.1 120.0	117.8 110.3 120.2	110°8 105°4 118°6	109.7 109.2 118.0	104.3 108.0 113.8	107°2 105°2 109°2	107.0 106.4 104.9	106.3 104.6 102.8	110.4 101.7 108.6	111.8 107.1 109.8	113.0 102.7 110.8
	4 5 6 7 8 9	116 2 114 4 116 0 116 3 113 4 104 3	117·2 111·3 121·8 73·5 114·2 98·8	118.4 116.0 122.2 95.5 117.0 100.4	111.0 114.2 120.0 111.0 117.4 103.3	107 ² 110 ³ 108 ³ 104 ⁰ 114 ² 105 ⁶	106°1 105°0 106°2 102°0 110°4 108°0	104.0 101.2 100.7 102.8 106.4 105.0	103.5 102.0 99.3 100.8 104.0 103.8	105.5 103.8 104.2 102.4 100.8 101.7	109.2 108.0 107.2 109.2 104.2 105.7	111.8 110.0 104.2 111.2 108.8 111.0	112:2 110:8 99:2 114:2 108:9 111:8
OCTOBER.	11 12 13 14 15 16	119.0 113.0 115.6 115.0 118.8 117.9	113·1 115·5 116·0 115·6 117·0 117·9	102.2 116.2 117.1 118.0 116.6 117.0	106.4 116.5 117.4 117.2 117.0 117.0	109.6 114.0 113.0 115.3 111.5 113.0	111.0 d 108.8 107.8 111.0 108.3 109.2	109.5 106.9 107.0 106.8 107.8 105.8	111.0 108.0 107.5 107.0 109.4 106.0	108.0 108.0 110.0 108.8 110.8 109.0	109.7 109.6 111.8 111.1 111.8 109.0	111.8 116.6 112.9 111.6 111.7 111.1	113.0 111.0 112.2 111.0 111.0
Ō	18 19 20 21 22 23 24	115.7 118.2 114.0 116.3 118.8 115.2	115.5 121.2 114.8 119.1 118.1 116.9	117.8 123.0 120.0 114.0 117.2 119.0	120.0 121.2 119.8 108.7 119.7 120.0	119.0 ° 119.8 119.1 114.0 118.5 117.8	114.0 109.4 112.5 110.2 114.0 112.5	105.8 107.6 109.8 108.8 109.9 110.0	103.0 106.0 107.4 103.0 107.2 110.7	106.4 106.8 108.0 103.5 107.0 106.4	106.0 107.8 110.5 107.6 109.0 107.2	106°0 109°2 108°9 112°5 110°0 108°2	105.2 110.1 114.0 110.3 112.0 110.4
	25 26 27 28 29 30 31	110·2 115·0 115·4 114·2 108·2 109·7	115.0 117.2 115.6 113.5 111.0 112.0	119.0 118.7 116.6 117.5 100.0 116.2	119 · 2 121 · 8 118 · 8 117 · 1 111 · 0 114 · 4	119.8 118.2 116.8 118.6 115.0 112.0	115°0 116°0 115°6 114°8 114°0 112°0	109'4 111'0 110'8 112'0 113'0 110'2	107.0 109.0 108.7 108.6 111.4 109.0	105°2 106°1 107°8 106°4 110°4 111°2	107.4 108.1 108.3 108.0 112.0 111.7	108·9 108·6 111·2 108·7 112·0 111·8	110.9 108.2 111.0 110.6 112.8 112.8
Novem	ber 1		114.00	114.96	115.37	$\frac{-}{113.76}$	110.37	107.55	106.37	106.44	108.55	110.27	104.4

^a Forty minutes late.

b Eighteen minutes late.

	Angul	ar Value of	one Scale I	oivision of th	ne De c linom	$\begin{array}{c} \text{DECLIN.} \\ \text{eter} = 0' \cdot 72 \end{array}$		ing Number	rs denote dec	ereasing We	sterly Decli	nation.
12h.	13 ^h .	14h.	15h.	16 ^h .	17h.	18h.	19h.	20h.	21h.	22h.	23h.	Means.
Sc. Div. 113 '2 111 '0 110 '2 110 '8	Sc. Div. 111 2 109 8 108 0 111 8	Sc. Div. 110 7 110 4 106 5 125 9	Sc. Div. 110°5 109°5 108°7 110°0	Sc. Div. 116.0 111.1 108.2 118.0	Sc. Div. 111 '4 111 '1 108 '8 109 '8	Sc. Div. 118°2 113°1 120°2 113°3	sc. Div. 114 '7 117 '2 112 '7 112 '8	sc. Div. 114 '2 115 '0 125 '0 110 '0	sc. Div. 112.8 119.8 109.0 104.0	Sc. Div. 112 0 115 8 124 0 100 0	Sc. Div. 116°5 118°0 114°2 110°0	Sc. Div. 111 '73 112 '03 111 '86 109 '51
153°2	112°5 111°8 113°0 112°0 152°2	111.2 112.5 112.2 110.8 118.7	112.0 111.0 110.9 	115.4 110.0 110.6 108.9 113.9 118.8	117.2 	109.8 112.2 110.4 107.8 109.0 102.0	103.0 115.0 110.4 108.9 121.2 108.8	112·2 112·7 113·3 112·3 123·2 108·6	111.0 111.3 112.2 115.7 123.0 102.2	107.8 120.0 112.5 117.7 128.4 113.4	113.4 } 115.0 115.9 116.0 123.8 119.3	113°93 113°02 111°54 112°06 112°47 111°05
114'0 	110°2 121°8 113°0 112°8 116°3 113°0 113°0	112.0 111.4 112.3 125.0 115.0 112.8 112.8	112.4 113.3 111.0 115.2 112.2 112.4 113.8	112.0 123.5 111.3 113.3 112.0 c 118.2 113.0	110 4 121 2 112 2 112 0 112 4 115 0 114 5	110°2 a 109°4 113°0 114°0 115°0 113°2	112.4 120.8 114.0 115.0 113.2 113.2	111.8 118.0 114.0 117.0 115.0 114.3	126.8 121.2 115.7 113.6 104.4 113.1	121.3 111.0 115.5 108.8 117.0 115.0	120.0 } 120.0 } 120.2 115.0 122.7 121.8 118.0	112'84 113'44 111'97 113'72 >112'41 113'47 112'74
111'4 108'2 127'0 99'3 108'4 113'2 115'4	113 0 	112 8 	101 · 1 121 · 5 107 · 8 111 · 0 125 · 0 111 · 5	113 0 	121.4 124.0 112.7 112.4 113.2 115.0	112·1 117·7 126·0 109·0 113·0 105·0	101'4 136'2 114'0 112'0 112'8 109'7	120.7 131.6 110.0 117.1 114.2 118.0	116.8 137.0 112.6 117.8 114.4 109.0	124.0 155.2 113.4 116.8 116.5 119.0	125·2 } 101·2 114·8 117·7 116·3 116·4	112.04 116.32 108.39 110.53 111.01 112.60
123.0 109.0 109.0	113·3 113·1 105·8	109°3 114°0 106°0	112.0 110.3 106.0	112.8 111.5 108.8	113.0 112.6 113.2 113.21	112.0 113.0 112.0 115.0	110°0 113°2 113°5 123°5	118·3 113·6 112·8 122·0	118.0 113.0 115.0 117.2	113.9 114.0 115.0 107.2	114.8 } 114.8 113.1 116.1	112.93 112.67 111.62 111.19 112.19 > 112.56
124.6 100.5 110.0	122°2 112°1 111°2	111.0 128.2 112.0	113°3 139°7 112°1	112°2 122°0 112°0	111.5 123.2 111.9	111.5	112.0	105.0	110.9	115°1 126°5 ————————————————————————————————————	107.5 126.0 	112.12 113.91 113.21
113.0 120.8 111.2 119.0 123.8 111.2	113.5 113.8 111.8 121.6 119.0 112.0	113°1 115°0 115°0 114°1 122°8	112 · 2 116 · 8 152 · 0 115 · 0 124 · 1	112·3 115·4 126·6 113·1 123·0 110·8	111.8 119.2 118.2 120.0 133.4 111.0	112.2 113.0 120.0 138.8 116.2 128.6	113·2 113·0 119·2 112·0 118·0 144·8	113.7 114.2 117.0 110.0 105.2 117.0	114.8 113.3 110.0 119.0 113.2 108.4	116.5 114.0 122.0 115.3 128.8	115°4 113°1 117°0 115°0 118°6	111.82 112.55 115.12 109.52 117.17
119.2 113.0 112.1 110.3 111.8	116.0 121.4 117.5 112.0 110.7 111.2	112.0 	110.4 	108.8 116.6 112.0 130.0 112.0 114.0	111.8 113.1 113.0 125.6 112.4 114.0	114.0 112.8 113.2 113.3 115.3 112.0	113°5 113°9 112°8 113°3 122°0 114°2	118.8 112.6 117.0 113.2 115.2 114.0	108.8 113.1 116.0 114.0 110.0 117.5	111.0 115.0 115.7 113.8 103.4 116.5	117.8 113.0 114.0 114.0 120.4 117.8	108.78 111.94 114.03 112.88 114.11 113.27 112.82
109:2 113:2 113:9 126:8 112:4 108:2	105.8 113.3 112.0 110.2 113.0 113.4	122.4 111.7 113.9 114.5 113.8 117.0	115.0 113.2 113.3 115.8 112.2 126.6	144.0 113.2 133.6 111.0 113.8 115.2	121 · 2 113 · 0 124 · 2 112 · 2 122 · 8 116 · 2	113°1 113°8 112°2 111°0 116°2 116°6	114.0 110.0 114.0 111.2 111.4 113.2	114.2 112.8 114.0 113.2 108.2 111.0	114.4 112.8 113.4 115.2 105.4 113.3	114.8 114.7 114.2 106.2 111.2 114.7	113·2 } 117·0 114·4 110·2 112·0 115·0 — }	112 62 113 88 113 34 114 03 111 79 113 88 113 50
112.0 111.2 111.8 112.2 113.8 112.2	112.6 112.0 112.0 113.4 111.8 112.4	113 · 2 113 · 0 119 · 0 113 · 0 116 · 4 113 · 0	113.7 114.2 113.0 118.6 119.4 113.7	114'9 116'0 115'0 114'2 120'6 113'2	116°3 115°2 115°4 115°8 118°9 113°3	113°8 112°8 112°2 117°2 115°6 115°6	111.1 113.8 111.2 112.0 117.6 107.8	112.2 114.1 112.6 113.2 113.0 115.5	113.0 112.0 113.2 117.8 115.5 115.0	113.8 112.3 113.7 115.0 115.2 111.1	109·2 } 112·0 115·2 118·1 116·4 115·0	112.78 113.23 114.00 113.77 112.99 113.02
113.67	113.63	115.06			116.84	115.66	114.95	114.8	114.2	114.80	114.5	113.09

	Angu	lar Value of	one Scale I	Division of th	ne Declinom		NATION. 21. Increa	sing Numbe	ers denote de	creasing W	esterly Decl	ination.	
	öttingen }	Oh.	1 ^h •	2 ^h •	3 ^h •	4 ^h .	5 ^h .	6 ^h .	7h.	8 ^h •	9h.	10h.	11h.
	2 3 4 5 6 7 8	Sc. Div. 114 ° 0 114 ° 2 114 ° 0 114 ° 3 116 ° 0 116 ° 2	Sc. Div. 112 '8 113 '4 114 '2 116 '0 114 '8 117 '2	Sc. Div. 100°0 105°8 115°1 117°0 118°2 121°0	Sc. Div. 100°0 110°6 115°2 118°0 120°4 120°8	Sc. Div. 111 '4 114 '4 113 '8 116 '8 118 '0 120 '2	Sc. Div. 104 '2 113 '1 110 '8 111 '0 112 '0 117 '4	Sc. Div. 103 2 110 6 108 8 106 8 109 2 112 8	sc. Div. 107 '7 110 '2 107 '8 104 '2 106 '2 108 '8	Sc. Div. 106 2 110 2 109 0 106 7 106 2 106 8	Sc. Div. 106°2 111°0 111°0 109°0 108°4 103°0	Sc. Div. 112 2 110 9 111 6 111 0 108 8 102 3	Sc. Div. 107'1 109'9 111'2 111'5 110'8 109'2
BER.	9 10 11 12 13 14	112.8 111.3 114.2 115.0 114.8 114.2	114.8 114.6 114.2 115.7 115.0 115.2	114.0 116.2 116.8 117.8 118.2 117.4	113.6 120.0 118.8 119.8 120.0 118.1	115 1 118 5 116 9 120 8 117 4 116 5	113°1 115°2 112°3 118°2 113°6 113°1	109.0 110.8 108.2 113.4 110.0 110.6	107.9 108.8 107.0 110.0 108.0 108.0	107.5 108.0 109.2 109.2 107.0 108.3	107.4 108.2 107.0 109.2 108.4 110.0	110.0 109.2 104.8 109.8 109.2 109.0	110°2 110°0 109°2 110°6 108°0 110°8
NOVEMBER.	15 16 17 18 19 20 21	114.2 115.3 120.0 114.0 116.0 115.4	115·3 115·7 117·0 115·0 117·4 116·2	115.6 115.4 117.4 115.7 118.4 115.4	115.8 113.0 116.0 115.0 119.2 121.0	110.0 116.0 116.0 116.0	112.0 109.6 105.0 110.0 109.8 115.8	110°8 110°1 109°2 105°2 107°9 111°9	110.4 90.0 108.0 105.8 107.8	110°3 84°0 108°8 108°0 108°0	108.6 94.0 109.9 111.0 108.8 109.0	109.0 98.0 109.5 111.2 106.8 111.0	109'4 108'2 109'2 112'0 127'0 111'7
	22 23 24 25 26 27 28 29	114.0 115.5 114.0 118.8 117.1 111.0	114.2 114.2 114.2 112.0 111.4 113.1	118.1 118.0 118.0 121.8 107.6 114.4	120.6 118.0 120.2 124.5 104.9 118.8	118.4 116.2 118.0 99.9 114.0 117.1	114.8 111.0 115.4 105.6 113.0 115.5	111.3 110.0 111.2 109.5 111.7 109.1	109°2 108°2 108°0 105°0 108°8 111°9	109°2 108°4 107°6 107°8 109°0 105°2	110°0 109°2 110°1 110°8 108°4 108°0	109.8 109.4 111.3 110.7 112.0 108.8	111.4 111.9 113.1 109.2 110.0 118.0
	30	109.8	109.9	112.6	108.5	112.0	112.2	113.0	110.5	109.0	111.0	112.1	113.6
Hourly	Means	114.64	114.94	115.44	116.42	114.73	112.12	109.77	107.43	107.10	108.30	109.14	111.3
	$\begin{pmatrix} 1\\2\\3\\4\\5\\c\end{pmatrix}$	114.7 118.4 115.5 116.0 118.5	118.2 117.5 115.6 112.0 119.3	116.0 109.2 113.6 114.2 117.2	116.0 115.8 116.8 116.4 118.3	116.9 114.2 115.9 112.1 115.0	112.4 109.5 113.8 105.1 112.2	109°2 108°1 111°5 104°0 106°3	108.0 107.0 110.0 105.2 106.0	108.5 109.0 110.8 104.4 105.4	111.0 111.2 110.2 106.2 106.6	111.1 112.0 111.2 111.2 111.3	111.2 113.3 110.7 116.2 112.9
	6 7 8 9 10 11 12	117.0 115.0 115.4 113.2 113.4 116.7	116.2 117.4 116.3 111.8 108.9 117.0	118.0 118.7 118.6 116.0 118.8 119.2	118.0 119.0 120.7 119.0 115.3 118.6	116.2 118.6 120.5 117.8 117.2 117.1	114.6 115.8 116.0 116.1 115.2 117.2	111.2 112.5 112.0 112.2 111.2 113.6	108.8 109.4 108.5 111.0 109.8 110.8	107.6 108.4 107.9 109.4 109.2 110.1	108.0 109.8 108.0 108.0 109.2 109.0	110.0 110.7 106.2 109.2 109.7 109.2	112.0 112.3 108.2 115.5 110.9 113.0
DECEMBER.	13 14 15 16 17 18 19	114.0 113.3 115.9 115.0 117.6 115.5	115.2 116.6 115.9 115.4 117.8 115.8	115.4 118.1 116.4 116.3 117.0 117.4	115.8 118.5 118.3 117.0 120.0 118.5	115.8 117.3 119.0 117.0 117.5 117.1	115.0 114.3 117.0 115.4 113.8 114.8	112.9 112.7 113.1 111.1 111.4 111.1	112.0 111.8 110.8 110.0 108.1 109.0	109.6 111.1 109.0 110.0 109.6	109.9 110.6 110.0 111.0 109.9 109.4	110°3 111°9 111°4 110°8 110°0 111°5	113.7 111.2 113.8 111.9 111.5 111.2
	20 21 22 23 24 25 a	113.9 115.0 114.0 111.2	113°1 116°2 116°8 116°5	114.3 116.0 117.5 118.1	118.7 120.0 120.0 117.4	117.4 117.0 114.8 120.0	113.0 113.8 109.0 115.0	111.0 110.0 107.4 112.0	109°9 109°7 110°0 110°0	110.0 110.0 105.4 109.2	111.0 110.2 107.0 110.4	111.8 111.0 107.0 112.1	114'7 111'6 107'5 114'0
	26 27 28 29 30 31	114.2 	115.4 	114.2 	115.2 	112.6 	110.7 	110°0 	109.0 	109.2 110.6 109.2 109.0 111.7	110.0 	111'2 	113.0 112.0 113.5 112.0 113.8
Hourly	Means	114.87	115.21	116.50	117.65	116.2	113.23	110.21	109.42	108.97	109.67	110.20	112.3

a Christmas Day.

		A	C -1- D		- D!'		ATION.	. N. 1		-coging Wa	ctorly Deelin	ation
	Angula	ar Value of	one Scale D	ivision of th	e Declinome	$\frac{\text{eter} = 0' \cdot 72}{1}$	l. Increasi	ing Number	s denote dec	reasing we	sterly Declin	ation.
12h.	13h.	14h.	15 ^h .	16h.	17h.	18h.	19h.	20h.	21h.	22h.	23h.	Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
112.0	114.0	116.6	112.8	113.2	113.0	116.0	111.0	112.0	112.4	106°2 114°2	113.2 114.4	109.90
112'1	111.7	113.2	113.6	113.4 116.8	111'0 117'0	113'0 115'0	113°4 114°2	114°2	114'0 117'9	115.1	116.1	113.31
110°2 112°5	112.0	115°5 113°8	117°2 114°1	113.2	113.7	118.8	109.0	112.5	115.2	114.5	113.0	112.72
112.6	112.0	120.6	117.9	113.0	116.8	115.8	115.0	115.2	118.0	116.1	116.0	114.15
110.0	119.7	117.0	115.0	113.0	113.0					113.8	$ {112 \cdot 2} $	113.41
111.3	112.0	112.8	112.6	115.0	113.5	112·3 113·8	113°2 112°2	113.7 112.5	113'2 113'0	113.8	113.1	112.11
110.5	116.0	112.9	112.5	113.5	113.2	113.4	113.1	112.4	113.1	113.1	113.7	112.83
111.8	111.4	112.3	112.4	113.2	113.1	112.8	112.1	112.0	113.8	114.0	114.0	112.12
111'5	112.1	113.1	113.0	112.8	113.3	112.0	112.2	113.0	113'6	114.0 115.2	114.4 97.4	113.52 >112.26 112.27
108 .4 111 .3	112.1	111.7	111'3 112'8	115.8 112.0	115 ·1 112 ·7	115.6	114.0	115.0	113.2	115 2	31 - 1	1
—	112 0		— — — — — — — — — — — — — — — — — — —	_		113.5	112.4	112.0	112.1	110.2	113.9}	112.43
112.8	112.0	112.8	113.0	113.0	112.8	115.0	113.0	113.2	113.7	114.2	115.0	112.75
112.8	113.0	111.8	116.1	116.3 119.0	115.8 113.0	122.0 111.0	122.0 113.0	111.0	113.0	124 . 9	103.4	112.00
110.2	111.0	114.6 114.2	112°2 115°5	114.5	113.9	112.6	112.2	112.0	114.0	115.5	113.8	112:27
105.0	116.2	110.0	113.8	114.5	113.0	114.4	109.5	109.5	113.0	115.2	115.4	113.01
111.8	113.4	113.8	127.2	113.4	113.5	110:0	100:4	113.1	112.8	114.4	$ {116\cdot 2}\} $	113.75
112.0	113.4	114.0	113.9	114.0	113.4	112°2 113°0	109 .4 113.0	112.4	113.2	113.7	115.0	113.43
113.2	113.8	114.1	113.4	113.7	113.9	112.9	112.9	113.0	113.2	114.0	114.4	113.02
113.0	114.5	114.0	114'9	115.1	114.2	114.6	114.0	113,6	113.0	113.4	118.8	113'93 114'07 113'27
115.9	117.1	111'1	119.0	123.0	123.0	117.6	116.0	95 4	112 . 2	123.6 107.8	118.1	114.07 \113.27 112.87 (
109°2	140°0 132°2	118°2 114°4	$\frac{117.2}{127.2}$	120°0 113°5	116.5 112.8	116.5	110.1	109.2		101 0	100 I	113.92
	-					110.8	106.2	114.2	114.4	115.0	113.3	1
114.5	114.1	120.1	114.3	115.0	114'8	113.8	105.0	112.9	115.3	114.1	114.0	112.55
111.41	115.26	114.19	115.32	114.54	114.54	114.31	112:31	111.90	113.76	114.38	113.17	112 76
110.0	115.7	114.5	117.0	117.8	112.3	117.0	115.6	115.0	112.3	115.0	105.8	113.37
114.7	114.0	114.0	113.8	114.0	115.7	113.0	113.0	115.2	112.5	113'4	114.9	113.05
112.3	113.2	114.2	114.2	113.4	114.6	113.0	121.9	113.1	116.4	115.2 117.0	118.0	113.84
117.0 114.1	118.4 115.1	115.9	116.0	126°4 115°4	118°2 115°4	116°7	116.0	116.0	114.2			113.24
	— —	— — — — — — — — — — — — — — — — — — —				115.0	112.0	114.2	113.8	114.8	114.2	1 1
113.0	114.3	114.5	114.0	114.3	114.0	113.8	113.2	114.0	113.5	113.8 114.6	114.0 115.0	113.47
112.7 101.6	113.2	113.0	116.0 120.2	$115.2 \\ 128.0$	115°8 123°4	115.0 120.8	114.8 109.7	113.4	114.0 113.7	112.3	113.9	114.59 >114.54
115.4	103.0	125°0	119.3	116.5	118.8	117.2	117.0	112.9	113.1	114.2	110.6	114.37
112.4	112.7	117.0	119.2	118.5	117.7	116.0	115.2	121.8	123.0	118.8	118.0	114.95
114.5	113.6	115.1	115.2	130.8	116.0	114:0	114.4	115.2	115 [.] 8	116.0	$\left \frac{-}{114.2} \right $	115.25
111.7	112.2	113.2	115.3	115.8	116.0	114.0 114.8	114.4 112.8	117.2	116.4	121.8	114.0	114.21
112.6	112.0	116.5	112.0	115.1	112.0	114'2	115.1	113.9	115.6	115.7	116.0	114.32
113.6	113.8	114.8	114.3	114'1	114.5	114.1	114.2	114.6	114.7	115.0	115.0	114·30 J 114·43)
113.2	112.9	120.6	114.0	114.9 116.0	114.7 115.5	114.0 115.8	114.8 115.0	115°2	115°2 115°4	118°1 115°2	115.0	114 43
112.0	115.8 112.2	114.7 114.0	114.7 114.4	113.0	114.0		115 0				113.1	113.42
					_	117.4	113.0	113.0	113.0	113.2	113.1	113.78
111.4	112.2	113.8	115.0	116.4	113.0	114.2	113.6	113.7	114.8 115.0	115°5 117°8	115.7 117.0	113 78
110.1	113.2	115.0 123.9	114.4 123.8	115°4 122°7	115.6 118.2	115'1 114'0	114.5 113.2	114.7 116.7	115.0	111.0	109.2	114.21
112.0	116.0	116.5	117.0	119.6	116.2					112.9	111.2	114.55 \ 113.81
114.0	115.0	119.8	115 · 9	118.1	115.0	114'1	111.5	112.0	— 114.0		$\left\{\begin{array}{c} 111 & 2 \\$	113.55
	_				 	113.0	114.0	113.5	115.4	115.0		113 47
113.0	115.0	115.4	114.8	114.7	113.0	114.0	112.5	112.8 115.8	$113.7 \\ 113.2$	113.0 114.0	112.8 114.2	113 47
113.8	114.7	114.2 114.0	114.2 114.0	114.0 113.7	113.7 113.4	112.3 112.2	112.0 112.5	112.8	113.2 113.4	114.0	114.1	112.92
114.0	114.0	114.6	114 0	114.5	113.8	113.2	113.1	112.9	113.9	114.3	114.5	113.28
112.71	114.46	116'08	116.05	117:21	115.2	114.77	114.00	114.43	114.63	115.08	114.03	113.96

	Απ	gular Value	of one Scale	Division of	f the Decline	DECLIN		easing Num	bers denote (decreasing V	Vesterly De	clination.	
Mean G	öttingen (Oh.	1 ^h .	2h.	3h.	4h.	5 ^h .	6 ^h •	7h.	8h.	9h.	10h.	11h.
	(1	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	8c. Div.	Sc. Div. 110°0 110°0	Sc. Div. 110°4 109°2	Sc. Div. 113°2 111°8	Sc. Div 114°2 112°5
JANUARY.	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	114'0	116.2	119'2 118'4 120'8 119'3 117'5 117'7 120'0 109'1 119'2 116'9 115'4 117'2	116 '2	114.5 — 118.6 117.1 120.7 117.0 116.4 117.1 — 112.1 119.1 116.8 115.7 115.4 — 115.0 114.0 111.2 113.8 114.7 117.0 —	111'8 112'2 114'5 117'1 113'0 111'3 113'2 108'5 114'3 115'0 111'4 112'0 114'1 112'9° 111'9 111'2 110'0 112'1 115'1	108.6	108'4	106·2 110·0 107·0 109·0 108·8 107·2	110.0 111.0 109.8 110.6 110.8 105.9 	111.1 112.1 112.8 113.0 112.6 108.0	110°C 112°1 114°7 115°C 113°6 112°C 112°C 112°C 112°C 112°C 115°C
Hourly	25 26 27 28 29 30 31	116.0 114.8 117.3 115.0 120.4 114.4 —	116.4 115.3 116.8 115.8 111.1 115.0	118.0 118.0 116.3 117.2 112.7 117.0	120.0 117.0 115.0 117.4 111.5 115.3	117'1 118'8 114'1 117'5 111'7 113'8	116.0 116.4 114.4 116.2 109.9 115.5 —	109.8 115.0 112.6 115.5 111.5 117.0	109'0 112'2 111'8 114'0 108'6 111'3	109°2 111°2 110°8 113°8 107°2 108°0 — 109°66	112.0 112.0 111.8 113.5 105.8 102.2 ———————————————————————————————————	113.0 112.8 112.3 112.0 105.8 114.2 ————————————————————————————————————	114.0 112.6 113.1 112.8 105.0 107.2
	1 2 3 4 5 6 7 8 9 10 11 12	113.0 113.8 115.2 116.0 113.8 119.3 	112'9 117'0 119'4 116'6 114'4 114'7 	115.7 116.2 119.0 118.0 116.6 123.5 115.0 117.0 116.8 116.7 115.2	110.0 113.0 117.0 114.7 115.1 111.0 	105:2 110:2 111:7 112:6 112:6 110:4 	107'8 106'8 106'1 108'8 110'2 93'6 	108'2 105'2 103'9 106'9 108'0 104'2 	109'3 105'5 104'8 108'0 108'0 103'8	112 ² 108 ² 107 ⁵ 108 ³ 109 ³ 103 ⁶ 	112'6 110'2 102'9 112'0 111'6 106'4 	112'3 112'2 110'6 112'9'd 112'3 105'1 - 108'0 105'9 109'0 109'7 107'4	111.3 111.7 111.2 112.4 112.0 109.1
FEBRUARY	13 14 15 16 17 18 19 20 21 22 23 24 25 26	113.0	113.4 114.8 115.6 115.0 119.1 117.0 115.8 114.1 115.2 117.1 110.0 114.0	113.0	112.0	111'1	109'8	109.8	109'9	110°0	110·1 109·5 110·2 e 111·0 107·8 107·6 106·4 106·0 108·2 106·0 105·1 108·0 106·7	111.0	110°C 111°C 110°C
Hourly	27 28 Means	112.9	112.18	115.78	113.46	115.4 — 111.79	108.4	102.8	102.5	104.1	108.40	109.12	110.4

a Twenty minutes late.

^b Twelve minutes late.

c Ten minutes late.

	Angul	lar Value of	one Scale I	Division of th	ne Delinome	$DECLIN$ $ter = 0' \cdot 72$	ATION. I. Increasi	ng Numbers	denote dec	reasing Wes	terly Declin	ation.
12h.	13 ^h .	14 ^h .	15 ^h .	16h.	17 ^h .	18h.	19 ^h •	20h.	21h.	22h.	23h.	Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
i	115.2	118.8	114.9	115.1	115.3	115.0	114.7	114.9	114.9	123.0	119.9	114.78
115.0 114.7	114.6	115.1	115.0	112.0	114.9	_		_			- }	113.42
111				_	—	118.0	112.3	114.8	108.2	112.0	115.0	113.59
111'1	114.1	120.0	120.0	117.0	116.0	114.0	98.2	120.2	115.2	$113.0 \\ 114.2$	115.0	115.08
112.9	113'2	122.5	119.4	118.0	116.6	112.0	115.4	118.0	114.8 113.2	113.4	114.0	114.79
115'0	115.6	119.0	117.4	116.2	115.2	114.2	114.0 113.3	113.0	113.2	115.0	112.0	114.59
115.0	115.6	117.9	116.1	115.1 112.1	114'3 116'5	114'3 116'0	114.0	114.8	115.2	116.0	115.4	114.47
114.4	115.2	116.0	115°9 116°5	116.7	115.7	110 0	—	_	_		, ,	113.80
113.0	112.5	117.4	110 9	110 7	110 1	114.8	115.0	114.7	114'8	114.5	117.2}	
114.0	114.3	116.3	116.3	116.0	116'4		115°2°a	115.4	116.5	114.0	116.2	113.76
112.0	114.8	116.2	119.2	113.5	115.0	116.2	115.0 р	114.9	114.2	113.8	108.4	113.26
111'4	114.5	115.0	115.0	114.9	114.7	114.5	115.0	111.0	114.9	114.8	115.3	113.56
113.4	112.2	113.2	116.3	117.2	118.0	109.2	114.7	113.5	113.0	113.0 113.0	113.2 110.4	113 30)
113.0	110.5	113.3	113.3	113.3	113.0	113.0	113.5	113.5	113.0	110 0		
112.0	113.8	114.0	114.3	113.5	113.4	113.6	112.5	113.4	112.8	116.4	115.2	113.42
		115:0	114.0	114.0	113.6	114.0	112.2	114.0	115.0	115.0	114'8	113.63
112.0	113'4	115°0 115°4	114.8 115.4	114°2 115°1	115.5	114.3	114.3	115.0	118.5	121.5	118.2	115.06
115'2 117'1	115°2 116°0	126.3	113 4	114.0	115.6	106.8	115.1	118.0	118.4	117.6	110.8	114.72
114.5	116.2	115.1	115.8	115.5	115.0	115.2	115.4	115.3	115.8	117.0	114.7	114.63 114.33
114.0	115.8	115.0	116.5	116.3	115.0	114.0	115.4	116.7	117.0	115.8	115.8	114'76
114.5	115.4	113.4	119.2	113.8	113.0					116.5	116.0	114.97
_				_		112.4	114.0	115'8	116'4 115'0	116 2	115.2	114.24
114.2	115.8	114.6	115.0	114.8	114.8	115.0	114.2	114°4 115°5	116.3	116.5	117.0	114.41
113.1	111.5	112.2	115.0	114.2	114'1	114.5	110°5 114°0	114.7	115.2	115.0	115.0	114.12
114'1	114.3	114.2	113.9	114'0 112'8	114'0 113'8	114°2 114°4	112.8	114.6	132.0	125.8	116.8	115:35
113.0	111.0	109.8 112.2	111°0 114°0	116.5	114.2	115.6	114.0	115.1	116.6	114.7	115.0	111.76)
101.5 111.5	112.0 111.4	124.4	110.5	116.2	116.1	-					}	113.63
	—			— —		114.4	114.4	115.0	112.0	113.0	118.0}	
113.09	113.97	116.54	115.22	115.14	115.00	113.94	113.48	114.97	115.44	115.72	115.13	114.07
										11010	117.0	111.33
110.9	111'4	110.2	111.5	111.0	111.0	112.0	110.2	111.6	112.3	113.8	115 . 2	1 1 1 1 1 1 1 1
111.2	111.6	111.9	112.0	111.1	111.0	110.8	111'2	110.6	112.0	110°2 112°5	111.4	$\left \begin{array}{c} 111.68 \\ 111.60 \\ \end{array}\right\rangle 112.14$
111.8	112.0	112.7	112.5	112.4	111.8	111.2	112.2	115.0	113'4 112'4	112.0	113.0	112.23
115.0	113.0	112.2	112.0	112.4	112.0	112.0	111.2	111.1	114.4	114.0	126.5	112.90
112.0	111.8	112.5	112.8	113.3	114.3	112.9	110.2	111 1		_		111.89
150.0	111.1	110.4	127.1	124.5	118.0	$\frac{111.1}{-}$	113.5	110.5	111.0	112.0	$\left \frac{-}{112 \cdot 3} \right\}$	l į
110.0	11110	120.0	114.9	113.0	120.3	116.8	113.0	113.5	114.0	114.8	117.0	113.12
114.8	111.8 113.2	112.0	114.3	112.0	111.4	112.6	112.0	111.8	112.4	115.0	115.5	111.92
110.3	111.0	111.4	113.6	111.0	114.0	112.8	111.4	112.1	113.0	114'0	114.2 114.8	112.14
111.5	113.0	114.5	112.3	111.7	111.6	111.8	112.0	112.0	113.5	114.0 112.2	114.8	111.21
108.1	110.9	111.5	112.0	113.5	112.2	111.6	112.0	112.0	112.3	1		i
110.4	111.0	111.9	111.9	112.0	112.5	110.0	119:0	114.0	114.6	114.7	$\frac{-}{112\cdot 6}$	111.75
11110					110.5	110.5 110.0	113°2 113°5	114.0	114.6	104.5	120.0	111.33
111.5	110.0	110.0	119.0	110.4	111.0	107.8	108.6	111.0	111.7	114.1	114.0	111.09
114.0	112 . 4 111.8	111.0 111.0	111'4 112'5	111.2 112.6	111.0	111.8	112.6	114.0	114.0	114.7	116.5	111.92
110.8	111.8	112.4	113.0	113.5	112.3	116.0	113.2	111'5	111.0	109.3	115.2	111.73
110.4	111.0	111.5	111.9	111.8	111.3	111.3	111.8	113.8	111.7	113.7	113.0	111.43
110.0	112.0	112.3	112.3	111.4	112.5				10010	10110	$\frac{-}{127\cdot 6}$	111.87
				_		112'4	111.2	104.2	123.8	121 · 2 115·2	116.3	109.50
100.0	103.7	10740	98.8	122.4	119.2	90.4	124.8	121.0	113.0 118.0	115.0	113.2	111.34
110.0	111.5	110.0	110.2	110.4	110.9	111.6	112.1	112°2 105°6	120.5	115.0	112.0	113.03
120.8	119.2	110.6	124.0	125.2	122.0	108.4	118°3	115.0	110.5	107.0	113.4	112.26
112.0	112.0	116.8	113.2	118.6	125.5	121'3 110'2	109.8	107.0	112.0	112.4	113.0	111.92
111.0	110.8	112.2	113.2	114.0	110°2 111°2	110 2					1 5	111.32
	— 113 . 0	121.0	<u></u>	112.7	——————————————————————————————————————	111.5	111.3	111.5	112.5	112.6	113.0}	
				1	l	l		l	!			111.82

d Five minutes late.

e Two minutes late.

f Three minutes late.

	Angu	lar Value of	one Scale I	ivision of tl	ne Declinom		ATION. 21. Increa	sing Numbe	rs denote de	creasing We	esterly Decli	nation.	
Mean Götti Time.	ingen }	O _p •	1 ^h .	2h.	3h.	4 h.	5h.	6h.	7h.	8h.	9 ^h .	10h.	11h.
	1 2 3 4 5 6	Sc. Div. 116 8 113 0 112 9 113 7 112 2 114 1	Sc. Div. 120'7 114'5 114'9 115'3 116'1 116'9	Sc. Div. 124 '9 117 '9 117 '4 116 '7 116 '8 114 '4	Sc. Div. 121 0 118 5 117 3 a 118 0 120 8	Sc. Div. 110'7 116'2 116'2 115'2 114'7 117'7	Sc. Div. 107 5 111 0 113 7 107 8 111 0 113 4	sc. Div. 102 ' 5 106 ' 7 108 ' 9 104 ' 9 106 ' 7 108 ' 9	Sc. Div. 95'9 104'5 105'8 101'1 103'7 105'1	Sc. Div. 95.7 104.9 104.8 102.7 104.7 103.1	Sc. Div. 94'9 106'9 105'9 99'7 105'0 103'3	sc. Div. 96.7 108.6 108.3 100.9 106.5 105.4	Sc. Div 97 1 109 6 109 7 106 7 107 8
	7 8 9 10 11 12 13	108.7 114.8 110.0 116.5 113.6 118.0	112.8 109.0 110.0 117.7 115.0 119.2	117.0 101.5 117.2 116.9 117.3 120.0	115.8 115.0 117.0 116.9 117.8 118.7	112.0 117.2 114.0 114.0 117.0 116.0	109.5 113.8 106.7 108.0 112.8 111.8	104.5 109.2 104.5 105.0 107.3 107.0	102.0 107.6 101.0 102.8 103.8 103.6	102 · 2 105 · 2 108 · 8 103 · 1 103 · 0 103 · 2	99.4 106.7 102.0 103.8 102.8 103.0	102.4 107.6 102.7 103.8 104.0 103.0	104.1 108.6 106.6 104.1 101.1
MARCH.	14 15 16 17 18 19 d 20	115 · 2 114 · 4 113 · 5 111 · 2 119 · 0 109 · 2	118.0 116.5 117.5 116.0 64.0 115.2	121.8 116.2 119.1 120.0 74.2 122.0	118.8 115.9 121.0 120.7 102.8 117.2	117.1 111.9 118.7 117.8 107.7 114.0	109 · 2 105 · 8 112 · 6 107 · 9 102 · 0 111 · 2	103.2 101.9 105.0 99.8 c 106.3 107.8	102.2 101.0 100.3 97.2 104.6 105.9	101.5 101.9 100.0 99.8 103.8 105.1	104.0 105.0 101.7 100.8 124.1 105.4	106.9 107.8 105.0 105.2 116.8 107.8	109 6 109 8 108 6 108 6 104 7 110 6
	21 22 23 24 25 26 27	114.8 114.0 111.0 110.4 114.0 110.2	116'4 115'0 110'0 111'2 112'2 112'8	119.0 113.8 108.0 113.0 114.2 113.8	118 · 2 114 · 2 111 · 2 115 · 1 115 · 4 115 · 2	115 · 2 111 · 2 109 · 7 113 · 9 113 · 1 111 · 5	112.8 106.0 109.2 109.2 108.8 105.9	108.1 102.9 104.8 105.4 105.0 102.6	104.0 100.2 102.7 101.9 102.7 103.0	103.0 99.5 103.0 101.0 101.9 105.3	102.5 100.1 108.4 102.4 104.0 106.2	103·3 102·1 104·2 104·0 103·1 106·8	105 °C 104 °C 103 °C 108 °C 107 °C
	28 29 30 31	112.4 118.6 112.0	115°1 117°8 118°8	117.2 122.0 119.9	117·2 117·7 118·6	112.8 115.0 114.8	106.4 107.6 107.6	101'3 103'2 101'4	100°3 100°0 100°2	101.4 101.4 101.8	103.0 104.0 102.4	105.0 107.2 108.9	108.
Hourly 1	Means	113:39	115.18	116.85	117:33	114.2	109.21	104.94	102.25	102.62	103.28	104.89	106
	1	116.0	116*4	113.0	118.6	116.4	109.8	105.0	102.8	103*2	104.0	107.5	109
	2 f 3	107.6	115.5	115.7	110.0	104.0	107.9	96.9	94.6	96.0 g	94.8	97.8	107:
٠	4 5 6 7 ^h 8 9	115.0 116.2 111.2 126.6 118.2 114.8	119.0 118.0 120.0 122.2 121.0 117.1	119.8 121.4 121.8 121.4 120.0 116.4	118.8 120.0 119.9 119.4 117.5 115.4	116.0 114.8 116.1 112.8 113.4 110.6	109°4 105°4 108°1 108°2° 106°2 105°0	103.0 102.0 101.6 105.6 103.4 102.6	100'8 100'2 100'6 103'4 103'0 103'2	100°9 101°6 95°0 106°0 107°2 103°2	105.0 104.0 101.1 107.6 109.0 105.4	108.8 105.7 98.3 109.4 109.4 109.6	111.9 108.8 101.4 109.8 109.6
APRIL.	11 12 13 14 15 16 17	115.8 116.0 117.0 114.4 121.6 109.6	118.0 117.0 118.4 117.0 123.6 109.7	117.2 115.0k 117.4 116.3 121.4 116.6	118.2 114.4 115.2 116.2 116.0 121.4	111.8 110.0 110.7 109.1 110.4 117.1	107.8 104.2 103.2 101.0 101.0° 108.6	102.6 105.6 98.4 96.6 101.4 102.2	101.4 100.4 97.2 97.4 95.8 99.5	99.8 101.4 97.2 99.4 97.4 100.4	101.5 103.7 99.4 102.2 99.2 103.6	97.6 108.0 101.6 105.4 105.9 106.5	109.7 107.3 102.0 108.2 108.8 109.4
	18 19 ^h 20 ^h 21 ^h 22 23 24	115.4 105.9 111.0 112.7 112.8 113.4	118 · 2 92 · 1 72 · 6 113 · 2 112 · 8 113 · 2	119.4 89.1 75.9 113.9 112.0 113.4	118.4 94.6 91.4 110.5 112.2 111.2	113.6 95.8 92.6 110.2 110.2 108.3	109.5 95.8 99.2 107.0 105.4 104.3	105.0 94.8 101.0 103.7 102.8 101.4	101'4 101'3 102'6 100'6 103'0 101'6	101.4 90.2 103.2 106.5 102.5 103.4	102.7 93.0 100.0 102.4 103.6 105.6	104.7 88.0 101.6 104.4 104.6 107.6	106 98 0 128 111 107 0 109 1
	25 26 27 28 29 30	119·3 117·9 118·2 120·0 111·6	119.5 120.4 118.0 123.4 112.7	116°3 119°6 115°0 123°0 118°6	113.9 117.5 110.6 117.8 113.4	110°8 107°4 110°4 113°6 115°5	107°1 106°4 103°5 104°4 106°5	104.6 103.9 99.2 104.9 101.3	102.7 102.4 103.0 104.0 101.6	105.4 102.0 103.4 103.8 99.5	108'9 103'0 105'7 106'8 104'3	109.5 107.4 107.4 115.0 107.1	110 0 108 8 108 4 119 3 113 2
Hourly I	Means	115.94	117.42	117:30	115.63	111.60	105.82	102.24	100.89	101.81	103.80	106.49	109

f Good Friday.

⁶ Six minutes late.

^g Four minutes late.

b Twelve minutes late.
b Omitted in the Means, on account of the great influence of disturbance on those days.

	Angula	ar Value of	one Scale D	ivision of th	ne Declinom	DECLIN		ing Number	s denote dec	ereasing We	sterly Decli	nation.
12 ^h .	13 ^h .	14 ^h .	15h.	16 ^h .	17h.	18 ^h .	19h.	20h.	21h.	22h.	23h.	Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.; 113 4	Sc. Div.; 108.51
98.9	99 . 1	113.2 109.8	109'1	108.5 110.5	120.8 109.8	111.8	110.7	110.2	111.9	110.5	111.0	110.65
109.4	109.7	110.7	110.7	110.9	110.7	110.6	110.9	110.9	111.0	111.9	112.2	111.07
97.4	99.9	99.5	124.2	118.0	116.1	114.1	115.3	113.9	111.9	113.5	119.8	109.52
107.0	118.9	110.9	111.7	111.9	111.2	111.7	110.8	111.8	112.7	111.7	112.1	111.03 >110.6
108.2	110.2	110.0	111.8	111.4	121.1						117.3	112.26
						118.0	115.0	109.0	118°2 113°7	120°0 87°0	117.3	110.64
110.4	113.2 111.0	113.4 113.4	122.0 117.1	111.0 112.0	118.0 115.0	112.0 109.3	110.0 118.3	115.7 110.3	110.8	111.5	113.0	110.65
108.3	108.6	109.0	110.7	112.0	112.0	110.8	112.4	106.4	114.5	115.0	114.9	109.70
110.8	111.5	109.8	110.4	110.0	111.5	111.4	111.9	112.1	112.2	113.5	113.0	110.21
106.6	107.0	113.4	110.5	112.2р	112.6	115.2	117.2	115.9	116.0	117.3	115.0	111՝56 լ
105.4	104.3	107.5	111.0	110.0	111.8						115.0}	110.02
	11010					111.8	110.0	111.8	113.0 113.0	104 '2 113 ' 3	113.5	111.07
110.0	110.3	110.8	111.0	111.8 111.8	112.0 110.8	112'6 110'8	111.2 111.0	111.5 111.4	111.8	111.8	112.4	110.00
110.0	111.5	111.8	111.2	111.0	111.0	111.0	110.5	110.0	110.6	113.9	114.0	110.79
109.5	110.6	112.4	118.2	116.9	117.9	120.6	123.4	123.9	115.2	110.0	117.5	112.23
130.2	97.0	105.0	129.4	132.3	162.0	132.7	117.0	120.0	116.0	114.1	113.0	112.45
108.0	114.4	110.0	111.0	111.1	142'2		1004		110:0	11110	112.0}	112.22
106.2	107.4	108.1	100:0	108.8	109.0	111.8	108.2 110.8	109'8 107'0	112.0 110.8	111.6 111.6	112.03	110.01
106 2	106.2	127.0	108 ·2 115·6	108.8	116.2	109 . 2	109.3	120.9	120.0	110.0	112.8	110.69
117.0	108.0	109.3	109.0	109.2	107.5	94.4	103 3	113.8	112.5	112.6	111.5	108.07
108.0	108.3	109.0	109.2	108.9	108.2	109.7	111.4 c	115.3	114.2	113.3	112.0	109.33
107.0	108.1	109.2	110.0	112.0	112.3	111.8	112.8	111.5	111.4	108.0	110.5	ر 109.31
108.0	109.2	110.0	112.8	114.2	110.8					110:0	110.1	109.47
110.0	11010	11040		11510		109.5	110.2	111.0	110°4 106°1	110°0 114°1	114.1	109.90
111.8	110.5	110.8 111.5	111.0 111.0	115°2	111'0 111'4	111 . 0	111.7 112.0	112.3	111.5	111.5	113.8	111.06
110.0	111.0	111.0	110.7	112.0	114.5	111.2	111.8	112.2	111.9	113.1	112.7	111.11
108.11	109.16	110.82	112.35	111.99	113.80	111.47	111.86	112.34	112.61	111.71	113.38	110.46
				1	<u> </u>			1				11015
110.0	111.5	110.7	114.0	116.0	113.0		116.3	110.8	116.6	114.3	112.9	111.71 \ 110.2
101.0	123.8	105.2	128.0	136.0	121.8	113.4	110 3	110 6	110 0	114 0	} '	109.09
_	120 0	100 0		100 0	121 0	108.4	107.7	113.0	108.2	107.0	110.0}	
112.0	110.9	120.1	112.4	111.7	103.2	112.2	110.7	107.6	109.3	112.1	113.0	111'11
107.8	109.0	116.0	119.4	106.8	111.0	111.7	115.0	113.0	113.0	114.3	114'4	106.77
105.4	98.4	96.4	132.4	0.5	120.1	117.0	153.1	103·0	83°1 104°7	132°3	124.0 112.8	111.76
112.8	108.4 113.0	110 . 4 108.8	117.6 109.1	109.0	112.4	115°2 110°8	109°0	114.0	112.5	111.8	112.8	111.45)
118.0	109.0	109.7	109.3	110.0	110.0							110.35
					<u> </u>	112.5	111.4	112.0	112.8	113.7	114.2	
110.4	110.5	110.0	110.8	113.2	111.2	112.4	113.2	113.0	113.6	114.6	113.4	110.31
108.6	109.2	115.0	109'4	109.2	110.0	110.4	105.8	112.2	114.8	114°2 112°4	115.8 112.0	109 '90 108 '30
107.8	106.4 109.0	109 · 2 108 · 8	109 .4 115.8	109.5 114.3	111'4 112'3	109 . 6	111.5 111.5	112.2 112.0	111 .4 121.3	120.0	120.5	110.00
110.8	111.4	116.0	117.0	116'4	115.0	117.0	111.9	98.6	114.0	114'6	118.5	110.38 110.17
112.4	112.3	112.4	112.8	111.7	112.4						$\frac{-}{113\cdot 4}$	110.37
10000	_					111.0	111.0	111.5	111.7	112.0		i i
101.8	109.9	110.2	111.8	110.4	111.2	113.6	120.0	92.3	120.2	114.6	112.1 116.0	110.45 103.33
126.4	103.9	107.4	109.2	110.5	111.0	111.5	117.5 108.4	118 ·4 109 · 8	109.3	118 . 4	110.0	103 55
103.3	107.4 109.3	113 .4 112 . 2	111.3	109.6 109.4	107°0	106.9	112.0	112.0	112.4	109.4	112.0	109.40
111.0	110.0	110.7	110.4	115.4	113.5	107.4	110.6	111.0	111.4	111.6	112.2	109:33
110.4	110.4	110.7	113.0	114.4	114.0						115.4	110.23
110.5				—		110.8	113.5	112.2	113.4	114.5		111.22
110.2	110.6 116.0	112.4	109.2	109.8	113.8	112.0	111.2 t	110.6 115.0	111.6	115°3 109°4	116.0 114.2	110.67
108.6	116.6	111°4 116°6	111.0 111.0	112.7 111.5	111 '4 111'8	112.5 112.4	119.5	124.6	117.6	100.5	116.0	111.51
109.0	122.4	129.4	104.4	116.2	115.4	107.6	110.0	95.0	120.0	124.0	120.4	113.75
108.4	115.6	114.5	106.4	112.7	119.6	119.0	108.2	113.3	109.6	111.2	114.2	110.75
109.63	112.13	112.87	112.20	113.18	112.68	111.83	111.68	110.65	112.96	112.82	114.47	110.67
!			00	-10 10		00					!	

d Omitted in the Means, on account of the great influence of a disturbance on that day.

Beyon minutes late.

Eight minutes late.

	Angu	ılar Value of	one Scale I	Division of t	ne Declinom		NATION. 21. Increa	sing Numbe	rs denote de	ecreasing W	esterly Decli	nation.	
Mean Gö Tim	ittingen [O ^h .	1 ^h .	2h.	3h.	4h.	5h.	6h.	7 ^h .	8h.	9 ^h .	10h.	11h.
	$\begin{pmatrix} 1 \\ 2 \end{pmatrix}$	Sc. Div. 115°8	Sc. Div. 119'4	Sc. Div. 121'8	Sc. Div. 120°0	Sc. Div. 117 4	Sc. Div. 110.8	Sc. Div. 107 3	Sc. Div. 107°0	Sc. Div. 105'4	Sc. Div. 109 * 5	sc. Div. 106°4	Sc. Div. 109'4
	3 4 5 6 7 ^a 8	114'9 115'4 116'6 116'6 120'0 94'4	115.5 118.4 118.2 116.8 117.4 95.6	115.2 119.4 119.6 119.2 119.2 101.5	113.4 117.0 117.8 119.2 118.0 98.8	112.8 111.6 112.4 115.5 114.4 106.2	107.2 105.0 105.6 110.0 110.4 103.0	104'3 101'8 101'2 107'4 107'4 109'2	102.0 99.2 99.4 105.2 106.5 112.6	103.0 99.4 99.2 103.9 104.4 111.8	104.4 101.7 100.8 105.3 105.6 114.0	106.6 104.2 103.4 107.7 106.4 114.4	109.4 107.9 106.6 111.0 108.3 114.4
MAY.	9 10 11 12 13 14 15	118.7 115.0 116.8 118.0 118.0 131.4	118'4 116'6 116'4 120'0 120'2 128'5	118.6 115.0 114.2 118.1 119.9 128.4	112·2 110·4 110·7 114·2 116·4 117·5	108.8 106.5 105.2 106.4 111.2 108.6	106.0 105.4 100.0 100.4 104.2 94.7	104.2 104.2 97.8 96.4 100.4 97.3	104.4 104.6 97.4 96.6 101.2 92.3	104.6 104.7 100.0 b 99.3 103.4 96.9	105.4 107.5 102.6 102.6 104.0 99.3	106.6 107.8 106.4 106.6 106.6	108'9 108'4 109'4 110'3 107'8 108'3
MA	16 17 18 19 20 21 22 23	116.8 120.5 121.3 119.4 117.6 116.8	118.8 122.9 117.6 120.4 118.8 118.6	118.8 121.2 118.0 116.0 118.6 118.4	118.4 119.4 117.4 112.4 116.0 117.4	113.6 118.5 112.4 103.6 112.4 112.0	105.4 112.3 110.0 100.0 103.8 106.4	104.3 107.0 108.0 105.4 102.4 104.8	105.4 106.1 105.6 101.0 100.0 103.3	101'4 104'4 104'1 101'4 ^d 100'8 104'4	100°4 105°0 104°0 107°6 104°4 106°3	104.0 106.4 106.4 104.4 105.8 107.5	106.4 109.4 108.0 116.0 113.4 110.4
	23 24 25 26 27 28 a 29 30	115.0 117.6 122.9 124.0 118.7 124.7	116.8 118.4 122.4 122.4 115.4 121.9	115 · 2 117 · 5 120 · 8 121 · 4 116 · 2 122 · 5	112.8 114.5 118.4 118.8 115.5 119.4	109.6 109.8 114.4 112.2 107.4 105.6	106°1 106°0 105°6 105°0 105°5 104°2	103.8 105.4 103.2 103.4 104.4 102.8	102.0 102.4 101.6 101.4 105.4 103.0	102.4 102.4 104.7 101.2 100.4 104.8	104.4 104.4 108.0 102.4 101.9 106.0	105.8 106.4 111.4 106.8 105.9 106.6	107.3 108.3 112.5 104.5 108.0 109.0
	31	116.6	117.4	117.3	116.3	114.4	111.4	107.4	105.4	105.0	104.6	107.4	108.2
Hourly	Means	117.70	118.32	118.19	115.37	110.88	105.35	103.72	102.02	102.86	104.77	106.80	109.38
	1 2 3 4 5	120°0 111°5 118°2 114°4 117°4	122.0 116.0 117.6 116.8 119.8	118.8 117.4 117.0 117.4 117.6	115.4 116.4 116.4 114.8 116.4	112.5 112.2 114.4 110.2 111.4	104.8 107.4 110.1 106.4 105.4	102.4 103.8 105.6 109.4 102.7	94.8 105.6 102.5 103.2 101.8	98.8 102.2 103.7 104.1 102.4	101'0 102'8 105'4 104'6 104'4	102.4 102.8 105.7 105.4 107.6	105.8 106.4 108.4 106.6 109.0
	6 7 8 9 10 11	120°4 122°2 120°5 117°2 118°8 121°4	119.0 124.2 119.9 113.0 119.4 123.2	121.5 121.6 118.7 116.0 119.2 122.4	119°2 115°0 115°8 112°5 118°6 117°0	114.0 111.4 106.8 111.1 109.6 113.4	105°2 107°0 104°2 103°4 112°2 109°2	102.0 103.9 103.0 91.7 103.9 103.4	101.6 104.0 102.0 98.2 102.6 102.6	103.0 104.2 101.3 102.6 102.6 98.6	107.4 105.6 102.2 105.4 99.8 97.4	108.4 108.7 102.8 106.1 102.2 104.6	110.5 112.0 105.6 108.3 108.4 100.5
JUNE.	13 14 15 16 17 18 19	116.2 120.4 115.5 122.6 113.6 116.8	109.4 120.4 115.6 119.5 118.4 119.0	114.9 122.8 118.5 119.6 118.4 119.8	112.4 121.8 115.8 116.4 117.4 117.8	110.8 121.4 112.9 115.8 114.4 112.2	110.4 112.1 c 105.4 109.2 111.0 106.6	108 · 2 106 · 7 102 · 9 104 · 6 106 · 0 103 · 0	99.5 103.4 100.6 101.4 100.8 101.9	102.2 102.5 103.6 102.4 101.6 101.2	106.4 104.0 104.6 102.6 102.4 102.5	107 · 2 103 · 0 106 · 6 102 · 6 110 · 8 105 · 3	111.0 104.4 105.2 107.4 110.9 109.0
	20 21 22 23 24 25 26	119.9 115.4 115.5 114.9 118.8	121 · 2 122 · 3 119 · 0 117 · 4 116 · 2 117 · 4	121.2 122.0 119.6 117.8 115.9 117.4	120°4 119°7 119°4 115°5 113°5 117°8	117 · 4 117 · 4 115 · 8 111 · 4 109 · 6 109 · 0	110°2 107°3 b 109°4 106°4 106°8 102°6	103.7 103.5 104.6 102.5 103.6 100.4	100°4 101°3 99°0 102°4 101°4 103°4	98·3 101·4 98·8 103·4 102·0 104·4	98.4 102.4 101.8 105.4 105.4	105.2 105.0 105.5 107.0 107.4 106.4	102'4 109'6 106'9 110'1 107'4 110'0
	27 28 29 30	119 . 9 114.4 117.6	119.8 119.8	118 ·9 118 ·4 118 ·9	115°4 114°2 116°6	112.6 112.4 113.4	111.3 111.6 108.2	105.4 102.2 105.4	100°7 101°2 106°3	104.4 102.0 104.0	104°2 102°4 104°9	107°4 105°4 104°9	112·2 106·7 107·3
Hourly	Means	117*65	118.67	118.91	116.60	112.83	107 .84	103.63	101.64	102:14	103.42	105.63	107.77

^a Omitted in the Means, in consequence of the influence of disturbance on those days.

b Seven minutes late.

12h.	13 ^h .	14 ^h .	15h.	16h.	17h.	18h.	19 ^h .	20h.	21h.	22h.	23h.	Me	ans.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. I	
	110 1	103 0	112 1			112.3	110.4	111.5	110.2	110.5	113.4}	112.15	} 110.8
09'2	115.4	112.2	113.0	112.2	110.8	110.5	110.0	110.4	110.4	111.3	111'4	110.52	Ì
12.0	111.2	111'2	109.8	110.2	109.2	109.6	109.6	107.6	111.2	112.9	115.0	109.63	1
10.6	112.6	110.2	110'4	110.8	110.5	110.4	110.0	112.4	112.4	112.7	116.4	110.01	İ
12.4	111.4	111'4	110.5	110.3	110.5	111.0	113.0	113.6	102.8	112.6	114.8	111'32	
11.5	109.0	129.2	112.8	121.5	131.2	125.5	12.7	130.3	118.5	98.4	102.4	110.00	1
14.8	111.4	110.2	109.3	109.4	109.3	112.0	111.8	105.1	110.5	115.8	114.4	108.75	
09.5	108.6	108.4	109.4	110.0	109.6	109.6	116.4	111.9	111.4	112.4	113.8	110.31	i
07.8	108.9	109.0	109.4	109.2	109.4	109.6	109.4	112.0	113.4	114.4	115.8	109.77	
11.0	111'4	114.6	109.4	109.0	109.2	110.5	111.0 c	110.4	109.6	111.0	115.2	108.70	
10.4	111.0	108.2	108.4	109.2	113.2	109.8	110.4	111.0	112.0	113.2	115.4	109.24	111.6
07.8	107.4	107.9	108.2	109.3	109.6	110.2	110.0	113.2	115.0	123.0	141'4	111.22	
08.4	115.8	100.0	105.4	119.5	111.5	110:4	109.4	100:6	111.0	113.4	114.2	109.95	
.09.8	112.0	114.0	109.6	113.4	110.4	110'4 114'4	110°5	109.6 112.4	104.8	112.0	114 2)	110.68	}
10.8	111.4	112.5	111.6	114.5	113.5	115.5	111.4	102.8	104.5	116.5	116.6	112.42	
10.3	110.4	106.5	115.8	110.2	118.4	112.6	113.6	106.3	116.3	117.4	115.8	111.93	
.08*8	109.4	112.8	112.7	108.4	110.2	113.2	113.2	111.4	111.4	109.0	110.0	109.95	
13.6	112.3	112.7	111.8	111.8	114.4	114.0	108.6	108.2	108.2	111.6	114.0	110.65	1
11.0	109.6	108.6	110.5	109.5	109.2						113.2	110'44	
					10014	110'4	109.0	111.5	111.0	111.4	113.23	109.18	
07.5	107.6	106.7	106.4	106.0	108.4	108 '6 115 '4	112 .4 110 . 8	112.2 110.6	112 .4 116.0	115.0 116.6	119.2	110.49	
09°3 12°2	108.2 110.2	107.0 110.5	106 . 4	109 . 3	110°0 109°4	109.6	110.0	110.0	110.5	114.0	117.0	111.22	
08.4	104.2	107.9	106.9	107.0	123.0	110.0	112.4	111.4	116.0	113.5	116.5	110.82	
11.9	112.5	113.4	115.4	111.5	111.4	111.4	124.0	81.8	110.6	115.4	125.2	110.37	
10.4	108.7	108.2	109.2	109°4 e	109.3						— 7	110.22	} 110°3
			_			106.8	107.0	107.8	110.4	112.8	114'6}		110 3
10.4	110.6	110.0	108.4	109.6	109.6	112.4	112.2	111.2	111.5	115.6	116.0	111.55	
11.00	110.28	109.61	109.72	110.53	111.50	111.19	110.82	110.50	111.08	113.67	116.50	110.46	
14.0	114.8	108'4	109.0	107.2	107.4	107.5	106.4	107.4	108.2	108.0	104.4	108.39	
08.2	108.5	108.3	110.6	110.0	112.8	112.8	113.4	110.4	109.2	115.6	113.6	109.90	
08.0	110.6	110.4	119.4	112.4	110.0	108.6	103.5	111.5	111.0	111.4	113.5	ر60 110	
08'4	109.1	109.2	109*4	109.2	109.2	113.0	111.5	110.4	110.4	111.2	112.0	109.857	
09.2	109.2	109.0	108.2	109.2	109.3						116.4	110.58	
10.2				11010	117.0	117.0	111.2	110.0	110.4	111.2	116'4)		
10.8	110.0	112.2	116.4	116.6	117.9	117.0	116.4 110.2	114 · 2	121.9	119 '4 113 '8	121.6 121.4	111.30	
10.7	109 ° 6 107 ° 4	109.5 108.4	108.6 108.2	108.6	113 ·7 113 ·4	110'6 112'2	109.6	111.4	112.2	113.6	114.0	109.75	
07.0	107 4	108 4	108.2	117.7	116.4	111.8	110.0	105.8	107.0	115.4	115.8	109.02	
10.8	109.4	133.8	112.3	107.6	108.4	108.1	108.4	110.0	110.9	109.6	117.8	111.02	110
99.0	115.6	121.4	111.4	119.2	119.0				-		112.2}	112.45	
			_			132.4	111.4	117.4	113.2	113.0	112.25	:	
05°4 06°4	106.2	108.9	105.2	112.2	109.4	109'4	111.4	111.0	111.4	111.8	116.4	109.47	
un / 1	110.4	110'4	110.0	117.4	113.6	111.5	108.4	109.4	111.0	112.5	113.4 116.1	111.54 109.06	
	108.4	108.0	106.4	110.4 110.0	108'8 117'5	108 ·2 112 ·4	108.7 104.8	110.4 t	104 . 9	111.7 111.4	111.4	110.43	
08.0		108.4 113.0	108 . 1	115.0	116.0	115.5	110.5	109.2	108.4	110.6	114.0	111.25	1
08.0 09.2	118 .4			109.2	109.4	-		-		_			
08.0	110.2		109.2			109.6	109.8	109.5	111.5	110.6	114.5}	109.88	
08.0 09.2 12.8 09.2	111.0 111.0	108.8	109.2		_		109.9	109.9	111.5	111.5	107.4	109'17	
08·0 09·2 12·8 09·2 	110.2 111.0	106.0	- 106 ·4	109.3	110.0	109.8					994-c H		
08.0 09.2 12.8 09.2 	110.2 111.0 102.8 114.0	108'8 	106.4 108.6	109°3 110°5	10°0	109.4	110.0	109.2	109.7	110.6	113.3	110.23	
08·0 09·2 12·8 09·2 	110.5 111.0 	108.8 106.0 109.2 109.4	106.4 108.6 109.0	109.3 110.2 108.0	108.6 108.8 110.0	109 . 4 108.8	110°0 109°4	109 . 2	109 .7 110 .0	110.6 110.4	112.3	109.57	- 110°
08:0 09:2 12:8 09:2 	110.5 111.0 	108'8 106'0 109'2 109'4 110'2	106.4 108.6 109.0 110.3	109°3 110°5 108°0 109°4	110.0 109.8 108.6 108.5	109 . 4 108.8 108.8	110°0 109°4 109°5	109 . 2 110 . 0 110.4	109.7 110.0 112.0 d	110.6 110.4 114.5	112°3 114°0	109.57 110.12	- 110 °
08:0 09:2 12:8 09:2 	110.5 111.0 	108'8 	106'4 108'6 109'0 110'3 108'2	109'3 110'5 108'0 109'4 108'0	110.0 109.8 108.6 108.5 109.6	109.4 108.8 108.8 111.4	110°0 109°4	109°2 110°0 110°4 110°1	109.7 110.0 112.0 d 111.0	110.6 110.4 114.5 112.4	112.3 114.0 114.9	109.57 110.12 109.32	- 110 °
08:0 09:2 12:8 09:2 	110.5 111.0 	108'8 106'0 109'2 109'4 110'2	106.4 108.6 109.0 110.3	109°3 110°5 108°0 109°4	110.0 109.8 108.6 108.5	109.4 108.8 108.8 111.4	110.0 109.4 109.5 109.6	109.2 110.0 110.1 —	109.7 110.0 112.0 d 111.0	110.6 110.4 114.5 112.4	112.3 114.0 114.9	109.57 110.12	≻110 °
08·0 09·2 12·8 09·2	110.5 111.0 	108.8 106.0 109.2 109.4 110.2 108.6 105.8	106.4 108.6 109.0 110.3 108.2 106.4	109'3 110'5 108'0 109'4 108'0 107'4	110.0 109.8 108.6 108.5 109.6 109.4	109'4 108'8 108'8 111'4 — 108'9	110°0 109°4 109°5	109°2 110°0 110°4 110°1	109.7 110.0 112.0 d 111.0	110.6 110.4 114.5 112.4	112.3 114.0 114.9 	109.57 110.12 109.32	≻ 110°
08:0 09:2 12:8 09:2 	110°5 111°0	108'8	106'4 108'6 109'0 110'3 108'2	109'3 110'5 108'0 109'4 108'0	110.0 109.8 108.6 108.5 109.6 109.4 — 110.4 111.0	109.4 108.8 108.8 111.4 	110.0 109.4 109.5 109.6 	109.2 110.0 110.4 110.1 	109.7 110.0 112.0 ^d 111.0 	110.6 110.4 114.5 112.4 ————————————————————————————————————	112·3 114·0 114·9 	109.57 110.12 109.32 109.57 111.17 110.26	≻ 110 ° -
08·0 09·2 12·8 09·2	110·5 111·0 105·8 114·0 109·3 110·0 108·2 110·0 	108'8	106.4 108.6 109.0 110.3 108.2 106.4	109'3 110'5 108'0 109'4 108'0 107'4	110.0 109.8 108.6 108.5 109.6 109.4	109.4 108.8 108.8 111.4 — 108.9 110.4	110.0 109.4 109.5 109.6 	109.2 110.0 110.4 110.1 	109.7 110.0 112.0 d 111.0 110.8 112.4	110.6 110.4 114.5 112.4 ————————————————————————————————————	112.3 114.0 114.9 	109.57 110.12 109.32 109.57 111.17	- 110 °

[°] Nine minutes late.

d Five minutes late.

e Four minutes late.

**************************************	Angu	lar Value of	one Scale I	Division of th	ne Declinom		NATION. 21. Increas	sing Number	rs denote de	creasing We	esterly Decli	nation.	
Mean Gö Tim	ittingen \	Oh.	1 ^h .	2h.	3 ^h .	4 ^h .	5 ^h •	6 ^հ •	7 ^h .	8 ^h •	9h.	10h.	11h,
	$ \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix} $	Sc. Div. 121 2 117 4 117 8	Sc. Div. 123°5 119°3 119°6	Sc. Div. 122°0 121°0 120°4	Sc. Div. 120°9 117°4 121°2	Sc. Div. 111 0 113 9 110 6	Sc. Div. 111'0 109'4 106'8	sc. Div. 108 4 104 2 104 4	sc. Div. 105 6 102 2 103 8	Sc. Div. 106.7 104.4 104.6	Sc. Div. 104 9 105 6 104 4	Sc. Div. 106.4 107.0 105.4	Sc. Div. 108'4 107'4 109'5
	4 5 6 7 8 9	119.0 122.2 119.8 116.4 119.2 121.8	121 '4 123 '4 120 '4 116 '0 119 '6 123 '6	118 '4 118 '8 121 '5 114 '0 116 '2 123 '9	114.2 115.5 117.4 109.0 114.6 123.2	112.4 112.2 114.3 109.4 111.4 119.3	105.6 109.7 97.3 106.0 107.5 111.5	103 · 2 106 · 1 94 · 4 104 · 3 102 · 4 108 · 9	103 '4 103 '9 101 '6 104 '4 105 '4 102 '2	103.6 106.8 101.7 105.4 99.4 109.9	107.6 106.0 101.5 105.4 101.4	108.8 107.4 104.0 106.4 96.2 106.5	109.2 108.3 106.4 112.8 102.6 110.4
JULY.	11 12 13 14 15 16 17	122.8 119.4 117.4 120.0 119.2 114.5	123 · 4 122 · 5 123 · 4 122 · 4 120 · 0 113 · 4	122°0 125°3 123°4 123°0 120°5 113°4	118 · 2 121 · 0 120 · 6 120 · 8 117 · 6 116 · 8	114.6 113.2 110.4 115.4 112.4 112.2	111.5 106.2 103.4 108.4 107.2 108.9	105.4 101.2 100.4 104.4 101.6 101.9	98.6 99.4 100.7 100.5 100.0 100.4	101.0 99.2 101.5 99.4 101.3 96.4	102·2 99·4 101·2 101·4 103·0	103.4 103.4 105.4 103.8 101.4 105.9	110'4 106'4 110'2 108'1 104'1 107'3
. 3	18 19 20 21 22 23 24	118°4 117°4 118°3 124°2 121°4 118°2	120°5 116°0 121°2 124°4 121°6 121°4	120°8 118°4 120°4 122°5 118°4 121°2	118'4 116'4 115'8 117'8 117'3 119'1	113.4 114.3 110.2 113.7 113.4 113.6	110'4 108'4 106'4 107'8 106'6 107'2	105°2 103°4 102°4 101°2 106°3 103°2	105.4 101.4 94.2 97.2 101.0 102.9	104.4 101.2 98.2 101.2 103.1 106.2	105.2 103.9 103.0 104.2 105.0 110.0	107.4 107.6 106.8 107.4 109.1 110.4	110'2 109'8 110'3 110'8 112'4 110'8
	25 26 27 28 29 30 31	118.0 120.9 118.5 119.4 120.0 118.8	119'4 120'9 122'2 118'6 123'3 121'0	120 ' 4 120 ' 1 119 ' 2 118 ' 4 123 ' 4 123 ' 6	113 ° 4 117 ° 4 115 ° 2 116 ° 4 120 ° 4 123 ° 0	104.0 109.9 105.9 112.7 111.6 117.2	104.5 105.9 103.4 109.4 105.0 108.6	95.5 104.4 100.6 104.2 102.9 104.6	98.4 104.6 101.4 102.5 101.9 102.6	98.5 106.6 105.2 103.4 99.6 101.4	103.0 108.4 106.5 106.0 105.4 104.3	109.4 110.8 110.2 107.4 106.4 107.4	110'4 115'3 111'2 109'4 109'9 110'4
Augu Hourly		119.32	120.83	120.39	117.74	112.32	107.18	103.12	101.69	102.60	104.24	106.36	109.35
	$\begin{pmatrix} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{pmatrix}$	118 2 121 0 115 4 121 3 123 4 116 6	121.8 124.6 129.8 124.4 127.4 121.5	124.2 119.4 125.4 121.1 125.0 122.2	123.0 118.6 114.8 124.2 124.6 117.4	119.5 115.9 114.6 111.9 112.6 112.0	113.4 111.4 110.2 110.9 107.6 105.4	105.2 107.8 104.7 104.5 103.9 101.5	100°4 103°8 103°3 100°6 95°0 99°2	98.8 101.3 104.7 103.9 100.4 102.8	98.4 104.5 106.0 105.6 104.6 107.2	103.4 105.5 106.6 105.6 107.4 116.2	108.3 106.4 109.0 109.2 106.2 110.4
	8 9 10 11 12 13 14	117:3 119:4 117:4 117:4 118:2 125:4	120°2 120°0 121°3 122°0 120°0 124°2	120.6 122.4 121.6 123.3 120.8 122.8	118.4 121.6 120.4 119.2 120.4 118.0	111.2 114.0 110.4 113.5 114.4 104.8	105.4 108.8 105.4 106.6 105.2 107.8	101.7 100.4 98.9 98.6 97.9 83.4	98°3 95°4 96°6 94°6 96°4 96°4	98.0 96.6 97.9 96.4 98.4 96.6	100°3 99°6 102°8 98°8 101°4 99°3	103.9 103.8 104.6 103.2 104.6 103.6	107.5 107.9 108.4 108.4 107.5 107.6
AUGUST.	15 16 17 18 19 20 21	116·2 124·7 121·9 119·9 117·8 118·6	120°4 130°3 126°3 122°9 121°4 121°8	125.5 127.2 126.9 121.6 121.4 122.6	123.6 120.5 121.8 116.6 114.0 118.0	115.6 117.9 115.4 109.0 110.2 108.4	106·3 110·0 109·7 103·6 107·5 102·9	100°3 110°2 101°9 99°4 105°4 100°4	93.8 98.0 96.0 99.0 104.0 98.5	94.8 97.6 96.8 102.2 107.6 97.0	109.6 98.5 98.8 106.0 107.4 98.5	102.6 103.7 98.4 110.4 108.3 105.9	105'4 106'4 102'4 108'9 108'9 107'6
	22 23 24 25 26 27 28 29	121 · 4 122 · 0 112 · 5 124 · 0 119 · 5 118 · 5	123.8 120.5 116.6 121.0 121.8 125.0	122·3 124·3 114·2 118·0 120·7 124·6	116.0 119.8 120.0 116.2 118.0 118.8	109.5 111.9 106.2 111.8 114.5 111.4	103 ° 9 103 ° 2 101 ° 6 105 ° 2 106 ° 7 104 ° 6	99.0 98.9 100.4 100.4 99.4 95.4	98.8 100.7 100.7 98.4 96.1 97.4	102.5 101.6 101.6 99.8 97.8 98.2	104.2 105.4 102.8 102.3 102.2 101.4	108.2 106.6 106.6 105.7 107.5 107.0	111.6 111.4 111.3 108.5 108.9 111.4
	30 a 31 a		_			_	_			=			
Hourly	Means	119.20	122.87	122.42	119*33	112.36	106.80	100.82	98.39	99.72	102.73	105.80	108.31

^{*} The Observations omitted, the Magnet having been affected considerably by the vertical iron shafts of Robinson's Anemometer.

	Angula	ar Value of	one Scale D	ivision of th	e Declinome	$\begin{array}{c} \text{DECLIN.} \\ \text{eter} = 0' \cdot 72 \end{array}$	ATION. 1. Increasi	ng Number	s denote dec	reasing Wes	sterly Declir	nation.
12h.	13h.	14 ^h .	15h.	16 ^h .	17 ^h .	18h.	19 ^h •	20h.	21h.	22h.	23h.	Means.
Sc. Div. 111 4 108 8	Sc. Div. 111.6 110.4	Sc. Div. 110.6 119.4	Sc. Div. 110°0 108°9	Sc. Div. 115.8 108.7	Sc. Div. 109 2 109 3	Sc. Div. 109'8 109'7	Sc. Div. 109 3 109 7	Sc. Div. 109 5 111 4	Sc. Div. 110.5 111.0	Sc. Div. 111.6 111.0	Sc. Div. 113*4 111*0	sc. Div. 111.78 110.35
109.0	109.2	110.0	109.4	109.4	107.5	111.6	112.0	111.1	111.2	111.2	116.4	110.72
108.8 109.6	110.0	109.7 109.8	109.4	109°3 119°4	110.6	110.4 111.4	114.3 110.2	116.7 113.0	123°4 114°6	118.4	96 ·3	111.89
107.4	107.4	103.0	107.2	127.4	122.8	117.4	108.4	111.1	112.2	112.4	110.0	110.20
113 · 2	95.0 95.0	108.2	108.5 78.5	109.6 124.8	110°1 126°4	111.5 122.6	111.0 127.4	111'6 115'2	112.3	112.9	116'4 119'8	$110.40 \\ 109.76 \\ 110.7$
108.4	108.0	117.4	114.6	112.6	112.0	108.2	114.4	97.4	104.6	111.4	112.4	111.97
111.7	112.0	121.5	109.2	111.4	108.0	110.4	98'4	106.4	111.8	112.2	116.8	110.97
110.4 111.6	110°4 109°4	122.4 110.2	108.8	109 . 4	106.4	108.4 112.5	109.4	110.2	110.7	111.6	112.0 115.4	110.37
109.4	110.9	109.8	109.2	109.0	109.5	110.4	109.0	109.3	109.5	111.2	115.4	110.43
104.0	108.4	108.4	108.4	110.5	110.5	111.4	108.4	109.8	110.5	101.8	110.4	108.682
110.5	106.4	105.4	106.6	108.4	109.4	109.2	109.2	109.4	110.4	111.8	$ _{111\cdot 4}$	108.44
110.4	108.5	108.0	108.2	109.4	111.6	111.7	109.8	109.0	111.4	108.5	110.0	110.66
110.8	109.6	109.4	109.4	110.5	110.8	112.5	110.2	112.0	108'0	111'4	114'6	110.58
111.8	110.0	108.4	108.0	108 . 9	110.7 128.4	127.6 118.4	117.6 110.4	116°4 103°6	112.8 111.5	110.5	119°0 115°5	111.19
110.9	109.4	110.4	112.8	110.2	111.8	111.6	112.4	111.4	112.5	112.4	115.0	111.52 >110.8
114.4	112.2	109.4	109.4	115.2	125.0		100:5		100:4	110:0	112.0	112.21
111.2	109.4	110.6	115.2	108.0	109.7	109 ' 3	113.8	110°2 114°0	109.4 112.5	112.2	114.9	109.82
115.2	111.8	112.3	111.2	112.0	111.0	112.3	120.2	120.1	115.2	113.4	116.4	113.22
112.0	110.8	107.6	108.6	109'4	109.6	110.0	110.2	109.9	109.3	113.1	116.4	110.28
110.6 110.2	110°9	110.6 110.7	112'8 115'4	112.8 117.5	114.4 123.2	111.5 114.6	111.0	114°5 111°1	117.4 112.4	110.8	112.2 112.1	111.67 J 112.11 J
111.6	109.0	110.4	111.5	116.4	113.1	110.4	110.0	111.6	111.5	111.0	107.6}	111.25
110.14	109:37	109.67	108.96	113.58	112.99	112.48	111.20	110.83	111.40	111.20	113.17	110.91
110.4	110.7	108.6	110.0	109.2	109.8	110.0	113.8	111.9	113.6	116.5	117.4	111.21
108.4	109.2	110.4	106.9	107.2	109.0	110.2	117.4	114.5	113.4	118.6	120.0	111.80
110.4	109.6	108.4	117.5	128.4	117.1	116.1	119.4	122.2	101.2	128.4	123°9 119° 4	114.78 >111.6
108.4 113.4	122.4 112.2	114.4 111.2	127.6 113.9	120.4 109.4	117.6 113.4	110'4 118'2	108.6	106.8 114.2	110.0	108.4	107.4	111.87
126.6	111.8	118.9	125.2	116.4	116.0			109.6	113.6	112.4	114.6	113.42
111.5	109.0	108.4	109.4	110.6	114.6	106.6 115.6	117.6 112.6	111.6	112.5	109.6	115.4	110.12
110.6	109.9	109.8	109.4	111.3	110.4	110.4	109.6	110.5	112.0	112.5	114.1	109.99
110.4 110.0	108.7	110.0	109 . 2	109°8 109°4	110°2	119.4	110.6	109.6 110.4	110.8	111.8	114·4 113·9	110.02 109.34
109.5	110.6 109.4	110.8	109 1	111.4	111.6	112.5	110.4	111.6	112.4	117.6	121.4	110.21
109.5	110.0	108.2	108.9	108.8	109.4	110.4	110.6	110.6	111.6	109.4	111:4}	108.40
107.2	106.4	108.4	112.6	110.0	112.6	114.6	116.8	113.5	105.8	114.2	119.2	110.63
107.2	107.2	106.2	107.8	110.6	109.6	112.8	112.1	110.2	111.9	109.4	112.0 116.5	110.94 111.10
111.6 108.7	109.4	107.8	128'4 111'0	115'4 111'6	110.0	108.6 110.4	110.4 112.6	110 °0 115 °4	111.5 107.4	112.0 112.4	113.7	110.42
109.7	110.8	109.2	110.5	109.7	110.4	110.2	111.5	111.2	113.3	113.4	115'4	111.23 >110.73
107.5	109.8	109.2	108.6	108.4	110.4	107:0	107:0	114.5	115.4	114.8	117.4	109.64
110.6	111.6	110.7	111.9	110.0	108.8	107.8 109.6	107.6 111.4	107.9	117.6	115.8	115.4	110.94
112.4	112.4	113.6	110.4	109.4	110.4	114.7	120.0	114.4	114.0	118.9	116.9	112.24
115.4 109.0	113.0	113.6	113.6	116.3	120.2	119'4	120.8	117.1	118.0 118.0	113.8 119.9	120.7 116.4	112.64
110.4	109 . 4 107.9	108 .4 109 . 5	108'4 117'4	111.6 111.6	108·4 109·4	109 .4 108.4	109°3 110°4	111°2 111°5	118.4	115.2	119.3	110.94
111.2	110.2	122.2	115.4	110.0	109.2						$\frac{113\cdot 3}{113}$	111.10
_	_	_	_	-	_	109.3	110.4	112.3	113.5	— 115.0		
11000												-
110.84	110.45	110.68	112.99	111.84	111.23	111.86	112.84	112.17	112.06	114.27	116.22	111.15

1	Angular Value	of one Scale l	Division of t	he Declinom		NATION. 21. Increas	sing Number	rs denote de	creasing We	esterly Decli	nation.	
Mean Göttinge Time,	en } 0h.	1h.	2 ^h .	3 ^h .	4 ^h .	5 ^h •	6 ^h .	7 ^h .	8 ^h •	9 ^h •	10h.	11ħ.
(1	a Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
2 3 4 5	119°3	121°3 115°3	122°4 122°5	 119°2 114°9	112.4 111.9	111°1 110°4 103°6	106.4 104.2 102.9	101'7 101'9 104'2	105.4 101.9 106.6	102.6 104.9 108.4	104°4 106°2 113°6	107°4 106°2 112°8
6 7 8 9 10	117°9 117°6 118°4 117°6 117°4 121°0	119'2 121'4 121'4 117'0 122'0 121'4	120°4 121°4 121°2 106°4 121°5 120°6	118.4 120.4 118.5 108.4 117.2 117.8	114.4 113.9 111.9 102.4 110.2 112.4	105.2 106.4 113.6 108.6 104.6 103.4	101.2 100.4 98.2 92.6 98.8 101.5	96.8 100.0 96.9 91.5 100.4 98.4	99.6 102.0 98.3 93.0 101.8 99.6	104.4 105.3 101.1 96.2 105.9 103.4	107.4 108.5 105.4 101.6 110.2 107.4	110°0 110°4 107°6 111°4 110°4 110°4
3 12 13 14 15 16 17 18 18	121.2 118.8 118.4 120.0 115.6 118.8	114'8 120'0 122'7 124'9 123'4 123'2	98'4 119'4 122'7 127'2 120'0 122'0	98.2 119.2 120.1 124.4 118.4 122.8	100.6 108.6 114.4 120.4 116.4 111.4	91.6 106.6 108.3 113.2 104.4 107.4	96.0 100.2 101.4 104.6 98.2 104.8	94.5 97.5 96.4 98.4 93.4 102.4	100°4 98°0 96°5 99°2 99°2 99°5	106.5 102.0 101.0 102.4 103.4 103.4	112.4 106.8 105.3 105.6 108.8 106.4	111.2 108.9 109.4 107.8 110.6 115.4
19 20 21 22 23 24 25 26	118.8 116.5 115.2 110.4 117.9 113.4	120'4 118'4 116'8 114'4 182'0 116'4	120°2 119°4 115°0 104°8 80°5 117°4	116.8 114.2 112.4 96.9 83.0 114.4	113.2 112.0 105.3 97.6 110.1 110.8	108·2 105·4 106·6 96·9 153·4 103·3	103.4 100.5 105.0 94.4 78.8 98.2	101.5 97.9 101.5 98.9 124.8 95.4	103°4 101°4 102°4 103°6 86°3 95°9	106°2 105°4 108°4 109°3 97°1 99°4	108.4 108.9 112.4 112.5 104.8 104.5	107.5 110.4 113.4 114.0 124.0 107.5
27 28 29 30	25.8 115.0 113.4	74.0 118.2 117.4 114.5	83.8 119.4 120.3 117.4	97'6 118'4 123'5 118'8	109'9 112'5 116'6 122'4	103'0 106'9 112'9 116'4	94.0 102.2 109.3 111.4	99°2 100°4 118°0 105°2	105'8 100'4 100'4 101'0	108'8 102'3 94'4 102'6	110°0 103°2 101°6 103°7	107'4 109'4 116'1 107'2
Hourly Mea	ns 116.88	109.30	118.18	116.06	111*44	106.24	101.34	99.62	100.19	103.47	107.31	110.36
$\left\{\begin{array}{c}1\\2\\3\end{array}\right.$	112.2	117°4 114°4	116°5 117°4	118.7 115.1	118.7 107.0	113.2 110.6	111.6 108.9	108 ·2 106 ·4	106°4 105°3	106°1 105°6	105°2 106°0	110.3
4 5 6 7 8 9	113.8 114.4 114.0 114.4 120.6 116.2	116'4 117'9 116'7 117'4 118'4 120'4	115.9 118.4 117.0 118.8 121.4 121.9	114.8 118.8 118.6 117.0 119.5 117.4	112.6 112.4 114.4 113.4 116.4 124.2	110.3 108.0 107.4 107.4 107.5 115.4	107'4 103'4 103'2 102'0 100'9 109'2	106.5 100.4 101.4 102.4 99.6 105.5	107.5 99.0 104.2 102.8 97.9 103.9	108.4 102.8 106.8 105.9 98.0 105.4	107.9 104.2 108.8 107.9 98.3 105.7	106'4 102'4 108'8 107'9 99'3 106'7
10 11 12 13 14 15 16 17 17 18	115.0 117.4 112.5 115.2 111.5 112.4	118'4 118'6 119'4 118'2 112'9 112'0	119'8 122'4 64'4 118'2 108'8 118'2	118'4 121'4 101'0 111'9 114'1 114'4	114.5 114.6 104.4 112.4 114.2 110.0	108.4 108.4 87.9 108.9 106.6 104.6	102.2 102.8 100.6 100.4 101.9 104.3	100.7 103.4 104.6 100.5 103.9 103.4	100°4 103°4 99°4 102°6 106°4 104°8	105.2 103.3 103.8 106.9 107.7 107.4	106'4 106'7 104'4 109'3 110'4 108'2	107.6 106.4 105.4 108.8 112.4 108.3
O 17 18 19 20 21 22 23 24	122.5 113.8 113.6 114.6 110.4 137.5	117'6 109'8 116'3 116'4 112'6 57'2	111.4 111.6 119.4 118.0 114.3 142.6	107.0 115.5 119.4 119.4 113.5 118.3	101.6 106.6 115.4 117.6 115.6 128.3	105.8 111.2 110.4 113.4 109.3 125.3	108'4 103'4 106'4 108'2 106'4 119'4	104.5 102.6 107.1 106.2 106.6 105.9	105.4 105.8 107.6 107.4 108.2 103.6	107.9 106.5 108.2 107.9 103.8 109.7	110.5 109.3 109.4 109.4 98.4 107.4	118.0 108.5 113.5 109.4 108.1 120.0
24 25 26 27 28 29 30 31	6d 110·1 113·5 113·8 113·6 102·2 112·4	110'3 117'2 116'8 116'4 120'4 117'4	95°2 118°6 121°4 120°4 122°9 119°3	107°3 119°2 121°6 119°7 124°8 120°3	114.9 115.4 119.5 116.5 122.2 116.3	98.4 106.0 114.3 110.8 125.6 111.7	104.4 103.4 109.6 105.4 106.4 106.9	119.4 104.2 106.4 101.8 106.4 104.4	111.0 105.4 106.4 103.6 102.2 105.0	108.0 108.4 105.4 104.6 102.4 106.6	109'4 110'0 106'4 107'2 105'1 108'2	108.4 108.4 106.8 109.2 108.2 108.4
Hourly Mea		116.40	118.08	117:59	114.36	110.58	105.59	103.80	104.25	105.79	107:30	108.27

^a Observations omitted, having been affected to an uncertain amount by the induced magnetism of the vertical iron shafts of Robinson's Anemometer.

	Angu	lar Value of	one Scale	Division of t	he Declinon		VATION. 21. Increa	sing Numbe	rs denote de	creasing W	esterly Decli	nation.
12 ^h .	13 ^h .	14 ^h .	15 ^h .	16h.	17 ^h .	18 ^h .	19h.	20h.	21 ^h .	22h.	23h.	Means.
Sc. Div.	Sc. Di▼.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
108.9	109.0	106.9	106.2	109.4	109.4	110.7	111.6	112.4	116.4	116.8	116.4	
115.4	118.2	123.4	115.8	115.4	110.4	111.0	112.5	112.4	112.6	113.8	113.8	112.41
110.5	110.4	128.2	117.3	109.7	104.9	11114	110:0	11110	111.0	113.6	114.5	111.89 >110.88
111.4	110.8	112.0	120.4	118.8	114.3	111 '4 118 ' 0	112.0 112.4	111'0 111'4	111.0	112.0	113.6	111.77
112.0	110.3	111.8	111.8	110.6	112.3	111.8	111.2	112.4	109.3	113.5	115.5	111.25
108.4	108.9	110.6	110.4	110.6	110.4	110.4	110.8	111.4	111.8	112.0	114.4	110.11
107.6	109.2	110.9	108.8	114.4	108.6	106.6	111.3	111.5	113.3	113.2	113.7	107:32
112.0	110.2	109.2	117.1	111.5	109.9	110'4	110.0	111'2	109.1	110.4	111.2	110.24
111.2	110.6	116.2	117.2	112.6	113.0				100:4	100:0	107:0}	112.63
					100:0	110.5	115.9	119.0	123.4 114.4	108 ·2 115 ·2	127.8 }	1
112.0	110'4 109'2	120.4	109.6	111'0 111'4	120°0 110°7	118.6 111.2	113.7 112.4	112.6 112.4 c	113.8	113.0	115.0	109.23
107.5 110.2	110.4	108.9	112.6	115.8	110.4	111.3	111.0	111.2	113.4	114.3	115.0	110.81
107.4	104.4	103.3	110.2	127.6	111.6	116.5	113.8	109.0	111.8	111.9	117.9	110.40
110.0	110.3	111.0	111.5	111.5	111.5	114.5	120.4	117.4	120.4	113.0	115.2	$\left \begin{array}{c} 112.43 \\ 111.55 \\ \end{array}\right> 111.09$
113.4	109.4	109.4	109.8	110.6	110.4		_	_				111.87
			_			108.2	117.2	113.4	116.2	112.6	116.6}	!
108.0	107.6	108.9	109.2	112'4	120.4	107.5	120.6	118'4	116.2	116.6	115.4	112.07
110.6	109.4	109.0	108.4	108'4	106.5	105.0	109'4	112.4	112.0	112.6	112.3	109.42
112.8	112.4	111.4	110.6	109.4	110.1	114.6	120°0 115°4	112.0 120.3	117'0 124'6	114°0 140°0	116.4 104.0	111.46
119.0 111.6	110.0 113.3	110.4	108.4 115.6	108.9	109.0	122.0 100.4	107.4	101.4	109.2	112.4	112.0	95.87
110.4	108.3	118'0 107'9	109.4	109.0	103 6	100 4	107 4	101 4	103 0			1 1
	100 0	101 9	-	105 0		118.8	130.4	109.4	107.5	107.2	98.6	108.37
109.7	110.4	109.0	107.8	107.4	109.2	111.4	111'2	110.8	110'6	111.8	112.0	99.23
134.0	124.4	105.4	112.9	111.3	109.4	103.3	109.2	110.0	106.2	107.0	109.8	110.48
121.2	107.5	131.9	114.5	120.0	118.9	114.0	120.4	105.4	110.6	109.9	110.0	113.67
108.4	108.5	108.2	108.6	110.0	110.4	110.4	110.2	110.3	113.4	112.3	115.4	110.81
112.10	110.65	112.86	112.07	112.74	111.36	112.11	114.22	112.48	113.68	113.47	113.75	110.94 \ 108.2
107.0	107.7	109.3	109.9	110.2	113.0	110.8	112.5	111.8	114.6	112.8	112.2	111.22
107.4	109.5	109.4	109.8	110.4	110.5	11115	112.4	112.5	113.2	112.6	113.0	110.31
108.5	109.4	109.6	110.0	110.5	111.5	111.2	112.4	112.0	114.9	113.8	113.4	110.99
101.5	109 4	109 6	108.3	109.4	109.7	109.6	110.3	111.4	111.4	112.0	112.4	108.88
109.5	109.2	110.0	109.2	109.6	109.7	110.4	110.2	110.4		113.7	112.4	110.56
108.6	108.9	109.4	109.4	109.6	110.4	112.4	113.4	119.5	125.2	125.2	117.5	111'95
93.5	103.0	109.6	109.2	110.4	109.8	95.2	114.8	117.2	113.8	113.6	113.6	108՝40 ๅ
105.4	106.7	106.7	115.2	111.7	110.4				11010	11440	113.9	112.02
109.5	1004		11011	110:0	110:0	111.0	115.2	113.0	113.8 115.0	114.0 115.6	113'9)	110.75
109 2	108.4	113.2	110'4 107'9	110'0 113'4	110.0	112.2 114.4	111.9 111.9	110.2	116.4	129.0	119.4	110 75
104.9	110.6	109.0	1107 9	110.5	110.6	110.4	110.4	111.8	111.4	112.2	113.4	105.60
108.9	109.6	109.0	113.4	110.5	110.6	114.6	119.2	115.7	117.4	112.5	112.4	1111101
155.6	112.5	110.8	110.2	111.6	113.5	111.0	115.4	112.8	120.4	114.6	112.0	111.28 > 110.8
108.6	112.4	114.4	115.0	114.8	114.8						}	113.10
					_	119.4	123.8	121.5	117.4	126.0	118.7	1
116.4	109.0	110.5	111.4	111.4	110.8	111'4	114.2	112'4	112.2	113.3	113.2	111.12
107'4 112'0	109.6	110.4	113.7	120'9	111'4	114.4	112.5	111.0	115°2 111°8	112°2 114°6	112'3 115'0	110.65
110.4	107.4 110.4	110.4	108.4	108°4 109°7	109.7 110.6	112.5 111.5	107.3	111°9	111.8	112.8	112.6	111.82
109.5	109.6	110.4 113.7	110 .4	114.0	113.7	115.4	113.4	135.2	87.0	133.7	142.3	112.85
120.4	112.4	115.9	106'4	105.9	79.0				_			1 1
-					_	33.7	112.4	176.2	132.6	78.3	$\frac{-}{125\cdot 8}$	111.43
199.4	110.4	119.4	111.4	107.4	107.6	109.2	102.2	109.4	112.5	113.2	112.6	109.25
110.6	112.4	109.8	110.2	110.4	113.2	111.5	110.8	110.0	111.6	112.4	112.8	111.06
108·2 107·7	107.4	109.6	110.4	110.5	108.8	110.9	111.5	113.2	110.5	110.8	118.2	111.28
108.8	108.6	108.8	109.4	109.4	107.5	108.0	109.3	109.3	110°0 110°2	111'0 111'2	115°8 112°6	$\begin{vmatrix} 110.17 \\ 111.42 \end{vmatrix}$ 110.96
109.0	$110.3 \\ 108.8$	110.3	111'6 111'4	110°5 115°6	110.3	109.7	110.2	110.4				112.50
_						115.4	113.2	111.6	110'5	112.4	122.8	114 20
108.52	108.94	110.00	110.70	111.30	110.89	111.32	113.10	112.61	114'03	114.81	114.72	111.15

^b Fifteen minutes late.

[°] Three minutes late.

^d Omitted in the Means, on account of disturbance.

	Angu	ılar Value o	f one Scale 1	Division of t	he Declinon		NATION. 21. Increa	sing Numbe	ers denote de	ecreasing W	esterly Decl	ination.	
Mean G Tir	öttingen ne.	0h.	1 ^h .	2 ^h .	3 ^h •	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8h.	9 ^h .	10 ^h .	11ħ.
	1 2 3 4 5 6	Sc. Div. 115 ° 6 118 ° 2 109 ° 3 111 ° 5 117 ° 8 117 ° 5	Sc. Div. 118'9 118'2 109'0 116'3 108'8 117'4	Sc. Div. 115°8 117°4 108°4 117°5 112°4 118°4	Sc. Div. 90'4 116'9 113'6 116'4 116'4 119'3	Sc. Div. 97 ' 4 113 ' 2 114 ' 4 112 ' 8 114 ' 1 114 ' 0	Sc. Div. 109 '3 111 '5 108 '2 109 '2 110 '4 108 '5	Sc. Div. 106'4 108'3 106'2 104'8 105'5 105'0	Sc. Div. 104 '9 107 '0 104 '4 103 '5 104 '4 104 '1	Sc. Div. 106°6 106°4 103°8 104°6 106°4 103°0	Sc. Div. 106 '7 107 '2 104 '6 105 '4 108 '4 104 '6	sc. Div. 102 '8 107 '6 106 '4 107 '0 108 '4 106 '5	Sc. Div. 93.6 108.4 108.2 108.8 108.4 108.2
ER.	7 8 9 10 11 12 13	118.0 115.2 111.6 113.7 111.7 114.4	109.0 114.2 112.2 115.4 117.4 112.2	110'4 113'6 122'4 119'6 121'4 121'8	111.6 113.0 118.5 121.1 122.8 121.9	103°4 114°9° 111°2 118°6 121°8 116°1	108.6 110.4 105.6 113.3 115.4 111.9	104.2 106.5 99.4 108.0 110.0 105.2	101.5 103.8 98.9 105.6 107.2 104.4	102.2 103.4 100.1 105.0 104.2 104.8	103.4 103.8 103.3 106.4 106.8 105.0	104.4 104.4 103.4 107.5 108.4 106.2	108.2 107.6 104.2 108.7 110.2 107.8
NOVEMBER.	15 16 17 18 19 20 °	112.5 108.6 112.8 114.3 114.8 117.4	114.2 116.2 115.2 115.5 115.4 84.8	116.6 116.4 116.4 115.2 117.6 105.0	116.4 120.0 113.3 111.4 113.2 122.8	115.4 110.8 112.2 113.8 114.8 118.0	110.4 111.4 109.6 109.4 109.0 111.4	107.5 106.2 107.4 106.5 105.8 104.4	105.4 97.8 103.0 106.6 105.2 103.6	104.4 100.0 106.6 107.4 106.4 103.4	105 · 4 104 · 3 107 · 4 108 · 4 104 · 4 105 · 4	107.7 102.4 107.4 107.2 120.4 106.4	110·3 100·9 109·2 107·4 98·4 107·4
	22 ° 23 24 25 ° 26 27 28	114.2 111.6 111.6 110.2 107.5 113.2	115.4 113.4 111.6 110.4 108.6 113.4	118·2 116·4 112·4 122·4 102·5 114·8	116.4 116.0 112.8 117.3 110.6 108.5	116.6 111.6 110.8 116.4 113.4 113.0	115.4 110.5 107.4 118.5 111.6 113.1	117'4 104'1 102'5 105'9 110'9 109'6	101.2 104.8 102.4 106.4 109.4 105.2	94.0 107.0 104.0 100.6 106.8 107.4	118.4 107.4 104.4 96.2 105.8 107.4	94.0 107.4 107.4 100.4 106.9 105.4	98.2 107.6 110.4 100.8 103.8 112.5
	29 30	113.4 113.5	114.3 114.3	115.4 115.2	116°1 115°4	116.2 112.4	113.0 114.4	108.8	114.3 107.4	105.0 107.0	106.4 107.4	108.4 107.8	109.9
Hourly	y Means	113.40	113.96	115.28	114.29	113.03	110.23	106.49	104.83	104.89	105.84	107.02	107.07
	$ \begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{pmatrix} $	115.0 114.6 108.4 114.8	115.5 113.0 108.2 112.5	115.4 114.4 114.9 109.7	115.6 113.6 117.4 102.5	116.6 114.2 107.0 109.8	115.6 111.3 106.6 107.4	112.5 111.9 107.6 107.3	116°2 107°4 105°4 105°4	116.9 107.0 105.8 106.4	108.6 105.2 106.3 107.0	110.4 105.2 106.7 107.4	109'8 111'4 107'8 109'0
	6 7 8 9 10 11 12	113.3 113.7 110.4 107.4 116.4 98.3	113·3 114·0 112·0 117·4 112·6 98·9	114.2 114.4 107.2 112.4 114.6 100.9	115.4 113.9 116.6 105.4 111.4 109.6	114.4 114.3 103.5 107.4 108.6 113.1	112.5 110.3 106.0 104.8 106.5 113.4	110°3 107°5 102°4 103°4 102°2 109°3	110.4 106.4 105.8 105.5 102.4 108.4	110.6 106.2 106.0 100.7 101.4 108.0	109.4 105.9 107.8 108.3 102.4 107.9	109'0 105'9 109'2 107'6 116'4 105'4	110°0 107°4 110°4 110°1 110°1
DECEMBER.	13 14 15 16 17 18°	112.5 106.6 112.5 112.8 115.4 104.5	113.5 110.2 114.3 113.4 114.4 112.4	114.6 103.4 115.4 118.3 98.4	113.6 117.4 118.2 117.2 130.4 116.9	112.6 119.4 116.4 118.7 139.4 104.5	110.8 116.5 d 116.6 117.0 104.6 108.4	109.0 110.4 110.2 112.6 119.6 109.6	105.0 106.2 107.6 109.4 106.0 108.2	105°2 106°0 106°6 108°9 89°5 101°6	106.6 106.2 107.4 107.4 97.8 111.4	109 2 108 8 108 0 106 5 109 4 108 4	109.8 109.8 110.0 110.2 102.5 111.0
I	19 20 ° 21 22 23 24 25 °	7.8 112.4 110.4 110.9 108.4	10·0 116·4 111·6 111·0 113·4	117.8 116.7 112.8 111.0 116.5	45.7 118.8 102.9 115.6 116.5	84.0 119.4 108.6 111.5 116.2	116.4 113.4 110.7 111.6 111.5	115.5 110.6 107.6 109.4 109.2	100°3 107°0 106°4 107°5 106°5	107.3 106.6 107.4 107.2 104.4	124.5 106.5 107.9 104.6 107.0	109'4 106'4 106'9 106'5 109'4	103.9 107.7 106.6 108.4 110.6
	26 27 28 29 30 31	113'4 112'4 111'8 112'5 113'3	115.4 113.5 115.4 113.0 113.3	118.6 114.8 115.5 113.8 114.6	118 · 2 116 · 2 119 · 5 116 · 2 117 · 2	117.2 117.6 118.5 116.9 117.6	111.6 113.4 109.9 114.5 114.5	108.4 110.4 107.3 111.4 113.0	106.4 106.4 109.3 110.4 111.2	107.5 108.0 99.9 107.3 110.4	109°2 108°0 105°8 106°9 110°2	109.6 107.5 105.9 106.3 108.2	110.5 108.8 107.6 107.2 108.8
Hourly	y Means	111.22	112.76	113.25	114.97	114.95	111:29	109.31	107.44	106.00	106.68	107.99	108.88

^a Thirteen minutes late.

b Two minutes late.

c Omitted in the Means, on account of disturbance.

	Angula	ar Value of	one Scale D	Divisio n of th	ne Declinomo	DECLINeter = 0' 72	ATION.	ing Numb er	s denote dec	reasing We	sterly Decli	nation.
12h.	13 ^h .	14 ^h .	15h.	16 ^h .	17h.	18ħ.	19 ^h .	20h.	21h.	22h.	23h.	Means.
Sc. Div. 107.6 109.6	Sc. Div. 103°4 109°4	Sc. Div. 117°1 109°8	Sc. Div. 115 4 109 5	sc. Div. 108 4 108 4	Sc. Div. 120.6 115.1	Sc. Div. 114'4 108'5	Sc. Div. 118'2 102'4	Sc. Div. 118'0 116'6	sc. Div. 115'8 112'4 117'2	Sc. Div. 114'6 117'8 112'4	Sc. Div. 112*8 109*6 112*4	Sc. Div. 109 78 111 23 109 65
108'3 110'0 110'4 109'2	108°5 110°4 111°2 110°4	110.8 110.2 111.3 110.6	114.5 109.9 110.7 110.2	114.4 110.4 111.5 111.2	111.2 119.2 111.3 114.4	112.0 114.0 116.9	98.4 111.4 112.4	114'8 110'6 118'2	111.3 120.8	113.4	112 4 114.0 121.4 	110.95 112.33 111.25
109°3 107°6	109.6 110.5	109·2 112·4	112.4 122.8	111.4 117.6	111.2 113.4	115.2 102.5 113.8	114.3 112.4° 111.4 109.7	111'4 112'0 112'6 111'0	110.3 110.4 113.4 114.3	115.6 111.0 115.4 112.4	117.8 5 111.3 112.6 111.8	108.66 111.42 110.48
112°4 109°4 109°6 110°6	111.0 109.8 111.0	112.8 114.6 116.4 112.8	119°4 113°4 111°6 113°3	115°9 113°4 117°4 112°5	120.6 118.8 113.4 112.4	107.4 112.4 112.2	109.2	109.4	109.4	111.5	110.0 108.7 	112.03 111.83 111.13
109.6 105.4	110.2 100.0	109.6 -	119.5 111.4	115.4 112.4	110·4 117·2	111.6 111.6	112.0 118.0 112.4 111.0	114.7 111.0 112.4 111.6	114.9 112.6 115.4 112.0	115.0 112.6 114.6 105.8	115.4 } 104.4 113.4 112.3	110.06 110.06
110.4 113.0 102.2 108.4	110°3 110°4 110°8 106°4	111°3 111°4 112°4 112°6	113.4 110.0 111.2 111.8	112.4 110.4 116.8 112.0	113.4 110.4 117.2 111.8	111.2 110.4 114.0	110.5	110.3	111.6 109.4	106.4	109.6 113.4	110 ·3 5 110·99 108 ·7 5
 104.4 109.2 114.2	124.0 110.2 112.4	109'0 110'4 113'4	123°2 109°2 113°4	123.0 108.4 144.2	115.0 108.4 118.4	107.4 119.4 108.6 109.2	106.4 103.0 108.0 100.2	106.4 102.6 107.4 107.7	110.9 104.0 109.4 112.4	111.6 109.8 111.4 110.7	114.4 } 109.8 111.1 110.8	111.11 109.26 111.03
112.6 116.0 114.4	113°3 116°6 112°0	99°4 111°6 112°2	182.6 106.0 111.6	119°3 115°2 112°6	125°0 111°6 113°4	121.3 111.4 — 114.2	122.6 110.4 — 112.6	121.4 109.2 — 111.4	113.3 113.3	113°2 104°4 — 112°5	$\begin{bmatrix} 110.2 \\ 111.4 \\ \\ 112.4 \end{bmatrix}$	115.18 109.41 111.20 >111.4
110°4 110°7	110°6 110°7	111.6 113.5	111.8	111.6	111.6 111.6	111.8 111.8	112.4 112.3	112.8 115.8	113.4	113.4	114.3	112.08
109.98	110.37	112.03	112.78	114.25	114.55	111.61	110.44	112.17	112.67	112.20	112.67	110.92
109°2 102°4 108°0 111°2	110°6 104°5 113°8 112°2	112.8 111.4 112.0 115.4	111°4 115°8 110°6 114°4	111.7 114.0 114.9 115.9	115°2 121°2 111°3 113°4	111.6 118.4 113.0	112°2 118°3 112°4	111.2 103.0 113.2	111°0 115°2 113°2	121.4 112.4 112.8	116.4 114.2 113.0 	113.45 111.67 110.43 110.97
110.6 109.4 111.9	110.6 108.5 109.4	111.4 106.2 108.5	111.6 107.4 114.9	112.8 109.6 112.1	113.0 111.4 112.2	109'4 113'0 107'4 113'0	115'4 112'3 112'0 114'5	116.5 112.0 119.0	113.8 112.5 114.8 114.6	113.4 113.0 119.2 111.0	112.8 121.4 112.6	112.02 110.94 110.37
110°0 109°4 112°4	111°4 114°2 113°4	111.6 108.4 112.2	112.4 113.8	111'4 122'2 113'2	111.3 124.6 112.4	111'4 128'0 — 110'4	112.4 119.4 — 109.3	111.6 111.8 96.6	113.5 112.4 — 111.4	114.8 107.5 — 112.0	111.8 101.6 	109°27 111°54 109°45
109.6 110.6 111.3 110.4 109.2	109.8 111.6 112.0 110.4 109.6	111°0 112°4 112°4 110°8 112°4	115.8 116.0 113.4 110.3 106.4	111.7 114.8 112.6 114.4 111.8	111.4 112.9 112.6 114.4 111.4	111.6 112.2 111.6 118.4 112.4	112.0 109.4 107.6 115.8 113.8	109'4 111'3 111'4 115'6 111'4	108'4 108'9 111'7 119'0 111'4	109'0 108'4 112'6 124'2 112'9	112.2 111.5 112.6 117.5 113.4	110.60 111.29 111.88 113.71 111.39
111.4 120.2 109.8 134.2 109.5	111.2 133.5 111.4 107.6	123.2 115.4 111.2 110.5	114.2 118.7 111.6 113.5	117'0 	121.9 112.4 111.3 114.4 113.4	106.0 114.8 114.6 121.6 112.6	143.0 122.4 108.6 105.6 114.7	123.0 113.4 109.6 116.4 116.4	120.0 114.0 110.8 111.0 113.4	81'8 114'4 113'5 115'4 116'2	155.8 113.4 107.8 110.4 115.4	100.51 102.30 111.40 111.43 111.45
109.8	109°9 112°4 —	112'5 114'5 —	113°4 114°4 —	112.5	112.2	113.4	115.3	112.4	112.2	112.2	$\left\{\begin{array}{c} 113.6 \\ - \end{array}\right\}$	111.80
111.0 109.4 108.4 108.0 109.7	110'9 110'9 111'5 112'4 110'7	111.0 112.2 122.4 110.2 111.3	113°4 112°8 111°0 112°4	112.6 112.4 112.4 112.5	114.2 111.5 113.6 114.4	113'4 110'6 112'4 112'2 110'4 110'4	112 3 111 5 112 4 110 5 111 8 112 3	112 4 112 0 112 4 112 2 113 4 112 4	112.6 111.6 113.6 111.5	112.9 112.8 111.6 114.0 112.4	112.4 113.3 112.0 112.3 112.4	112°13 111°71 111°56 111°74 111°95
110.64	110 7	111.87	111.8	113.19	110.4	113.33	112.35	111.40	112.29	113.29	112.94	111.42

	lar Value of											
Mean Göttingen } Time.	Oh.	1 ^h .	2h.	3h.	4 ^h .	5 ^h .	6 ^h .	7 ^h ·	8h.	9 ^h .	10 ^h .	11h
$\begin{pmatrix} 1\\2 \end{pmatrix}$	Sc. Div.	Sc. Div.	Sc. Div. 116.8	Sc. Div. 116°2	Sc. Div. 114°2	Sc. Div.	Sc. Div.	Sc. Div. 110°8	Sc. Div. 110°0	Sc. Div. 108.7	Sc. Div. 107°7	Sc. Di 108
3 4 5 6 7 8	112.8 108.3 113.9 114.1 113.4 113.4	112.6 106.8 114.5 115.0 110.4 115.8	116.2 111.6 116.9 116.4 106.6 119.2	119'4 114'5 118'6 120'0 114'4 120'0	119'4 107'4 118'6 120'2 112'0 117'2	116.5 107.5 114.9 116.4 110.2 113.3	113 · 2 112 · 4 110 · 9 110 · 3 109 · 0 107 · 4	111.3 110.6 109.2 109.0 107.8 105.9	106.9 107.7 108.6 108.8 107.4 104.4	99.4 106.4 108.4 109.2 106.7 114.0	97.4 109.7 107.6 109.2 108.4 106.4	105. 109. 110. 110. 111. 108.
10 11 12 13	113.6 112.9 116.4 111.7 113.4 113.4	110.9 116.0 108.4 109.8 112.5 114.2	116.5 118.8 124.4 101.9 117.4 111.2	128.8 121.6 125.0 105.4 120.4 112.0	116.4 116.6 113.2 113.2 116.4 112.2	112.1 112.4 113.4 115.4 118.7 111.8	109 ° 9 107 ° 5 89 ° 4 111 ° 6 105 ° 1 106 ° 7	107.4 104.2 106.5 105.4 100.9 106.6	104.9 100.6 112.4 99.6 97.0 106.0	105.4 104.1 96.6 107.7 95.0 107.6	107.9 107.0 109.2 100.2 102.0 108.8	110° 108° 100° 107° 108°
14 15 16 17 18 19 20 21 22 23	113.0 111.6 113.4 112.5 112.3 113.5	114.4 114.4 112.4 113.9 113.4	114.4 116.6 113.6 118.2 114.5 118.4	114.4 117.4 131.6 118.3 118.2 116.8	111'6 117'6 121'0 117'6 116'1 117'4	110.4 114.9 111.8 110.6 112.7 111.9	107.8 110.6 106.2 111.0 109.5 108.6	106.4 106.2 104.9 107.6 105.9 105.3	106.5 106.4 103.0 103.8 101.8 105.5	107.5 105.8 105.4 103.2 105.9 108.4	107·3 105·6 106·8 106·4 107·6 107·1	108° 108° 107° 108° 103° 106°
24 25 26 27 28 29	106.9 114.5 112.0 115.8 112.8 116.6	120.4 110.0 118.4 112.5 115.4 115.0	115°3 118°4 123°2 122°4 115°9 119°0	103.7 115.4 122.7 120.3 119.0 115.9	104'4 112'2 108'8 119'2 118'6 118'4	101'6 107'4 108'8 114'0 126'0 113'8	105.4 101.9 103.4 104.6 105.0 108.5	99.8 97.4 101.4 104.2 104.5 106.2	95.0 95.4 105.3 103.8 104.2 107.4	101.2 99.4 109.4 105.6 106.5 107.4	101.8 103.8 102.8 106.2 105.2 107.8	100° 104° 105° 106° 104°
$\begin{array}{c} 30 \\ 31 \end{array}$	110.2	111.2	115.7	117.2	117.2	114.8	110.8	108.5	107.9	107.0	105.6	105
Hourly Means	112.93	113.25	116.13	117.97	115.27	112.75	107.61	105.91	104.63	105.46	105.98	107
$\begin{pmatrix} 1\\2\\3\\4\\5 \end{pmatrix}$	117.5 122.6 115.9 118.4 117.6	118·1 111·6 120·6 117·2 118·6	120°1 119°5 121°4 120°3 123°2	124°2 122°6 123°4 124°4 126°0	121.7 122.5 122.8 122.6 120.8	122°3 120°9 119°6 118°4° 118°6	118°4 118°2 116°4 115°4 116°4	115.5 113.4 114.5 113.8 115.1	113.7 111.6 113.3 111.2 114.3	112.2 112.3 112.6 110.6 114.1	111.5 113.3 112.4 110.4 114.2	114° 114° 113° 112° 115°
6 7 8 9 10 11 12 12	120°8 118°6 124°2 117°6 118°5 118°8	121.4 118.7 121.0 120.0 115.7 119.0	123°0 123°8 124°2 124°7 122°8 116°2	126.6 122.0 133.0 126.2 128.2 117.2	122 · 2 122 · 3 123 · 8 127 · 4 127 · 2 120 · 2	118°2 118°0 116°6 122°4 122°0 121°4	114.4 106.4 115.4 117.6 116.4 119.7	113.9 107.2 108.8 115.8 111.4 117.4	109.5 109.3 107.4 111.4 109.3 114.4	106.4 110.0 108.5 110.2 109.4 112.4	109.6 112.9 104.4 111.8 109.3 113.1	105 110 110 109 110 112
FEBRUARY 13 14 15 16 17 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19	118'4 121'4 119'4 119'3 120'2 124'4	119.0 119.2 120.4 121.5 122.4 124.0	121.5 110.4 123.0 127.0 125.6 124.6	123.7 118.4 124.8 125.4 126.4 127.4	124.6 120.0 122.6 123.6 124.7 117.4	124.3 118.0 117.4 118.6 118.6 111.5	119.2 110.0 113.3 114.6 113.4 106.0	116.6 107.5 112.4 112.5 109.8 101.6	115.0 107.7 112.4 111.7 108.5 107.4	111.6 110.6 113.2 112.4 110.3 110.4	106.0 113.5 112.4 113.3 112.6 112.2	93° 110° 112° 113° 114° 112°
20 21 b 22 b 23 24 25 26	110.4 121.4 122.4 104.2 119.6 118.5	98.0 128.3 119.4 109.5 104.3 119.0	131.8 125.4 123.6 105.8 106.4 122.3	131.0 126.4 124.2 119.5 116.7 125.4	125 · 4 123 · 6 121 · 6 110 · 7 125 · 6 126 · 4	120.0 120.6 118.8 114.3 124.4 121.8	119.8 116.2 122.5 113.0 115.7 120.0	116.6 108.8 121.4 114.7 115.2 115.4	109.8 101.6 112.0 109.5 114.0 114.0	100.0 89.0 108.3 111.4 114.2 111.2	127.5 103.8 107.2 125.4 112.4 112.3	141. 105. 109. 113. 117. 112.
27 28 29	115.6 119.2	113'4 121'4	124.4 122.6	129°3 123°4	120°6 125°8	122.5 121.4	115.2 117.2	110.4 113.4	103.6 111.4	106·4 111·1	110.8	111° 112°

^{*} Three minutes late.

b Omitted in the Means, on account of disturbance.

[•] Five minutes late.

	Angula	ır Value of o	one Scale D	ivision of th	e Declinome	$DECLIN$ $eter = 0' \cdot 72$		ng Numbers	denote dec	reasing Wes	terly Declin	ation.
12h.	13h.	14h.	15 ^h .	16 ^h .	17h.	18h.	19 ^h •	20h.	21h.	22h.	23h.	Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
108.4	109.4	111.4	112.6	110.8	112.8	112.6	112.3	112.4	111.4	111.4	112.8	111.63
107.8	107.0	115.4	118.7	118.4	119.4	122.6	113.4	113.2	128.4	124.5	112.2	113.82
110.6	111.2	112.3	112.4	113.4	113.4	111.5	112.4	111.8	109.4	112.3	113.0	110.57
110.8	111.4	111.8	113.5	112.0	111.8	110.7	112.9	111.9	111.9	109.5	113'4	112.24
111.6	111.7	111.7	112.4	112.0	113.2	112.8	113.7	114.0	116.7	111'4	113.4	113.10
111.5	111.2	112.0	115.4	117.0	112.2	110.6	113.2	112.8	113.2	112.2	111.8	$ 111.29 \rangle 111.5$
108.8	111.2	111.4	111.4	110.8	110.4	_					111.4}	111.33
				_	_	112.2	112.4	111.5	114.6	110.5		
110.6	109.6	114'4	111'2	112.4	112.6	112.8	113.7	113'4	113.4	114.2	114.0	112:35
109.6	120.0	126.4	120.4	118.2	108.4	113.2	115.0	114'5	117.5	124'0	118.4	113.87
113.2	110.0	110'4	108.0	108.8	110.8	111.0	111.6	111.6	113.4	104.9	108.8	109.92
108.2	106.8	109.0	114.3	112.4	109.9	108.6	109.7	108.2	110.5	108.2	109.2	108.21
109.3	117.6	111'4	111'4	109.9	109.2	108.9	109.2	109.2	110.4	109.6	112.2	109.82
108.4	108.4	109.3	109.4	109.4	110.5		<u> </u>			110.4	111.0}	110.54
						110.6	113.5	113.0	110.5	110 4	111.4	110.66
108.6	107.4	110.6	110.6	110.8	115.4	111.6	112.2	111.2	111°5 112°4	113.6	1112.3	111.40
107:5	109.2	111.4	112.4	113.0	110.9	111.3 111.0	111 · 9	112 ' 3 104 ' 4	107.6	117.4	112.2	111.22
107.6	109.7	114.0	116.1	113.3	113.4		112.4	110.0	112.2	112.5	113.4	111.26
109.5	110.9	111.6	110.4	111.7	112.4	113 · 2 110 · 4	111.5	110.0	111.2	111.6	111.4	110.30
109.4 110.2	108.7	109.9	110.8	110'8 115'2	110°6 111°7	110 4	111 2	110 3		_		}111 1
110 2	107.6	111.4	109.6	110 2	111 /	112.7	112.8	111.4	116.8	115.0	$\begin{bmatrix} -123.6 \end{bmatrix}$	112.11
103.0	108.7	110.3	110.8	111.0	112.8	109.4	110.4	111.4	111.4	112.8	112.6	107.50
105.0	110.2	111.5	111.0	112.6	111.6	111.0	111.4	114.5	114.4	113.4	111'8	109.10
106.6	106.6	112.4	107.2	111.2	115.4	108.6	109.4	108.4	114.4	114.2	113.9	110.44
108.3	108.2	110.3	110.4	111.4	115.4	124.0	119.2	117.4	123.4	125.5	110.1	113.31
110.4	119'4	136.2	121.4	120.3	118.8	129.6	108.9	110.5	106.2	130.0	128.4	115.73)
108.8	108.7	109.5	109.2	110.0	110.5						109.4	111.39
			_		_	115.4	113.1	109.2	111'6	113.6		l .
107.0	108.0	108.8	109.2	109.6	110.4	110.2	110.4	110.2	110.5	111.3	112.4	110.47
108.86	110.40	112.87	112.33	112.21	112.41	112.95	112.17	111.23	113.27	114.07	113.27	111.32
114.6	115.3	116.5	116.4	122.6	116.0	120.5	116.4	116.6	118.8	110.8	116.2	117.08
115.4	115.6	116.4	116.4	117.6	118.8	116.4	116.1	116.8	117.8	117.4	117.0	116.86
115.2	115.6	116.8	120.6	124.4	120.5	120.3	120.4	119.0	119.0	119.4	117.6	118 13
113.3	112.3	116.2	116.0	118.3	117.8	117.0	116.6	117.4	116.6	117.1	117.6	116.43
117.0	117.4	116.8	119.8	116.6	116.2	_	_	_	l —	_	}	120.08
	_		_	_		140.0	134.4	119.6	130.6	116.4	122.6}	1
108.9	107.6	111.4	117.2	122.3	121.4	117.5	118.8	115.6	116.4	117.0	117.4	115.96
111.2	112.4	108.4	123.8	124.4	130.5	129.4	124.7	112.2	115.7	109.3	112.2	116.42
110.5	111.4	122'4	113.3	123.5	118.4	117.9	117.8	116'4	116.6	116.5	116.0	117.14
111.4	114.4	116.6	116.4	117.9	118.6	118.0	116.3	116.6	116'4	116.9 118.4	117.4	116.85
112.0	112.8	115.6	116.2	117.4	117.8	118.4	119.4	117.7	119.5			! 5
113.3	114.4	115'4	116.2	120.6	116.3	10040		117:0	110.4	117.6	117.6}	117.05
107.4	110:0			115.0	101:0	120.6	118.2	117.8	118 .4 121 . 2	113.4	116.0	116.48
112.4	112.5	115.8	115.2	115.0	121.6	121.6	122'1	120.7 120.0	118.8	122.4	121.4	115.57
114.7	113.0	114.4	115.2	116.3	118.0	117.5	117.2	120.0	118.4	119.6	121.4	117.29
114.4	116.3	115.7	117.0	117°2 116°6	119'8 116'7	117.8 115.4	113'4 116'3	117.0	117.6	118.4	119.0	117.20
115.0	115.4	116.5	116.4	116.6	116.2	117.3	123.6	119.6	119.0	120.6	118.8	117.52 >117.
114.3	114.4	115.6 114.4	116 .4 112.1	110 2	120.2			_		-		115.50
_	111 1	114 4	112 1	112 4		118.4	124.2	91.2	121.2	123.9	$\frac{118\cdot 2}{118\cdot 2}$	1
117.8	106.8	116.4	293.5	128.9	128.2	119.2	120.0	118.0	118'8	116.4	121.0	126.56
107:3	123.4	116.8	118'4	117.8	128.4	120.4	83.4	97.6	104.6	102.6	107.4	112.46
110.5	114.8	116.2	126.6	127.4	141.8	128'4	142.0	126.0	114.4	124.0	104.2	120.31
112.4	110.9	116.4	117.7	110.4	116.1	143.0	121.5	112.4	122.8	98.4	130.2	115.14
121.0	112.4	115.4	120.8	119.8	116.2	115'6	116.4	115.8	116.8	116.8	117.4	116.527
113.8	114.8	116.5	136.5	118.4	118.4			_				117.94
112:4	_		_			116.8	117.0	113'4	113.0	113.8	120.0}	115.74
113.4	115.2	116.3	116.8	117.0	116.6	118.3	116.6	113.6	118.3	111'4	120.0	118.07
112.5	115.4	114.8	111.5	134.5	130.4	117.6	117.1	117.4	113.6	$\frac{116.44}{116.44}$	118.10	117.01
113.23									118.29			

1 Sc. 1 119 2 119 3 118 4 118 5 6 122 7 122 8 125 9 120 10 121 11 121 12 13 122 14 122 15 123 16 131 17 112 18 120 19 20 20 20 20 20 20 20 2	9.7 121. 8.4 121. 8.3 120.	Div. Sc. Div. '4 124'4 '8 124'4 '8 124'4 '8 126'2	125.8 126.5 125.0 126.5 123.8 128.2 132.4 126.6 129.2 128.4 127.4 116.4 127.4 116.4 122.7 101.3 129.0 125.6 123.6 123.4 123.4 123.4 123.4 123.4 126.4 125.3 119.4	4h.	5h. Sc. Div. 119 '7 123 '4 118 '6 115 '4	Sc. Div. 114'5 118'5 111'4 109'6	Sc. Div. 115 '4 113 '4 113 '4 113 '4 108 '6 107 '4 109 '4 109 '4 115 '2 112 '1 109 '4 106 '6 107 '2 111 '8 114 '5 111 '0 107 '8 109 '5 104 '6 106 '4 105 '5 112 '4 105 '6 107 '2 104 '3 109 '0 103 '4	8h. Sc. Div. 112'4 112'2 108'4 107'6 104'4 108'9 102'6 104'3 109'0 109'4 107'9 106'2 110'2 108'2 125'2 108'4 136'6 107'6 103'8 103'6 101'8 112'4 107'5 108'0 104'2 106'5 105'6	9h. Sc. Div. 112'4 111'8 110'2 109'6	10h. Sc. Div. 114'3 112'4 112'6 110'8	Sc. Div 113.0 113.5 114.2 113.1 109.6 115.5 112.4 111.6 111.7 110.4 110.4 110.4 110.4 110.4 110.4 110.4 110.4 110.4 110.4 110.5 110.4 110.5 110.4 110.5 110.4 110.5 110.4 110.5 110.4 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 11
1 119 2 119 3 118 4 118 5 - 6 122 7 120 8 125 9 120 10 121 11 121 12 123 14 122 15 123 16 131 17 112 18 120 20 126 22 120 23 119 24 118 25 121 28 120 30 116 31 113	9.6 121. 9.7 121. 8.4 121. 8.3 120. 2.5 124. 2.4 126. 5.9 125. 1.3 124. 2.4 125. 2.0 119. 3.2 121. 2.1 6 130. 2.0 107. 0.4 120. 9.7 106. 6.4 126. 0.6 122. 8.4 114. 4.5 129. 2.1 0 126. 2.0 4 122. 3.3 6 114. 2.0 0 121.	'4 124'4 '8 124'4 '8 126'2 '6 126'6 '2 128'4 '9 129'6 '4 127'4 '0 128'3 '4 127'0	125.8 126.5 125.0 126.5 123.8 128.2 132.4 126.6 129.2 128.4 127.4 116.4 127.4 116.4 122.7 101.3 129.0 125.6 123.6 123.4 123.4 123.4 123.4 123.4 124.9	120.7 125.4 121.3 122.4 119.6 121.4 122.6 121.7 127.4 125.8 	119.7 123.4 118.6 115.4 112.4 116.3 114.6 122.4 120.6 118.4 112.6 115.2 108.6 115.2 108.6 115.4 117.0 115.5 108.4 117.6 117.6	114.5 118.5 111.4 109.6	115 '4 113 '4 118 '6 107 '4	112'4 112'2 108'4 107'6 104'4 108'9 102'6 104'3 109'0 109'4 107'9 106'2 110'2 108'2 125'2 108'4 136'6 107'6 103'8 103'6 101'8 112'4 107'5 108'0 104'2 106'5	112.4 111.8 110.2 109.6	112.4 112.6 110.8	113.0 113.5 114.2 113.1 109.7 115.5 112.4 111.6 111.7 110.5 115.2 114.4 118.0 110.4 109.4 109.4 109.4 109.4 109.4 111.2 112.4 113.5 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 110.6 11
6 122 7 122 8 125 9 120 10 121 11 121 12 -1 13 122 14 122 15 123 16 131 17 112 18 120 19 -2 20 109 21 126 22 120 23 119 24 118 25 114 26 -2 27 121 28 120 30 31 31 113	2 · 4 126 · 5 · 9 125 · 0 · 4 124 · 1 · 6 125 · 1 · 3 124 · 1 · 6 125 · 1 · 3 · 2 121 · 1 · 6 120 · 1 · 1 · 1 · 1 · 1 · 1 · 1 · 1 · 1 ·	128.4 129.6 14 127.4 10 128.3 127.0 14 126.8 122.4 133.6 16 119.2 121.8 123.0 14 123.6 123.3 124.3 126.4 123.6 123.3 126.4 123.6 123.3 126.4 123.6 123.3	128.2 132.4 126.6 129.2 128.4 	121.4 122.6 121.7 127.4 125.8 122.6 117.8 99.4 121.6 118.2 118.4 	116·3 116·3 114·6 122·4 120·6	108.4 102.2 107.6 116.6 114.4 	109'4 103'6 104'4 115'2 112'1	104'4 108'9 102'6 104'3 109'0 109'4 107'9 106'2 110'2 108'2 125'2 108'4 136'6 107'6 103'8 103'6 101'8 112'4 107'5 108'0 104'2 106'5	110.9 103.4 104.6 108.4 108.4 107.9 106.4 114.5 112.2 117.4 109.5 120.0 108.4 104.2 104.6 102.5 113.6 108.4 108.4 108.4 107.8 106.2	114'0 103'5 108'6 110'2 110'2 109'4 109'1 114'5 112'6 114'7 108'4 117'6 110'0 107'8 108'6 107'8 112'6 111'5 110'8 110'2 107'4	113 2 109 3 115 4 111 6 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4 110 4
13 122 14 122 15 123 16 131 17 112 18 120 19 - 20 109 21 126 22 120 23 119 24 118 25 114 26 - 27 121 28 120 29 120 30 116 31 113	2:0	122.4 113.5 18 132.6 119.2 121.8 121.8 14 114.5 123.0 123.4 125.5 120.0 123.3 123.3 123.3 123.3 124 126.4 126.4 126.4 126.4 126.4 126.0 122.5	124.9 107.4 127.4 116.4 122.7 101.3 129.0 125.6 123.6 123.4 122.3 123.4 126.4 125.3 119.4	117.8 99.4 121.6 118.2 118.4 	115.4 112.6 115.2 108.6 113.6 	109.6 105.7 113.4 110.2 110.9 	106'6 107'2 111'8 114'5 111'0 107'8 109'5 104'6 106'4 105'5 112'4 105'6 107'2 104'3 109'0	106·2 110·2 108·2 125·2 108·4 136·6 107·6 103·8 103·6 101·8 112·4 107·5 108·0 104·2 106·5	106·4 114·5 112·2 117·4 109·5 — 120·0 108·4 104·2 104·6 102·5 113·6 — 108·4 108·4 107·8 106·2	109°1 114°5 112°6 114°7 108°4 — 117°6 110°0 107°8 108°6 107°8 112°6 — 111°5 110°8 110°2 107°4	110°6 115°2 114°6 110°6 114°8 112°6 100°6 100°6 111°2 111°2 112°6 113°6 110°6
20	6 · 4 126 · 0 · 6 122 · 9 · 4 122 · 8 · 4 114 · 4 · 5 129 ·	123.0 123.4 125.5 120.0 123.3 123.3 126.4 126.4 126.4 126.6 129 122.5	129.0 125.6 123.6 123.4 123.4 122.3 123.4 126.4 125.3 119.4	126.6 122.2 121.5 122.5 99.6 	115.6 115.4 117.0 115.5 108.4 	111.6 110.2 112.4 111.0 117.6 	109.5 104.6 106.4 105.5 112.4 	107.6 103.8 103.6 101.8 112.4 — 107.5 108.0 104.2 106.5	108.4 104.2 104.6 102.5 113.6 	110.0 107.8 108.6 107.8 112.6 — 111.5 110.8 110.2 107.4	112.4 109.6 110.4 109.4 107.2 111.2 112.4 113.8 106.6
27 121 28 120 29 120 30 116 31 113	20°4 122° 20°4 122° 3°6°4 125° 3°6 114° 20°09 121°	123.6 126.4 126.0 122.5	123.4 126.4 125.3 119.4	120.6 121.4 122.5 121.4	118'4 112'4 117'6 117'6	108.5 106.4 111.7	107°2 104°3 1 0 9°0	108.0 104.2 106.5	108.4 107.8 106.2	110°8 110°2 107°4	112° 113° 106°
eans 120		124.3	5 123.77	119.58							
li	22.4 121.	1		1 2 2 2	115.60	110.22	108.60	109.00	109:17	110.66	111
$\begin{array}{c c} 1 & 122 \\ 2 & - \end{array}$	_	3 124.2	127.2	121.6	115.8	111.6	108.6	107.8	109.4	113.3	112
3 103 4 122 5 129 6 121 7 129 8 115	03'4 108' 22'8 127' 29'0 118' 21'4 128' 29'0 118' 15'6 122'	7 2 128 0 3 0 110 4 3 7 132 1 3 0 110 4 2 4 124 6	120°2 129°2 98°0 127°4 98°0 123°2	116.6 129.0 118.6 124.4 118.6 119.5	115.8 112.8 117.6 119.0 117.6 116.6	114·2 105·8 114·2 113·5 114·2 112·6	111.6 103.4 109.5 106.7 109.5 109.6	104.4 107.4 113.4 105.4 113.4 109.4	108.6 106.6 113.4 107.6 113.4 110.4	123°3 108°3 122°2 110°6 122°2 112°6	115': 114': 116'- 116'- 116'- 113':
11 120 12 119 13 120 14 123 15 124	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0°4 120°6 0°3 123°5 2°4 123°0 5°0 125°0	122.4 120.5 121.3 122.6 123.4 119.4	118.6 116.6 117.8 118.1 119.4 115.8	113.4 111.8 114.0 113.6 113.2 112.4	110.4 109.4 112.6 108.6 109.6 110.2	107.0 106.4 111.6 105.6 107.4 105.4	106.4 108.4 111.3 106.0 107.2 105.3	108.4 109.7 112.6 108.9 109.2 103.6	111'4 113'0 113'0 111'6 112'4 102'6	113°4 115°6 113°6 113°6 114°6 107°8
17 18 19 119	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{bmatrix} 1.4 & 122.4 \\ 2.5 & 122.7 \end{bmatrix}$	119°2 120°4	121.2 115.4 117.4 120.4	112.4 110.4 113.6 117.2	108.3 108.8 110.7 113.9	108°2 106°8 107°7 109°6	108.4 104.4 107.6 107.2	104'3 105'4 108'4 108'3	106.0 108.7 111.2 109.4	104: 113: 113: 112:
22 120 23 - 24 120 25 121 26 122	20°5 121°21°0 124°22°4 125°20°4 123°24°7 124°	-	119.4 122.6 122.8 122.4 123.4 121.2 124.2	113.4 	115.4 112.2 114.4 110.8 112.5 111.3 101.9	108.5 109.2 111.5 109.2 110.3 108.0 98.2	105.7 	106.6 108.6 107.4 110.3 110.4 107.0 106.2	107.4 110.4 108.5 111.3 111.7 109.0 108.4	110°8	114.3 114.4 113.4 115.0 113.2 106.4
13 14 15 16 17 18 19 20 21 22 23 24 25 26	19 19 19 19 19 19 19 19 19 19 19 19 19 1	120.0 122 123.4 123 124.2 123 122.4 123 120.3 121 119.2 122 121.4 123 120.6 127 120.5 121 121.0 124 122.4 123 120.4 123 120.4 123 124.7 124	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

	Angulai	r Value of o	ne Scale Di	ivision of th	e Declinome	DECLIN		ing Number	s denote dec	ereasing We	sterly Decli	nation.
12h.	13h.	14h.	15h.	16 ^h .	17h.	18h.	19 ^h .	20h.	21h.	22h.	23h.	Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
119.4	115.4	115.6	134'4	120.4	116.4	118.4	115'4 117'4	117 . 8	118'6 118'6	117.9	119 .4 116.0	118.47 117.60
114.6 115.2	115°4 115°6	115 ' 9 116'4	116 · 2	116.2 117.4	117.6 117.3	116.6 116.7	117.0	116.4	116.5	117.0	118.6	116.23
115.4	116.3	117.2	118.4	118.0	117.4					_		l i ••⊢••.
	_		_			117'4	116.6	116.4	119.6	117.6	120.5	110 09
110.0	111.4	111.6	117.4	115.8	117.4	120.4	121.2	121.5	119.4	121'4	1130 1	115.85
114.2	114.8	115.8	115.8	117.4	117.4	117°4	121'4	120.8	120°4 118°6	122°2 118°7	121°2 117°8	116.72
113.5 112.8	114°2 112°4	113°2 115°4	115°2 116°7	121.8 118.2	127.6 117.4	120°4 117°5	122.4 117.7	120'4 118'3	118.4	119.0	119.4	115.98
113.4	114.4	115.2	116.4	116.9	120.0	119.4	117.6	118.4	119.4	118.4	119.3	118.12
112.0	114.2	115.4	115.8	117.2	117.4						- 3	117.77
						117.4	119.3	119.4	120.4	122'2	121.8 }	1
112.8	115'6	116'3	118.4	118.2	119'4	120.4	120'4	120.0	120.2	120'6 122'4	119'4 125'4	117.65
113.2	114°2 116°2	116°2 117°2	118.4	120°2 116°7	120°4 118°0	124.6 130.3	130'8 128'2	122.6 127.0	124.7 128.0	121.8	118.4	116.63
115.2 114.9	115.4	117.2	117°4 114°0	114.1	133.6	115.8	116.6	144.9	135.6	137.3	124.4	121.43
117.4	111.4	112.6	114.4	115.6	115.0	115.4	115.4	117.2	118'4	118.6	119.4	115.23 (119.84
110.4	111.4	111.6	114.2	113.9	115.2						115.4	115.40
						118.0	105.4	125.4	134.4	118.2	121.2	114.65
120.0	114.4	107.2	111.8	109.4	124.4	126.2	113.2	118.6	116 '7 117 '0	124·4 118·4	118.0	116.24
116 . 2	113.5 109.3	114 . 2	115 ·2 11 5· 5	115°5 116°4	115'7 114'4	115'4 116'9	115.0 117.6	116'8 116'6	115.8	117.2	117.4	114.64
113.4	113.0	114.8	124.4	117.2	118.0	118.2	120.0	118.4	128.5	127.8	112.8	116.75
111.5	112.6	114.3	119.4	121.7	145.4	128.0	124'4	126'4	124.6	12 0°5	117.2	117.42
105.6	111'5	113.0	113.8	115.2	119'2						}	114.88
						125.3	121.6	123.6	107.7	114'4 122'0	112.0}	116.26
117.4	110'4	112.6	112.9	114.7 120.9	131.9	117.6	115'4 117'3	115.0	126 ·2 119 · 4	117.0	118.6	116.39
113.4 114.0	114.4 114.4	115°0 114°4	122 . 8 11 7. 6	115.5	117°8 115°6	117.0 117.6	117.4	116.4	119.4	119.4	112.2	115.40
111.6	108.5	109.6	117.9	121.5	116.6	124.4	123.2	124.8	122.0	119.3	116.2	116.20
113.7	111.6	110.7	143.2	126.6	117.4	123.2	130.2	119.8	109.7	122.6	115.0	116.67
113.74	113.39	114.16	118:37	117:50	120.14	119.87	119.22	120.59	120.63	120.63	118.38	116.4
110.4	10440	11010	100.5	11015	10415							
113.4	124.2	118.8	132.7	116.2	124.7	128.0	120.5	112.3	112.0	123.5	113.6	118.16
109.3	107.0	117:0	129.0	126.0	110.0	126.2	115.0	116.6	119.2	115.2	117.8	114.96
112.8	113.0	113.4	113'3	119.4	115.4	118.4	118.5	116.2	115.2	119.0	119.2	116.20
112.8	117.4		115.4	115.8	137.4	135.0	122.4	115.4	115.8	110.0		116.80
117.3 112.8	116.2	122.8	134.6	141.4	108.5	118.4	102.8	110.4	115.8	156.0 110.0	133.0 105.6	116.80
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113.0	114.0	114.2	114.6	114'7	116.5	106.0	117.6	118.4	119.4	120.0	118.8	115.27
115.4	115'4	115.4	115.2	115.2	116.4	116.7	117.8	119.4	120'1	119.0	119.2	115.75
113.7 114.4	114.3	115.0	115.4	115.6	116.4	117.2	117.6	118.7 117.0	119'4 119'8	119.0	118'8 121'4	115.68
114.4	114.4 114.2	114.2 114.2	114.6 114.3	117.7 115.5	116 ' 3	116'7 116'0	116 '9 118 ' 4	118.0	118.6	119.1	121.2	116.28
110.0	125.6	116.0	109.4	108.0	115.6	-					119.8}	114.34 >116.31
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105.4	112.4	142.2	113.6	116.6	118.8	116.4	122.5	118.2	118.4	118.5	118 .8	116.23 112.12
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	122.8	121.2	119.4	120.4	116.8	116.7	116.4	117.5	117.2	117.4	118.0	116.28
		119.2	116.4	116.0	116.4	117.0	116.5	118.0	118.0	118.0	119.4	116.37
115·4 115·4	116.9				116.6	117.2	118.0	118'4	118.6	117.6	119.5	116.33
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	Ang	ılar Value o	f one Scale l	Division of t	ha Daelinom		NATION.	sing Numbe	rs denote de	ereasing W	esterly Decl	ination.	
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	8 9 10 11 12 13 14	114.4 123.4 109.3 123.4 126.5 123.8	116.4 125.0 115.9 126.5 125.4 127.7	111.3 122.4 111.6 122.0 126.0 128.0	108.2 116.9 110.4 124.6 121.5 123.8	106.6 112.0 115.6 117.2 112.4 116.0	108 · 2 113 · 4 123 · 4 113 · 8 107 · 0 107 · 4	108.8 113.4 102.4 110.3 105.4 104.0	107.7 110.4 104.6 109.2 103.4 104.3	108.4 108.8 102.4 109.0 104.8 104.0	116.0 105.2 107.6 109.4 107.4 108.9	112.4 105.3 107.8 111.5 110.4 113.1	109.6 108.8 114.5 113.4 112.7 115.9
MAY.	15 16 17 18 19 20	124.4 124.4 125.4 121.0 123.2 112.8	128 · 4 126 · 2 133 · 4 135 · 0 123 · 4 115 · 6	127.2 126.9 130.6 137.0 126.4 121.4	123·3 123·4 130·8 132·9 124·5 120·2	117.4 117.4 116.4 127.4 119.4 119.7	112·3 106·4 112·6 120·6 119·2 114·4	109°3 103°4 104°6 125°4 110°0 110°0	107.2 101.8 93.4 84.4 101.7 110.4	105 ' 4 105 ' 4 95 ' 2 94 ' 2 103 ' 0 110 ' 4	108.6 107.0 99.4 114.4 105.6 109.5	112.9 110.0 105.6 114.4 107.4 110.2	115.4 115.6 109.4 117.4 111.0 111.6
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	29 30 31	123 ° 4 124 ° 0 125 ° 4	123 · 9 124 · 4 129 · 3	124°0 124°4 127°5	121.8 124.4 132.4	117.6 119.4 120.8	113°2 113°6 108°8	108.4 107.2 108.4	108°3 103°8 105°4	110'4 104'8 101'6	111.7 107.6 104.4	113.7 109.0 106.4	114°2 110°4
Hourly	y Means	122.99	125.41	124.27	122.24	117:10	112.68	108.51	104.24	104.66	107.23	109.71	113.4
	$\left(\begin{array}{c}1\\2\\3\end{array}\right)$	124·4 124·3 126·2	126.6 125.4 129.0	123°2 125°5 129°6	121 · 4 122 · 5 126 · 0	116.5 118.4 121.0	109.7 112.4 114.4	107.6 106.6 106.2	110°0 104°4 102°9	107.5 103.6 101.5	107.8 106.6 103.5	110°4 109°2 108°8	113.0 112.4 111.2
	4 5 6 7 8 9	120°2 117°2 124°4 124°5 123°7 126°0	126.6 122.6 124.4 125.7 124.2 125.6	122°0 126°6 125°2 125°7 124°8 124°4	123°3 124°4 124°2 124°4 123°4 122°4	121 '4 121 '4 119 '2 116 '2 118 '6 116 '4	112·5 114·4 115·3 109·4 112·6 113·6	105.6 107.8 110.4 104.3 109.4 109.2	102.7 105.5 109.0 105.0 109.4 106.4	100°2 104°7 106°4 103°4 110°7 109°2	105.5 107.2 106.6 104.4 110.7 108.6	110°2 110°2 110°3 107°8 112°4 108°4	119.2 114.2 113.6 110.6 112.4 112.4
JUNE.	11 12 13 14 15 16 17	123.0 126.4 129.4 123.6 124.8 121.8	125 '4 127 '2 126 '8 124 '0 127 '3 125 '4	125 · 4 127 · 4 128 · 4 122 · 6 125 · 3 125 · 4	122°2 126°5 128°4 121°8 122°2 121°6	118.6 122.2 120.0 112.5 115.8 117.8	112.4 115.1 113.4 107.4 110.5 111.7	106°0 113°2 106°0 107°0 110°4 108°4	107.2 107.4 104.8 108.2 107.2 107.4	107.6 108.2 103.4 111.4 106.4	110.5 109.6 109.0 111.5 109.2 108.3	114.6 111.8 112.0 112.5 112.4 111.7	116.7 114.0 117.9 116.4 115.3 114.4
	18 19 20 21 22 23 24	124 · 4 115 · 5 124 · 8 117 · 4 121 · 2 122 · 4	127'4 120'2 127'5 126'1 123'4 121'9	126.5 126.9 120.2 126.4 124.4 123.4	121 '4 124 '0 121 '3 125 '0 123 '6 123 '6	119'4 121'4 118'5 123'0 118'8 120'4	113 · 4 118 · 4 108 · 4 112 · 6 112 · 0 115 · 6	109.4 110.8 107.8 114.9 107.1 111.3	106.4 108.0 107.4 106.2 107.2 112.0	105 '4 108 '4 106 '5 106 '4 109 '7 102 '4	103.4 106.0 109.7 111.5 113.4 107.3	103.8 109.6 110.2 118.9 113.0 111.4	109.4 112.8 109.2 117.4 114.8 115.0
	25 26 27 28 29 30	124·5 125·4 124·6 125·2 127·4	125 ° 6 127 ° 4 126 ° 6 126 ° 2 130 ° 8	124 · 4 129 · 4 126 · 6 126 · 8 129 · 0	121 · 4 127 · 6 124 · 8 126 · 2 125 · 4	118.7 118.1 117.0 123.0 117.7	114.6 111.3 109.2 115.4 112.6	110°8 108°4 104°2 107°8 110°3	105.6 104.6 104.4 105.4 107.4	103.8 103.4 103.4 100.8 107.4	105.6 104.6 105.8 101.4 109.4	110·9 109·0 110·2 106·4 111·5	115.5 113.2 114.2 111.7 113.5
Hourly	y Means	123.57	125.74	125.60	123.81	118.92	112.63	108.20	106.62	105.70	107.68	110.68	113.8

	12h.	13h.	14 ^h .	15h.	16 ^h .	17 ^h .	18 ^h .	19 ^b .	20 ^h •	21h.	22h.	23h.	Means.
14	12".	10.	11.	10.	10.		10.	13.	20 .	21.		20.	Means.
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	$\left(\begin{array}{c} 1\\2\\3 \end{array} \right)$	Sc. Div. 629 2 617 0 614 8	Sc. Div. 624°0 618°0 616°0	Sc. Div. 622 * 5 614 * 0 614 * 2	Sc. Div. 620 ° 0 613 ° 2 608 ° 8	Sc. Div. 619 0 609 3 611 4	Sc. Div. 612 4 602 6 606 2	Sc. Div. 614.6 604.6 603.2	Sc. Div. 612.7 608.7 604.0	Sc. Div. 614.4 612.6 607.3	Sc. Div. 620°2 615°0 613°2	Sc. Div. 619*4 613*4 625*4	Sc. D 621 612 614
	5 6 7 8 9	620°0 614°1 616°0 603°0 609°4 614°4	619.8 615.9 615.1 594.5 610.7 614.0	620°2 615°7 610°0 602°0 607°4 614°2	617.0 615.0 610.0 612.6 600.0 612.0	599.6 604.5 606.5 600.0 608.0	605.6 597.9 603.5 592.4 596.8 602.0	605 · 1 603 · 0 578 · 0 594 · 0 598 · 7 608 · 2	607.2 608.0 592.4 596.8 602.7 610.0	614.8 611.0 606.0 600.4 604.0 612.0	620.0 617.7 611.3 607.5 608.0 608.0	622.5 617.5 614.0 605.2 608.0 610.7	611. 618. 611. 610. 611. 612.
JANUARY.	11 12 13 14 15 16 17	624.2 621.0 609.2 621.8 602.0 614.5	623°8 623°5 611°6 616°6 609°0 612°5	611 ° 2 626 ° 0 622 ° 6 618 ° 5 605 ° 8 615 ° 0	622.0 625.4 618.7 623.9 609.5 612.5	615.0 622.2 608.1 615.6 603.0 605.2	606.0 615.0 605.3 611.2 601.5 610.9	602.0 613.9 604.6 612.8 600.0 607.7	603°0 614°9 607°8 615°0 605°0 601°5	603.0 617.3 599.3 611.8 602.5 603.9	610°5 620°0 601°5 609°0 592°0 608°2	618.5 620.9 608.5 613.9 608.5 611.9	618 609 611 606 606
JA	18 19 20 21 22 23 24	630.0 627.5 621.4 624.9 631.5 607.0	630°0 629°0 621°7 624°3 631°1 618°0	627 · 8 627 · 0 623 · 4 624 · 0 628 · 1 619 · 0	626.0 624.5 618.1 618.5 619.2 620.0	626.0 616.1 613.1 610.8 606.0	627.5 614.6 611.4 608.2 607.0 599.5	623°0 616°2 608°0 608°4 610°0 603°5	620°4 619°9 612°0 616°0 616°0 589°8	624.5 624.7 621.0 624.8 626.0 594.7	627.0 625.0 625.0 634.5 632.0 600.9	628 · 2 628 · 8 625 · 0 639 · 0 640 · 0 608 · 9	629 628 621 637 632 607
17-	25 26 27 28 29 30 31 31	611.0 610.0 610.3 605.0 606.0 604.0	610°0 610°8 612°8 605°6 605°0 605°0	608.0 608.0 613.4 604.2 601.0 606.5	603·2 602·1 597·3 600·8 596·0 605·1	593.7 596.2 605.0 596.6 589.5 600.0	590°7 595°0 597°0 594°1 590°0 597°0	594.8 597.4 597.0 597.1 593.2 594.0	600°8 606°2 601°3 603°5 593°0 605°4	606.5 609.2 606.2 609.0 593.6 611.0	612.0 615.3 613.0 612.0 597.6 615.8	610.0 611.0 614.8 616.0 596.0 619.6	606° 613° 617° 612° 603° 618°
	y Means	615.53	615.86	615.17	613.01	607.25	603.75	603*44	606.44	610.06	613.79	616.87	615
	ė i	0	0	0	темр. 41°5		41°7		иет. 41°5	4 î °7	42.0	42°6	42°
	$\begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$	41°4 46°7 46°6	41°5 46°7 46°5	41°5 46°4 46°5	41.5 46.6 46.2	41°5 46°8 46°3	41°7 47°0 47°0	41°5 47°0 47°2	41°5 47°0 48°0	41 7 47 0 48 0	47.0 48.3	46.8 48.6	47 49
	4 5 6 7 8 9	43.0 45.0 47.5 51.5 48.7 47.6	42°8 45°5 47°8 51°0 48°6 47°4	42.6 45.6 47.4 50.4 48.0 46.8	42.6 45.4 47.5 49.7 47.8 46.4	43.0 46.2 47.8 49.5 47.8 46.2	43.8 47.2 48.5 50.0 48.0 46.9	44.8 47.4 49.0 50.0 48.2 47.0	45.2 48.0 48.8 49.8 48.5 47.0	46°2 48°0 49°0 49°4 48°7 47°5	46.5 48.0 49.4 49.2 49.2 47.5	46.4 48.0 49.2 49.0 49.2 47.0	47 47 49 48 49 46
JANUARY.	11 12 13 14 15 16	41.5 39.6 41.6 44.7 51.2 41.5	41.8 39.9 41.7 44.8 50.5 41.0	41.8 39.5 41.6 44.7 49.7 40.0	41.2 39.2 42.2 45.0 49.0 39.4	41.0 39.4 42.5 46.6 49.0 39.3	41.8 40.2 43.3 47.6 49.0 39.2	42.5 40.8 44.2 48.4 49.0 39.0	43.0 41.8 45.1 48.9 48.7 38.8	43 · 2 42 · 6 46 · 7 49 · 4 48 · 4 38 · 2	43.5 43.2 48.0 50.5 48.5 38.0	43.6 43.0 48.6 51.0 47.9 38.0	43: 42: 48: 51: 47: 37:
JA	18 19 20 21 22 23 24	32·2 35·5 42·2 37·0 36·1 42·0	33.0 35.5 41.7 37.1 36.2 41.5	32.9 35.0 41.0 36.6 36.1 41.5	33.0 36.0 41.0 37.5 36.2 41.5	34·1 36·4 40·7 38·0 37·5 42·0	35.0 37.0 41.0 37.5 39.4 43.0	35.6 37.4 41.4 37.0 40.5 43.5	36.6 38.2 41.7 37.2 41.0 43.8	37.0 39.0 42.3 37.6 41.5 44.0	37.6 39.8 43.6 38.7 42.1 44.6	39°3 40°6 43°8 39°5 43°4 45°2	40° 40° 43° 40° 43° 44°
	25 26 27 28 29 30 31	47.0 47.2 44.8 48.8 52.2 47.0	47.0 46.0 45.2 48.8 52.4 45.5	47.0 45.0 45.2 49.0 52.0 44.7	47.0 44.6 44.8 49.4 51.8 43.8	47.2 45.0 45.6 49.5 52.0 43.3	47.8 45.4 46.5 50.2 52.5 43.0	48.4 45.8 47.8 50.5 52.7 42.8	49.0 46.5 48.4 51.0 53.0 43.0	49.0 46.7 48.5 51.0 53.0 43.3	49.8 47.5 48.8 51.0 53.0 44.3	50°2 47°6 49°1 51°0 53°4 44°8	50° 47° 49° 50° 53° 45°
$-\mathbf{F}$	eb.1	-	_		-	-	-		-		_		

	One Scal	e Division =	• • • • • • • • • • • • • • • • • • •	rts of the I	I.F. Increa	ise in Scale	Division, co	rresponding	to 1º decrea	ise of Temp	erature, 1°63	
12 ^h .	13h.	14h.	15h.	16 ^h .	17h.	18 ^h .	19h.	20h.	21h.	22h.	23h.	Daily an Monthly Means.
Sc. Div.	8c. Div.	Sc. Div. 617.6	Sc. Div. 619.0	Sc. Div. 613 8	Sc. Div. 618.0	Sc. Div. 616.2	Sc. Div. 617.0	Sc. Div. 617.0	Sc. Div. 620.0	Sc. Div. 618.0	Sc. Div. 618.0	Sc. Div.
511.7	610.4	609.7	608.0	610.4	610.0	608.0	608.0	610.0	610.0	611.7	614.2	610.95
607.7	599.0	607.0	601.0	608.2	611.0				_			
				-		614.0	615.2	617.0	616.5	617.4	$\{619.6\}$	611.3
19.0	614.0	605.0	614.8	612'0	611.2	612.4	611.0	611.8	613.0	615'4	614.7	613.23
615 ' 8	607.7	606.0	606.8	611.0	609.9	608.0	621.4	614.3	612.6	610.9	608.0	611.29
210.0	600.8	601.2	592.0 606.7	605.5 606.2	610 .0	601.7 607.0	600°0 607°0	595 . 2	595.4 609.5	601.0	602.5	603.78
513.8	611.8	610.0	610.0	610.0	611.0	610.2	610.4	611.0	611.6	613.0 610.0	609.0	605°03 607°68
512.4	614.5	612.4	611.5	611.2	612.0	-	— — — — — — — — — — — — — — — — — — —	UII U			1 11	
	_	_	_	_		618.8	614.5	623.4	612.0	617.1	$\left\{\begin{array}{c} -626.0 \\ 620.5 \end{array}\right\}$	612.96
617.0	614.8	613.2	615.0	616.0	617.4	617.0	616.0	618.0	617.1	619.0	620.5	614.93
612.4	607.7	567.6	599.2	595.5	609.0	608.0	614.0	615.0	615.0	617.0	617.7	613:2:
609.0	595.0	612.4	610.0	611.0	611.0	611.0	613.0	610.4	608.2	610.0	616.6	$609 \cdot 33$
612.0	614.0	613.0	614.9	611.2	607.0	601.8	600.1	605.0	607.6	606.3	606.0	611.67
610 ° 8	606.9	608.0	605.6	609.0	615:0	608.8	596.2	597.7	598.0	605.0	613.2	605.00
520.2	623.1	623.0	612.0	615.1	615.0	628.0	630.0	630.0	632.0	637.0	626.0}	616.7
528 ·2	628.2	626.8	626.7	628.5	628.9	627.4	628.0	628.0	628.0	630.0	$\begin{vmatrix} 626.07 \\ 626.7 \end{vmatrix}$	627:28
524.3	625.2	627.2	625.0	628.9	627.0	621.2	$\begin{array}{c} 623.0 \\ 617.7 \end{array}$	620.0	622.0	622.0	622.6	623.5'
522.0	621.0	620.0	618.0	621.2	621.2	620.7	620.4	620.8	622.6	622.8	624.1	619.84
332.9	628.0	628.0	624.0	623.4	625.0	625.0	625.4	626.5	629.0	630.0	630.2	625.0
290.0	616.3	618.0	613.2	611.8	611.2	610.0	598.0	571.0	577.7	595.2	610.0	612.76
50 7·2	611.6	613.8	611.9	613.0	612.2						612.0}	608*68
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50 5 °9 514°0	606.0	606.8	607.0	608.0	607:0	607:0	606.0	607.0	608.5	608.2	610.2	605.6
614.0	614.9 597.0	614.4	611.1	$605.1 \\ 589.4$	609.0 596.4	602.0 602.0	610 .0	610°4 596°8	613.8	616.0	612.6	608:94
510.5	611.2	605.0	589.5 606.8	598°5	607.4	602.8	99.0	600.2	599.3 601.9	600.0 600.0	604.0	603.2
8.909	602.8	598.8	602.8	603.9	599.6	579.0	598.8	594.2	602.0	604.0	601.2	604.60 579.13
614.0	614.2	610.8	612.8	612.0	613.0				_		1 51	
_	-		_		_	627.0	625.0	626.0	629.0	629.0	$\left \frac{1}{629\cdot 4} \right\}$	613.20
613.94	612.01	610.79	610.19	610.76	612:33	612.32	611.63	610.99	611.93	613.97	615.00	611.77
				TE	MPERATUR	E OF THE E	BIFILAR MA					
43.2	43.0	42.8	43.0	43.0	42.8	43.3	44.0	44.2	44.6	45°7	46.4	42.80
47.7	48.0	48.0	48.4	49.0	49.0	48.7	47.4	47.0	46.5	46.2	46.5	47.28
49.0	49.0	49'0	48.3	48.4	48.5						२∥	46.3
47.5						41.5	41.5	41.7	42.0	42.5	43.0}	
47.5	47.5	47.2	47:0	46.8	46.8	46.5	46.2	45.4	45.0	45.0	45.0	45'4
49.4	47.0	46.5 50.2	46.5 50.5	46°5 50°7	46.2 50.7	46°2 51°0	46.2 50.8	46.6	47.2	47.2	47.4	46.79
48.2	48.8	48.8	49.0	49.0	48.9	49.0	49.0	51.0 49.5	51.5	52.0 49.5	51.5 49.0	49.60 49.43
49.2	48.8	48.2	48.1	48.1	48.4	48.2	48.2	48.2	49.5 48.4	48.3	47.9	43.43
46.0	45.8	45.6	45.6	45.4	45.2	_		-				
						40.2	40.2	40.4	40.5	41.0	41.0}	45.03
43.2	43.2	42.6	42.0	42.0	41.6	41.5	41.2	41.4	41.4	40.8	40.0	42.0
43.0 48.0	42.7	42.8	42.0	41.6	41.9	42.0	42.0	42.2	42.0	42.0	42.0	41.58
-tC	47.4 51.2	47.4	47.6	47.7	47.5	47.0	46'6	46.2	46.0	46.0	45.0	45.69
	46.8	51.2 46.4	51.2	51.2	51.0 44.7	51'0 44'6	50.8	51.2	51.5	51.5	51.2	49.4
51.2		40 4	45.5	45.2			44.2	43.8	43.6	42.6	41.9	46.8
51.2 47.2		36.4	36.9	36.0	1 36.0						{ } }	36.4
51.2 47.2 37.2	37.0	36.4	36.2	36.0	36.0	30.4	30.6	31.2	31.6		31.2	30 4
51.2 47.2 37.2 — 39.2	37.0	36.4	ł .	$\frac{36.1}{26.0}$	36.0	30.4 36.0	$\frac{30.6}{35.2}$	31.2	31.6	31.7 35.7	$\begin{bmatrix} -1 \\ 31 \cdot 2 \\ 35 \cdot 6 \end{bmatrix}$	
51.2 47.2 37.2 — 39.2 41.0	37.0 38.0 41.7	37.4 42.2	—		36·2 43·0	30°4 36°0 43°0	30.6			31.7		35.9
51·2 47·2 37·2 ————————————————————————————————————	37.0 38.0 41.7 45.0	37.4 42.2 45.0	36'9 42'8 44'5	36·1 42·5 43·5	36·2 43·0 42·0	30.4 36.0 43.0 41.6	30.6 35.2 42.2 41.3	31.2 35.4 42.5 39.6	31.6 35.4 42.5 38.4	31.7 35.7	35.6 42.5 37.0	35°9′ 39°98 41°88
51·2 47·2 37·2 ————————————————————————————————————	37.0 38.0 41.7 45.0 39.3	37.4 42.2 45.0 38.6	36.9 42.8 44.5 38.2	36°1 42°5 43°5 38°0	36.2 43.0 42.0 37.6	30.4 36.0 43.0 41.6 37.2	30.6 35.2 42.2 41.3 36.3	31.2 35.4 42.5 39.6 35.8	31.6 35.4 42.5 38.4 35.5	31.7 35.7 42.5 38.0 35.3	35.6 42.5 37.0 35.5	35°9' 39°98 41°88 37°5
51·2 47·2 37·2 39·2 41·0 44·2 39·5 43·5	38.0 41.7 45.0 39.3 43.0	37.4 42.2 45.0 38.6 42.7	36.9 42.8 44.5 38.2 41.8	36.1 42.5 43.5 38.0 41.4	36.2 43.0 42.0 37.6 41.0	30.4 36.0 43.0 41.6 37.2 40.8	30.6 35.2 42.2 41.3	31.2 35.4 42.5 39.6	31.6 35.4 42.5 38.4 35.5 41.0	31.7 35.7 42.5 38.0 35.3 41.2	35.6 42.5 37.0 35.5 41.5	35.9 39.9 41.8 37.5
51·2 47·2 37·2 	37.0 38.0 41.7 45.0 39.3 43.0 44.0	37.4 42.2 45.0 38.6	36.9 42.8 44.5 38.2	36°1 42°5 43°5 38°0 41°4 45°5	36.2 43.0 42.0 37.6 41.0 45.7	30.4 36.0 43.0 41.6 37.2 40.8	30.6 35.2 42.2 41.3 36.3 40.4	31·2 35·4 42·5 39·6 35·8 40·7	31.6 35.4 42.5 38.4 35.5 41.0	31.7 35.7 42.5 38.0 35.3 41.2	35.6 42.5 37.0 35.5 41.5	35.9° 39.98 41.88 37.53 40.55
51·2 47·2 37·2 39·2 41·0 44·2 39·5 43·5 44·0 50·0	38.0 41.7 45.0 39.3 43.0	37·4 42·2 45·0 38·6 42·7 44·8	36.9 42.8 44.5 38.2 41.8 45.3	36·1 42·5 43·5 38·0 41·4 45·5	36·2 43·0 42·0 37·6 41·0 45·7	30.4 36.0 43.0 41.6 37.2 40.8 — 45.5	30.6 35.2 42.2 41.3 36.3 40.4 	31·2 35·4 42·5 39·6 35·8 40·7 46·3	31.6 35.4 42.5 38.4 35.5 41.0 46.3	31.7 35.7 42.5 38.0 35.3 41.2 	35.6 42.5 37.0 35.5 41.5 	35.9' 39.99 41.83 37.53 40.55 44.35
51·2 47·2 37·2 39·2 41·0 44·2 39·5 43·5 44·0 	37.0 38.0 41.7 45.0 39.3 43.0 44.0	37.4 42.2 45.0 38.6 42.7	36.9 42.8 44.5 38.2 41.8	36·1 42·5 43·5 38·0 41·4 45·5 —	36.2 43.0 42.0 37.6 41.0 45.7 50.0	30.4 36.0 43.0 41.6 37.2 40.8 — 45.5 50.0	30.6 35.2 42.2 41.3 36.3 40.4 	31.2 35.4 42.5 39.6 35.8 40.7 	31.6 35.4 42.5 38.4 35.5 41.0 46.3 48.5	31.7 35.7 42.5 38.0 35.3 41.2 47.0 48.0	35.6 42.5 37.0 35.5 41.5 	35.99 39.99 41.88 37.55 40.55 44.32 48.7
51·2 47·2 37·2 — 39·2 41·0 44·2 39·5 44·0 — 50·0 47·0 49·3	37.0 38.0 41.7 45.0 39.3 43.0 41.0 49.8 46.5 49.5	37.4 42.2 45.0 38.6 42.7 44.8 	36.9 42.8 44.5 38.2 41.8 45.3 	36°1 42°5 43°5 38°0 41°4 45°5 — 49°4 46°0	36·2 43·0 42·0 37·6 41·0 45·7	30.4 36.0 43.0 41.6 37.2 40.8 — 45.5	30.6 35.2 42.2 41.3 36.3 40.4 	31·2 35·4 42·5 39·6 35·8 40·7 46·3	31.6 35.4 42.5 38.4 35.5 41.0 46.3 48.5 45.4	31.7 35.7 42.5 38.0 35.3 41.2 	35.6 42.5 37.0 35.5 41.5 	35.9' 39.98 41.86 37.5; 40.55 44.32 48.7' 46.00
51·2 47·2 37·2 — 39·2 41·0 44·2 39·5 44·0 — 50·0 47·0 49·3 50·2	37.0 	37.4 42.2 45.0 38.6 42.7 44.8 	36.9 42.8 44.5 38.2 41.8 45.3 - 49.2 45.6 49.3 50.4	36·1 42·5 43·5 38·0 41·4 45·5 —	36·2 43·0 42·0 37·6 41·0 45·7 — 50·0 46·2	30.4 36.0 43.0 41.6 37.2 40.8 — 45.5 50.0 45.8	30.6 35.2 42.2 41.3 36.3 40.4 	31·2 35·4 42·5 39·6 35·8 40·7 — 46·3 48·8 45·4	31.6 35.4 42.5 38.4 35.5 41.0 46.3 48.5	31.7 35.7 42.5 38.0 35.3 41.2 	35.6 42.5 37.0 35.5 41.5 	35.9° 39.9° 41.8° 37.5° 40.5° 44.3° 48.7° 46.0° 48.0°
51·2 47·2 37·2 ————————————————————————————————————	37.0 	37.4 42.2 45.0 38.6 42.7 44.8 	36.9 42.8 44.5 38.2 41.8 45.3 -49.2 45.6 49.3 50.4 53.8	36·1 42·5 43·5 38·0 41·4 45·5 	36·2 43·0 42·0 37·6 41·0 45·7 50·0 46·2 49·2 50·8 53·2	30.4 36.0 43.0 41.6 37.2 40.8 — 45.5 50.0 45.8 49.0	30.6 35.2 42.2 41.3 36.3 40.4 	31.2 35.4 42.5 39.6 35.8 40.7 	31.6 35.4 42.5 38.4 35.5 41.0 	31.7 35.7 42.5 38.0 35.3 41.2 	35.6 42.5 37.0 35.5 41.5 — 46.7 47.5 45.0 49.0 52.0 48.0	35 90 35 90 39 90 41 86 37 50 40 50 44 32 48 7 46 00 48 04 50 56 52 40
51·2 47·2 37·2 39·2 41·0 44·2 39·5 44·0 50·0 47·0 49·3 50·2	37.0 	37.4 42.2 45.0 38.6 42.7 44.8 	36.9 42.8 44.5 38.2 41.8 45.3 - 49.2 45.6 49.3 50.4	36·1 42·5 43·5 38·0 41·4 45·5 	36·2 43·0 42·0 37·6 41·0 45·7 50·0 46·2 49·2 50·8	30.4 36.0 43.0 41.6 37.2 40.8 	30.6 35.2 42.2 41.3 36.3 40.4 	31·2 35·4 42·5 39·6 35·8 40·7 	31.6 35.4 42.5 38.4 35.5 41.0 46.3 48.5 45.4 48.5 51.8	31.7 35.7 42.5 38.0 35.3 41.2 	35.6 42.5 37.0 35.5 41.5 — 46.7 47.5 45.0 49.0 52.0	35 '9' 39 '9' 41 '8. 37 '5: 40 '5: 44 '3: 48 '7 46 '0: 48 '0- 50 '5:

Vol. III.

tin- }	O ^h •	1h.	2h.	3h.	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8h.	9 ^h .	10h.	11h.
2 3 4 5 6 7	Sc. Div. 630 2 617 4 612 7 611 5 608 0 610 0	Sc. Div. 627 ° 0 618 ° 8 615 ° 0 611 ° 0 607 ° 0 604 ° 6	Sc. Div. 628.8 615.0 611.7 608.7 607.0 607.2	sc. Div. 618 ' 4 610 ' 0 603 ' 0 605 ' 2 605 ' 4 604 ' 0	Sc. Div. 610.6 595.4 595.0 600.5 601.0 593.6	Sc. Div. 607 2 595 0 593 0 594 0 597 0 591 8	sc. Div. 608 8 596 0 590 9 594 5 600 0 594 2	sc. Div. 608 2 596 2 586 0 596 0 600 6 599 6	sc. Div. 614*2 600*0 594*0 600*0 603*4 604*4	sc. Div. 619 0 605 0 604 0 601 4 603 4 602 6	Sc. Div. 620 2 610 0 606 5 602 0 604 4 607 2	sc. Div 618 8 610 0 610 0 604 8 603 6 605 6
8 9 10 11 12 13	627'4 628'0 620'4 624'0 619'8 604'6	630°5 623°0 618°0 621°0 619°7 602°4	611.6 631.4 619.0 614.0 608.8	555 ° 0 633 ° 0 612 ° 0 616 ° 2 608 ° 2 607 ° 2	628 ° 0 631 ° 5 610 ° 0 612 ° 4 608 ° 0 608 ° 0	621.6 627.4 614.0 609.2 606.0 603.2	618.8 624.2 613.0 609.2 606.5 606.6	621 ° 0 630 ° 0 617 ° 0 614 ° 6 610 ° 8 610 ° 6	623.0 635.5 614.2 608.2 614.8 609.0	622°0 630°5 623°0 622°2 615°6 627°0	621 ° 0 627 ° 0 623 ° 0 613 ° 2 616 ° 0 611 ° 8	622°0 627°8 619°0 615°0 614°0 617°5
15 16 17 18 19 20	612'0 617'0 614'0 615'0 619'2 612'0	619°2 618°0 616°0 614°2 620°4 610°8	607°3 609°0 607°0 614°0 620°0 608°0	613°5 605°0 604°0 616°8 618°4 606°0	608.0 611.0 607.0 617.7 616.0 609.2	604.4 608.2 605.0 616.8 616.0 612.2	608 '4 606 '5 596 '0 618 '8 614 '0 612 '5	597 · 2 605 · 2 599 · 8 617 · 4 614 · 2 610 · 0	605 · 4 610 · 0 596 · 2 616 · 0 617 · 0 609 · 5	612.2 594.0 602.2 610.2 618.8 605.0	606°0 604°8 601°5 611°6 615°4 610°0	598.0 605.4 606.0 611.0 612.0 610.4
22 23 24 25 26 27 28 1	626.0 622.5 623.0 622.8 627.6 622.1	626'0 621'0 619'4 621'4 627'8 620'0	625°0 620°0 618°4 620°5 625°5 616°6	621 ° 0 619 ° 4 619 ° 2 614 ° 0 621 ° 4 613 ° 2	618.0 622.0 618.0 610.4 618.5 608.1	615°0 624°2 617°2 613°6 614°5 604°8	615.2 621.2 618.6 603.4 615.0 606.3	615.0 620.4 619.0 620.0 616.0 610.0	617 · 2 622 · 0 624 · 0 615 · 0 611 · 0 613 · 8	618 · 4 622 · 4 628 · 2 629 · 0 620 · 0 618 · 0	620.8 620.8 609.0 617.0 622.0	619*4 618*4 614*0 605*0 623*2 620*4
leans	618.63	618.01	615.26	610.40	610.75	608.80	608*28	609.78	611.28	614.75	613*26	612.5
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2 3 4 5 6 7 8 9 10 11 12 13	35.6 43.5 46.0 49.0 49.2 49.2 	35:4 43:6 46:2 48:8 48:9 48:6 33:0 33:0 42:5 38:7 44:0 44:6	34.8 43.8 43.8 49.0 48.5 47.4 33.0 33.0 42.0 38.9 43.8 44.0	35:0 44:0 47:2 50:1 48:5 48:2 	36.0 44.3 48.6 51.0 49.0 49.2 34.5 34.0 41.9 40.5 43.6 43.4	36·2 45·0 49·1 51·4 50·0 50·2 34·6 34·3 43·2 40·7 44·6 44·2	37:2 45:6 49:0 51:0 50:0 50:4 34:6 35:0 43:5 41:3 45:5 45:0	38.7 46.0 48.5 50.8 50.6 50.5 - 34.6 36.0 43.8 41.8 46.2 45.8	39·2 46·8 48·5 51·4 51·2 50·1 35·0 37·3 44·0 42·2 47·1 46·8	39.7 47.8 49.0 52.0 51.6 50.0 	40'4 48'7 49'0 52'0 52'0 50'0 — 36'0 38'4 44'0 42'8 48'0 47'8	40.5 48.5 48.2 51.7 49.7
15 16 17 18 19 20 21	43.0 44.0 44.5 42.0 42.0 46.7	43°2 44°0 44°0 41°8 42°0 46°5	43.0 43.5 43.9 41.0 41.6 46.4	43.2 44.0 44.5 40.6 41.7 46.4	44.0 44.5 45.5 41.2 42.0 46.6	44.5 46.0 46.6 42.0 43.0 48.0	44.6 47.0 46.8 43.0 43.5 48.6	44.7 47.0 47.4 43.5 44.0 49.2	44.6 47.4 47.8 43.7 44.8 48.4	44.8 47.7 48.4 43.7 45.5 48.0	45.0 48.0 48.5 43.4 46.4 47.8	44 6 47 4 48 2 43 0 46 5 47 5
22 23 24 25 26 27 28 1	37.4 39.4 40.0 36.2 30.0 39.0	37.4 38.6 39.2 34.8 29.0 39.0	37·2 38·8 38·4 34·9 29·7 38·0	38.8 38.8 38.0 35.1 30.5 37.8	39.5 38.8 38.6 35.8 31.2 38.0	40.4 39.6 39.4 36.7 33.4 39.0	40.5 40.8 40.4 37.2 35.0 40.0	40.6 41.6 40.8 37.2 37.0 40.4	40.7 42.6 41.0 37.5 38.0 40.8	41.0 42.8 41.4 38.4 38.7 41.0	41.6 42.8 42.0 37.8 38.8 41.4	41 : 42 : 41 : 42 : 41 : 42 : 41 : 42 : 42
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Div. 22 630°2 627°0 628°8 611°14 618°8 615°0 611°7 55 611°5 611°5 611°0 608°7 6608°0 607°0 607°0 607°0 610°0 604°6 607°2 80 623°0 631°4 618°0 628°0 623°0 631°4 618°0 619°0 628°0 623°0 611°6 619°0 619°8 619°8 619°7 614°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 619°0 610°0 610°0 610°0 610°0 610°0 610°0 610°0 610°0 610°0 620°0 610°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 620°0 6	Sc. Div. Sc. Div. Sc. Div. Sc. Div.	Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div.	Sc. Div. Sc. Div.	Sc. Div. Sc. Div.	Sc. Div. Sc. Div.	Sc. Dir. Sc. Dir.	Sc. Div. Sc. Div.	Sc. Dir. Sc. Dir.

	One Sca	le Division :	= ·000087 I	parts of the		IZONTAL ase in Scale		orresponding	to 1° decre	ase of Temp	oerature, 1°6	3.
12h.	13h.	14 ^h .	15h.	16 ^h .	17 ^h .	18h.	19h.	20h.	21h.	22h.	23h.	Daily an Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
	622.0	618.0	615.0	620.0	620.0	618.2	619.2	618.4	618.0	616.2	621.4	618'34
622.0								611.0	614.2	613.2	613.7	608.73
614.5	614.0	614.0	607.6	607.2	609.0	611.2	611.2					
609'2	608.7	609'4	607.8	609.2	609.2	609.2	610.8	610.7	611.0	612.2	612.2	605.89
606.2	607.0	606.2	607.3	607.2	607.4	607.0	608.0	607.5	608.0	607.0	608.0	604.86
604'0	605.0	599.2	603.0	601.0	605.0	604.0	599.0	601.0	598.0	602.0	606.0	602.83
607.0	606.0	606.0	606.0	608.0	608.2						$\{-\frac{1}{623\cdot 6}\}$	604.86
					C14:0	608.0	607.4	605.0	602.0 624.8	604.4 624.4	623 6 7	619.04
622.0	624.0	626.0	613'4	614.2	614.0	620.2	623.0	623.2			020 0	
52 2·2	621.0	617.2	620.0	618.6	619.6	622.0	621.6	617.2	618.2	619.4	620.0	624.43
317'4	617.8	616.4	620.0	620.4	619.6	618.2	620.0	620.0	618'4	621.2	618.0	617.92
614.0	613.7	610.0	617.0	619.0	619.0	617.0	617.0	617.0	617.0	617.0	617.0	615.79
507.5	603.0	598.0	612.0	603.0	607.0	607.0	606.2	606.0	606.8	605.0	602.2	609.06
602.0	611.0	617.0	607.6	607.2	610.0			_				
002 0	011 0	017 0	00, 0	00, 2	010 0	606.6	607.4	611.8	615.4	613.2	$\{607.2\}$	609.71
	610.0	600:0	610:0	611.7	613.4	615.0	615.0	618.0	613.2	608.8	611.0	608.96
91.2	610.2	606.2	610.0	611.5					613.0	613.0	611.0	609.85
09.5	613.8	611.9	609.0	612.2	612.0	611.0	614.0	612.2				
07.0	609.0	608.0	609.0	609.0	610.0	608.5	610.0	612.0	612.0	610.5	613.0	607:20
16.0	614.0	615.0	618.0	618.0	618.2	617.5	617.8	619.4	618.0	619 .2	618.6	616.23
913.0	609.0	616.0	608.0	608*0	610.0	609.2	606.4	606.6	608.8	610.0	607.2	613.07
10.0	610.0	612.0	610.5	611.4	610.0						_ 11	613.03
10 0	010 0	012 0	010 2	011 1	010 0	622.0	623.0	620.0	618.6	625.0	625.0}	613 03
	600.0	C00:0	600:0	601.0	622.7	622.8	623.0	623.0	623.0	622.4	622.0	621:11
21.0	623.2	622.8	622.0	621.8						621.0	621.4	620.28
18.5	618.0	618.1	618.0	620.0	621.0	621.0	621.0	621.0	621.0			
08.0	604.0	602.0	611.0	612.0	616.0	615.0	612.0	612.7	618.0	618.7	619.6	615.71
17.0	617.0	608.0	604.7	614.0	620.0	622.0	620.8	624.0	624.2	622.0	626.2	617.18
23.0	623.4	624.2	625.4	619.8	619.6	618'4	622.4	622.1	621.0	621.3	622.0	621.05
519.8				621.0	622.7	010 1					1 /1	010100
	620.6	620.0	622.0	021 0	-	625.7	627.0	628.0	631.2	627.0	$\{-628.0\}$	619.30
612.56	613.26	612.28	612.67	613.07	614.34	614.88	615.15	615.32	615.57	615.59	616.68	613.23
				TEM	PERATURE	OF THE B	IFILAR MA	GNET.				
0	0					0	0	0	•		•	٥
40.5	41.0	41.0	41.4	41.5	42.0	42.4	42.5	42.8	43.0	43.2	43.2	39.74
	41.0	41.2	41.4			ì			47.0	46.6	45.7	46.58
48'4	48.5	48.5	48.0	47.8	47.8	47.4	47.4	47.2	/ ·	3		47.76
47'8	47.8	47.8	47.6	47.8	47.8	47.4	47.0	47.0	47 2	47.2	47.7	50.68
50.6	50.4	50.4	50.3	50.7	51.0	51.0	51.2	51.0	51.0	50.2	49.6	
51.0	51.1	51.0	50.2	50.2	50.2	50.4	50.5	50.0	49.6	49.5	49.0	50.18
49.8	49.5	49.0	47.8	46.5	45.2				_		$\frac{-}{32\cdot 8}$ }	45.3
_				_	_	33.7	34.0	34.8	35.0	35.6		
35.5	35.2	35.2	35.4	35.1	35.0	34.2	34.0	34.5	33.8	33.8	33.3	34.56
38.5	38.6			38.2	38.6	39.4	39.9	41.0	41.7	42.0	42.5	37.5
43.6		38.8	38.2			41.7	41.5	41.2	41.2	41.4	40.0	42.3
42°6	42.8	41.8	41.2	41.2	41.5			43.0	43.4	43.8	43.9	41.80
	42.6	42.0	41.8	42.0	42.0	42.4	42.9			46.7	45.6	46.5
48.2	48.6	48.4	47.5	47.4	47.8	48.4	47.6	47.7	47.2	101		
47.0	46.9	46'1	45.8	45.2	45'0					1010	$\{-\frac{1}{42\cdot 7}\}$	44.5
	_		l —			40.2	40.6	40.8	41.8	42.2	42 7)	
44°4	44.2	44.0	43.8	43.6	43.6	43.4	43.2	43.6	43.9	44.0	44.0	43.9
47.0	46.4	46.5	45.6	45.2	45.2	45.5	45.2	45.0	45.2	45.6	45.0	45.7
47.9	48.0	47.8	47.0	47.0	47.0	46.6	45.0	44.2	43.5	42.5	42.0	46.0
41.8	42.0					42.0	42.0	42.4	42.5	42.4	41.8	42.10
47.0		41.6	41.5	41.5	41.5				47.6	47.4	47.0	45.5
	48.0	48.0	47.2	47.0	47.3	47.5	47.4	47.6	J			
47.0	47.3	47.0	46.6	46.4	46'0				20:4	38.0	$\frac{-}{37.8}$	45.00
	-	—	l —		-	38.0	37.6	38.9	39.4		90.0	00.00
41.0	40.8	40.8	41.0	40.7	40'6	40.4	40.0	39.9	39.5	39.4	39.0	39.99
41.7	41.4	41.6	41.4	41.0	40.6	40.6	40.4	40.0	39.2	39.5	39.3	40.59
	40.8	39.8	39.4	40.0	40.0	39.8	39.6	39.4	38.4	38.0	37.0	39.72
40°4	36.0					33.0	32.4	31.8	31.5	31.2	30.2	34.97
40°4 36°0		35.5	35.0	34.6	33.2				39.2	39.2	39.2	36.8
36.0	38.8	40.0	40.2	40.0	40.1	40.1	39.8	38.9	03 4	55 0		
36 · 0 37 · 8		41.4	41.7	41.4	41.1		33.7	33.6	33.4	33.4	$\frac{-}{33\cdot 4}$	38.60
40'4 36'0 37'8 41'2	41.4		1			34 9	1 00 4	000				
36 · 0 37 · 8		43.93	_	-		34.2	41.89	41.92	41.88	41.81	41.36	42.7

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25 610·5 611·0 607·0 601·2 594·8 589·9 591·2 593·1 595·2 594·7 602·5 590·1 509·2 27 602·4 600·5 595·9 595·9 596·9 593·1 505·2 594·7 602·5 590·1 592·8 603·7 599·9 592·9 591·2 589·4 580·9 574·7 583·9 586·5 602·1 598·2 603·7 599·9 592·9 591·2 589·4 583·7 585·9 583·9 586·7 592·4 601·9 602 29 30 616·7 611·4 607·4 596·9 577·9 584·9 578·9 582·1 588·9 596·2 607·9 614 610·9 608·9 607·0 599·2 594·0 588·1 589·0 594·5 600·7 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·2 604·1 614·				608.0	599.0		584.0							608
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28 603.77 599.9 592.9 591.2 589.4 583.7 585.0 583.9 586.7 592.4 601.0 602. 30 616.7 611.4 607.4 595.9 577.9 584.9 578.9 582.1 588.9 596.2 607.0 604.1 614.2 604. 31 610.9 608.9 607.0 599.2 594.0 588.1 589.0 594.5 600.7 604.1 614.2 604. 600.00000000000000000000000000000000		26												598
29		28												598 605
Ourly Means 607*35 605*48 602*59 597*21 592*54 588*78 587*84 590*24 595*47 600*62 603*16 604 **Temperature of the Biflar Magnet.** C2		30				— 595`9	577:9	584.9		582.1	588.9	596.2	607.9	614
TEMPERATURE OF THE BIFLAR MAGNET. 2				ļ]						604
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	lourly	Means	007 33	605 48	602*59	597.21	592.54	588.78	587.84	590.24	595.47	600.62	603.16	604
## HO						· · · · · · · · · · · · · · · · · · ·	ERATURE (OF THE BIF	ILAR MAGN	ET.				
## HO	1									$4\overset{\circ}{2}$ ·2				43.1
## HOME ##										$45^{•}4$				46
## HOAP 6	- 1								48.4					49
AW 44'0 43'9 44'0 45'2 46'2 47'0 46'8 46'8 46'6 46'8 47'0 46'8 9 47'7 47'6 47'3 47'6 49'2 50'3 50'8 51'4 52'0 52'6 53'0 53'0 53'3 53'3 53'1 53'5 51'4 52'0 52'6 53'0 53'3 53'3 53'3 53'3 53'1 53'5 51'0 55'4 55'1 52'2 52'0 52'0 52'0 52'5 53'8 54'0 54'4 54'4 54'4 54'4 54'4 54'4 54'4 54'4 54'4 54'4 54'0 55'4 55'1 55'0 55'0 52'0 52'0 52'0 52'0 52'3 53'1 53'5 53'6 53'7 54'0 54'8 55'1 55'0 55'0 52'0 52'0 52'0 52'1 52'1 52'1 52'1 52'1 52'1 55'1 52'1 52'1 52'1 <td></td> <td>6</td> <td></td> <td>54 51</td>		6												54 51
HOAVE HO		7												46
HONE HIS Series of the series	Ì	9		47.6	47.3	47.6	49.2	50.3	<u> </u>	<u></u> 51'4	52.0	<u></u> 52.6	53.0	53
H	l					50.9	52.5	53.0		53.3	53.1			54
HONE IN Section 1.1														55
HONE HIS Series	l													53
Here the state of														54
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		14		40.4	40.0	46.5	46.2	46.7	47:0		<u></u> 47:5	47.6	47.5	48
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ЭН.	14 15	46°8	40 4	40 8									50.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	RCH.	14 15 16 17	44.6	44.0	43.7	44.0		43 4					52.4	52
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	MARCH.	14 15 16 17 18	44.6 44.5	44.0 44.0	43.7 44.0	44.0 44.2	45.8	47.5					56.3	56
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	MARCH.	14 15 16 17 18 19	44.6 44.5 53.5	44.0 44.0 53.0	43.7 44.0 52.6	44.0 44.5 53.4	45.8 54.0	47.5 55.0	55.2	56.0	56.4		1 1	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	MARCH.	14 15 16 17 18 19 20 21	44.6 44.5 53.5 52.2	44°0 44°0 53°0 51°8	43.7 44.0 52.6 52.4	44.0 44.5 53.4 53.6	45.8 54.0 54.2	47.5 55.0 55.0	55.2 55.3	56.0 55.8	56.4 56.3	57.0	57.0	57
$ \begin{bmatrix} 25 & 52.0 & 51.5 & 51.4 & 51.2 & 51.4 & 51.2 & 51.4 & 52.2 & 52.6 & 53.0 & 53.2 & 53.6 & 53.6 & 53.6 \\ 26 & 51.4 & 51.2 & 51.0 & 51.0 & 51.7 & 52.2 & 52.6 & 53.0 & 53.2 & 53.6 & 53.6 & 53.6 \\ 27 & 50.8 & 51.3 & 51.0 & 51.0 & 51.8 & 51.7 & 52.0 & 52.2 & 52.2 & 52.2 & 52.5 & 52.2 \\ 28 & 50.5 & 50.4 & 50.1 & 50.3 & 50.8 & 51.5 & 52.0 & 52.5 & 52.5 & 52.5 & 52.0 & 52.2 \\ 29 & - & - & - & - & - & - & - & - & - & $	MARCH.	14 15 16 17 18 19 20 21 22	44.6 44.5 53.5 52.2 52.4	44.0 44.0 53.0 51.8 51.8	43.7 44.0 52.6 52.4 51.0	44.0 44.5 53.4 53.6 50.5	45.8 54.0 54.2 50.0	47.5 55.0 55.0 50.0	55°2 55°3 49°9	56.0 55.8 50.0	56.4 56.3 50.0	57.0 50.8	57.0 51.8	57: 52:
$ \begin{bmatrix} 26 \\ 27 \\ 50.8 \\ 50.5 \\ 29 \\ 30 \end{bmatrix} \begin{bmatrix} 51.4 \\ 50.8 \\ 50.5 \\ 46.0 \end{bmatrix} \begin{bmatrix} 51.2 \\ 50.3 \\ 50.1 \\ 46.0 \end{bmatrix} \begin{bmatrix} 51.0 \\ 51.0 \\ 51.0 \\ 50.3 \\ 50.3 \end{bmatrix} \begin{bmatrix} 51.7 \\ 52.2 \\ 50.8 \\ 51.5 \\ 52.0 \\ 49.4 \end{bmatrix} \begin{bmatrix} 53.2 \\ 53.2 \\ 52.2 \\ 52.2 \\ 52.5 \\ 52.5 \\ 52.5 \\ 52.5 \\ 52.5 \\ 52.0 \\ 52.5 \\ 52.0 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52.2 \\ 52$	MARCH.	14 15 16 17 18 19 20 21 22 23 24	44.6 44.5 53.5 52.2 52.4 47.2 52.5	44.0 44.0 53.0 51.8 51.8 	43.7 44.0 52.6 52.4 51.0 48.4	44.0 44.5 53.4 53.6 50.5 — 50.0	45.8 54.0 54.2 50.0 — 51.9	47.5 55.0 55.0 50.0 ——————————————————————	55.2 55.3 49.9 — 52.8	56.0 55.8 50.0 — 53.0	56.4 56.3 50.0 — 53.0	57.0 50.8 — 53.3	57.0 51.8 — 53.2	57:52:52:52:52:0
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	MARCH.	14 15 16 17 18 19 20 21 22 23 24 25	44.6 44.5 53.5 52.2 52.4 47.2 52.5 52.0	44.0 44.0 53.0 51.8 51.8 47.6 52.5 51.5	43.7 44.0 52.6 52.4 51.0 	44.0 44.5 53.4 53.6 50.5 - 50.0 52.1 51.2	45.8 54.0 54.2 50.0 — 51.9 52.2 51.4	47.5 55.0 55.0 50.0 ——————————————————————	55.2 55.3 49.9 — 52.8 52.4 52.0	56.0 55.8 50.0 — 53.0 52.6 52.4	56.4 56.3 50.0 	57.0 50.8 — 53.3 52.5 52.8	57.0 51.8 — 53.2 52.7 53.4	57: 52: 52: 52: 54:
29	MARCH.	14 15 16 17 18 19 20 21 22 23 24 25 26	44.6 44.5 53.5 52.2 52.4 	44.0 44.0 53.0 51.8 51.8 47.6 52.5 51.5 51.2	43.7 44.0 52.6 52.4 51.0 48.4 52.5 51.4 51.0	44.0 44.5 53.4 53.6 50.5 50.0 52.1 51.2 51.0	45.8 54.0 54.2 50.0 51.9 52.2 51.4 51.7	47.5 55.0 55.0 50.0 52.2 52.0 51.8 52.2	55.2 55.3 49.9 — 52.8 52.4 52.0 52.6	56.0 55.8 50.0 — 53.0 52.6 52.4 53.0	56°4 56°3 50°0 	57.0 50.8 	57.0 51.8 — 53.2 52.7 53.4 53.6	57: 52: 52: 52: 54: 53:
	MARCH.	14 15 16 17 18 19 20 21 22 23 24 25 26 27	44.6 44.5 53.5 52.2 52.4 47.2 52.5 52.0 51.4 50.8	44.0 44.0 53.0 51.8 51.8 47.6 52.5 51.5 51.2 51.3	43.7 44.0 52.6 52.4 51.0 	44.0 44.5 53.4 53.6 50.5 50.0 52.1 51.2 51.0 51.0	45.8 54.0 54.2 50.0 51.9 52.2 51.4 51.7 51.8	47.5 55.0 55.0 50.0 	55.2 55.3 49.9 — 52.8 52.4 52.0 52.6 52.0	56.0 55.8 50.0 53.0 52.6 52.4 53.0 52.2	56.4 56.3 50.0 53.0 52.4 52.4 53.2 52.2	57.0 50.8 	57.0 51.8 — 53.2 52.7 53.4 53.6 52.5	57: 52: 52: 52: 53: 53: 53:
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	One Scale	Division =	·000087 pa	irts of the H		IZONTAL ase in Scale		rresponding	to 1º decre	asc of Temp	erature, 1·6	3.
12h.	13h.	14h.	15 ^h .	16h.	17h.	18h.	19 ^h •	20h.	21h.	22h•	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 620 0	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 621 0	Se. Div.
619.2	622.0	621.6	620.0	619.4			620.0	620.0	621.0	621.5	1	619:32
617.0	617.0	616.0	613.0	613.0	612.0	616.0	612.4	612.0	618.0	616.0	615.6	612.79
611.0	612.5	611.5	610.0	607.8 a	600.0	602.0	601.8	605.4	603.2	603.0	610.0	607.16
605.2	610.0	608.2	603.4	$598.2 \\ 609.3$	604.8	601.0 607.2		604.0	602.2	$\begin{array}{c} 608.0 \\ 613.5 \end{array}$	608.0	604.17
607.8	615.0	615.0	615.2	614.0	614.3	007 2	607.7	612.2	612.4	019 9	614.3	605.90
616.0	013 0	013 0	010 2	014 0	014 2	613.0	613.0	614.8	613.0	613.8	614.3	610.35
608.0	608.0	608.0	609.0	609.0	607.0	607.0	606.2	607.4	609.2	610.0	014 0)	605.87
606.2	606.0	604.0	605.0	604.7	605.0	604.2	606.8	608.4	608.0	608.8	609.2	602.73
607.2	606.0	593.0	596.4	596.2	597.4	609.0	603.0	602.2	600.5	604.2	603.8	602.53
594.0	594.8	599.4	597.0	597.6	600.1	604.0	600.9	604.5	600.0	606.0	610.0	598.05
582.0	592.4	588.2	580.0	580.2	583.0	580.0	569.0	571.2	586.0	577.0	594.8	583.93
284.0	585.2	579.5	587.0	587.0	586.0	000 0	005 0	0,1	000 0	011 0		
J31 U	000 0	019 0	001 0		000 0	600.2	610.0	607.2	607.0	607.4	$\frac{-}{607.0}$	588.23
590.9	592.0	597:0	597.0	595.2	620.4	594.8	604.5	599.0	599.2	604.0	597.0	597.77
607.2	604.0	608.0	600.0	595.6	601.4	597.8	598.7	594.2	564.4	576.4	601.0	594.28
600.8	595.0	602.8	603.4	603.2	601.8	602.0	602.0	600.0	600.0	600.0	601.0	599.29
600.1	600.6	598.6	597.3	598.2	598.2	598.0	597.5	599.0	599.0	601.0	599.2	593.47
595.8	597.6	594.5	594.5	598.8	599.0	600.0	599.4	601.0	599.4	599.6	599.8	592.29
299.0	598.0	903.0	600.4	601.6	602.0	000 0	055 1	001 0	0.00	035 0	_ 1	
033 0	030 U	000 0	000 4	001 0	002 0	604.4	607.2	608.8	610.5	611.2	611.0	598.29
602.0	607.2	607.0	606.4	605.8	604.2	603.4	603.2	604.0	605.2	607.4	605.0	601.06
602.1	605.8	606.0	606.2	605.6	605.6	607.0	607.0	607.4	609.0	612.0	610.0	602.23
606.1	607.9	608.4	604.9	604.1	604.1	602:3	603.6	601.9	604.9	609.1	611.2	603.76
603.2		600.9	299.9	598.9	608.9	598.4	601.9	603.7	601.9	605.2	600.7	600.16
592.9	601.7 598.1		601.9	601.3	602.2	602.1	603.9	603.7	604.3	605.2	607.9	596.20
607.1		601.9		597.3	603.3	002 1	003 3	000 1	004 0	000	,	
007 1	587.9	583.9	598.3	997 9	003 3	607.7	610.9	613.9	612.9	613.7	$\{618.1\}$	598.85
614.3	610:0	C00:0	600:5	608.9	608.3	608.8	605.0 p	609.9	611.2	613.9	613.0	603.68
600.7	610.2	609.9	608.5		609.1	608.4	607.9	609.9	609.9	611.9	612.1	604.39
000 /	604.7	604.9	602.4	607.9	009 1	000 4	007 9	009 9	003 3	011 3	012 1	001 55
603:32	603.53	602.78	602.55	602:30	604.03	603.80	604.32	604.85	604:31	606.18	607.81	601.03
	1		1	Т	EMPERATU	RE OF THE	BIFILAR M	AGNET.	<u>'</u>	1		1
42°9	43.5	44.0	44.0	43°5	43.2	43.0	42.0	42.0	41.4	4ΰ0	40°.5	41° 15
47.0	47.0	46.5	46.0	45.9	45.7	45.6	45.6	45.7	45.4	45.5	45.0	44.75
49.3		49.0	49.3	49.3	49.7	49.8	49.8	49.6	49.2	49.0	48.9	48.33
54.5	49.0	1	1	52.2	1	50.8	50.1	50.3	49.8	49.5	49.2	51.17
50.4	53.8	53.0	52.6 49.5	48.8	51.6	47.2	47.0	45.6	45.2	44.2	44.1	48.69
46.3	50.4	50.0		47.8	48.4	71.2	710	40 0	10 2	11.0		ł
	46.7	46.9	47.2	4		46.0	46.0	46.2	46.6	46.9	47.0}	46.37
52.6	52.5	52.0	51.2	51.5	51.5	51.1	50.9	50.7	50.4	50.5	1, 0,	50.76
53.8	53.4	53.0	53.1	52.7	51.8	51.3	51.2	49.8	49.6	49.2	48.2	51.83
55.3	54.8	54.2	54.0	53.4	52.6	52.2	52.0	51.7	51.5	51.5	51.0	52.70
53.2	53.6	53.2	53.2	53.4	53.5	53.3	53.2	53.2	54.5	55.0	55.0	53.40
55.6	55.8	56.5	56.4	56.4	56.5	55.8	55.6	55.6	55.4	55.0	54.8	55.27
53.2	23.0	52.4	52.4	51.7	51.4		00 0	-	00 1	_		
_	33 0	02 4	02.4	— ·	_	45.4	45.8	46.1	46.0	46.4	46.6}	51.70
47.9	47.5	47.5	47.3	47.0	46.8	46.2	46.5	45.8	45.4	45.0	44.9	46.75
50.6	49.8	49.2	48.5	47.8	47.4	47.0	47.0	46.2	46.4	47.0	45.0	46.29
52.0	49.8 52.7	53.0	53.3	53.9	54.0	54.0	53.6	53.2	53.5	53.0	53.2	50.29
26.0	56.0	56.0	55.4	55.0	54.5	54.5	53.2	53.1	52.6	52.2	52.0	54.23
55.6	55.7		55.1	54.2	54.5	53.7	53.5	52.8	$\frac{52.7}{52.7}$	23.0	52.6	54.45
52.5		55.7	1	20.0	49.7		00 2	02 0				1
_	51.2	51.1	50.6	50 0	49 /	46.4	46.6	46.6	46.6	46.8	47.3	49.85
52.6	52.0	51.6	51.4	51.4	51.6	51.6	51.3	51.6	52.0	$52.\overline{5}$	52.2	51.55
52.0	51.6	51.6	51.6	51.8	51.9	51.2	51.0	50.7	51.4	51.8	51.7	51.96
54.5	54.5	54.0	53.1	52.5	52.5	52.2	51.6	51.2	51.2	51.2	51.4	52.35
53.0	52.2	52.5	52.4	52.0	52.4	52.4	52.0	51.7	51.2	51.2	51.4	52.50
52.1	51.8	52.1	52.0	52.0	51.8	51.6	51.6	51.2	51.2	51.2	50.2	51.69
51.8	51.7	52.0	51.8	51.2	51.0							1
_	01 /	02.0	01.0	01 2	01.0	44.9	44.8	44.8	45.0	45.4	$\frac{-}{45.5}$	49.87
49.8	47.4	49.4	48.8	48.7	48.4	48.2	48.0	48.0	47.8	48.1	48.4	48.64
52.6	50.4	50.2	49.9	49.7	49.7	49.4	48.5	48.0	47.5	46.2	46.5	49.40
51.81	51.55	51.40	51.17	50.93	50.75	49.81	49.55	49.33	49 20	49.19	48.93	50.25

^{*} Three minutes late.

	0	ne Scale Di	vision = •0	00087 parts	of the H. F.		NTAL FO		sponding to	1º decrease	of Temperat	ure, 1°63.	
Mean Gö gen Tir	ittin- }	0h.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h •	6 ^h •	7 ^h •	8 ^h •	9 ^h .	10 ^h •	11 ^h .
	1 2 3 4	Sc. Div. 612°8 609°9 615°0 606°0	Sc. Div. 610 '9 608 '1 612 '2 611 '6	Sc. Div. 610.7 607.5 610.0 612.5	Sc. Div. 607 7 612 8 606 0 607 0	Sc. Div. 600°3 607°7 600°4 591°0	Sc. Div. 596 3 601 7 593 5 586 0	sc. Div. 594 1 602 4 591 0 581 0	Sc. Div. 595°5 602°0 590°0 581°6	Sc. Div. 600°1 601°0 597°5 592°0	sc. Div. 611'9 608'0 602'5 610'4	sc. Div. 600°9 611°0 604°0 598°6	sc. Div 607 ° 0 613 ° 5 603 ° 8 601 ° 2
	5 6 7 8 9	591.0 584.6 590.0 600.8	571°2 580°0 586°0 599°0	570.0 575.0 585.4 595.0	600°5 575°6 583°8 588° 5	572.5 572.9 578.5 582.5	574.0 574.2 582.0 578.9	567 2 573 6 585 6 581 4	577.0 570.0 587.0 587.0	591.6 578.8 592.0 591.0	608.5 583.5 585.0 601.0	630°2 587°8 594°4 602°0	577°0 585°2 599°0 602°8
1	10 a 11	602.0	595.2	595.3	595.4	598.2	591.0	597.2	589.2	597.2	598.2	595.0	599.8
APRIL.	12 13 14 15 16 17 18	605.8 612.5 608.0 610.0 595.2 597.2	612.8 603.0 603.7 600.0 593.4 594.2	602.4 610.0 594.0 568.0 589.0 590.6	599°4 604°9 593°2 563°2 582°4 577°2	599°0 593°7 584°2 566°4 585°0 570°5	583.8 586.0 586.0 560.0 583.2 569.2	576.2 587.6 588.8 581.8 575.0 571.0	578.9 590.0 595.7 588.8 579.4 579.6	596.0 602.0 598.6 604.2 592.0 587.0	616.0 584.0 604.4 609.0 608.2 586.5	594.5 611.0 612.4 621.8 604.5 585.2	609.0 601.0 605.2 611.6 604.0 589.0
	19 20 21 22 23 24 25	602°2 597°6 591°5 593°8 598°8 586°0	600.6 599.0 594.5 592.6 597.8 586.1	597.0 594.0 586.5 588.0 591.2 583.5	587.0 585.0 580.6 574.2 579.0 577.9	582.0 577.5 574.2 570.5 579.2 576.0	577 0 574 0 579 7 571 4 581 0 582 0	582.5 575.0° 589.8 576.1 583.8 578.9	587.0 580.3 ° 587.8 580.8 592.0 582.0	587.0 585.2 584.8 585.0 600.0 585.0	592.0 589.4 586.8 597.8 603.0 577.0	603.0 589.6 588.5 594.2 599.8 596.0	598 ° 0 589 ° 2 593 ° 2 598 ° 0 598 ° 0 584 ° 2
	26 27 28 29 30	599.0 595.0 596.6 596.8	601 ° 0 590 ° 0 594 ° 2 592 ° 0	589.5 583.0 588.0 583.8	576.0 578.2 583.2 575.2	585.0 580.0 579.8 582.0	597.0 584.6 575.0 583.8	595.6 586.3 585.2 588.6	600°0 590°2 591°0 591°0	603°3 591°4 594°8 588°0	597.0 593.8 597.2 596.0	590°0 587°9 599°2 593°4	591.8 593.0 607.0 589.0
Hourly 1	Means	599.92	597.16	592.00	587.76	583.26	582.05	583.83	586.96	593.02	597.88	599*80	598.0
					ТЕМР	RATURE O	F THE BIFI	LAR MAGN	ET.		1		1
	· 1 2 3 4	45.7 46.4 46.9 50.6	45.4 47.0 47.5 50.3	45°8 47°8 49°0 50°5	46.8 49.0 50.0 51.9	48.4 50.1 51.8 52.7	49°2 50°5 52°5 53°5	49°4 51°4 52°7 54°0	49.9 52.0 53.0 54.5	50°5 52°0 53°0 54°8	51.6 52.2 53.9 56.0	52°0 52°2 54°5 56°5	51°9 52°5 54°8 56°8
	5 6 7 8 9	53.7 54.5 51.8 48.6	53.5 54.0 51.4 49.5	53 · 2 54 · 0 51 · 7 50 · 1	53.6 54.4 51.7 51.0	54.5 54.9 51.8 52.4	55°5 55°0 52°0 52°5	56.0 55.2 52.4 52.4	56°4 56°5 52°5 53°0	56.6 56.5 52.6 53.0	57.0 57.0 52.6 54.0	57°2 56°8 53°2 54°5	57.2 56.9 53.6 54.3
	10 a 11	49.6	49.4	49.0	49.2	50.1	51.0	52.0	53.4	53.2	53.2	53.0	52.8
APRIL.	12 13 14 15 16 17 18	44.2 44.3 48.5 47.0 50.0 53.4	44°3 45°5 48°5 48°0 50°3 54°0	44.4 46.3 48.5 49.0 51.0 54.2	45.2 46.9 49.0 49.0 52.2 54.6	46.2 47.4 49.6 49.6 53.9 55.4	45.7 48.0 49.5 50.0 55.2 55.9	45.5 47.9 49.5 50.8 55.8 56.3	45.4 48.2 49.6 51.0 56.5 56.6	45.4 48.5 49.8 51.6 56.7 57.0	46.4 49.4 50.4 51.6 57.0 58.0	47.4 50.0 51.0 52.2 57.5 58.5	47.7 50.0 51.5 52.6 57.4 59.0
	19 20 21 22 23 24 25	50.7 57.0 59.4 59.6 59.8 60.4	51°3 57°2 59°0 59°5 59°8 60°0	52.8 57.5 58.5 59.7 59.6 59.5	53°4 58°7 58°5 60°0 59°6 58°8	55°0 59°6 58°3 60°8 60°0 58°4	55.6 60.7 58.5 60.7 60.8 58.4	56.0 61.4 58.5 61.0 61.2 58.6	56.9 62.2 59.3 61.2 61.6 59.0	57.4 63.0 59.6 61.2 61.9 58.6	58.0 64.0 60.0 61.3 61.8 58.5	58.6 64.3 60.2 61.3 61.9 58.5	59.0 64.2 60.3 60.6 62.0 58.2
	26 27 28 29 30	51.4 56.5 57.5 57.2	52°7 57°4 57°4 56°7	54.0 58.0 57.0 57.8	55°0 58°2 56°4 57°8	57.0 58.6 57.2 58.7	57.4 59.4 57.4 57.4 59.2	57.5 59.6 57.6 59.8	57°9 59°8 57°8 60°5	57.9 59.8 57.7 61.2	58.6 60.0 57.8 61.8	59°4 60°2 57°5 62°0	60°0 60°3 57°5 62°0
lourly I	Means	52.19	52.38	52.76	53.24	54.10	54.26	54.90	55.39	55.29	56.10	56.42	56.5

² Good Friday.

b Two minutes late.

[°] Three minutes late.

12% 13% 14% 15% 16% 17% 15% 19% 20% 21% 22% 23% M 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66% 66%		One Scal	le Division	= '000087	parts of the			L FORCE. le Division,	correspondi	ng to 1° dec	rease of Ter	npe r atur e, 1	63.
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	596.15	593.49	592.85	591.52	593.10	591.36	592.98	594.68	595.04	595.56	597.76	597.86	593.09
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	$\begin{pmatrix} 1 \\ 2 \\ 0 \end{pmatrix}$	Sc. Div. 593 ° 0 593 ° 5	Sc. Div. 591*2 592*1	sc. Div. 584.6 583.8	5c. Div. 575 0 573 0	Sc. Div. 577 0 571 0	Sc. Div. 575 2 578 5	Sc. Div. 578.8 587.0	sc. Div. 586'4 594'0	Sc. Div. 591 ° 0 592 ° 2	sc. Div. 591 2 592 0	sc. Div. 594 ° 0 589 ° 4	Sc. D 593
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lourly	Means	583*92	581.66	575.85	567.84	566.90	570.67	575.10	5 81.57	589*19	590*32	592*30	591
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	$\begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$	59°9 61°2	60°2 61°2	60°6	61°0 62°1	61°0 63°4	61.0 64.0	61°4 64°0	62°0 64°2	62°0 64°2	62.0 64.6	62°0 65°2	62. 65.
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	7 8 9 10	57°2 58°6 62°0	57.8 59.5 62.0	58°0 60°4 62°0	58.8 62.4 61.8	59.5 63.4 61.6	60°2 63°5 61°8	60.2 64.0 61.8	61.0 64.5 62.0	61.6 61.6	61.4 61.8	61.5 64.6 62.0	61 64 62
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MAY.	14 15 16 17	62.0 63.2 59.6	62°2 63°0 59°2	62.5 62.5 59.4	63°4 62°3 60°4	64.3 62.7 61.9	65°3 63°2 63°0	65.8 63.6 63.6	66.0 64.4 64.2	66'4 64'3 64'7	66°8 64°8 65°2	67°0 65°2 65°7	65.
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	26 27 28	66.0 69.0 69.2	66.5 70.4 69.6	67.4 71.0 70.8	68.4 72.0 71.5	69.7 72.8 71.9 71.7	70.4 73.6 71.9 72.0	$ \begin{array}{c cccc} 71.2 \\ 73.8 \\ 72.0 \\ 72.0 \end{array} $	71.8 74.0 72.3 72.0	$egin{array}{c c} 72.5 \\ 74.4 \\ 73.1 \\ 73.0 \\ \end{array}$	73°2 75°0 72°9 73°0	$73.4 \\ 75.4 \\ 72.8 \\ 73.2$	73 75 73 73
	29 30	68 .2	69.0 68.9	69.0 69.8	70.7 68.7	69.4	70.5	70.8	71.7	72.4	73.0	73.5	73

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	1 2 3 4 5 6 7	68.5 69.4 65.5 66.4 65.4 61.1	69.5 69.2 66.3 67.0 65.2 61.2	70°0 69°0 66°7 67°4 65°0 62°0	70°5 69°5 67°2 67°5 64°9 62°9	69.8 69.8 67.3 67.8 64.5 63.6	70°6 69°8 67°5 68°1 64°4 63°5	70.8 70.0 67.6 68.7 64.4 63.7	71.0 69.8 67.5 69.4 64.9 63.7	71.5 70.0 67.6 69.4 65.0 64.0	72.0 70.0 68.2 69.5 65.0 64.5	72.6 70.2 68.9 69.4 65.7 64.5	73. 70. 69. 65. 65.
	8 9 10 11 12 13	58.5 60.0 62.6 65.5 63.6 63.2	59.0 60.5 63.2 65.7 64.2 64.0	60°1 61°2 64°3 66°0 65°0 64°5	61:3 62:2 65:2 66:4 65:9 65:2	62.7 64.0 66.4 68.0 66.0 66.4	63.7 65.4 66.7 68.6 66.7 67.2	64.2 65.7 67.2 68.7 67.0 67.5	64.6 66.1 67.8 69.0 67.0 67.9	65.2 66.5 68.9 68.5 67.2 68.1	65.8 67.2 70.0 68.5 67.2 68.3	66.4 67.7 70.5 69.2 67.0 68.4	66 68 71 69 67 68
JUNE	14 15 16 17 18 19 20	66.2 69.4 67.1 69.5 71.5 70.6	66.5 69.4 67.4 69.4 71.6 70.4	67.0 69.8 68.2 69.5 71.6 70.2	68.4 70.2 68.8 70.0 71.7 69.8	69.9 71.0 69.7 71.2 72.0 69.6	70°8 71°4 70°3 71°8 72°6 70°0	71.2 71.2 71.0 72.6 73.5 70.2	71.7 71.2 71.5 73.4 74.5 70.2	72·2 71·4 72·4 73·8 75·4 70·0	73.0 71.5 73.5 74.0 76.5 69.8	73.8 71.8 74.0 74.5 76.7 69.5	74: 72: 74: 74: 77: 69:
	21 22 23 24 25 26 27 28	59.2 61.5 65.0 68.7 70.8 72.0	59.0 61.2 65.3 69.0 70.5 71.8	59°4 61°9 66°0 69°8 70°7 72°0	60°5 62°7 67°0 70°8 70°6 72°0	61.7 64.8 67.9 71.7 71.4 72.2	62.8 66.0 68.7 73.2 72.5 73.0	63.5 66.9 70.0 73.8 73.2 73.6	64.0 68.0 70.7 75.0 74.0 73.8	64.4 68.4 71.7 75.7 74.5 74.0	64.8 69.5 72.0 76.4 75.5 74.0	65 · 2 70 · 3 73 · 3 76 · 5 76 · 0 74 · 0	65: 70: 73: 77: 76: 74:
	28 29 30	71·5 73·3	71·5 74·0	71°5 74°7	71.5 75.7	71.4 76.9	73°4 77°5	74·4 77·8	75.0 78.2	75.5 78.3	76.0 78.7	76.4 79.0	76: 79:
lal	Means	66.38	66.62	67.06	67.63	68:37	69.08	69.55	70.00	70.37	70.82	71.21	7

	One Scale	Division =	*000087 pa	arts of the H		ZONTAL :	FORCE. Division, co	orresponding	to 1º decre	ase of Tem _I	perature, 1° (33.
12h.	13h.	14 ^h .	15 ^h .	16 ^h •	17h.	18h.	19 ^h .	20 ^h .	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div. 575 8 603 5 585 0 576 0 590 2	Sc. Div. 574.8 569.2 587.2 574.0 584.3	Sc. Div. 570°2 561°0 571°0 574°0 581°6	Sc. Div. 544.5 555.2 572.0 579.0 586.2	Sc. Div. 532 4 546 0 574 0 576 8 588 5	Sc. Div. 548 2 549 0 571 2 573 2 569 8	Sc. Div. 531 8 550 0 573 0 571 8 568 0	sc. Div. 545.2 565.0 572.2 570.0 581.0	Sc. Div. 552°2 558°0 574°6 565°7 587°1	Sc. Div. 555°0 570°0 573°2 563°8 584°2	Sc. Div. 550°0 575°6 572°0 575°2 589°0	sc. Div. 565 ° 0 576 ° 0 578 ° 4 575 ° 6 589 ° 2	Sc. Div. 561 * 58 568 * 24 572 * 64 570 * 33 579 * 13
598.2 606.8 592.0 588.0	594.8 	581.2 595.0 575.0 577.0	572.8 	574.0 	574.7 	587.0 571.0 569.0 572.4	585°8 558°0 572°0 574°2	588.0 581.0 574.3 576.8 579.2	588.2 559.0 575.2 578.4 577.2	590.8 586.0 574.3 579.0 575.5	594.0 } 590.8 577.5 576.4 577.0	587°18 583°06 574°25 576°72 578°76
588.2 585.8 588.0 	584.3 581.8 588.2 — 582.2 589.0	580°2 582°4 578°2 	573°4 582°8 574°8 — 561°5 566°0	576°5 585°4 575°6 — 560°0 582°6	577.4 587.0 575.5 —————————————————————————————————	579.8 596.0 	579.8 590.0 — 577.0 566.0 571.0	590°2 584°0 574°6 578°8	594.0 574.5 570.0 572.0	594.0 575.0 568.0 557.8	601.0 583.2 577.0 580.6	584°98 585°39 572°75 572°77
568.0 584.2 571.4 582.0 	573°2 569°2 566°0 582°0 — 604°0	570.0 574.0 568.0 581.0 575.0	570°0 560°5 568°0 579°0 — 569°2	571.8 559.4 566.0 581.0 581.4	572.8 565.8 567.0 576.0 — 585.0	575.0 564.0 567.2 — 596.0 587.4	577.0 544.5 568.0 599.8 589.4	573.5 560.0 567.0 	576.5 569.2 567.0 	574.0 569.0 571.0 578.2 592.4	574.0 566.0 573.2 	574.63 570.65 569.70 578.41 588.65
590°2 571°0 576°0 574°0 581°0	591.0 575.6 561.6 579.0 581.0	581.2 575.8 567.5 581.8 578.0	577.2 575.2 564.7 571.0 570.0	582.2 577.6 566.8 570.2 574.6	578.6 578.5 567.4 576.0 574.0	580.4 577.8 572.0 579.0 — 556.8	585°4 579°0 574°0 571°5 — 573°8	584.8 581.0 572.0 570.2 569.2	583.5 579.0 571.0 569.0 	581.2 584.0 572.2 575.3 — 576.2	582.0 585.6 576.0 573.8 — }	583.75 581.11 572.81 573.42 570.52
577.0 563.0 583.97	577·2 569·8 580·77	571.0 565.2 575.06	554.8 565.0 569.63	559°2 567°6 570°84	556.4 560.7 569.98	557.2 558.0 571.43	560.8 560.0 572.71	565.6 568.0 575.28	568.5 567.2 573.90	560°0 566°4 575°47	565.2 578.5 579.70	567.80 565.05 575.55
				TE	MPERATUR	E OF THE I	BIFILAR MA	AGNET.				
73°0 70°2 69°6 68°5 65°5	. 72°8 69°6 69°4 68°4 65°5	72°4 69°2 69°0 68°0 65°2	72°2 69°0 69°0 67°8 64°8	72°1 68°5 68°6 67°6 64°5	71°6 68°0 68°4 67°4 64°2	71°3 67°8 68°0 67°0 63°5	70°9 67°3 67°8 67°0 62°6	70°5 66°8 67°6 66°6 62°2	70°3 66°5 67°2 66°4 62°0	69°9 66°0 67°0 66°0 61°5	69°4 65°5 66°6 65°8 61°3	71°10 68°80 67°83 67°75 64°29
66.5 68.4 71.0 69.4 67.6	64.2 66.5 68.6 71.0 69.2 67.4	66.0 68.5 70.4 68.7 66.6	63°2 	62.7 	62.2 64.2 66.0 68.7 67.6 65.1	60°3 63°7 65°6 68°5 67°0 64°7	60.0 62.5 64.6 67.6 66.0 64.1	59.8 62.0 64.0 67.2 65.5 64.0	59.5 61.2 63.4 66.5 64.8 63.5	59.0 60.6 63.2 66.5 64.2 63.4	58.6 59.8 62.4 65.6 63.5 63.0	62*40 63*40 65*17 67*74 67*32 65*65
68.0 74.6 72.2 74.6 74.8 77.0	67.5 	67.1 	66.6 73.0 71.3 73.4 74.5 75.2	66.4 	66.0 72.0 70.2 72.4 73.8 74.5	68.0 71.5 70.0 72.0 73.5 74.1	67.6 71.0 69.2 71.4 73.0 73.0	67.0 70.8 68.6 71.0 72.6 72.5	66.6 70.0 68.2 70.8 72.3 72.0	66.6 69.0 67.6 70.3 72.0 71.5	66:3 69:0 67:2 70:0 71:5 71:0	66.77 71.10 70.37 71.49 72.77 73.87
69.0 64.7 70.5 73.9 77.0 76.6	68.2 	67.6 	67.0 	66.5 64.0 68.6 72.1 75.0 75.0	66.0 63.8 68.0 71.9 74.7 74.7	60°3 63°5 67°4 71°4 73°9 74°5	60.4 63.1 66.7 70.6 73.0 74.0	60°2 63°0 66°5 70°4 72°5 73°6	60°0 62°5 66°0 69°6 71°9 73°5	59.7 62.0 65.6 69.3 71.5 73.2	59·2 } 61·7 65·0 68·7 71·0 72·5	66*81 62*95 66*90 70*36 73*59 73*81
74.0 77.0 79.5	73·5 	73.0 77.0 78.7	73.0 76.4 78.2	72·7 — 76·0 78·0	72·5 — 75·4 77·6	73·3 75·0 77·2	73°0 74°4 77°0	72·7 74·0 76·2	72°4 73°7 75°4	72.0 73.2 74.8	71.7}	72.93 74.46 77.10
71.45	71.27	70.77	70.34	69.95	69.50	68.96	68.38	67.99	67.55	67.14	66.69	69.10

Mean G Tim	öttin-}	Oh.	1 ^h .	2 ^h .	3h.	4 ^h .	5 ^h .	6h.	7 ^h .	8h.	9h.	10 ^h .	11h.
	1 2 3 4	sc. Div. 568 5 561 0 557 5 554 6	Sc. Div. 568 ° 0 571 ° 4 570 ° 2 542 ° 6	Sc. Div. 570°0 563°2 567°8 560°9	Sc. Div. 571 6 554 8 559 4 568 9	Sc. Div. 565°0 552°8 561°0 569°0	Sc. Div. 554 8 550 0 571 0 570 0	Sc. Div. 557 4 567 2 577 8 574 2	Sc. Div. 561 5 563 0 572 0 582 0	Sc. Div. 562 5 564 4 574 2 584 0	Sc. Div. 563 2 571 0 564 1 580 0	sc.Div. 565°1 576°5 578°8 583°0	Se. Div 579*5 576*0 579*0 586*0
	5 6 7 8 9 10	561.5 569.0 571.4 568.0 574.6 582.2	570°8 570°0 576°2 569°0 570°2 575°4	556.0 558.0 568.8 568.0 571.0 558.6	561 °0 550 °0 567 °5 564 °4 568 °3 558 °8	555°2 560°8 566°0 554°0 564°0 565°5	554°0 562°0 561°8 557°3 564°2 573°5	537 · 5 560 · 6 560 · 5 561 · 2 559 · 0 551 · 0	568 · 2 581 · 0 579 · 2 563 · 6 566 · 4 547 · 2	567.0 580.4 572.0 565.0 565.3 536.5	573°2 571°8 578°4 562°4 569°4 562°0	584.0 569.2 586.0 569.8 570.8 579.5	593 · 2 573 · 2 581 · 0 582 · 6 559 · 4 576 · 0
JULY.	12 13 14 15 16 17 18	571.4 575.2 586.2 585.6 587.4 582.2	570°8 566°8 587°8 586°0 585°0 582°0	577°2 569°2 584°6 588°0 583°5 572°0	579°2 568°4 578°0 577°0 573°0 572°8	573°5 565°0 569°2 563°5 579°0 562°0	558°8 568°2 575°0 576°0° 576°0 566°2	558°4 571°8 580°4 580°6 580°0 567°0	563°8 577°4 589°0 583°0 593°2 591°8	578°4 589°0 583°0 593°0 593°0 592°2	587.0 592.6 589.0 586.5 599.4 600.8	590°0 575°0 594°0 591°0 598°2 614°2	580°2 590°0 596°0 590°8 593°2 578°0
	19 20 21 22 23 24 25	580.6 579.2 572.0 585.4 581.2 582.4	583°0 567°8 569°8 587°2 580°0 566°0	582.0 572.8 567.6 580.4 576.2 573.8	570°0 573°9 566°0 559°5 569°8 562°7	557 0 571 7 561 5 564 5 553 0 557 0	570°6 571°5 564°2 565°5 563°5 565°4	576°2 572°2 568°0 574°0 571°8 576°5	579 ° 4 568 ° 8 571 ° 5 572 ° 0 575 ° 6 581 ° 0	580°6 572°0 580°5 571°5 565°7 596°5	576.0 579.0 588.0 572.0 568.8 577.2	580°0 574°8 584°8 577°5 595°2 580°4	580°4 577°0 581°2 581°0 586°0 586°0
	26 27 28 29 30 31	578.4 578.6 573.4 549.5 574.0	580°0 578°5 573°0 557°0 571°8	568.6 574.0 575.5 570.0 554.8	562.0 575.7 565.0 564.0 568.5	552°0 568°6 549°8 548°2 545°8	554.0 568.2 562.5 552.0 540.4	562.0 578.7 542.5 561.8 544.6	564.0 578.5 572.0 556.2 568.2	573.4 592.0 582.0 571.4 587.0	573°0 584°0 590°0 584°8 583°6	569°0 585°0 575°8 556°4 591°0	575 °C 583 °C 563 °C 592 °C 594 °C
lourly	Means	573.74	573.20	570.83	567.04	561.28	563.28	565.66	572.94	576.76	578.79	581.30	581.9
		74.5	75.5	76.1				LAR MAGNI	$\frac{\text{ET.}}{ 7\mathring{9}\cdot 2 }$	79.4	79.6	79.5	79°:
	1 2 3 4	74.5 73.8 71.8 69.8	75°5 74°3 72°4 70°5	76.1 74.8 73.2 71.2	77.2 75.4 74.2 72.0	78·2 75·8 75·0 73·0	78.7 76.5 75.5 74.0	78.8 76.6 75.5 75.0	79.2 76.6 75.6 75.5	79°4 77°0 75°8 76°0	76.8 76.0 76.8	79 5 77:0 75:9 77:5	79 : 77 : (76 : (77 : 3
	5 6 7 8 9 10	74.0 72.8 70.4 72.0 75.3 78.0	74.5 72.4 70.0 72.5 76.4 78.4	75.0 72.8 70.0 73.2 77.5 78.6	75.9 73.3 70.0 73.8 78.6 79.0	76.2 74.0 70.2 74.8 80.2 80.0	76°2 74°7 71°0 75°3 82°0 81°4	76.4 74.8 71.2 75.3 83.2 81.7	76.8 75.0 71.8 75.0 83.2 82.5	77'3 75'4 72'6 74'8 83'2 82'3	78°3 75°4 74°2 75°2 83°8 81°5	79.4 76.0 75.1 75.6 84.5 81.2	79°6 76°6 75°6 85°6 81°6
JULY.	12 13 14 15 16 17 18	72.7 69.5 65.1 64.0 63.7 65.6	73.0 69.6 64.8 64.8 64.4 66.5	73.7 70.3 65.4 65.4 65.8 67.4	74·4 70·4 66·0 65·8 67·0 68·2	74·4 70·8 66·4 66·2 68·0 69·0	74.6 70.8 66.7 66.5 68.5 70.0	74.6 70.8 66.8 66.7 69.0 70.2	74.6 70.7 67.0 66.9 69.2 71.0	75.0 70.7 67.0 67.2 69.2 71.5	75'4 71'0 67'2 67'5 70'6 72'1	75.8 70.9 67.4 67.7 71.0 72.4	76 · 2 70 · 3 68 · 0 68 · 0 71 · 1 72 · 6
	18 20 21 22 23 24 25	72.0 72.2 72.9 71.5 73.7 70.6	71.7 72.3 72.5 72.2 73.7 71.4	72.0 73.4 72.5 73.0 73.5 71.8	72.4 74.5 72.7 73.8 73.2 72.0	73.0 75.0 73.0 74.6 73.0 73.7	74.2 76.0 73.4 75.0 73.6 74.5	74.6 76.8 73.9 75.5 73.0 74.9	75°2 77°0 74°2 76°0 72°9 75°5	75.6 77.4 74.5 76.5 72.7 76.4	76.0 77.6 75.0 77.0 73.2 76.7	76.6 77.6 75.5 77.3 73.3 77.3	77.6 77.6 75.6 77.4 73.6 77.4
	26 27 28 29 30 31	71.6 70.5 73.0 77.0 76.3	72·2 71·2 74·0 77·5 76·0	72.6 71.5 74.5 77.7 75.6	73.0 72.5 75.4 78.5 76.0	74.8 73.0 76.1 79.0 76.4	75°0 73°7 77°4 79°6 77°2	75.0 74.7 78.4 79.8 77.8	74.9 75.0 78.7 80.5 77.6	75.5 75.5 78.7 81.2 77.8	 75·7 76·0 79·2 81·8 78·5	75.9 76.5 80.3 82.2 79.0	76.0 76.2 80.4 82.0 79.0
		71.64	72.03	72.54	73.12	73.84	74.52	74.85	75.11	75.41	75.86	76.54	76:

² Four minutes late.

	One Scal	e Division =	= .000087 1	parts of the	IIOF II. F. Incre	RIZONTAL ease in Scale	FORCE.	orresponding	g to 1° decre	ease of Tem	perature, 1	63.
12h.	13h.	14h.	15h.	16h.	17h.	18h.	19h.	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
582.4	568.8	556°2 554°0	560.5	563.0	565.5	568.8	565.0	565.0	545.0	558.0	557.2	564.27
564.5	571.0	563 0	562.5	549.0	555.5	563.0	548.0	552'2	554.3	550.2	563°0 554°0	560.76 563.33
596.2	594.4	574'2	574.4	547.0 587.6	530.2	534.3	582.8	568.2	549.8	550 5	1	1
000 2	0.51	0,12	0111	337 0	304 4	564.2	568.0	559.0	561.8	566.4	554.0 564.2	572.50
571.4	563.5	565.2	556.8	556.6	554.2	561.0	557.0	560.2	561.4	561.0	564.2	563:10
572.0	572.4	561.8	560.1	560.0	558.5	558.0	565.0	564.8	566.4	567.2	564.4	565.69
568.0	570.0	569.0	573.2	566.3	570.0	567.0	561.0	565.0	562.3	567.5	566.2	569.77
579.2	575.4	570.8	568.8	568.2	563.8	563.4	568.4	566.0	570.2	566.6	571.4	567.40
561.8	565.0	554.0	561.4	559.0	563.0	564.8	590.8	564.7	566.0	570.2	580.0	566.80
564.0	559.0	554.4	551.2	556.2	537.0	_					- 1	562.06
_		-				558.0	560.4	567.6	562.0	579.0	574.4}	(•
574.5	576.0	560.8	562.8	563.6	567.0	567.2	568.0	563.0	557.0	548.0	550.2	568.62
585.0	582.0	580.6	579.0	581.0	581.0	560.0	593.7	592.0	588.4	587.2	575.4	578.91
589.0	587.0	585.0	583.2	582.0	580.4	579'3	586.4	585.0	585.8	586.4	588.0	584.57
587.3	580.0	579'3	578'8	585.8	583.6	585.8	587.0	592.0	562.5	577.4	584.0	582.69 584.50
584.0	579°0 571°4	579°2 578°0	582.6 584.5	584.0 583.6	581.7	583.4	583.4	587.0	580.2	581.8	581.0	1
010 0	3/1 4	310 0	304.3	384 0	580.8	571:0	577.0	552.0	581.5	574.8	577.0}	578.74
579.0	575.5	562.5	572.0	568.0	565.0	574°0 570°0	577°0 572°4	570.6	571.0	568.2	570.4	573:35
572 5	572.0	572.5	574.0	573.2	568.4	556.2	550.0	562.2	563.7	575.0	570.0	570.43
579.8	577.8	579.6	578.8	581.8	580.9	582.0	581.0	582.0	578.0	559.7	577.0	575.56
582.0	584.4	575.4	574.0	575.0 в	575.0	573.2	573.5	574.5	576.0	577.5	579.0	575.42
596.0	589.0	560.0	576.0	575.0	571.0	568.0	558.0	561.4	565.0	566.2	577.4	572.91
569.0	570.5	573.2	571.0	572.0	572.4		_				l → 1	574.77
-						577.0	576.3	579.4	575.2	576.3	577.2}	
574.0	582.0	563.2	561.2	563.6	566.4	564.0	573.2	578.6	582.2	578.0	579.0	569.87
572.4	575.0	575.2	577.4	578.2	580.0	576.0	588.0	581.4	577.0	576.0	576.0	578.23
569.0	564.4	555.8	562.0	563.5	565.0	567.2	568.5	568.0	562.9	570.0	566.0	566.98
555.8	556.0	561.0	569.0	563.9	548.0	550.0	560.0	566.0	567.0	561.5	568.2	562.07
263.0	569.0	552.8	571.8	563.2	567.0	560.8	574.2	570.0	566.2	576.0	574.0	568.00
575.91	573.94	567.29	569.60	569.28	567.25	566.22	571.74	570.29	568:11	569.68	571.08	571.16
	<u></u>			TEN	IPERATURI	E OF THE I	BIFILAR MA	GNET.		<u></u>		
79°0	78.3	77.7	77.4	77.0	76°6	76°2	75°5	75°0	74°5	74.2	73.7	77.13
77.3	77.2	77.2	76.5	76.0	75.2	76.2	74.0	74.0	73.4	72.6	72.0	75.49
76.0	75.8	75.0	74.0	73.8	73.2	73.0	72.2	71.6	70.8	70.4	70.0	73.86
77.5	77.5	76.2	76.4	76.2	75.8	75 0	12 2	110			— 1	
<u> </u>		_				76.0	75.7	75'3	74.5	74.3	73.9}	
79.5	78.2	77.8	77.2	76'9	76.3	75.7	75.0	74.5	74.2	73.9	73.0	76.32
76.3	76.0	75.0	74.8	74.6	73.8	73.1	72.3	72'0	71.8	71.6	71.2	73.97
75.8	76.2	75.9	75.3	74.8	74.2	73.8	73.6	73.2	72.8	72.6	73.0	73.05
77.0	77.4	77'2	76.8	76'6	76.2	76.0	75.8	75.8	75.5	75.2	75.0	75.35
84.0	83.4	82.2	81.6	81.0	80.7	80.5	79.7	79.0	79.0	78.6	78.2	80.87
81.4	81.5	80.4	80.2	80.5	80.0					70.0	$\{-73.0\}$	79.18
76.5	76.0		===		<u> </u>	76.8	76.5	75.8	74.6	73·9 71·0	71,0	74.09
70.0	69.6	75.5	75.0	74.7	74.2	73.8	72.7	72.1	71.5 66.0	65.2	65.2	69.00
68.0	68.0	69.0 67.5	68.6 67.0	68°2 66°6	67.6 66.4	67°0 66°0	66.7	65°0	64.6	64.4	63.6	66.26
68.5	68.2	68.5	67.3	67.1	66.8	66.5	65.4	65.0	64.6	64.1	63.8	66.32
71.0	70.8	$70.\overline{2}$	69.6	69.1	68.2	68.0	65.5	67.0	66.6	66.5	65.6	68.23
72.7	72.6	72.0	71.2	71.1	70.9	00 0	67.4	0, 0				
			'-	'	-	72.0	72.0	71.2	71.3	70.9	70.6}	10 00
77.4	77.0	76.5	76.0	75.5	75.0	74.2	74.0	73.6	73.0	72.2	72.0	74.46
77:5	76.7	76.2	75.7	75.6	$75 \cdot 2$	75.0	74.6	74.2	73.8	73.4	73,2	75.35
75.5	75.2	74.8	74.5	73.6	73.0	73.0	73.0	72.5	72.3	72.0	71.5	73.61
77.4	77:3	77.0	76.5	76.0	75.7	75.4	75.1	75.0	74.6	74.5	74.0	75.35
73.4	73.4	73.2	73.0	73.0	72.9	72.5	71.8	71.4	71.0	71.0	70.6	72.77
1	77.5	77.2	76.6	76.4	76.4		_				70:0}	74.81
76.0	75.7	75.0				74.7	74.0	73.6	73.2	73.2	73.0}	73.80
76.3	76.2	75.0	74.3	74.0	73.5	73.0	72.6	72.0	71.4	71.0	70.6 73.3	74.37
80.0	79.8	76.0 79.6	75.8	75.4	75.0	74.6	74.5	74'5	73.6	73:4 77:7	77.2	77.92
82.0	81.2	80.8	79.0	79.1	78.5	78.5	78.5	78'1 78'0	78:0 77:5	77.3	77.0	79.57
79.2	78.2	77.4	76.8	80'4 76'5	80°0 75°6	79°2	78.5 74.3	78.0	73.2	73.2	72.4	76.38
76:37	76.14	75.60				75.0				$\frac{73.16}{72.16}$	71.76	74.19
- 01	10 14	19 60	75.13	74.79	74.34	73.85	73.37	72.96	72.49	72 10	(1 10	14 19

^b Fifteen minutes late.

	One Scale Di	vision = '00	00087 parts	of the H. F.		NTAL FO n Scale Div		sponding to	1º decrease o	of Temperat	ure, 1°63.	
Mean Göttir gen Time.	0h.	1h.	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8 ^h .	9հ.	10 ^h .	11ħ.
(1		Sc. Div. 573 4	Sc. Div. 562*4	Sc. Div. 557 2	Sc. Div. 560°2	Sc. Div. 547 ° 0	Sc. Div. 563 ° 0	Sc. Div. 572.0	Sc. Div. 575 5	Sc. Div. 591 ° 0	Sc. Div. 586°5	Sc. Div 587 (
2 3 4 5 6 7 8	580°0 571°5 570°0 573°0 531°6 561°8	580.8 569.0 568.0 576.4 558.0 554.0	592.0 564.0 558.2 564.0 557.6 553.5	565.0 561.0 552.2 545.0 549.0 547.0	556.0 553.5 554.2 564.0 556.0 542.5	555.0 556.0 559.2 569.8 556.5 549.8	565.6 562.0 566.4 567.2 560.5 564.0	576.0 571.4 575.8 566.0 577.0 575.5	583.0 576.3 580.0 570.4 562.5 582.5	678.0 571.8 574.2 568.5 572.1 588.5	579°0 576°8 593°6 564°2 577°0 583°3	576 : 6 575 : 6 564 : 6 590 : 6 579 : 6 571 : 6
11 12 13 14 15 16	557°0 582°5 584°0 575°8 576°2 558°8	556°0 578°0 582°2 537°8 576°5 561°0	568.2 572.0 573.6 560.5 552.0 564.5	571 · 2 571 · 2 552 · 0 562 · 5 545 · 0 564 · 6	566.0 566.0 545.2 549.0 537.5 551.0	556.0 a 568.8 566.2 561.8 557.5 c 551.0	553.0 576.4 572.0 572.0 571.2 556.5	562.2 575.8 583.5 581.0 580.0 570.0	566.4 592.8 601.5 589.0 568.0 569.2	573.0 591.2 587.0 593.2 566.5 578.2	574·2 568·6 591·2 585·2 560·0 579·2	571 584 567 583 582 581
17 18 19 20 21 22	579.5 583.4 582.4 589.0 571.4 585.0	581.0 584.2 592.5 582.0 580.0 574.0	575°0 577°0 585°0 577°8 586°0° 577°0	572.4 570.0 574.8 568.5 568.0 565.4	566.6 568.0 579.0 574.0 571.0	554.4 566.2 579.4 586.5 572.5 569.4	555.4 558.5 576.2 583.2 576.5 578.0	568.0 577.2 587.0 588.5 579.2 580.8	578.5 587.5 592.6 596.5 577.3 583.8	586.0 587.2 600.0 596.5 576.2 604.4	591.6 590.5 581.4 591.6 578.8 582.5	591° 583° 586° 589° 595° 581°
23 24 25 26 27 28 29	589.0 582.0 583.8 577.0 576.3 576.2	589°2 582°4 586°5 580°5 578°5 573°2	588.8 578.2 584.5 576.0 576.0 561.0	578.5 571.0 570.8 573.0 572.0 554.5	570.7 562.0 565.8 568.0 567.8 568.5	568.8 563.4 566.5 568.0 566.6 574.0	570.0 573.0 575.0 572.5 569.2 570.0	582.0 573.0 583.8 585.0 587.5 568.2	572.0 580.0 586.5 601.4 592.2 578.1	583.0 589.0 587.5 581.0 590.8 589.6	591 0 594 2 588 0 589 8 614 8 583 5	602: 605: 584: 631: 577: 593:
30		575.6	571.2	566.8	567.0	563.0	561.0	571.0	579.0	579.2	580.4	576
Iourly Mea	ins 575.15	574.26	571.38	563.41	561.37	563.59	568.01	576.82	581.63	583.98	583.73	584
		1 0			ERATURE O				1 0	. 0	1 0	
1 2 3 4 4 5 6 7 8	71.0 73.0 76.5 78.7 76.8	73.0 71.5 73.4 77.0 78.3 77.6 75.5	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	74·4 73·0 75·2 78·5 79·2 77·0 75·0	75·4 73·7 76·0 79·5 80·6 77·4 75·0	76.0 	76.0 75.8 78.5 81.5 81.7 79.4 75.5	76.5 77.0 79.2 82.2 81.8 80.0 76.2	77.0 77.7 79.7 82.6 82.2 81.0 76.5	77·2 78·7 81·0 83·3 82·4 81·5 77·0	77.2 	77.7 79.0 81.3 83.3 82.0 77.0
10 11 12 13	73.0 69.3 70.0 75.0 76.7 73.0	72:3 70:0 70:4 75:0 77:5 73:5	72·4 70·5 70·7 74·8 75·2 74·1	72.5 71.2 71.6 74.8 75.9 75.0	73·4 72·3 73·0 76·2 76·9 76·0	$ \begin{array}{c c} \hline 74.1 \\ 73.0 \\ 74.2 \\ 77.0 \\ 77.3 \\ 77.2 \end{array} $	74.5 73.6 75.3 78.0 77.4 77.5	75.0 74.0 75.8 78.7 77.5 78.2	75.7 74.4 76.4 78.9 78.0 78.7	76.5 74.8 77.3 78.5 78.5 79.6	77.2 75.3 77.8 78.8 78.5 80.0	77: 75: 78: 79: 79: 80:
15 16 17 18 19 20 21 22 22 22 22 22 22 22 22 22 22 22 22	71.5 68.2 65.8 67.5 67.0 70.6	72.0 68.2 66.2 67.4 67.4 70.6	72.5 68.5 66.4 67.2 68.0 70.6	72.8 69.4 66.6 67.0 68.6 70.4	73.6 69.5 66.5 67.2 69.7 70.5	74·4 69·9 67·4 67·4 71·0 71·0	74.6 69.8 67.8 67.5 71.7 71.5	74.6 69.8 68.5 68.0 72.0 71.8	74.8 70.0 69.0 68.4 72.5 72.3	75.0 70.4 69.5 68.4 73.2 72.6	75.3 70.7 69.5 68.6 73.5 72.6	75: 71: 69: 68: 74: 72:
23 24 25 26 27 28 29	68.5 66.6 69.4 69.6 71.0 71.9	69.0 67.0 69.5 70.0 70.8 72.0	69.5 68.0 70.7 70.5 70.8 72.5	70°4 69°4 71°4 72°0 71°0 73°2	71·2 70·7 72·0 72·8 71·5 74·0	72.0 71.4 72.6 74.2 72.4 75.0	72·3 71·8 73·0 75·0 73·0 76·2	72·4 72·4 73·5 75·0 73·6 76·2	72.5 72.7 74.0 75.6 74.6 75.7	72.6 73.8 74.8 75.8 75.6 75.8	72·7 74·0 75·0 75·8 76·0 75·3	73. 74. 74. 75. 75. 75.
$\begin{pmatrix} 30\\31 \end{pmatrix}$		72.5	73.8	74.5	75.4	76.0	76.6	77.5	78.4	78.9	79.2	79.
lourly Me	ans 71.59	71.83	72.08	72.69	73.46	74.28	74.83	75.28	75.74	76.26	76.48	76

^a Fourteen minutes late.

b Five minutes late.

c Ten minutes late.

	One Scale	e Division=	: •000087 pa	arts of the H		IZONTAL ase in Scale		rresponding	to 1º decrea	ase of Temp	erature, 1·65	3.
12h.	13h.	14h.	15h.	16h.	17 ^h .	18h.	19 ^h .	20 ^h •	21h.	22h.	23h.	Daily an Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div. 564 0	Sc. Div.	sc. Div. 568 6	Sc. Div. 568 0	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
577.0	573.0	304 0	303 4	303 0	303 0	567.5	577.4	576.5	580.2	578.8	577.2}	572.00
			550:0	500.0					574.0	568.4	569.0	571.94
572.0	566.2	564.8	570.2	569.0	569.2	570.2	572.0	575.0		571.0	572.0	568.43
565.8	564.0	567.8	571.0	577.5	571.0	567.0	570.0	568.2	568.0			568.42
572.0	574.0	556.5	560.0	563.9	564.2	563.0	567.0	573.0	578.0	577.5	577.2	
565.0	552.7	564.0	567.5	570.0	519.5	567 .7	561.4	557.2	4891	538.4	536.0	558.63
561.2	551.7	562.5	562.0	568.2	566.2	548.0	479'0	547.8	559.5	53518	522 .2	$554^{\circ}25$
	562.2	565.0	562.8	562.4	571.0						—]	566.03
577.6	002 2	000 0	002 0	002 1	0.1.0	561.5	569.0	559.0	566.0	579.2	₅₇₅ ·5}	000 00
	70111	566.8 р	573.0	571.0	571.8	571.5	572.0	577.0	580.0	584.0	581.0	568.65
560.2	564.4								583.0	583.2	583.2	577:57
572.2	578.6	569.5	571.0	564.8	577.2	579.0	589.0	583.2		566.0	579.0	568.74
5 70°0 -	564.0	564.0	549.0	555.5	556.0	567.0	561.2	552.0	560*2			563.64
571.0	569.5	568.0	551.2	560.8	543.0	542.2	497.4	559.4	563.2	572.8	578.0	
572.4	569.2	575.0	540.3	552.8	554.5	555.2	563°5	555.0	578.2	560.6	550.8	562.20
610.5	564.4	555.0	564.0	560.2	551.0						— <u>}</u>	564.23
	JUL 1	1 330 0	1			552.8	545.0	558.9	560.0	561.0	574.0	
70.0	505.2	505.4	584.8	565.0	573.0	576.6	582.2	582.0	580.0	576.0	580.2	576.12
76.6	565.5	585.4	ı					585.0	583.8	582.0	575.4	577:82
81'2	581.0	565.6	564.0	577.2	570.0	584.5	585 .2		I	588.2	589.2	585 26
582.2	581.2	582.5	574.0	585.0	586.2	588.2	589.2	596.8	587:0			585.25
80.5	586.0	586.2	587.2	588.0	588*8	588.4	587.8	588.4	585.5	586.0	570.5	
575.2	582.2	581.0	583.8	585.5	583.0	585.0	582.8	582.0	579'9	580.0	580.0	579.70
82.2	572.5	577.0	579.5	579.0	579.0						— \ \ \	580:36
02 0	012 0	0110	013 0	0.50	0.00	586.0	585.0	584.8	583.8	590.0	582.2 }	
			70010	504.0	774:0			580.6	582.2	578.0	566.5	578.60
577.2	568.0	568.0	569.0	564.0	574.0	592.8	581.0			583.2	585.0	577.79
88.0	570.5	566.2	557.0	563.2	578.7	578.7	582.5	581.5	578.6		580.0	578 19
586.0	581.6	578.0	577.8	568.8	563 ·2	579.4	568 ·2	577.8	577.5	575 4		
64.0	565.0	569.0	570.0	572.8	582.5	581.5	590.6	585.0	587.0	571*2	582.0	580.18
60.4		578.0	587.5	561.0	564.0	571.0	575.0	567.4	579.6	567.4	567.8	575°9 4
	574.0					011 0	0.00				_ n i	574.86
573.0	574'5	575.0	572.0	577.0	582.8	507:0	~ ~ 0:0	584.2	580.0	576.0	573.0}	3/4 00
					_	567.2	572.2			576.2	575.5	572.84
572.0	571.0	572.0	568.0	569.0	572.2	573.0	573.2	574.4	580.5	370 2		
574 °83	570.27	570.26	568.65	569.24	586.46	571.73	568.42	573.55	573.25	573:34	572.41	572.61
				TEM	IPERATURI				0		1 0))	0
77.5	77.0	76°1	75°7	75°.7	75°5	74.3	0	•				75.06
11 3	77.0	76.1	15 1	10 1	10 0	143	72:0	73.2	73.0	72 ·2	71.5}	75 00
			-				73.6			73.8	73.2	7 5.64
78.7	78.5	77.6	77.2	76.8	76.4	75.8	75.0	74.2	74.2		76.9	78.53
82.0	81.6	81.2	80.2	80.5	79.5	79.0	78.7	78.2	78.0	77.8		81.3
83.8	83.2	83.4	83.0	82.7	82.2	82.1	81.4	81.0	80.2	80.0	80.2	
82.6	82.6	82.4	81.8	81.2	80.6	79.8	79.2	78.7	78.0	77.6	77.3	80.48
81.8		1	80.0	79.6	79.0	78.8	78.0	77.8	77.2	76.6	76.2	78.98
77.0	81.2	80.5				'''					— i	75.28
110	76.5	76.2	76.5	75.8	75.6	70:0	72:0	73.0	72.8	72.6	$\{-\frac{1}{72\cdot 0}\}$	
	<u> </u>	l —			-	73.6	73.6		71.2	70.4	69.2	73.88
77.4	77.3	75.8	74.4	73.8	73.0	72.5	72.2	71.7		70.2	70.2	72.70
75.5	75.2	74.2	73.5	73.0	72.8	72.5	71.4	71.1	71.0		$74\cdot 2$	74.9
78.0	77.4	76.6	76.5	76.0	75.7	75.4	75.0	74.7	74.5	74.4		77.04
79.0	79.0	78.5	78.0	77.6	77.5	76.7	76.4	75.8	75.4	75.0	75.4	
79.0	78.8	78.0	77.8	77.6	76.6	76.0	75.0	75.0	74.2	74.0	73.4	76.8
80.4					78.2						- - }	76.4
. · ·	80.5	79.6	79.0	78.7	i	73.2	72.8	72.5	72.2	72.0	71.5	
7:.0					70:0				69.8	69.2	68.8	72.8
75.2	74.8	74.0	73.2	72.5	72.0	71.5	70.8	70.2		67.0	66.6	69:20
71.0	70.9	70.2	70.0	69.3	68.7	68.4	67.8	67.8	67.6		67.6	68.08
69.2	69.0	69.0	68.6	68.6	68.5	68.2	68.0	67.7	67.9	68.0		
68.8	68.8	68.8	68.7	68.6	68.4	68.4	68.9	68.0	67.8	67.5	67.2	68.0
74.0	74.0	73.6	73.3	73.3	72.6	72.4	72.0	71.7	71.2	71.5	71.0	71.6
72.5					71.6	ł		_			`	71:26
	72.4	72.0	71.9	71.7	I .	71.0	70.9	70.4	70.0	69.5	69.0}	
70.4									68.4	67.7	67.2	70.88
73.4	73.2	72.8	72.0	71.4	70.5	70.0	69.2	69.0	70.6	70.4	69.8	71.58
74.5	74.0	73.2	73.0	72.6	72.2	71.8	71.5	71.0				72.36
74.7	74.0	73.8	73.6	72.8	72.2	72.0	71.2	71.0	70.6	70.2	70.0	
75.3	75.0	74.6	74.2	73.8	73.5	72.6	72.1	72.0	71.8	71.7	71.5	73:31
75.8	75.6	75.6	75.4	75.0	74.5	74.1	74.0	73.7	$73^{\circ}2$	73.0	72.6	73.69
						17.1						71.11
	74.8	74.0	73.6	73.2	73.0		74.4	74.0	73.6	73.2	73·0}	74.1
75.4	l			ı	1	74.7	74 4	1 /4 U	100	1 10 4		
75°4											74.3	76.41
	78.3	77.7	77.4	77.0	76.7	76.3	76.0.	75.6	$\frac{75.2}{72.71}$	$\frac{75.0}{72.34}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	76.4

	ł				_		l					101	
Mean Göt gen Tim	e. }	O ^h •	1 ^h .	2 ^h .	3h.	4 ^h .	5 ^h .	6 ^h .	7h.	8h.	9h.	10h.	11h.
	1 2 3 4 5	Sc. Div. 576°0 574°5 572°0 528°0 575°2	sc. Div. 572 2 570 4 567 0 544 2 537 8	Sc. Div. 566°0 561°0 559°0 564°2 555°4	sc. Div. 569°6 555°4 552°0 551°4 575°2	sc. Div. 564'0 558'5 547'3 547'0 522'5	Sc. Div. 566°5 562°2 552°0 541°4 544°0	Sc. Div. 571°5 568°2 561°8 546°2 538°0	Sc. Div. 571 ° 0 572 ° 2 573 ° 2 558 ° 0 548 ° 0	Sc. Div. 576 ° 0 575 ° 2 581 ° 0 571 ° 4 567 ° 0	\$c. Div. 576°5 583°0 590°2 579°4 624°0	Sc. Div. 576 0 577 0 589 6 576 3 585 0	Sc. Div 570 7 573 2 585 2 579 0 548 0
1 1 1	6 7 8 9 0 1 2	575.2 565.8 574.0 584.0 525.8 572.0	574.0 571.5 577.0 585.2 578.8 574.8	568°5 551°0 569°3 583°0 556°4 575°0	560°8 547°5 560°0 574°4 571°0 541°0	556.0 532.5 565.2 568.5 568.0 544.0	552.0 526.0 561.4 568.2 543.0 557.0	554.0 548.5 563.0 572.2 535.0 567.0	564.0 557.0 568.8 589.0 580.0 571.0	569°2 575°2 577°2 592°0 578°0 583°2	573°0 585°0 587°4 594°8 594°0 576°0	573 · 2 573 · 2 585 · 8 592 · 0 569 · 0 578 · 8	568 4 568 2 590 0 587 0 582 0 580 0
SEPTEMBE	3 4 5 6 7 8 9	575°2 575°0 592°0 595°4 606°2 603°0	551.0 570.0 586.2 595.0 597.5 596.5	550°0 569°5 579°8 594°2 596°6 595°4	549.0 558.2 581.2 587.0 591.2 591.0	551.0 561.9 583.6 574.0 586.6 578.0	549.0 569.2 585.6 572.5 582.9 575.0	557.4 569.6 586.6 580.0 587.0 583.0	566.4 575.2 586.5 584.2 594.0 581.2	576 · 2 583 · 0 592 · 0 595 · 0 601 · 0 594 · 0	574.5 591.6 597.0 601.0 606.5 590.2	576°8 583°0 594°0 596°2 602°0 588°0	568*4 576*4 592*7 598*0 600*0 593*2
2 2 2 2 2 2 2 2	0 1 2 3 4 5 6	600°0 514°4 596°6 588°9 598°4 606°4	596.5 488.7 592.8 585.8 591.2 599.4	586.5 456.1 587.5 573.9 589.4 594.4	576.0 467.7 577.2 566.2 580.9 591.6	572·2 516·8 568·2 564·4 579·4 578·2	577.0 525.9 572.0 563.8 578.4 583.6	583.6 545.4 574.0 568.5 595.9 583.8	594.2 596.1 581.4 574.4 593.8 595.2	606.4 603.5 593.0 586.4 601.4 603.2	586.6 626.3 589.0 603.4 604.2 605.2	590°5 639°0 590°4 593°4 606°4 605°9	580 ° 0 612 ° 4 589 ° 4 606 ° 2 614 ° 2
$\begin{vmatrix} 2\\2 \end{vmatrix}$	7 8 9 80	611.8 611.8 608.6	608.0 608.0	608.4 604.0 600.6	602.6 601.4 594.0	598'8 596'8 590'6	598.8 596.0 588.8	600°0 600°1 590°6	608.6 600.6 598.1	603.6 603.6 603.6	608.6 606.6 606.9	610.8 601.1 617.6	612°6 606°6 616°8
Iourly M	[eans	581.01	577.93	572.89	568.21	564.38	565.08	570.42	580.08	588.55	594.64	591.19	588*4
		1			TEMP	ERATURE O	F THE BIFI	LAR MAGN	ET.				1
	1 2 3 4 5	73.6 76.5 77.2 74.8 75.8	73°8 76°0 77°0 75°3 76°4	74.4 76.0 77.0 75.7 76.5	75.4 77.0 76.7 76.2 77.5	76°·4 77°·6 76°·7 76°·2 78°·0	77°3 78°3 77°0 76°5 78°5	78·8 78·8 77·0 76·8 78·5	79° 5 79° 7 77° 2 77° 0 78° 2	80°0 80°5 77°2 77°5 78°4	80°4 81°0 77°2 78°0 78°5	80°6 80°2 77°0 78°2 78°8	80°7 81°0 76°8 78°0 78°7
	6 7 8 9 0 1 1 1 2	74.2 75.0 67.2 66.8 68.5 72.5	75°0 75°4 67°4 66°8 69°0 73°4	76.0 75.4 68.0 67.5 69.6 74.4	77.5 75.9 68.6 68.6 70.6 75.5	78°3 75°8 69°0 69°0 71°4 76°4	78 '9 76 '0 69 '6 69 '6 72 '2 77 '4	79.4 76.1 69.5 69.6 73.0 78.2	80.6 76.1 69.4 69.8 73.6 76.8	81.6 76.2 69.4 69.9 74.4 76.4	81.9 . 76.0 . 69.5 . 70.3 . 75.2 . 75.8	82:1 75:6 69:6 70:5 75:0 75:6	82.0 75.0 69.6 70.7 75.4 75.8
SEPTEMBE	13 14 15 16 17 18	74.2 73.0 66.0 65.8 64.1 64.2	74.2 72.5 66.0 65.6 64.0 64.0	74.5 73.0 66.2 65.4 64.0 64.4	75·2 73·2 67·0 65·2 64·8 65·5	76.6 73.0 67.7 65.3 65.9 66.3	77.8 72.8 68.1 65.5 66.5 67.5	78.2 72.2 68.2 65.7 67.0 68.4	78.8 72.0 68.4 66.0 67.5 69.0	79.4 72.0 68.6 66.4 68.0 69.7	79.8 72.4 69.0 66.4 68.5 70.4	79.7 72.4 69.0 66.4 68.6 71.0	79.6 72.4 69.4 66.0 68.8 71.4
6 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	20 21 22 23 24 25 26	65.5 61.4 61.4 68.0 63.8 60.0	65.0 61.6 61.4 68.0 63.0 60.0	64.5 61.7 62.2 68.0 63.0 60.5	64.2 63.0 62.8 68.0 62.6 61.4	65°1 63°5 64°0 68°0 62°4 62°0	64.5 63.8 65.2 68.1 62.4 62.7	64.8 64.3 67.4 68.3 62.4 63.0	65.2 64.5 67.5 68.4 62.4 63.4	65.4 65.2 68.2 68.2 62.4 63.2	66.0 66.0 68.9 68.2 62.6 63.5	66°4 66°5 69°4 68°0 62°6 63°5	66° 5 66° 5 70° 2 67° 7 62° 0 63° 5
	27 28 29 30	56.8 60.5 63.0	56.4 60.5 63.0	56.8 60.8 63.5	57.4 62.4 64.4	58°1 62°4 65°5	59.0 63.6 65.9	59.4 64.4 66.4	59.8 64.6 66.9	60°4 65°2 67°7	61.2 65.8 68.2	62.0 65.8 68.5	62:2 65:6 68:0
	- 1		1	1	1		·						71

	One Scal	e Division =	= ·cooos7]	parts of the			FORCE. Division, c	orresponding	g to 1° decre	ase of Temp	perature, 1°6	3
12h.	13 ^h .	14 ^h .	15 ^h .	16h.	17h.	18h.	19h.	20h.	21h.	22h.	23 ^h .	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
571.4	567.2	571.2	573.2	571.6	567.8	569.2	574.0	569.0	568.4	571.2	574.5	571.03
571'2	582.4	574.0	575.6	574.8	576'1	574.6	571.0	572.0	572.0	571.2	572.0	571.57
585.6	583.0	583.2	585.0	591.0	581.0	591.0	572.0	546.0	556.0	542.0	536 .3	570.10
560'4	566.0	558.0	567.0	564.3	573.0	568.0	574.8	546.2	530.0	546.2	569.4	558.95
562.0	543 2	554.5	557.6	557.0	558.2		 —	_	[— 1	561.95
						570.6	573.8	572 ·2	572.0	572.2	573.4}	
568.0	567.0	564.8	568.2	562.4	565.0	557.8	549.2	546.4	550.0	558.8	558.0	562.66
572.0	571.8	575.0	578.0	577.8	579.0	581.0	576.6	579.0	579.0	576.9	573.0	567.52
585.8	579.0	582.2	584.0	585.0	584.0	583.6	583.0	581.5	581.0	583.0	584.2	578.10
580.0	577.8	586.0	a	586.5	590.0	584.5	588.0	569.0	568.2	566.0	596.8	581.87
578.0	578.0	580.0	560.2	541.6	564.8	563.2	570.5	560.0	531.4	579.4	570.8	564.95
576.4	576.2	573.0	581.8	580.0	580.2		0,00	000 0	_		1 1	
	J J J	0.00				577:2ь	578.5	534.0	566.0	577.5	574.0}	570.61
566.0	565 .2	566.8	573.5	566.4	563.0	574.0	567.0	558.9	566.6	555.8	585.0	564.73
581.0	583.4	583.8	585.8	586.4	587.0	587.2	587.5	587.5	586.2	589.2	586.2	579.77
589·9	592.8	590.0	584.0	589.3	583.0	586.2	592.0		587.4	582°2	599.8	588.55
			595.0	595°2°	597.0			591.2		602.4	993.9	592.54
594 0	579.0	591.2				597.2	600.0	597.0	596.6			596.62
597.2	594.6	595.8	595.8	601.0	593.8	594.8	595.2	597.0	598.6	600.2	603.2	
592.0	592.8	591.0	590.0	591.4	593.0	500.0					$\frac{-}{596\cdot 2}\}$	591.01
						593.0	598.8	592.0	590.0	595.5		
605.2	586.0	591.0	601.0	589.0	568.0	610.0	541.2	548.5	533.0	506.0	571.8	580.10
558.2	567.5	564.2	560.0	558.0	561.2	565.0	581.6	587.0	593.7	594.0	595.4	560.26
587.6	590.0	591.2	593.4	571.4	584.4	586.0	593.2	587.8	581.4	587.4	590.4	586.61
596.7	589.4	592.6	595.6	594.2	596.6	596.0	596.6	596.0	598.4	601.6	599.9	588.00
607.9	604.6	598.4	606.2	600.4	602.6	602.4	598.8	598.4	585.4	603.4	607.4	597.56
596.2	609.4	609.2	607.5	605'4	606.4						II	
_						611.9	510.4	611.9	609.4	612.4	616.4	602.86
89.4	601.9	610.6	611.1	608.1	610.8	610.6	610.8	612.8	615.3	614.0	613.2	607.72
507.6	606.4	609.4	607.6	608.6	603.6	602.8				609.8	608.6	605.24
9.00							605.8	608.6	609.8		603.4	599.47
	593.6	594.0	603.6	612.1	600.6	590.8	583.6	591.0	590.4	599.6	000 4	
283.88	582.63	583.89	585.63	583.46	583.48	585.73	583.61	578.46	577.56	580.70	587:06	580.78
				TE	MPERATUR	E OF THE	BIFILAR MA	GNET.				
80.6	79°8	79.4	79.2	78.6	78.3	78.0	77.5	77.2	77°0	76 .8	76.7	77.92
81.0	80.6	80.4	80.0	79.5	79.0				78.2	78.0	77.5	78.86
76.7					79.0	78.8	78.7	78.4				76.21
78.0	76.5	76.5	76.4	76.5	76.5	76.2	75.5	75.5	75.5	75.5	75.0	
	77.8	77.5	77.5	77.4	77.0	77.0	76.5	76.2	76.4	76.2	76.0	76.83
78.2	78.2	78'1	77.7	77.0	76.8						$\frac{-}{74.5}$	77:13
91:0						75.5	75.5	75.2	75.0	75.0	74:55	HOLOM
81.8	81.3	81.0	80.2	79.8	79.4	79.0	78.0	77.0	76.0	76.0	75.5	78.87
74'4	74.0	73.6	73.0	72.3	71.5	71.0	70.6	70.0	69.0	68.6	68.0	73.52
69.6	69.0	69.0	68.2	68.3	68.0	67.8	67.4	67.2	67.0	67.0	66.8	68.43
70.9	70.5	70.5		70.0	69.2	69.3	69.0	69.0	68.8	68.5	68.5	69.29
75.2	75.2	75.0	74.7	74.7	74.2	74.2	73.6	73.2	73.2	73.0	72.8	73.22
75.8	76.0	75.6	75.2	75.0	74.6							75.49
- 1						75.7	75.7	75.2	75.3	75.0	$\frac{-}{74 \cdot 2}$	
80.0	80.0	79.8	79.5	79.2	78.6	78.3	77.5	77.0	75.7	74.2	73.5	77.57
72.6	71.2	71.5	70.8	70.2	69.2	69.0	68.2	68.1	67.5	67.0	66.8	71.00
69.0	68.2	68'4	68.0	68.0	67.7	67·5		00 1	66.2	66.5	65.8	67.63
66.0	65.6						67.0	67.0		64.4	64.2	65.39
68.6	60.2	65.6	65.3	65.0	65.0	64.8	64.6	64.6	64.5		64.5	
71.3	68.5	68.0	67.6	67:0	66'8	66.2	65.6	65.2	65.1	64.8		66.20
	71.2	70.6	70.1	69.9	69.4				-		66.4	68.38
66.8			_	_		68.4	68.5	68.3	68.2	67.4	00 4 3	
66.4	66.3	65.7	65.4	64.8	64.4	64.2	63.2	63.0	62.6	62.2	62.0	64.75
66.4	66.1	66.0	65.5	65.0	64.5	64.0	63.2	63.0	62.8	62.8	62.0	64.15
70.5	70.2	70.0	69.7	69.5	69.6	69.6	69.4	69.0	69.0	69.0	68.4	67.59
67:3	67.2	66.6	66.6	66.4	66.3	65.8	65.4	65.0	64.8	64.5	64.2	66.96
65.0	62.0	62.0	61.9	61.6	61.4	61.5	61.0	60.8	60.2	60.4	60.4	61.95
63.2	63.4	63.0	62.6	62.6	62.2	; <u> </u>					1	
_		_				5 7 .5	58.0	58.0	57.5	57:3	57.0}	61.22
62.0	61.8	61.4	61.5	61.0	60.8	60.2	60.2	60.7	60.6	60.6	60.6	60.02
65.2	65.2	65.0	64.6							63.5	63.0	63.77
67.8	67.6	67.4		64.4	64.0	63.8	63.6	63.4	63.1		65.0	66.16
			67.2	67.0	66.8	66.4	66.0	65.2	65.5	65.0		
71.61	71.32	71.05	70.75	70.42	70.07	69.60	69.24	68.98	68.65	68.42	68.02	69:97

	o	ne Scale Di	vision = ·0	00087 parts	of the H. F.		NTAL FO		sponding to	1° decrease	of Temperat	ure, 1°63.	
Mean G gen T	öttin- ime. }	Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h •	6 ^h •	7h.	8h.	9h.	10 ^h .	11h.
	1 2 3	Sc. Div. 598*0 598*0 608*2	Sc. Div. 594 ° 0 595 ° 0 601 ° 2	Sc. Div. 588 ° 0 585 ° 0 594 ° 0	Sc. Div. 576°0 586°8 587°5	Sc. Div. 583°0 582°8 587°2	Sc. Div. 577 5 581 6 589 8	Sc. Div. 589°0 580°6 597°3	Sc. Div. 585 2 593 6 594 6	Sc. Div. 587.6 593.2 605.0	Sc. Div. 590°2 602°0 610°6	Sc. Div. 593 * 5 601 * 5 612 * 2	Sc. Div. 590.6 596.2 607.0
	4 5 6 7 8 9	608.0 605.2 598.0 557.5 578.0 582.0	604.2 601.0 599.0 513.0 583.4 574.0	594·2 596·0 591·2 546·0 585·0 558·0	593.0 586.9 570.5 538.1 579.8 555.2	588 · 8 583 · 5 556 · 0 553 · 0 567 · 2 572 · 8	585 · 2 578 · 8 559 · 0 558 · 0 562 · 4 583 · 0	590°2 587°5 558°0 559°2 565°5 583°2	594.0 588.0 567.0 565.8 567.0 584.4	596·2 594·1 584·5 574·4 575·0 584·6	600°5 601°0 591°0 585°5 573°0 594°0	603 ² 601 ⁰ 588 ⁰ 582 ⁴ 587 ⁵ 599 ⁰	603.0 602.2 588.8 582.0 589.0 601.0
OCTOBER.	11 12 13 14 15 16 17	611.5 601.4 611.5 614.0 614.5 612.8	596.0 599.0 606.2 611.2 609.4 610.0	593.0 596.7 603.0 605.8 605.4 606.0	599.0 593.5 598.7 599.8 596.8 604.0	595.0 587.0 598.8 595.6 596.2 601.0	593°0°a 584°5 599°2 594°5 600°2 602°0	593.0 585.0 603.2 596.8 602.0 605.0	590.0 595.2 606.2 603.0 609.0 611.7	587.9 599.8 608.4 606.0 607.8 616.0	595.0 603.2 605.8 606.0 610.0 626.0	600°0 599°2 603°8 609°5 605°4 620°0	593 '8 601 '4 603 '1 614 '5 605 '0 618 '4
00	18 19 20 21 22 23 24	629°0 620°2 614°0 620°2 624°0 625°0	628.0 624.6 612.2 618.2 621.5 625.4	622.5 611.0 613.7 599.0 612.2 618.0	619.0 603.2 611.0 591.0 609.0 611.0	611.0 b 603.3 608.5 584.0 605.0 610.5	604.0 594.0 602.4 584.3 603.5 611.0	600°0 601°2 609°0 587°0 607°7 617°0	604.2 605.5 608.2 585.6 610.0 619.0	613.0 605.4 619.8 595.3 619.0 606.2	630°0 614°2 613°2 618°8 623°5 619°2	629°0 613°4 629°0 614°2 622°2 621°2	610.5 620.6 613.0 613.5 628.0 625.8
No	25 26 27 28 29 30 31	626.5 617.0 620.2 622.0 622.0 617.5	623°0 616°2 618°5 614°0 617°0 624°0	622.0 610.6 615.0 619.0 613.8 621.0	613.8 603.2 605.8 613.5 622.0 618.2	609.0 599.0 601.5 608.4 612.5 616.0	604 ² 593 ⁸ 600 ⁰ 606 ⁰ 608 ⁰ 617 ²	603.8 594.2 599.0 604.0 608.1 615.0	610°4 600°2 601°0 606°0 608°8 620°2	620°0 603°4 613°2 606°2 614°0 620°0	612.4 606.2 614.0 609.0 616.2 620.8	614.8 606.8 618.8 613.4 620.0 627.0	616°2 612°0 625°0 619°3 620°0 629°0
	Means	609.49	605.16	600.93	595.79	593.51	591.74	594.13	597.55	602.07	607.09	608.74	608'48
						ERATURE O						1 0	1 0
	1 2 3	64.2 59.0 55.7	63°8 59°0 55°2	63°5 58°5 56°0	63°0 58°5 57°8	63°0 58°4 58°4	62°.8 58°.5 58°.8	63°0 58°8 59°5	60.0 59.3 60.0	63°0 59°4 60°0	60.0 60.4	63.0 60.2 61.1	62°6 61°1 61°2
	4 5 6 7 8 9	56.4 58.4 61.0 66.0 64.4 59.0	56.2 58.4 61.1 66.0 64.2 58.5	56.4 59.0 62.0 66.0 64.0 58.2	58.0 60.1 63.5 66.2 64.8 58.0	58.4 60.9 64.4 66.4 66.2 58.1	59.6 62.1 65.4 66.8 67.0 58.5	60°5 62°5 65°6 67°0 67°4 58°7	61.2 63.5 66.4 67.0 67.5 59.0	61.4 63.9 66.7 66.6 67.0 59.2	62.9 64.5 67.2 66.6 66.5 59.6	63.5 64.7 67.5 66.6 65.7 60.2	64.0 64.5 67.7 66.0 64.9 60.5
OCTOBER.	11 12 13 14 15 16 17	56.8 61.8 55.9 56.8 56.0 55.8	57·2 61·6 55·5 56·5 55·6 55·1	58·1 61·4 56·0 56·6 55·6 54·8	58.8 61.0 56.7 57.0 55.6 54.5	59.9 60.6 57.0 58.0 56.3 54.3	60.7 60.8 57.6 58.2 57.1 54.6	61.0 60.8 58.0 58.4 57.5 55.0	62.0 60.4 58.3 58.5 58.1 55.0	62.4 59.7 58.4 58.4 58.4 55.0	63°2 59°0 58°8 59°0 58°6 55°1	63°5 58°6 59°0 59°4 59°3 55°0	63.4 58.2 58.7 59.0 59.5 54.3
	18 19 20 21 22 23 24	48:3 52:6 51:0 54:0 48:2 50:5	48.2 52.5 51.2 53.6 47.8 50.5	48.7 52.5 51.0 52.7 47.2 50.4	50°0 52°3 50°6 53°0 46°8 51°0	51.2 53.0 51.7 53.0 47.3 52.3	52.0 53.8 52.4 53.0 47.8 52.6	52.5 53.4 52.9 52.8 48.4 53.0	52.8 55.0 53.4 52.6 49.2 53.5	53°0 55°2 53°3 52°4 49°3 53°6	53.5 54.8 53.8 52.1 50.0 54.2	54.2 54.8 53.5 52.1 51.0 54.7	53.6 54.5 53.7 51.9 51.3 54.8
	25	49.6	50°0 57°4	50.0 57.0	50°2 56°5 52°4	50.8 56.6 52.0	51'8 57'4 52'2	53.0 57.8 52.2	54°2 58°0 52°5	54.6 58.2 53.8	55°5 58°5 54°0	55°8 58°3 54°5	54.6 57.3 54.5
No	26 27 28 29 30 31	57.4 52.8 52.5 51.4 49.0	52.4 51.5 51.2 48.8	52.6 51.1 50.6 48.5	51.7 50.4 49.0	52.5 50.5 49.0	53°2 51°0 49°0	53.7 51.5 48.7	54.0 51.7 48.5	54°2 52°0 48°5	54.6 52.0 48.2	54.6 52.5 48.2	54.6 51.6 48.1

a Twenty-five minutes late.

_		O-a Saala	Di-i-i	- *000007			IZONTAL			- 40 10 Jane	age of Tom	omotuwa 1°6	3
	12h.	13h.	14h.	15h.	arts of the l	1. F. Incre	18h.	19h.	20h.	21h.	22h.	23h.	Daily and Monthly
				 						<u> </u>		6 8	Means.
	Sc. Div. 593 0	Sc. Div. 602.5	Sc. Div. 601.8	Sc. Div. 598 0	Sc. Div. 599.0	Sc. Div. 601.0	8c. Div. 602°0	Sc. Div. 604'2	Sc. Div. 600°0	Sc. Div. 601'0	Sc. Div. 605 0	Sc. Div. 583 5	593 48
	592.0	568.8	576'1	569.3	575.0	572.0	570.0	562.6	575.5	586.0	589.0	590.8	584°3 1
	608.0	607.7	607.0	604.0	604.0	595.0	_					610.0}	602.68
	C01:0	599.5	599.0	599.2		500:4	605.0	607°2 600°8	605.6 602.4	603.8	607:3 605:5	605.0	598.90
	601°0 576°4	593.2	594°0	594.2	597.8 592.6	599 . 4	599°8 581°2	591.2	594.1	599.0	596.6	600.0	593.00
	571.2	571.4	545.5	529.0	535.0	474.0	476.2	539.0	537.4	545.0	583.0	586.2	560.17
	569.4	576.2	579.0	580.0	588'0	588.0	574.0	566.2	579.0	590.0	588.0	588.6	570.07
	574°2 601°0	567.0 603.0	565.0 602.2	547.5 604.0	557.8 600.2	553.5	534.2	547.2	530.0	558.4	562.8	591.0	566.74
	_	_		- 004 0		602.0	600.2	602.8	582.2	585.0	611.6	606.0}	590.20
	596.6	595.8	592 . 2	601.2	599.0	599.2	595.8	600.8	598.8	601.4	601.0	605.0	597.26
	594.2	591.8	595.6	602.0	598.2	601.2	601.5	605.0	605.0	605 '4 610 ' 0	607°0 609°2	607:0 613:0	598 ·33
	607 . 2	604°0	606.2 599.0	607°2 595°0	607°0 625°0	606 . 2 584 . 0	607°0 593°5	607°5 599°0	610°0	610.0	610.5	610.2	603.75
	606.0	604.0	609.0	606.2	604.0	604.5	605.2	599.2	602.8	606.2	608.0	613.0	605.40
	615.8	615.0	616.0	618.2	618.2	620.0						630.0}	616.67
i	603.8	603.6	605.8	596·5	600:0	600.8	626'4 605'0	625.8 609.0	627°2 610°4	626 . 2 612.0	$628.4 \\ 617.2$	617.0	612.05
	609.2	613.8	614.0	615.0	608°0	613.8	613.0	616.0	617.0	619.0	618.0	611.2	612:11
	605.0	619.0	619.0	604.2	590.0	596.0	611.0	610.0	614.2	610.4	594.6	620.6	610.35
	616.5	617.0	618.0	619.0	610.0	615.2	612.3	615.4	617.5	604'2	610°0 623°2	616°4 624°0	607.61 618.09
1	628°2	625.0 611.6	623 · 8 606 · 4	622.2 636.0	620°0 616°2	616.2 610.1	613.0	614.0	617.2	621.8	023 4 —	. 11	
	_	-			010 2		621.2	621.0	620.0	620.0	626.0	$\frac{-}{627\cdot0}$	618*26
	620.0	620.2	620.4	623.0	615.5	614.4	617.0	616.0	615.0	612.0	614.0	614.8	615.77
	612.0	616.0	611.8	612.5	614.0	613.0	617.0	616.2	616.0	615.6 620.0	$616.3 \\ 622.2$	619.6 624.6	610.11 614.88
İ	619.0	623.0 622.8	$614.0 \\ 621.2$	620°0	615.8 616.2	616'0 617'4	613'8 614'4	$\begin{array}{c} 620 \cdot 0 \\ 618 \cdot 2 \end{array}$	614 . 2 622.0	622.2	622.8	622.0	615.74
	621.5	616.8	607.2	602.0	608.6	615.0	616.0	620.0	621.5	620.0	620.0	626.0	615.70
	632.8	630.2	631.2	629'9	630.2	630.0	620.5	616.0	622.0	625.0	624.0	$\{624.8\}$	623.45
	604.36	604.26	602.99	602.03	602.20	598.21	598.04	601.87	602:30	605.13	608.18	610.65	602.27
Ì					ТЕ	MPERATUR	E OF THE	BIFILAR M.	AGNET.				
-	62.4	62°1	61°8	6Î 5	61.0	60°5	60°0	59.7	59°7	59°4	59°0	59°0	61.8 3
	61.0	60.8	60.2	59.2	59.4	58.6	58.5	57.5	57.1	57.0	56.2	56.2	58.89
	60.7	60.2	60.0	60.0	59.8	59.5	_		<u> </u>	-	50.7	56.4}	58.52
l	64.0	63.2	63.0	62.7	60:0	61:0	57.0	56.7	56.8 60.3	56.7 60.1	56.7 59.7	59.0	60.71
1	64.0	63.7	63.2	63 ·2	$\begin{array}{c} 62.2 \\ 63.2 \end{array}$	63.0 61.8	61.5 62.6	60.8	62.0	61.6	61.2	61.2	62*26
į	67.5	67.3	67.2	67.5	67.4	67.1	67.1	67.0	66.9	66.7	66.2	66.0	65.95
	65.6 64.0	65.2	65.1	65.2	65.0	64.8	64.8	64.2	64.5	64.5	64.5	64.5 59.5	$\begin{array}{c} 65.65 \\ 64.02 \end{array}$
i	60.5	63°5 60°2	63°1 59°4	63.0	63.0 58.8	62.6 58.8	62.0	62.0	61.7	61.2	61.0	4 1	
		- 1		59°4 —	-		56°5	56.6	56.6	56.8	57.0	56.9	58.53
	63.2	63.2	63.0	62.8	62.6	62.6	62.6	62.5	62.0	62.0	61.8	61.6	61.54 58.51
:	58·1	57°3 58°1	57.0	56.6	56.7	56.6	56°5	56.2	56.5 56.6	56.6 57.0	56°2 57°0	56.6 56.6	57·32
1	58.8	58°4	57.8 58.0	57°5 57°5	57°2 57°5	56.8 57.0	56°5 56°8	56.6 56.6	56.6	56.4	56.5	56.0	57.57
	60.0	60.2	60.2	60.6	60.2	60.3	90.0	59.2	58.8	58.2	57.6	56.6	58*34
	53.8	54.0	53.7	53.4	53.0	52.6	40.4		40.1	48.0	48.0	48.0}	52.82
	53.6	53.4	53.2	53.0	53.0	52.7	48°4 52°7	48°2 52°5	48°1 52°2	52.4	52.4	52.6	52.15
1	54.0	53.2	53.5	53.7	52.5	52.4	52.1	52.0	52.0	52.0	51.6	51.4	53.07
	54.0	54.1	54.5	55° 0	54.7	54.3	54.0	53.7	54.0	54.0	54.2	54.2 48.0	53°30 51°18
	51.1	51.3	50°9	50.6	50.4	50.0	49.6 51.0	49°2 50°6	48.6 50.3	47.8 50.3	48.0 50.2	50.0	49.75
!	54.6	54.4	54.5	51°4 53°6	51.0 53.4	51.0 53.0	<u>—</u>					49.5}	52.22
1	55°3			-			50.0	50.0	49.8	49.8	50.0	49.5 } 57.3	54.38
Mary Walter	57.0	55°5 57°2	55°6 56°5	56°0	56.0	56.0	56.0	56.5 54.6	56.8 54.4	57°0 54°2	57°1 54°0	53.4	56°48
	54.4	54.0	53.2	56°7 52°7	56°4 52°7	55.7 52.7	55°0 52°2	52.2	52.2	52.0	52.6	52.2	52.89
	51.6	53.7	53.7	53.4	53.5	53.0	53.0	53.0	52.0	51.8	51.8	51.2	53.00
1	48.0	51.6 48.0	51.6 48.0	51°0 47°9	50.6	50.4	50.2	50.0	49.8	49.8	49.5	49.2	50.90
			-		47.9	47.7	50.0	50.2	51.0	51.7	52.0	$\begin{bmatrix} \overline{52\cdot3} \end{bmatrix}$	49.10
	57.78	57.62	57.41	57.20	57:00	56.72	56.16	55.97	55.83	55.75	55.66	55.36	56.70

Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carrell Carr	621.8 600.0 603.4 607.0 609.2 614.4 607.5 603.0 605.2 610.4 611.0 613.0 609.2 610.4 611.0 613.0 609.2 610.4 611.0 613.0 609.2 610.4 611.0 611.0 609.2 610.4 611.0 611.0 609.2 609.2 610.4 611.0 611.0 609.2 609.2 610.4 611.0 609.2 609.2 610.4 611.0 611.0 609.2 609.2 609.2 610.4 611.0 609.2 609.2 609.2 610.4 611.0 611.0 609.2 609.2 609.2 609.2 609.2 609.2 610.4 611.0 611.0 609.2 609.0 609.2 609.0 608.8 609.0 608.8 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 609.0 60	624.2 622.0 608.0 621.3 617.4 613.8 611.2 600.0 614.0 613.5 609.2 603.3 618.0 618.5 613.8 607.0 625.0 620.0 615.0 609.2 622.0 622.2 619.2 614.2 617.8 616.8 612.0 609.0 609.0 612.0 609.0 607.0 614.0 612.2 608.0 603.0 618.3 620.0 616.2 610.0 618.3 620.0 616.2 610.0 621.8 620.8 616.2 611.0 621.2 620.8 616.2 611.0 621.2 620.2 614.0 611.0 621.4 611.0 633.0 592.0 620.2 620.8 616.2 611.0 604.5 602.0 598.0 592.0 620.2 620.8 616.0 609.0 621.4 61	Sc. Div. 616'0 607'5 601'5 602'0 603'0 607'6 605'6 605'0 600'5 602'2 603'8 604'1 608'0 613'0 581'8 592'4 603'5 602'5 612'8 604'8 624'5 623'4 635'2 617'9 630'8	Sc. Div. 603 '0 600 '2 602 '0 598 '0 600 '2 604 '2	sc. Div. 603 '5 605 '0 606 '6 600 '0 600 '0 605 '2 	sc. Div. 604'6 606'0 607'0 601'2 604'2 607'0	Sc. Div. 607 '8 605 '5 612 '0 606 '2 609 '2 601 '0 606 '0 606 '0 605 '4 609 '4 614 '0 604 '0 615 '0 609 '0 610 '0 621 '2 632 '0 625 '5 625 '0 614 '0 625 '4	Sc. Div. 608 '0 605 '8 610 '0 612 '0 610 '2 599 '0 608 '0 608 '0 609 '0 615 '4 622 '4 608 '0 	Sc. Div. 600'0 612'5 616'0 611'3 617'8 601'8	sc. Div 606 0 601 0 601 0 611 2 611 8 620 0 593 8 611 2 609 2 608 2 617 2 614 0 612 0 591 4 598 6 617 0 608 0 619 2 641 0 609 5 636 0 614 4 635 8
Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second Second	0 607.5 603.0 605.2 610.4 611.0 613.0 613.0 609.0 608.8 609.0 617.5 613.4 624.2 619.0 628.0 621.2 621.0	609 ° 0 612 ° 0 609 ° 0 607 ° 6014 ° 0 609 ° 0 607 ° 6014 ° 0 608 ° 0 603 ° 603 ° 603 ° 603 ° 603 ° 603 ° 603 ° 603 ° 604 ° 604 ° 602 ° 8 616 ° 6 615 ° 0 611 ° 0 605 ° 601 ° 0 605 ° 601 ° 0 606 ° 2 610 ° 601 ° 0 605 ° 601 ° 0 601 ° 0 601 ° 0 601 ° 0 601 ° 0 601 ° 0 601 ° 0 601 ° 0 601 ° 0 601 ° 0 601 ° 0 601 ° 0 601 ° 0 602 ° 0 603 ° 0 602 ° 0 602 ° 0 602 ° 0 602 ° 0 602 ° 0 602 ° 0 602 ° 0 602 ° 0 602 ° 0 603 ° 0 602 ° 0 603 ° 0 602 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0 603 ° 0	605.0 600.5 602.2 603.8 604.1 — 608.0 613.0 581.8 592.4 603.5 602.5 — 612.8 604.8 624.5 623.4 635.2 617.9 — 630.8	602.0 596.5 598.4 603.0 597.0 — 606.2 620.3 592.0 598.5 — 610.0 600.2 615.0 612.2 627.5 614.0 — 634.0	599.0 598.0 598.0 603.2 595.0 — 608.6 602.0 594.0 603.2 609.0 602.6 — 611.0 607.0 624.5 604.0 620.0 604.0 620.0 604.0 634.6	600°0 599°2 604°2 610°5 599°2 608°0 593°2 594°2 608°9 614°0 607°1 616°2 610°8 621°4 611°2 617°0 611°5	606.0 605.4 609.4 614.0 604.0 — 615.0 603.0 595.5 617.0 609.0 610.0 — 621.2 632.0 625.5 625.0 614.0 —	608'0 609'0 615'4 622'4 608'0 ———————————————————————————————————	607.0 602.0 616.2 614.4 611.0 — 618.0 597.4 597.9 611.6 617.0 618.0 — 628.4 629.2 643.5 617.5 637.0 616.5	609.2 608.2 617.2 616.2 614.0 591.4 598.6 617.0 608.0 619.2 631.0 628.2 641.0 609.5 636.0 614.4
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23	613.4 624.2 619.0 628.0 621.2 621.0	626.5 623.0 620.0 613. 625.2 625.0 627.0 624. 652.2 655.5 652.0 619. 642.0 633.8 630.2 628. 634.5 631.0 626.0 621. 628.5 638.6 639.5 621.	604 '8 624 '5 623 '4 635 '2 617 '9 	600°2 615°0 612°2 627°5 614°0 ————————————————————————————————————	607.0 624.5 604.0 620.0 604.0 634.6	610.8 621.4 611.2 617.0 611.5	617 · 2 632 · 0 625 · 5 625 · 0 614 · 0	625 8 639 2 621 0 636 0 607 5	629 2 643 5 617 5 637 0 616 5	628 2 641 0 609 5 636 0 614 4
Carry Means 621.85 638.6 639.				ļ		626.0	625.4	632.8	635.5	625.0
	73 610.96	621.82 620.83 616.43 610.	608.38	605.38	1 1					
$ \begin{pmatrix} 2 & 52.4 & 52.6 & 52. \\ 3 & 56.2 & 56.0 & 56. \\ 4 & 57.5 & 57.0 & 56. \\ 5 & 53.8 & 53.4 & 54. \\ 6 & 51.9 & 51.5 & 52. \\ 7 & 53.0 & 53.0 & 52. \\ 8 & & \\ 9 & 56.6 & 57.0 & 57. \\ 10 & 60.0 & 59.6 & 59. \\ 11 & 59.4 & 59.2 & 59. \\ 12 & 57.5 & 57.1 & 57. \\ 13 & 57.4 & 57.2 & 56. \\ \end{pmatrix} $	ı				605.32	607.22	611.61	614.24	615.26	614.4
	TEMI	TE	ERATURE O	F THE BIF	LAR MAGN	ET.				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	56°2 57°0 54°9 52°0	52.4 52.6 52.8 52. 56.2 56.0 56.0 56. 57.5 57.0 56.2 57. 53.8 53.4 54.0 54. 51.9 51.5 52.0 52.	53.0 56.7 57.7 55.4 52.5 53.0	54·1 57·4 58·0 56·4 53·2 53·6	54.7 58.1 58.5 57.0 54.0 54.0	55°1 58°4 58°7 57°5 54°8 54°1	55°3 58°6 58°9 58°2 55°2 54°4	55°9 58°8 59°0 59°0 55°8 55°0	56.4 58.8 59.2 59.0 56.5 55.2	56.5 58.6 58.8 59.2 56.5 55.0
M 16 54.9 55.1 54. 17 55.9 55.7 55. 18 57.0 57.0 56.	4 59.0 59.0 56.7 6 56.6	60°0 59°6 59°4 59° 59°4 59°2 59°0 59° 57°5 57°1 57°0 56° 57°4 57°2 56°6 56° 56°0 55°6 55°2 55°	57.8 59.9 59.0 56.5 56.6 55.5	58.5 60.5 59.5 56.8 56.6 55.6	58.7 61.0 59.6 57.0 56.6 55.8	59.0 61.6 59.6 57.2 56.8 56.3	59°5 61°5 59°4 57°4 56°8 56°1	59.6 61.9 59.6 57.8 57.2 56.6	60.0 61.3 60.0 58.2 57.0 56.8	60°0 61°0 59°8 57°9 56°4 56°5
20 50.6 50.4 50.	5 54°4 5 56°0 7 56°8 6 56°4 50°0	54.9 55.1 54.5 54.5 55.9 55.7 55.5 56.5 57.0 57.0 56.7 56.5 57.4 57.0 56.6 56.6 50.6 50.4 50.0 50.5 52.3 51.6 51.3 50.0	55°2 56°6 57°2 55°8 51°0 50°6	55.5 56.7 58.0 56.0 51.5 51.0	55.8 56.9 59.0 56.3 51.8 51.0	56.0 57.2 59.8 55.6 52.2 51.5	56°1 57°4 60°0 54°9 52°5 51°5	56.5 57.7 59.9 54.9 53.0 52.0	56.5 57.7 59.4 54.6 52.8 51.3	56.6 57.2 58.9 54.4 52.5 51.3
23 45.6 45.7 45. 24 50.0 50.0 49. 25 46.7 46.4 45. 26 39.6 38.8 38. 27 39.6 39.2 38.	3 45.5 8 49.2 0 45.0	45.6 45.7 45.3 45. 50.0 50.0 49.8 49. 46.7 46.4 45.0 45. 39.6 38.8 38.2 38. 39.6 39.2 38.6 39. 49.4 49.4 49.4 49.4	46.0 49.7 43.6 39.5 39.6 49.6	47.0 50.3 42.2 39.6 39.7 49.6	47.5 50.7 41.8 39.8 40.6 49.8	48.2 51.2 41.0 40.0 41.5 49.9	49.0 51.0 40.3 39.6 42.0 50.5	49.4 51.0 40.2 39.5 42.3 51.2	49.4 51.0 39.8 39.5 42.7 51.5	48.6 50.4 39.5 39.6 43.0 51.4
	6 39°3 4 49°6	42.2 43.0 43.0	43.5	43.2	43.2	43.5	43.5	43.3	43.2	43.5

										i	erature, 1°65	
12 ^h .	13h.	14 ^h .	15h.	16 ^h .	17 ^h .	18h.	19h.	20 ^h .	21h.	22h.	23h.	Daily an Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
0.906	606.4	618.0	613.0	611.0	610.4	617.2	610.8	612.4	610.2	608.0	615.0	610.97
14.2	611.2	612.2	612.8	610.0	610.4	611.0	611.4	610.0	612.8	616.0	612.4	609.62
06.0	603.2	598.0	606.0	602.2	602.5	605.0	605.2	614.0	608.6	611.0	611.8	607.50
12.0	613.4	611.0	613.8	612.1	612.0	612.9	618.0	619.2	616.5	618.0	624.0	611.78
20.4	620.0	605'2	597.0	604.4	611.0	610.2	608.0	617.0	620.0	619.0	619.8	
04'0	600.2	608.0	611.5	611.8	611.0	614.0	615.0	616.2	615.3	613.2	616.2	609.73
11.0	611.0	612.0	609.0	609.2	607.4	608.6	608.2	609.2	609.8	610.0	610.2	608*29
	602.0	611.2	612.0	611.2	611.8	611.2	613.0	$\begin{bmatrix} 603.7 \\ 613.0 \end{bmatrix}$	613.0	615.8	614.0	608.8
06 . 2	611.4	609.0	608.0	606.0	609.0	608.0	610.0	609.2	612.0	614.0	615.0	607.30
16.8	617.1	616.8	614.0	613.8	613.5	613.0	614.0	618.0	619.0	620.0	620 ·2	612.70
17.0	613.8	614.4	608.0	607.0	608.0	613.0	614.2	615.0	612.4	613.0	604.8	612.2
15.0	615.0	615.0	614.2	614.8	615.5	—		_			—)	
		010 0	-			621.2	620.2	621.8	622.0	617.6	623.1 }	613*22
12.6	622.0	621.8	617.4	613.2	609.8	610.0	613.8	616.1	618.0	621.5	622.2	615.02
95.2	589.5	593.8	595.4	590.0	566.0	595.8	584.0	591.8	596.0	586.0	574.0	597.38
04.2	603.9	604.8	604.2	605.0	605.2	605.0	605.0	605.0	605.0	605.0	604.4	600.23
13.5	612.0	611.0	615.0	617.0	616.0	618.0	617.0	618.0	617.6	618.0	620*4	610.73
0.11	610.0	615.0	619.7	616.0	617.2	617.7	616.5	620.0	620.2	622.4	618.8	614.20
19.0	621.4	618.4	622.2	620.0	621.8		_		_		— <u>}</u>	617:12
		_				619.2	626.0	618.0	628.5	630.2	630.2	
30.5	629.8	629.6	629.1	629.0	627.2	627.2	627.8	627.0	630.2	628.0	628.0	624.72
28.9	628.5	627.0	625.0	626.0	624.9	625.1	628.0	629.0	629.0	630.0	626.0	622.23
41.0	642.9	640.0	643.0	640.5	642.0	642.0	640.0	638.3	633.0	631.2	653.0	634.50
03.0	621.0	626.0	618.2	630.0	627.0	625.3	614.2	627.4	642.4	639.2	640.0	625.70
919.0	622.2	628.4	620.1	641.4	622.2	626.2	624.0	628.0	621.2	620.0	631.1	627.99
616.5	618.8	609.2	653.3	624'0	626.1			C24:0	628.0	632.2	$\{\frac{-}{635\cdot 5}\}$	622.96
37.1	628.2	624.0	628.8	636.0	634.2	630 ° 0	631 · 2	634 . 0	630.0	635.0	636.2	632.73
514.74	615.12	615.20	616*42	616.08	614.47	616.78	616.73	618.62	618.84	618.97	620.25	614.80
	! 	I		TE	MPERATUR	E OF THE	BIFILAR M.	AGNET.			"	
0	0	0	0		0	0	0	0	0	0	0	٥
56.5	56.4	56.2	56.9	56.9	57.0	57.2	57.3	57.2	57.0	57.0	56.6	55.59
29.0	59.4	59.2	59.0	59.0	58.7	58.4	58.1	57.8	57.5	57.2	57.8	57 • 98
59.0	58.7	58.2	57.5	57.0	56.6	56.2	55.7	55.2	54.5	54.3	53.7	57.2
58.4	57.8	56.8	56.0	55.6	54.8	54.2	53.5	53.0	53.1	52.7	52.0	55.6
56.5	55.7	55.1	54.6	54.2	54.2	54.0	53.2	53.5	53.2	53.3	53.3	54.0
5 5'0	55.2	55.4	55 . 5	55.6	55.7				_		55·8}	54.3
						53.2	53.8	54.6	55.0	55.4		
60.1	60.1	60.1	60.0	60.5	60'4	60.2	60.5	60.2	60.2	60.2	60.0	59.2
60.8	60.2	60.2	59.8	59.8	60.0	60.0	59.7	59.5	59.2	59.1	59.0	60.18
59.7	59.8	59.8	59.6	59.4	59.1	58.7	58.5	58.3	58.4	58.2	57.5	59°19 57°2'
57.7 56.0	57.5	57.3	56.9	56.7	56.8	57.1	57.4	57.4	57·5	57°5	57.5 56.2	56.4 56.4
56'2	56.6	56.4	57.0	56.8	56.3	56.9	56.7	56.8	56.6	56.6		
56.6	56.6	56.7	56.7	56.6	56.3	54.3	 54·4	54·5	54.8	55.0	54.6}	55.78
56·3	56.0	57.0	<u></u>	56.8	56.6	56°4	56·2	55.8	55°9	55.8	55.8	55*99
57·2	56.8 57.2	57·2 57·3	57°1 57°4	56 8 57.4	57.4	57.5	57·5	57.4	57·4	57.4	57.4	57.0
58.6	58.1	58.0	57.6	57.5	57.4	57.5	58.0	58.0	58.0	57.6	57.6	58.0
23.6	53.3	52.2	52.0	51.7	51.2	51.2	51.2	$51 \cdot 2$	51.0	51.0	50.4	53.7
52.2	52.2	52.5	52.5	52.0	52.0	52.0	52.0	51.8	51.7	51.7	52.0	51.8
51.3	51.6	51.6	51.2	51.2	51.5	_			_		$\frac{-}{45\cdot 5}$ }	49.9
	_	_			_	46.0	46.0	45.6	45.6	45.6		
48.6	48.8	49.3	49.0	48.8	48.7	48.8	48.8	48.7	49.4	49.8	49.6	48.1
50.1	49.5	49.2	49.0	49.0	48.0	47.4	47.0	47.0	47.0	47.0	47.0	49.23
39.3	39.2	39.0	38.2	38.2	38.8	39.5	39.5	39.2	39.7	39.7	39.0	40.90
40.1	40.4	40.2	40.5	40.0	40.0	39.5	39.5	39.7	40.0	40.4	39.9	39.6
44.0	44.5	44.4	44.8	45.6	46'4	46.8	46.2	46.5	46.8	48.4	48.9	43.3
51'6	50.8	50.4	50.0	20.0	50.0		41.5	41.5	41:0	40:4	$\{-\frac{1}{42\cdot 5}\}$	48'1
43.0	42.1	41.5	41.0	40.7	40.5	41.5 41.0	41.2 41.0	41.2 41.0	41.9 41.2	42.4 41.3	42 5)	42*2
	t .			1								

Iean Göttii gen Time	-}	Oh.	1h.	2h.	3h.	4 ^h .	5 ^h .	6h.	7h.	8h.	9 ^h •	10h.	11h.
		Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Di
(}	L '	636.6	641.4	638.7	637.2	630.8	627.8	628.2	623.0	630.8	639.0	643.0	641'
2		641.2	641.9	634.0	636.0	633.9	625.1	628.4	630.0	627.5	631.2	630.0	631.5
{		628.7	625.5	623.0	618.0	615.9	611.2	613.0	617.0	622.0	625.5	626.2	628
4		630.0	632.7	632.5	629.0	620.0	617.0	619.0	622.2	628.0	627.0	634.0	632
	5	633.0	631.7	629.0	625.8	620.4	618.2	622.0	622.0	628.8	632.6	630.7	633
1 7	7 I	643.0	639.0	637.6	635.2	629.0	625.8	621.4	622.5	628.4	635.1	640.4	639
8	3 1	635.0	638.2	634'2	630.8	624.8	618.6	615.6	618.0	625.0	635.8	638°2	635
9) (634.8	636.2	634.2	631.0	626.0	622.5	622.0	622.0	625.0	634.5	626.0	628
10)	633.7	629.0	629.0	628.0	620.0	616.0	610.0	610.4	622.0	623.2	622.8	625
13	L	636.0	633.2	635.6	631.4	633.0	625.2	618.4	622.5	625.8	631.0	630.6	631
12	2	630.4	636.0	637.4	635.0	632.0	629.7	626.2	625.2	633.0	634.0	639.0	634
DECEMBER.		655.0	653.2	652.0	654.4	652.0	647.8	643.6	645.8	648.4	655.0	655.9	646
A is		652.6	647.6	646.5	646.0	642.3	638.3	636.0	641.0	645.0	646.0	647.1	648
a die		649.0	650.0	649.0	647.0	643.0	638.0	638.0	640.0	642.2	643.0	645.2	647
B \i'		645.0	645.0	642.2	638.4	636.6	635.0	637 .3	639.9	$642^{\circ}2$	645.2	647.0	645
日 日 i		647.6	646.8	642.6									
_, T;	9	643.4	640.4	638.8	644'0 635'8	641 ° 0 634 ° 4	636.2 631.0	637 . 4 627 . 0	638.8 632.5	645°5 635°4	647.9 638.0	$642.0 \\ 641.0$	639°
20)	_											
2		649'1	646.8	645.8	644.0	640.0	637.4	639.5	643.0	646.5	648.0	650.0	652
2	4	647.0	647.0	646.0	647.0	640.0	638.0	643.5	647.3	651.0	654.2	653.0	654
2		650.0	656.0	649.8	648.4	643.0	634.0	632.2	637.0	$635^{\circ}2$	626.2	623.0	631.
24	1 5 a	640.0	642.5	640'2	635.0	625.0	620.0	622.2	616.6	632.2	633.4	641'5	642
20	6	651.0	651.2	637.0	637.0	622.0	627.0	628.0	630.4	635.2	635.4	641.4	640.
2		635.8	636.0	632.0	628.2	627.7	622.2	617.6	622.8	626.8	631.2	634.5	633
2	9	641'0	639.2	637.8	635.4	629.8	625.6	625.0	629.2	629.0	637.0	639.6	641
3		638.8	637.0	637.5	636.3	624.3	618.0	620.0	625.0	630.0	633.8	633.2	633.
(3		637.0	634.0	631.4	627.8	624.4	621.0	621.0	625.2	632.0	634.7	634.0	637
ourly Me	ans	640.95	640.67	638.22	636.53	631.50	627:19	626.65	628.82	633.57	636.87	638.06	638
			· · · · · · · · · · · · · · · · · · ·		ТЕМР	ERATURE O	F THE BIF	LAR MAGN	ET.	·			
	1	4i°2	40.6	40.0	39°6	39.5	39°8	40.2	40°4	40°5	41.1	41.6	4 <u>1</u> °8
	2	43.6	43.8	43.7	44.1	45.0	46.1	46.4	46.6	47.3	48.2	48.6	49
	3	50.8	49.9	48.6	48.3	47.9	48.0	48.2	48.0		48.0	47.6	47
	. !!	44.0	44.0	44.0	44.0					47.6			
	4 5	47.0	47.0	46.9	46.8	$\begin{array}{c c} 44.2 \\ 47.2 \end{array}$	44.6	45.0	45.2	45.5	45.7	46'3 49'2	46
	6	47 U		40 9	40 0	41 2	48.0	48'0	48.4	48.6	49'0	49 2	48
	6	43.5	44.0	43.7	43.6	43.7	44.5	45.0	45*4	45.2	45.7	46.2	46
- 1 -	8	49.6	49.5	48'8	48.5	49.2	49.6	49.4	49.2	49.2	49.4	49'4	49
1 :	9	$47^{\circ}5$	47.0	46.7	46.2	46.0	46.6	47.2	48.0	48.0	48.0	48.0	48
1		$45^{\circ}5$	45.5	45'1	44.4	44.5	45.7	46.2	46.7	47.0	48.0	48.8	48*
1	1	46.0	45.6	45.3	45.7	46.8	47.0	46.3	46.5	45.8	45.6	45'8	45
1	2	43.0	42.6	42.0	41.2	40.4	40.4	40.4	40°4	40.2	40.2	40.2	40°
DECEMBER.		31.4	31.7	32.0	32.0	32.6	33.0	33.6	34.2	35.4	36.5	36. 8	36.
器li	5	34.0	33.2	33.3	33.9	34.9	36.5	36.8	37.5	38.4	39.2	39.7	39.
⊠/i	6	37.9	38.2	37.3	36.7	38.0	39.0	40.0	40.6	41.5	40.7	41.3	41.
国人	7	39.6	39.2	39.0	39.8	40.7	41.8	40.0	43.0	42.6	42.7	42.7	42.
) [급	8	38.8	38.7	38.3	38.0	38.5	39.2	42.8	40.8	41.8	42.4	42.6	43
	9	42.2	41.8	41.8	42.0	43.0	39 2 43 1	43.4	43.8	43.7	43.7	42 6	43
	0	38.2	38.5	38.0	38.0	37.7		38.9	39.9	40.7	41.5	41.7	41
	22	40.3	40.2	39.5	38.9	35.6	38·2 34·6	34.0	33.6	33.6	34.0	35°0	36.
	23	38.2	38.0	36.6	36.7	37.3	37.3	37.0	38.0	39.2	40.6	41.3	41
1 4	4	41.8	41.7	41.6	41.4	42.0	43.0	44.0	44.2	44.6	44.8	44.8	44.
	5 a 26	39.0	39.2	39.0	38.2	39.4	40.4	41.0	41.5	41.4	41.2	41.0	41.
2 2	· ·		1000	46.0	46.0	46.2	46.5	46.0	45.8	45.6	45.6	45.5	45
2 2 2	27 28	46.5	1 45 5			1 40 Z	1 40 0	1 TU U	100	ס טיבין	ט טידי ו	ויטיביו	10
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	8	46°5 43°4	46.5				41.0	40.0	40.0	40.1			
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	8	43.4	42.8	42.0	41.4	41.5	41.8	42.2	42.0	42.1	42.7	43'1	43
	8 9 80	43°4 43°8	42.8 44.0	42.0 44.7	41°4 45°2	41°5 45°6	46'1	46.7	48.0	47.5	42.7 48.0	43°1 48°0	43° 47°
	8	43.4	42.8	42.0	41.4	41.5					42.7	43'1	43

[•] Christmas Day.

	One Scale	e Division =	= •000087 p	arts of the I		IZONTAL ase in Scale		orresponding	to 1º decre	ase of Temp	perature, 1°6	3.
12 ^h .	13 ^h .	14h.	15h.	16 ^h .	17 ^h .	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
633.2	631.0	636.8	642.0	634.0	646.0	632.0	634.2	630.0	636.2	634.2	637.6	635.20
626.9	630.9	629.0	628.6	630.0	628.2	625.0	625.4					630.01
627.2	629'2	631.2	636.2	637.8	631.0	627.0	612.5	618.7	626.2	629.0	630.2	624.60
630.6	632.0	630.8	627.2	634.3	629.8	628.0	630.2	632.0	633.8	633.8	633.2	629.18
629'9	631.0	630.2	630.6	631.0	633.2	000:0	CALLO	64714	C41:0	C49:0	$\left \frac{-}{642 \cdot 2} \right\}$	631.67
		-	20210	205:0	004.7	638.2	641.0	641.4	641.2	642.0		 }
638.2	638.0	636.8	635.8	635.0	634.7	633.2	634.0	633.6	635.2	635.0	634.8	634.22
628.2	624'0	621.0	621.2	620.8	620.6	626.6	630.0	633.8	638.6	634.2	634.4	628.45
625.0	625.6	595.6	605.8	607.8	618.0	617.2	623.2	626.8	627.1	629.6	621.0	623.55
626.2	630'8	624.8	611.6	614.7	620.2	623.3	623.7	630.2	627.6	623.5	635'0	623.36
629'9	627.0	618.4	625.0	632.4	638.0	633.0	635.0	637.0	633.0	631.2	631.0	630.20
637.4	642.0	643.6	639.2	634.2	640.5			25010	04014	240.0	$\{655.4\}$	638.72
						648.4	648.6	650.0	648'4	649.0		1
653.5	649.0	651.0	651.2	651.4	648.3	649'0	651.2	647.8	645.6	653.2	648.7	650:37
647.4	641.0	641.0	648.8	648 2	647.2	648.8	647.2	647.0	647.8	647.8	648.0	645.69
647.4	645.4	645.4	646.9	644.1	644.7	644.7	644.9	644.7	645.0	645.0	645.0	644.81
646'1	645'1	638.6	643.0	643'1	643.0	643.2	644.8	644.8	644 0	647.0	647.6	642.92
640.0	639.0	639.0	645.5	643.0	641.3	641.1	642.0	642.4	642.2	642.2	642.0	642.05
642.5	642.8	642.0	642.7	643.3	640.2) —			- 1	640.92
						646.4	648.0	647.8	648.2	648.8	650.2}	l
652'0	641.2	643.3	641.2	642.5	642.5	643.0	644.9	646.3	646.9	646.5	646.0	644.95
647.8	647.5	646.8	644.1	644.0	641.6	643.5	646.2	646.0	644.2	645.6	649.0	646.43
629.0	587.0	611.0	617.5	623.0	635.0	636.5	636.5	633.0	634.0	632.6	632.3	632.22
640.2	636.2	631.4	631.0	641.0	633.0			`			1 1	
639.2	638.0	641.0	640.1	640.1	633.9	638.0	640.6	641.8	637.0	638.2	639.0	634.93
			-			640.7	633.0	634.9	633.0	633.4	$\{634.0\}$	636.54
630.7	633.7	634.5	635.2	634.0	635.4	635.0	637.5	638.5	635.0	636.2	638.0	632.20
642.0	641.0	640.2	638.0	635.2	637.5	639.0	636.4	636.8	637.4	640.0	639.0	636.37
633.0	633.0	633.2	634.2	633.2	635.0	633.6	635.8	638.4	635.2	635.8	636.2	632.70
637.0	635.2	633.0	633.0	633.2	632.8	632.0	632.4	635.0	634.8	633.8	636.0	632.00
636.94	634.20	633.47	634.45	635.07	635.83	636.41	636.89	637.90	637.81	638.50	639.02	635.55
000 31	034 30	000 47	004 40				BIFILAR M	<u> </u>	001 01	000 20	000 02	000 00
0	0	0	0					1 0	0_	. 0		0
41°5	41°2	41°2	42.0	42.0	42.2	42.5	42.4	42.5	43.0	43.7	43.4	41.41
20.0	50.2	50.9	50.7	50.9	51.3	51.8	52.0	51.8	51.6	51.5	51.2	48.64
47'6	47.0	46.8	46.5	46.2	46.0	45.6	45.0	44.6	44.6	44.6	44.4	47.06
46.5	46.8	47.2	47.6	47.7	47.5	47.4	47.1	46.9	47.4	47.4	47.2	46.07
48.9	48.5	48.5	48*2	48.0	48.0	_	-	<u> </u>		-	43.0}	46.47
			-			40.0	40.7	41.5	42.5	42.7		
46.7	47.5	47.7	47.6	48.0	48.4	48.5	48.6	49.0	49.2	49.4	49.5	46.55
49.0	49.0	48.8	48*2	48.2	47.8	48.2	48.2	47.8	47.8	48.2	47.7	48.74
48.5	48.5	48.2	48.0	47.8	47.6	47.8	47.3	46.6	46.0	45.6	45.4	47.27
48.3	48.3	48.2	48.0	47.8	47.0	46.7	46.6	46.4	46.6	46.8	46'1	46.79
44.8	44.5	44.2	44.0	44.0	44.0	44.0	43.8	43.5	43.8	43.2	43.2	44.94
40.7	40.4	40.2	40.2	40.5	40.5						- }	38.59
_	_	_	_		-	31.8	31.9	35.0	32.2	32.0	31.4}	
36.2	36.0	35.6	35.8	36.0	35.8	35.6	$35^{ullet}4$	35.1	35.0	35.1	34.6	34.67
40.2	40.0	40.2	40'1	40.0	39.4	39.0	38.7	38.1	37.6	37.5	37.3	37.73
41.6	41.6	41.5	41.5	41.5	41.5	41.0	40.4	40.0	40.3	40.4	39.9	40.15
42.6	42.4	42.0	41.2	41.0	40.2	39.8	39.0	38.8	38.9	39.0	38.8	40.85
43.1	43.3	43.4	43.2	43.0	43.0	43'3	43.6	43.3	43.0	43.0	42.7	41.65
43.2	43.2	43.2	43.4	43.4	43.1						33	
			_	^		35.7	36.1	36.6	37.6	38.4	38.0}	41.60
41.0	40.7	40.5	40°1	40.2	40.0	39.8	39.2	39.9	40.0	40.0	39.7	39.76
37.0	38.0	38.6	38.5	38.5	38.7	38.9	38.7	38.7	38.6	39.2	38.9	37.39
42.0	41.8	41.4	41.6	42.0	42.1	42.0	42.0	42.3	42.3	42.2	42.2	40.24
45.0	45.8	46.4	46.5	46.5	46.5						"	
41.6	_	_				38.0	38.0	38.0	38.2	38.7	39.0	42.72
	42.0	42.4	43.6	44.5	44.4	45.3	45.6	45.7	45.9	46.4	$\frac{-}{46.5}$	42.37
44.8	43.6	43.5	43.2	43.2	43.0	43.0	43'2	43.5	43.5	43.5	43.5	44.71
43.5	42.8	43.0	42.4	42.2	42.8	43.0	43.0	43.2	43.3	43.3	43.4	42 * 68
47.2	47.0	46.7	46.7	46.7	46.4	46.8	46.9	47.4	48.0	48.2	48.5	46.74
49.7	49.6	49.4	49.4	49.2	49.0	48.8	48.6	49.0	48.7	48.8	48.8	48.70
44.29	44.24	44.23	44.14	44.18	44.07	42.86	42.78	42.78	42.92	43.04	42.87	43.25

lean C					of the H. F.			1		1	1	1	
gen T	öttin- }	Oh.	1 ^h .	2h.	3h.	4h.	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .	10h.	11h.
		Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
	$\left(egin{array}{c} 1 \ 2 \end{array} ight)$	636 . 2 632 . 5	638.0 638.0	636.0 633.2	635.0 633.0	631.0 629.6	628.0 620.0	627 ° 0 620 ° 0	$629\cdot2$ $622\cdot4$	634°3 630°8	638°0 637°0	641°0 636°7	640'4 640'9
	3												
	4	641.6	640.8	640.5	631.2	624.8	618.6	619.2	625.0	633.8	639.5	641.0	637.0
	5	634°2 635°8	638.2	640.4	636.4	624.0	$624.0 \\ 614.2$	622.0 610.6	624°0 614°0	$628.0 \\ 619.5$	633.0	$\begin{array}{c} 635.2 \\ 636.2 \end{array}$	634°0
	6 7	635.0	639°2 634°2	640.6 634.3	633°0 629°0	621°0	616.0	616.0	624.0	628.6	635.0	638.0	635.4
	8	647.5	645.0	647.0	640.5	630.0	625.2	629.4	637.5	643.0	645.4	647.5	645
	9	655.0	655.0	653.2	650.0	639.5	637.5	641.2	641.0	648.5	648.0	651.5	652.0
	10 11	653.8	652.2	654.0	649.0	636.0	638.8	641.2	647.0	650.0	658.0	657.0	662.0
	12	660.5	658*8	653.2	661.0	654.0	642.0	641.5	638.5	646.0	652.0	658.2	658.8
.	13	646.0	648.0	653.0	647.0	646.0	642.0	633.0	625.2	634.8	635.0	643.0	645
3Y	14	636.0	638.5	638.0	637.4	631.5	623.0	620.4	627.4	632°2 626°2	635 . 4 629 . 5	630.7	637.2 630.2
JAI	15 16	632.0	631.8 630.2	632.0	623°2 629°1	618.5	$614.2 \\ 620.2$	619.0	624.8	624.0	629.5	630°1	632.0
JANUARY.	17 18	650.0	650.5	648.3	643.0	636.1	633.0 ª	634.0	639.0	642.0	644.0	647.0	645.6
J_{ℓ}	19	647.0	647.0	642.0	634.0	633.2	632.5	636.8	639.3	642.0	646.7	649.0	651'
	20	664.0	648.5	662.0	659.8	647.0	649.4	650.0	650.0	650.5	647.5	642.0	640.0
	21	650.4	649.5	642.5	628.0	620.4	629.8	631.0	630.6	635.0	634.5	642.1	640.0
	22	651.5	653.0	650.4	658.8	650.2	650.8	650.2	652.5	650.1	655.0	650.5	654.8
	23 24	652.0	655.0	653.2	649.0	643.5	642.0	643.0	646.0	647.0	650.0	648.0	648.0
	25	648.5	648.0	646.5	644.0	637.5	635.0	637.0	640.0	647.0	650.8	649.2	648.8
	26	646.0	646.5	645.2	638.0	630.2	630.0	629.8	633.5	637.5	641.2	642.7	637.9
	27 28	650.0	644.7	645°2 651°4	644.0	639.2	638 ·2 644 · 4	639°2 644°1	640.0	642.0	645 · 2 648 · 0	648°0 652°0	649.0
	29	643.6	643.0	648'1	638.0	648.2	641.0	638.1	641.8	632.0	637.0	637.0	624
	$\begin{bmatrix} 30 \\ 31 \end{bmatrix}$	637.5	637.0	637.0	642.0	642.8	630.0	612.0	608.0	636.0	654.0	627.2	621.6
Hour	ly Means	644.24	644.2	644.57	640.86	634.28	631.23	630.97	633.45	637.99	642.41	642.78	642'3
		lt.		<u> </u>	ТЕМР	ERATURE (OF THE BIE	ILAR MAGI	NET.		·	<u> </u>	<u></u>
	(1	47°5	47°5	47°6	48°4	48°5	48.8	47°8	48°3	47°8	47°5	47.5	47°6
	2	46.9	46.9	46.0	45.2	45.8	46.0	46.5	46.3	46.7	47.0	47.2	47.1
	3 4	43.0	43.0	43.0	42.8	42.7	43.2	43.6	44.4	45.0	45.5	45.6	45.6
	5	47.0	46.8	45.8	44.8	46.0	46.0	44.0	45.4	46.2	47.4	47.2	46.6
	6	45.5	45.5	45.1	44'8	45.5	46'1	46.4	46.7	47.0	48'0	48.6	49'0
	7	47.4	47.4	46.8	46.0	46.0	46.5	46.3	45.5	44.8	45.0	44.8	44.2
	8 9	37.2 33.7	36.9 33.2	36.0 33.2	33.0 36.0	36.0 39.6	36.0 34.5	35.5 35.5	35°0 35°7	34.6 36.0	34 . 8 36.6	35°1 37°0	34°7
	10	28.6	28.7	28.2	28.4	29.9	30.4	29.2	28.5	28.0	28.0	27.6	29.3
	11 12	28.5	28.1	28.8	30.0	31.4	32.4	33.0	33.2	34.2	35.7	36.9	37.2
			36.0	35.8	35.9	36.9	39.0	40.2	41.3	42.0	43.2	43.6	43.4
		36.0	1 30 0					Į.	48.4	48.3	48.3	48.3	48'
ŁY.	13 14	45.0	45.4	45.5	45.6	46'2	47.5	48.0					
ARY.	13 14 15	45°0 49°4	45°4 49°2	45.5 48.6	48.5	48.3	48.8	49.6	50.2	50.2	50.7	50.8	
NUARY.	13 14 15 16	45.0	45.4	45.5	48.5 49.0					50°5 46°3		44.7	44.
JANUARY.	13 14 15 16 17 18	45.0 49.4 50.5 — 37.7	45.4 49.2 50.1 — 38.0	45.5 48.6 49.8 — 38.0	48.5 49.0 — 37.5	48°3 48°5 — 38°5	48.8 48.1 — 38.7	49.6 46.1 — 40.6	50°5 46°4 — 41°1	50°5 46°3 — 41°4	50.7 45.5 — 41.9	44.7 42.3	44.1
JANUARY.	13 14 15 16 17 18 19	45.0 49.4 50.5 — 37.7 -37.4	45.4 49.2 50.1 — 38.0 37.4	45.5 48.6 49.8 — 38.0 37.2	48.5 49.0 - 37.5 36.4	48°3 48°5 — 38°5 36°0	48.8 48.1 — 38.7 35.7	49.6 46.1 40.6 35.5	50.5 46.4 — 41.1 35.5	50°5 46°3 — 41°4 35°7	50.7 45.5 — 41.9 35.8	44.7 42.3 35.6	44° 5 42° 5 35° 5
JANUARY.	13 14 15 16 17 18 19 20	45.0 49.4 50.5 — 37.7 -37.4 33.0	45.4 49.2 50.1 — 38.0 37.4 33.2	45.5 48.6 49.8 — 38.0 37.2 32.8	48.5 49.0 37.5 36.4 33.5	48.3 48.5 — 38.5 36.0 34.4	48.8 48.1 ————————————————————————————————————	49.6 46.1 — 40.6 35.5 35.7	50°5 46°4 — 41°1	50°5 46°3 — 41°4	50.7 45.5 — 41.9	44.7 42.3	44.1 42.3 35.3 38.0
JANUARY.	13 14 15 16 17 18 19 20 21 22	45.0 49.4 50.5 37.7 -37.4 33.0 37.4 30.5	45°4 49°2 50°1 ————————————————————————————————————	45.5 48.6 49.8 — 38.0 37.2 32.8 37.4 30.5	48.5 49.0 — 37.5 36.4 33.5 37.0 31.0	48.3 48.5 — 38.5 36.0 34.4 36.2 30.9	48.8 48.1 	49.6 46.1 - 40.6 35.5 35.7 35.5 31.7	50°5 46°4 — 41°1 35°5 36°0 35°7 32°0	50°5 46°3 	50.7 45.5 	44.7 	44.1 42.5 35.5 38.0 34.6 32.9
JANUARY.	13 14 15 16 17 18 19 20 21 22 23	45.0 49.4 50.5 	45.4 49.2 50.1 38.0 37.4 33.2 38.0	45.5 48.6 49.8 — 38.0 37.2 32.8 37.4	48.5 49.0 37.5 36.4 33.5 37.0	48°3 48°5 — 38°5 36°0 34°4 36°2	48.8 48.1 ————————————————————————————————————	49.6 46.1 - 40.6 35.5 35.7 35.5	50°5 46°4 — 41°1 35°5 36°0 35°7	50°5 46°3 	50.7 45.5 	44.7 	44.1 42.5 35.5 38.0 34.6 32.9
JANUARY.	13 14 15 16 17 18 19 20 21 22 23 24 25	45.0 49.4 50.5 	45.4 49.2 50.1 	45.5 48.6 49.8 — 38.0 37.2 32.8 37.4 30.5 33.1 — 35.6	48.5 49.0 	48.3 48.5 — 38.5 36.0 34.4 36.2 30.9 34.7 — 37.5	48.8 48.1 — 38.7 35.7 35.0 36.4 31.4 36.0 — 38.0	49.6 46.1 — 40.6 35.5 35.7 35.5 31.7 37.3 — 38.5	50.5 46.4 ——————————————————————————————————	50°5 46°3 — 41°4 35°7 36°2 36°0 32°0 39°0 — 39°5	50.7 45.5 - 41.9 35.8 36.6 35.9 32.5 39.5 - 40.2	44.7 	44 · 1 42 · 8 35 · 8 38 · 0 34 · 6 32 · 9 40 · 8 40 · 8
JANUARY.	13 14 15 16 17 18 19 20 21 22 23 24 25 26	45.0 49.4 50.5 37.7 37.4 33.0 37.4 30.5 32.4 35.8 41.1	45.4 49.2 50.1 	45.5 48.6 49.8 — 38.0 37.2 32.8 37.4 30.5 33.1 — 35.6 41.8	48.5 49.0 	48.3 48.5 — 38.5 36.0 34.4 36.2 30.9 34.7 — 37.5 42.7	48.8 48.1 — 38.7 35.7 35.0 36.4 31.4 36.0 — 38.0 43.7	49.6 46.1 — 40.6 35.5 35.7 35.5 31.7 37.3 — 38.5 44.4	50.5 46.4 ——————————————————————————————————	50.5 46.3 	50.7 45.5 	44.7 	44.1 42.3 35.3 38.0 34.6 32.9 40.5 40.2 44.5
JANUARY.	13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	45.0 49.4 50.5 	45.4 49.2 50.1 	45.5 48.6 49.8 	48.5 49.0 	48.3 48.5 — 38.5 36.0 34.4 36.2 30.9 34.7 — 37.5 42.7 38.9	48.8 48.1 	49.6 46.1 — 40.6 35.5 35.7 35.5 31.7 37.3 — 38.5 44.4 38.6	50.5 46.4 ——————————————————————————————————	50.5 46.3 	50.7 45.5 	44.7 42.3 35.6 37.0 35.4 32.5 39.8 40.2 44.6 37.5	42.5 35.5 38.0 34.6 32.5 40.5 40.5 44.5 36.8
JANUARY.	13 14 15 16 17 18 19 20 21 22 23 24 25 26	45.0 49.4 50.5 37.7 37.4 33.0 37.4 30.5 32.4 35.8 41.1	45.4 49.2 50.1 	45.5 48.6 49.8 — 38.0 37.2 32.8 37.4 30.5 33.1 — 35.6 41.8	48.5 49.0 	48.3 48.5 — 38.5 36.0 34.4 36.2 30.9 34.7 — 37.5 42.7 38.9 34.0	48.8 48.1 — 38.7 35.7 35.0 36.4 31.4 36.0 — 38.0 43.7	49.6 46.1 — 40.6 35.5 35.7 35.5 31.7 37.3 — 38.5 44.4	50.5 46.4 ——————————————————————————————————	50.5 46.3 	50.7 45.5 	44.7 	44°14 42°16 35°16 38°16 32°15 40°16 40°16 41°16 36°18 39°14 42°16
JANUARY.	13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	45.0 49.4 50.5 	45.4 49.2 50.1 	45.5 48.6 49.8 	48.5 49.0 	48.3 48.5 — 38.5 36.0 34.4 36.2 30.9 34.7 — 37.5 42.7 38.9	48.8 48.1 	49.6 46.1 — 40.6 35.5 35.7 35.5 31.7 37.3 — 38.5 44.4 38.6 35.9	50.5 46.4 ——————————————————————————————————	50°5 46°3 — 41°4 35°7 36°2 36°0 32°0 39°0 — 39°5 44°8 37°8 37°3	50.7 45.5 	44.7 42.3 35.6 37.0 35.4 32.5 39.8 40.2 44.6 37.5 39.4	44: 35: 38: 32: 40: 44: 36: 39:

^a Missed.

b Twenty minutes late.

	One Scale	Division =	•000087 par	ts of the H		IZONTAL se, in Scale		orresponding	g to 1° decre	ease of Tem	perature, 1 · (33.
12 ^h .	13 ^h .	14h.	15 ^h .	16h.	17h.	18h.	19 ^b •	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div. 638 4	Sc. Div. 641 2	Sc. Div.	Sc. Div. 637.0	Sc. Div.	Sc. Div. 634°0	Sc. Div. 633'9	8c, Div. 635°0	Sc. Div.	Sc. Div. 632.6	Sc. Div. 636 0	Sc. Div. 635 35
636.2	633.0	635.8	635.0	633.9	634.0		-				640.4}	633.86
						640.0	639.0	635.0	635.0	641.0		
637.4	636.0	634.0	634.0	636.0	634.0	629.0	633.0	630.0	632.0	633.0	631.2	633.02
631.3	626.5	643.0	620.2	626.0	631.0	635.2	635.6	632.4	633.0	636.2	635.0	631.62
634.0	633.6	613.7	624'4	628.8	633.0	631.2	631.0	632.1	632 . 9	633 ° 2 64 4° 6	634.0 647.0	629°07 633°64
634'4	634.2	634.0	636.8	637.1	636'1	638.2	640°0 651°0	641 .4 654 . 0	652.0	653.0	652.2	646.64
549 3	652.1	654'1	655°1 651°5	655 ' 9 648 ' 0	$\begin{bmatrix} 654.0 \\ 646.2 \end{bmatrix}$	653'8	001 0	034 0	002 0		i !!	
350.0	648.5	653.0	001.0	040 0	040 2	653.8	656.0	654.4	656.5	656.0	$\{655.8\}$	650.09
664.5	662.2	662.0	661.2	660'4	658.2	a	654.8 р	656.0	657.3	658*5	661.0	654.57
654.0	644.2	639.2	653.2	648.4	645.4	646.5	651.1 c	649.0	650.2	650.0	643.0	649.96
641.8	642.0	642.6	643.3	644'1	642.2	640.0	638.2	638.4	640.0	641.0	640.0	641.32
637.3	636.1	626.1	623.0	628.2	627.4	630.2	630.0	631.5	634.0	635.0	632.8	631.62
630.0	630.0	630.2	631.0	629.0	629.0	629.2	630.0	630.3	631.6	629.0	623.8	627.72
634'1	635.0	635'0	631.3	637.4	637.4						}	634.53
_	_					648 ·2	648.2	649.8	650.4	651.8	651.0	
545.2	646.0	645.2	643.2	642.0	641'6	641.4	642.4	644.0	645.1	646.8	647.0	643°43 648°07
552.2	652.8	653.0	656.0	653*3	653.8	656.2	656.6	657:0	653.0	655.0	654.0	
546.5	643.1	645.0	646.4	645.0	642.0	645.0	647.0	647.0	647.4	645°8 649°4	642.6 652.2	648.06 642.55
644.2	646.2	647.8	650.0	649.0	650.0	647.5	649.0	651.0	651·2 650·0	653.2	650.7	651.31
551.0	651.5	651.0	654'0	650.4	648.0	650.2	646.8	647.2	000 0	000 2	000 1	
648.0	644'6	641.8	646.0	645*4	643.0	649.6	650.3	651.2	651.2	651.5	652.0}	647.97
647.8	647.0	C47:0	647.8	645.8	645.0	645.2	645.2	645.0	644.2	645.0	647.0	645*21
32.0	634.0	647.8 632.1	633.0	633.0	636.5	636.0	638.0	637.0	639.0	642.0	643.2	637.25
550.0	646.0	646.0	644.2	646.2	648.0	649.8	650.2	649.3	649.0	649.2	649'8	645.68
554.0	653.7	643.0	642.7	641.2	646.0	644.0	638.4	640.0	635.8	640.4	646'8	646'14
642.0	631.4	631.0	630.0	628.2	629.0	631.6	631.1	631.4	633.9	636'1	637.0	636.02
613.0	632.2	615'4	610.0	614.0	622.0						- }	628:38
_	_		—	_	_	626.0	628.0	629.2	634.0	635.2	637.0}	020 30
642.30	641.55	640.13	640.05	640.14	640.33	641.27	642.11	642.25	642.95	644.02	643*94	640.48
					MPERATUR				0 1	. 0	0	0
48.0	47°6	47°4	45°9	45°9	45°6	45°6	4а9	46°4	46°8	47.0	46°9	47.24
48'1	47.6	47.6	47.2	47.0	46.7	40.0	43.04	42.0	43.0	43.4	$\frac{-}{43\cdot 3}$	45.63
46:0	40.0		40.5	47.0	47.1	40.2	41.4		48.0	47.6	47.6	45.53
46.2	46.0	46.6	46.5	47:3	47.1	47°0 46°6	47°5 46°4	48'0 46'2	46.2	46'0	45.6	46 ·3 4
47.0 49.5	47.0 49.0	47.0	47.0 47.6	47.0 47.0	46.7 46.5	46.5	46.2	47.1	47.3	47.3	47.2	47.00
43.6	42.5	48'4 41'8	41.6	41.1	40.5	39.2	39.2	39.2	40.4	40.1	38.2	43.29
34.6	34.5	33.8	33.2	33.3	32.2	32.4	32.6	32.9	33.0	33.3	33.2	34.47
36.4	35.7	36.0	35.2	35.2	35.2							33.63
_						29.6	29.2	29.2	29.2	29.0	$\frac{-}{28.7}$	
30.2	31.0	31.2	31.3	30.8	30.4		30.5	30.4	30.4	29.8	49 1	29.61
37.5	37.0	36.4	36.3	35.7	35.6	36.1	36.0	35.7	36.1	36.1	35.8	34.35
43.2	43.2	42.7	42.6	42.5	42.8	43.0	43.2	43.2	44.0	44'6	44.6	41.40
48 8	48.8	48.9	49.4	49.5	49.5	49.5	49*4	49.4	49.5	49.5	49.5	48.18
51.0	51.0	51.4	51.4	51.5	51.5	51.2	51.2	51.5	51.2	51.3	51.0	50.46
43.2	42.9	41.6	40.8	40.3	40.0	24.0	24:6	25:0	35.5	36.3	3 7. 0}	42.95
43:0	4040	40.0	40:5	10:0	41:0	34.2	34.6	35'0	40 .0	39.2	39.0	40.55
43.0 35.7	42.8	42.6	42.5	42.0	41.8	41.2 33.5	$\frac{40.5}{33.2}$	40.2 33.0	33.4	33.2	33.0	35.15
38.6	35.2	35.3	35.3	34.7	38.0 38.2	38 ° 4	39°0	38.6	38.0	37.6	37.6	36.70
35.4	38.5 35.1	38.5 33.7	38 · 2 33·6	38.4 33.5	33.0	32.8	32.6	32.0	31.2	30.7	30.4	34.57
33.2	33.6	33.0	32.7	32.5	31.8	31.8	31.8	31.7	31.6	31.9	31.9	31.92
41.5	40.7	40.7	40.6	40.2	40.4							37.10
-						34.0	34.3	34.6	35.0	35 .2	$\frac{-}{35.7}$	
40.2	40.4	40.8	41.3	41'3	40.6	40.6	40.7	40.8	40.9	41.1	41.0	39.43
44'7	44.0	43.3	42.2	42.0	42.0	42.4	41.8	41.0	40.5	40.2	40.0	42.70
37.2	37.0	37.0	36.2	36.2	37.0	37.0	37.0	36.7	35.7	35.2	34.4	37.55
40.4	40.1	40.4	40.6	39.8	39.6	39.4	39.0	38.7	38.2	38.8	38.2	37.73
43.4	43.0	43.2	42.8	42.5	42.0	41.6	40.6	40.4	40.2	40.6	40.6	41.42
40.3	40.0	40.0	38.2	38.2	38.2	35.7	35.7	35·7	36.0	36°4	37.0}	39.03
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1 639°3 660°3 638°4 638°7 639°6 638°4 632°1 632°7 638°6 633°3 638°6 638°3 638°6 632°5 632°3 638°6 632°5 632°3 638°6 632°5 632°3 638°6 632°5 632°3 638°6 632°5 632°5 632°3 638°6 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5 632°5		0	n e Scale Di	vision = '00	0087 parts	of the H.F.		NTAL FO		sponding to	1° decrease	of Tempera	ture, 1 63.	
1 639-3 6607-3 637-6 638-7 639-9 638-8 632-1 632-7 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-3 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5 639-5	Mean (gen T	Föttin-}	0h.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9h.	10h.	11h.
8 639.3 634.0 622.0 620.0 620.0 630.8 626.14 622.8 624.2 624.2 624.0 630.0 621.0 622.0 620.0 621.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 622.0 6		2 3 4 5 6	639°3 628°5 626°0 641°6 648°0	640°3 627°3 622°5 638°7 648°4	637°3 628°7 612°2 632°2 643°5	634°3 626°9 617°8 631°8 640°5	617.5 623.8 617.8 629.0 637.0	633.0 622.1 620.0 629.2 639.0	635.6 622.7 619.2 632.0 642.0	637.3 625.7 622.0 640.0 650.0	637.5 628.1 623.1 644.0 650.3	636°3 629°3 626°8 648°2 650°2	634.6 629.5 624.0 650.0 a 650.3	sc. Div. 633 '4 629 '3 629 '0 648 '2 650 '0 623 '6
18	TARY.	8 9 10 11 12 13	633°0 633°2 636°0 640°0	631.0 632.5 633.9 641.0	626.0 629.0 635.8 642.5	618.0 626.8 626.8 636.0	617.0 624.6 623.0 626.0	614.7 622.0 626.0 625.8	617.5 621.0 624.0 625.0	622.0 620.0 624.3 630.2	619*2 624*0 626*0 630*8	616.0 622.0 630.0 628.5	624.0 629.0 633.8 630.2	627.8 622.0 632.4 638.0 631.4 639.0
Courty Means 636'90 636'96 631'08 641'0 642'5 628'7 629'0 629'0 629'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'0 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 639'1 63	FEBRU	15 16 17 18 19 20	649.0 644.2 640.2 632.0	648 2 642 4 638 0 636 3	631.0 639.0 636.5 632.0	638.0 631.5 641.0 627.2	637.4 629.2 635.7 622.1	635°8 626°0 638°2 620°6	646'0 631'0 642'2 623'2	644.0 638.4 639.2 628.8	649.0 637.7 643.2 635.0	649°0° 639°4 633°2 636°0	647.6 640.0 638.5 635.0	636.06 637.6 637.0 634.5
TEMPERATURE OF THE BIFILAR MAGNET. 1		22 23 24 25 26 27	636.0 619.5 623.5 633.4	636.0 648.0 634.0 630.2	630°5 641°5 635°2 628°0	625°0 642°2 637°4 626°4	625°0 643°2 610°3 620°0	620°8 633°0 625°4 619°0	620.8 a 624.2 616.8 618.9	624.0 630.0 617.4 621.5	636°0 610°0 613°2 622°2	636.5 634.6 631.1 634.0	639.0 631.5 642.8 636.0	642.0 643.0 630.2 624.5
1 37.5 37.9 38.4 38.6 38.7 39.0 39.8 41.0 41.8 42.6 43.1 43.3 43.5 44.7 44.6 44.6 45.0 45.5 46.5 47.5 48.0 48.3 48.5 48.9 49.0 49.4 49.4 49.4 49.2 49.0 48.4 47.0 45.5 46.5 35.4 35.4 36.1 37.5 37.9 39.2 39.5 39.5 39.5 35.4 35.4 34.5 34.5 35.5 36.2 37.0 38.0 39.2 40.0 41.0 41.7 41.6 41.0 41.7 41.6 41.6 41.6 41.6 41.6 41.6 41.6 41.6 41.0 41.7 41.6 41.0 41.7 41.6 41.0 41.7 41.6 41.0 41.7 41.6 41.0 41.0 41.7 41.6 41.0 41.0 41.7 41.6 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.0 41.	Hourly	Means	636.90	636.98	632.22	631.08	626*39	626.70	627*11	629.86	631.18	633*89	635.72	634.67
THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O						ТЕМР	ERATURE (OF THE BIF	TLAR MAG	NET.				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	FEBRUARY.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	37.5 44.7 49.5 36.0 35.4 38.0 43.5 46.4 44.5 43.0 41.6 41.7 42.4 37.5 40.2 41.2 45.7 46.0 36.8 35.2 32.4 39.8	37.9 44.6 49.1 35.2 35.4 38.0 43.5 46.2 45.9 42.5 41.6 41.6 42.5 37.2 40.3 41.4 45.6 45.6 36.5 34.4 32.7 39.3	38.4 44.6 49.0 34.6 34.5 38.5 43.3 46.2 45.7 41.7 41.0 42.2 36.5 40.4 41.4 45.2 45.3 36.2 34.5 33.0 39.0	38.6 45.0 49.0 34.4 35.5 39.3 43.6 46.8 45.2 41.8 42.2 41.0 41.5 44.8 44.9 36.4 35.6 34.0 39.8	38.7 45.5 49.4 34.9 36.2 40.0 43.9 47.2 45.5 42.4 41.7 35.9 41.5 42.2 44.9 45.4 37.0 36.5 35.3 41.0	39.0 46.5 49.4 35.4 37.0 40.3 44.6 47.4 46.2 42.4 43.0 42.2 42.6 36.3 42.5 43.0 45.3 45.3 45.3 45.3 45.3	39.8 47.5 49.4 36.1 38.0 40.5 45.2 47.5 46.5 43.2 43.8 42.9 36.2 43.8 45.7 44.8 	41.0 48.0 49.2 37.5 39.2 41.2 45.5 47.4 47.1 43.7 45.3 42.9 	41.8 48.3 49.0 37.9 40.0 41.8 45.4 47.2 43.2 45.8 42.6 	42.6 48.5 48.4 39.2 41.0 42.5 45.9 47.3 47.5 43.0 42.6 43.0 44.5 47.5 44.5 47.5 44.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5 47.5	43.1 48.9 47.0 39.5 41.7 43.5 46.0 47.6 47.5 42.8 46.0 42.6 43.4 39.0 45.7 46.3 47.4 40.9 39.1 40.9 45.7	43°3 49°0 45°8 39°5 41°6 44°4 45°9 47°7 42°9 46°0 42°3
1941 14 MENUS II ALCOM I ALCOM I ALCOM I ALCOM I ALCOM I AUCUS I AUCUS I AUCUS I AUCUS I ALCOM I ALCOM I ALCOM	Hourt-					_			-					45.0

^{*} Five minutes late.

b Two minutes late.

[°] Three minutes late.

12 ^h .	13h.	14h.	15 ^h .	16 ^h .	17h.	18հ.	19 ^h .	20h.	21h.	22h.	23h.	Daily an
	! 			<u> </u>	<u> </u> 							Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
634°7	635.3	635.1	634'3	634.3	633.1	632.5	634.3	635 .3	632.6	632.6	631 .2	634.25
528.6	629.3	628.2	628.3	627.3	627.5	628.3	634.3	629.3	628.5	628.5	628.3	627.85
531.2	631.0	630.0	631.0	632.6	635.0	633.0	636.0	635.5	628.7	635.2	627.0	626.95
648.0	648.0	646'3	646.0	645.2	638.8	643 ·2	645.1	646.3	647.0	647.2	647.4	642.22
649 ° 8	647.8	648.0	646.4	646.2	640.1	642.0	643.2	642.4	637.9	639.0	642.0	644.75
28.4	630.0	624.1	610.0	623.1	624.0							629.51
	l —					637.5	632.5	637.2	637.0	638.0	$\left\{ \begin{array}{c} - \\ 640.2 \\ 627.0 \end{array} \right\}$	626.40
31.5	631.0	627.8	627.0	633.1	614.5	623.0	622.4	623.5	621.8	626.7		
23.2	631.0	622.0	627.2	628.8	630.3	628.7	628.5	629.2	630.0	631.5	631.3	625.10
30.3	630.0	6 30.0	632.0	633.0	630.2	630.0	628.8	631.1	631.3	633.8	626.0	628.46
32.2	634.6	637.0	639.2	639.6	639.8	638.0	637.0	637.2	635.9	636.8	639*2	633.20
33.1	633.0	635.8	632.0	633.2	638.5	638.0	638.0	639.0	640.0	641.2	640.3	634.20
40.0	641.4	642.4	644.0	644.0	644.0							641.7
					_	645.2	644.0	645.0	645.8	651.6	649.2}	
40.0	641.0	641'5	637.0	635.2	634.0	633.8	633.0	639.8	640.5	6 35 . 2	644.8	639.3
37.0	641.2	642.0	643.8	643.0	643.2	644.4	643.9	643.8	643.7	645.2	645.0	642.80
37.8	639.6	640.0	637.8	635.8	635.0	636.0	636.0	638.5	639.0	641.5	640.2	637:23
37.0	637.0	636.0	635.0	635.0	631.0	637.5	634.0	636.0	634.2	636.0	635.0	636.9
									633.0	633.5	632.8	632.3
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34.5	618.2	615.0	570:0	618.2	625.4	606.4	619.1	620.0	627.0	628.0	633.4	625.7
			579.8							639.5	640.0	635.30
40.8	639.0	635.4	632.1	639.0	637.9	638.8	643.0	644.4	646.0			
35.1	609.0	633.9	628.0	642.4	640.0	625.4	631.0	607.5	623.0	631.0	634.7	630.9
21.8	620.2	618.8	629.0	617.0	611.0	614.0	616.0	619.6	612.2	608.0	629.2	622.2
30.0	626.4	627.0	646.6	632.8	634.8	634.2	634.2	632.1	631.4	633.8	634.6	629*68
34.0	634.2	644.0	634.4	634.5	633.8						656.0}	632*39
	-					642.8	644.2	642.0	643.9	651.1	656.03	
34.60	633.32	633.95	632.38	634.53	633.14	634.18	635 · 30	635.16	635.00	636.35	637.57	633*26
				TE	MPERATUR	E OF THE E	BIFILAR MA	GNET.				
0		0	0		o		۰	۰		0		0
43.5	l				43.0			44.0	44.3	44.4	44.8	41.92
	43.6	43.6	43.5	43.3		43.0	43.4					
49.3	49.3	48.9	48.6	48.6	49.0	49.9	49.7	49.8	49.8	50.0	49.8	48.0
45.0	43.6	42.4	41.2	40.8	40.2	39.6	38.8	37.8	37.6	37.4	36.8	44 3
40.5	39.6	39.2	39.2	39.0	38.7	38'4	37.8	37.3	37.1	36.8	36.0	37.4
41.8	41.8	42.0	41.6	41.6	41.5	41.0	40.4	40.0	39.8	39.2	38.7	39.3
45.0	44.0	43.2	42.0	41.2	40.8		_				- 1	41.4
						40.9	41.0	41.5	42.0	42.6	$\{-\frac{1}{43\cdot 3}\}$	41 4
46'1	46.1	46.4	46.0	46.0	46.2	46.2	46.4	46.4	46.4	46.4	46.4	45.4
47.6	47.6	47.6	47.6	47.6	47.2	47.0	47.0	46.6	46.0	45.2	45.5	46.9
48.0								44.8	44.2	43.8	43.2	46.10
43.0	47.6	47.5	47.3	46.8	46.0	45.3	45.0				41.5	42.4
	42.0	42.2	43'0	42.8	42.5	42.2	41.7	41.4	41.9	41.9		43.0
45.4	44.2	43.2	43.0	42.7	41.4	41'1	41.0	41.0	41.4	41.8	41.8	43.0
42.4	42.2	41.3	41'4	41.6	42'0						$\{-\frac{1}{42\cdot 8}\}$	41.7
		-				39.0	40.0	41.2	42.0	42.6	42.87	
43.5	43.1	43.0	42.7	42.2	41.7	41.3	40.7	39.8	39.4	38.8	37.8	41.9
40.2	41.0	40.2	40.1	39.8	39.8	40.0	40.7	40.5	40.3	40.1	39.9	38.6
45'8	46.0	46.0	46.0	44.3	43.2	43.1	42.8	41.9	41.0	41.4	41.0	43.1
46.4	45.9	45.6	45.3	45.1	44.8	44.2	45.0	45.0	45.0	45.4	45.6	44.4
47.8									46.2	46.2	46.2	46.4
44'2	47.4	47.4	47.6	47.0	46.9	46.7	46.7	46.6	10.0		1	
	43.6	43.8	44.5	44.0	43.2	25.7	26.0	36.5	36.3	36.8	37.0}	42.4
40.8	1	1	43.4	1	4010	35.7	36.0			37.3	36.0	39:1
40.0	41.2	41.3	41.4	41.2	40.8	40.6	39.4	38.5	37.8			
~: · · · ·	40.0	39.4	37.9	36.2	36.0	35.2	34.6	34.0	33.6	33.2	32.4	36.5
	40.8	39.0	39.4	39.4	39.2	39.4	38.9	38.2	39.0	39.1	39.7	38.2
41.4		45.3	45.0	44.0	44.0	43.2	42.0	41.2	40.2	39.5	38.4	42.6
41°4 45°8	45.8				43.2	43.2	43.4	43.6	43.3	42.8	41.6	42.2
41.4		43.6	43'4	1 45 5				,	,			
41°4 45°8	43.9	43.6 44.8	43.4	43.3			_				- 1	40.00
41°4 45°8 43°5		43.6 44.8 —	43.4	44.2	44.5	36.6	36.7	36.9	37.1	37.1	37.4}	42.2
41.4 45.8 43.5 45.2	43.9	44.8	44.0	44.2	44.2	36.6	36.7	36.9		37.1		
41°4 45°8 43°5	43.9 44.8		44.0		44.2				37.1		37.4}	42:3

)ii	e Scale Divi	1 1 1 1	ooor parts t	i the II. F.	Increase, i	n Scale 171v	isions, corre	sponding to	1 decrease	or rempera	ture, 1 oo.	
lean Gött gen Tim	tin-}	Oh•	1 ^h .	2h.	3h.	4h.	5 ^h .	6 ^h •	7 ^h .	8h.	9h.	10 ^h .	11h.
	1 2 3 4 5 6	Sc. Div. 657 6 629 2 634 2 635 2 631 5 635 2	Sc. Div. 652'4 628'2 633'2 636'6 629'3 638'2	Sc. Div. 640 2 624 7 630 4 631 4 626 2 634 2	Sc. Div. 613 '2 624 '2 626 '6 624 '0 620 '2 629 '2	Sc. Div. 622 '3 618 '2 621 '6 613 '0 618 '3 624 '0	Sc. Div. 627 '0 618 '2 614 '2 606 '2 614 '7 613 '2	sc. Div. 613 2 619 4 610 2 609 3 612 6 612 7	Sc. Div. 616 6 620 2 610 6 615 2 612 2 614 8	Sc. Div. 608 0 622 7 619 8 620 7 614 2 625 5	sc. Div. 635 ' 4 625 ' 2 623 ' 3 623 ' 2 623 ' 9 627 ' 7	sc. Div. 626 6 626 4 631 2 626 2 629 4 632 0	Sc. Div 624 2 623 2 630 8 621 2 624 2 635 8
	7 8 9 10 11 12 13	635°0 635°2 627°6 632°2 645°2 647°0	635.0 616.5 635.0 631.3 647.0 645.0	632.5 632.0 631.4 629.0 641.0 639.0	625 · 2 616 · 5 633 · 9 629 · 0 639 · 8 643 · 0	613 · 8 622 · 5 623 · 2 627 · 0 636 · 0 641 · 7	612 · 4 614 · 4 619 · 1 626 · 2 632 · 0 638 · 3	612.0 613.8 619.0 628.6 634.6 636.0	617.8 614.0 612.5 629.5 632.4 637.8	630.8 629.8 621.0 632.0 635.0 639.2	616 2 631 7 632 0 632 0 638 2 651 4	628.6 635.8 629.0 637.0 644.0 651.2	631 ° 0 640 ° 0 626 ° 8 637 ° 8 644 ° 8 656 ° 5
MARCH	15 16 17 18 19 20 21	650°0 646°0 649°1 642°0 628°0 607°6	645.2 641.2 648.1 640.0 585.0 607.0	637.4 636.2 644.2 637.0 558.0 610.0	632 · 2 628 · 0 635 · 0 624 · 0 541 · 1 610 · 0	619.7 621.0 627.7 613.2 554.0 604.5	620.5 617.1 623.8 610.0 575.0 609.8	621.6 625.0 622.5 615.0 c 586.5 608.8	624.4 637.0 624.0 620.0 586.5 609.8	624'1 643'0 636'0 628'6 600'1 609'2	638'8 648'0 642'5 628'0 637'7 609'0	638.5 642.7 648.0 632.2 634.0 606.8	640.0 641.0 646.7 635.8 614.8 606.5
	22 23 24 25 26 27	631 · 2 636 · 8 620 · 0 621 · 3 617 · 0 628 · 8	633°0 631°4 622°0 616°0 611°2 631°0	631 ° 0 626 ° 0 612 ° 7 616 ° 5 612 ° 0 630 ° 2	626°5 623°0 605°5 612°6 611°6 623°5	618.6 614.0 609.0 606.0 601.5 621.0	613.2 614.0 602.5 596.0 601.0 623.1	615.3 612.0 600.5 603.2 602.8 626.2	615.0 614.0 609.8 607.5 611.8 628.2	620°0 618°0 611°2 610°0 611°0 633°2	623°0 624°5 618°2 615°2 621°0 634°0	628.0 630.0 628.7 614.2 617.0 633.2	629'0 634'8 630'2 620'4 620'0 634'7
	28 29 30 31	641°0 637°0 638°0	639°2 634°5 641°0	634.0 627.2 635.0	625.6 622.2 626.8	617·7 612·5 617·3	614.0 614.5 617.2	614.0 615.5 618.0	616.0 616.5 622.5	619°8 625°0 625°8	624.0 630.2 634.8	631.0 633.8 637.8	630°4 636°8 639°8
Hourly M	Ieans	635.03	633.40	630.05	624.28	618.67	615.87	616.10	618.83	623.60	628.90	631.21	632.4
	i	37.0	. 0	0 .			F THE BIF				4Î.0	41.1	4 <u>1</u> °·2
	1 2 3 4 5 6	40.5 44.7 44.8 43.5 45.4	37.0 40.4 44.5 44.4 42.2 44.6	37.0 40.6 44.0 45.0 41.5 45.2	37.6 42.7 44.2 46.2 42.4 46.4	38.6 43.5 44.6 47.1 44.5 47.4	39.7 43.5 45.2 48.0 46.1 48.5	40°2 44°5 46°1 48°3 47°0 49°0	40.7 45.3 46.8 48.8 47.3 49.5	41°2 46°0 47°2 48°9 48°4 49°5	46.5 48.2 49.9 49.0 50.0	41 1 47 2 48 8 50 4 49 6 49 8	41 2 47 6 48 9 50 4 49 7 49 4
	7 8 9 10 11 12 13	44°1 42°2 40°6 41°1 35°7 37°5	43.5 41.3 40.5 40.6 35.4 37.5	44.8 40.7 41.0 40.3 36.4 37.7	45.6 40.4 42.2 40.7 38.0 38.5	45.8 40.4 42.8 40.6 39.2 39.6	46.6 40.4 44.4 40.8 40.0 41.3	46.8 40.6 44.9 42.0 41.1 41.8	47.4 41.0 45.5 42.4 41.5 42.4	47.4 40.9 45.6 43.0 41.7 43.2	47.4 41.1 46.0 43.5 43.0 44.2	47.9 41.2 46.0 44.5 43.0 44.8	47 · 9 41 · 0 46 · 0 44 · 2 43 · 6 45 · 2
MARCI	14 15 16 17 18 19 20	38.7 37.4 36.5 44.2 44.9 49.0	38.7 36.4 36.2 44.0 44.9 48.3	39.0 37.0 36.8 44.2 46.4 48.0	39.2 37.0 38.0 44.9 47.0 48.0	39.9 37.5 39.4 46.0 48.8 48.4	41:3 38:0 41:2 47:1 48:7 48:8	42.2 38.8 41.8 48.4 49.7 49.5	42.6 39.6 42.7 49.0 49.9 50.1	42.4 40.4 42.9 49.7 50.0 50.2	42.5 41.4 43.9 51.2 50.6 50.4	42.5 41.7 44.7 52.0 50.8 50.4	42.4 41.9 44.7 52.4 51.7 50.0
	21 22 23 24 25 26 27	41.8 46.8 47.2 50.0 49.5 40.6	42.0 46.6 47.2 48.7 48.6 40.0	42.4 46.6 48.4 50.5 48.0 40.0	43°0 46°7 49°0 51°4 48°4 40°4	43°0 47°0 49°8 52°0 48°7 40°9	43°1 47°7 49°9 52°4 49°4 41°4	43.8 48.4 49.9 52.4 49.8 41.2	44.0 49.1 50.0 52.1 50.3 41.0	44.0 49.4 50.5 52.2 50.6 41.4	44.4 50.5 51.3 52.6 51.0 42.4	44.9 50.8 51.8 52.6 51.0 42.6	44°5 51°3 52°6 52°5 50°4 43°0
	28 29 30 31	43.2 44.4 42.0	43.7 44.0 43.3	44.8 44.8 44.9	46.4 45.0 45.5	48.0 45.2 45.9	49.0 46.0 46.2	49.8 46.0 46.3	50°0 46°0 46°8	50°0 46°0 46°8	50°0 46°2 46°8	50°3 44°8 46°8	50°0 44°6 46°6
Iourly N	Means	42.64	42.29	42.68	43.38	44.07	44.85	45.41	45.84	46.13	46.71	46.97	47.0

^a Six minutes late.

	One Scale	Division =	*000087 pa	rts of the H		ZONTAL I se, in Scale		orresponding	to 1° decre	ease of Tem	perature, 1°6	53.
12h.	13 ^h .	14 ^h .	15h.	16 ^h .	17h.	18h.	19 ^h .	20h.	21h,	22h.	23h.	Daily an Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 628 2	Sc. Div. 627 29
635.4	633.0	620.2	632.1	624.1	622.2	623.8	624.2	624.2	625.6	625.2	633.2	626.97
627.6	628.3	628.9	630.2	630.4	629.2	629.3	632.2	632.2	632.2	633.7		
630.2	632.0	632.2	631.2	629.2	630.4	631.2	632.4	632.6	633.2	633.4	634.2	627.85
612.7	619.2	614.4	619.6	611.4	616.0	613.5	621.6	619.7	623.0	624.0	625.3	620.11
626.4	612.8	620.2	622.0	630.2	631.7	631.4	631.6	633.2	634.4	634.2	634.0	624.95
335.8	633.8	630.6	612.0	633.7	623.0						$\frac{-}{628.6}$	626.30
						628.0	618.8	619.0	626.5	619.0	628.6	
615.6	618.9	609.8	635.0	623.8	626.7	634.2	626.0	628.5	621.2	619.0	632.6	624.23
538.5	640.0	640.0	638.0	641.0	643.0	643.5	639.6	639.4	640.0	638.8	640.0	632.67
930.0	631.8	633.0	634.5	634.0	635.0	635.8	635.0	635.4	635.2	635.0	633.1	629.93
933.0	637.2	638.0	638.0	640.4	639.8	641.2	642.0	641.7	644.8	646.0	646.4	635.84
645.0		638.0							639.0	640.8	644.0	639.68
	644.8		638.0	634'1'b	638.2	641.4	640'1	639.0	099 0	040 6		003 00
32.8	638.1	641'9	634.0	638.8	638.0						$\frac{-}{647.8}$	$642^{\circ}55$
_	<u> </u>	—				641.0	645.9	644.5	643.5	648.8		
640.4	640.9	644.0	643.0	641.5	644.0	643.8	642.8	643.2	643.8	645.2	644.4	637.89
41.0	643.0	644'0	646.2	646.0	646.2	646.6	646.5	646.4	648.2	650.2	649.0	640.81
46.0	645.8	644.2	641.2	644.2	643.4	643.2	642.9	641.1	642.8	637.8	639.0	639.97
33.8	630.8	624.8	611.2	621.0	621.4	610.0	607.9	609.8	619.0	607.0	617.0	622.49
82.5	606.1	604.0	584.2	508.0	443.2	576.7	604.0	617.0	597.0	604.0	610.8	584.9
						370 7	004 0	017 0	037 0	0010	. 1	
89.0	589.4	610.0	607.5	602.0	567.5		20510	605.6	600:0	600:3	$\frac{-}{631\cdot 2}$	609.33
						622.5	625.0	625.6	626.0	629'3	001 2)	000.00
31.6	632.2	631.0	630.3	630.2	631.8	629.2	626.8	627.2	630'1	630.0	631.8	626.92
20.3	612.6	600.0	604'4	604.8	604.5	599.8	602.0	612.0	609.0	618.0	615.4	615.89
17.5	622.8	615.8	617.8	619.1	621.9	607.0	607.5	619.0	622.0	621.6	624.2	616.10
21.0	619.0	619.6	618.0	619.8	619.0	614.4	613.0 q	614.0	614.5	614.0	611.0	614.0
20.0	620.8	622.0	624.8	625.0	624.5	624.3	624.2	627.3	624'4	624.0	632.2	617.99
39.0	636.2	635.8				024 0	024 2	021 0	021 1	021 0		
03 0	000 0	000 0	633.4	638.0	632*2		000:0	633.8	633.6	639.3	641.2	632.40
						637.2	632.0				041 47	628.60
31.8	633.0	632.6	632.2	622.8	630.4	633.0	633'1	633.7	630.0	632.0	635.0	
28.4	632.5	636.0	636.8	637.1	635.0	636.9	637.0	636.4	640.3	638.0	638.7	630.63
35.5	636.2	636.3	635.4	632.1	633.4	636.2	638.2	640.0	639.2	642.8	642.0	633.39
	629.44	628.59	628.72	629.03	628.02	629.95	629.56	630.73	631.61	631.81	633.84	627.88
				<u> </u>	MPERATUR		1		· · · · · · · · · · · · · · · · · · ·		1	
0	. 0	0	0						0	0	1 0 1	0
4i°3	4η5	4Î.8	42°0	41.8	41.3	4i°0	40.7	40.9	40°8	41.0	40.6	40°29
46.3	45.7	45.4	45.0	44.7	45.0	45.0	44.7	44.9	45.2	45.2	44.8	44.59
48.8	48.6	48.5	48.1	48.0	48.0	47.5	46.6	46'4	46.0	45.3	44.7	46.6
50.5	49.6	49.2	48.2	48.0	47.2	46.8	46.0	45.2	44.2	43.8	43.1	47.2
49.3									46.1	46.0	45.6	46.5
	48.6	48.2	48.0	47.5	47.4	47.2	46.6	46.1	1	1		Į.
49.2	48.6	48.4	47.1	46.6	46.3	. .				44:4	44.1}	47.0
47.0		_				45.4	45.2	45.0	44.6	44.4	44 1)	I
47.6	46.5	45.6	45°0	44.4	43.8	43.2	42.9	43.0	43.0	42.9	42.6	45.2
40.7	40.4	40.0	40.0	40.0	40.6	41.0	41.0	40.8	40.7	40.7	40.8	40.7
45.7	45.0	44.6	44.2	43.7	43.0	42.0	42.0	41.6	41.5	41.6	41.6	43.4
43.6	43.0	42.6	42.0	41.2	40.6	40.2	39.3	38.4	37.8	37.1	36.2	41.0
43.5	43.6	43.0	41.5	40.6	39.6	38.6	37.6	37.3	37.0	37.0	37.4	39.8
43.7	42.4	42.6	41.9	41.5	41.2	-						1
_	t	1	i		1	39.9	40.4	40.7	41.0	40.9	40.4	41.2
$\frac{-}{42 \cdot 3}$	41:4	41:4	41:0	40.5	40:0	,				38.0	37.6	40.4
	41.4	41.4	41.0	40.5	40.0	39.8	39.7	39.5	38.8		$\begin{vmatrix} 37.6 \\ 37.2 \end{vmatrix}$	39.0
41.5	40.6	40.2	40.2	39.8	39.0	38.8	38.4	37.8	37.9	38.0		ſ
44.8	44.3	44.5	44.0	43.9	44.0	44.2	44.5	44.5	44.8	44.6	44.4	42.5
52.3	51.4	50.3	49.1	48.8	48.5	47.9	47.2	46.4	46.0	45.9	45.1	48.0
51.5	51'2	50.4	49.7	49.0	48.5	48.4	48.5	48.5	48.6	49.0	49.0	48.9
20.0	50:0	50.1	50.1	50.0	49.5			_			1	47.6
	_	_		_	15 0	42.2	42.2	42.2	42.2	42.0	$\frac{1}{41.6}$	410
44.9	45.4	45.4	45.6	45.6	l .	45.7	45.4	45.4	45.8	46.2	46.5	44.5
51.2					45.7				48.3	47.9	47.4	48.9
52.8	51.0	50.6	50.2	50.0	50.0	49.7	49.3	48.9			50.0	50.1
	52.2	51.2	51.0	50.4	50.1	50.0	49.8	49.6	49.3	49'4		
52.2	51.6	51.6	51.4	51.2	51.2	51.4	51.1	51.1	50.5	50.3	49.8	51.3
49.9	48.5	48.0	46.6	46.0	45.4	44.9	44.3	43.7	42.8	42.2	41.5	47.4
42.9	42.5	42.5	41.6	41.4	41.2	_	_				— 1	41.6
						41.4	41.6	41.8	42.1	42.5	$\left\{\begin{array}{c} -1 \\ 43 \cdot 1 \end{array}\right\}$	41 0
20.0	48.8	48.3	48.2	47.6	47.2	47.3	46.6	46.4	$\frac{12}{45.7}$	45.1	44.8	47.50
45.2	45.2	48.5					43.5	42.4	41.8	41.7	41.3	44 2
46.3		3	44.0	43.7	43.5	43'4				41.5	41.2	44.4
-∨ ບ	45.0	44.2	43.9	43.6	43.2	43.0	42.6	42.0	41.6	41.0	71 4	77 4
46:79	46.21	45.88	45.39	45.02			43.80	43.24	43.30	43.12	42.83	44.7

^{*} Five minutes late.

	Oı	ne Scale Div	vision = '00	0087 parts o	of the H. F.		NTAL FO		sponding to	1° decrease	of Tempera	ture, 1°63.	
Mean (Göttin-}	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h ·	8h.	9h.	10h.	11h.
	(1 2 a	Sc. Div. 642 2	Sc. Div. 636 7	Sc. Div. 636°2	Sc. Div. 634 • 5	Sc. Div. 627 3	Sc. Div. 622 8	Sc. Div. 622 4	Sc. Div. 626 2	Sc. Div. 631 0	Sc. Div. 636'8	Sc. Div. 641 4	sc. Div. 636°0
	3	640.0	631.0	608.0	617.0	612.5	597.0	582.2	593.0	613.0 р	613.5	659.0	631.4
	4 5 6 7 8 9 10	629 ° 0 622 ° 0 621 ° 2 619 ° 2 609 ° 0 617 ° 0	622.5 615.8 626.0 601.0 608.0 617.5	613.5 610.6 619.4 601.0 605.0 612.0	610°2 602°2 609°9 598°2 600°0 606°8	601.0 593.2 599.5 592.4 591.0 600.0	600.8 595.5 596.1 591.0 ° 590.0 602.0	600.8 603.8 599.1 594.5 d 600.5 604.0	606.4 608.0 620.8 599.2 604.2 610.8	606°0 617°0 635°0 614°5 612°2 614°2	620.8 625.3 602.0 613.5 617.0 618.8	630°8 625°0 620°0 610°0 614°0 618°2	624.2 620.0 633.0 611.2 609.8 616.8
APRIL.	12 13 14 15 16 17	633.6 628.0 617.7 614.0 626.0 608.4	630°2 628°4 614°8 612°0 625°0 619°7	624.6 620.4 c 611.8 603.0 617.0 613.0	616.0 610.2 604.0 589.0 604.2 603.8	610.0 601.0 590.8 583.2 593.0 594.1	610.0 600.6 592.5 584.0 593.2 f 594.2	616.8 610.1 598.0 592.2 606.0 598.5	633.4 620.8 608.5 607.2 604.0	638 · 8 632 · 7 610 · 0 620 · 0 612 · 5 608 · 6	649.0 645.4 621.5 628.0 626.0 624.1	639°1 639°0 624°2 632°2 628°8 626°2	606.0 620.0 628.0 623.9 632.0 629.0
	18 19 20 21 22 23 24 25	640°0 572°2 592°4 600°7 609°0 625°5	637 · 2 504 · 5 530 · 0 598 · 0 605 · 2 621 · 0	630°0 490°5 575°0 584°0 602°4 614°0	622°0 545°1 572°0 585°6 600°0 608°0	621.6 561.0 569.5 582.8 596.2 605.0	625°4 581°0 573°6 575°5 599°8 613°8	629°0 599°0 595°0 586°2 607°5 622°8	633°0 616°0 609°0 587°0 614°2 626°9	646°0 635°0 605°2 602°0 614°1 628°0	642.8 640.0 597.0 604.0 620.5 625.0	645.0 632.0 607.4 596.0 616.8 621.0	647.0 615.8 640.5 603.8 614.0 617.5
	25 26 27 28 29 30	627 ° 0 621 ° 8 628 ° 5 626 ° 4 598 ° 2	623.8 617.7 621.0 621.0 595.0	617.8 613.0 616.2 615.0 607.8	616°0 602°0 619°0 610°0 612°0	611.0 603.0 615.0 610.5 614.0	614.8 604.0 629.0 617.4 600.2	620°0 605°0 619°0 626°2 593°0	623 · 5 621 · 0 630 · 2 625 · 1 609 · 1	628.0 622.6 637.4 632.0 612.9	632.0 617.0 631.0 648.2 618.2	626 ° 9 620 ° 0 628 ° 2 635 ° 9 648 ° 0	627.0 621.8 629.5 637.0 641.0
Hourly	Means	621.10	617.40	611.73	607.08	601.29	601.34	605.51	612.66	619.40	625.49	627.65	622.85
					ТЕМРІ	ERATURE O	F THE BIF	LAR MAGN	ET.		,		
1	1 2 a	4Î °0	40°5	4i°0	42.2	43.5	44.5	45.0	45.6	45°5	46°0	46°1	45.8
	3 4	44.4	44.8	45.2	46.6	47.8	49.0	50.0	50.6	51.0	51.8	52.4	52.6
	5 6 7 8 9 10	45.5 49.4 51.8 54.0 52.0 51.9	46.9 49.2 51.6 53.7 52.3 52.5	48.3 49.5 51.9 54.0 52.8 53.7	50.0 49.8 51.9 54.3 53.4 54.2	51.4 50.4 52.1 54.8 53.7 54.2	51.8 51.8 52.8 55.5 53.9 54.2	52.3 51.8 53.1 56.4 54.3 54.4	52.6 52.4 53.8 57.5 54.0 54.6	52.6 52.5 54.5 58.5 54.1 54.8	52.6 53.0 55.7 59.4 54.8 54.6	52.5 53.4 56.4 60.0 55.3 54.6	52·3 53·7 57·4 60·5 55·4 54·1
APRIL.	12 13 14 15 16 17	48.2 49.5 51.0 49.5 45.7 48.6	48°3 50°1 51°4 49°8 46°4 48°6	48.8 51.2 52.3 49.9 47.1 48.6	49.5 51.5 52.8 50.0 48.2 48.6	50°3 51°6 53°2 49°9 48°6 48°5	50.5 51.9 53.2 49.9 48.8 48.9	50.9 51.9 53.0 49.9 48.7 49.4	51.4 51.9 53.0 50.5 49.2 49.4	51.8 51.9 53.4 51.0 48.7 49.0	52.5 52.4 54.0 51.6 48.3 49.0	53.7 53.0 54.9 52.0 48.3 48.5	53.5 53.0 54.7 52.0 48.7 47.8
	18 19 20 21 22 23 24	41.6 48.9 52.4 61.5 53.5 49.6	41.9 49.1 52.4 61.5 53.0 50.2	42.2 49.3 53.0 61.0 52.6 50.9	42.5 49.0 53.2 60.8 52.4 51.5	43°1 49°6 53°3 60°5 53°0 52°4	43°5 50°0 53°5 60°4 53°6 53°5	44.3 50.8 54.5 60.2 54.0 53.9	45.2 51.4 55.6 60.0 54.0 54.0	46.0 51.6 55.5 59.5 54.4 54.2	46.7 51.9 57.0 59.5 55.3 54.7	47.2 52.4 59.4 59.5 55.7 55.3	48.5 52.2 59.9 59.0 55.5 55.7
	25 26 27 28 29 30	52:3 54:8 49:0 49:8 49:8	52.4 55.0 50.4 49.5 49.8	52.5 55.0 51.0 49.3 49.8	52.8 56.0 51.5 49.0 50.6	53.8 55.8 52.0 49.4 50.9	54.5 55.2 52.3 49.8 51.3	55.5 55.0 52.3 50.2 51.4	56.5 54.7 52.5 50.2 51.8	57.4 54.7 52.6 50.7 52.4	58°3 55°0 52°8 51°8 53°0	58.8 55.0 52.5 51.9 53.4	59°0 55°3 52°3 51°7 53°2
Hourl	y Means	50.02	50.30	50.69	51.52	51.70	52.12	52.40	52.69	52.89	53.35	53.66	53.61

a Good Friday.

^b Four minutes late.

^e Seven minutes late.

:	One Scale	Divsiion =	*000087 pa	rts of the II.		ZONTAL se, in Scale		orresponding	to 1° decre	ease of Tem	perature, 1 · (33.
12h.	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
sc. Div. 639 ° 0	Sc. Div. 641 ° 0	Sc. Div. 639.0	Sc. Div. 633.5	Sc. Div. 631 0	Sc. Div. 632 2	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	sc. Div.	Sc. Div.
641.1	598.8	597.0	629.0	607.2	584.6	640 · 9	637.8	636.6	640.6	637.0		616.12
619.6	618.8	625.5	619.4	617.0	628.8	619 . 0	627.0 622.0	617 . 4	617 .0 623 . 0	$622.5 \\ 623.2$	629·0 622·0	617.99
620.0	625'4	611.0	618.2	620.0	613.0	617.0	623.3	616.6	622.0	620.0	613.8	614.95
625°0 593°7	614.2 596.3	606°0 597°0	570°0 582°5	530 .4 59 6.2	463.5 591.2	49 3 8 593 0	407 . 8 597 . 1	240°0 601°6	435 ° 9 603 ° 0	489°0 609°0	610.8	561.15 600.71
611.2	607.8	608.0	613.0	613.1	612.8	613.4	615.0	614.4	614.0	618.4	618.0	609.16
616.4	— 616.0	617.2	615.0	617.0	616.4	627.0	629.2	629.2	632.0	634.0	634.7	617:59
619.6	619.8	620.1	622.0	625.0	623.0	627.0	625 .2 617.0	628 . 0	628°0 619°0	628.2 618.2	630 . 8 623 . 1	$625.18 \\ 620.18$
623.5 617.0	625°0	600.0 612.0	601.6 603.0	615.0	620°0 606°4	622 . 2	613.9	611.9	616.0	616.2	617.4	610.13
617.8	615.8	621.2	615.0	618.0	620.6	624.7	620.0	620.0	618.8	619.0	626.2	613:57
629 · 2 628 · 8	634·1 625·9	$610\cdot2$ $623\cdot4$	59 1. 0 626.0	607.2 627.0	611.0 626.0	626.0	623.5	611.5	624.0	626.2	623.4	616.16
			-			639.2	639.3	639.8	640.2	640.7	$\begin{bmatrix} -639.2 \\ 547.2 \end{bmatrix}$	621.63
645°0	645.0 606.0	$645.0 \\ 610.0$	639 . 2 612 . 8	643.4 610.0	649°0 614°8	641.2 615.5	$625.9 \\ 612.0$	519 . 4 598.0	$\frac{477.1}{611.2}$	536°6 620°8	547°3 624°0	618.05 597.59
619.5	596.8	299.0	590.9	601.1	604.2	598.0	600.2	597.1	599 °0	599.0	601.2	594.70
603.0	602*1	602.0	604.8	604.0	604.8	606.0	604'0 614'2	603°5 615°2	605°2 617°6	608°0	609°2 622°4	598'42 611'86
617.0	616.0	611.5 617.5	618.0 613.0	615 .0 617.4	613°0 617°0	615.0					11	619.75
						622.0	623.8	625.0	623.4	$\frac{623\cdot 2}{620\cdot 2}$	$\frac{-}{626\cdot 1}\}$	619.32
618.8 620.0	605°2 617°8	609.8 617.8	618 . 2	616 . 4 620 .0	615.6 622.1	616.0 621.1	617.4 ° 622.0	619 . 0 621 . 8	619 . 4 624.0	620.2	626.2	617.61
621.1	618.0	616.5	619.0	622.0	626.0	628.1	625.0	613.0	615.0	605.0	627.0	622.47
619.0	618.0	605.0	618.0	614'0	620.0	617.0	613.0	580°3 618°2	610.0	612 ` 2 620 ` 0	595.8 61 5 .0	617.79 614.70
	631.0	608.2	608.8	615.2	611.5	612.0						
619.92	616.70	613.00	613.98	615.41	615.03	620.19	620:37	617.26	620.52	621.02	620.96	616.12
,				TEM	PERATURE	OF THE B	IFILAR MA	GNET.			1	
45.4	44.6	44°3	4 4 °4	4ŝ·0	45°6	<u>-</u>	-	<u>-</u>	<u>•</u>	0	· 44·4}	。 44·36
52.9	52.4	52·4	51.8	51.3	50.6	44.9	45.0	44.9	44.6	44.8	1	48.96
52.0	_				40:5	46.7	46.1	46.1	46.0 49.2	$\frac{46.0}{49.2}$	46.6 } 49.2	50.33
53.6	51.0 53.4	50.8 53.2	$50^{\circ}2$ $53^{\circ}2$	53.0 50.0	49.5 52.8	49.4 52.5	49.4 52.3	$\frac{49\cdot2}{52\cdot3}$	$52 \cdot 2$	$\frac{49}{52}$	52.2	52.07
58.3	57.6	57.5	57.0	56.0	55.7	55 • 2	54.7	54.0	54.2	54.0	53.9	54.63
59.6 55.1	58.2 54.2	57.4 53.8	57.0 53.4	56.6 52.9	55.7 52.4	55°2 52°1	54.4 52.0	54.0 52.0	53 ·4 51·8	$\begin{array}{c} 52.9 \\ 51.7 \end{array}$	52.5 51.6	56.06 53.29
53.8	53.1	52.4	51.9	51.2	51.2						48.4}	51.88
53.7	52.6	52.3	52.0	51.8	51.5	46°5 51°1	46.5 51.0	46.6 51.0	47.4 50.8	48.0 50.4	49.6	51.13
53.4	5 3.0	52.9	52.9	52.8	52.6	52.6	52.2	51.8	51.3	51.1	51.1	51.98
51.3 51.3	53.5 50.4	53°3 49°7	52.9 49.1	52.6 48.7	$\begin{array}{c} 52\cdot2\\ 48\cdot2\end{array}$	52.0 48.0	51.5 47.2	50°9 46°8	50°4 46°5	50.0 46.2	49.8 46.0	52.50 49.34
48.9	48.2	48.1	47.8	47.8	47.8	48.2	48.2	48.2	48.4	48.5	48.7	48.16
48.0	47.1	46.6	46.2	43.2	43.0	<u></u> 40 ° 4	41.0	41.4	 41.4	41.6	41.4}	46.10
49.4	49.4	49.4	49.5	49.5	49.4	49.4	41 0	49.0	49.2	49.4	49'1	46.85
52·2 60·6	52.0	52.4	52.5	52.8	53.0	53.4	53.0	53.0	52.8	52.6	52·3 61·6	51.59
59.0	61.4	62°1 58°2	62.5 57.8	62.5 57.2	62.0 56.6	62'0 56'0	61.9 55.5	61.5 55.0	61.5 54.5	61.5 54.5	54.5	58:37 58:35
55.5	54.6	54.3	54.0	53.4	53.0	52.6	52.0	51.7	51.3	51.3	20.0	53.36
55 . 6	55.1	55.0	54.2	54.5	54.0	51.2	51.2	51.3	51.4	51.7	$\left[\begin{array}{c} \overline{} \\ 52 \cdot 0 \end{array}\right]$	53.02
59.0	58.7	58.7	58.2	57.5	57.0	57.2	56.8	56.6	56.2	55.5	55.2	56.27
21.9	54.0	53.0 50.4	52 .5 49.7	51.6 49.5	51'1 49'7	50.6 49.6	50°3 49°5	49'8 49'5	49.4 49.5	49°2 49°5	48.5 49.8	53.19 50.87
51.7	51.4	51.3	51.2	51.2	51.1	51.1	51.0	50.8	50.8	50.4	20.0	50.66
52.5	51.6	51.3	51.3	50.8	50.5	50.5	49.6	49.2	49.0	49.1	48.2	50.86
53.42	52.71	52.35	52.01	51.28	51.23	50.39	50.13	49.96	49.79	49.70	49.21	51.56

⁴ Five minutes late.

e Eight minutes late.

f Ten minutes late.

	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	Sc. Div. 623·1 — 624·0 621·0 621·3 624·8 622·8 450·7 — 613·0 607·8 604·8 599·5 608·0 581·5 — 598·8 595·9 599·0 599·0 599·0	Sc. Div. 621'9 	Sc. Div. 625'0 — 621'2 614'4 612'0 616'4 618'0 538'0 — 609'0 600'0 596'0 592'5 597'0 610'2	sc. Div. 622'0 — 616'0 603'0 603'8 609'8 605'0 545'2 — 603'2 596'4 594'0 588'0	Sc. Div. 603'9 ————————————————————————————————————	sc. Div. 598 '0 — 611 '0 603 '0 602 '0 597 '2 598 '0 580 '0 — 598 '4 602 '5	Sc. Div. 609 0 615 9 609 0 607 8 600 0 603 8 593 5	Sc. Div. 613 '2 ————————————————————————————————————	Sc. Div. 625 0 	Sc. Div. 636'0 	Sc. Div. 632 0 ————————————————————————————————————	Sc. Div 627'4 619'4 625'4 622'2 616'0 615'2
	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	624.0 621.0 621.3 624.8 622.8 450.7 — 613.0 607.8 604.8 599.5 608.0 581.5 — 598.8 595.9 599.0	624.5 621.0 620.8 620.0 623.0 539.0 	621'2 614'4 612'0 616'4 618'0 538'0 — 609'0 600'0 596'0 592'5 597'0 610'2	616.0 603.0 603.8 609.8 609.0 545.2 	614.0 601.2 598.8 603.4 596.2 589.0 598.0 596.8	611.0 603.0 602.0 597.2 598.0 580.0	615 '9 609 '0 607 '8 600 '0 603 '8 593 '5	622'0 616'2 613'4 609'6 605'0	618.0 621.2 624.4 613.7 605.0	625.8 624.0 614.0 613.0	620°2 628°2 621°8 616°2	619 .4 625 .4 622 .2 616.0
	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	621'0 621'3 624'8 622'8 450'7 — 613'0 607'8 604'8 599'5 608'0 581'5 — 598'8 595'9 599'0	621'0 620'8 620'0 623'0 539'0 — 607'0 602'7 601'2 600'9 607'0 596'5 — 594'4 598'0	614'4 612'0 616'4 618'0 538'0 — 609'0 600'0 596'0 592'5 597'0 610'2	603.0 603.8 609.8 605.0 545.2 	601°2 598°8 603°4 596°2 589°0 — 598°0 596°8	603.0 602.0 597.2 598.0 580.0 	609'0 607'8 600'0 603'8 593'5	616*2 613*4 609*6 605*0	621.2 624.4 613.7 605.0	625.8 624.0 614.0 613.0	628.2 621.8 616.2	625 . 4 622 . 2 616 . 0
	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	624 '8 622 '8 450 '7 — 613 '0 607 '8 604 '8 599 '5 608 '0 581 '5 — 598 '8 595 '9 599 '0	620.0 623.0 539.0 	616.4 618.0 538.0 ————————————————————————————————————	609.8 605.0 545.2 	603.4 596.2 589.0 	597.2 598.0 580.0 — 598.4	600.0 603.8 593.2	609.6 605.0	613.7 605.0	614.0 613.0	616.2	616.0
	7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	622.8 450.7 613.0 607.8 604.8 599.5 608.0 581.5 598.8 595.9 599.0	623.0 539.0 	618.0 538.0 — 609.0 600.0 596.0 592.5 597.0 610.2	605.0 545.2 	596.2 589.0 598.0 596.8	598°0 580°0 — 598°4	603°8 593°5 —	605.0	605.0	613.0		
	8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	450.7 ————————————————————————————————————	539.0 	538.0 609.0 600.0 596.0 592.5 597.0 610.2	545.2 603.2 596.4 594.0 588.0	589.0 598.0 596.8	580°0 	593 · 5				019 0	010 2
	10 11 12 13 14 15 16 17 18 19 20 21 22	607.8 604.8 599.5 608.0 581.5 598.8 595.9 599.0	602.7 601.2 600.9 607.0 596.5 594.4 598.0	600.0 596.0 592.5 597.0 610.2	596.4 594.0 588.0	596.8		600.0				604'0	597.0
	11 12 13 14 15 16 17 18 19 20 21 22	607.8 604.8 599.5 608.0 581.5 598.8 595.9 599.0	602.7 601.2 600.9 607.0 596.5 594.4 598.0	600.0 596.0 592.5 597.0 610.2	596.4 594.0 588.0	596.8			609.0	608.8	610.4	608.4	608.4
	12 13 14 15 16 17 18 19 20 21 22	604.8 599.5 608.0 581.5 598.8 595.9 599.0	600.9 607.0 596.5 594.4 598.0	592.5 597.0 610.2	588.0	593.5	1002 0	602.8	607.9	607.0	607.2	602.8	605.0
MAY.	14 15 16 17 18 19 20 21 22	608.0 581.5 598.8 595.9 599.0	607.0 596.5 594.4 598.0	597.0 610.2			596.8	601.9	606.0	608.0р	609.1	607.7	601
MAY.	15 16 17 18 19 20 21 22	581.5 598.8 595.9 599.0	596.5 594.4 598.0	610.5		583.0	585.6 590.0	590°0 597°0	599.0 599.0	608°0 628°0	$614.0 \\ 622.8$	614.2 618.2	610°
MA	17 18 19 20 21 22	595 . 9	598.0		589.8 604.4	586°5 580°4	584.2	598.8	613.2	619.8	607.8	622.0	614
	18 19 20 21 22	595 . 9	598.0	586.2	577.9	569.0	575.6	594.6	612.0	611.2	611.4	619.0	609
	19 20 21 22	599.0		591.2	589.2	583.2	577.1	568.0	586.0	588.0	597.0	597.4	605
	21 22	599.0	589.0	596.9	590.0	593.2	595.2	597.0	602.0	607.0	603.0	601.2	604
	22		596.0	593.0	581.8	589.0	588.0	594.0	595.4 599.0	607.5 d	616.0 610.0	$611.4 \\ 616.2$	630
	23	603.0 603.8	597.5 604.5	591.0 598.4	588.4 597.0	586.4	590.0 591.8	597 . 4 589 . 8	594.9	600.8	602.7	605.0	604
	24	605.4	602.2	598.0	594.8	594.0	597.6	600.1	600.9	608.0	611.0	609.4	612
	25	613.0	612.4	605.0	602.0	595.0	594.0	598.0	604.0	611.0	614.0	606.8	614
1	26	607.0	614.0	613.0	602.0	598.0	599.5	604.0	612.8	611.4	611.0	609.8	612
	27	625.0	624.1	619.0	605.0	596'8	602°0 595°4	611.2	621.8 609.0	636.0	643°2 609°4	645.8 608.0	643
	28 29	599.8 599.8	593.8 593.8	604.8 592.0	597.2 570.0	588.8 568.5	596.2	608.4	605.8	612.4	597.8	608.0	601
l	30	616.6	619.0	613.8	608.7	596.0	590.5	611.0	618.0	622.0	623.0	634.0	624
lourly	Means	608.57	607:33	603.97	597.27	592.40	594.20	600.25	607.52	612.92	614.97	615.48	614
			<u>'</u>		ТЕМРЕ	ERATURE O	F THE BIFI	LAR MAGN	ET.		·		
	1	48°5	49°3	50°2	5 <u>i</u> .0	5η4	5 <u>1</u> .4	5i°4	5 1 .9	52°4	53.1	53.0	52.0
1	$\begin{bmatrix} 2 \\ 3 \end{bmatrix}$	48.5	49.0	51.5	51.6	51.6	51.6	51.7	52.2	52.5	52.5	53.0	53.0
	4	51.7	52.2	53.6	54.2	54.2	54.8	55.5	55.6	55.8	56.1	56.2	56
- 1	5	52.5	53.3	54.3	55.2	56.1	56.8	57.2	57.8	58.5	59.1	59.5	59
į	6	54.0 57.6	54.9 57.8	55°4 58°8	56.5 60.2	58.1 61.3	58.4 62.2	59°0 62°4	$60.0 \\ 62.9$	60.7 63.2	61.8 63.5	62°3 63°5	62.63
.	7 8	90.0	60.0	59.9	60.2	61.3	61.4	61.6	61.3	61.3	62.0	62.8	63
	9		58.2		59.0	60.8	62.0	62.2	62.4	62.8	63.4	63.6	63.
1	10 11	58°1 61°7	61.4	59.0 61.2	61.4	62.3	$63 \cdot 2$	64.0	64.2	64.9	65.4	65.6	65
	12	63.0	63.3	64'1	65.2	66.1	66.8	67.4	67.4	67.9	67.5	67.2	67
1	13	63.2	63.4	64.4	65.2	66.4	66.2	66.0	66.0	66.3	66.5	66.5	66.
	14 15	61.0 59.5	61.8	62.2	64.0	65°1	63.9 63.9	65°2 64°3	65.2 64.8	65°2 65°5	65°2 66°3	65°4 66°9	67
MAY.	16 17	60.0	60.6	60.8	61.5	62.4	63.3	63.6	64.4	65.0	65.5	65.8	65
\geq	18	90.0	60.4	61.0	61.8	62.6	63.2	64.2	65.0	65.7	66.4	66.7	66
	19	62.0	62.8	62.6	62.9	63.7	64.4	64.7	65'4	65.9	66.5	67:0	67
	20	62.0	64.0	62.4	62.5 59.0	63°1 59°4	63.6 60.0	64°0 60°5	64.0 61.2	64.2 61.8	$64.7 \\ 62.5$	63.0 62.0	65. 63.
	$\frac{21}{22}$	59.4 60.0	61.0 20.0	59.0 61.3	61.6	62.0	62.8	63.2	64.0	64.2	65.5	65.4	65
	$\begin{array}{c} 23 \\ 24 \end{array}$	61.4	61.4	61.4	61.2	61.6	62.0	62.1	62.4	$\frac{-}{62.7}$	63.5	63.4	63
1	25	60.0	60.0	60.9	62.0	62.9	63.6	64.0	64.8	65.7	66.1	66.0	66
	26	57.3	57.7	58.4	58.6	59.0	59.3	59.1 60.5	58.8 61.0	58.8 61.2	59.0 61.8	$\begin{array}{c} 59.4 \\ 62.2 \end{array}$	59 62
	27 28	56.0 57.8	56.7 58.0	58.0 58.0	58.6 58.5	59.6 59.6	60°0 60°4	61.3	62.6	63.6	65.0	65.6	66.
	28 29	64.2	64.1	63.6	64.0	64.2	65.3	65.3	65.4	65.2	65.6	65.9	65
1	30	58 ·5	58.1	58.0	57.5	57.5	57.4	56.9	56.8	56.4	56.2	56.5	56

^a Off scale.

^b Seven minutes late.

[·] Nine minutes late.

						IZONTAL						
	One Scale	Division =	'000087 par	rts of the H.	F. Increase	se, in Scale	Divisions, c	orresponding	g to 1º decre	ease of Tem	perature, 1°	63.
12h.	13h.	14h.	15h.	16 ^h •	17h.	18 ^h •	19h.	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div. 620 2	Sc. Div. 617.2	Sc. Div. 633'5	Sc. Div. 623 8	Sc. Div. 617.5	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
007 0				_		628.8	630.0	629.7	627.9	629.6	624.0}	623.03
621.8	621.3	623 ·2	620'6	618.8	621.9	622.0	622.8	622.0	621.4	623.0	619.0	620.71
621.1	621.0	620.0	617.7	617.0	620.0	619*2	623.0	620.0	622.0	621.5	621.0	618.04
620.0	620.0	619.0	616.0	618.0	620.0	620.0	620.2	622.0	623.0	623.4	626.2	617.50
616.5	614.8	613.5	614.2	615.8	612.4	612.6	617.0	618.2	613.2	624.2	614.8	613.70
625.0	620.2	594.6	603.2	586.4	592.0	539.8	a	473.5	279.4	534.7	454.3	574.84
595.8	593.6	593.0	594 °0	595 ° 0	595.6	_			_		614.0}	586.71
						605.0	607.2	600.0	608.2	609.5		1
606.2	603.9	601.9	604.0	604.0	603.7	604.0	608.0	601.0	606.0	607.0	607.4	605.45
603.4	602.5	602.0	602.2	603.0	604.8	603.2	605.0	600.2	598.0	600.8	599.8	602.68
596.0	599.5	600.0	600.8	603.0	603.8	600.4	600.0 c	599.8	601.4	600.2	601.2	601.10
610.4	610.8	601.2	602.0	600.8	603.0	599.6	600.3	601.9	602.2	604.5	608.0	601.23
602.2	605.0	609 .0	609.2	611.1	610.9	609.5	610.0	607.0	604.6	593.9	596.2	605.75
615.8	609'2	584.9	608.0	614.0	614.4				504.0	F0010	$\left \frac{1}{594\cdot 2} \right $	601.26
		,				590.0	590.0	592.0	594.0	598.2	500.0	l .
604.0	593.7	589'0	581.0	579.0	583.8	576.0	588.2	584.8	584.5	595.0	598.0 598.1	592.34
606.2	593.0	589.0	591.2	591.4	595.6	593.0	596.0	596.8	596.0	598.8	598 1	592.56
608.8	587.0	598.8	612.2	583.8	586.0	593.2	593.1	593.7 598.8	589°8 598°4	592°1 596°0	598.0	596°20 598°81
601.4	600.0	593.2	600.9	597.1	601.0	596.9	594.2				603.4	
613.2	602.1	592.9	591.0	590.8	602.0	599 .0	602.0	599.0	600.2	598.0		599.57
605.2	602.3	602.0	602.2	600.7	600.3	61210	606:0	604.2	604.2	606.0	$\{605.8\}$	601.80
-						613.0	606.0				612.0	605.21
609.0	610.0	608.5	607.4	607.3	603.2	603.2	607.8	595.0	607 . 8	610°0 601°2	606.0	603 21
610'4	603.2	606'4	598.2	594.0	597.0	596.2	597.8				622.0	
610.0	611.4	613.5	613.0	614.2	616.0	616.9	617.5 608.0	618.8 612.0	619.0 604.2	618.8 602.5	608.0	613.61
610.0	604.8	606.3	606.0	609.2	584.2	597.8			583.7	576.5	604.1	600.72
612.2	611.2	604.0	601.0	604.2	611.0	616.0	602.0	553.2	000 /	010.9		li
604.0	598.8	597.0	595.4	596.0 °	596 .2	600.0	611:0	612.2	612.0	611.0	614.1	600.45
696:0		600:0	610:0	622.2	628.4	620°0	61 1 .0	618.8	621.0	627.8	627.0	618.60
626.0	623.2	620.0	619.2						606.66	607.98	608.24	606.31
611.11	606.86	604.72	606.38	605.00	605.20	605:39	607.13	606.66	606 66	607 98	608 54	000 31
0 1	0		1 0		MPERATUR	e of the	BIFILAR MA	AGNET.	0	0	0 . 1	•
52.6	52°3	52°3	5 î·7	5η6	5 i°3			47.00	40.0	40:1	$\{-\frac{1}{48\cdot 2}\}$	50.62
				<u> </u>	<u> </u>	47.2	47.5	47.8	48.0	48.1		52.00
53.6	53.7	53.7	53.5	53.4	52.6	52.3	52.0	51.4	51.2	51.0	50.4 52.3	
56.3	56.0	55.5	55.4	54.9	54'2	53.8	53.4	53.4	53.4	53.0 54.4		54.52 56.56
59'4	59.0	57.9	57.5	57.0	56.8	56.4	55.8	55.0	54.7 57.8	54.4 57.4	53°8 56°5	59.06
62.2	61.5	60.9	60.5	60.2	59.8	59.4	59.0	58.4 60.8	90.8	60.7	60.6	61.46
63.2	62.6	62.2	61.8	61.5	61.2	61.2		i				1
63.0	62.6	62 .2	61.3	61.0	60.9	60.4	60.0	59.8	59.2	58.8	58.4}	60.92
63.6		63:0	60:5	62.4	62.2	62.0	61.8	61.8	62.0	61.6	61.7	61.81
65.5	63 ·3	63.0	62.5	64.0	63.6	63.2	64.0	63.2	63.0	63.0	62.6	63.64
66.9	65.6 65.6	64.4	64.0 65.5	65.3	65.3	65.0	65.0	64.8	64.6	64.1	63.6	65.63
67.0	67·0	65 . 9	65.8	65.4	64.6	64.0	63.5	62.6	62.1	61.6	61.5	64.95
65.2	65.0	64.6	64.0	63.6	63.5	62.7	62.0	61.4	60.9	60.2	59.6	63.45
67.4	67°1	66.6	65.8	65.4	65.0				—	_		
-	0/ 1		000		- 05 0	62.2	61.9	61.4	60.7	60.5	60.0}	63.70
65.9	65 ·5	64.8	64.1	63.7	63.3	62.5	62.4	62.0	61.6	61.5	60.2	63.19
66.9	66 .2	66.1	65.8	65.2	65.2	64.6	63.8	63.5	62.8	62.6	62.1	64.12
67.0	67.0	66.6	66.5	65.2	64.2	64.2	63.2	63.0	62.2	62.5	62.0	64.23
65.0	64.6	64.0	63.2	63.3	62.9	62.2	62.0	61.4	61.0	60.4	59.6	63.13
63.5	62.9	62.6	62.0	61.8	61.2	61.0	60.8	60.2	60.4	90.0	59.8	61.00
65.4	65.1	64.4	64.2	64.3	64.0	-		_				
_	05 1	-	U I J		-	63.8	63.0	62.7	62.7	62.5	$\frac{-}{62 \cdot 0}$	63.39
63.9	63.7	63.2	63.5	63.5	63.0	62.2	62.2	61.8	61.4	61.0	60.4	62.37
65.6	65.3	65.0	64.6	64.2	63.2	62.4	61.0	60.0	59.0	58.5	57.4	62.85
59.8	59.6	59 ·2	58.6	58.1	57.8	57.5	57.0	56.6	56.3	56.0	55 ·5	58.27
62.2	62.3	61.9	61.4	$\frac{61.2}{61}$	60.8	60.5	59.4	59.0	58.2	58.0	57.7	60.03
66.4	66.4	66.2	66.5	66.0	65.8	65.6	65.4	65.4	65.2	65.0	64.5	63.56
66.0	65.2	65.0	64.5	64.0	63.7				_			63.26
				l —		60.4	60.0	59.6	59.5	59.2	58.8	
56°2	56.2	55.8	55.6	55.2	55.2	55.6	55.2	55.2	55.2	55.2	55.3	56.41
	62.64	62.22	61.73	61.44	61.04	60.27	59.83	59.43	59.11	58.78	58.31	60.82

	0	ne Scale Div	rision = '00	00087 parts	of the H. F.		NTAL FO in Scale Div		esponding to	1° decrease	of Tempera	ture, 1.63.	
Mean Gö gen Tir	ittin- }	Oh.	1 ^h •	2 ^h .	3 ^h .	4 ^h •	5 ^h .	6 ^h •	7h.	8 ^հ •	9 ^h .	10h.	11h.
	1 2 3 4 5	Sc. Div. 618'0 612'0 612'2 611'9 619'0	sc. Div. 620 ° 0 620 ° 0 610 ° 4 613 ° 9 624 ° 8	Sc. Div. 620 ° 0 612 ° 4 610 ° 2 607 ° 3 618 ° 0	Sc. Div. 615 0 615 8 602 8 600 0 613 0	Sc. Div. 599°5 598°2 597°3 601°0 609°0	sc. Div. 592 ° 0 594 ° 8 602 ° 2 605 ° 0 609 ° 0	Sc. Div. 611 8 593 0 606 0 615 0 613 2	Sc. Div. 617 0 605 2 609 0 617 0 620 0	Sc. Div 615 ' 4 601 ' 4 618 ' 0 617 ' 0 626 ' 0	sc. Div. 634 ' 2 601 ' 6 618 ' 0 619 ' 0 629 ' 0	Sc. Div. 633 2 620 0 617 9 618 0 625 0	Sc. Div 615 4 613 1 617 0 614 0 619 8
	6 7 8 9 10 11 12	620°2 615°0 609°8 605°0 605°8 617°0	617.0 608.8 613.1 584.0 600.0 611.0	610°5 604°0 607°0 599°0 598°8 605°0	610.0 598.5 605.4 594.2 592.0 603.7	598.6 595.4 600.0 575.0 581.5 604.2	597.2 601.0 600.5 571.4 588.0 594.0	605 · 4 603 · 2 609 · 6 591 · 1 588 · 2 593 · 8	603.4 608.2 612.1 606.5 590.0 602.2	614.4 612.9 620.5 622.0 603.8 618.4	614.2 621.1 623.0 628.0 593.8 612.0	619.0 621.1 616.0 614.0 592.0 621.0	616·1 614·0 614·0 621·8 610·0 637·0
JUNE.	13 14 15 16 17 18 19	601.0 623.2 615.9 611.0 608.0 606.0	574°0 620°8 612°3 613°5 605°2 605°0	588.0 617.0 613.4 612.0 604.5 600.8	575°2 612°4 606°0 606°2 604°7 595°0	573.5 606.1 596.7 599.0 600.7 587.8	585°8 617°2°4 601°0 598°0 592°2 593°2	601.2 617.5 607.5 602.5 600.2 601.2	586°3 620°0 622°0 607°6 603°8 611°8	630 · 2 620 · 7 631 · 0 614 · 4 617 · 0 616 · 0	641.3 633.8 623.0 619.3 621.2 617.9	644.0 622.0 634.0 621.2 627.8 616.2	632·0 622·5 622·0 622·4 619·4 613·0
	20 21 22 23 24 25 26	618.0 617.0 614.0 612.8 606.0 604.8	614'3 612'0 611'0 603'0 605'8	611'8 601'0 603'5 604'6 597'0 600'2	597.0 613.0 594.8 598.0 595.0 596.0	602.6 604.0 590.0 593.0 593.0	601 · 2 595 · 0 c 584 · 8 593 · 5 594 · 0 597 · 0	601.0 596.0 585.6 595.0 601.8 600.0	601.5 600.0 593.0 602.0 605.0 601.9	614'8 606'0 594'0 607'8 607'2 611'0	616.8 607.5 600.8 613.8 610.5 610.0	621.8 607.0 604.1 614.2 606.0 605.0	619.0 605.0 606.1 607.0 598.0 595.6
	27 28 29 30	607°0 606°0 603°2	607.4 605.5 604.8	601.0 601.1	592.0 602.4 594.2	589°0 605°4 585°0	593.0 592.5 579.0	594°2 596°2 588°1	603.0 608.8 598.3	604°8 598°2 607°0	597°2 605°4 614°0	602.0 608.2 608.0	607:2 607:5 602:5
lourly l	Means	611.23	608.79	605.85	601.24	595.21	595.10	600.70	606.02	613.46	616*40	616.87	614'3
	1	· · · · · · · · · · · · · · · · · · ·					F THE BIFI		1	1	<u> </u>	<u> </u>	I .
	1 2 3 4 5	55.7 59.2 59.8 61.0 57.0	55.6 59.2 60.5 61.0 57.4	55.6 59.4 61.2 61.8 57.9	56.2 60.0 61.5 61.9 58.0	56.9 60.7 61.8 62.6 58.8	57.6 61.5 62.4 62.6 59.5	58.4 62.3 63.0 63.5 60.0	59°4 63°0 63°4 63°7 61°0	60°0 63°2 64°0 63°7 61°4	60°3 63°0 64°4 64°3 62°4	61.0 64.6 64.4 63.0	61°0 64°5 64°1 63°2
[6 7 8 9 10 11 12	59.0 62.3 61.6 67.3 65.0 60.0	59.4 62.3 61.7 67.3 65.4 60.5	60°5 62°0 62°1 67°3 65°7 61°4	61.7 62.4 62.8 67.3 66.0 62.0	62.8 62.5 63.6 67.2 66.4 62.0	62.8 62.9 64.8 67.5 66.8 62.6	64.0 63.2 65.5 67.5 67.0 62.6	64.8 63.8 66.2 67.5 66.8 62.8	65.4 63.5 67.3 67.5 66.9 63.4	66.7 64.0 68.4 67.5 66.8 63.8	67.0 64.4 69.7 67.5 66.5 64.4	67.6 64.2 70.4 67.3 66.2 64.9
JUNE.	13 14 15 16 17 18 19	59.0 53.4 57.4 56.8 58.7 62.2	59.0 53.0 58.0 57.0 59.8 62.2	59.0 53.0 58.8 58.4 60.8 62.2	59.0 53.0 59.4 60.3 61.0 62.2	59.0 53.3 59.9 60.6 62.0 62.5	59.0 54.0 60.6 61.1 62.8 63.0	58.6 54.5 61.0 61.7 64.0 63.4	58°0 55°2 61°4 62°1 64°6 63°6	57°5 56°0 61°9 62°5 65°0 63°9	57.4 57.5 62.0 63.2 65.4 64.1	57.4 58.6 62.2 63.6 65.4 64.5	57.1 59.7 62.2 64.6 65.3 65.0
	20 21 22 23 24 25 26	61.5 62.2 63.5 65.3 66.0 68.9	62.5 62.4 63.5 66.1 66.5 69.5	63.4 62.1 65.2 67.2 66.9 70.4	64.2 63.4 66.1 67.9 67.4 71.6	65°4 63°6 67°0 68°5 68°0 72°1	65.6 64.0 67.4 69.2 68.9 73.0	66.0 64.5 67.4 69.4 69.6 73.3	66.0 65.5 68.0 70.0 70.4 73.8	66.2 66.3 68.1 70.3 71.5 74.0	66.4 66.9 68.8 71.1 72.5 74.5	66.6 66.8 69.6 71.6 72.6 74.9	66.6 67.4 69.8 72.0 72.6 75.1
	27 28 29 30	70°9 67°9 66°2	70°5 67°7 67°0	70.4 67.7 68.0	70°4 68°3 68°9	70.4 68.6 70.0	71.0 69.4 70.6	71.3 69.7 71.0	71.2 70.6 71.4	72.1 71.6 71.8	72.8 72.0 71.9	73.4 72.0 72.4	73·4 72·2 72·4
Tourly 1	Means	61.84	62.15	62.63	63.19	63.70	64.25	64.71	65.17	65.28	66.08	66.47	66.6

² Nine minutes late.

	One Scale	Division =	*000087 ps	arts of the H		IZONTAL		orrespondin	g to 1° decr	ease of Tem	perature, 1°	63.
12 ^h .	13h.	14h.	15h.	16h.	17h.	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Se. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 613 65
625.0	618.0	600.2	607.0	608.9	609.4	609.6	614.4	610.8	614.0	613.8	-	608.99
612.7	608.9	608.0	610.0	609.8	610.0	611.2	608.0	609.0	620.5	608.8	611.4 611.3	609.42
607.4	607.5	610.0	610.0	601.0	606.0	610.0	610.0	611.4	610.2	610.2	617.9	613.60
614.0	611.0	611.0	617.0	615.0	620.0	617.2	615.0	616.9	614'0	618.4		1
619'4	613.6	612.0	614'1	614.2	614.6			C15.7	613.4	616.8	$\{619.0\}$	616.33
-						607.0	606.4	615.7	586.5	606.0	606.6	605.55
613.0	609.0	608.7	596.0	599.8	598.7	599.0	599.0	585°0 610°5	909.0	609.4	612.0	609.00
606.0	608.0	609.0	608.0	611.5	609.0	610.0	610.3	605.0	609.2	607.8	608.0	610.39
621.0	603.2	608.5	615.0	610.0	609.2	606.2	614 . 9	599.4	600.5	600.0	600.0	598.92
590.6	591.4	598.0	601.2	591.4	597.9	595.9	608.2	608.0	610.0	909.0	616.2	601.21
615.6	605.8	596 `5	599.0	603.1	606.1	610.0	000 0	000 0	010 0	000 0		
627.0	617.0	602.0	597.0	591.0	597.2	584.2	585.0	618.0	618.0	614*4	616.0	607.77
			600.0	605.0	605.0	614.0	612.6	612.2	613.0	612.7	618.2	606.55
612.0	614.0	606.0			614.0	614.0	609.4	614.2	615.0	616.2	618.1	617.40
619.0	619.2	613.2	613.4	618 . 4	612.2	613.0	616.0	616.4 _p	603.7	612.1	611.0	614.27
619.4	610.2	613.0	612.2		606.9	600.0	602.2	608.0	608.0	610.4	609.0	609.61
624.0	612.0	608.8	607.1	607.2	598.4	598.0	603.2	604.2	603.0	604.0	606.2	606.50
611.9	615.3	604.1	601.5	601.0	605.0	3 90 0	000 0	0010			1	
608.0	608.0	605.0	607.8	606.0	000 0	610.5	612.0	612.8	612.5	611.0	$\{614.0\}$	607.34
C10:0	C15:0	614.0	601.2	605.0	609.2	608.2	611.3	613.0	613.9	613.9	614.0	610.75
619.2	615.0	614.0	604.1	605.0	603.1	605.2	606.0	606.2	607.0	610.0	611.1	605.92
606.8	608.4	605.8	602.0	602.0	601.2	601.2	600.0	601.8	603.2	605.8	609.4	600°8 5
604.0	604.0	603.2 602.0	600.0	597.5	593.2	595.0	596.0	588.0	597.4	601.5	604.0	601.23
602.0	600.0	598 .2	599.8	600.2	601.8	601.0	600.2	601.1	602.2	603.3	604.0	600.96
599.0	598.5	594.4	597.0	598.0	600.4	001 0					- 3	600.67
003 0	597.2	094 1	031 0	050 0		596.1	599.0	600.7	601.4	600.5	[606.0 1	ĺ
593.2	596.8	593.2	590.7	593.1	594.0	594.9	594.4	601.8	593.8	596.0	596.0	597.34
608.0	599.0	293.0	599.0	597.0	597.6	597.0	595.2	594.5	580.0	603.0	600.0	600.45
607.7	591.1	291.0	5 86.0	578.5	571.0	585.0	586.4q	596.5	593*4	600.0	601.1	594.70
611.19	607.02	604.46	603.70	603.40	603.23	603.62	604.30	606.21	605.87	608.12	609.45	606.21
011 19	001 02	001 10	000 10					CANAR]
				1	MPERATUR		1	1 _		l .	0	l
6ì·2	6ì·2	61.3	61.0	61.1	60.8	60°5	60°2	6ე. 0	59.5	59.1	59.0	59.27
65.0	64.6	64.1	63.8	63.4	62.8	62.6	62.0	61.2	61.0	60.4	59.8	62.11
64.4	64.0	63.6	63.4	63.0	62.6	62.5	62.2	61.8	61.8	61.4	61.1	62.62
64.0	63.5	62.2	61.8	61.4	60.5	60.0	59.2	58.8	58.2	28.0	57.8	61.69
63.3	63.3	63.0	62.6	62'1	61.2	_					59.0}	60.81
_	_					61.9	61.6	61.0	60.4	60.2		
67.4	66.6	66*1	65.2	65.1	64.7	64.3	63.9	63.5	63.2	63.0	62.4	64.06
64.4	64.0	63.8	63.2	63.2	63.0	62.7	62.7	62.4	62.2	62.0	62.0	63.06
70.6	70.4	70.1	69.7	69.7	69.3	69.0	68.6	68.2	68.2	68.0	67.7	67.25
67.3	67.3	67.0	66.6	66.2	66.0	65.9	65.7	65.5	65.3	65.3	65.0	66.75
65.8	64.6	64.1	63.3	62.9	62.2	61.9	61.1	60.7	60.3	60.0	59.4	64.24
65.1	65.2	64.8	64.4	64.5	64.0					<u> </u>	59.5	62°3 3
						60.0	59.8	59.6	59.5	59°5	53.6	56.80
57.2	57.0	56.3	55.8	55.5	55.0	55.0	55.0	54.6	54°2	54.0 57.4	57.0	56°97
60.5	60.2	60.5	60.2	59.7	59.0	58.5	58.2	57.8	57.6		57.0	90.08
62.2	62.5	62.0	61.1	60.4	60.2	59.8	58.9	58.2	57.6	57·2 59·2	58.4	61.60
64.9	65.0	64.6	64.0	63.5	62.7	62.0	61.6	60.5	60.0	62.8	62.8	63.21
65.1	64.2	64.1	63.7	63.5	63.5	63.4	63.0	63.0	62.8			
65.3	65.2	65.2	64.2	64.0	63.2	61.0	61.0	61.7	61.2	61.2	61.0}	63.16
-						61.8	61.9	64.0	63.6	63.1	63.0	65.04
66.6	66.6	66.4	66.2	65.8	65.5	65.1	64.6 64.8	64.7	64.2	63.4	63.0	65.03
67:5	67.4	67.0	66.4	66.0	65.6	65.2	67.6	67.1	66.6	66.5	65.2	67:57
70.0	69.9	69.4	69.3	69.0	68.6	68.2	68.2	68.0	67.5	66.8	66.2	69.25
72.4	72.5	71.8	71.0	70.4	69.5	69.6 69.0	69.2	69.0	68.9	68.8	68.4	69.81
72.6	72.6	71.5	71.2	70.6	70.1	ס פט	09 4	U9 U			- 1	
75.0	74.0	73.8	73.4	73.4	73.0	73.5	73.4	73.0	72.5	$\frac{72\cdot 1}{}$	$\frac{-}{71\cdot7}$	72.91
73.2			71.0	71.4	71:0	70.6	70.2	69.8	69.0	68.7	68.4	71.13
$72 \cdot 2$	72.8	72.4	71.6	71.4	71.0	69.7	68.0	67.5	67.0	66.2	66.5	69.57
72.4	$\begin{array}{c} 72.1 \\ 72.2 \end{array}$	71.6 71.6	70°8 71°0	70°3 70°5	70°0 70°0	69.0	68.2	67.8	67.4	66.6	65.7	69.75
66.74	66.48	66.09	65.61	65.25	64.79	64.30	63.85	63.46	63.10	62.74	62.33	64.46

Mean Göttin-) gen Time.	Oh.	1h.	2 ^h .	3h.	4 ^h .	5 ^h .	6h•	7 ^h .	8h.	9h.	10h.	11h.
	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc . Div.	Sc. Div.
$\begin{pmatrix} 1 \\ - \end{pmatrix}$	606.5	604.0	595.0	584.7	588.0	594.7	595.8	594.0	593.4	593.6	598.8 598.8	599 . 0
$\begin{bmatrix} 2 \\ 3 \end{bmatrix}$	603.1	599.0 600.2	594.0 594.8	590'8 588'8	592.0 591.0	591.2 596.5	587.8 600.0	590 . 9	594°0 605°4	596.0 601.0	598.2	595.8
4	002 0			-	-	_	_					
5	594.0	592.8	590.0	587.4	583.4	584.0	591.2	602.2	601.2	601.0	591.4	591.8
6	592.0	588.0	586.4	578.7	577'1	584.0	598.0	600'4	610.7	601.8	603.0	598 . 0
7	601°1 589°0	590.3 580.0	578.0 576.8	581.2 580.0	566°0 578°8	569°0 577°0	585°0 577°2	607°0 578°5	607°0 585°2	601.4 586.0	597.0 589.0	593.4
8 9	288.0	582.4	578.0	571.0	573.4	569.5	571.8	587.4	582.0	611.4	618.0	608.5
10	568.2	584.0	556.0	550.0	540.0	556.3	569.5	557.0	592.0	591.0	588.0	574.5
11			572°0	557.2	548°0	 541·7	552.0	563.0	 579°3	582.4	577:2	576.0
12 13	584.4 577.4	586.4 578.6	577°5	576.0	565.0	567.0	565.0	566.4	562.3	564.0	572.0	581.0
14	583.2	582.0	570.0	574.0	567.0	571.4	585.0	590.0	593.2	595.8	604.0	598.0
15	593.5	588.0	583.2	574.2	572.2	570.8	579.8	584.2	592.8	602.2	600.2	597.8
15 16 17	592.2	587.0	580.8	579.2	576.0	578.0	584.0	586.8	593.5	595.0	598.0	589.0
ات 17 18	585.5	575.7	581.2	576.0	568.0	564.0	563.8	570.0	582.0	590.2	596·0	600.0
19	590.2	587.5	581.6	572.5	571.4	578.0	574.8	574.5	582.5	578.0	581.4	591.2
20	585.0	584.2	577.2	576.0	570.0	565.0	561.0	575.3	585.0	598.4	598.0	588.2
21	590.0	586.8	581.4	574.8	568°2 591°8	569.7 590.0	571.0 589.5	575°0 589°0	588°2 595°8	591 .4 598 . 8	593.8 594.8	593°2
$\begin{vmatrix} 22\\23 \end{vmatrix}$	592.1 591.0	592.0 593.0	583 . 4 593 . 9	589'0 585'0	581.2	587.6	585.4	588.0	597 ° 0	612.4	598.1	603.8
$\begin{vmatrix} 23 \\ 24 \end{vmatrix}$	598.6	597.0	590.2	585.0	583.0	586.4	591.0	601.0	606.0	610.0	606.0	595.8
25								609.5	620.0	622.5	620.0	608.2
26	592°1 618°0	584.6 606.5	584.0 598.5	580.5 591.5	570°0 591°5	579°0 590°5	589.5 591.5	601.2	611.8	610.5	620 0	604.0
$\begin{array}{ c c }\hline 27\\28\\ \end{array}$	608.2	608.2	601.2	597.0	599.5	606.2	609.5	608.6	610.8	610.0	910.0	608.0
29	612.0	600.6	603.5	590.1	590.8	590.9	592.4	597.5	600.5	606.0	607.7	606.5
30	611.2	609.4	605.0	595.7	589.0	593.0	606.4	609.5	607.5	624.0	614.2	608.2
31 August 1	610.8	607.0	605.0	597.0	590.0	589.5	591.2	595.0	601.2	602.8	606.8	602.8
Hourly Mean	595.07	592.04	586.19	581.25	577.28	579.68	584.14	589.10	596.11	598.69	598.21	595.7
Toury mean	-1 000 01	032 01	000 15	<u> </u>	ERATURE (· · · · · · · · · · · · · · · · · · ·		1 40 - 40		
	66.0	66.1	66.8	67.8	69.0	69.9	70°8	71.4	72°2	73.0	73°4	74.0
$\int \frac{1}{2}$	66.0	68.2	66.8	70.9	72.1	73.0	70.8	74.5	72 2 75 4	73 0 76 0	76·2	76.4
$\begin{pmatrix} 2\\3 \end{pmatrix}$	70.0	70.2	71.4	72.3	73.4	74.6	75.4	76.7	77.4	78.0	78.4	78.5
4	l											
5	71.6	72.0	72.9	73.2	74.6	75.8	76.4	77.2	77'8	78.4	78.8 77.2	78°4
6 7	73·2 72·2	73°0 72°2	73.0	73°0 73°0	73°1 74°3	73°7 75°0	74°4 76°2	75°3 76°5	76°1 77°5	76.6 78.5	79.0	79.4
8	$73 \cdot 2$	73.5	74.2	75.0	77.7	78.4	79.0	79.8	79.3	79.0	79.4	79.8
9	74.9	75.9	76.5	77.1	78.6	79.4	79.8	80.4	80.4	80.6	80.2	80.0
10	76.5	75.8	75.4	75.6	76.0	77.0	77.4	78.0	79.0	79.9	80.0	79.8
$\begin{vmatrix} 11 \\ 12 \end{vmatrix}$	75.2	76.0	77.0	77.7	78.0	78.2	78.0	78.4	79 · 1	80.0	80.6	80.2
13	76.0	76.4	77.1	77.6	78.5	79.7	80.7	81.2	81.0	81.0	80.8	80.5
. 14	71.3	71.4	72.0	72.5	73.2	73.7	73.6	$\begin{array}{c} 73.9 \\ 72.4 \end{array}$	$74.0 \\ 73.2$	73.9	73.5 74.6	73°4 74°4
70 15 16 17 17	69.3	69.0	69°0 71°8	69°4 72°7	69.8 74.0	70°8 75°0	71.7 76.1	76.8	77.5	74°4 78°0	78.4	78.0
$\frac{5}{5}$ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	74.1	74.2	74.0	75.0	76.1	77.8	79.0	80.4	80.8	80.2	80.1	80.0
18	∥ —		77.5	79°4	79.4	80.6	81.2	82.7	82.0	83.0	83.2	84.0
$\begin{pmatrix} 19 \\ 20 \end{pmatrix}$	76.4 77.5	77.0	77°5 79°0	79.4	79.4	79 · 2	79.4	79.0	$\frac{32.0}{79.2}$	79.8	79·5	79.8
21	76.2	76.5	76.6	76.6	76.7	77:3	78.0	78.4	78.8	79:3	79.7	79.2
22	76.2	76.6	76.8	76.6	77.2	77.5	78.0	78.2	78.5	78.8	79.0	79.0
$\begin{vmatrix} 23 \\ 24 \end{vmatrix}$	71.7 69.4	72.1 69.3	72.7 70.0	73°4 70°6	73°5 71°5	73.6 71.5	73°5 71°6	73°5 71°5	73.5 72.0	$\begin{array}{c} 73.6 \\ 72.4 \end{array}$	74°4 72°4	74°5 72°4
25	 		_							_		_
26	71.0	70.4	70.0	69.0	69.2	68.8	$\begin{array}{c} 68.5 \\ 67.5 \end{array}$	68.5 67.5	68.4 67.6	68.8 67.4	69°0 67°5	69°4
$\begin{vmatrix} 27 \\ 28 \end{vmatrix}$	63.0	64.0 63.5	66.0 64.6	66 . 6	67.0 65.5	67.5 66.5	67.5	67.5	68.3	68.7	69.1	69.0
28	64.4	65.2	96.0	67.0	67.5	68.2	69.0	69.4	69. 9	70.0	70.3	70°8
30	66.6	66.6	66.6	66.4	66.6	66.6	66.2	67.5	67.5	68.0	69.0	69.5
		65'1	65.2	65.8	67.4	67.4	68.0	69.0	69.0	69.5	69.2	69.4
(31	64.8	00 1	00 2	000	0. ~			l	00 0			
\\ \dagust 1	-		-									75:9

	One Scale	Division=	·000087 pa	rts of the H.		IZONTAL se, in Scale		orresponding	to 1º decre	ase of Temp	erature, 1·6	3.
12h.	13h.	14h.	15h.	16 ^h .	17 ^h .	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div. 600 0	Sc. Div. 599 0	Sc. Div. 598 2	Sc. Div. 598'4	Sc. Div. 595.8	Sc. Div. 590°0	Sc. Div. 596.8	Sc. Div. 598 2	Sc. Div. 598 1	8c. Div.	Sc. Div. 601.8	Sc. Div. 596 89
598.0	600.2	594.0	591.1	592.1	595.2	594.0	593.0	591.0	591.0	592.0	595.9	594.21
591.1	595.0	598.0	592.4	590.0	592.0				<u> </u>		1 1	594.44
			-	_		587.8	587.0	589.0	587.8	588.0	593.0}	
592.0	593.0	593.0	593.0	593.2	593.0	594.0	598.0	605.6	589.2	587.0	597.4	593:30
598.0	597.4	593.0	595.0	586.1	593.5	597.0	598.0	594.8	591.2	593.5	586.1	593.40
591.2	590.0	589.0	593.6	578.4	569.8	573.8	580.0	578.5	586.8 581.0	578.8	586.0	586°27 583°65
216.0	586.8	583.4 616.4	583°1 545°5	585°0 542°5	583°2 542°0	585°1 549°0	585°1 428°0	583.8 567.5	576.9	$\begin{array}{c} 585.0 \\ 552.2 \end{array}$	587·1 577·2	574.36
616 ° 0 574 ° 0	630 .0 574.4	580.4	568.0	567.4	569.4	349 0	428 0	307 3	310 3	002 2		
774 0	0/4 4	350 4	000 0	307 1	005 1	582.0	575.0	574.2	575.0	576.0	$ \overline{_{574}\cdot_{2}}\} $	571.52
80.0	580.4	580.0	573.2	573 ·5	579.8	575.0	581.8	572.8	576.0	577.2	573.3	572.61
87.8	582.0	587.5	578.8	579.0	584.2	580.0	583.4	584.0	585.4	579.2	580.1	576.82
94.2	588.2	581.8	581.0	587.4	589.0	590.0	574.0	582.0	582.0	572.0	595.0	584.63
290.0	589.8	590.0	591.7	591.7	591.0	592.2	588.0	590.0	590.0	592.0	593.0	588.70
86.4	590°2	589.0	595.0	594.2	592.5	588.8	590.0	589.6	590.0	584.8	587.1	588.21
597.0	586.8	561.0	572.0	583.0	581.3	_] [}	580.94
					-	582.0	583.7	586.1	585.0	587.8	584.4	
87.4	582.0	578.8	579.5	579.5	581.5	581.2	579.8	585.0	587.4	581.2	586.4	581°39 582°74
85.8	584.2	583.5	586.0	583.9	583.9	584.6	584.2	584.0	587.4	585.0	590.0 589.0	585 '44 585 '44
89.7	583.0	587.5	590.8 592.0	594.5	597°0 595°0	586.5 581.6	585°0 595°2	594.0 591.0	584·2 593·0	585 * 8	595.0	592.35
93 · 8	597.2	592.5 592.0	586.8	587.4	591.8	591.2	592.8	593.0	594.0	596.0	597.5	592.50
98.8	587°2 590°0	594.0	595.0	598.0	590.4	031 2	092 0	000	051 0		031 0	
	090 0	004 0	030 0	-	050 1	592.1	593.2	591.4	593.1	593.4	593.2}	594.70
87.8	592.0	597.0	593.0	598.0	600*2	599.0	599.7	599.0	606.2	607*0	610.0	597:87
04.0	598.1	603.9	603.0	603.0	603.2	603.9	595.0	592.0	605.0	606.0	608.0	602.17
910.0	604.0	603.7	604.2	604.5	604.5	605.0	605.0	606.0	607.7	608.0	609.2	606.26
01.0	601.2	605.0	607.0	603.0	604.0	604.0	606.8	607.0	603.8	604.4	603.2	602.04
514.2	607.0	609.0	593.4	590.8	603.8	604.8	607.1	606.0	605.0	606.7	606.2	605.30
502.4	602.0	605.4	606.1	606.0	299.0	606.0	606.4	607.2	609.6	609.4	$\left \frac{-}{608 \cdot 5} \right\}$	602.81
593.75	591.64	591.21	590.12	590.00	590.92	590.45	590.92	591:35	591.74	591.20	593.49	590.43
					MPERATUR		BIFILAR MA					
73°8	73.8	73.0	72°6	$7\mathring{2} \cdot 2$	71.6	71.0	70°0	69.2	68·7	68°5	67°7	70°52
76.5	76.5	75.8	75.0	74.4	73.8	73.3	72.9	72.2	71.4	70.8	70.0	73.19
78.5	78.2	77.5	76.6	75.3	74.8	_			_		71.9}	74.87
_	—	_	—		i—	74.5	74.1	73.6	72.7	72.3	71.95	
77.8	77.4	77.0	76.4	76.1	75.5	75.3	74.6	74.4	74.0	73.7	73.2	75.52
77.1	76.9	76.0	75.6	75.4	74.9	74.5	74.0	73.7	73.2	73.0	72.4	74.69
79.4	79.2	78.5	77.8	77.0	76.2	75.4	75.1	74.6	74.0	73.8	73.6	75°85 77°48
79°6 79°4	79.2	79.0	78.5	78.2	77.6	77.5	77.2	77.0	76.0	76.5	75.0 76.4	78:50
79.4	79.6	79°2 78°5	79°0 78°4	79.0	78.8 77.8	78.8	78.0	77.6	77.5	77.0		
-	79.0	100	1		11.0	77.0	76.6	76.3	76.0	75.5	$\left \begin{array}{c} -75\cdot 2 \end{array}\right\}$	77.41
80.4	80.0	80.1	80.0	79.2	78.6	78.2	78.0	77.6	77.2	76.8	76.0	78:38
80.0	79.2	78.3	77.2	77.0	76.2	75.2	74.7	73.9	73.1	72.8	72.5	77.58
73.2	73.0	72.6	72.0	71.6	71.4	70.7	70.4	70.0	69.5	69.2	68.7	72.03
74.4	74.0	73.5	73.2	73.0	72.7	72.5	72'1	72.0	71.2	71.2	70.8	72.04
77.8	77.6	77'0	76.6	76.4	76.0	75.7	75.4	75.3	75.0	74.6	74.2	75.51
80.0	79.6	79.4	79.2	79.0	78.6						77.6}	78.16
94:0					-	78.8	78.5	78.0	77.7	77:5	77.61	
84.0	83.7	81.9	81.5	80.9	80.4	80.0	79.6	79.0	78.6	78.5	78.0 76.6	80.55
79 . 0	79.6	79.2	78.8	78.6	78.1	78.0	77.8	77.4	77.2 76.3	77.0 76.0	76.0	78°61 77°47
79.0	78.5 78.0	78.0	77.5	77.4	77.2	76.9 74.7	76.6 74.2	76°4 73°6	73.0	72.4	71.9	76.43
74.2	78.0	77.4	76.7 74.0	76.0 73.6	75.0	72.0	72.0	71.0	70.8	70.5	70.0	70 43
72.2	72.0	71.8	71.6	71.4	71.2	1	.2 0	- 10				
		`	-			74.0	73.8	73.6	73.4	72.9	$\left[\begin{array}{c} \overline{72\cdot4} \end{array}\right]$	71.87
69.5	68.2	68.0	67.5	67.1	66.6	66.0	65.6	65.2	64.2	64.0	63.2	67.75
68.0	68.0	67.6	66.9	66.6	65.9	65.4	65.2	65.0	64.2	63.2	63.0	66.20
68.8	68.2	68.0	68.0	67.5	67.0	66.2	66.0	65.2	65.0	64.5	64.0	66.58
70.0	70.0	69.2	69.5	69.0	68.8	68.2	63.4	68.2	67.7	67.5	67:1	68.40
69.0	69.0	68.5	68.4	68.2	67.6	67.4	67.0	66.7	66.3	65 .8	65.4	67:36
69.4	69.2	68.6	68.1	68.0	67.5	67.1	66.7	66.2	65.9	65.5	65.0}	67:39
	75.2	74.96	74.52	74.12		ļ			72.03			

	Oı	ne Scale Div	ision = '00	0087 parts o	f the H. F.		NTAL FO n Scale Divi		sponding to	1° decrease	of Temperat	ure, 1°63.	
Mean G gen T	öttin- }	Oh.	1 ^h .	2 ^h •	3h.	4 ^h •	5 ^h •	6 ^h •	7 ^h .	8 ^h •	9 ^h .	10 ^h .	11h.
	2 3 4 5 6 7	Sc. Div. 610 ° 0 614 ° 0 611 ° 8 576 ° 0 594 ° 0 598 ° 2	Sc. Div. 610 2 610 0 618 8 567 0 588 2 596 0	Sc. Div. 610 2 603 0 610 1 566 6 589 5 577 5	Sc. Div. 603 0 604 0 608 6 550 0 587 5 572 5	Sc. Div. 597 ° 0 593 ° 8 606 ° 1 579 ° 0 583 ° 0 580 ° 0	sc. Div. 592 · 5 589 · 8 602 · 4 578 · 5 578 · 0 572 · 5	Sc. Div. 593 ° 0 592 ° 0 603 ° 2 549 ° 0 575 ° 0	Sc. Div. 598 2 600 1 604 1 582 5 584 0 581 4	Sc. Div. 601 2 597 8 613 7 594 0 600 0 588 2	Sc. Div. 603 ' 5 608 ' 9 608 ' 4 605 ' 0 603 ' 0 601 ' 8	Sc. Div. 609 5 607 0 614 6 583 5 597 0 608 0	Sc. Div. 613 1 601 8 611 0 587 5 599 8 603 2
r.	8 9 10 11 12 13 14 15	593°0 596°2 597°0 603°0 602°2 609°5	597°0 595°8 594°0 595°0 602°0 597°0	592°5 585°0 586°0 583°0 596°0 578°8	585.0 583.1 578.2 573.5 582.0 572.2	580°3 582°4 578°0 572°5 571°0 556°0	579°8 582°0 578°5 577°5 566°5 554°0	587°3 584°8 580°0 580°0 568°0 581°2	595°0 590°0 583°5 586°0 575°8 602°2	603°1 593°5 591°0 594°0 587°0 597°6	606°0 598°0 591°2 603°0 592°8 597°9	621.0 596.5 596.0 602.5 603.2 592.8	599.0 592.5 591.5 604.8 600.8 596.5
AUGUST.	16 17 18 19 20 21 22	594·2 609·8 607·0 610·0 607·0 614·8	593.0 609.8 606.0 612.5 605.5 610.0	595°0 600°0 599°8 607°5 600°0 600°2	587.9 594.5 593.5 602.0 598.6 590.0	576.5 584.4 587.5 600.8 597.0 587.0	566.5 577.0 585.0 598.0 601.2 590.5	575°8 581°0 587°5 606°0 600°5 597°2	579°0 581°5 592°5 619°0 601°5 609°8	588 · 8 605 · 0 606 · 0 618 · 8 605 · 9 612 · 2	595.0 596.0 607.5 620.2 600.5 611.0	600°0 594°0 597°5 612°2 600°8 624°0	594.2 603.5 612.2 608.0 604.0 599.6
	23 24 25 26 27 28 29 30 a 31 a	600°8 597°0 595°5 600°0 601°0 597°0	598.0 595.0 585.0 599.0 598.8 595.0	591.5 589.0 568.5 611.9 591.2 586.0	583.0 582.8 571.0 599.0 583.2 580.0	576.0 575.0 569.0 580.8 579.0 570.0	573·5 573·0 552·0 579·8 580·0 571·8	582.8 582.0 573.0 583.8 579.6 571.2	591'0 594'0 509'6 592'1 586'7 582'8	597·5 596·5 598·4 599·0 603·0 591·5	601.5 604.4 596.2 608.0 605.5 598.8	607'0 601'8 595'0 597'8 615'0 609'0	600°0 602°4 590°6 608°0 617°0 606°0
Hourl	y Means	601.62	599:11	592.45	586.02	581.75	579.18	582.87	591.76	599.32	602.67	603.57	601.86
		1	1	1	TEMP	1	OF THE BIF	ILAR MAGI	. 	1	ı	1 .	I _
	2 3 4 5 6 7	65.1 65.9 66.8 68.1 68.8 69.5	66.0 66.4 67.4 69.0 69.2 69.5	66.0 67.0 68.2 70.0 70.5 70.5	68.0 68.0 69.6 71.4 71.5 70.2	68.5 69.0 69.6 72.4 74.0 70.6	68.5 69.8 71.4 73.4 75.0 71.5	69°0 69°8 71°5 73°4 75°5 72°2	69.8 69.6 71.9 73.5 75.4 72.6	70°2 70°0 72°1 74°0 76°0 72°9	70°4 70°6 73°4 74°5 75°8 73°2	71.0 71.0 73.7 74.5 76.5 73.4	71°0 71°4 73°5 74°2 76°0 73°1
ŗ.	8 9 10 11 12 13	67·4 70·6 72·4 69·0 71·5 72·6	67.5 70.6 72.4 69.0 71.8 73.0	67.5 70.6 72.6 69.0 72.8 73.4	68.0 71.2 72.5 70.0 74.0 74.4	68.5 72.5 73.0 71.0 74.6 75.4	69.6 74.0 72.5 72.0 75.5 75.6	70.2 74.5 73.0 73.0 76.0 76.0	71·1 74·4 73·5 78·5 75·4 76·8	72.6 75.4 73.5 74.0 76.2 77.1	74.0 75.5 73.5 74.8 76.3 78.0	75.0 75.8 73.5 75.1 75.6 77.9	80.7 76.0 74.5 74.6 75.7 77.5
AUGUST.	15 16 17 18 19 20 21	74.4 74.5 69.6 64.5 65.0 64.8	74.8 75.2 69.4 65.0 65.0 65.2	75.4 75.5 69.5 64.0 64.7 66.0	76.4 76.2 70.5 64.0 65.4 66.6	77.3 76.0 70.5 64.7 66.5 67.3	78.4 76.5 70.0 65.2 67.0 67.5	78.6 76.4 70.0 65.5 67.9 67.7	79°3 76°0 70°1 65°5 68°5 68°0	79.7 76.5 70.3 65.6 68.8 68.4	80°2 76°5 70°5 66°5 69°6 69°7	80°2 76°0 71°0 67°0 69°9 70°5	80.0 76.0 70.7 67.2 70.0 70.8
	22 23 24 25 26 27 28 29	65.4 65.7 65.8 68.0 69.2 66.3	66.5 66.0 65.8 67.0 68.8 66.9	67.5 66.4 67.5 67.0 68.8 68.5	68°3 66°9 68°5 68°0 69°0 68°8	69.2 68.0 70.0 68.6 68.9 69.5	69.5 68.5 70.8 69.6 69.1 69.7	70.0 69.0 71.3 70.4 68.8 69.8	70°0 70°0 71°8 71°5 69°0 69°7	70.8 70.4 72.6 72.1 69.4 70.0	71.0 71.2 73.5 73.0 69.8 70.7	71.5 71.6 73.4 74.0 70.5 71.0	71.5 72.2 73.5 73.2 70.4 71.5
	30 a 31 a					<u>-</u>							
Hourly	y Means	68:37	68.64	69.12	69.89	70.65	71.27	71.65	71.95	72.44	73.01	73.32	73.55

^a The 30th and 31st days are omitted from the Means, the readings having been affected to an uncertain amount by the induced magnetism of the vertical iron shafts of Robinson's anemometer.

	One Scale	Division =	·000087 pa	rts of the H		IZONTAL se, in Scale		orresponding	g to 1º decre	ase of Temp	perature, 1°6	3.
12 ^b .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17հ.	18 ^h .	19հ.	20h.	21h.	22 ^h .	23հ.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
609.0	604.1	605.0	604.0	603.8	604.0	604.4	605.2	604.0	601.5	604.2	610.0	604.20
603.7	603.0	606.9	606.0	607.5	608.8	610.0	610.0	609.0	607.0	609.2	607.0	604.60
615.0	613.0	621.9	597.0	547.2	455.6	5 40.6	538.7	569.2	575.5	580.0	575.0	589.23
588.0	588.5	587.0	596.8	581.0	578.4	583.8	587.3	588.0	577.0	592.0	590.2	581.52
578*2	582.4	584.0	590.0	597.9	588.6	593.0	589.2	573.0	572.2	593.8	594.0	588.14
618.2	584.0	584.0	590.0	584.4	580.4						595.0}	589.76
						585.0	594.0	591.5	597.5	596.0		
602.0	594.8	596.0	600.0	604.0	605.0	597.0	593.0	594.0	596.0	592.0	598.2	596.29
596.0	596.0	599.0	594.0	597.0	596.0	595.8	595.4	595.2	595.5	595.0	597.5	593.01
$600^{\circ}2$	596.0	597.5	599.8	601.0	598.2	602.8	595.0	597.8	597.3	598.6	599.2	592.85
598.2	591.0	597.0	597.0	597.9	597.1	597.0	597.2	597.6	592*2	597.0	600.5	593.10
601.2	602.9	598.2	598.6	592.7	590.8	591.0	598.8	599.5	599.8	607.5	612.0	593.35
587.0	585.4	592.0	591.4	592.0	593.5		_			l —	- 1	588.83
						590.0	591.5	592.0	593.5	593.0	595.0}	
590 . 5	590.0	593.0	597.2	597.0	594.5	594.2	593.2	598.0	593.5	601.4	605°0	5 91 4 0
602.5	601.0	601.5	600.2	597.4	597.0	592.8	597.0	593.0	603.4	602.0	602.0	596.93
601.2	611.0	606.0	597.0	592.9	599.2	604.0	604.9	604'0	607.5	607.2	608*5	601.06
307.2	607.8	610.0	609.0	610.8	610.4	611.0	608.2	611.2	601.5	611.2	610.0	609:33
604.2	608.4	610.8	609.4	608.5	611.4	611.0	616.5	614.0	614.0	611.2	613.2	606.49
306.2	608.0	609.0	609.0	621.0	573.0	_				-	1 . 1	
_						592.5	587.8	589.2	582.4	587.4	599.0}	600.45
597.5	599.0	591.0	588.2	591.4	595.8	594.4	595.5	600.7	594.1	596.1	596.9	593.47
595.4	592.4	597.2	592.1	595.9	596.0	588.8	566.4	566.0	575.4	579.0	589.5	588.62
20.0	585.2	586.4	581.0	579.2	572.0	572.2	578.5	580.2	582.2	581.2	592.0	581.87
201.0	292.0	594.0	595.0	596.0	600.0	595.0	599.0	602.0	599.5	600.0	600.8	597:35
299.0		603.0	598.5	587.2	900.0	601.6	600.0	598.0	590.0	592.0	599.2	596.15
298.0	599.0			603.4	603.8	001 0	000 0	030 0	390 0	032 0	055 2	
090 0	602.0	596.0	590.6	003 4	005 6	610.0	608.7	610.8	611.0	610.0	610.8	596.42
		_			_	010 0	000 /	010 0	011 0	010 0	010 0)	
_		_	_		_	_		_			_	
599.56	597.51	598.60	597.16	595.30	589.26	594.09	593.80	594.94	594.16	597.40	600.03	594.77
				Т	CMPERATUR	RE OF THE	BIFILAR M	AGNET.				
7°1.2	71.3	71°0	70°5	70°3	70°0	69°0	68.0	68.0	66.8	66°5	66.0	68.84
72.0	71.8	71.4	71.4	71.4	70.0	69.5	69.5	69.0	67.3	67.0	66.2	69.39
73.5	73.5	73.5	72.7	72.1	71.9	71.4	70.7	$70.\overline{2}$	69.4	69.0	68.6	71.07
74.0	73.2	73.0	72.6	72.0	71.6	70.8	70.2	70.0	69.5	69.4	69.2	71.84
73.4	73.1	$73 \cdot 2$	72.7	72.5	$72 \cdot 3$	72.1	71.7	71.0	70.7	70.7	70.2	72.84
73.0	72.5	72.5	$\frac{12}{72} \cdot \frac{1}{3}$	72.1	71.9		11 '	11 0				
_	12 0	12 0	120			67.5	67.5	67.4	67.5	67.5	67.3	70.76
75.3	74.4	74.3	73.5	73.0	73.0	72.5	72.0	72.0	71.2	71.0	70.8	71.89
75.5	75.3	75.0	74.5	74.4	74.0	74.0	73.6	73.4	73.2	72.6	72.2	73.71
74.7	74.0	72.8	72.4	72.2	71.4	71.0	70.6	70.5	70.0	69.6	69.2	72.30
75.0	74.4	74.0	73.8	73.6	73.2	73.0	72.8	72.6	$72 \cdot 2$	71.9	71.9	72.64
76.0	75.6	75.5	75.0	74.7	74.2	74.0	73.7	73.2	73.0	73.0	72.6	74.44
77.8	77.2	77.0	77.0	77.0	76.8			10 0	,,,,		. 11	
		110	''	'	, , , ,	77.0	76.7	76.0	75.5	75.5	$\left\{\begin{array}{c} -75\cdot 2\end{array}\right\}$	76.10
81.0	80.2	80.0	79.0	78.2	77.7	77.5	76.7	76.2	76.0	75.4	75.0	77.84
76.0	75.2	75.1	75.0	74.6	$74 \cdot 2$	73.6	73.0	72.5	72.0	71.2	71.2	74.81
70.0	69.0	68.0	67.5	66.8	65.9	65.6	65.3	65.1	64.9	64.7	64.7	68.35
67.8	67.0	66.2	66.3	65.8	65.4	65.0	65.0	64.2	64.5	64.0	63.2	65.42
70.0	69.7	68.8	68.0	67.7	67.2	66.2	66.4	65.9	65.4	65.0	65.6	67.27
71.8	72.0	71.4	70.4	69.7	69.4	50.0	UU 4	00 3	- OU T			
	12 0	114	10 4	03 1	U3 4	68.4	67.8	67.4	66.8	66.4	66.0}	68.33
71.5	71.0	70.7	70.4	69.6	69.2	68.6	68.0	67.5	66.8	66.2	66.0	69.04
72.4	72.0	70.9	69.8	69.5	69.0	68.5	68.2	67.6	67.2	66.4	66.5	68.90
73.6	73.0	72.1	71.5	70.6	70.2	69.8	69.5	69.2	69.5	68.0	67.0	70:37
73.0	72.7	$\frac{72.1}{72.4}$					71.0		70.4	70.0	69.6	
70.7	71.0		72.2	71.0	71.0	71.0		70.7			66.6	70.73
71.6		71.0	70°5	70.2	70.0	69.4	69.0	68.2	68.0	67.5	_ 11	69.34
	71.0	70.6	70.4	70.2	70.0	69.0	68.8	 68 ° 5	68.2	68.0	$\frac{-}{67\cdot7}$	69.43
_	. —				_		-					
_	_				1						1	
-	72.95	72.25	72.06	71.65	71.24	70.61	- 70·25	<u>-</u>	69.43	69.05	<u>-</u>	71:07

	Or	ie Scale Div	ision = •00	0087 parts o	of the H. F.	Increase,	n Scale Div	isions, corre	sponding to	1° decrease	of Tempera	ture, 1°63.	1
Mean G gen T	öttin- ime. }	O ^h .	1 ^h .	2 ^h .	3h.	4 ^h .	5 ^h •	6 ^h •	7 ^h •	8 ^h •	9 ^h .	10h.	11h.
	1 a	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div					
	2 a 3 4	602°0 606°2	601.5 596.0	600.7 598.0	593.2 593.2	588.0 591.0	593.0 596.2	594.0 603.0	599·5 602·0	606.0 604.0	604.0 611.2	623°0 616°0	623°C
	5 6 7 8 9 10	615.0 611.0 611.8 621.4 600.4 610.5	610°2 606°2 605°5 601°0 600°0 605°0	605.5 602.0 597.7 595.0 599.8 598.5	593.0 589.8 587.0 591.5 592.0 588.5	583.0 578.2 579.4 593.8 586.0 579.5	585°0° 584°0 576°0 580°0 585°0 575°0°	586.0 586.8 581.6 595.6 592.0 580.0	592.0 596.8 590.0 588.5 607.0 586.8	602.5 607.0 598.0 600.0 616.0 595.8	600°2 609°8 604°1 617°0 620°5 605°8	612.8 615.7 604.0 618.0 617.0 612.5	614°2 610°0 606°0 600°0 622°8 612°0
SEPTEMBER.	12 13 14 15 16 17 18	598·5 621·2 620·9 627·0 614·0 613·0	582.0 617.8 616.1 626.0 613.0 607.5	573°0 608°0 607°0 625°0 608°0 597°8	581.0 600.0 596.0 615.0 598.0 585.4	557°2 597°0 590°0 598°0 583°0 578°0	574·2 601·1 594·0 591·0 579·0 582·5	571.0 608.5 594.0 589.0 586.0 582.2	581.6 615.0 598.0 591.5 591.2 586.1	608 2 624 0 604 0 605 0 594 8 596 8	600°2 624°0 614°0 610°0 601°0 595°6	604.8 624.2 617.0 625.5 603.4 606.5	610°4 620°6 620°6 620°6 606°6 608°6
<i>3</i> 2	19 20 21 22 23 24 25	617.8 615.8 617.0 611.0 597.0 570.3	614.2 618.0 608.0 	606.8 604.0 612.5 603.4 — e 557.0	596.8 598.9 600.0 602.2 502.8 548.1	585.0 592.0 609.0 605.0 491.8 546.1	586°1 588°0 604°5 602°5 439°9 546°2	594.8 593.0 604.5 611.0 490.2 555.0	594°0 603°0 607°0 619°0 603°7 572°2	609.4 615.0 631.0 605.0 515.0 581.0	618 ° 0 619 ° 0 620 ° 0 612 ° 5 602 ° 7 585 ° 0	621.0 618.0 607.4 613.0 584.0 583.0	619° 616° 613° 623° 577° 586°
	26 27 28 29 30	598.0 582.0 600.5 602.5	277.7 577.5 602.0 605.0	475°8 574°0 596°5 600°0	518.5 564.0 593.0 593.4	545.4 560.0 589.0 584.8	557°5 565°0 577°2 580°0	551.0 572.5 543.0 578.2	563°5 581°5 608°0 576°2	597.5 589.0 616.0 583.1	602.0 598.0 631.2 605.8	592.0 598.5 646.8 609.2	580° 590° 642° 606°
Hourly	Means	608.63	603.97	598.65	590.91	584.53	583.90	586.44	594.86	604.30	609.42	613.21	612
		1	1		TEMP	PERATURE	OF THE BIL	FILAR MAG	NET.			<u></u>	
	(1 a 2 a	<u> </u>	-	<u> </u>	-	<u>-</u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>
	3 4 5	66·5 66·7	66.6 65.4	66.7 65.3	66.7 65.0	67.7 65.0	68.5 65.2	69°0 65°2	70.0 65.2	70·3 65·2	71.3 65.2	71·7 65·2	71 · 65 · 1
	6 7 8 9 10 11	62:1 63:7 66:4 65:8 61:5 60:1	62.5 64.2 66.6 65.5 61.7 60.0	63.5 65.2 67.4 65.2 62.2 62.0	65.0 66.6 67.6 65.0 63.0 62.7	65.0 67.6 68.6 64.9 63.7 63.5	65.0 68.2 70.0 65.4 64.2 64.0	65°3 68°4 70°9 65°4 64°3 64°4	65.6 68.6 71.5 65.6 65.0 64.6	66°2 68°7 71°7 66°0 65°4 65°2	66.8 68.9 72.0 65.8 66.0 65.6	67.4 68.7 72.0 66.0 66.4 66.2	67 68 66 66 66 66 66 66 66 66 66 66 66 66
SEPTEMBER.	12 13 14 15 16 17 18	62.7 56.5 54.2 56.4 59.5 62.9	62.5 56.2 55.0 57.0 59.3 63.0	62°5 56°4 55°7 57°5 59°8 63°3	62.6 56.5 57.2 58.8 60.9 63.3	62·5 56·7 57·8 60·0 62·2 63·6	62.8 57.0 58.2 61.0 63.3 64.0	62·5 57·2 58·8 61·4 63·9 64·2	62.5 57.4 59.3 61.9 64.4 64.5	62°3 57°8 59°8 62°0 64°8 64°5	62.0 58.2 60.5 63.0 65.2 64.6	61 · 4 58 · 9 61 · 7 64 · 0 65 · 5 65 · 0	60 : 6 58 : 6 62 : 6 64 : 6 64 : 6
J 1	19 20 21 22 23 24 25	60.8 60.0 57.5 60.5 63.5 60.0	61.2 60.2 58.0 60.5 — 59.2	61.3 60.8 59.0 61.3	61:4 61:7 60:0 62:2 63:2 59:2	61.5 62.0 60.5 63.0 63.0 59.5	61.7 62.3 61.2 63.8 63.1 60.0	62.0 62.9 61.8 64.0 63.1 60.3	62.4 63.3 62.4 64.5 63.3 60.7	62.5 63.5 62.6 65.3 63.3 61.0	62.4 64.2 63.5 66.5 63.3 60.9	62.8 64.9 64.2 67.0 63.3 61.4	62:8 65:4 64:8 67:4 63:3 61:0
	26 27 28 29	62·1 61·7 56·8	62.5 61.5 56.5	62.7 61.6 56.9	63.0 62.1 57.0	63.5 62.1 57.4	64.0 62.6 57.4	64.5 62.6 58.0	65°5 62°4 58°6	66°2 62°7 58°4	67.5 62.7 58.4	68°3 62°4 53°8	68 3 62 2 58 6
	30	55.0	55.0	56.0	57.2	58.0	58.4	58.8	59.0	59.0	59.0	59.4	59 '

The observations on the 1st and 2d days are omitted from the Means, the readings having been affected to an uncertain amount (up to four hours on the 2d) by the induced magnetism of the vertical iron shafts of Robinson's anemometer.

• Eight minutes late.

	One Seels	Division —	:00 0 002 par	rts of the H	HOI F. Ingress	RIZONTAL	FORCE.	rresponding	to 1° decre	ase of Temp	erature, 1°6	3.
12h.	13h.	14h.	15 ^h .	16h.	17h.	18h.	19h.	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
606.0	596°0	604.0	604.8	607.2	604.2	605.0	605.0	607.0	607.9	609.9	610.5	603.95
615.0	608.8	607.8	600.0	605.0	615.0	609.0	611.2	612.0	612.4	616.0	616.0}	606.68
617.0	615.1	605°2	603.0	603.5	$\frac{-}{597.2}$	604.2	609.8	611.0	609.2	610.0	613.0	604.07
611.2	609.2	609.0	608.8	609.0	608.0	611.2	611.0	611.0	612.0	612.0	612.0	605.10
606.2	605.0	606.0	607.0	604.8	605.0	606.1	607.2	608.2	610.0	610.2	612.2	601.23
611.0	613.0	598.0	610.0	608.4	606.2	603.8	604.4	611.0	608.0	608.2	609.2	603.89
624.8	616.8	609.0	606.6	610.2	612.9	612.9	612.0	611.8	613.2	613.2	616.0	608.27
611.9	610.2	605.1	607.2	607.7	608.2						$\left\{ \frac{-}{598.0} \right\}$	598.98
-		-		_		593.5	602.0	598.8	601.0	582.0		597.56
599.0	597.2	597.0	606.0 q	603.0	601.0	603.0	611.0	618.5	620.0	$\begin{vmatrix} 620.5 \\ 620.6 \end{vmatrix}$	$\begin{array}{c c} 623.2 \\ 620.9 \end{array}$	617.19
627.5	620.0	620 0	619.0	621.0	621.0	620.0	621.4	618.8 c	$621.0 \\ 624.2$	625.0	625.0	612.98
619.8	617:0	620.0	614.5	615.8 631.0	615.8	619.8	620.2	623.5	613.2	617.0	614.0	612.98
622.4	612.8	617.0	614.5		609.0	612.0	612.2	613.0	606.2	612.0	612.0	604.39
611.0	611.0	613.0	612.0 611.0	611.8 612.0	614.2 614.0	611.9	611.2	602.0	000 0		1 1	
012 2	012 0	015 0	611 0	012 0	014 0	609.0	605.8	610.0	610.0	620.5	617.8	603.63
612.2	609.0	614.0	610.0	608.8	601.0	603.2	605.0	610.0	609.2	615.8	616.2	607.40
615.0	616.0	615.0	615.4	620.2	622.2	617.0	616.1	616.2	618.0	616.0	615.4	611.28
615.0	610.5	608.9	613.6	616.1	611.0	611.0	608.0	611.2	608.8	613.5	616.2	612.03
609.1	583.6	604.8	604.0	609.0	608.8	584.8	554.0	537.5	570.5	579.5	531.0	595°5 1
594.2	583.0	561.4	561.3	560.2	561.5	557.5	559.0	553.8	569.0	573.5	576.0	$555^{\circ}24$
586.2	586.2	588.8	591.5	592.0	592.0				-		$\{-\frac{1}{472\cdot 2}\}$	$566^{\circ}24$
			 			566.2	565.0	580.0	527.6	548.0		
584.0	576.0	583.0	587.2	589.8	575.0	594.4	586.0	582.0	581.9	583.8	583.4	548.56 585.74
580.0	577.5	585.0	594.0	596.4	597.7	593.0	601.6	600.0	593.5	591.4	595.5 608.0	598.88
598.7	605.5	584.0	585.0	589.8	574.0	579.0	605.5	597.5	600.0	613.0	613.2	602.53
610.0	614.4	610.0	610.0	609.5	610.0	612.0	611.0	611.0	612.0	010 0	010 2	002 00
610.10	606.67	606.07	606.72	608.74	606.76	604.01	605.04	605.48	604.95	607.07	603.07	602.76
	<u> </u>		<u></u>	TE	MPERATUR	E OF THE I	BIFILAR MA	GNET.				
0	0	0	0	0	0	0	0	0	0	· -	<u> </u>	<u> </u>
71.0	70.0	69.5	68.8	68.6	68.3	67.6	67.1	66.6	66.4	66.1	65.7	68.42
65.1	64.8	65.0	65.0	64.9	64.8		<u> </u>				$\left \begin{array}{c} -1 \\ 62 \cdot 8 \end{array} \right\}$	64.83
	<u> </u>			 		64.7	64.3	63.9	63.7	63.2		1
67.9	67.7	67.4	66.9	66.7	65.9	65.7	65.2	65.0	64.6	64.4	64.0	65°56 67°16
68.5	67.8	67.6	67.5	66.7	66.7	66.7	67.0	66.6	66.5	66.5	66.3	69.55
72.0	72.0	71.5	71.0	70.6	69.7	69.0	68.2	67.8	67.5 62.1	67.0 61.9	61.7	64.68
66.6 66.6	65.5	65.0	65.0	64.6	64.2 63.6	$\begin{array}{c} 63.6 \\ 63.2 \end{array}$	63°1 62°9	62.7	61.2	61.3	60.2	63.85
66.4	66°2 66°0	$65.6 \\ 65.0$	64.9 64.4	64°1 64°0	63.8		02 9	02 2	— OI 0	""		63.91
	00 0	00 0	04.4		- 00 0	63.2	63.5	63.4	63.2	63.0	63.0}	
60.2	59.7	59.4	58.2	58.2	58.0	57.7	57.2	57.0	57.0	56.7	56.8	60.15
59.5	58.8	58.4	57.7	57.0	57.0	56.2	56.2	56.0	55.4	55°1	54.6	57.08
63.0	62.3	61.2	61.0	60.6	60.2	59.8	58.9	58.2	58.0	57.5	57.2	59.13
64.0	63.2	63.0	62.1	61.5	61.1	61.0	60.6	60.2	60.0	60.0	59.5	60.99
64.8	64.4	63.0	63.7	63.2	62.6	62.3	62.3	62.3	62.8	63.0	63.0	62.99
64.7	64.7	64.3	63.7	63.6	63.6	<u> </u>			61:0	61.0	$\frac{-}{60\cdot 2}$	$63^{\circ}22$
62.5	C0:0		-	C1:0	<u> </u>	60.6 60.6	60.3 61.0	61.0	60.1 61.0	$\frac{61.0}{60.2}$	60.0	61.43
65.2	62.0 64.5	62.0 64.0	61.5	$61.2 \\ 62.5$	61.0 62.2	61.5	60.2	60.0	59.5	59.0	58.4	62.12
64.8	64.8	64.3	63.2	63.0	62.8	62.4	62.5	61.8	61.2	61.0	61.0	62.02
67.1	66.7	66.2	66.5	65.2	65.4	65.0	64.6	64.4	64.4	64.0	63.2	64.55
63 .5	62.9	62.5	62.0	62.0	62.0	61.9	61.2	61.3	61.0	60.8	60.2	$62^{•}44$
61.0			61.0	61.0	61.0						$\frac{-61.6}{61.6}$	60.63
61.5	61.3	61.2	0-0		i	60.6	60.6	60.8	61.5	61.2	61.6	
	61.3		—						00	00.0		65.00
68.0	61.3	67.0	66.6	66 2	65.6	65.0	64.5	63.7	63.2	62.5	62.4	65.03 60.67
68.0 65.0	61.3	67.0 60.8	66.6 60.2	60.0	59.2	65.0 58.8	64°2 58°3	63.7 57.9	57.0	56.5	62.4 57.0	60.67
68.0 62.0 58.5	61.3 67.6 61.4 58.5	67.0 60.8 58.2	66.6 60.5 58.4	60.0 58.3	59°2 57°5	65.0 58.8 57.2	64°2 58°3 57°0	63.7 57.5 57.5	57°0 57°3	56.5 56.2	62.4 57.0 55.0	60.67 57.60
68.0 62.0	61.3	67.0 60.8	66.6 60.2	60.0	59.2	65.0 58.8	64°2 58°3	63.7 57.9	57.0	56.5	62.4 57.0	60.67

	0	ne Scale Div	vision = '00	0087 parts	of the H. F.		NTAL FO in Scale Div		esponding to	1º decrease	of Tempera	ature, 1.63.	
	Göttin- }	Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8h.	9 ^h .	10h.	11h,
100	$\begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$	Sc. Div. 612°2 616°4	Sc. Div. 610.0 616.8	Sc. Div. 611.8 613.0	sc. Div. 603 * 8 602 * 0	sc. Div. 596°2 594°0	Sc. Div. 593°2 609°2	Sc. Div. 592°0 613°0	Sc. Div. 598°0 604°5	Sc. Div. 600 5 613 0	Sc. Div. 604 2 608 3	Sc. Div. 615 0 611 0	Sc. Div. 606°0 610°0
	3 4 5 6 7 8 9	622.0 623.5 617.5 615.8 607.2 617.8	620°0 618°0 613°0 610°2 603°7 615°0	620°0 609°0 603°2 604°4 604°0 609°0	619.0 600.0 599.2 597.6 597.0 605.0	613.5 600.0 592.0 592.0 595.0 595.0	611.0 605.0 593.0 592.0 596.2 601.5	605°0 610°0 598°2 598°0 599°5 603°0	613 · 0 614 · 0 603 · 0 612 · 2 610 · 0 602 · 0	616.5 611.2 609.6 612.8 622.5 608.0	616°1 619°0 613°1 618°2 619°0 618°0	617'0 622'8 611'8 619'2 608'0 621'0	621'0 606'0 613'6 622'0 613'0 627'2
OCTOBER.	11 12 13 a 14 15 16	618.8 630.8 625.0 616.4 626.8 619.5	616.5 623.0 611.0 611.0 626.0 618.8	610°0 613°0 540°0 606°2 622°0 613°0	607.0 614.2 567.0 591.0 614.0 612.0	599.0 605.8 589.0 603.5 603.0 605.7	599.0 607.5 595.0 603.8 607.5 597.5	604.0 615.0 617.0 599.0 604.0 609.0	611.5 624.0 610.0 610.0 614.5 615.0	614.2 626.0 610.0 611.0 613.0 608.2	607 · 2 619 · 2 611 · 0 615 · 5 620 · 0 619 · 5	624 ° 0 617 ° 2 613 ° 0 618 ° 5 621 ° 0 620 ° 2	624.4 627.8 599.0 620.0 620.2 620.9
.00	17 18 19 20 21 22 a 23 a	619·2 613·0 621·0 621·0 630·5 403·0	612.0 600.0 618.2 617.5 625.5 38.0	611.0 596.0 607.0 614.8 618.0 423.3	592.2 590.1 605.0 611.0 619.0 399.6	601 · 2 606 · 5 599 · 7 603 · 8 613 · 0 587 · 4	604·2 592·4 597·0 594·1 609·0 522·6	602 · 9 584 · 0 601 · 2 600 · 0 608 · 0 627 · 7	599.0 598.7 607.0 604.0 613.8 600.7	600°1 597°3 604°0 611°0 620°2 607°0	606°0 601°0 612°5 619°5 625°8 525°4	604°3 605°0 619°0 620°2 626°6 577°7	607'8 611'2 621'6 623'0 619'0 630'0
	24 25 a 26 27 28 29 30 31	585°3 607°0 628°0 633°5 620°0 631°5	551.2 601.0 624.0 629.0 640.0 629.4	460°0 598°8 616°0 623°4 611°0 622°0	503°8 595°0 607°8 615°0 628°0 617°9	544.2 591.4 600.4 604.0 618.8 607.0	590.6 589.0 596.5 600.0 612.2 604.0	597.5 597.0 599.0 606.5 610.5 609.2	554.0 602.5 603.0 615.0 602.0 614.0	628 ° 0 606 ° 5 612 ° 2 622 ° 0 609 ° 7 619 ° 0	590°0 609°5 618°0 623°0 616°0 622°7	606°0 609°6 622°0 626°0 620°8 626°0	601'5 608'0 627'5 632'0 623'0 621'5
Hourly	y Means	619.95	616.96	610.82	605.63	601.25	600*26	602.73	608.04	611.59	614'80	617:25	618.28
	<u>. 1 </u>	57.4	58.2	59.0	темрі 59°0	58.7	59.0	LAR MAGN	ьет. 59°0	59.2	59°4	59°8	59.9
	$\left[\begin{array}{c}1\\2\\3\end{array}\right]$	54.5	54·4	55·2	56·7	57.8	58.5	29.0	29.8	60.6	61.9	62.5	62.5
	3 4 5 6 7 8 9	55°0 60°0 61°5 62°4 62°1 58°9	55.4 60.0 61.5 61.9 62.1 58.0	56.4 60.0 61.4 61.8 62.1 59.8	58°2 60°5 61°2 61°6 62°1 60°2	59.0 60.7 61.3 61.5 62.4 60.8	59.6 61.5 61.4 61.7 62.8 60.8	60°3 62°5 61°8 61°9 63°0 60°9	61.2 62.9 62.0 61.9 63.0 60.9	61.7 63.7 61.9 61.7 63.0 61.0	62.2 64.8 62.1 61.7 63.0 61.7	62.4 65.3 62.1 61.8 63.2 62.0	62.4 65.2 62.0 61.8 63.0 62.0
OCTOBER.	11 12 13 a 14 15 16	54.2 54.5 53.4 50.8 47.4 50.9	54.6 54.5 53.2 50.2 47.3 51.0	55.5 54.5 53.3 50.0 47.5 51.9	56.4 54.6 53.5 50.9 47.0 52.9	56°3 55°0 53°4 51°4 48°5 54°0	56.5 55.2 53.5 52.2 50.0 54.5	56.5 55.3 53.6 52.8 50.8 55.0	57.0 55.0 53.9 53.3 51.0 55.8	57.4 54.4 54.4 53.4 51.4 56.4	57.5 54.6 54.5 53.5 51.8 57.4	57.6 54.8 55.0 53.5 51.9 58.0	57.8 54.5 55.3 53.5 52.0 58.0
OC1	17 18 19 20 21 22 a 23 a	56°1 59°4 54°0 55°4 52°5 52°9	55.5 58.6 53.4 54.3 52.0 52.6	56.5 58.6 53.8 54.0 51.9 52.6	57.4 59.5 54.0 54.4 51.9 53.1	57.6 59.5 55.7 54.6 51.9 54.1	58.8 60.0 56.5 55.1 52.4 54.9	59.4 60.0 57.0 55.1 52.5 55.5	60°2 60°4 57°3 55°5 52°6 55°8	61.5 61.0 57.5 55.5 52.8 56.8	62.5 61.5 58.6 55.9 53.2 57.8	63.0 61.9 59.5 55.5 53.4 59.0	62:9 61:1 59:5 55:4 53:0 59:0
	24 25 a 26 27 28 29	55.6 49.0 43.9 44.8 48.1 52.0	55.4 49.0 43.4 44.5 48.5 51.4	55.6 49.4 43.5 45.8 48.7 51.4	55°5 49°4 44°3 47°0 49°3 52°2	56.1 49.6 45.4 48.3 51.3 53.0	56°3 49°8 45°8 49°0 52°2 54°0	56.4 50.1 46.1 49.4 52.5 55.0	56.6 50.1 46.9 49.7 53.0 55.7	56°5 49°8 47°7 50°6 53°6 55°7	56.4 50.3 48.4 51.7 54.2 56.2	55.6 50.3 48.4 51.8 55.1 56.6	54.5 49.5 48.6 51.6 54.3 56.3
	$\begin{bmatrix} 30 \\ 31 \end{bmatrix}$	∥ —							_				

^a Not included in the Means, on account of disturbance.

129. 139. 144. 159. 164. 179. 189. 199. 209. 219. 229. 239.		One Scale	Division =	*000087 pai	rts of the H.		ZONTAL :		orresponding	g to 1° decre	ease of Tem	perature, 1°6	33.
608 0 612*8 614*5 614*0 618*0 612*0 610*8 613*5 616*8 616*6 616*8 618*2 618*0 612*0 612*0 612*5 614*0 613*0 615*2 615*0 615*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0 610*0	12h.	13h.	14 ^h .	15h.	16 ^h .	17h.	18h.	19 ^h .	20 ^h .	21h.	22h.	23h.	Daily and Monthly Means.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								Sc. Div.				Sc. Div.	Sc. Div.
6207-2 (6207-5 (6207-0 (6207-0 (6197-3 (6227-1 (6197-6 (6197-0 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6 (6157-6													613.60
6137-6 612-4 614-2 615-6 613-8 613-5 619-9 617-0 619-0 616-0 616-5 616-5 616-8 616-8 616-8 616-8 616-8 616-8 616-8 616-8 616-8 616-8 616-8 616-8 616-9 616-9 616-5 616-5 616-5 616-9 616-9 616-5 616-5 616-9 619-4 618-9 619-4 618-9 619-4 618-9 619-4 618-9 619-5 620-6 617-6 617-5 618-9 620-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6 617-6			_				620.0					621.2	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	620.2	620.5	620.0	620.0	619.3			620.2	620.0	620.8			618:37
$ \begin{array}{c} 62000 & 61918 & 61975 & 62015 & 62110 & 66270 & 62370 & 62772 & 61418 & 60778 & 61122 & 61676 \\ 61676 & 62374 & 60911 & 60990 & 61448 & 61611 & & & & \\ 62578 & 62578 & 62210 & 62220 & 62178 & 62370 & 62370 & 62070 & 62448 & 62870 & 62970 & 63970 \\ 62936 & 63570 & 63112 & 62220 & 62118 & 61125 & 61370 & 62070 & 62448 & 62870 & 62970 & 63970 \\ 62936 & 63570 & 63112 & 62220 & 61240 & 6125 & 61370 & 61412 & 61670 & 61977 & 61990 \\ 62915 & 62170 & 62200 & 61240 & 61275 & 61370 & 61412 & 61674 & 6177 & 61970 \\ 61170 & 61672 & 62204 & 62471 & 62470 & 622870 & 62873 & 62570 & 62448 & 62370 & 6222 & 62885 \\ 62175 & 62170 & 622074 & 62471 & 62470 & 622870 & 62873 & 62570 & 62448 & 62370 & 6222 & 62885 \\ 62171 & 66170 & 61075 & 61155 & 61070 & 61575 & 601875 & 60187 & 60187 & 60197 & 61997 \\ 61170 & 61672 & 62204 & 62471 & 62470 & 62870 & 62873 & 62570 & 62448 & 62370 & 6222 & 62285 \\ 62171 & 60677 & 61070 & 61175 & 61070 & 61575 & 61195 & 61175 & 61179 & 61475 & 61672 & 61675 \\ 61370 & 61477 & 61370 & 60675 & 61370 & 60575 & 61170 & 60970 & 61573 & 61670 & 61575 & 61875 \\ 62570 & 62578 & 62678 & 62771 & 62776 & 62870 & 62970 & 62972 & 62320 & 63178 & 63070 \\ 62270 & 62578 & 62678 & 62771 & 62776 & 62870 & 62970 & 62972 & 62320 & 63178 & 63070 \\ 62270 & 59470 & 58470 & 58570 & 58570 & 58570 & 58570 & 58570 & 62770 & 62875 & 60170 & 60972 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62970 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 & 62972 &$	613.0	612.4	614.2		613.2								612.99
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	614.8	616.0	615.8										611.34
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					1		_						613.70
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S32'0 594'0 581'0 565'5 548'0 565'0	24.0	614.4	619.0	618.0	619.0	631.0	632.8	641.3	583.0	503.0	222.2	480.5	592:37
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Mean (Föttin- }	Oh.	1 ^h .	2h.	3 ^h .	4 ^h .	5 ^h .	6 ^հ .	7 ^h .	8h.	9h.	10h.	11h.
	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{pmatrix}$	sc. Div. 617 0 605 2 610 0 623 5 623 2 631 0	sc. Div. 615 '9 605 '0 610 '0 620 '0 620 '0 627 '8	Sc. Div. 585°0 601°2 610°0 616°0 622°8 622°2	sc. Div. 573°0 600°0 609°0 609°2 614°1 612°7	Sc. Div. 610°5 597°0 600°0 602°0 608°1 608°0	sc. Div. 616°0 597°5 593°0 597°2 605°1 617°5	Sc. Div. 594*5 596*0 591*8 595*8 610*6 605*0	Sc. Div. 606°0 599°0 598°2 596°1 615°0 612°0	sc. Div. 603 *8 602 *4 607 *2 606 *0 618 *9 630 *0	Sc. Div. 610 ° 0 600 ° 5 605 ° 4 605 ° 0 620 ° 0 621 ° 5	Sc. Div. 620 ° 0 602 ° 2 607 ° 2 604 ° 0 624 ° 0 621 ° 5	Sc. Div. 613 0 598 8 609 7 611 0 628 0 626 0
ER.	7 8 9 10 11 12 13 14	637.0 633.0 625.0 630.0 633.1 638.0	623°0 622°5 627°0 624°4 630°3 632°4	624.0 615.0 623.0 618.2 623.0 628.0	621 '4 605 '0 614 '0 607 '0 615 '0 621 '5	620°5 605°4°6 601°2 596°0 607°0 615°0	612.5 596.0 596.5 590.3 601.2 597.5	609 · 5 593 · 0 598 · 0 593 · 2 603 · 2 597 · 0	615 ° 0 592 ° 5 606 ° 2 599 ° 0 609 ° 0 617 ° 0	610°5 606°2 610°0 608°5 621°0 613°0	609.0 614.4 605.8 618.0 624.5 622.0	621.0 608.8 613.6 623.0 632.0 636.0	633'8 613'1 614'0 620'4 636'0 625'0
NOVEMBER.	15 16 17 18 19 20° 21	639.0 649.5 631.8 631.0 630.8 630.5	638.0 650.0 630.6 626.6 631.0 550.0	632.5 635.0 625.0 618.0 624.5 627.0	621 ° 0 618 ° 2 614 ° 0 617 ° 0 619 ° 0 637 ° 4	619.0 619.0 608.2 623.5 615.0 609.0	604.0 614.8 607.2 622.0 610.0 608.0	609°0 608°2 605°0 621°2 614°0 610°0	616 2 605 0 602 0 621 5 624 0 622 2	620.0 610.0 615.0 624.0 635.0 635.8	629.6 630.3 624.0 620.8 665.0 636.8	636.0 617.1 629.0 632.0 622.4 641.2	638.0 629.0 623.5 628.5 625.7 641.3
	22 ° 23 24 25 ° 26 27 28	650.0 604.2 604.4 604.0 604.5 631.4	646.5 601.2 604.0 604.8 604.5 630.2	640°0 598°8 602°0 607°0 575°0 627°0	631.0 596.0 594.5 598.5 606.0 615.8	625°2 593°0 586°7 600°0 604°0 615°0	592.8 595.0 584.0 602.0 598.0 619.0	644.5 594.0 586.5 583.0 596.0 615.3	627.5 599.0 593.0 576.0 604.2 615.0	661.0 602.5 604.0 597.0 609.2 624.0	649.0 596.0 607.0 599.0 621.0 628.8	648.0 600.5 608.7 632.2 623.9 633.5	659.0 598.0 596.0 643.8 610.0 612.5
	29 30	657°2 658°2	652.0 656.0	652.0 651.3	646°5 647°5	642°3 645°0	638.0 638.0	638.0 633.0	641.0 642.0	642.0 641.0	648.0 643.0	651.0 647.0	652°0 651°0
Hourly	Means	628:17	625.32	618.67	612.93	610.20	606.53	604.69	609.91	615.83	620.42	622:37	621.43
		0	0	0	i ·	l .	F THE BIF	1			57.9	58.6	58.4
	1 2 3 4 5 6	53.9 57.2 58.6 57.8 54.4 51.1	54 ° 0 57 ° 2 58 ° 3 57 ° 2 53 ° 8 50 ° 6	54·1 57·1 58·5 57·2 53·4 51·0	54·4 57·4 58·5 58·5 53·4 51·5	55.0 58.8 59.0 58.6 53.6 51.6	55°3 59°3 59°2 59°4 54°1 51°9	56.4 59.9 59.7 59.7 54.5 52.3	56.7 60.3 60.1 60.0 54.7 52.3	57.3 60.9 60.2 60.0 54.9 52.8	57.9 61.5 60.1 60.4 55.8 53.5	58.6 62.0 60.0 61.0 56.0 53.7	58 4 62 0 60 0 60 8 55 0 53 1
3R.	7 8 9 10 11 12 13	49.4 55.8 52.2 50.4 49.4 49.2	50.0 56.2 52.2 50.0 48.4 49.0	49.9 56.2 52.0 50.0 49.0 49.0	50.0 56.2 52.4 50.0 49.4 49.7	50.5 56.5 52.3 49.8 49.8 49.9	51.1 57.0 52.4 50.5 50.0 50.7	51.6 57.5 52.5 51.2 50.8 51.0	52.4 57.8 52.6 51.4 50.9 51.5	52.8 58.4 52.7 51.3 51.1 51.7	53.4 59.2 52.6 51.0 51.2 52.0	53.7 59.3 52.5 51.2 50.7 52.0	53.9 59.1 52.0 51.0 50.5 51.8
NOVEMBER.	14 15 16 17 18 19 20 °	47.2 47.0 53.2 54.2 51.3 42.5	47.3 47.0 53.0 54.0 51.0 42.5	47.4 47.0 53.0 53.6 50.4 43.0	47.9 47.4 52.7 53.2 49.5 43.9	48.5 47.6 53.0 53.5 48.8 44.4	49.5 48.4 53.6 53.8 48.8 45.2	49.5 49.2 54.0 54.0 48.3 46.0	49.6 50.0 54.2 54.0 48.2 46.2	50°5 50°3 54°2 53°6 48°0 46°6	50.0 51.0 54.9 54.1 47.8 47.1	49.7 51.1 54.9 54.3 47.0 47.2	49°1 51°2 55°3 54°0 47°0 46°4
	21 22 ° 23 24 25 ° 26 27 28	45.7 51.6 55.5 54.2 49.0 45.6	46.0 51.0 55.4 54.2 48.0 45.5	46.4 50.8 55.4 53.9 47.4 44.9	47.0 50.6 55.0 53.9 47.0 44.7	47.4 50.6 55.2 54.8 46.9 45.2	48.7 51.6 55.8 55.0 47.3 46.0	49.8 52.0 56.0 55.0 47.5 46.2	50.4 52.8 56.1 54.8 47.4 46.2	51·2 53·2 56·2 54·5 46·8 46·6	51.6 54.2 56.3 54.5 46.5 47.2	52.2 54.4 56.5 54.6 46.9 47.0	52.5 54.4 56.4 54.0 46.9 45.7
	29 30	34.2 35.8	34.4 32.8	34°2 35°5	34·2 36·1	34·1 37·7	35°1 38°5	35.6 39.4	36.2 39.8	37.5 40.0	38·2 40·8	39·0 41·2	38.8 41.2
Hourly	Means	50.62	50.40	50.30	50.42	50.72	51.27	51.69	51.98	52*22	52.59	52.73	52.50

^a Thirteen minutes late.

^b Two minutes late.

[°] Not included in the Means, on account of disturbance.

	One Scale	Division =	: 000087 p:	arts of the H		AIZONTAL ase, in Scale		correspondin	g to 1° decr	ease of Tem	perature, 1	63.
12 ^h .	13h.	14 ^h .	15h.	16h.	17h.	18h.	19h.	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Se. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 601 2	Sc. Div.	Sc. Div. 600 31
602.6	642.0	637.2	591.4	554.0	582.0	580.2	576.0	584.2	591.1	612.2		
599.9	605.8	601.0	604.2	602.2	597.0	599.3	590.4	612.0	602.4		607:0	601.59
610.5	612.0	611.8	607.0	607.4	607:5	607.4	604.0	614.5	610.0	608.0	620.0	
613.4	613.8	615.0	614.1	611.0	618.0	616.8	616.0	620.2	622.5	622.0	622.0	612.11
627.5	631.4	629.5	629'1	633.0	626.0	625.0	623.8	624.5	615.2	624.8	628.5	621.99
629.0	628.2	630.0	629.2	630.0	631.2	C01:0	617:6	637.0	638.0	640.6	639.0	625.30
	696:0	605:0	616:0	C00.7	60416	621.9	617.6	625.2	627.5	627.0	630.3	622.70
630.2	626.8	625.2	616.0	623.7	624.6	626.0	625.0ª		622.0	626.5	626.0	611.95
610.0	606.2	603.9	611.7	610.0	611.0	611.8	621.0	621.0	627.0	626.0	629.5	615.24
622.4	614.0	618.2	619.0	611.5	612.5	603.4	620.0	628.0		631.2		617.97
623.0	619.2	617.0	625.0	625.0	617.0	622.0	631.0	632.0	630.8		630.5	
631.5	633.0	630.0	632.2	627.2	629.2	632.8	632.7	631.5	630.5	631.1	632.0	625*36
622.0	635*0	636.8	635.0	635.0	633.0				C2710	637.2	$\{637.8\}$	627.71
						638.0	636.8	637.0	637.0			
637.0	637.0	637:0	633.9	634.0	637.0	636.8	633.0	635.0	637.8	638.0	632.0	630.45
629.0	629.2	627.2	623.7	627.2	625.2	628.0	629.0	630.0	630.0	634.2	633.7	626*35
620.5	615.0	614.0	627.0	629.0	625.5	622.1	625.8	625.0	624.2	622.4	629.0	620.62
621.0	631.0	632.0	627.2	630.0	628.0	630.0	630.0	631.2	623.9	625.3	629.0	626.03
632.2	641.8	628.4	636.0	639.6	612.0	627.0	629.0	629.0	630.0	631.2	632.0	628.53
638.0	635.0	637.0	638.0	637.8	639.4					0.45.0	$\frac{-}{648.0}$	631.01
		l		_		645.8	641.0	643.0	645.0	647.0	648.0]	
616.0	654.0	629.0	641.0	471.0	661.0	578.0	590.0	579.0	577.0	592.0	l oo i	619.12
501.3	606.3	605.0	605.0	603.1	603.0	602.0	602.4	601.2	603.2	604.0	605.0	600.85
624.5	621.0	623.7	621.0	593.2	582.8	600.8	596.2	603.7	601.0	595.9	598.3	601.36
636.8	638.0	648.7	585.5	567.1	574.4	567.7	534.2	538.4	597.4	575.0	598.5	596.21
624.3	607.0	614.1	629.0	629.0	622.0	620.0	621.5	621.5	619'9	621.9	627.5	613.08
626.0	630.5	631.0	633.0	635.0	632.0							
_					_	647.0	650.5	648.0	651.0	655.0	$\{-\frac{1}{657\cdot 2}\}$	631.81
654.0	656.0	654.0	654.0	655.8	655.0	654.8	655.0	655.4	656.0	656.4	655.7	650.71
223.0	651.0	651.0	652.2	652.2	653.3	652.2	652.8	651.7	650.0	644'3	648.8	648.77
623.69	625.79	624.81	624.17	621.66	620.51	621.97	622.28	626.02	625.25	626.80	628:32	620.34
20 03	020 19	024 31	024 17	021 00	020 21	021 37	022 00	020 02	020 20	020 00	020 02	020 01
	;	1	1	1	1	E OF THE I	BIFILAR MA	1			1 _ 1	<u> </u>
$58^{\circ}2$	57.5	57.5	57°6	57.5	57°8	58°0	57.5	57°4	57°2	57.0	56.9	56°75
61.4	61.1	60.5	60.5	60.0	59.9	59.2	59.2	59.1	59.1	59.0	58.7	59.64
60.0	60.0	60.0	59.9	59.9	59.4	59.2	59.5	59.2	59.3	29.0	58.1	59.42
60.2	60.3	59.2	58.8	58.2	58.5	57.3	56.5	56.0	55.6	55.2	55.3	58.43
54.8	54.6	54.3	53.9	53.6	53.2	53.2	53.2	53.0	52.8	52.2	51.2	53.94
23.0	52.6	52.0	51.2	51.3	51.0	00 0	00 2	00 0				
	32 0	32 0	01 0	01 0	51 0	48.0	48.0	48.4	48.5	48.5	48.8	51.12
53.8	54.6	54.5	54.2	54.5	54.2	54.1	54.0	54.0	54.6	54.8	55.5	52.97
58.7		57.0	56.5	56.0	55.4	55.0	54.0	53.2	53.0	52.8	52.2	56.58
52.3	57.5 52.2	52.0	51.8	51.8	51.8	51.8	51.2	51.4	51.3	51.0	50.7	52.00
51.0	50.8	50.6	50.0	20.0	50.0	50.0	50.0	20.0	20.0	50.0	50.0	50.42
50.6	50.4	50.4	50.4	50.7	51.3	51.2	50.2	50.5	50.1	49.2	49.2	50.52
51.8	51.4	50.6	50.1	49.8	49.1	01.2	1	00 2	-	- T3 2	- 1	
~ <u> </u>	014	30.0	90 I	ספד	73 1	46.5	46.3	46.8	46.7	46.6	47.1	49.60
49.4	10.0	10.2	10:0	10.0	47.8	47.5		47.4	47.2	47.4	47.0	48.37
51.3	48.8	48.5	48.2	48.0			47.5	52.5	52°5	52.8	23.0	50.24
26.0	51.4	52.0	52.0	52.0	52.3	52.5	52.5	55.0 55.0	54.8	55°0	54.7	54.61
54°4	56.0	56.0	55.5	55.5	55.5	55.5	55.2			52.2	51.6	53.85
	54.2	54.4	54.5	54.6	54.6	54.6	54.0	53.6	53.1	43.8	43.0	
47.8	47:2	46.6	46.5	46.1	45.1	44.7	44.2	44.5	43.9	400	. 11	47.08
46.0	45.0	45.0	44.9	44.7	44.7	44.4	1444	1 - 1	14:0	44.4	$\frac{-}{45\cdot 4}\}$	44.94
59:0		50:-				44.4	44.4	44.4	44.2			
52.9	52.6	52.5	52.0	52.0	52.3	52.6	53.0	52.0	51.7	51.7	51.8	50.67
54.9	55.0	55.2	55.2	55.5	55.7	55.6	55.4	55.3	55'1	55.5	55.9	53.81
57.0	56.2	56.2	56.0	55.7	55.2	55.4	54.9	54.5	54.2	53.7	53.4	55.53
54.2	54.0	53.0	53.0	52.9	52.8	52.6	52.0	51.7	51.4	50.5	49.5	53.37
47.0	46.6	46.8	46.8	46.7	46.5	46.2	46'0	45.0	45.3	45.5	45.6	46.73
45.5	44.8	44.9	44.5	44.3	44.1			_			— 1 l	42.57
						34.0	33.6	33.4	33.2	34.0	34.3 }	
38.6	37.8	37.4	37.5	37.4	37.0	37.0	37.2	37.2	36.8	36.4	35.6	36.58
41.9	41.2	41.4	41.4	40.8	40.7	41.0	40.2	40.2	40.8	40.5	40.2	39.71
											49.93	51.31

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1 652 0 651 0 650 0 649 0 647 5 646 0 646 0 663 0 663 0 653 0 652 0 649 0 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6 647 6	dean Göt gen Tim	ttin- }	O ^h •	1 ^h .	2h.	3h.	4 ^h .	5h.	6 ^h .	7 ^h •	8h.	9 ^h .	10 ^h .	11h.
2 636°5 666°0 646°0 647°5 646°5 692°2 615°5 610°2 629°5 615°6 617°1 628°2 629°3 630°6 645°6 645°0 640°0 639°6 645°7 633°8 630°6 633°0 627°0 630°0 630°9 640°6 630°6 633°0 627°0 630°0 630°6 640°6 630°6 630°0 627°0 630°0 630°0 640°0 630°0 640°0 630°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°0 640°														Sc. Div
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2	(1	40°·4	40°·3	40°5	41.0	41.9	42.4	43.0	43.5	44.0	44.6	45.2	45°6
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56 41.6 41.6 41.2 41.2 42.6 43.4 44.5 44.8 45.2 45.5 45.2 45.5 45.2 45.5 45.2 45.5 45.2 45.5 45.2 45.5 45.2 45.5 45.2 45.5 45.2 45.5 45.2 45.5 45.2 45.5 45.2 45.5 45.2 49.4 49.8 49.9 49.2 49.9 49.2 49.9 49.2 49.4 49.8 49.8 49.8 49.9 9.51.5 51.4 50.5 50.4 50.6 50.6 50.5 50.0 50.5 50.7 51.1 51.6 51.1 51.0 51.2 51.3 51.4 51.5 51.7 51.5 50.2 50.5 50.7 51.1 12	į.				46.0					46.4	ŧ .			45'2
6			44.6	44.3	43.6	43.6	43.6	44.0	44.0	44.0	44.5	44.4	44.3	43.8
8 47.0 46.5 46.1 46.4 46.9 48.0 48.6 49.2 49.4 49.8 49.8 49.8 9 51.5 51.4 50.5 50.4 50.4 50.6 50.6 50.5 50.0 50.5 50.7 51.0 10 54.0 53.8 53.6 53.9 53.8 54.4 54.7 55.4 55.0 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.2 55.3 51.1 12		6			41.2	41.2	42.6	43.4	44.5	44.8	45.2	45.5		45'2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ľ	7												49'4
10	- 1													49.7
11	1,													
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	11			51.0			51.4						51.4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			49.0	49.0		48.5	48:5				49.5	49.5		49.5
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	BE 1	14			46.2	46.4	46.5							47.0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	[2]					46.7								48 4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	8/1													
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		18 a							I .					42.6
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	2	20 a	40.6	39.9	39.4	39.0	38.1	38.3	38.6	38.8	39.0	38.8	38.8	37.5
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	2	21	34.6	35.4	35.2	35.0	35.2	35.7	35.8	36.4	36.7	37.5	37.5	36.8
$ \begin{bmatrix} 24 & 38.6 & 38.2 & 38.2 & 38.7 & 39.0 & 39.5 & 39.5 & 40.5 & 40.6 & 41.3 & 41.6 & 42.5 & 25.5 & 26.5 & 2.6 & 2.7 & 32.5 & 33.1 & 33.0 & 33.0 & 33.2 & 33.8 & 34.0 & 33.8 & 34.0 & 33.0 & 33.0 & 33.2 & 33.8 & 34.0 & 33.8 & 34.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 33.0 & 3$		$\frac{22}{2}$												43'0
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$														40 4
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	2	25 в 📗							_	_				_
28 37.9 38.2 38.2 38.7 39.2 39.6 40.0 40.7 41.4 41.9 42.0 42.0 29 45.0 45.0 45.1 45.4 46.7 47.2 48.4 48.9 48.9 49.3 49.3 49.3 48.3 30 49.4 49.9 50.1 50.3 50.5 51.3 51.4 51.4 51.4 51.9 52.1 52.1 31 52.5 52.6 53.0 53.0 53.0 53.0 52.9 52.9 52.8 53.4 53.6 53.6		26 27		33.1										33.0
29 45.0 45.0 45.1 45.4 46.7 47.2 48.4 48.9 48.9 49.3 49.3 49.3 48.3 30 49.4 49.9 50.1 50.3 50.5 51.3 51.4 51.4 51.4 51.9 52.1 52.1 52.1 31 52.5 52.6 53.0 53.0 53.0 52.9 52.9 52.8 53.4 53.6 53.6											41.4			42.0
31 52.2 53.0 53.0 53.0 53.0 53.0 52.9 55.8 53.4 53.6 53.	2	29	45.0	45.0	45'1	45.4	46.7	47.2	48'4	48.9	48.9	49.3	49°3	48.5
														52°2
		اندرت	- U	02 0	000	000			. Uiii U	114 7	•14 O	**** T	1717 17	- UU 4

^a Not included in the Means on account of disturbance.

	One Scale	Division =	*000087 pa	rts of the H		ZONTAL 3 se, in Scale		orresponding	g to 1° decr	ease of Tem	perature, 1° (33.
12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h •	17h.	18h.	19 ^h .	20 ^h .	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div. 645 ° 0	Sc. Div. 649.5	Sc. Div. 654 0	Sc. Div. 651 0	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 648.2	Sc. Div.	Sc. Div. 648 21
624.0	616.9	619.0	614.2	647.0 614.0	645.0	645.9	646°2 610°0	624.0 615.0	644.0 628.0	629.6	631.0	628.78
634.4	636.0	635.0	638.8			621.2	_	639.0	641.0	643.0	645.8	630.20
644.2	633.0	649.0	641.0	637.0	633.0	640.0	637.9	009 0	041 0	045 0	1 - !!	
044 0	000 0	049 0	041 0	643.0	641.0	641.2	645.4	648.2	648.8	651.5	$\{651\cdot1\}$	641.19
648.0	648.5	649.0	649.2	649.4	649.8	649.2	650.2	651.0	652.0	652.7	652.0	646.05
653.0	651.8	640.8	637.1	640.6			634.8	635.0	634.0	630.0	638.0	643.11
637°1	630.0	624.4	618.2	619.0	639.2	632.0 624.0	640.0	635.0	633.0	635.0	626.0	631.63
637.0	639.0	639.2	637.1	634.2	632.2	634.3	629.0	633.0	633.8	631.0	635.8	630.31
615.0	613.0	606.0	605.0	591.0	590.0	608.2	616.4	624.0	635.0	621.8	623.0	617.38
630.0	622.0	624.0	630.0	631.8	633.2	000 0	010 4	024 0	000 0	021 0	020 0	
000 0	022 0	024 0	050 0	051 6	000 2	637.1	637.8	637.8	640.0	641.8	640.4	627.53
642.0	637.8	634.8	632.9	638.1	639.1	638.0	637.0	641.2	643.0	642.8	640.9	635.93
645.0	642.0	641.4	640.2	641.0	643.4	642.8	644.7	643.0	645.0	642.0	646.5	639.28
646.0	646.8	646.0	645.8	646.8	644.0	642.0	649.5	645.2	647.5	650.0	652.0	643.13
663.5	658.7	643.0	654.0	652.0	651.0	644.0	646.8	645.8	639.0	638.8	644.0	650.25
625.0	626.0	635.0	648.8	618.0	619.2	626.0	623.0	622.0	631.0	612.0	620.5	625.83
638.0	638.2	645.0	640.0	633.1	638.1	020 0	020 0	022 0	001 0	012 0	020 2	
_	000 2	010 0	010 0	000 1	000 1	458.0	422.2	518.5	455.7	308.0	110.8}	557°47
660.0	880.0	733.0	695.0	643.0	635.0	634.8	595.0	598.0	605.0	605.0	612.0	553.42
629.2	634.8	635.0	636.0	635.2	634.0	646.0	637.5	638.2	640.0	637.5	636.8	626.44
655.0	642.0	638.0	640.0	636.2	624.5	624.4	633.2	636.1	636.0	642.0	639.0	634.20
648.0	645.0	642.5	645.0	642.8	641.8	643.8	640.0	641.0	642.9	641.0	640.8	639.10
644.2	647.5	646.5	647.0	644.0	644.6	010 0	010 0	011 0	012 3	011		
	01. 0	010 2	041 0	011 0	011 0							647.97
					1 _	662.0	662.0	665.0	664.0	664.5	665.0	0 41 01
662.8	664.0	663.0	661.0	661.0	660.0	659.6	663.0	663.0	663.0	661.0	661.2	657.70
656.1	655.0	655.2	650.0	650.0	647.5	647.0	648.0	649.2	648.0	652.2	654.0	650.21
631.0	630.0	620.7	636.0	638.2	632.8	629.4	631.0	633.3	634.0	636.0	636.5	635.31
631.8	626.8	632.2	630.5	629.0	626.1	627.7	626.8	628.0	627.8	627.4	629.9	627.53
632.7	633.1	633.7	632.0	634.8	633.0	635.0	633.2	632.0	630.7	630.2	631.8	629.74
640.82	638.72									640.10	640.85	636.88
010 00	038 72	637.80	638.38	636.45	635.32	637.55	638.49	638.54	640.90	040 10	040 85	030 90
46°0	0		1 0				BIFILAR MA		1 0	1 0	1 0 1	
	46.3	46.0	46.0	$4\r{6}$ $\cdot 2$	47.0	47.0	46.8	46.7	46.6	46.9	46.8	44°61
48.4	47.5	47.6	48.0	47.8	47.4	47.2	47.2	47.4	47.2	47.0	46.5	47:39
45.0	45.0	44.9	44.7	44.7	44.2	44.2	44.2	44.2	44.2	44.5	44.4	45.35
43.7	43.0	43.0	42.7	42.6	43.0		l . .				<u> </u>	42.97
16:0	-					40.4	40.4	40.4	40.6	41.5	41.6}	
46.0	45.6	45.6	45.8	45.4	45.2	45.2	44.0	43.6	43.5	43.4	43.3	44.11
49.2	48.7	48.5	48.0	47.4	47.0	47.0	46.8	47.0	47.0	47.2	47.0	46.70
50.5	50.5	50.5	50.4	50.5	50.2	50.1	50.6	50.7	51.3	51.5	51.5	49:39
51.1	51.5	51.6	52.0	52.2	52.4	52.7	53.0	53.5	53.5	53.5	53.6	51.61
55.0	54.7	54.5	54.0	53.6	53.4	53.2	53.0	52.6	52.2	52.2	51.6	53.92
51.4	50.2	50.0	49'6	49.5	49.0		<u>-</u>			40:0	$\{-\frac{1}{48\cdot 2}\}$	50.20
49.5	4000					47.5	47.5	47.5	47.8	48.0	48 2 3	
49 5	49.0	48.2	47.8	47.5	47.5	47.2	47.0	46.6	47.5	47.8	47.3	48.45
	47.5	47.9	47.5	47.4	48.0	48.2	47.8	47.6	47.5	47.5	47.0	47.48
48'1 41'5	48.1	47.6	47.2	46.5	45.5	45.0	43.0	42.6	42.4	42.0	42.0	46.43
42.2	41.8	42.0	41.9	41.5	41.5	41.5	41.2	41.0	40'4	40.1	30.0	40.84
42.6	42.5	42.0	41.8	41.6	41'4	41.2	40.8	40.2	38.9	39.4	39.0	40.28
	42.7	43.2	43.5	43.2	43.2				40.0	40:4	40.7	41.03
36.4	05.0					38.2	38.8	39.5	40.2	40.4	40 ()	
36.6	35.6	36.1	36.0	36.4	36.0	36.0	34.9	33.9	33.5	32.9	33.4	37.00
43.0	35.8	36.0	36.0	35.0	34'9	34.0	34.9	36.0	37.0	37.9	38.4	36.02
41.0	42.5	41.5	41.1	41'4	41.8	41.2	41.5	41.5	41.5	42.0	41.8	40.93
42.8	40.6	40.6	40.5	40.8	41.0	40.4	40.1	40'1	40.0	39.4	39.0	40.21
	42.3	41.7	40.7	40.3	40.0		-		_		= }	00.05
_	-		_	<u> </u>	-		20:4			20:0	20.7	38.02
32.7	2010				-	30.0	30.4	31.0	31.6	32.0	32.5	
42.7	32.6	32.7	33.0	33.0	33.0	33.2	33.5	34.5	36.1	37:0	37.6	33.72
49.1	43.0	43.8	43.5	44.4	44.5	44.7	45.2	45.2	45.3	45.7	45.5	42.22
52.8	49.4	49.5	49.6	49.2	48.6	48.7	49.2	49.2	49.2	49'4	49.4	48.27
53.2	52.4	52.5	52.3	52'1	52.2	52.5	52.5	52.6	52.8	52.8	52.7	51.77 53.17
0	53.2	53.0	53.0	53.0	53.2	53.0	53.0	53.4	53.5	53.9	54.2	53.17
46.51	46.00	45.88	45.71	45.55	45.2	44.82	44.75	44.80	44.90	45.11	45.01	45.17

Me	Göttin-)	Ob	1 h	Ch	Oh	4h	5h.	Ch	⊢ Th	Oh	9h.	10h.	11 ^h .
gen T	ime.	Oh.	1 ^h .	2h.	3 ^h .	4 ^h .	ə	6 ^h .	7 ^h •	8h.	9	10".	11",
	$\begin{pmatrix} 1 \\ 2 \end{pmatrix}$	Sc. Div. 632 ° 0	Sc. Div. 633.5	Sc. Div. 633 5	Sc. Div. 634'0	Sc. Div. 629 2	Sc. Div. 625 4	Sc. Div. 622*4	Sc. Div. 621.7	Sc. Div. 617.1	Sc. Div. 619'0	Sc. Div. 623.6	627 C
	3	643.8	645.4	644.0	641.9	637.1	627.4 623.4	$627.0 \\ 622.4$	627.0 619.4	623.0 615.5	626.0 615.7	634.6 628.2	627 633
	4 5	640°0 649°4	636°0 650°4	$637^{\cdot}2$ $650^{\cdot}4$	631.5 644.9	628°0 631°4	624.4	629.6	633.4	634.2	637.4	644.0	645
	6	652.3	653.8	656.0	651.0	641.0	634.0	633.5	637.5	640.2	643.8	648.2	650
	7 8	$\begin{array}{c} 662 \cdot 0 \\ 658 \cdot 2 \end{array}$	660°0 656°4	659°0 657°8	671.2 652.0	656.8 642.1	643.2	634 · 2 635 · 9	635.6 630.8	637.0 628.8	644.8	653.0 649.0	654. 651.
	9 10		670.5	676.0	680.0	650.0	645.0	647.0	650.8	660.5	670.5	677:5	676
	11	674.0	673.8	673.0	667.5	656.5	642.5	650.0	658.5	663.0	670.0	676.0	682
	$\begin{array}{c c} 12 \\ 13 \end{array}$	625°0 640°0	624.5 630.0	$610.5 \\ 619.0$	626.0 573.2	631.5 622.8	620.0	$620.0 \\ 615.0$	632.7	638.0 616.0	613.8	638.0 646.0	649° 622°
RY	13	626.6	621.8	620.0	608.0	605.0	600.0	605.9	609.0	613.0	625.0	606.0	630.
UA	15 16	629.0	630.0	626.0	625.8	613.9	606.0	607.0	613.2	621.2	626.5	628.0	628
JANUARY	17	621.0	623.8	625°0 639°5	624.0 637.0	615.0	610.0	613.0 621.8	616.8 616.0	617.0 628.8	623.5 636.8	631 °0 647 °0	632 645
ث	18 19	640°0 652°5	639.0 652.5	652.0	662.8	641.2	638.0	628.4	636.0	634.5	631.0	645.0	648
	20	643.3	640.0	646.0	642.0	639.0	627.0	628.5	633.2	638.2	642.0	630.0	641
	$\begin{array}{c c}21\\22\end{array}$	642.4 644.0	$642.9 \\ 642.5$	643.6 643.8	640.5 640.0	633.0 640.0	628.5 631.8	625°0 626°0	628.5	627.5 632.0	629°0 640°0	627.5 652.0	623.
	$\frac{23}{24}$	631.0	649.0	630.0	625.0	629.0	625.0	628.0	621.8	626.0	639.2	644.0	639.
	25	640.0	639.0	634.0	624.0	613.2	606.2	608.2	614.0	621.0	627.9	642.5	635
	26	630.0	634.2	632.2	623.9	612.0	611.2	611.0 597.0	620.0	$621.0 \\ 624.0$	625.0	634.0	637
	$\begin{array}{c c} 27 \\ 28 \end{array}$	627.0 635.0	627°0 638°0	630°0 637°4	625°0 624°0	616.0 611.0	600.0	620.0	627.5	637.2	638.0	649.0	638
	29	610.0	606.2	616.0	610.0	614.0	605.0	602.0	610.2	616.0	621.2	625.5	625
	30 31	641.2	640.0	638.9	636.0	627.8	618.8	615.8	620.0	623.9	628.9	632.6	638
Iourl	Means	640.85	640.78	639.65	635.43	629.52	622:34	622.10	625.82	629.01	633.74	640.39	641
	1	5 4 °5	54°5	54.2	темрі 54°6	ERATURE (54°5	54.8	ILAR MAGN	vет. 54°9	54.6	54.6	54.4	54.5
	$\left[egin{array}{c} 1 \\ 2 \end{array} ight]$						-	_	<u> </u>		<u> </u>		_
	3	45.6	45.5	45.4	45.7	46.1 46.4	46.1	46°2 47°0	46.4 46.4	$\frac{46.2}{46.3}$	46.9 46.4	47.4 46.8	47°.
	$\begin{array}{c c} 4 \\ 5 \end{array}$	47.5	47.0	$\frac{46.2}{41.7}$	46.6 41.3	41.3	41.7	42.0	42.2	44.4	45.6	46.2	45.
	6	38.0	37.6	37.3	37.2	37.9	39.0	39.1	39.8	39.8	39.7	39.8	39.
	7	35 · 9 39 · 4	36.0 39.2	36.4 39.5	36.4 39.8	36.6 40.3	37.1 41.0	37.6 41.9	38.0 42.9	37.6 43.2	37°3 43°8	38'1 44'0	37°4 44°2
	$\begin{bmatrix} 8 \\ 9 \end{bmatrix}$		l —						28.0	28.0	28.8	29.2	29
	10 11	$\begin{array}{c} 26.9 \\ 25.2 \end{array}$	26.5 26.5	$\begin{array}{c} 25.0 \\ 26.7 \end{array}$	25°2 26°7	$25.5 \\ 26.7$	26.0 27.5	27.0 28.3	$\frac{26.0}{29.7}$	30.2	31.8	$\frac{32.5}{}$	33
	12	34.3	34.0	34'3	35.0	36.0	37.0	37.5	39.2	40.1	40.6	41.6	41
RY	13	42.4	42.6 47.7	42.6 47.5	43.0 47.6	43°4 47°9	43.7 48.2	43.8 48.5	44°3 48°6	44°2 48°4	44.6 49.0	45.0 49.4	45 49
TYD	14 15	47.6 50.0	50.4	50.1	50.5	49.8	50.2	50.2	51.3	51.6	52.2	$52^{\circ}5$	52
JANUARY.	16 17	43.7	43.5	43.1	43.3	43.3	43.5	43.5	43.8	44.0	41.8	45.4	45
, 5	18	43.0	42.5 35.1	41.5 35.4	41.5 36.2	$\frac{41.5}{37.6}$	$\frac{41.4}{37.8}$	40°5 38°1	40.6 38.7	40°9 38°6	41.7 38.9	41.8 39.5	40° 39°
	19 20	43.0	43.1	42.8	42.7	43.5	44.9	45'1	45.6	46.4	47.5	48.4	48
	$\begin{bmatrix} 21\\21\\22 \end{bmatrix}$	$\frac{46.5}{42.2}$	46.4 42.2	46.4 41.4	46.5 41.2	47.4 41.0	48.4 41.6	49°0 42°0	49.5 41.9	49°5 41°5	49.8 42.5	49.5 44.0	48 '44 '
	$\begin{bmatrix} 22 \\ 23 \\ 24 \end{bmatrix}$	37.2	37.5	38.0	38.2	39.0	40.5	<u></u> 41 · 4	41.8	42.8	44.0	 44`8	44.
	$\begin{vmatrix} 24 \\ 25 \end{vmatrix}$	44.0	44.2	44.2	44.6	45.4	45.8	46.3	46.6	46.9	47.8	48.4	48
	26	49.8	49.4	48.7	48.4	48.0	48.8	49.0	49°2 51°9	48.9 51.9	49.4 52.1	49.4 52.1	49°3
	$\begin{bmatrix} 27 \\ 28 \end{bmatrix}$	50°5 48°8	50.0 48.2	50°0 48°2	49°9 48°3	50°0 48°8	50°6 49°7	51.4 49.5	20.0	49.5	49.5	49.5	49
	29	46.0	46.0	45.8	46.0	46.4	47.0	47.0	47.4	47.4	47.3	47.8	47
					. — \								
	$\begin{bmatrix} 30 \\ 31 \end{bmatrix}$	43.7	44.0	44.0	44.6	44.6	45.1	45.2	45.6	45.8	47.1	48.1	48

	ne So	cale I	Division =	·000087 pai	rts of the H		IZONTAL se, in Scale		orresponding	r to 1° decre	ease of Tem	perature, 1	5 3.
637 630 630 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631 631	13h	•	14 ^h •	15h.	16 ^h .	17 ^h .	18 ^h .	19 ^h •	20h.	21h.	22h.	23h.	Daily ar Monthl Means.
634**0 622**0 613**2 621**0 611**0 610**0 622**0 613**1 610**0 613**9 612**2 641**6 634**4 636**4 636**4 636**4 636**4 636**4 636**4 636**4 636**6 631**2 641**0 641**2 641**3 643**5 642**5 641**5 630**6 649**1 644**4 644**4 644**4 644**4 636**5 641**5 630**6 649**1 644**1 644**3 644**6 644**4 644**6 644**6 636**6 649**1 644**1 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 644**6 64							Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$5\mathring{3}$	8	$5\ddot{3}$ $\cdot 4$	53°4	53.3	53.3						46.2}	52.1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$. [<u> </u>								i
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	47	7	47.5	47.5	47.6	48.0	48.0	48.0	48.4				47.1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			44.5	43.8	43.5	43.0	42.3	42.0	41.8				44.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					40.7	40.2	40.2	40.0	40.0	39.7			42.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					36.7	36.2	36.4	36.0	35.0	34.4	35.4		37.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										39.0	39.0	39.2	37:39
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					L								38.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			11 0		Į.		28.6	28.3	27.8	28.0	28.0	27.7 }	J 35 8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			90.0			28.6							27.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$											_		31.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$													38.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$													45.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								l .	1				49.1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							1	ł	50.6				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	51	9	51.6	51.4	51.0	50.2						1 (2:0)	49.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				44.2	44.0	43.9		43.2	42.2				43.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$													39.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												42.5	38.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$											47.6	47.0	46.4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					1							42.7	46.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							1						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	±0 (0		40 U	72 0				35.7			36.6	40.89
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				40:4	4014							43.7	42.1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$													47.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							i				- (50.5	49.86
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													50.77
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			l,										
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							47.2	46.8	46.5	46.3	1	- 41	48.44
- $ $ $ $ $ $ $ $ $ $ 41.3 $ $ 41.6 $ $ 41.6 $ $ 42.3 $ $ 42.5			47.0	46.6	46.2	46.0						}	45.54
		.		_								42°5 } 43°1	45.12
												41.96	43.3

	On	e Scale Divi	sion = '000	0087 parts o	f the H. F.		NTAL FO		sponding to	1º decrease	of Temperat	tu re, 1 °63.	
Mean (gen T	Göttin-}	O ^h .	1 ^h .	2 ^h .	3 հ.	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8 ^h •	9 ^h .	10 ^h .	11h.
	1 2 3 4 5	sc. Div. 646 ' 9 657 ' 8 650 ' 0 648 ' 2 648 ' 1	sc. Div. 647 ' 3 646 ' 1 650 ' 0 646 ' 0 647 ' 4	sc. Div. 646.5 650.4 650.8 645.5 646.0	Sc. Div. 640 ° 0 650 ° 0 641 ° 5 639 ° 5 643 ° 4	sc. Div. 636.0 636.4 631.5 631.5	Sc. Div. 628 * 5 628 * 8 622 * 0 622 * 4 a 630 * 2	Sc. Div. 624 2 622 0 623 0 621 0 631 9	Sc. Div. 624°0 628°0 626°0 619°8 635°0	sc. Div. 631 ° 0 639 ° 0 628 ° 0 626 ° 8 637 ° 8	Sc. Div. 633 ° 0 643 ° 5 634 ° 0 634 ° 2 638 ° 6	Sc. Div. 638 0 648 5 640 0 638 8 643 0	Sc. Div 641 ° 0 648 ° 5 641 ° 0 643 ° 2 645 ° 0
ŁY.	6 7 8 9 10 11 12 13	656°0 644°2 645°0 647°0 660°0 661°0	652.2 641.0 641.2 648.1 653.5 661.5	649.2 635.5 640.4 648.0 661.0 658.2	643 · 2 641 · 5 634 · 0 648 · 0 663 · 8 657 · 4	635.0 629.0 621.5 636.0 665.0 659.0	632.0 613.0 605.0 634.0 645.4 648.0	637.0 598.0 623.0 627.0 641.8 640.0	643.0 633.5 623.0 613.0 642.1 636.0	639 · 2 643 · 0 652 · 5 629 · 2 650 · 0 638 · 8	638 · 8 642 · 8 625 · 0 638 · 2 654 · 0 643 · 0	650.0 647.5 643.0 641.8 655.1 646.2	659 ° 0 652 ° 0 632 ° 4 645 ° 0 656 ° 2 655 ° 0
FEBRUARY	14 15 16 17 18 19	660 · 2 650 · 0 647 · 3 646 · 0 648 · 2 643 · 0	661.0 648.2 646.0 647.0 646.8 641.2	658 · 1 636 · 0 646 · 2 646 · 0 641 · 2 636 · 0	652°0 646°0 641°0 639°0 638°0 625°0	646.0 642.5 631.0 636.0 626.0 628.5	648 ° 0 638 ° 0 624 ° 0 628 ° 2 620 ° 0 635 ° 0	649.0 628.0 626.0 627.8 622.0 635.0	655.0 628.0 630.6 629.0 628.0 639.0	658°0 640°0 635°4 638°0 638°0 641°0	653.0 642.0 634.0 642.0 638.5 638.6	652°0 638°0 636°9 643°5 642°0 639°0	641.0 640.0 645.0 645.0 637.0
	20 21 22 23 24 25 26	584°0 597°5 616°0 565°8 636°8 645°5	320°0 595°0 618°0 553°6 588°0 647°0	506.0 586.0 613.0 545.2 621.6 643.0	638 · 8 591 · 5 615 · 0 578 · 0 639 · 0 639 · 5	616.5 592.5 610.5 601.7 612.4 630.0	588°5 588°2 601°2 600°5 613°0 624°0	618.5 601.5 572.5 610.6 617.5 611.3	617.0 595.0 614.0 612.0 614.0	569°3 570°0 624°2 612°0 624°0 618°0	608'3 642'0 613'0 623'0 623'5 623'0	729 · 5 609 · 8 624 · 0 626 · 0 634 · 0 627 · 5	736'9 613'0 614'0 619'0 631'0
	27 28 2 9	653°0 645°0	642°0 645°0	648.0 643.0	640°0 638°8	630.2 636.0	621.8 628.2	616°4 620°6	628·2 622·8	598°0 625°2	621.8 628.2	635°0	635 .2 640.0
Hourly	Means	644*39	639.92	639.21	638.85	632*43	625.70	622.85	627.74	633.35	635.03	640.25	640.8
					TEMP	ERATURE (F THE BIF	ILAR MAGI	NET.				
	1 2 3 4 5	43.2 41.8 46.3 44.8 46.0	42 7 41 8 46 0 44 5 46 2	42·1 41·4 45·5 44·7 46·0	41.6 41.8 46.3 45.0 45.4	41.7 42.7 47.2 46.4 46.2	42.0 43.5 47.8 47.3 46.8	42.4 44.0 48.3 47.6 46.8	42.4 44.7 49.0 48.0 46.0	43°0 45°0 49°2 48°0 45°5	43.6 47.0 50.1 48.4 45.5	44.2 48.1 51.1 48.4 45.2	44.0 48.5 51.3 48.6 43.9
•	6 7 8 9 10 11 12	39.0 39.4 41.5 40.5 32.0 36.1	38.4 39.0 41.4 40.5 31.5 36.0	37.8 38.4 41.6 40.0 32.0 35.2	37.0 37.6 42.5 39.4 33.0 34.9	37.0 38.0 42.5 39.4 33.9 35.9	37.4 39.0 42.3 39.4 34.4 37.0	37.8 40.1 41.8 39.4 34.4 37.2	38.4 41.3 42.5 39.4 34.9 38.5	39.2 41.5 43.0 39.6 35.7 39.7	40.5 42.6 43.0 39.8 35.9 41.0	41.0 43.0 44.0 40.3 38.4 41.8	42.7 43.2 43.5 39.8 38.8 42.6
FEBRUARY.	13 14 15 16 17 18 19	38.7 43.0 42.8 44.0 45.6 46.0	38.5 42.4 42.5 43.4 45.6 45.5	38.9 42.0 42.9 44.0 45.6 45.1	40°2 42°3 44°5 45°0 46°5 45°2	41 · 4 42 · 7 46 · 0 46 · 0 47 · 0 46 · 0	42.2 42.8 47.0 47.0 48.0 46.8	42.8 43.0 47.5 47.6 48.5 48.0	43.7 43.7 48.4 47.6 49.8 48.6	44.6 44.7 48.6 48.4 50.4 48.8	45°3 46°0 49°2 49°5 50°7 48°7	45.5 47.5 49.9 50.3 51.0 50.3	45.4 48.0 49.6 50.9 51.3 50.0
	20 21 22 23 24 25 26 27	45.2 49.8 49.4 45.2 42.0 43.3	45.2 49.8 49.0 44.3 40.4 42.7	45.2 49.2 49.3 44.0 40.7 43.5	46.3 49.0 49.2 44.0 41.0 45.2	46.9 49.0 49.6 43.7 42.0 46.1	47.9 49.5 49.6 44.2 42.9 46.1	48·2 49·9 49·2 44·5 43·3 45·9	47.5 50.2 48.7 45.3 43.6 46.0	49.5 50.4 48.5 46.0 43.4 46.3	51.0 50.5 49.0 46.4 43.8 46.7	51.5 50.8 49.0 46.4 45.0 47.6	52.4 50.5 49.0 46.6 45.2 47.4
	27 28 29	42.8 44.5	42.0 44.4	41.8	41.2 44.4	42°3 45°0	43°1 45°4	44°5 45°4	45°1 45°3	45.8 44.9	46°3 44°9	46°8 44°5	46°5 44°2
		42.52	42.12	42.02	42.33	42.99	43.57	43.91	44.39	44.77	45.39	46.06	46.1

^a Three minutes late.

	One Scale	Division =	·000087 pa	rts of the H		SIZONTAL se, in Scale		orresponding	to 1° decre	ase of Temp	perature, 1.6	3.
12h.	13h.	14h.	15 ^h .	16h.	17 ^h .	18h.	19h.	20h.	21h.	22h.	23h.	Daily ar Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
	i	1	1	ĺ	i .	C47.0	615.5	010.0	í		1 :	
$646^{\circ}2$	647.0	647.4	646.5	648.0	646.0	647.0	645.5	646.8	648.4	646.8	651.0	641.79
644.0	642.0	641.3	642.8	644.5	645.0	647.2	646.0	647.0	645.6	648.0	647'4	643.31
641.4	641.2	642.4	629.3	624.0	630.0	635.1	632.0	640.2	644.8	645.0	649.0	637.18
642.9	642.8	642.8	643.0	642.0	641.8	643.4	646.7	647.7	650.0	647.5	649.0	639.8
648.0	647.0	647.2	650.0	650.9	651.2			_			1 1	ľ
040 0	011 0	011 2	000 0	000 5	001 2	623.0	610.0	638.0	628.0	638.0	$\{653\cdot 2\}$	640.20
		245.0		20010	20015	_	_				000 27	0.00.0
629.0	645.2	645.0	634.0	638.0	638.2	636.0	641.2	642.8	643.2	644.8	641.4	642.25
642.0	640.8	631.2	642.0	631.2	627.8	626.0	632.0	640.2	629.0	628'1	630.5	634*24
633.8	637.8	633.8	637.7	640.0	642.0	640.0	641.4	648.0	645.8	647.0	648'0	636.72
647.0	643.8	644.2	652.0	653.0	653.0	658.0	657.0	656.7	657.7	658.5	658.5	645.61
660.0	661.0	661.8	663.0	663.0	660.0	663.0	662.0	662.0	662.0	662.0	662.2	657:91
				658.0	657.0	000	00.	002	002 0	002 0	002 -	
$652 \cdot 2$	653.0	654.0	653.0	000 0	001 0	055:0	650:0	000:0	CCLLA	00010	0000	653.65
				00 = : =	00115	655.0	659.8	660.0	661'4	660.0	660.0}	
643.0	652.0	648.2	646.8	635.2	634.8	630.0	627.7	619.0	641.0	642.0	640.8	645.58
640.2	644.0	642.2	640.8	640.6	637.0	638.9	638.7	638.0	638.2	641.0	645.5	640.12
641.0	644.5	644'1	643.3	643.0	638.5	639.0	645.0	647.3	646.2	646'3	647.1	640.14
			643.0	643.5	644.0	647.1	643.1	644.0	645.0	647.0	648.4	641.69
642.0	642.2	643.8										
$645^{\circ}6$	646.8	647.5	649.0	645.0	646.5	640.0	638.8	635.2	642.8	638.0	648.0	639.8
639.0	645.0	636.2	636.0	633.8	636.6					_	- 7	626.79
					1 —	610.0	617.1	563.0	600.0	594'1	593.9	
577.2	594.0	667.5	573.6	631.4	610.2	638.2	617.0	590.0	586.2	589.0	570.0	599.07
			609.1	607.8	641.0	620.2	525.1	594.0	585.0	602.5	606.0	599.36
605.0	605.0	602.0					599.0	543.0			530.5	607.06
622.0	618.0	641.0	617.5	623.5	628.5	630.0			585.0	596.0	! !!	
621.0	622.0	616.0	627.5	623.0	614'0	612.0	540.5	501.2	536.4	480.7	640.7	590.93
619.0	632.0	636 ·2	626.2	631.4	634.2	636.3	633.1	635.0	636.0	637.5	640.0	627.15
636.2	638.8	633.4	645.1	626.0	636.7						1 - 1	
	0000	000 1				642.0	640.9	647.0	645.4	645.0	650.8	635.12
623.0	625:0	620.0	640.0	637.0	639.0	641.0	640.5	640.0	638.6	641.2	648.0	635.10
633.0	635.2	638.9	640.0									
641.4	646.8	644.8	644.0	645.5	647.0	643.0	645.0	645.0	646.0	649.0	651.2	639.90
639.56	642.13	641 • 90	641.41	639.99	640.40	638.39	634.04	629.87	635.20	634.07	640.64	636.62
				TE	MPERATUR	E OF THE	BIFILAR MA	AGNET.	<u> </u>	<u> </u>		
0	0	0	0					0	0	0	0	0
	l i				ł	12.7	43.6	43.4	43.3	43.0	42.0	43.15
44.0	43.7	43.6	43.9	43.9	43.9	43.7						
48.2	47.5	47.5	47.5	47.0	46.4	46.3	46'2	46.3	46.3	46.3	46.4	45.5
51.4	50.5	49.7	49.0	47.5	47.4	45.7	45.9	45.5	45.4	45.2	44.9	47.76
49.0	48.7	48.4	48.2	47.4	47.0	46.8	46.3	46'1	46.0	46.0	46.0	46.9
43.7	42.9	42.6	42.5	42.0	41.8							
	729			120	j.	37.0	37.2	37.5	37.7	38.0	38.8}	42.9
40:5	12:5	40.5	40:0	41.0	41:0					40.2	40.2	40.0
42.7	42.5	42.2	42.0	41.6	41.0	41.0	40.6	40.4	40.2			
43.5	43.3	43.4	43.6	43.8	43.5	43.2	43.1	43.0	43.0	42.5	42.3	41.7
43.7	43.6	43.6	43.6	43.4	43.4	43.0	42.7	42.6	42.4	42.7	42.0	42.70
39.5	38.7	37.8	37.0	37.0	36.0	35.1	34.9	3 3.5	32.2	32.8	32.5	37.70
38.2	38.2	37.4	37.0	36.9	36.5	36.2	36.0	36.0	35.7	3 5 ·7	36.0	35.6
42.5						1	1	1	30 1	JU 1	J i	
	42.6	42.5	42.0	41.6	41.2	20:0	20:4	20:0	2010	97.0	38.8	38.80
						36.0	36.4	36.6	36.9	37.8		40.0
46.0	46.0	46.1	46.0	45.8	45.6	45.6	45.5	45.1	44.2	44.0	43.7	43.8
48.0	47.6	46.6	46.0	45.4	44.7	44.2	44.0	44.0	43.8	43.6	43.0	44.5
49.0	48.6	47.8	46.8	46.6	45.5	45.2	45.0	44.7	44.2	43.8	44.0	46.2
20.6	50.8	50.4	49.5	49.5	49.1	48.2	47.4	46.5	46.3	46.0	46.0	47.6
						li .				47.1	46.6	48.5
51.0	50.3	50.3	49.8	49.5	49.0	48.5	48.2	47.6	47.4		l .	
5 0.1	20.0	49.9	49.5	48.8	48.6			440.5	44.7	44.6	44:4}	47.2
	_				_	44.5	44.5	44.5	44.7	44.6	44.4 }	l
52.2	52.4	52.4	52.0	51.8	51.7	51.2	51.4	51.1	50.9	50.0	49.7	49.7
5 0.0	50.0	49.6	49.2	48.8	49.0	48.8	48.3	48.6	48.6	48.8	49.0	49.4
49.0	48.0	47.6	47.7	47.0	46.8	46.6	46.3	46.0	46.2	46.0	45.6	48.0
46.2	45.0					44.3	44.2	44.5	44.0	44.0	43'1	44.7
	45.3	45.0	44.5	44.0	44.0							44.0
45.0	45.5	46.6	46.6	46.3	45 .2	45.7	45.7	45'6	44.2	43.8	43.5	
47.0	46.7	46.4	45.9	45.4	44.8		_				43.0}	45.03
	l —	_]	43.0	42.8	42.9	42.7	43.2		
46.5	46.2	46.5	46.4	46.4	46.5	46.5	46.1	45.1	44.5	44.5	44.5	44.9
	43.4	43.1	42.2	42.2	42.6	42.8	42.2	42.5	42.5	42.2	42.5	43.75
44.0					1	1	1	,	1	1	1 11	,

Mean Göttir gen Time.	1-} Oh.	1 ^h .	$2^{\mathrm{h}}.$	3h.	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8h.	9 ^h .	10h.	11h.
$\begin{pmatrix} 1\\2\\3\\4 \end{pmatrix}$	655.0	Sc. Div. 649°2 647°0 655°4 656°0	Sc. Div. 644 ° 0 643 ° 1 647 ° 0 652 ° 0	sc. Div. 634 °0 639 °0 640 °0 648 °0	Sc. Div. 637 5 635 0 633 0 638 8	sc. Div. 633 ° 0 627 ° 2 625 ° 5 630 ° 2	Sc. Div. 631 1 626 0 625 8 628 0	Sc. Div. 634 ° 0 632 ° 2 631 ° 6 630 ° 5	Sc. Div. 637.8 637.5 640.0 640.0	sc. Div. 638'0 641'0 647'0 647'0	Sc. Div. 640 0 646 0 650 5 648 8	Sc. Div 641'0 650'0 651'2 650'0
5 6 7 8 9 10	648.5 639.8 638.0	658.0 644.8 632.4 635.0 644.0 652.0	654.0 639.2 637.8 631.0 644.0 647.5	646.5 635.6 629.0 625.0 640.0 639.2	634'8 629'0 616'0 621'0 632'0 630'8	632.8 624.8 597.2 615.0 623.0 621.2	635.0 623.9 608.5 614.4 618.0 616.4	640°5 635°0 620°0 617°8 620°2 619°4	661 · 3 637 · 6 626 · 0 625 · 0 628 · 2 623 · 8	651.7 641.0 621.0 632.0 635.5 634.4	643°8 638°0 636°0 637°0 639°2 641°8	651.0 643.8 627.5 640.2 643.0 644.2
MARCH. 12 13 14 15 16 17 18	648.8 657.0 658.0 672.0 607.0 633.3	649°2 651°8 655°0 667°0 617°0 631°2	641.4 655.1 643.0 660.5 607.0 634.0	634.0 651.4 621.0 645.0 596.8 632.9	629.0 648.0 643.5 636.5 587.5 629.6	626'8 646'4 642'3 637'5 607'8 624'4	623 · 4 645 · 0 634 · 0 629 · 5 626 · 4 624 · 8	632.0 648.0 652.5 642.0 629.3 633.0	640.0 645.0 658.0 635.5 653.0 632.2	641.5 650.8 655.0 642.2 657.1 643.0	646.5 644.2 651.7 652.2 648.4 627.0	648°0 649°0 640°2 656°6 648°0 636°5
19 20 21 22 23 24 25	589.0 616.0 632.5 635.5 622.4 633.7	580°2 612°0 633°0 631°4 629°8 632°0	553°0 614°0 630°5 626°8 639°4 603°0	561.0 611.4 622.0 623.0 633.5 597.0	576.0 602.0 614.0 613.0 626.0 596.0	558'8 602'0 609'0 610'0 616'1 618'0	592.0 603.0 602.0 609.6 608.1 608.5	625.0 613.0 605.8 612.6 613.0 618.0	663.0 608.5 619.8 619.0 617.8 616.0	696.0 618.0 628.2 615.8 619.0	664.6 619.0 633.0 629.2 641.0 622.0	657 0 617 4 638 8 633 0 633 5 628 5
$\begin{bmatrix} 26 \\ 27 \\ 28 \\ 29 \\ 30 \\ 31 \end{bmatrix}$	640.6 642.0 637.2 635.4	641.0 639.0 632.0 634.2 611.3	625°0 .635°8 627°2 633°8 605°0	615.0 629.0 619.4 627.9 614.7	608.5 623.0 613.8 617.1 610.0	608.8 613.5 609.2 610.7 593.0	612.6 613.5 613.4 612.0 593.5	608.5 623.8 615.9 620.0 612.0	620°8 638°0 623°1 628°8 618°0	631 '9 626 '0 628 '9 644 '0 624 '0	626°0 637°4 634°1 645°0 643°8	640°2 637°6 632°4 635°0 632°0
ourly Mca	ms 639.66	637:81	632.37	626.34	621.53	617:19	617.72	625.39	633.10	638.10	640.23	640.9
	42.2	1 .9	i .º		RATURE ()			ет. 45°7	45.9	45°6	45.8	45°7
$\begin{pmatrix} 1\\2\\3\\4\\ 2 \end{pmatrix}$	41.0 39.8 40.5	41.4 40.0 39.8 40.0	42°2 39°0 39°2 40°3	42.7 38.5 39.0 42.0	43°3 38°9 39°7 44°7	44.3 39.6 41.3 44.5	45°3 40°2 42°2 44°9	45 7 41 7 43 0 44 8	41.7 44.0 44.0	45 6 42 3 45 0 43 6	45.0 43.0	41 '9 45 '3 42 '0
56 77 88 99 100	38.4 44.4 48.6 46.3 42.0	38.5 44.2 48.2 45.7 41.5 44.0	39.0 44.2 48.6 45.5 41.5 45.5	39.7 44.4 48.6 45.3 42.4 46.8	40.4 44.6 49.0 45.7 44.0 47.4	41 · 2 45 · 0 50 · 0 46 · 3 45 · 0 48 · 3	41.6 46.0 51.0 46.9 45.7 48.4	42·2 46·7 51·7 47·2 45·8 48·4	43.2 48.1 51.9 48.4 47.0 48.8	44.6 49.4 52.5 49.4 48.2 49.3	46.0 49.8 53.2 50.0 49.2 50.0	46°2 50°0 52°5 49°4 49°2 49°4
MARCH. 13 14 15 16 17 18	45.2 40.8 34.0 34.5 41.0 41.4	44.2 40.1 34.0 34.7 41.5 41.5	43.6 40.1 34.4 35.7 41.6 41.6	43.6 40.8 35.2 36.4 41.6 43.7	43.6 40.8 35.6 37.0 41.5 45.0	44·1 41·0 35·8 38·0 42·4 46·3	44.1 41.0 36.0 39.0 42.8 46.6	43.8 41.5 36.4 39.4 43.1 47.0	44.0 41.6 37.2 40.2 43.7 47.4	44.3 41.7 38.1 40.6 44.1 47.4	44.6 41.9 38.7 41.6 44.6 47.5	44.7 41.9 39.2 41.7 45.5 47.5
19 20 21 22 23 24 25	44.8 49.2 48.8 53.6 47.6 51.0	44.4 49.0 48.8 52.8 48.4 50.8	44.4 50.0 49.2 52.0 49.3 50.1	44.0 51.6 49.5 51.5 50.0 51.0	44.5 52.5 49.8 52.1 50.5 51.0	45.7 53.2 50.5 52.7 51.2 51.3	46.0 53.5 51.0 52.9 51.5 51.4	46°3 54°1 51°2 53°0 52°0 51°9	46°2 54°5 51°3 52°5 52°5 52°0	47°3 55°5 51°4 52°6 53°4 52°8	47°3 56°3 51°6 53°6 55°0 53°3	47.2 56.6 51.9 53.8 54.0 53.3
26 27 28 29	$\begin{array}{c c} 47.2 \\ 47.2 \end{array}$	47.0 47.5 52.8 52.6	47.0 48.0 53.8 53.0	47'3 48'5 54'8 54'0	47.9 49.9 55.2 54.5	49.0 51.0 55.6 54.7	50°3 51°9 55°6 54°7	51'3 52'1 55'6 55'0	51.6 52.4 56.6 55.0	52.2 53.0 57.6 55.4	52°5 53°8 58°8 58°4	52°2 54°4 60°0 55°5

	One Scale	Division =	.000087 pa	erts of the H		IZONTAL		orresponding	o to 1° decr	ease of Tem	perature, 1·	63.
12 ^h .	13h.	14 ^h .	15h.	16h.	17 ^b .	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div. 644'0 651'0	Sc. Div. 643 5 654 0	Sc. Div. 645.6 652.0	Sc. Div. 648 0 652 0	Sc. Div. 646 8 653 0	Sc. Div. 645 0 653 8	Sc. Div. 646 0 654 0	Sc. Div. 647.4 655.0	se. Div. 647.8	Sc. Div. 648 0 654 6	Sc. Div.	8c, Div. 648*2 655*8	Sc. Div. 642 65 646 67
650°4 652°3	642.0	649.0 656.8	648.8	651.8 657.0	652.9 657.2	659.0	658.0	657.3	663.0 626.0	655.0	$\left \frac{654.0}{660.6} \right\}$	646.84
647.0 637.6	646.0 643.0	646°2 646°0	641.0	642.0 644.2	642·4 642·0	645.2 641.0	640.5 638.4	644.0	645°0 638°0	645.0	647.2	645°80 638°55
634.0	642.0	626.0	630.0	627.8	628.8	623.2	634.1	634.6	633.7	636.1	635.8	628.22
641.8 644.7 646.0	638'4 645'8 645'0	640.0 647.3 645.0	641.2 647.8 646.5	643.0 647.0 645.5	643.0 649.0 646.0	645°0 648°4	645°4 651°0	646°0 652°0	645.8	646°2 651°2	648.0	635.63 641.76
650.6	651.0	652.0	653.0	651.5	652.0	650°0 655°0	647.8 655.0	651.5 657.4	651.0 659.5	650°0 657°2	648.0 }	641.46 646.37
658.8	654.0	659.0	669.6	665.0	659.5	624.8	618.7	635.0	653*2	654*1	655.0	649.93
645 ° 0 655 ° 4	$\begin{array}{c} 653.0 \\ 658.2 \end{array}$	651.8 647.2	$653.8 \\ 642.8$	651°2 643°4	$650.2 \\ 610.0$	654°0 606°4	643°8 611°0	659 . 0	657:4 626:5	657°0 610°4	675°0 590°0	636°93
$650.2 \\ 644.0$	643.4 620.8	630.0 631.0	636.2 631.0	630.0 632.0	635.0 632.0	635.0	636.2	636.8	638.0	639.0	637.8	630.80
640.0	617.0	617.0	620.5	594.0	598.2	619 . 8 588.4	551.6 570.0	580.7 583.6	588.6 593.0	623·2 624·0	$\begin{bmatrix} 583.5 \\ 622.2 \end{bmatrix}$	621.55 607.63
608.8	616.4	620.8	622.8	623.5	623.7	625.5	626.2	630.0	631.8	631.0	631.0	617.82
625°0 629°0	622.4 634.0	617.0 628.5	621.8 624.5	628°0 632°0	625 ° 0 634 ° 0	633 ° 6 63 4° 8	630.3	632 * 0	630 ' 8	633 ° 0	633°0 641°2	625.11 626.55
633.0 614.0	630.0	626.5 622.5	625°0 616°8	620°0 622°2	587.5 621.0	611.0	630.2	631.2	629.5	629.4	620.9	623.91
622.4	633.5	637.4	636.5			619°8 634°0	637°3 632°8	623 *9 630 *0	623°1 642°5	636*1 640*0	$\begin{bmatrix} - \\ 634.8 \\ 643.5 \end{bmatrix}$	620°11 629°66
638.3	633.5	637.1	626.5	637°1 628°0	643 . 8 632 . 0	630.8	633.0	639.5	635*4	640.5	638.0	632.13
630.0	630°0 626°0	633.0 622.0	625.0 628.5	629°8 633°0	630.0	631.7 632.8	634.0 618.8	634.0 634.0	633°0 617°5	635°0 604°8	631.5	$627.66 \\ 625.26$
614.2	626.0	622.0	600.0	602.3	605.5	611.0	612.0	622.0	612.1	624.5	620.5	614.45
638.62	637.97	637.36	636.63	636*46	634.42	633.84	631.28	634.60	636.67	638.26	637.27	633.20
45.4	41.7						BIFILAR N			. 0	1 9 1	.0
43.4	$\frac{41.7}{42.4}$	$\begin{array}{c c} 44.5 \\ 42.0 \end{array}$	44.3 41.6	44.0 41.2	44°0 41°0	$4\overset{\circ}{4}.0$	43°2 40°0	43°3 39°6	43°3 40°0	40.0	42°5 39°8	44.06 40.70
44'6 41'2	43°2 40°4	42.6 40.1	42°1 40°0	41.6 39.8	41.2 39.5	40.8	40.4	41.0	41.2	41.4	41.0	41.85
46.5	45.2	44.4	44.0	44.0	44.0	33.2 43.9	33.9 43.5	34.6 43.8	36.5 43.5	36.7 44.4	37.6 } 44.6	40°34 43°02
49.8 52.0	49.5	49.0	49.0	49.0	49.0	49.2	49.2	49.0	48.8	48.9	48.7	47.75
48.6	51.5 47.6	51.1 46.6	51.0 46.2	50.4 46.0	50°0 45°5	49°5 45°1	49.5 44.9	48.7 44.8	47.6 44.8	47°1 44°0	46.6 43.0	50°03 46°38
49°1	47.5 48.5	46.5 48.2	45.2 47.5	44.7 47.5	43.6 47.4	43.0	44.0	44.2	44.6	44.6	44.2	45.14
44.7	44.0	43.6	43.4	42.7	42.0	$\begin{array}{c} 45.5 \\ 42.0 \end{array}$	$\begin{array}{c} 45.4 \\ 42.2 \end{array}$	45°4 42°1	45.4 41.6	45.4 41.3	45.2 }	47°13 43°36
40.5	39.0	38.0	36.8	36.2	36.3	36.6	37.0	36.2	35.2	34.7	34.2	38.94
39.4 40.5	38.4 39.5	37.6 39.2	36.5 39.0	35.6 39.0	34.6 38.8	34.6 38.7	34·3 39·3	34·2 39·5	34°1 40°5	34.4 41.7	34°1 41°5	$39.00 \\ 32.93$
45.6 48.0	44.6 47.9	44.4	43.4	43.4 48.2	43·4 48·0	42.7	42.0	41.5	42.0	42.0	41.9	42.93
48.5	48.4					45.0	44.8	45.0	45.1	45'1	$\frac{-}{45\cdot 1}$ }	45°90 47°22
56.4	55.4	48.6 54.4	48.6 53.2	48.6 52.5	48.8 52.0	49°0 51°5	49°1 51°0	49.0 50.3	49.0 50.0	49.0 50.0	49.3	52.28
51.6 54.0	51.1 53.4	50.6 52.9	50.5 52.1	50.5 51.6	50.6 51.3	50.7 51.0	51.5 50.4	52.4 50.0	52 . 9 49 . 5	53°1 49°1	53°5 48°8	51.00 51.97
54°3 53°5	53.6 53.5	53.2 53.5	52.5 53.6	52.5	53.0	53.0	52.2	52.0	51.2	51.2	51.2	51.92
52.3		_	_	53.6	53.2	48.7	48.5	48.0	48.2	48.0	47:7	51.26
54.4	51°5 53°8	50.6	50°3 52°8	50.0 52.5	49.6 52.4	49°2 52°2	48.8 51.8	48.4 51.7	48'0 51'9	47.7 52.0	48.0 52.3	49.58 51.70
60°4 55°7	59.6 54.8	58.6 54.5	56.8 54.4	56.0 54.4	55°2 53°9	54.8 53.5	54.4 53.4	54.4 53.2	54°0 53°0	53.1 53.1	52.6 53.0	55.77 54.12
58.2	58.4	28.0	57.6	57.6	57.2	56.3	55·3	54.0	53.2	53.3	23.0	55.20
49.11	48.42	47.94	47.43	47.15	46.88	46.07	45.94	45.81	45.78	45.83	45.26	46.86

	Oı	ne Scale Div	rision = '00	00087 parts	of the H. F.	HORIZO Increase,	NTAL FO in Scale Div	RCE.	sponding to	1º decrease	of Tempera	ture, 1.63.	
Mean Göt gen Tim	ttin- }	Oh.	1h.	2 ^հ .	3h.	4 ^h •	5 ^h .	6 ^h •	7 ^h .	8 ^h •	9 ^h .	10h.	11h.
	1	Sc. Div. 630.0	Sc. Div. 620 ° 0	Sc. Div. 619 0	Sc. Div. 614.5	Sc. Div. 613.0	Sc. Div. 612*0	Sc. Div. 617.5	Sc. Div. 623 8	Sc. Div. 629*8	Sc. Div.	Sc. Div. 635 2	Sc. Div. 635 2
	2 3 4 5 6 7 8	605°0 623°0 631°8 624°3 598°0 621°0	618.0 614.0 625.0 627.2 575.0 619.0	611.0 617.5 623.2 610.0 568.0 618.0	588.5 610.2 616.9 600.5 562.0 611.0	594.0 597.8 608.2 601.0 581.5 607.0	592.0 593.5 601.6 598.0 585.6 607.0	602.5 603.2 598.9 594.0 579.5 607.8	621 '4 606 '8 601 '8 595 '0 575 '0 606 '8	620°8 618°8 615°0 613°0 606°0 610°4	632°8 626°6 635°0 620°0 624°5 621°8	665 ' 4 626 ' 4 625 ' 0 628 ' 5 640 ' 0 619 ' 8	634.0 628.0 640.0 633.0 631.2 620.0
3IL.	9 10 11 12 13 14 15	628.0 625.8 627.6 631.0 643.0 645.2	630°5 620°0 631°2 630°8 642°0 639°3	627 ° 0 621 ° 2 622 ° 4 627 ° 0 635 ° 2 624 ° 0	618.0 617.0 623.2 618.0 627.9 626.5	608.4 612.5 619.0 615.8 621.0 617.2	598.2 604.5 624.0 615.6 619.0 613.8	596°2 610°0 623°3 615°0 620°2 618°4	601 ° 0 608 ° 0 627 ° 0 618 ° 0 623 ° 0 621 ° 0	605 · 0 620 · 0 621 · 8 624 · 0 626 · 8 637 · 8	610.6 624.5 626.0 634.0 633.8 640.2	617·3 625·5 625·0 636·7 638·8 637·0	621.0 623.0 624.8 638.2 639.2 639.0
	16 17 18 19 20	625 · 4 630 · 0 636 · 0 643 · 0	628.0 627.5 640.0 641.5	626.6 619.2 635.0 638.2	630.0 610.0 630.0	613.4 609.0 624.0 623.5	610.6 612.0 621.3 618.0	618.4 622.0 626.8 624.0	621 ° 0 627 ° 0 630 ° 0 622 ° 0	624.0 633.0 641.0 628.0	638.5 635.2 641.0 634.0	640.0 628.0 642.4 639.2	652.0 635.0 645.0 633.8
2	21 a 22 23	626.2	624.0	603.0	603.0	603.0	611.2	608.0	612.5	613.2	614.0	624 · 0	621°0
	23 24 25 26 27 28 29 30	639 0 643 0 644 0 646 4 644 0 621 5	638'8 642'0 640'0 646'0 642'0 620'8	635°0 629°0 630°0 638°2 635°8 630°0	628.0 621.0 618.2 629.1 628.0 621.8	621 ° 0 617 ° 0 611 ° 2 626 ° 8 626 ° 5 589 ° 0	615.0 625.0 613.8 631.0 632.1 589.0	626.0 629.0 620.4 636.0 638.2 618.0	629 ° 0 630 ° 0 629 ° 0 639 ° 0 647 ° 0 637 ° 5	634.8 635.2 634.0 641.0 648.5 619.0	636.0 637.8 637.0 641.5 652.0 639.2	638.0 637.8 637.3 643.0 654.0 637.5	638.0 637.9 638.0 642.0 646.5 640.2
Hourly M		630.78	628.50	623.20	616.43	611.30	610.70	615.62	619.90	625.57	632.57	635.36	634.9
				<u>' </u>	ТЕМРІ	ERATURE O	F THE BIF	LAR MAGN	ET.				
	1 2 3 4 5 6 7 8 9	52°0 45°3 53°4 51°2 50°0 54°0 50°8	52°0 45°8 53°4 51°6 50°4 54°0 51°7	51°9 47°3 53°0 52°0 51°4 54°9 52°5	50°·5 48°·5 53°·2 52°·4 52°·2 55°·7 53°·5	50°·3 49°·5 53°·4 52°·9 53°·2 56°·1 54°·4	50°.7 51°.0 53°.6 53°.5 54°.0 56°.5 55°.0	51°0 51°5 53°6 53°9 54°2 56°6 55°5	50°.6	50°·4 52°·2 53°·8 54°·2 55°·2 56°·6 56°·8	50°·4	50°·4	50°4 53°0 53°7 55°3 57°5 58°0 59°2
SIL.	10 11 12 13 14 15	54.5 59.6 54.1 54.5 49.9 51.5	55.4 59.4 55.2 54.5 50.4 52.9	55.9 58.6 56.0 54.2 50.7 54.0	58.0 58.5 56.2 53.5 51.2 54.8	59.2 58.4 57.0 53.5 51.5 55.5	59.4 58.8 57.5 53.5 52.0 56.6	60°2 59°2 57°5 53°5 52°8 56°6	61.0 59.2 58.2 54.0 53.2 56.6	62.0 59.5 58.5 54.0 53.6 57.2	62.7 59.5 59.1 54.0 54.0 58.0	63.5 59.4 60.0 54.0 54.6 58.9	64.9 59.0 60.0 54.1 54.5 59.9
	16 17 18 19 20	52.8 50.0 44.0 47.4	53.4 49.5 44.2 48.0	54.0 49.3 45.8 49.2	54'1 49'6 47'5 49'8	54'1 49'6 48'0 50'3	54.6 50.5 48.9 51.0	55°0 50°7 49°7 51°4	55°2 50°3 50°0 51°8	56.0 49.5 50.4 52.4	56°3 49°5 50°9 53°0	56°3 49°5 51°7 54°0	56.6 49.0 51.9 54.7
	21 a 22 23 24 25 26 27 28 29 30	53.4 47.4 46.2 50.0 49.4 52.1 53.2	53.0 	53.0 	52.9 	53·3 48·2 50·0 53·0 52·4 51·5 53·7	53.6 49.0 50.4 53.0 53.0 52.0 54.2	54.2 49.5 50.9 53.0 53.6 52.2 54.5	54.7 50.1 51.2 52.8 54.0 52.5 55.3	55.8 50.6 52.0 53.0 54.5 52.6 55.5	56°2 51°2 52°4 53°0 55°4 53°4 56°2	56.8 51.2 52.6 53.5 56.0 54.0 56.9	57.3 51.0 52.6 58.4 56.3 54.0 57.0
	Means	51.16	51.55	52.05	52.47	52.86	53.40	53.77	54.04	54.40	54.82	55.29	55.6

^a Good Friday.

	One Scale	Division =	·000087 pa	rts of the H		IZONTAL se, in Scale		orresponding	g to 1° decre	ase of Temp	perature, 1°6	3.
12 ^h .	13 ^h .	14 ^h .	15h.	16 ^h .	17 ^h .	18h.	19 ^h .	20h.	21 ^h .	22h.	23հ.	Daily an Monthl Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
$638^{\circ}2$	621.2	628.0	636.1	622.0	605.0	CO7:0	610.5	602.0	600.4	605.0	$\{621.5\}$	619.98
			61410		500:0	607.0	599.0	627.0	628.5	625.5	626.0	615.08
633.2	617.7	616.1	614.0	597.5	590.0		626.8	627.5	629.0	631.0	631.4	621.28
629.8	626.5	627.0	630.0	628.0	629.0	629.0	i e	618.3	633.5	625.8	620.2	615.20
632.0	631.0	627.0	629.0	634.0	546.5	565.5	587°1 462°7	181.8	$\frac{033}{277\cdot5}$	$\frac{525}{519.7}$	579.9	560.88
639.0	643.0	602.0	647.8	635.5	405.4	522.3	610.0	613.0	611.2	608.2	603.2	600.10
616.4	603.2	596.2	607.2	610.0	593.0	604.4	010 0	013 0	OII Z	000 2	, I	
618.2	617.0	617.0	619.0	618.8	618.0	618.0	615.8	616.0	624.0	626.0	$\{626.5\}$	616.83
	017.0	C10.C	614:0	C17:C	C12:0	620.0	618.2	622.5	621.0	622.5	622.0	616:33
523.2	617.0	619.6	614.0	617.6	613.0	1		627.0	$\frac{627}{627}$	628.8	628.9	621.62
622.0	623.0	623.0	625.0	625.0	624.1	626.0	627.0		630.6	630.1	631.0	626.2
525.8	624.0	625.0	625.8	626.2	627.2	628.8	629.2	630.0				
637.6	636.0	634.4	635.0	637.0	638.2	638.0	638.0	637.8	641.5	641.6	644.0	631.80
640.0	640.0	640.0	640.0	640.8	638.0	638.8	639.0	639.2	641.6	642.0	645.0	635.6
37.4	602.0	605.5	603.0	612.0	597.0						$\{628\cdot 2\}$	623.63
			J			620.0	624.0	627.2	626.5	625.0		
624.0	599.0	587.0	619.0	619.0	617.2	615.0	625.0	623.8	622.0	625.8	628.8	621.7
38.0	637.0	632.0	628.0	626.4	633.8	635.8	636.0	638'1	632.6	634.9	634.9	629.2
40.5	631.9	636.0	636.0	636.1	636.9	637.0	639.0	638.5	639.0	637.0	642.0	635.90
34.0	635.0	623.0	615.8	619.0	619.2	_					- 7	620.89
	000 0		_		_	618.2	592.4	555.0	556.5	622.0	636.1	020 8
24.0	623.1	617.0	622.2	625.0	623.4						—)	C01.7
	020 1	011 0	022 2	020		633.2	635.0	636.5	641.0	638.5	638.2	621.70
63 7 .8	638.0	639.2	630.0	645.0	638.0	640.4	641.2	643.0	643.2	644.4	643.0	635*9
			639.0	638.8	641.0	641.6	640.6	641.0	642.8	642.5	643.0	636.1
640.0	637.3	635.9			639.0	639.8	641.0	642.1	643.1	644.0	644.2	635.00
637.0	637.8	639.0	639.2	640.5				640.2	642.2	642.2	643.2	638.80
642.0	638.2	634.0	637.0	638.0	639.0	637.0	637.8		616.1	620.0	622.2	638.4
641.0	639.0	642'1	639.8	644.2	656.2	656.0	634.0	617.7	010 1	020 0	1 . 1	000 4
634.8	616.8	607.8	618.0	625.0	616.1	-	010:0	C17:0	617.8	632.0	631.0	621.2
						614.0	616.6	617.0			[
632.46	625.74	623.99	626.18	627.21	620.82	624.59	624.47	625.25	626.57	630.21	631.95	625.18
				TI	EMPERATUF	RE OF THE	BIFILAR M	AGNET.			1	
50.5	50°0	49.6	49.4	49.0	48.7	<u>-</u>	<u>-</u>	<u>°</u>	<u> </u>	<u>-</u>	° 7	9°24
				.		46.0	45.8	45.6	45.6	45.5	45.5	
52.9	52.6	52.6	52.2	52.2	52.2	52.4	52.4	52.7	53.5	53.6	53.4	51.4
53.4	53.0	52.8	52.9	52.3	51.8	51.5	51.4	51.4	51.4	51.4	51.2	52.8
55.7	55.1	22.0	54.5	54.1	54.0	54.0	$53^{\circ}2$	53.2	53.2	52.6	51.0	53.5
57.9	57.0	56.5	55.6	55.5	54.8	54.0	53.6	53.2	53.0	53.1	53.2	54.2
58.5	57.8	57.2	56.0	55.0	54.2	53.7	53.4	53.0	52.5	51.7	51.5	55.3
59.8	59.0	58.6	57.9	57.6	57.4							
	99 0	99.0	019	010	1	56.4	56.0	55.7	55.2	55.1	54.6}	56.0
64.4	62:0	62.5	62:0	62.5	61.9	61.0	90.9	60.4	60.1	60.0	59.8	60.7
58.2	63.9	63.5	63.0		57.8	57.6	57.2	57.0	56.4	56.0	55.4	58.2
	58.3	58.0	58.0	58.0					57°0	26.0	55.5	57.6
60.0	59.2	59.0	58.6	58.4	58.2	58.0	57.6	57.3		49.6	50.0	52.7
54.0	53.8	53.2	52.5	52.0	51.5	51.0	50.7	50.4	50.0			
54.0	53.5	53.2	53.0	52.7	52.8	52.8	52.5	52.3	51.2	51.5	51.4	52.4
59.9	58.6	57.2	56.2	56.1	56.0					<u> </u>	$\frac{-}{53\cdot 2}$	55.8
	_		<u> </u>			55.0	54 . 5	54.0	53.6	53.5	03 2)	
57.0	56.2	56.0	55.5	55.0	55.0	54.0	54.0	53.4	53.0	52.6	51.6	54.6
	48.2	48.6	48.6	48.4	48.2	48.3	48.0	46.7	46.0	45.5	45.1	48.6
	52.0	51.5	51.0	50.2	49.9	49.0	48.9	48.3	48.1	47'8	47.5	49.1
52.2	54.5	53.6	53.4	53.2	53.1			_			54.0}	52.4
52.2					<u> </u>	53.3	53.6	54.0	54.2	54.6		02 4
52°2 55°0			56'1	55.8	55.6	49.5	49.0	48.5	48.0	48.0	$\{-\frac{1}{47\cdot 6}\}$	53.4
52°2 55°0	57.2	56.7		l			48.2	47.7	47.4	46.9	46.2	48.9
48.8 52.2 55.0 — 57.5 — 50.8	57.2	l —		49:0		1 48'5					1	
52.2 55.0 57.5 50.8	57.2	50.2	49.6	49.0	48.8	48.5 50.5				50.0	50.0	50.5
52·2 55·0 57·5 50·8 52·6	57·2 50·4 52·0	50°2 51°5	49.6 50.7	49°0 50°4	48.8 50.4	50.2	50.2	50.0	50.0	50.0 50.0	50°0 49°7	
52·2 55·0 57·5 50·8 52·6 54·4	57·2 50·4 52·0 53·8	50°2 51°5 52°7	49.6 50.7 52.2	49.0 50.4 51.9	48.8 50.4 51.6	50°5 51°5	$\begin{array}{c} 50.2 \\ 51.2 \end{array}$	50°5	20.3 20.0	50.0	49.7	52.3
52·2 55·0 - 57·5 - 50·8 52·6 54·4 56·5	57·2 50·4 52·0 53·8 55·5	50°2 51°5 52°7 55°0	49.6 50.7 52.2 54.5	49.0 50.4 51.9 54.4	48.8 50.4 51.6 54.1	50°5 51°5 54°0	50°2 51°2 53°4	50°0 50°5 53°2	50.0 50.3 50.0	50.0 52.8	49.7 52.5	52°30 53°5'
52·2 55·0 	57·2 50·4 52·0 53·8 55·5 54·6	50°2 51°5 52°7 55°0 54°6	49.6 50.7 52.2 54.5 54.4	49.0 50.4 51.9 54.4 54.4	48.8 50.4 51.6 54.1 54.4	50°5 51°5 54°0 54°4	$\begin{array}{c} 50.2 \\ 51.2 \end{array}$	50°5	20.3 20.0	50.0	49.7 52.5 54.0	50°53 52°30 53°5' 53°3
52·2 55·0 - 57·5 - 50·8 52·6 54·4 56·5	57·2 50·4 52·0 53·8 55·5	50°2 51°5 52°7 55°0	49.6 50.7 52.2 54.5	49.0 50.4 51.9 54.4	48.8 50.4 51.6 54.1	50°5 51°5 54°0	50°2 51°2 53°4	50°0 50°5 53°2	50.0 50.3 50.0	50.0 52.8	49.7 52.5	52°3 53°5

	Or	ne Scale Div	ision = '00	0087 parts o	f the H. F.		NTAL FO		sponding to	1° decrease	of Tempera	ture, 1.63.	
Mean Gen T	Göttin-}	0 ^h .	1 ^h .	2h.	3 ^h •	4 ^h •	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .	10 ^h .	11h.
	1 2 3 4 5 6	Sc. Div. 627 * 5 638 * 0 635 * 2 631 * 0 632 * 0 623 * 0	Sc. Div. 628 ° 0 638 ° 0 633 ° 2 630 ° 0 632 ° 0 610 ° 0	Sc. Div. 626 0 633 0 617 2 623 8 623 0 619 5	Sc. Div. 612 0 614 8 619 0 620 5 612 5 603 2	Sc. Div. 617 0 608 5 610 0 605 0 603 0 607 0	sc. Div. 611°5 605°5 606°9 598°0 604°0 595°0	sc. Div. 612 2 620 5 611 3 612 0 603 0 598 0	Sc. Div. 616 2 630 0 620 0 626 0 612 0 600 8	Sc. Div. 626 2 640 8 628 5 639 0 615 0 606 4	Sc. Div. 634 * 6 637 * 1 630 * 0 648 * 0 621 * 0 621 * 2	Sc. Div. 651 8 642 0 625 0 630 0 631 0 616 0	Sc. Div 638 4 643 0 630 0 635 5 624 6 611 0
	7 8 9 10 11 12 13	600°0 618°2 611°5 622°0 636°5 628°0	597 ° 0 616 ° 0 586 ° 0 619 ° 2 635 ° 5 623 ° 0	597°5 605°4 579°0 620°0 629°0 618°0	585.0 602.0 597.0 610.0 623.5 615.4	591.8 608.6 589.5 610.0 621.0 610.5	590.4 608.0 614.0 607.5 616.0 612.2	600°5 625°0 585°5 607°0 633°5 616°0	603.7 621.2 602.0 610.0 635.0 627.0	611 · 2 623 · 0 599 · 0 618 · 5 640 · 8 627 · 0	625°0 633°0 614°0 623°5 644°2 637°1	622.2 616.0 619.8 624.0 633.0 635.8	630°0 628°0 625°0 623°8 626°1 634°5
MAY.	14 15 16 17 18 19 20	642 · 2 635 · 9 634 · 0 595 · 4 599 · 5 600 · 4	636.8 624.7 633.0 617.0 612.0 598.6	624.4 626.9 625.0 611.0 593.0 595.0	618.0 619.0 611.0 612.0 574.2 584.9	616.2 613.0 609.5 607.0 575.0 594.0	618·2 616·0 603·0 605·0 578·2 605·8	623°0 625°0 617°0 599°0 591°8 595°0	632.0 626.0 625.0 582.2 586.1 603.0	640°0 640°5 635°0 621°5 593°2 610°0	642.0 642.2 630.8 622.8 603.0 605.8	638 ° 0 635 ° 0 658 ° 0 629 ° 2 614 ° 2 608 ° 0	638.0 632.5 643.4 612.8 605.0 611.5
	21 22 23 24 25 26 27	621.8 624.0 630.5 616.0 610.0 617.0	626.7 623.0 627.0 606.0 612.2 608.0	620°0 622°8 611°5 607°0 612°4 588°5	607.8 611.0 610.0 614.2 604.3 597.0	600°0 600°0 606°4 606°0 603°0 588°0	598.8 597.5 609.0 600.4 604.1 598.5	606.0 598.0 610.0 603.2 607.0 602.0	619.8 603.0 616.8 610.4 619.8 616.9	618.5 614.0 624.8 616.1 621.0 614.0	621.5 618.0 591.2 625.0 618.8 627.2	610.0 617.2 612.2 615.0 621.0 638.0	620°0 621°4 614°0 626°5 619°0 647°0
	28 29 30 31	608.0 615.2 630.9	612.0 613.0 627.5	631.6 600.0 610.8	589.0 601.0 617.2	591.8 598.0 606.8	600°0 600°0 612°8	602.5 604.0 620.5	605°0 606°5 617°2	607°0 613°2 618°2	610°2 618°8 633°6	614.0 614.8 636.0	612.2 614.3 619.8
Hourl	y Means	621.63	619.46	613.97	606.87	603.28	604.31	608.46	613.84	620.83	625.17	626.30	625.4
								ILAR MAGN					
	$\left(\begin{array}{c}1\\2\\3\\4\\5\\6\end{array}\right)$	50.7 52.0 56.0 57.2 59.7 63.5	50.6 52.2 57.0 57.5 60.5 64.3	50.7 52.5 57.8 57.8 62.0 64.8	51°5 53°6 58°7 58°4 63°5 65°5	52.2 54.6 60.0 59.7 64.4 66.0	53°3 55°6 60°5 60°5 65°2 66°8	53.6 56.2 60.5 61.2 66.0 67.5	53.7 57.0 60.7 60.8 66.7 68.2	53.8 58.0 61.0 60.6 67.5 68.8	54.0 59.0 61.8 60.2 67.3 69.8	54.4 59.2 62.4 60.1 68.6 70.4	54.6 59.2 62.7 59.6 68.4 70.6
	7 8 9 10 11 12 13	59.5 58.0 58.7 57.6 53.6 54.0	59.5 58.5 59.5 57.5 54.3 53.8	59.9 59.2 60.5 57.0 55.1 53.5	60°8 60°0 61°2 57°3 56°0 53°6	60°5 60°7 62°2 57°6 57°0 53°8	60°8 61°0 62°2 58°2 57°6 53°3	61.2 61.4 62.2 58.5 58.0 53.0	61.5 61.8 62.5 58.0 58.6 53.9	62.0 62.2 62.4 58.0 59.2 54.1	62.4 62.4 62.4 57.8 59.8 55.0	62.9 62.0 62.5 58.0 60.6 55.7	63 ° 0 62 ° 0 62 ° 4 58 ° 2 61 ° 0 54 ° 9
MAY.	14 15 16 17 18 19 20	52.6 56.6 56.1 58.8 62.5 65.0	53.5 56.7 56.7 60.0 62.5 64.8	54·3 57·0 57·8 60·9 63·2 65·1	55.0 57.4 58.7 62.0 64.4 65.9	56°1 58°2 59°7 62°5 66°0 66°9	56 9 58 9 60 4 63 0 67 0 67 7	57.7 59.4 60.8 63.5 68.3 68.8	58.2 59.5 61.5 64.4 69.2 69.0	58.8 60.0 62.4 65.0 69.9 69.6	58.8 60.3 63.4 66.2 70.5 69.7	58.6 60.7 64.0 67.2 70.5 69.7	58.3 61.0 64.4 67.6 70.5 69.5
	21 22 23 24 25 26 27	64.0 62.4 60.9 63.5 64.2 62.2	63.7 62.0 61.5 64.0 64.9 62.8	63.6 62.3 62.0 64.0 65.6 63.5	63.8 62.3 62.2 64.6 66.0 64.2	64.5 62.1 63.2 64.8 66.5 65.1	64.5 62.6 64.0 65.8 66.7 65.8	65.6 62.6 64.9 67.0 67.0 66.1	65.0 62.4 65.9 67.6 67.2 66.5	65.7 62.5 67.0 68.5 68.0 67.2	66°3 63°0 67°6 69°6 68°4 68°0	66.2 63.4 68.6 71.1 70.4 68.5	66.1 63.5 74.2 71.2 70.3 69.5
	28 29 30 31	65°3 66°3 59°5	60.0 62.2 62.2	66°1 67°4 60°5	66.2 68.0 60.8	67.5 68.5 61.0	67·7 68·5 60·9	68.5 68.5 60.9	69°2 63°8 61°0	69.5 69.2 61.0	70°3 69°2 62°0	71.0 68.9 62.4	71'8 68'6 62'4
Hourl	y Means	59.27	59.65	60.12	60.81	61.23	62.05	62.55	62.92	63.40	63.90	64.37	64.6

12h.	13 ^h .	14 ^h .	15 ^h .	16⁴•	17 ^h .	18հ.	19 ^h .	20h.	21h.	22h.	23h.	Daily an Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
341.0	630.9	634.0	635.0	634.9	638.0	638.4	623.0	628.8	632.0	630.0	636.5	629:33
640 ° 0	637.0	622.0	616.0	617.0	614.4	617.0	625.8	627.0	628.0	625.0	631.2	627.15
632.0	623.0	624.5	628.0	625.0	622.1	624.1	625.8	626.2	630.0	618.5	639.0	624 35
534.2	630.0	631.5	627.2	630.0	630.8	631.5	631.2	631.4	627.0	631.0	632.0	627.77
626.4	612.2	612.8	617.1	610.8	615.9	619.2	618.4	615.0	616.2	617.8	621.0	617:33
620.0	615.0	617.8	608.2	608.8	609.4	614.0	608.2	601.2	603.0	611.0	$\left \frac{-}{615.5} \right $	610.17
531.2	611.0	607.0	597.5	605.2	598.5	602.0	598.2	602.5	616.2	618.0	618.4	606.69
522.5	622.0	621.8	$\begin{vmatrix} 597 & 5 \\ 621 & 0 \end{vmatrix}$	620.0	620.0	623.0	621.2	622.0	623.2	614.8	604.0	618.33
520 . 0	611.7	617.5	608.0	602.0	605.0	608.8	606.0	597.1	610.0	619.0	618.4	606.07
527°0	626.8	622.0	633.0	631.3	634.0	629.0	627.8	632.0	631.8	632.0	637.0	623.30
625°9	626.1	624.5	624.5	624.0	615.0	615.4	627.6	628.0	625.0	627.2	629.0	627.75
35 . 8	632.2	633.0	635.2	633.0	638.0	010 4	021 0	020 0	020 0	021 2		
000 0	002 2	000 0	000 0	000 0	050 0	636.0	636.0	637.1	637.0	639.0	$\left \frac{-}{642 \cdot 8} \right\}$	630.00
635.0	635.0	634.0	635.0	637:3	639.0	638.0	636.8	638.2	637.8	637.0	638.0	633.75
37 . 0	629.5	630.2	630.8	636.6	633.8	635.8	633.9	630.0	629.0	633.0	632.0	630.36
518.5	634.2	631.8	627.1	597.1	601.0	592.0	515.2	546.5	606.2	621.0	603.2	613.28
$32^{\circ}3$	780.0	666.3	597.0	613.0	600.0	599.0	597.5	594.0	601.2	603.2	605.0	616.42
97.0	605.0	604.0	603.0	604.5	609.5	625.0	603.0	614.6	612.0	597.5	599.8	600.00
04.0	608.0	606.1	612.0	609.5	610.0	020 0	000 0	011 0	012 0	031	1	
						612.2	593.5	609.8	609.2	610.0	$\{609.2\}$	604.40
16.0	616.0	617.0	615.8	616.0	616.2	616.4	615.5	617.5	619.2	620.0	621.0	615.73
22.8	620.5	621.4	622.8	623.9	624.3	627.9	627.4	630.0	630.8	623.2	631.0	619.00
39.0	609.0	605.8	606.0	606.0	607.2	607.0	610.2	608.2	612.0	613.0	612.0	612.48
317.0	605.0	605.4	606.0	607.0	600.0	587.0	601.0	608.2	610.0	610.0	608.4	608.78
19.0	616.0	617.2	619.0	607.0	613.5	634.2	597.8	585.0	603.7	616.8	616.0	612.41
28.0	611.0	606.2	615.4	616.2	618.0	0010					1 1	
	011	-	019 1	010 2	0.0	609.0	609.0	610.0	610.2	609.0	608.8	612.22
09.2	611.0	612.2	612.0	611.9	611.1	608.3	610.5	610.8	610.0	612.5	612.0	608.06
913.0	612.2	616.3	618.0	618.4	618.8	613.0	619.0	613.0	613.0	621.0	620.0	612.66
640.0	636.2	638.0	612.0	608.0	611.0	625.0	627.0	622.5	628.2	631.2	628.5	624.15
624.94	626.16	621.20	617.90	616.83	616.82	618.09	612.86	614.34	618.99	620.07	621.11	617.48
	020 10	021 00	011 30	<u> </u>	EMPERATUI				010 00		021 11	01, 10
55°.0	54°6		54.0	5 4 '0	53°4	53.0	53.0	52°·5	52.4	52°3	52.0	53°07
		54.4										
59.0	58.8	58.5	57.5	57.3	56.8	56.3	56.3	56.3	56.3	56.0	56.0	56.43
62.8	62.0	61.8	61.5	61.4	61.0	60.2	59.8	59.2	59.0	58.2	57.1	60.13
59.5	59.4	59.4	59.3	59.1	59.2	59.3	59.2	59.2	59.4	59.4	59.3	59.39
67.6	66.7	66.0	65.5	65.3	64.6	64.2	64.3	63.8	63.2	63.0	62.2	64.87
70.2	70.0	69.0	68.2	68.4	68.0	-	60.0				59.5	66.15
60:6	-	-			<u> </u>	62.5	62.0	61.3	60.9	60.3	59 5)	
62.6	62.4	61.8	61.3	60.8	60.4	60.0	59.5	59.0	58.6	58.0	57.6	60.6
65.0	61.5	61.0	60.6	60.5	60.4	60.2	60.0	59.7	59.4	59.4	58.6	60.52
69.0	61.5	61.0	60.6	60.2	59.6	59.2	58.9	58.7	58.3	58.0	58.0	60.61 57.07
	58.2	57.6	57.5	57.0	56.6	56.8	55'9	55.2	54.8 55.0	54°5	53.9	
58.5			58.6	58.5	57.2	56.8	56.0	55.5	55.0	54.9	54.0	57.40
61.0	60.2	59.5		go • 0		l					— \	53.40
58·5 61·0 54·1		52.8	52.6	52.3	52.0	53:0	59:0	50.0			1 50.0 (1	
58·5 61·0 54·1	60°2 53°3	52.8	52.6 —		52.0	53.0 57.0	52.9 57.0	52.8 56.7	52.5	52.5	52.3 }	
58.5 61.0 54.1 — 58.3	60.2 53.3 — 58.0	52.8 57.5	52.6 — 57.4	57.2	52.0 57.0	57.0	57.0	56.7	52.5 56.9	52.5 57.0	57.0	56.91
58.5 61.0 54.1 58.3 61.0	60°2 53°3 58°0 60°5	52.8 57.5 60.0	52.6 57.4 60.0	57·2 59·2	52.0 57.0 58.4	57.0 57.8	57°0 57°5	56.7 57.0	52.5 56.9 56.6	52.5 57.0 56.2	57.0 55.8	56 · 91
58.5 61.0 54.1 58.3 61.0 64.4	60°2 53°3 — 58°0 60°5 63°6	52.8 57.5 60.0 63.0	52.6 57.4 60.0 62.4	57°2 59°2 62°0	52.0 57.0 58.4 61.0	57.0 57.8 60.5	57.0 57.5 60.0	56.7 57.0 59.8	52.5 56.9 56.6 59.7	52.5 57.0 56.2 59.4	57.0 55.8 58.8	56°91 58°57 60°86
58:5 61:0 54:1 58:3 61:0 64:4 68:0	60°2 53°3 	52.8 57.5 60.0 63.0 67.5	52.6 	57°2 59°2 62°0 66°5	52.0 57.0 58.4 61.0 65.5	57.0 57.8 60.5 64.8	57.0 57.5 60.0 64.3	56.7 57.0 59.8 63.6	52.5 56.9 56.6 59.7 63.5	52.5 57.0 56.2 59.4 63.5	57.0 55.8 58.8 62.5	56°91 58°57 60°86 64°46
58.5 61.0 54.1 58.3 61.0 64.4 68.0 70.2	60°2 53°3 	52.8 57.5 60.0 63.0 67.5 69.5	52.6 57.4 60.0 62.4 66.9 68.0	57·2 59·2 62·0 66·5 67·6	52.0 57.0 58.4 61.0 65.5 67.2	57.0 57.8 60.5	57.0 57.5 60.0	56.7 57.0 59.8 63.6 66.3	52.5 56.9 56.6 59.7	52.5 57.0 56.2 59.4	57.0 55.8 58.8 62.5 65.2	56.91 58.57 60.86 64.40 67.23
58.5 61.0 54.1 58.3 61.0 64.4 68.0 70.2	60°2 53°3 	52.8 57.5 60.0 63.0 67.5 69.5 68.8	52.6 57.4 60.0 62.4 66.9 68.0 68.2	57.2 59.2 62.0 66.5 67.6 67.9	52.0 57.0 58.4 61.0 65.5 67.2 67.5	57.0 57.8 60.5 64.8 67.0	57.0 57.5 60.0 64.3 66.5	56.7 57.0 59.8 63.6 66.3	52.5 56.9 56.6 59.7 63.5 66.0	52.5 57.0 56.2 59.4 63.5 65.5	57.0 55.8 58.8 62.5 65.2	56.91 58.57 60.86 64.40 67.23
58·5 61·0 54·1 58·3 61·0 64·4 68·0 70·2 69·5	60.2 53.3 — 58.0 60.5 63.6 68.0 70.0 69.0	52.8 	52.6 	57·2 59·2 62·0 66·5 67·6 67·9	52.0 57.0 58.4 61.0 65.5 67.2 67.5	57.0 57.8 60.5 64.8 67.0 — 63.6	57.0 57.5 60.0 64.3 66.5 — 63.5	56.7 57.0 59.8 63.6 66.3 — 63.9	52.5 56.9 56.6 59.7 63.5 66.0	52.5 57.0 56.2 59.4 63.5 65.5 	57.0 55.8 58.8 62.5 65.2 - 64.2}	56°91 58°57 60°86 64°40 67°23 66°90
58:3 61:0 64:4 68:0 70:2 69:5	60.2 53.3 	52.8 	52.6 	57·2 59·2 62·0 66·5 67·6 67·9	52.0 57.0 58.4 61.0 65.5 67.2 67.5 64.4	57.0 57.8 60.5 64.8 67.0 — 63.6 63.8	57.0 57.5 60.0 64.3 66.5 	56.7 57.0 59.8 63.6 66.3 — 63.9 63.0	52.5 56.9 56.6 59.7 63.5 66.0 — 63.8 63.0	52.5 57.0 56.2 59.4 63.5 65.5 64.0 62.8	57.0 55.8 58.8 62.5 65.2 	56.91 58.57 60.86 64.40 67.23 66.90
58·5 61·0 54·1 - 58·3 61·0 64·4 68·0 70·2 69·5 - 66·3 63·6	60.2 53.3 	52.8 	52.6 	57.2 59.2 62.0 66.5 67.6 67.9 — 65.0 62.0	52.0 57.0 58.4 61.0 65.5 67.2 67.5 64.4 61.5	57.0 57.8 60.5 64.8 67.0 — 63.6 63.8 61.5	57.0 57.5 60.0 64.3 66.5 63.5 63.4 61.3	56.7 57.0 59.8 63.6 66.3 — 63.9 63.0 61.0	52.5 56.9 56.6 59.7 63.5 66.0 — 63.8 63.0 60.8	52.5 57.0 56.2 59.4 63.5 65.5 64.0 62.8 60.8	57.0 55.8 58.8 62.5 65.2 	56.91 58.57 60.86 64.40 67.28 66.90 64.58 62.28
58·5 61·0 54·1 	60.2 53.3 	52.8 	52.6 	57.2 59.2 62.0 66.5 67.6 67.9 — 65.0 62.0 67.8	52.0 	57.0 57.8 60.5 64.8 67.0 — 63.6 63.8 61.5 66.5	57.0 57.5 60.0 64.3 66.5 — 63.5 63.4 61.3 65.6	56.7 57.0 59.8 63.6 66.3 —————————————————————————————	52.5 56.9 56.6 59.7 63.5 66.0 ——————————————————————————————————	52.5 57.0 56.2 59.4 63.5 65.5 64.0 62.8 60.8 64.3	57.0 55.8 58.8 62.5 65.2 	56.91 58.57 60.86 64.40 67.23 66.90 64.58 62.23 66.07
58·5 61·0 54·1 	60.2 53.3 	52.8 	52.6 	57.2 59.2 62.0 66.5 67.6 67.9 — 65.0 62.0 67.8 67.6	52.0 	57.0 57.8 60.5 64.8 67.0 — 63.6 63.8 61.5 66.5 66.6	57.0 57.5 60.0 64.3 66.5 63.5 63.4 61.3 65.6 66.0	56.7 57.0 59.8 63.6 66.3 —————————————————————————————	52.5 56.9 56.6 59.7 63.5 66.0 — 63.8 63.0 60.8 64.6 65.0	52.5 57.0 56.2 59.4 63.5 65.5 64.0 62.8 60.8 64.3 64.5	57.0 55.8 58.8 62.5 65.2 	56.91 58.57 60.86 64.46 67.23 66.90 64.59 62.23 66.07 67.01
58·5 61·0 54·1 	60.2 53.3 — 58.0 60.5 63.6 68.0 70.0 69.0 — 66.0 63.4 69.9 71.0 69.0	52.8 	52.6 	57·2 59·2 62·0 66·5 67·6 67·9 — 65·0 62·0 67·8 67·6 67·2	52.0 	57.0 57.8 60.5 64.8 67.0 — 63.6 63.8 61.5 66.5 66.6 65.7	57.0 57.5 60.0 64.3 66.5 — 63.5 63.4 61.3 65.6	56.7 57.0 59.8 63.6 66.3 —————————————————————————————	52.5 56.9 56.6 59.7 63.5 66.0 ——————————————————————————————————	52.5 57.0 56.2 59.4 63.5 65.5 64.0 62.8 60.8 64.3 64.5 63.2	57.0 55.8 58.8 62.5 65.2 	56.91 58.57 60.86 64.46 67.23 66.90 64.55 62.23 66.07 67.01 66.63
58·5 61·0 54·1 	60.2 53.3 	52.8 	52.6 	57.2 59.2 62.0 66.5 67.6 67.9 — 65.0 62.0 67.8 67.6	52.0 	57.0 57.8 60.5 64.8 67.0 — 63.6 63.8 61.5 66.5 66.5 66.6 65.7 —	57.0 57.5 60.0 64.3 66.5 — 63.5 63.4 61.3 65.6 66.0 65.2	56.7 57.0 59.8 63.6 66.3 — 63.9 63.0 61.0 65.0 65.5 64.5	52.5 56.9 56.6 59.7 63.5 66.0 — 63.8 63.0 60.8 64.6 65.0 63.9 —	52.5 57.0 56.2 59.4 63.5 65.5 64.0 62.8 60.8 64.3 64.5 63.2	57.0 55.8 58.8 62.5 65.2 	56.91 58.57 60.86 64.40 67.23 66.90 64.59 62.23 66.07 67.01 66.63
58·5 61·0 54·1 	60.2 53.3 	52.8 	52.6 	57·2 59·2 62·0 66·5 67·6 67·9 — 65·0 62·0 67·8 67·6 67·2 67·4 —	52.0 57.0 58.4 61.0 65.5 67.2 67.5 64.4 61.5 67.0 67.1 66.6 67.0	57.0 57.8 60.5 64.8 67.0 — 63.6 63.8 61.5 66.5 66.6 65.7 — 67.0	57.0 57.5 60.0 64.3 66.5 — 63.5 63.4 61.3 65.6 66.0 65.2 — 66.5	56.7 57.0 59.8 63.6 66.3 — 63.9 63.0 61.0 65.0 65.5 64.5 — 66.0	52.5 56.9 56.6 59.7 63.5 66.0 — 63.8 63.0 60.8 64.6 65.0 63.9 — 65.9	52.5 57.0 56.2 59.4 63.5 65.5 64.0 62.8 64.3 64.5 63.2 — 65.6	57.0 55.8 58.8 62.5 65.2 	56.91 58.57 60.86 64.40 67.23 66.90 64.55 62.23 66.07 67.01 66.63
58·5 61·0 54·1 58·3 61·0 66·4 66·4 66·0 70·2 69·5 71·0 70·5 71·0 70·6 66·1	60.2 53.3 	52.8 	52.6 	57.2 59.2 62.0 66.5 67.6 67.9 65.0 62.0 67.8 67.6 67.2 67.4 70.7	52.0 57.0 58.4 61.0 65.5 67.2 67.5 — 64.4 61.5 67.0 67.1 66.6 67.0 — 70.0	57.0 57.8 60.5 64.8 67.0 — 63.6 63.8 61.5 66.5 66.5 65.7 — 67.0 69.3	57.0 57.5 60.0 64.3 66.5 — 63.5 63.4 61.3 65.6 66.0 65.2 — 66.5 69.0	56.7 57.0 59.8 63.6 66.3 — 63.9 63.0 61.0 65.0 65.5 64.5 — 66.0 68.6	52.5 56.9 56.6 59.7 63.5 66.0 — 63.8 63.0 60.8 64.6 65.0 63.9 — 65.9 68.0	52.5 57.0 56.2 59.4 63.5 65.5 64.0 62.8 60.8 64.3 64.5 63.2 65.6 67.2	57.0 55.8 58.8 62.5 65.2 	56.91 58.57 60.86 64.40 67.23 66.90 64.59 62.23 66.07 67.01 66.63 66.41 68.99
58·5 61·0 54·1 	60.2 53.3 	52.8 	52.6 	57·2 59·2 62·0 66·5 67·6 67·9 65·0 62·0 67·8 67·6 67·2 67·4 70·7 64·5	52.0 57.0 58.4 61.0 65.5 67.2 67.5 — 64.4 61.5 67.0 67.1 66.6 67.0 — 70.0 64.0	57.0 57.8 60.5 64.8 67.0 — 63.6 63.8 61.5 66.5 66.6 65.7 — 67.0 69.3 63.3	57.0 57.5 60.0 64.3 66.5 — 63.5 63.4 61.3 65.6 66.0 65.2 — 66.5 69.0 62.0	56.7 57.0 59.8 63.6 66.3 — 63.9 63.0 61.0 65.0 65.5 64.5 — 66.0 68.6 61.0	52.5 56.9 56.6 59.7 63.5 66.0 — 63.8 63.0 60.8 64.6 65.0 63.9 — 68.0 60.5	52.5 57.0 56.2 59.4 63.5 65.5 64.0 62.8 60.8 64.3 64.5 63.2 65.6 67.2 60.0	57.0 55.8 58.8 62.5 65.2 	56.91 58.57 60.86 64.40 67.23 66.90 64.53 62.23 66.07 67.01 66.65 66.41 68.99 65.85
58·5 61·0 54·1 58·3 61·0 66·4 670·2 69·5 66·3 63·6 70·5 77·3 69·0 72·6 68·1	60.2 53.3 	52.8 	52.6 	57.2 59.2 62.0 66.5 67.6 67.9 65.0 62.0 67.8 67.6 67.2 67.4 70.7	52.0 57.0 58.4 61.0 65.5 67.2 67.5 — 64.4 61.5 67.0 67.1 66.6 67.0 — 70.0	57.0 57.8 60.5 64.8 67.0 — 63.6 63.8 61.5 66.5 66.5 65.7 — 67.0 69.3	57.0 57.5 60.0 64.3 66.5 — 63.5 63.4 61.3 65.6 66.0 65.2 — 66.5 69.0	56.7 57.0 59.8 63.6 66.3 — 63.9 63.0 61.0 65.0 65.5 64.5 — 66.0 68.6	52.5 56.9 56.6 59.7 63.5 66.0 — 63.8 63.0 60.8 64.6 65.0 63.9 — 65.9 68.0	52.5 57.0 56.2 59.4 63.5 65.5 64.0 62.8 60.8 64.3 64.5 63.2 65.6 67.2	57.0 55.8 58.8 62.5 65.2 	56.93 58.5 60.86 64.40 67.23 66.90 64.53 66.03 66.63 66.43 68.99

Vol. III.

Mean G	öttin-}	0h.	1h.	2 ^h .	3h.	4 ^h .	5 ^h .	6h.	7 ^h .	8h.	9 ^h .	10h.	11 ^h .
gen Ti	me.												
		Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	8c. Div.	Sc. Div.	Sc. Div.	Sc. Div
($egin{array}{c c} 1 \\ 2 \end{array}$	631.8 621.0	624.4 618.8	$621.2 \\ 616.0$	611.3	603.6 595.0	606°5 597°4	618.4 607.8	626.0 620.0	630°0 625°0	631.0 629.0	$\frac{628.0}{628.5}$	626°0
1	$\frac{2}{3}$	617.0	614.8	606.2	607°0 598°3	591.5	597.0	600.0	606.2	616.0	619.0	623.0	626.5
	4					-	-	_				— I	
	5	616.0	612.0	601.2	604.0	597.0	594.0	601.0	606.0	610.4	622.2	621.2	621.2
	6	620.5	619.0	616.0	614'8	599.9	605.0	601.2	614.1	616'1	621.4	626.8	629'0
1	$\begin{bmatrix} 7 \\ 8 \end{bmatrix}$	635.2	$631.8 \\ 623.1$	$625.0 \\ 620.0$	618'1	612.0	613.0 602.0	613.0	$625.0 \\ 622.0$	633.5 625.0	632.5 628.0	631.0 626.0	631.0
1	9	$629.8 \\ 628.0$	627.0	624.2	616.0 620.0	610.0 617.6	618.0	624.0	631.5	634.0	625.0	625.2	619 8
	10	624.0	619.2	617.0	611.0	609.0	622.0	622.2	632.5	644.2	625.8	628.2	635
	11							<u> </u>					
	12 13	622.0	626.5	622.5	613'8 626'2	604°2 608°0	$602.2 \\ 608.0$	614.8 612.0	627°0 611°6	630 . 5	631.8 637.0	631.1 636.0	623°0
.	14	637.0	638.8	637.0	632.2	618.0	599.0	619.0	637.5	639.5	662.5	651.0	647.0
JUNE	15	628.0	624.0	622.0	610.0	608.2	610.0	608.7	612.0	613.1	622.0	606.0	609.2
F)	16	607.0	602.0	597.3	594.0	589.0	591.8	591.2	596.2	596.0	600.2	602.2	597.0
ا ي	17 18	602.8	604.2	598.4	590.0	589.0	587.5	592.0	596.0	596.2	600.0	601.2	599.0
	19	615.8	615.2	606.0	598.0	591.4	582.0	587.0	604.0	617.5	616.0	625.0	629.0
1	20	600.0	612.0	612.0	604.0	599.0	598.5	601.0	607.0	617.0	603.0	610.2	611.8
	21	617.5	605.0	595.0	596.0	593.2	595.0	607.5	628.0	630.0	652.0	625.4	624.2
	$\begin{array}{c c} 22 \\ 23 \end{array}$	605.5	588.8	604.5	598.0	580.0	585.0	587.0	602.1	604.0	643.0	656.0	627.5
1	$\frac{25}{24}$	607.0	608.0	606.8 607.0	595.5 601.0	589°0 594°0	589.0 601.0	598.0 612.0	610.0	620.0	$\begin{array}{c} 622.0 \\ 622.0 \end{array}$	618 · 2	619.0
1	25	—	_	_			-						
	26	603.0	605.0	603.8	600.0	586.0	587.0	595.0	598.5	612.0	608.0	625.0	613.0
j	$\begin{bmatrix} 27 \\ 28 \end{bmatrix}$	608.0	603.5	599.5 599.5	590.8 590.0	590.5 591.8	594°0 596°2	594.0 607.8	597.0 613.8	607.0 611.2	602.0	606.0 614.4	616.0
İ	29	616.5	607.0	598.2	592.0	592.0	591.2	602.0	610.0	608.0	605.0	614.0	618.0
(30	615.0	613.2	607.0	606.2	594.0	600.0	607.5	605.0	601.0	618.0	612.0	611.8
lourly	Means	618.06	615:38	611.31	605.34	598.20	598.93	605:36	613.49	618.60	622.60	622.90	621.1
			1	1	ТЕМР	ERATURE (F THE BIF	ILAR MAGN	NET.	<u></u>	1		<u> </u>
	. 1	57°4	58.4	59°4	60°0	60°·4	6η2	6η5	62°2	62°·4	63.5	63°5	63.6
ſ	$egin{array}{c c} 1 \\ 2 \end{array}$	58.8	59.6	60.8	62.0	63.2	64.0	64.5	62.2	$62^{\circ}4$ $65^{\circ}4$	66.1	63.5	67.4
	3	64.2	65.3	65.6	66.3	67.4	68.3	69.3	70.0	70.0	71.0	71.3	71.2
	4			l —	l —					_			
	5	65.6	66.3	67.3	67.5	67.9	68.0	68.3	68.3	68.2	68.2	68.4	68.2
	$\begin{bmatrix} 6 \\ 7 \end{bmatrix}$	61.9 58.6	61.9 59.2	61.9 59.8	62.0	61.0 61.3	$61.0 \\ 61.0$	$\begin{array}{c} 62.2 \\ 61.5 \end{array}$	62.6 62.0	63.0 62.8	63°3 63°4	63.9 64.2	64.2 65.2
İ	8	59.1	60.0	61.0	62.0	63.4	64.5	64.2	65.1	65.7	66.2	67.0	67.4
1	9	62.7	64.0	64.4	65.2	66.3	66.8	67.3	68.0	68.7	69.8	70.4	70.8
	10	66.3	66.4	67.3	68.0	68.7	69.0	69.7	69,8	70.2	70.8	71.0	71.0
	$\frac{11}{12}$	61.9	62.0	62.4	62.8	63.0	62.8	$\frac{-}{62.5}$	$\frac{-}{62.4}$	62.9	63.2	64.2	64.6
	13	58.4	59.0	59.4	60.0	60.7	61.0	61.0	61.2	62.5	62.2	63.0	63.7
63	14	57.6	57.4	57.8	57.8	58.0	59'3	59.7	59.7	60.5	61.0	61.8	62.6
\mathbf{z}	15	60.8	61.9	63.6	65.0	67.4	70.0	72.5	75.0	76.9	78.5	80.2	80.4
JUNE.	16 17	74°5 75°0	75°0 75°4	76:5 75:6	77.6	78.7 77.5	79°6 78°7	80°8	81 · 4 79 · 8	81 · 9 79 · 5	82 · 8 79 · 9	83.0	82°2
1	18	·		_	_		_						
i	19	73.0	72.8	73.7	73.9	74.3	74.5	75.8	76.4	76.7	76.6	76.2	76.5
	$\frac{20}{21}$	72.0 69.0	72 . 4 69.3	72.5 69.3	73°3 69°5	73.5 69.9	74.0	74°3 70°0	74.5 70.2	74.8 70.5	75°1 71°0	75 ·4 71·8	74°5
	22	67.4	67.0	67.5	68.2	69.4	$69.9 \\ 70.0$	70.5	70 2	70.5	71.0 72.2	71.8 72.3	72.0
		67.6	67'8	67.8	68.0	68.5	70.0	70.7	71.8	73.8	$74 \cdot 2$	74.0	72.6
	23	67.2	67.5	68.3	69.0	69.2	70.3	70.3	70.5	70.8	71.5	72.3	72.5
	$\begin{bmatrix} 23 \\ 24 \end{bmatrix}$	J. 2			72.3	73.8	74.6	75.7	76.5	77.6	78.2	78.7	78.7
	23 24 25		71.0	71.9				74.3	75.0	76.0		77.0	
	23 24 25 26 27	70°0 70°8	71.0 71.0	71.9 71.6	72.5	72.9	73.9	1 4 0	, , ,	100	104		76.5
	23 24 25 26 27 28	70°0 70°8 73°0	71.0 73.0	71.6 73.0	$\begin{array}{c} 72.5 \\ 73.4 \end{array}$	73.6	73.5	73.8	73.8	73.8	76°4 74°4	74.6	74 8
	23 24 25 26 27 28 29	70.0 70.8 73.0 69.4	71.0 73.0 69.6	71.6 73.0 70.8	$72.5 \\ 73.4 \\ 72.0$	73.6 72.8	$\begin{array}{c} 73.5 \\ 72.8 \end{array}$	$\begin{array}{c} 73.8 \\ 72.6 \end{array}$	73°8 72°9	73 · 8 73 · 8	74°4 74°4	74.6 74.8	74°8 75°8
	23 24 25 26 27 28	70°0 70°8 73°0	71.0 73.0	71.6 73.0	$\begin{array}{c} 72.5 \\ 73.4 \end{array}$	73.6	73.5	73.8	73.8	73.8	74.4	74.6	74

12h.	13 ^h .	14 ^h .	15h.	16 ^h .	17 ^h .	18h.	19 ^h •	20 ^h •	21 ^h .	22h.	23 ^h •	Daily an Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 619.0	Sc. Div.
625 `0 627 `2	619.0 622.0	617°0 625°0	$616.3 \\ 622.0$	616.0	617.0 613.5	$\begin{array}{c} 617.0 \\ 612.8 \end{array}$	616'2 613'0	619.0 613.3	619 · 2	619.8	616.2	616.68
524.0	628.0	609.8	615.0	609.1	597.2		-	— I				611.94
		_	_		-	614.0	613.8	618.0	618.4	612.2	611.0}	
20.5	611.0	612.8	612.8	616.0	617.0	620.0	622'1	621.8	619.0	618.0	618.0	613°12
28.0	627.2	628.0	629.0	630.0	628.0	627.8	627.0	627.5	$630.0 \\ 626.2$	$\begin{array}{c} 628.0 \\ 628.2 \end{array}$	631'2 630'0	626.09
29.0 25.0	625°0 621°0	628 ·2 626 · 0	$628 \cdot 8$ $623 \cdot 8$	629°0 624°8	628°0 624°2	626°0 624°0	621'8 619'1	624.8 621.8	623.0	625.1	624.8	621 '94
21.2	616.5	621.2	622.0	612.1	602.1	608.6	608.2	608.4	615.2	614.8	621.2	619.40
16.0	605.0	606.2	607.0	606.8	610.0						}	618.78
						625.0	617.0	617.0	617.5	617.0	614.0 } 629.0	623.74
26.0	625.0	623.0 632.0	626.0	626°0 630°1	626.5	626.5	$625.9 \\ 631.2$	630°0 629°4	$630.0 \\ 628.2$	626.5 631.8	630.2	628.34
32.0 21.0	630.0	$632.0 \\ 627.2$	633.5 626.0	620.4	$633.5 \\ 622.8$	632 . 0 621 . 8	630.0	619.0	624.2	627.0	626.0	629.72
02.5	600.0	598.8	600.0	600.4	596.8	597.0	602.0	601.0	601.0	602.0	604.9	607.48
$94.\bar{2}$	590.0	592.0	590.3	591.0	592.5	592.0	593.2	596.0	595.5	599.0	601.2	595.48
95.2	595.0	595.0	598.0	595.0	597.0	_					(19:0)	598.7
			608.2			604.0	603.0	605°0	606 · 1	607 . 9	$\frac{-}{612.0}$	604.9
05°0 21°0	612.0	603 . 8	608 2	598.0 597.2	598 . 8	601.0	600.8	604.2	605.0	610.0	611.0	606.1
01.5	613.0	607.0	602.2	602.0	599.4	602.0	604.2	609.9	600.9	609.0	603.2	609.2
28.0	615.0	591.0	595.0	604.0	595.2	598.0	586.5	591.0	602.5	607.1	610.0	604.3
14.0	618.0	607.5	605.0	607.0	603.0	602.0	598.2	609.0	611.8	607.4	609.8	607:30
12.0	606.0	611.0	611.0	613.0	607.0		602.8	607.2	601.4	602.2	604.0	609.38
07.0	593.2	596.0	598.2	599.2	598.5	608.8 602.2	600.0	601.0	601.4	598.8	603.0	601.4
01.0	601.4	606.5	605.0	605.4	605.4	606.0	605.0	605.2	909.0	607.0	607.0	602.4
09.4	610.5	614.0	604.2	602.0	608.0	610.0	610.0	613.5	610.0	611.6	611.5	607.5
10.0	612.0	607.5	614.0	606.9	607.0	608.0	600.0	602.0	596.0	606.0	606.2	605.3
0.80	608.0	609.0	616.8	611.8	606.2	607.8	606.0	605.8	618.0	617.2	607.5	608.8
315.20	612.99	611.62	612.01	610.19	609.03	611.47	610.07	611.2	612.28	613.70	614.07	612.3
				TEN	MPERATUR	E OF THE P	BIFILAR MA	GNET.	`			
64.5	64.2	63.5	63.0	62.4	61.6	61.0	60.4	60.0	59.6	59.2	58.9	61.3
67.6	67.4	67.0	66.9	66.4	66.1	66.0	65.7	65.2	65.2	65.0	64.8	64.9
70.8	70.2	70.0	69.2	69.3	68.7		_	_			- }	68.1
			-			66.5	66.3	66.0	65.8	65.5	65 2]	66.5
68.0	67.5	66.6	66.2	66.0	65.7	64.4	63.5	63.0	62.5 59.0	62°1 58°5	61.4 58.2	61.8
64°0	63.8 63.8	63.0 64.0	62.6 63.1	$62^{\circ}0$ $62^{\circ}4$	61.6 61.5	61.2 60.6	$\begin{array}{c} 60.2 \\ 60.2 \end{array}$	59.8 59.8	59°4	29.0	58.2	61.2
67.4	66.2	66.0	65.6	65.5	64.8	64.4	64.0	63.2	63.1	62.7	62.5	64.2
70.6	70.4	69.6	69.4	69.0	68.2	68.1	68.0	67.6	67.0	66.6	66.3	67.7
71.2	71.4	71.0	71.0	70.5	69.5						$\frac{-}{61\cdot 4}$	67.9
64.3					60.7	64.5	63.8	63.3	62.7 58.5	62°3 58°0	57.9	61.8
63.7	63.8	$\begin{array}{c} 63.0 \\ 62.5 \end{array}$	$\begin{array}{c} 62.2 \\ 62.0 \end{array}$	61.6 61.5	61.0	60°3 60°4	59.5 60.0	59.6 59.6	59.5	58.6	58.0	60.9
63.4	63.4	63.4	63.6	62.8	62.4	62.0	61.8	61.5	60.8	60.2	60.3	60.7
80.8	80.4	79.2	78.6	78.2	77.0	76.0	75.5	75.3	74.9	74.3	74.0	74.0
83.3	82.8	81.8	80.8	80.0	79.5	78.2	77.5	77.0	76.2	76.0	75.2	79.2
79.5	78.3	78.0	77.5	77:3	77.0	75.4	75.0	74.5	74.0	73.8	$\frac{-}{73\cdot 6}$	77.1
76.0	75.6	75·5	75.0	74.5	74.3	74.0	73.6	73.2	73.0	72.4	72.2	74.5
74.0	73.5	72.2	72.6	72.2	71.5	70.7	70.2	70.0	69.2	69.0	68.6	72.5
72.6	72.2	71.5	71.3	70.4	69.6	69.5	69.3	68.6	68.5	68.0	67.8	70.0
$71.6 \\ 72.6$	71.0	70.8	70.5	70.3	70.0	69.5	69.0	68.8	68'4 67'8	68°2 67°6	68°1 67°4	69.8 70.0
72.4	71.8 71.7	71°2 70°5	70°6 70°2	70°0 69°8	69.0 69.2	69.1	68.6	68.2	67.8			
		70 3				$\frac{-}{72.4}$	72.1	71.8	71.0	70.6	$\frac{-}{70\cdot 4}\}$	70.4
78.4	77.0	76.0	75.7	75.0	74.2	73.5	73.1	72.9	72.6	72.0	71.6	74.6
76°0 74°1	75.6	75.6	75.3	75.0	74.5	74.2	73.8	73.5	73.3	73.3	73.0	$74.2 \\ 72.7$
74·1 75·1	73.7	73.4	72.8	72.5	72.3	71.5	71.0 71.2	70°5 71°0	70°0 70°7	69.7 69.6	69 . 4	72.4
75.4	74.6	74°1 74°5	74°0 74°6	73.2 74.5	72·4 74·1	72.0 73.7	73.4	73.2	70.7 72.4	71.8	$71.\overline{2}$	73.0
10 4	1 10											
75·4 71·64	75.1	70.22					67.95	67:58	67:12	66.40	66.36	68.9

	Oı	ne Scale Div	rision = '00	0066 parts	of the V.F.		CAL FOR n Scale Div		sponding to	1° decrease	of Tempera	ture, 1°80.	
Mean Gör gen Tim	ottin-}	O ^h .	1 ^h .	2 ^h .	3 հ.	4հ.	$5^{ m h}$.	6 ^h .	7 ^h .	8 ^h •	9հ.	10 ^h .	11 ^h .
	1 2 3	Sc. Div. 183°3 171°0 170°8	Sc. Div. 180°4 171°0 170°9	Sc. Div. 180°4 171°6 170°9	Sc. Div. 179*9 169*9 170*9	Sc. Div. 180°5 169°8 170°3	Sc. Div. 178°7 169°1 168°3	Sc. Div. 179°0 169°6 167°6	Sc. Div. 180°3 171°3 169°9	Sc. Div. 180'3 172'3 172'0	Sc. Div. 180°3 172°3 171°8	Sc. Div. 180°3 171°7 169°8	Sc. Div. 180°3 170°7 169°0
	4 5 6 7 8 9	179.8 175.8 171.1 160.6 167.4 171.4	179.8 176.6 171.1 164.3 167.7 172.2	180°5 175°1 171°6 163°5 170°0 170°5	179°3 174°1 171°3 164°2 169°7 170°6	178 · 4 172 · 4 170 · 4 164 · 9 169 · 7 170 · 6	176.7 170.7 169.9 165.4 169.7 169.3	175.6 170.7 170.1 165.4 169.7	175.6 171.8 171.7 167.8 169.7 167.6	174.5 172.3 172.1 169.2 169.7 170.3	174.2 171.2 170.6 169.2 169.5 169.7	173°1 172°0 169°8 168°5 169°0 170°4	173°1 172°6 169°2 169°5 169°3 170°4
NUARY.	11 12 13 14 15 16 17	178°1 182°0 178°2 172°1 161°9 174°7	175.7 182.8 175.5 172.5 164.1 179.0	178 · 2 183 · 2 179 · 4 173 · 5 164 · 6 180 · 2	178 · 9 183 · 6 178 · 8 170 · 3 164 · 4 178 · 5	178.6 182.0 178.3 166.6 162.5 179.9	178.6 180.6 177.6 166.9 164.9 180.9	178°8 181°6 176°4 167°2 165°5 178°1	179 '4 181 '2 175 '2 166 '7 165 '5 178 '2	178.6 179.6 172.4 164.4 167.7 184.7	179°5 179°6 171°2 162°5 169°0 187°2	179.5 179.6 172.8 162.5 170.5 188.0	179 · 2 179 · 6 171 · 3 161 · 4 169 · 6 187 · 7
64 44 64 64 64 64 64 64 64 64 64 64 64 6	18 19 20 21 22 23 24	193.7 191.1 178.3 181.7 188.4 176.8	193°1 191°1 179°1 180°2 187°8 179°4	193°1 190°0 179°9 183°0 184°9 179°2	193.0 188.9 179.8 182.3 184.8 177.3	192°3 188°9 180°8 182°8 183°1 175°8	189.9 187.1 179.8 184.6 181.7 174.8	188.9 187.1 180.0 182.5 179.7 175.8	189.8 186.6 180.4 188.1 179.7 174.7	189.8 187.7 180.2 187.2 179.7 182.3	188.7 184.7 178.0 186.2 179.7 181.3	185 · 8 181 · 7 176 · 5 184 · 4 179 · 0 179 · 6	184.4 181.3 175.9 183.7 176.7 178.4
	25 26 27 28 29 30 31	170°6 168°5 169°4 169°0 161°7	170.6 167.7 169.3 169.0 161.1 170.6	170.6 168.9 169.3 168.3 161.1 170.7	169.0 170.9 167.9 166.8 160.5 169.5	168.6 172.1 170.2 166.8 159.8 169.6	169°1 172°0 168°5 165°4 158°2 174°9	168.6 172.0 166.4 164.5 158.2 176.5	169 · 2 171 · 3 166 · 4 164 · 5 159 · 8 176 · 5	169°1 170°9 168°1 165°0 160°4 177°3	166°1 170°7 168°1 164°6 159°9 176°3	164.7 169.1 167.1 163.0 159.9 175.6	164.5 168.5 168.4 164.0 160.3 173.9
Hourly M	leans	174.71	174.91	175.27	174.63	174.29	173.83	173.53	174.03	174.77	174.15	173.48	173.07
	1 2	40°0 46°2	40°3 46°4	40°5 46°0	40°7 46°0	40°8 46°2	41°0 46°8	41°0 47°0	40.8 47.0	41°2 47°0	41°6 46°8	41°8 46°8	42°0 47°6
	3 4 5 6 7 8 9 10 11 12 13 14	47.2 42.6 45.2 46.6 51.2 49.0 47.6 — 41.8 40.0 41.8	47.0 42.6 45.6 46.6 50.8 48.8 47.6 41.0 40.0 41.8	47.0 	46.6 	46.6 	46.8	47.4 	47.8	47.8 45.4 47.3 48.2 49.6 48.6 47.6 41.6 46.0	48.0 	48.6 	48.4
JANI	15 16 17 18 19 20 21 22	45.2 50.5 42.0 - 31.6 35.0 41.7 38.3	45.2 50.2 41.6 32.1 35.0 41.3 37.7	46.0 49.6 40.6 	45.0 49.1 40.2 — 33.0 35.5 40.5 38.6	46.4 49.1 39.8 — 33.8 36.2 40.2 39.1	47.0 49.0 39.6 ————————————————————————————————————	47.5 48.7 39.4 — 34.5 37.1 40.7 37.6	47.8 48.6 39.6 35.5 37.6 41.0 37.7	48.5 48.2 38.8 	49°3 47°6 38°8 — 36°3 38°6 42°6 38°6	49.6 47.6 38.4 - 37.6 39.8 42.6 39.0	50°2 47°6 37°8 — 38°6 39°9 42°8 39°7
	23 24 25 26 27 28 29 30	36.0 42.6 46.6 47.3 44.8 48.8 51.3	36·3 41·6 46·6 46·0 45·0 48·8 51·3	37.0 42.6 — 46.6 46.6 45.2 48.9 51.4	36.7 41.6 46.6 45.8 45.0 48.6 51.3	37°3 42°1 — 46°8 45°4 45°4 49°0 51°6	38.7 42.7 — 47.2 45.6 46.4 49.6 52.2	39.8 43.2 — 47.6 45.8 47.2 49.7 52.2	40.0 43.6 48.6 46.6 48.0 50.3 52.4	40.5 43.6 48.6 46.6 47.8 50.3 52.4	41.0 43.8 49.4 47.0 48.4 50.3 52.7	41.7 44.4 	42.2 43.8
Feb.	31 1 Jeans	47.3	46°3 — 43°83	45.3	45.2	$\frac{43.9}{-}$	43.5 — 44.19	43.2	43.3	43.3	43.8	44.0	44.6

	One Scale	Division =	·000066 pa	rts of the V		RTICAL F		orresponding	to 1° decre	ase of Tem _[erature, 1°8	0.
12 ^h .	13 ^h .	14 ^h .	15h.	16 ^h .	17 ^h .	18 ^h .	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div. 170'8	Sc. Div. 167.5	Sc. Div. 165 4	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 177.5	Sc. Div. 176'0	Sc. Div. 176°0	Sc. Div. 173°4	sc. Div. 173'4	Sc. Div. 173°2	Sc. Div. 177 03
169.5	169.5	169.5	169.5	168.4	168.4	168.4	170.0	171.1	172.3	172.3	172.3	170.48
169.0	169.9	170.7	172.2	169.9	171 Q	170.6	179.6	 179 · 4	- 179 · 9	179.9	179.8	172.63
$\frac{-}{172.4}$	173.5	173.7	173.6	172.5	172.5	179 ° 6 172°5	173.7	179 4	175.2	175 9 175 2	175.2	175.23
171.4	173.0	175 1	175.6	175.1	175.3	175.3	168.5	174.3	174.4	172.7	172.7	$173 \cdot 28$
170.2	170.3	169.8	169.8	167.5	167.8	166.7	164.8	164.8	157.1	1551	162.4	168.13
170.0	169.5	169.5	169.2	169.2	169.8	169'8	169.8	168.8	168.8	167°0 169°6	167.2	167.55
169°3 171°7	169°3 172°4	169'3 172'4	170.6 172.5	170°6 173°4	170°6 172°4	170.1	169, 2	169.2	169.7	109 0	170'5	169.56
						180.3	176.7	181'1	176.0	180.2	177.7 }	172.90
178.8	178.8	179.6	179.6	180.0	179.8	180.0	180.0	180.4	180.4	180.4	181.0	179.25
178.2	180.3	183.2	186.6	183.1	179.5	179.5	179.5	179.5	179.5	178'6	177.8	180.86
169°5 162°0	169'8 162'0	171.7 162.5	171°3 162°4	170°5 163°4	170°5 162°7	$170.5 \\ 162.7$	170°0 164°4	171°3 162°7	166.7 162.7	161.9	171.6 161.9	172:77 164:91
170.9	170.9	170.9	172.0	170.2	170.2	171.8	170.4	163.3	163.5	168.6	174.7	167.84
187.7	186.5	186.5	185.8	183.2	183.2	_			_		— _}	185.77
						195.5	196.6	196.3	193.5	193.2	$\frac{-}{193.8}$	
185.7	186.8	188.8	188.8	189.3	190.5	189.3	189.3	190°2 174°6	190°0 178°2	189 ° 9 178 ° 2	189.6 177.6	189 . 61 182.84
181.0 171.9	180°5	179°3 173°2	179°3 171°9	178 · 2 172 · 9	178.6 174.2	177'8 174'5	178°6 175°5	174 6	178 2	$\frac{178.2}{180.2}$	180.2	177.11
182.8	183.5	184.7	183.7	183.7	185.7	185.7	186.4	186.8	188.2	188.5	189.6	184.81
188.6	180.8	180.8	180.3	181.7	181.4	182.3	178.4	165.9	176.9	$168^{\circ}2$	172.3	180.15
178.4	176.5	174.9	173.4	173.2	172.8			171.1	170.0	170.6	170.6	175.56
164.9	164.9	166.0	166.2	166.2	165.5	172 · 9 165 · 5	172°9 167°3	171°1 167°3	170°8 167°9	170 ° 6 167°9	169.1	167.47
168.7	169.2	170.2	170.2	169.4	170.0	170.3	171.1	171.0	171.2	168.4	170.8	170.13
167.6	169.4	167.9	179.2	170.3	174.9	172.2	170.5	172.1	172.1	168.7	170.9	169.79
164.0	164.5	163.9	163.9	165.1	160.5	163.1	161.6	159.7	160.5	160.5	160.8	164.12
158.9	159.0	159.0	159.0	159.3	160.4	157.4	157°1	157.1	160.2	162.5	167.7	159.94
174°9 —	175°5	176°2 —	175'8 —	175°8 —	175.8	191.6	191.4	191.4	190.0	189.5	186.9	178.15
172.92	172.71	173:13	174.07	173:30	173.40	174.92	174.42	174.02	174.01	173.59	174.75	173.99
				TEMPE	RATURE OF	THE VERT	CICAL FORCE	E MAGNET				
42.8	42°6	42.6	43.0	43.0	43.4	43.6	43.1	$4\r3 \cdot 5$	44.0	$4\overset{\circ}{4}$. 6	45.4	$4\overset{\circ}{2} \cdot 22$
47.6	48.2	47.8	47.6	48.2	48.4	48.1	47.6	47.2	46.8	46.6	47.0	47.12
48.6	48.4	48.6	48.4	48'4	48.5	40.0	40.0	40:0	40:4	40:4	$\left\{\begin{array}{c} -1 \\ 42.8 \end{array}\right\}$	46.41
46.7	46.8	46.7	46.9	46.8	46.8	42°0 46°7	42.0 46.4	$\begin{array}{c} 42.2 \\ 45.6 \end{array}$	42.4 45.2	42.4 45.0	45.2	45.15
47.0	47.0	46.6	46.6	46.4	46.0	45.8	46.1	46.5	46.4	46.6	46.4	46.42
48.8	49.2	49.5	49.8	50.1	50.3	50.6	50.1	50.2	50.7	50.9	51.0	48.87
48.8	49.0	49.0	49.2	48.8	48.6	48.6	48.7	49.0	49.2	49'1	49.0	49.38
49°0 46°2	48.6	48.2	48.4	48.4 46.0	48°4 45°8	48.4	48.4	48.3	48.5	48.3	48.0	48.45
-	46.4	46.0	46.0	40 0		40.8	40.8	40.8	40.8	41.2	40.8	45.37
42.6	42.6	42.4	42.2	42.2	42.0	42.0	41'1	41'1	41.0	40.6	40.2	41.84
42.6	42.8	43.2	42.6	42.0	42.0	42.2	42.4	42.4	42.4	42.4	42.4	41.62
47°5 50°5	46.8	47.0	47.5	47.6	47.6	47.2	47.0	46.4	46.2	46.0	45.2 50.5	45°46 48°94
47.2	50.6 47.0	50.6 46.8	50.6 45.7	50°5 45°6	50.4 45.2	50°3 44°9	50°3 44°2	50.7 43.8	50°9 43°6	51.0 42.6	42.5	46.87
36.6	37.6	36.9	36.9	37.0	37.0			_				37.00
			_			30.9	30.8	31.3	31.8	31.9	31:7}	
38.5	37.4	36.8	36.9	36.3	36.3	35.9	35.9	35.6	35.4	35.5	35.1	35.43
39 · 9	40.5	40.8	41.1	41.0	41.4	41.6 41.8	$\begin{array}{c} 41.5 \\ 41.2 \end{array}$	41.5 40.2	41.6 39.7	41.6 39.3	41.6 38.8	39°12 41°84
39.4	45.6 39.0	44.6 38.7	44.8 38.2	44.1 38.0	42.8 37.7	37.3	36.6	36.4	36.0	35.8	35.8	37.93
42.8	42.6	42.4	41.8	41.2	40.8	40.6	40.2	40.8	41.2	41.6	41.8	40.22
43.6	43.6	44.2	45.0	45.2	45.4	4	_		4014	40.5	$\frac{-}{46.5}$	44.15
20.0	40:5	40:0	40:1	40:0	40:4	45.7	45.5	46.1	46.4 48.4	46.7 48.0	46.5 } 47.5	48.39
46.6	49°5 46°1	49.6 46.2	49°1 45°7	48.8 46.5	49.4 46.5	49.5 46.2	48.7 45.8	48.6 45.8	48 4 45 7	48 0	47.5	48 39
49.0	49.5	49.5	49.2	49.3	49.3	49.2	48.8	48.2	47.8	48.8	49.3	47.84
50.0	50.0	49.8	50.4	50.4	50.4	50.2	51.0	51.3	51.3	51'6	51.6	50.14
53.5	53.4	53.4	53.7	53.7	52.9	52.3	51.3	50.7	50.2	49.5	48.4	52.02
44.6	44.4	44.0	43.5	43.5	43.4	32.6	33.0	33.2	34.0	34.5	35.0}	41.64
		l	l		1		l					

	On	e Scale Divi	ision = •00	0065 parts o	f the V. F.		CAL FORC n Scale Div		sponding to	1° decrease	of Tempera	ture, 1 •80.	
Mean G gen T	öttin- }	Oh.	1 ^h .	2h.	3h.	4h.	5 ^h .	6 ^h •	7 ^h .	8h.	9 ^h .	10 ^h .	11 ^h .
	7 2 3 4 5 6 7	sc. Div. 184'8 177'2 171'6 167'0 166'1 165'9	sc. Div. 187.3 177.2 172.7 167.0 166.8 166.8	sc. Div. 188'3 176'7 170'8 167'3 167'5 169'4	sc. Div. 188.5 173.7 167.3 164.7 164.5 166.3	sc. Div. 188.5 173.3 166.2 162.5 163.5 164.5	sc. Div. 188.8 172.7 164.9 163.3 162.1 163.7	sc. Div. 188 1 171 8 165 9 164 2 163 2 164 2	.Sc. Div. 187 · 2 170 · 6 167 · 3 163 · 9 163 · 7 161 · 6	Sc. Div. 186.0 170.3 168.1 163.9 163.7 164.1	sc. Div. 186.2 169.5 170.3 162.5 162.8 164.6	sc. Div. 184.0 168.3 169.7 162.5 161.7 165.6	sc. Div 183°1 167°6 169°7 164°0 162°7 165°6
JARY.	8 9 10 11 12 13 14	188.6 194.1 180.7 181.1 175.5 171.0	189 8 195 0 179 7 182 8 175 7 171 6	190°0 194°6 179°9 185°0 174°8 173°9	184.0 193.4 179.9 181.9 177.1 174.0	189.6 191.5 180.2 181.7 175.2 173.0	189.6 190.8 178.4 181.7 174.5 171.4	190°5 191°5 177°8 181°3 173°2 171°4	190°4 190°2 177°1 179°6 172°3 169°8	191°1 188°4 177°1 179°6 171°0 170°2	190.6 187.1 178.7 178.5 170.0 169.9	189 ° 9 186 ° 7 176 ° 8 177 ° 3 169 ° 5 169 ° 2	190°6 186°7 175°9 178°6 169°5 171°0
FEBRUARY	15 16 17 18 19 20 21 22	169°3 175°3 173°0 176°6 180°8 170°6	166.0 175.2 176.0 178.6 181.4 170.5	173°4 174°5 175°3 180°0 178°7 169°8	172 · 4 173 · 9 171 · 9 179 · 1 178 · 9 168 · 4	171.6 172.4 169.4 177.6 176.2 167.8	171.7 169.5 169.4 176.0 175.6 166.5	173.8 169.2 169.4 176.0 175.6 166.1	173.6 168.5 171.0 176.3 175.3 165.8	177.2 170.0 170.3 176.7 175.3 166.4	178°3 170°1 170°6 176°8 172°6 166°9	176°2 170°6 171°3 177°5 170°5 167°8	176.4 170.6 170.3 178.0 170.5 169.0
Marc	23 24 25 26 27 28	183.7 180.3 182.0 186.8 198.8 183.0	184.5 182.2 183.9 189.8 198.9 184.7	184'3 182'2 183'9 193'6 199'5 185'2	177.7 181.9 182.7 175.9 192.9 185.6	178.6 180.4 181.0 185.5 194.3 185.2	178.6 180.4 181.0 184.8 192.0 184.7	177.1 178.8 179.9 185.7 189.9 183.7	177.6 176.2 179.9 185.7 186.0 183.3	178°3 176°2 180°0 185°7 187°2 182°4	177.0 176.0 180.0 188.8 185.9 182.7	178°3 175°6 181°0 188°8 185°9 182°3	178.4 177.0 182.9 189.7 185.2 180.3
Hourly	y Means	178.49	179.34	179.94	177:36	177.07	176.34	176.18	175.24	175.80	175.68	175.29	175.5
			····		TEMPERAT	URE OF TH	IE VERTICA	AL FORCE I	MAGNET.		·——·		
JARY.	2 3 4 5 6 7 8 9 10 11 12 13 14	35.6 42.6 46.6 48.6 49.4 49.0 — 33.8 33.8 40.2 40.0 43.3 46.8	35:4 42:8 46:6 48:4 49:1 48:6 33:8 33:6 41:4 39:5 43:4 45:4	35.0 43.2 49.0 48.8 48.6 48.8 — 34.2 33.6 41.0 40.0 43.4 44.8	35.0 43.9 47.5 49.4 48.7 48.4 — 34.4 33.6 41.1 40.0 43.4 43.5	35.6 44.0 48.4 50.3 48.9 49.0 35.2 33.7 41.1 40.2 43.5 43.6	36·2 44·5 48·6 50·4 49·8 - 35·0 34·0 41·9 40·4 44·0 44·3	37.0 45.2 48.6 50.4 49.5 50.1 - 34.9 34.8 42.6 40.8 45.0 44.6	37.9 45.1 48.6 50.6 50.0 50.3 34.5 35.6 43.0 41.3 45.6 45.6	38.5 45.9 48.6 50.6 50.5 50.0 	\$\\ \frac{39.0}{46.7}\$ 48.8 51.0 51.0 49.7 	39.8 47.6 48.6 51.0 51.3 49.9 	39'8 47'8 48'0 50'7 51'3 49'6 - 36'1 37'4 43'4 42'5 47'6 46'7
FEBRUARY.	15 16 17 18 19 20 21 22 23	42.0 43.8 44.7 42.4 41.4 46.8 38.2	42°3 43°6 43°9 41°8 41°6 46°6 — 37°8	42·3 43·4 44·7 41·3 41·3 46·6 — 37·6	42·2 43·9 44·8 41·2 41·5 46·6	43.6 44.4 45.4 41.6 41.5 46.8 — 39.6	44.0 45.5 45.8 41.8 42.1 48.0 — 39.8	44·4 46·2 46·6 42·6 42·7 48·5 — 40·4	44.6 46.6 46.8 43.0 42.8 48.8 —	44.6 46.6 47.0 43.0 43.4 48.5 —	44.6 47.0 47.4 43.0 44.6 48.2 — 41.0	44.8 47.4 47.6 42.9 45.0 48.4 —	44.6 47.0 47.8 42.4 45.7 47.8 —
Mar	24 25 26 27 28	39.4 39.8 37.2 31.2 40.0	39·2 38·8 36·3 30·5 39·5	39.4 38.8 36.8 31.0 38.4	38.8 38.6 44.0 34.1 38.3	38 · 9 39 · 0 37 · 9 32 · 1 38 · 5	39 8 39 4 39 2 37 8 33 1 39 4	40.7 39.8 38.0 34.6 40.0	41.5 40.5 38.0 36.5 40.0	42.2 40.6 38.0 37.6 40.1	42.6 41.0 38.1 38.2 40.6	42.6 41.5 38.0 38.3 40.8	42:2 41:1 37:3 38:1 41:0
Hourl	y Means	41.53	41.25	41.33	41.81	41.78	42.26	42.83	43.24	43.21	43.92	44.18	44.0

											23h.	Daily ar
12h.	13h.	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18 ^h •	19 ^h .	20 ^h .	21h.	22h.	25"•	Monthl Means
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
	i .			1	[.		177.8	177.7	176.3	175'8	174.8	183.1
83.1	183.1	182.4	182.3	181.0	179.6	179.6	168.8	168.8	168.0	167.7	168.8	170.1
68.0	167.6	167.6	166.7	167.6	167.6	167.6		170.1	170.1	170.0	163.2	168.8
69.7	169.1	169.6	169'1	168.5	169'4	169.4	170.3	163.8	163.8	164.2	165.3	164.5
63.7	164.0	164.0	164.8	163.8	163.8	164.1	163.8		166.5	161.8	164 1	164.5
64.2	163.9	163.9	163.9	165.2	165'1	164'6	164.6	165.7	100 2	101 0		
65.9	165.9	166.9	169.5	170.9	171.3	150.0	100:0	100:0	184.4	184.4	$\frac{-186\cdot3}{186\cdot3}$	170.3
_						179.6	180.3	180.8		194.8	193.1	190.9
91.3	192.5	191.4	191'3	191.3	191.6	192.9	192.8	192.8	192.8	181.0	181.0	187.4
86.2	186.2	184.4	184.7	185.8	186.2	184.5	184.0	183.1	181'9		180.6	179.3
77.0	179.0	179.5	181.7	181.1	180.9	180.7	180.7	180.7	180.4	179.6		180.1
79.9	181.3	181.3	181.3	181.3	181.3	178.4	179.9	179.2	178.9	176'3	175.4	
69.5	171.6	170.0	167.9	172.2	171.4	169.7	170.7	170.6	170'8	168.3	170.9	171.7
73.9	174.8	172.8	174.7	173.1	170.9						$\frac{-}{174\cdot 4}$	172.3
	l		—		·	172.5	167.1	171.3	177.5	178.0		1 17 4 1 17
78.5	178.4	176.3	176.1	177.8	175.8	175.8	174.7	175.5	175.2	174.8	175.3	174.7
71.5	171.5	172.4	172.4	172.2	172.2	170.3	170.5	170.5	172.9	172.9	173.0	171.7
70.3	170.2	171.0	170.5	170.2	171.0	172.6	172.6	172.6	175.3	176.9	177.2	172.0
80.3	179.6	179.6	182.9	182.9	182.9	181.2	179.3	179.3	179.2	179.3	179.3	178.9
71.3	170.0	171.7	171.7	171.3	171.3	167.7	169.8	170.2	170.2	170'2	170.7	173.2
69.4	168.7	168.7	168.8	170.8	170.8						$\frac{1}{183\cdot 7}$	171.1
	100			-,		179.0	174.7	177.4	176.4	182.8	183.7	
78.3	178.3	178.3	179.6	179.6	179.3	180.5	180.0	180.0	180.3	180.3	180.3	179.5
77.3	179.4	179.4	179.0	179.5	179.5	180.3	180.3	180.3	181.3	182.0	181.6	179.4
92.4	192.4	198.2	193.1	186.2	184.6	184.0	181.9	182.1	184.3	182.6	184.7	184'3
89.7	190.3	190.3	190.9	190.0	187.6	188.0	189.1	189.8	191.4	191.6	195.8	188.5
85.0	182.7	180.2	179.7	181.4	180.2	180.3	179.4	179.0	179.7	181.5	182.1	186.1
81.9	181.8	181.8	180.9	181.2	181.2					-	— 7	185 1
	_	—	_	-	_	193.6	191.2	191.2	190.5	190.2	193.8}	100 1
76.60	176.76	176.75	176.81	176.91	176.50	177:37	176.85	177'19	177.83	177.80	178.14	177.0
				TEMPE	RATURE OF					0	0	0
_	0	0	0	0	0	0	0	° 42.2	。 42 · 0	42.4	42.4	39.1
0	1	4043	40.5									09 1
39.8	40.0	40.1	40.5	40.6	41.4	41.4	41.6		46.6			
39°8 47°8	40°0 48°0	48.0	47.8	47.8	47.8	47.4	47.4	47.0	46.6	46.8	46.6	46'1
39.8 47.8 47.8	40°0 48°0 47°8	48.0 47.6	47.8 47.6	47.8 47.6	47.8 47.6	47·4 47·4	47.4 47.2	47.0 47.3	47.5	46'8 47'5	46.6 47.6	46°1 47°8
39.8 47.8 47.8 50.4	40°0 48°0 47°8 50°4	48°0 47°6 50°3	47.8 47.6 50.3	47.8 47.6 50.5	47.8 47.6 50.7	47°4 47°4 50°8	47.4 47.2 50.3	47.0 47.3 50.2	47.5 50.5	46.8 47.5 50.3	46.6 47.6 49.7	46°1 47°8 50°1
39.8 47.8 47.8 50.4 50.9	40°0 48°0 47°8 50°4 50°9	48.0 47.6 50.3 50.7	47.8 47.6 50.3 50.3	47.8 47.6 50.5 50.3	47.8 47.6 50.7 50.3	47.4 47.4 50.8 50.3	47.4 47.2	47.0 47.3 50.2 50.0	47.5 50.5 49.7	46.8 47.5 50.3 49.5	46.6 47.6 49.7 49.2	46.1 47.8 50.1 50.0
39.8 47.8 47.8 50.4 50.9 49.4	40°0 48°0 47°8 50°4	48°0 47°6 50°3	47.8 47.6 50.3 50.3 48.3	47.8 47.6 50.5 50.3 47.5	47.8 47.6 50.7 50.3 46.6	47.4 47.4 50.8 50.3	47.4 47.2 50.3 50.3	47.0 47.3 50.2 50.0	47.5 50.5 49.7	46.8 47.5 50.3 49.5	46.6 47.6 49.7 49.2	46.1 47.8 50.1 50.0
39.8 47.8 47.8 50.4 50.9 49.4	40.0 48.0 47.8 50.4 50.9 49.4	48.0 47.6 50.3 50.7 49.0	47.8 47.6 50.3 50.3 48.3	47.8 47.6 50.5 50.3 47.5	47.8 47.6 50.7 50.3 46.6	47.4 47.4 50.8 50.3 — 33.5	47.4 47.2 50.3 50.3 - 34.0	47.0 47.3 50.2 50.0 — 34.2	47.5 50.5 49.7 — 34.6	46.8 47.5 50.3 49.5 — 35.0	$ \begin{array}{c} 46.6 \\ 47.6 \\ 49.7 \\ 49.2 \\ \hline 33.0 \end{array} $	46°1 47°8 50°1 50°0 45°3
39.8 47.8 47.8 50.4 50.9 49.4 — 35.6	40.0 48.0 47.8 50.4 50.9 49.4 — 35.4	48.0 47.6 50.3 50.7 49.0 — 35.5	47.8 47.6 50.3 50.3 48.3 — 35.3	47.8 47.6 50.5 50.3 47.5 — 35.2	47.8 47.6 50.7 50.3 46.6 — 35.0	47.4 47.4 50.8 50.3 — 33.5 34.7	47.4 47.2 50.3 50.3 — 34.0 34.2	47.0 47.3 50.2 50.0 — 34.2 33.8	47.5 50.5 49.7 — 34.6 34.0	46.8 47.5 50.3 49.5 — 35.0 34.0	46.6 47.6 49.7 49.2 	46°1 47°8 50°1 50°0 45°3 34°7
39.8 47.8 47.8 50.4 50.9 49.4 35.6 37.4	40.0 48.0 47.8 50.4 50.9 49.4 — 35.4 37.6	48.0 47.6 50.3 50.7 49.0 35.5 38.3	47.8 47.6 50.3 50.3 48.3 — 35.3 38.2	47.8 47.6 50.5 50.3 47.5 — 35.2 38.0	47.8 47.6 50.7 50.3 46.6 — 35.0 38.0	47.4 47.4 50.8 50.3 — 33.5 34.7 38.4	47.4 47.2 50.3 50.3 — 34.0 34.2 39.4	47.0 47.3 50.2 50.0 — 34.2 33.8 40.0	47.5 50.5 49.7 — 34.6 34.0 40.0	46.8 47.5 50.3 49.5 — 35.0 34.0 40.3	46.6 47.6 49.7 49.2 	46°1 47°8 50°1 50°0 45°3 34°7 36°9
39.8 47.8 47.8 50.4 50.9 49.4 — 35.6 37.4 43.0	40.0 48.0 47.8 50.4 50.9 49.4 — 35.4 37.6 42.5	48.0 47.6 50.3 50.7 49.0 - 35.5 38.3 41.6	47.8 47.6 50.3 50.3 48.3 ————————————————————————————————————	47.8 47.6 50.5 50.3 47.5 — 35.2 38.0 40.9	47.8 47.6 50.7 50.3 46.6 — 35.0 38.0 41.2	47.4 47.4 50.8 50.3 — 33.5 34.7 38.4 41.2	47.4 47.2 50.3 50.3 - 34.0 34.2 39.4 41.1	47.0 47.3 50.2 50.0 — 34.2 33.8 40.0 40.9	47.5 50.5 49.7 	46.8 47.5 50.3 49.5 — 35.0 34.0 40.3 40.9	46.6 47.6 49.7 49.2 	46°1 47°8 50°1 50°0 45°3 34°7 36°9 41°6
39·8 47·8 47·8 50·4 50·9 49·4 — 35·6 37·4 43·0 42·2	40.0 48.0 47.8 50.4 50.9 49.4 - 35.4 37.6 42.5 42.2	48.0 47.6 50.3 50.7 49.0 35.5 38.3 41.6 41.7	47.8 47.6 50.3 50.3 48.3 — 35.3 38.2 41.1 41.5	47.8 47.6 50.5 50.3 47.5 — 35.2 38.0 40.9 41.6	47.8 47.6 50.7 50.3 46.6 — 35.0 38.0 41.2 41.6	47.4 47.4 50.8 50.3 — 33.5 34.7 38.4 41.2 42.0	47.4 47.2 50.3 50.3 — 34.0 34.2 39.4 41.1 42.3	47.0 47.3 50.2 50.0 — 34.2 33.8 40.0 40.9 42.5	47.5 50.5 49.7 	46.8 47.5 50.3 49.5 	46.6 47.6 49.7 49.2 	46.1 47.8 50.1 50.0 45.3 34.7 36.9 41.6 41.6
39.8 47.8 47.8 50.4 50.9 49.4 	40.0 48.0 47.8 50.4 50.9 49.4 — 35.4 37.6 42.5 42.2 48.3	48.0 47.6 50.3 50.7 49.0 35.5 38.3 41.6 41.7 48.2	47.8 47.6 50.3 50.3 48.3 — 35.3 38.2 41.1 41.5 47.6	47.8 47.6 50.5 50.3 47.5 — 35.2 38.0 40.9 41.6 47.7	47.8 47.6 50.7 50.3 46.6 — 35.0 38.0 41.2 41.6 47.6	47.4 47.4 50.8 50.3 33.5 34.7 38.4 41.2 42.0 47.8	47.4 47.2 50.3 50.3 - 34.0 34.2 39.4 41.1	47.0 47.3 50.2 50.0 	47.5 50.5 49.7 34.6 34.0 40.0 40.9 42.7 47.0	46.8 47.5 50.3 49.5 	46.6 47.6 49.7 49.2 	46.1 47.8 50.1 50.0 45.3 34.7 36.9 41.6 41.6
39.8 47.8 47.8 50.4 50.9 49.4 	40.0 48.0 47.8 50.4 50.9 49.4 - 35.4 37.6 42.5 42.2	48.0 47.6 50.3 50.7 49.0 35.5 38.3 41.6 41.7	47.8 47.6 50.3 50.3 48.3 — 35.3 38.2 41.1 41.5	47.8 47.6 50.5 50.3 47.5 — 35.2 38.0 40.9 41.6 47.7 45.6	47.8 47.6 50.7 50.3 46.6 — 35.0 38.0 41.2 41.6 47.6 45.3	47.4 47.4 50.8 50.3 — 33.5 34.7 38.4 41.2 42.0 47.8	47.4 47.2 50.3 50.3 - 34.0 34.2 39.4 41.1 42.3 47.4	47.0 47.3 50.2 50.0 — 34.2 33.8 40.0 40.9 42.5 47.4	47.5 50.5 49.7 — 34.6 34.0 40.0 40.9 42.7 47.0	46.8 47.5 50.3 49.5 — 35.0 34.0 40.3 40.9 43.1 46.7	46.6 47.6 49.7 49.2 	46.1 47.8 50.1 50.0 45.3 34.7 36.9 41.6 41.6
39.8 47.8 47.8 50.4 50.9 49.4 35.6 37.4 43.0 42.2 47.7 46.6	40.0 48.0 47.8 50.4 50.9 49.4 — 35.4 37.6 42.5 42.2 48.3 46.5	48.0 47.6 50.3 50.7 49.0 — 35.5 38.3 41.6 41.7 48.2 45.9	47.8 47.6 50.3 50.3 48.3 — 35.3 38.2 41.1 41.5 47.6 45.8	47.8 47.6 50.5 50.3 47.5 — 35.2 38.0 40.9 41.6 47.7 45.6	47.8 47.6 50.7 50.3 46.6 — 35.0 38.0 41.2 41.6 47.6 45.3 —	47.4 47.4 50.8 50.3 — 33.5 34.7 38.4 41.2 42.0 47.8 — 40.0	47.4 47.2 50.3 50.3 - 34.0 34.2 39.4 41.1 42.3 47.4 - 40.2	47.0 47.3 50.2 50.0 — 34.2 33.8 40.0 40.9 42.5 47.4 — 40.4	47.5 50.5 49.7 — 34.6 34.0 40.0 40.9 42.7 47.0 — 41.0	46.8 47.5 50.3 49.5 — 35.0 34.0 40.3 40.9 43.1 46.7 — 41.4	46.6 47.6 49.7 49.2 	46.1 47.8 50.1 50.0 45.3 34.7 36.9 41.6 41.6 46.2 44.4
39.8 47.8 47.8 50.4 50.9 49.4 35.6 37.4 43.0 42.2 47.7 46.6 44.4	40.0 48.0 47.8 50.4 50.9 49.4 — 35.4 37.6 42.5 42.2 48.3 46.5 — 44.6	48.0 47.6 50.3 50.7 49.0 — 35.5 38.3 41.6 41.7 48.2 45.9 — 44.2	47.8 47.6 50.3 50.3 48.3 — 35.3 38.2 41.1 41.5 47.6 45.8 — 43.8	47.8 47.6 50.5 50.3 47.5 — 35.2 38.0 40.9 41.6 47.7 45.6 — 43.6	47.8 47.6 50.7 50.3 46.6 — 35.0 38.0 41.2 41.6 47.6 45.3 — 43.4	47.4 47.4 50.8 50.3 — 33.5 34.7 38.4 41.2 42.0 47.8 — 40.0 43.2	47.4 47.2 50.3 50.3 34.0 34.2 39.4 41.1 42.3 47.4 40.2 43.3	47.0 47.3 50.2 50.0 — 34.2 33.8 40.0 40.9 42.5 47.4 — 40.4 43.5	47.5 50.5 49.7 34.6 34.0 40.0 40.9 42.7 47.0 41.0 43.6	46.8 47.5 50.3 49.5 — 35.0 34.0 40.3 40.9 43.1 46.7 — 41.4 43.6	46.6 47.6 49.7 49.2 	46.1 47.8 50.1 50.0 45.3 34.7 36.9 41.6 46.2 44.4 43.7
39.8 47.8 47.8 50.4 50.9 49.4 	40.0 48.0 47.8 50.4 50.9 49.4 	48.0 47.6 50.3 50.7 49.0 — 35.5 38.3 41.6 41.7 48.2 45.9 — 44.2 46.2	47.8 47.6 50.3 50.3 48.3 — 35.3 38.2 41.1 41.5 47.6 45.8 — 43.8 45.8	47.8 47.6 50.5 50.3 47.5 — 35.2 38.0 40.9 41.6 47.7 45.6 — 43.6 45.9	47.8 47.6 50.7 50.3 46.6 — 35.0 38.0 41.2 41.6 47.6 45.3 — 43.4 45.7	47.4 47.4 50.8 50.3 33.5 34.7 38.4 41.2 42.0 47.8 40.0 43.2 45.6	47.4 47.2 50.3 50.3 34.0 34.2 39.4 41.1 42.3 47.4 40.2 43.3 45.2	47.0 47.3 50.2 50.0 — 34.2 33.8 40.0 40.9 42.5 47.4 — 40.4 43.5 45.0	47.5 50.5 49.7 34.6 34.0 40.0 40.9 42.7 47.0 41.0 43.6 45.2	46.8 47.5 50.3 49.5 — 35.0 34.0 40.3 40.9 43.1 46.7 — 41.4 43.6 45.5	46.6 47.6 49.7 49.2 — 33.0 40.6 40.1 43.5 46.8 — 41.6 43.6 45.0	46.1 47.8 50.1 50.0 45.3 34.7 36.9 41.6 46.2 44.4 43.7 45.5
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39.8 47.8 47.8 50.4 50.9 49.4 35.6 37.4 44.4 46.8 47.6 41.7 46.7 37.0 38.3	40.0 48.0 47.8 50.4 50.9 49.4 	48.0 47.6 50.3 50.7 49.0 — 35.5 38.3 41.6 41.7 48.2 45.9 — 44.2 47.6 41.4 47.1 47.4 — 41.0 41.6 40.0 36.2 40.0	47.8 47.6 50.3 50.3 48.3 — 35.3 38.2 41.1 41.5 47.6 45.8 45.8 46.8 41.5 47.0 47.2 — 41.2 41.0 40.0 36.0 40.0	47.8 47.6 50.5 50.3 47.5 35.2 38.0 40.9 41.6 47.7 45.6 41.2 46.8 47.0 40.8 40.6 40.0 35.3 40.0	47.8 47.6 50.7 50.3 46.6 — 35.0 38.0 41.2 41.6 45.3 — 43.4 45.7 46.6 41.2 47.0 47.0 47.0 40.8 40.3 40.0 34.6 40.2	47.4 47.4 50.8 50.3 	47.4 47.2 50.3 50.3 34.0 34.2 39.4 41.1 42.3 47.4 	47.0 47.3 50.2 50.0 34.2 33.8 40.0 40.9 42.5 47.4 40.4 43.5 45.0 44.5 41.4 47.5 	47.5 50.5 49.7 34.6 34.0 40.0 40.0 42.7 47.0 	46.8 47.5 50.3 49.5 — 35.0 34.0 40.3 40.9 43.1 46.7 — 41.4 43.6 45.5 43.1 41.8 47.4 — 38.2 39.8 40.0 38.3 32.0 40.0	46.6 47.6 49.7 49.2	46.1 47.8 50.1 50.0 45.3 34.7 36.9 41.6 46.2 44.4 43.7 45.5 45.8 41.8 44.9 45.2 40.1 40.6 39.7 36.2 37.2

	0:	ne Scale Div	rision = '00	0065 parts o	of the V. F.		CAL FORC n Scale Divi		sponding to	1° decrease	of Temperat	ure, 1°80.	
Mean G	Göttin-}	O ^h •	1 ^h .	2 ^h .	3 ^h .	4 ^h •	5 ^h •	6 ^h .	7 ^h .	8h.	9 ^h •	10h.	11 ^h .
	7 2 3 4 5 6 7 8	sc. Div. 193 *8 182 *2 174 *8 166 *6 165 *6 172 *6	sc. Div. 193 ° 6 183 ° 5 173 ° 7 166 ° 6 165 ° 4 173 ° 6	Sc. Div. 191 ° 0 182 ° 2 173 ° 4 165 ° 0 165 ° 4 173 ° 1	Sc. Div. 186 ' 7 180 ' 6 170 ' 7 163 ' 3 163 ' 1 171 ' 2	Sc. Div. 183 ' 9 176 ' 2 167 ' 0 161 ' 9 162 ' 6 168 ' 6	Sc. Div. 181 ° 0 173 ° 5 165 ° 5 158 ° 8 163 ° 7 167 ° 7	Sc. Div. 181 ° 0 172 ° 1 165 ° 4 157 ° 5 163 ° 3 167 ° 7	Sc. Div. 180 ° 0 171 ° 5 · 165 ° 3 158 ° 5 163 ° 0 166 ° 8	Sc. Div. 179°4 170°3 165°8 160°1 162°7 168°8	Sc. Div. 179°4 170°9 164°7 159°7 162°2 169°5	sc. Div. 179 ° 6 171 ° 4 164 ° 1 157 ° 9 162 ° 3 169 ° 5	Sc. Div. 178 2 170 0 165 9 157 6 161 5 170 6
	8 9 10 11 12 13 14 15	167.0 159.3 166.2 161.3 155.1 150.2	167.3 162.9 166.3 160.0 150.2 150.7	168.0 162.9 163.4 159.9 146.7 156.9	166.8 161.8 163.8 158.8 148.4 153.8	162.6 158.5 156.7 157.7 148.6 159.3	159.8 156.5 153.9 157.7 149.8 158.9	160°4 157°1 153°2 157°1 151°3 158°7	161·1 157·1 154·3 157·5 157·0 160·8	160.6 157.7 156.1 157.5 158.2 164.5	160°0 157°9 157°0 157°5 158°8 161°1	160°0 157°9 155°7 158°9 162°1 163°7	159°5 157°8 154°7 158°0 168°7 163°7
MARCH.	16 17 18 19 20 21 22	169.9 168.8 169.3 156.7 159.7 160.2	171.5 159.6 170.9 155.5 159.1 160.2	168.4 162.3 170.9 159.7 159.1 162.1	167.7 167.2 173.3 159.3 156.4 161.6	168.4 169.8 170.5 158.6 154.5 162.3	168°4 170°7 167°4 156°3 153°4 161°8	168°1 172°2 167°4 155°0 153°4 161°8	168.8 169.6 167.9 154.9 154.1 161.8	171 · 9 171 · 7 166 · 6 153 · 9 155 · 1 163 · 7	179 ° 7 173 ° 5 165 ° 1 154 ° 3 155 ° 1 164 ° 0	179°5 174°4 163°4 155°4 155°3 162°5	179'9 167'5 164'4 156'6 156'0 162'5
	23 24 25 b 26 27	169°9 158°1 162°4 —	169°9 159°2 162°4 —	168.0 160.3 162.4	164.2 159.5 160.8	166'9 158'5 159'2 —	159.0 159.7 	158°1 160°0	157°1 159°7 —	158°3 160°6 —	158'9 161'2 — —	159°3 160°1 —	159°3 161°5 —
	28 29 30 31								_ _ _			_ _ _	
Hourly	Means	166.32	165.98	165.94	164.91	163.70	162.17	162.04	162.34	163.18	163.52	163.65	163.69
		34.0	0000	35.0	36.6		HE VERTIC	40.0	40.6	.0	.0	.0	0
	$\left(egin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{array} ight)$	34.0 40.2 44.6 48.8 49.7 44.7	34·2 39·8 44·0 48·4 49·3 44·5	35.0 40.0 44.6 49.2 49.2 44.6	36.6 40.8 45.6 49.2 49.5 44.9	38·2 42·0 47·3 49·6 49·5 46·0	38.7 43.4 48.1 50.3 49.1 46.7	40.0 44.0 48.2 50.6 49.6 46.7	40.6 44.6 48.0 51.3 49.7 46.7	41.0 45.2 48.1 51.3 49.9 46.7	41.6 45.7 48.8 51.9 50.5 46.8	41.8 46.2 49.2 53.2 50.8 46.8	42.0 45.8 49.1 53.3 50.5 46.6
	8 9 10 11 12 13 14	47.5 50.6 49.0 51.5 54.6 54.9	47.4 49.4 48.6 51.6 54.6 54.5	47°3 49°6 49°7 51°5 54°4 54°1	47.6 50.3 50.0 51.8 54.0 54.3	48.8 51.5 51.7 52.6 54.0 54.3	50.0 52.3 52.2 52.8 54.3 54.5	50°0 52°6 53°2 53°0 54°6 54°5	50.6 52.4 53.7 53.1 55.2 54.7	51.0 52.4 53.7 53.5 55.2 54.7	51.6 52.7 53.9 53.6 55.0 55.1	51.9 53.1 54.4 53.5 54.6 54.8	52.0 53.3 54.5 53.7 55.3 54.3
MARCH.	15 16 17 18 19 20 21 22	46.8 45.4 44.9 53.3 53.2 52.7	46.8 44.3 44.6 53.3 52.5 52.3	47.2 44.1 44.6 53.1 52.6 51.5	46.7 43.7 45.0 53.4 53.6 51.1	46.8 43.6 45.9 54.1 50.6	46.7 43.9 47.2 54.3 54.6 50.6	46.9 44.2 47.7 54.9 55.0 50.3	47.0 45.5 48.2 55.5 50.2	47.4 45.8 48.7 55.6 55.7 50.2	47.6 47.0 50.4 56.1 56.5 50.4	47.6 48.2 51.1 56.2 56.4 51.1	47.6 49.4 51.1 56.0 56.3 51.7
	22 23 24 25 ^b 26 27 28 29 30	47.4 52.0 51.7 ————————————————————————————————————	47.5 52.0 51.2 ————————————————————————————————————	48.2 51.9 50.8 — — —	48.9 51.8 50.6 — — —	50.0 51.6 50.7 — — —	50.6 51.5 	51·2 51·8 — — — — —	51·5 51·9 — — — — —	51.7 52.0 — — — — —	53.0 52.0 — — — — —	52·4 52·0 — — — — — —	52·2 52·0 — — — —
	31												
	Means	48.29	47.98	48.12	48.44	49.11	49.59	49.95	50.29	50.49	51.01	51.27	51.3

^a Three minutes late.

^b This day not included in the Sums and Means.

	One Scale	Division =	· 000065 par	ts of the V.		RTICAL E		orresponding	to 1° decre	ase of Tem	perature, 1°8	0.
12h.	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18h.	19h.	20h.	21h.	22h.	23h.	Daily and Monthly Means.
sc. Div. 178 2 170 4 165 9 157 3 163 3 169 9	sc. Div, 178 2 170 4 165 9 157 6 163 4 168 9	Sc. Div. 176 8 170 4 163 5 157 6 162 7 168 9	sc. Div. 176 · 8 170 · 9 162 · 8 157 · 2 163 · 0 167 · 9	Sc. Div. 176 '7 170 '9 164 '3 a 160 '3 163 '0 167 '9	Sc. Div. 177.6 172.5 162.9 160.6 166.2 168.0	78c. Div. 177 '6 171 '1 163 '1 162 '2 165 '8	Sc. Div. 180 0 171 1 163 8 160 7 165 7	sc. Div. 180 ° 0 170 ° 4 163 ° 0 160 ° 7 169 ° 2	sc. Div. 180 ° 0 167 ° 9 165 ° 3 162 ° 0 169 ° 2	Sc. Div. 180°9 169°9 165°3 160°0 169°2	sc. Div. 183 '8 171 '3 165 '5 160 '3 169 '4	sc. Div. 181'42 172'98 166'15 160'42 164'62
158 1 157 8 155 4 159 8 161 9 163 4	156 '8 157 '8 154 '5 160 '6 157 '6 163 '4	157.8 156.4 155.0 159.6 157.4 163.7	160°3 157°2 158°4 159°5 157°7 159°1	160°3 158°3 159°0 157°5 153°3 163°3	160.5 159.6 158.1 158.7 157.5 160.9	170°4 160°5 160°9 150°8 158°4 160°2	169.7 160.8 161.1 154.1 156.6 142.9	169.5 160.4 161.8 157.3 156.5 137.9	169 1 160 4 163 2 159 3 154 0 149 8	167.7 160.5 162.4 161.3 155.0 149.2		169'38 161'28 159'50 157'78 158'05 153'87 162'06
183 · 2 166 · 3 164 · 7 156 · 3 156 · 0 162 · 0	176 ° 7 166 ° 3 161 ° 2 155 ° 3 155 ° 6 162 ° 3	174 · 4 165 · 9 156 · 5 154 · 4 156 · 8 163 · 8	174.0 165.9 155.9 154.8 157.7 163.8	172 · 1 164 · 6 156 · 2 154 · 8 157 · 3 164 · 6	164.6 163.6 156.2 156.9 157.5 164.6	169°3 163°8 164°4 156°2 156°9 157°5 — 168°5	168.5 166.6 164.4 153.8 158.1 158.4 ————————————————————————————————————	169.0 166.2 164.0 154.4 158.1 158.5	168.8 172.7 157.2 156.2 158.1 157.6	168.9 173.2 157.4 156.5 158.1 155.6 ———————————————————————————————————	168 9) 166 · 2 169 · 3 155 · 2 158 · 1 157 · 9 167 · 9 158 · 1	171.50 166.52 162.50 156.50 156.57 164.24 161.70
159.7 160.9	160.6 161.7 — — — —	161·3 162·9	159·7 161·5 — — — — —	161.0 ————————————————————————————————————	163.0 — — — — — —	161.8 162.5 — — — —	162 · 9 162 · 4 ———————————————————————————————————	162·9 162·4 — — — —	162·5 162·4 ————————————————————————————————————	161.9	161.9	160.95
163.53	162.74	162.29	162.50	162'36	162.57	163.09	162.61	162.60	163.27	163.07	163.90	163.40
	!			TEMPEI	RATURE OF	THE VERT	ICAL FORC	E MAGNET		1		
41°9 46°0 49°1 53°5 50°2 46°6	42.4 46.1 49.3 53.3 50.2 46.8	42.8 45.8 49.5 52.8 50.0 47.0	43.0 45.8 49.8 52.8 50.2 47.2	42·4 45·7 49·7 52·1 49·5 47·2	42°5 45°7 50°0 51°7 48°8 47°2	42°1 45°6 49°8 51°0 48°2 — 46°2	41°3 45°8 49°9 50°8 48°0	41°6 45°7 49°6 50°7 47°8 — 46°6	41°1 45°7 49°2 50°9 47°0 — 46°7	40°7 45°8 49°0 50°3 46°4 — 46°8	$ \begin{array}{c c} 40^{\circ}3 \\ 45^{\circ}4 \\ 49^{\circ}1 \\ 50^{\circ}0 \\ 45^{\circ}6 \\ \hline 47^{\circ}0 \end{array} $	40°24 44°45 48°32 51°12 49°13 46°40
51.7 53.6 54.5 53.3 55.3 54.1	52°2 53°2 54°5 53°3 55°6 53°3	51.5 53.4 54.0 53.4 56.3 53.0	51.5 53.2 54.0 53.3 56.3 53.2	51.5 52.7 53.3 53.3 56.0 52.8	51.5 51.8 52.8 53.3 55.8 52.2	51.2 51.5 52.5 53.3 55.8 — 45.8	51.0 51.0 52.5 53.3 55.6 — 46.4	51.2 50.0 52.2 53.2 55.6 — 46.8	51.4 49.8 51.6 53.7 55.6 - 46.5	51.4 49.5 51.5 54.0 55.3 —	49°1 51°4 54°5 55°2 - 46°8}	50.51 51.63 52.47 53.09 55.17 52.18 46.94
47.5 49.4 51.1 56.0 55.9 51.8	47.5 49.3 53.5 56.0 55.6 52.0	47.5 48.9 54.1 56.2 55.4 51.3	47.3 48.4 54.0 56.1 55.6 50.7	47.2 47.8 54.3 55.0 55.2 50.3	46.9 47.5 54.1 54.5 54.8 50.0	46.9 47.2 53.9 54.2 54.3 — 47.0	46.8 47.2 54.4 54.2 54.3 — 46.8	46.4 46.4 54.3 53.8 53.9 — 47.0	46.0 46.6 53.8 53.2 53.5 — 47.0	45.6 46.3 53.5 53.2 53.5 — 47.0	45.8 45.0 53.5 53.2 53.3 	46.46 50.59 54.64 54.64 50.05
52·3 51·8	51.0 51.2	51.2 51.3 —	51°5 —	51.5 51.6	51.6 51.7 —	51.8 51.5 —	51.7 50.6 —	51.4 50.3 —	51.2 50.2 —	52°1 51°2 —	51.6 51.4 —	50.99 51.56
	— — —		— — — —		——————————————————————————————————————	— — —					_ _ _ _	
										49.49	49.25	50.03

	0:	ne Scale Div	vision = '00	0066 parts	of the V. F.		CAL FORG in Scale Div		esponding to	1º decrease	of Tempera	ature, 1 • 64.	
Iean G gen '	öttin-}	O ^h .	1 ^h .	2 ^h •	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8 ^h .	9 ^h .	10h.	11ħ.
	1 2 a	Sc. Divi	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
	3 4 5 6	225 · 9 221 · 6 — 214 · 5	225 · 9 221 · 2 — 207 · 0	222.9 221.2 	220°9 216°0 — 204°9	215.5 212.7 — 208.3	214.5 211.3 — 210.5	214.7 213.2 — 220.4	216°1 212°9 — 223°7	216.9 215.3 — 230.4	216'9 216'2 — 240'1	216°2 214°0 — 250°3	215 · 6 213 · 5 ———————————————————————————————————
	7 8 9	214.5 219.4 226.4	216.6 219.2 224.6	217·5 219·3 223·1	216.8 218.1 223.1	217·2 217·0 219·0	215·8 217·1 218·9	215.8 217.1 219.1	216 ° 2 218 ° 1 218 ° 5	217.4 222.3 218.8	218.7 220.3 218.8	219.2 220.1 218.8	218 7 219 4 217 8
	10 11 12	226.6	226.9	226.9	225.1	224.8	221.7	221.7	221.9	221.7	224.0	224.0	224.5
APRIL.	13 14 15 16 17 18	228.6 231.5 224.2 209.0 222.9 217.4	228'9 224'5 224'5 217'2 223'9 216'1	229 · 2 221 · 6 224 · 6 216 · 2 223 · 9 216 · 1	229·2 222·3 223·6 216·4 220·4 214·7	225.6 221.5 221.9 221.4 219.5 214.3	226·2 221·8 221·9 223·0 218·3 212·9	227'3 221'8 221'9 229'3 219'9 212'9	228 · 2 221 · 8 223 · 6 233 · 5 218 · 4 212 · 8	231 · 8 229 · 3 224 · 4 236 · 2 217 · 9 212 · 8	234.7 225.7 224.4 238.1 220.1 211.2	234.0 231.3 228.5 237.8 219.6 210.2	232 1 231 3 230 4 235 6 215 6 209 3
	19 20 21 22 23 24 25	223.6 210.8 202.2 202.8 203.1 201.4	222.4 210.8 203.3 202.7 202.2 203.8	219 · 5 209 · 2 203 · 3 203 · 7 202 · 5 203 · 8	218.0 207.4 205.2 202.7 202.7 203.7	214·4 204·0 203·7 202·1 203·3 204·5	212·5 202·1 204·7 200·6 203·3 205·7	211.1 200.4 b 205.0 199.6 202.9 204.8	212.5 200.4 c 204.5 199.4 203.2 204.6	213 · 5 200 · 4 204 · 7 200 · 6 202 · 5 208 · 7	213.5 200.3 206.3 202.7 203.0 209.6	213.5 201.0 206.4 203.5 202.9 208.6	213 · 5 200 · 4 207 · 6 203 · 1 202 · 7 215 · 6
ļ	26 27 28 29 30	218.8 209.4 210.3 208.6	216°3 208°2 210°3 209°5	213.5 207.6 209.9 207.6	211.0 206.6 209.3 207.3	208.2 206.8 208.0 206.3	208°1 204°6 207°4 203°0	207.7 203.7 208.8 201.7	208:8 203:9 207:6 201:5	208'8 203'9 208'6 201'8	207'9 205'1 208'6 203'9	208.5 204.3 208.6 202.6	205 '4 206 '3 209 '8 201 '9
lourl	y Means	216.24	215.91	215.01	214.15	213.04	212.43	213.08	213.57	215.16	216.09	216.70	215.8
		1		(TEMPERAT			1					
:	1 2 a 3 4	- 47.6 50.3	48.2 50.6	9.6 50.2	9.6 52.2	51.0 52.4	51'3 53'2	52.0 53.5	- 52.4 54.3	52.4 54.2	52.8 54.6	52°3 53°6 55°3	52 · 8 53 · 6 55 · 6
	5 6 7 8 9	54°1 55°0 52°5 49°2	53.4 54.5 52.5 49.5	53.5 54.2 53.0 50.3	53.6 54.5 52.9 51.0	54.6 54.7 52.7 51.8	55°3 55°2 52°6 52°2	55.5 56.6 52.9 52.1	55°8 56°3 52°7 52°4	56°1 56°4 52°7 52°6	56°5 56°6 52°7 53°2	56.7 56.6 52.6 53.6	57 · 1 56 · 3 53 · 3 53 · 6
:	10 11	48.5	48.3	47.7	48.5	49.4	49.9	51.0	52.1	51.9	52.5	52.4	51.8
APRIL.	12 13 14 15 16 17 18	44.2 44.4 48.3 47.2 50.0 53.5	44.3 46.0 48.4 47.6 50.3 54.0	44.3 46.8 48.1 48.7 50.8 54.0	44.7 47.0 48.7 49.0 51.6 54.4	45°4 47°1 49°0 49°6 53°1 55°1	45.8 47.5 48.5 49.8 54.3 55.5	45.6 47.4 48.8 49.9 54.8 55.7	45°1 47°6 48°8 50°1 55°3 56°3	45°0 47°8 48°8 50°5 55°6 56°3	45.7 48.6 49.3 51.0 56.0 57.2	46.2 49.1 49.8 51.3 56.3 57.3	46.6 49.0 50.2 51.5 56.7 58.2
	19 20 21 22 23 24 25	50·7 57·1 59·0 60·1 59·6 59·8	51·3 57·0 59·2 59·7 59·4 59·4	52·9 57·2 59·0 59·0 59·3 59·2	52.6 58.2 58.7 59.2 59.4 58.8	54·1 59·3 58·5 60·0 59·4 58·3	55.2 60.0 58.5 60.0 59.8 58.3	55°3 60°0 58°5 60°4 60°2 58°3	56.0 61.0 59.1 60.4 60.2 59.2	56°3 62°0 59°2 60°3 61°0 59°0	57.0 62.5 59.3 60.5 60.8 58.5	57.5 62.5 59.4 61.0 60.8 58.4	58 · 2 62 · 2 59 · 6 60 · 0 60 · 8 58 · 4
	26 27 28 29 30	51.3 56.3 57.2 57.2	52°3 57°2 57°5 57°2	53.7 57.8 57.0 57.3	54°3 57°7 56°6 58°0	55.8 58.3 57.1 58.5	56°3 58°4 57°3 59°0	56°5 59°0 57°3 59°2	57°1 59°2 57°5 59°5	57.5 59.2 57.5 60.0	57°6 59°2 57°5 60°1	58°5 59°0 57°3 60°0	59°8 59°8 56°8 60°5
Jourl	y Means	52.74	52.95	53.50	53.23	54.14	54.2	54.80	55.12	55.32	55.63	55.88	56.0

a Not included in the Means.

	One Scale	Division =	*000066 pa	rts of the V		RTICAL F		orresponding	g to 1º decre	ease of Tem	perature, 1°	64.
12h.	13h.	14 ^h .	15 ^h .	16 ^h •	17 ^h .	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc, Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
218.9	218.9	220.2	219.9	220.9	219.8	221.1	223.1	214.1	217.9	222.5	225.4	_
216.1	215.8	215.5	216'4	218.9	219.2	220.7	220.7	221.3	221.9	221.6	221.6	218.82
212.1	214'4	214'4	215.2	214.6	215.3	010:4	010:5	015:6	215.6	215.6	$\left\{ {214.5}\right\}$	215.02
227.7	224.2	224.2	223.3	221.3	221.3	212.4	212.5 214.5	215.6 217.5	207.3	198.9	214 6	218.91
218.7	215.7	215.7	215.4	214.3	206.0	206.1	211.1	209.3	207.0	207.0	219.4	214.60
219'4	218.5	218.9	218.2	219.8	219.5	219.1	218.4	223.8	223.8	223.8	226.4	219.89
218.2	218.4	218.5	218'4	220.7	220.7		010:0	005:0	000:2	000.0	225.5	221.55
224.5	224.4	224.0	223.0	223.0	223.0	219.5	218.2	225.8	228.3	228.3	220 0)	207100
						231.1	232.9	232.6	231.0	231.0	$\left[\begin{array}{c} -1 \\ 231 \cdot 0 \end{array}\right]$	225.86
229.3	234.3	230.6	225.4	227.5	232.4	232.3	231 9	231.9	231.3	233.7	232.4	230:37
231.1	231.1	226.9	226.6	223.7	224.3	223.0	220.7	224.1	219.5	224.4	223°3 203°1	225.13 220.80
230.4	223.6 235.9	228·1 232·8	$227.1 \\ 225.6$	223.7 210.1	223.5 211.2	209.8 214.0	206.2	205'6	205°1 197°1	204 ° 6 215 ° 4	$\frac{203}{221.3}$	222.60
213.1	213.4	213.4	212.7	212.7	212.7	212.1	213.8	213.8	214.0	212.7	214.5	216.63
209.3	211.1	211.1	210.6	210.6	210.6		-			-	$\left\{ \frac{-}{222\cdot 1}\right\}$	213.59
01217	01117		000:			206.5	215.6 210.4	219 ·3 210 ·4	219 .3	219°3 209°2	222.1 }	212.90
213.5	211.5 200.4	209.5 200.2	209.5	209.5	209.5	209 . 5	204.7	204.4	209 8	204.0	206.3	202.84
209.4	209 1	202.2	200.3	200.6	203.1	203.3	203.7	204.5	204.4	204.2	201.7	204.32
203.1	200.9	201.5	202.6	202.8	202.8	203.6	203.7	203.7	202.2	204.2	204.2	202.46
201.2	202.6	202.6	202.6	200.6	202.8	220.3	193.9	188.0	193.7	193.2	202.7	200.78
215.6	213.4	213.3	213.3	198.7	208.6	212.6	213.7	215.7	216.3	218.0	$\left \frac{-}{217.6} \right\}$	209.65
204.5	204.3	204.2	206.1	204.0	202.2	205.8	206.7	206.7	206.0	209.3	209.3	208.03
205.6	206.7	206.7	206.6	206.5	206.6	206.6	205.6	205.8	208.4	208.4	210.3	206.43
209.8	209'8	209.8	210.6	210.4	209.0	209.1	205.5	206.6	208.6	207.5	210.4	208.93
201.0	201.0	201.5	201.2	201.2	201.0	201.2	200.8	200.6	200.6	202.6	202.5	202.99
215.24	214.82	214.18	213.24	212.00	212.43	212:36	212.02	213.03	211.98	212.93	214.95	214.02
				ТЕМРЕ	RATURE OF	THE VERT	ICAL FOR	E MAGNET	•		<u>'</u>	
°	°	<u>.</u>	•	°_	•	•	·	°	°	°	<u> </u>	<u> </u>
52.2	52.5	51.7	51.0	51.0	50.2	50.3	49.7	49.0	48.8	48.4	48.2	
54.3	53.8	54.2	53.4	52.5	52.0	51.7	51.6	51.3	51.2	51.1	21.0	51.76
55.7	55.2	55.3	55.0	55.1	54.7	54.0	54.0	54.1	54.1	54.1	$\begin{bmatrix} -54 \cdot 2 \end{bmatrix}$	53.84
56.7	58.0	58.0	56.2	56.0	55.5	55.3	55.4	55.5	55.5	$5\overline{5}\cdot\overline{2}$	55.3	55.60
56.3	56.8	56.9	56.8	56.6	56.5	56.2	55.6	55.5	54.5	54.3	53.4	55.68
54.0 53.0	53.5	52.9	51.8	51.6	51.5	51.0	50.2	50.5	20.0	49.5	49'4	52.04
	53.2	53.3	52.5	51·7	51.2	46.8	47.5	47.5	47.7	48.0	$\frac{-}{47.8}$	50.92
51.4	20.3	50.8	50.6	50.3	50.0				44.0	44.9	44.4}	48.94
46.6	46.6	46.6	45.8	45.4	45.2	44.6 44.6	44.5 44.6	44°4 44°2	44.3 44.0	44°3 44°0	44 4)	45.20
49.0	49.0	48.8	49.2	49.0	$\frac{43}{49}$.2	49.0	48.8	48.4	48.6	48.8	47.6	48.07
50.2	51.0	51.2	51.3	50.5	49.7	49.5		49.3	49.1	48.3	47.5	49.33
51.9	52.8	52.7	52.3	51.7	51'6	51.2	51.2		50.8	50.2	50.2	50.57
56.6 58.3	56.8 58.3	56°3	56.6	56.2	56.0	55.8	55.2	54.7	54.6	54°0	54.0	54.66
-	58.3	58.2	57.8	57·6	57·4 —	53.3	52.3	52.0	51.8	51.4	50.9	55.28
58.0	58.2	58.2	58.2	57.8	57.6	57.5	57.8	57.7	57.5	57.5	57.2	56.29
62.4 60.0	62.0	62.0	62.2	62.0	61.8	61.8	61.0	60.6	60.1	59.8	59.6 60.6	60.60 59.62
60.0	60.0 60.2	61°1 60°4	61.1 60.2	60.0 60.6	60°2 59°8	59.6 59.0	60°0 59°7	59 ° 2	59 · 4	60.6 59.8	59.8	59.97
60.8	60.9	60.8	60.8	60.6	60.2	60.3	60.4	60.5	60.4	60.4	60.0	60.58
57.8	57.6	57.3	57.2	57.0	56.6		_				$\frac{-}{51 \cdot 1}$	56.40
59.4	-					53.0	52.5	52.2	51.7	51.3		56.90
59.0	59.5 59.2	59°4 59°0	59°1 58°3	58.7 58.1	58.1	57.7	57·1 58·1	56.6 58.1	56°9 57°7	56°6 57°4	56.2 57.0	58.58
57.0	57.0	57.2	57.4	57.4	58°1 57°3	58°1 57°2	57.3	57.2	57.3	57.5	57.3	57.24
60.2	60.2	60.2	60.2	60.7	60.7	61.0	60.4	60.2	60.0	60.0	59.6	59.63
00 0	, 00 0		ł								,	1

	On	e Scale Divi	ision = '00	0066 parts o	f the V. F.	VERT	ICAL FOF n Scale Div	RCE. isions, corre	sponding to	1º decrease	of Tempera	ture, 1°64.	
Mean gen T	Göttin-)	Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6h•	7 ⁿ .	8h.	9 ^h .	10 ^h .	11h.
		Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 199 5	Sc. Div.	Sc. Div. 200'2	Sc. Div. 200'4	Sc. Div. 200 4	Sc. Div 201 3
	$\left(egin{array}{c} 1 \ 2 \end{array} ight]$	204.2	203.4	201.8	200°0 197°6	198°8 196°5	198 . 8	195.6	196.6	199.8	198.8	198.7	198.8
	3 4	203.6	203.4	201.9	198.6	203.2	204.4	202.3	201.9	203.1	209.3	220.2	222.2
	5	204.2	202.3	199.3	199.3	199.3	201.2	202.2	202.8	205.8	207.1	209.2	210.5
	6	203.6	203.6	202.3	200.0	197.0	199.2	199.7 204.9	199.7 204.9	203.9 205.2	206.0	203 0 203 3	$\frac{204.2}{205.3}$
	7	207.4	206.9	206.0	206.0	204°1 199°0	202.8 199.3	198.7	198.7	201.3	202.4	204.3	205.1
	8 9	201.2	203.9	199.5	199.2	199.8	202.4	197.7	202.4	209.6	214.6	216.0	210.5
	10 11	209.8	209.7	211.4	215.2	214.8	215.6	215.1	216.3	218.3	218.3	217.8	218.7
	12	206.2	196.9	211.0	211.0	212.2	211.5	215.3	225.0	233.5	216.2	246.3	244 3
	13	201.7	205'2	209.7	210.7	210.7	211.9	211.6	211.6	210°3 198°4	213°8 197°4	207°6 195°8	205.2
	14	199.9	199.0	199 . 4	198·1 199·4	198°1 198°4	196 . 8	198.4 195.4	198 · 4 197 · 0	193 4	196.3	195.6	197:9
$ ext{MAY}_{\hat{\cdot}}$	15 16	196°0 205°6	199.4 205.4	203.7	202.1	198.3	195.5	194.3	194.5	194.5	195.6	196.5	195.3
Z	17 18	199.4	199.0	198.8	199.4	195.1	193.9	193.1	194.6	197:9	198.2	199.1	200:2
	19	215.8	213.1	210.3	207.0	206.6	206.6	206.7	209.1	209.1	209.4	209.4 203.6	207.6
	20	205.1	206.1	205.4	203.2	203.2	204.1	204.1	204.1	208·5 211·0	203.6	208.1	206.6
	$\begin{bmatrix} 21 \\ 22 \end{bmatrix}$	194 . 9 210.4	200 ·2 204·3	199.0 205.3	199.0 205.8	205.4	204.1	204.2	204.4	205.7	207.0	207.0	207.0
	23	210.4	208.5	204.0	203.5	199.8	203.8	203.8	200.7	200.8	200.8	199.2	198'4
	24 25	 193`7	— 194·5	191.0	193.3	193.0	193.0	193.4	194.4	194.4	196.7	194.6	194'6
	26	192.9	191.9	188.2	188.5	186.3	186.1	184.0	180.7	179.1	180.6	182 . 0	183°0
	27	186.8	184.5	183.0	182.7	178°3 178°3	176°9 177°2	177°5	178.4 178.1	178°9 178°9	178°9 179°4	179.7	180.3
	$\frac{28}{29}$	184°3	182.9 185.7	180.8 183.8	179°5 182°7	182.7	178.0	178.3	178.3	178.3	178.3	179'1	181.4
	30	181.2	183.0	184.2	184.3	182.6	179.1	177.2	177.7	179.6	183.5	185.9	191.6
	31		199.77	199.36	198.71	197.92	197.77	197.58	198:30	200.15	200.36	201.23	201.8
ourry	Means	200.36	199 11	1	l	<u> </u>		1				<u> </u>	
		0		59°8	TEMPERAT	60°2	60.3	60.4	60°4	60°8	6 <u>1</u> .0	6j.0	61.5
	$\begin{pmatrix} 1 \\ 2 \end{pmatrix}$	59.2 60.6	59°6	91.0	61.2	60 2	62.6	63.0	63.6	63.8	64.3	64.6	64.4
	3	59.0	59.4	60.0	$\frac{-}{61.2}$	62.0	63.0	63.3	63.5	63.6	64.0	64.4	65.2
	4 5	60.8	60.8	61.0	60.6	61.0	61.4	61.4	61.6	61.6	62.3	62.2	62.6
	6	61.6	61.6	61.0	61.6	62.0	62.3	62.4	62.0 60.0	60.0 61.6	62.0 60.0	$62.1 \\ 60.2$	62°2
	7	57.7	58.2 60.0	58.7 60.4	$\begin{array}{c} 58.9 \\ 60.8 \end{array}$	59.1 61.6	59.6 62.0	59.8 62.6	62.4	62.8	63.8	63.4	63.0
	8 9	58.8 61.4	61.2	61.0	61.0	61.0	61.5	61.2	61.4	61.4	61.0	61.0	61.0
	10 11	52.7	52.7	52.8	52.1	51.8	52.3	52.2	52.7	53.0	53.3	54.0	54.8
	12	54.2	54.8	55.7	56.5	57.0	57.5	57.7	58.0	58.4 60.0	58.9 61.0	59°5	59.6 62.0
	13	56.9	56.9	56.7 62.1	57°2 63°0	58°1 63°6	59°0 64°4	59°3 64°6	59.6 64.8	65.2	65.6	65.9	65.8
	14	63.0	$\begin{array}{c} 61.6 \\ 62.4 \end{array}$	62.0	62.0	62.0	62.5	62.8	63.3	63.4	63.7	64.0	64.0
		00 0	U - 1					62.4	63.0	63*4	63.9	64·4 —	64.2
AY.	15 16	59.7	59.6	59.7	60.0	61.0	62.0	i i	·				corr
$\max_{\widehat{\Omega}} Y.$	15	59·7 62·7	59.6 62.3	61.6	61.9	61.6	61.6	61.2	61.0	61.4	61.0	60.7	
$\max_{\widehat{\Omega}} \mathbf{X}.$	15 16 17 18 19	62·7 55·6	62·3 56·3	61.6 56.7	61.9 57.3	61.6 57.8	61.6 58.3	61.2 58.0	61.0 58.2	58.2	58.8	59.3	59.7
MAY.	15 16 17 18 19 20	62.7 55.6 56.3	62°3 56°3 57°0	61.6 56.7 58.1	61'9 57'3 58'4	61.6 57.8 59.0	61.6 58.3 59.0	61°2 58°0 59°3	61.0 58.2 59.7	58.5 61.0			59.7 61.6 60.0
$\max_{\widehat{\Omega}} \mathbf{Y}.$	15 16 17 18 19 20 21 22	62.7 55.6 56.3 58.3 54.8	62°3 56°3 57°0 59°0 55°8	61.6 56.7 58.1 59.2 56.6	61.9 57.3 58.4 59.4 57.0	61.6 57.8 59.0 59.4 58.5	61.6 58.3 59.0 59.5 59.0	61°2 58°0 59°3 59°5 59°2	61.0 58.2 59.7 59.4 59.8	58.2 61.0 59.3 59.9	58.8 61.4 59.3 60.0	59°3 61°6 59°3 60°0	60°5 59°7 61°6 60°0 60°0
MAY.	15 16 17 18 19 20 21 22 23	62.7 55.6 56.3 58.3	62°3 56°3 57°0 59°0	61.6 56.7 58.1 59.2 56.6 58.6	61.9 57.3 58.4 59.4 57.0 59.2	61.6 57.8 59.0 59.4 58.5 59.8	61.6 58.3 59.0 59.5 59.0 60.6	61.2 58.0 59.3 59.5 59.2 61.0	61.0 58.2 59.7 59.4 59.8 61.1	58.2 61.0 59.3 59.9 61.9	58.8 61.4 59.3 60.0 62.9	59°3 61°6 59°3 60°0 63°4	59.7 61.6 60.0 63.6
MAY.	15 16 17 18 19 20 21 22 23 24 25	62.7 55.6 56.3 58.3 54.8 57.3 61.4	62°3 56°3 57°0 59°0 55°8 57°4 ————————————————————————————————————	61.6 56.7 58.1 59.2 56.6 58.6	61.9 57.3 58.4 59.4 57.0 59.2 — 62.6	61.6 57.8 59.0 59.4 58.5 59.8 ————————————————————————————————————	61.6 58.3 59.0 59.5 59.0 60.6 —	61.2 58.0 59.3 59.5 59.2 61.0	61.0 58.2 59.7 59.4 59.8 61.1	58.2 61.0 59.3 59.9 61.9	58.8 61.4 59.3 60.0 62.9 — 66.6	59°3 61°6 59°3 60°0 63°4 — 67°0	59.7 61.6 60.0 63.6 67.8
MAY.	15 16 17 18 19 20 21 22 23 24 25 26	62.7 55.6 56.3 58.3 54.8 57.3 61.4 65.6	62:3 56:3 57:0 59:0 55:8 57:4 — 61:6 66:4	61.6 56.7 58.1 59.2 56.6 58.6 ————————————————————————————————————	61'9 57'3 58'4 59'4 57'0 59'2 62'6 67'5	61.6 57.8 59.0 59.4 58.5 59.8 — 63.4 68.7	61.6 58.3 59.0 59.5 59.0 60.6 — 64.5 69.3	61.2 58.0 59.3 59.5 59.2 61.0 — 65.1 69.8	61.0 58.2 59.7 59.4 59.8 61.1 — 66.0 70.3	58.2 61.0 59.3 59.9 61.9 — 66.3 71.0	58.8 61.4 59.3 60.0 62.9 — 66.6 71.6	59°3 61°6 59°3 60°0 63°4	59.7 61.6 60.0 63.6 67.3 73.0 74.3
MAY.	15 16 17 18 19 20 21 22 23 24 25 26 27	62.7 55.6 56.3 58.3 54.8 57.3 61.4 65.6 68.8	62:3 56:3 57:0 59:0 55:8 57:4 61:6 66:4 69:6	61.6 56.7 58.1 59.2 56.6 58.6	61'9 57'3 58'4 59'4 57'0 59'2 62'6 67'5 70'8	61.6 57.8 59.0 59.4 58.5 59.8 ————————————————————————————————————	61.6 58.3 59.0 59.5 59.0 60.6 —	61.2 58.0 59.3 59.5 59.2 61.0 	61.0 58.2 59.7 59.4 59.8 61.1 	58.2 61.0 59.3 59.9 61.9 — 66.3 71.0 73.1 72.1	58.8 61.4 59.3 60.0 62.9 — 66.6 71.6 73.6 72.2	59'3 61'6 59'3 60'0 63'4 67'0 72'8 73'8 71'8	59.7 61.6 60.0 63.6 67.8 73.0 74.8
MAY.	15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	62.7 55.6 56.3 58.3 54.8 57.3 61.4 65.6 68.8 69.4 69.1	62:3 56:3 57:0 59:0 55:8 57:4 ————————————————————————————————————	61.6 56.7 58.1 59.2 56.6 58.6 ————————————————————————————————————	61'9 57'3 58'4 59'4 57'0 59'2 —62'6 67'5 70'8 71'0 70'1	61.6 57.8 59.0 59.4 58.5 59.8 	61.6 58.3 59.0 59.5 59.0 60.6 	61.2 58.0 59.3 59.5 59.2 61.0 ————————————————————————————————————	61.0 58.2 59.7 59.4 59.8 61.1 — 66.0 70.3 72.7 71.5 71.0	58.2 61.0 59.3 59.9 61.9 — 66.3 71.0 73.1 72.1 71.5	58.8 61.4 59.3 60.0 62.9 — 66.6 71.6 73.6 72.2 71.9	59°3 61°6 59°3 60°0 63°4 — 67°0 72°8 73°8 71°8 71°9	59.7 61.6 60.0 63.6 73.0 74.3 71.8
MAY.	15 16 17 18 19 20 21 22 23 24 25 26 27 28	62.7 55.6 56.3 58.3 54.8 57.3 61.4 65.6 68.8 69.4	62:3 56:3 57:0 59:0 55:8 57:4 61:6 66:4 69:6 70:0	61.6 56.7 58.1 59.2 56.6 58.6 ————————————————————————————————————	61'9 57'3 58'4 59'4 57'0 59'2 62'6 67'5 70'8 71'0	61.6 57.8 59.0 59.4 58.5 59.8 	61.6 58.3 59.0 59.5 59.0 60.6 	61.2 58.0 59.3 59.5 59.2 61.0 	61.0 58.2 59.7 59.4 59.8 61.1 	58.2 61.0 59.3 59.9 61.9 — 66.3 71.0 73.1 72.1	58.8 61.4 59.3 60.0 62.9 — 66.6 71.6 73.6 72.2	59'3 61'6 59'3 60'0 63'4 67'0 72'8 73'8 71'8	59.7 61.6 60.0 63.6 67.8 73.0 74.8

1					VE	RTICAL F	ORCE.					
	One Scale	Division=	•000066 par	ts of the V.	F. Increas	e, in Scale 1	Divisions, co	rresponding	to 1° decrea	ase of Temp	erature, 1.6	
12h.	13h.	14 ^h •	15 ^h .	16 ^h .	17 ^h .	18 ^h .	19 ^h .	20h.	21h.	22h•	23.	Daily and Monthly Means.
8c. Div. 201 2	Sc. Div. 201 5	Sc. Div. 200'8	sc. Div. 200 7	Sc. Div. 200'7	Sc. Div. 201'2	Sc. Div. 198'9	Sc. Div. 199 3	Sc. Div. 199'2	Sc. Div. 199'2	Sc. Div. 199'2	Sc. Div. 199'2	Sc. Div. 200 39
196.2	196.3	196.1	193.9	193.3	193.3	-					$\left \frac{-}{202 \cdot 6} \right $	196.12
_	_	<u> </u>	—			177.7	189.0	195.2	195 ° 2 196 ° 0	$200.7 \\ 200.2$	199.4	200.42
209.0	209.2	195.7	200.6	175.0	185.4	177.5	191.8 194.9	196°0 194°7	190 0	198.7	201.3	202.13
210.2	208.9	205.5	205.5	203.9 199.6	192.9 199.1	193.9 201.6	202.2	201.4	201.4	204.2	204.2	201.68
201.9	201.5	200.5	199.5	203.5	202.0	203.6	196.3	198.8	203.5	206.0	206.0	204.52
209.2	209°2 204°4	203 3	201.7	201.2	199.0	198.9	200.1	200.1	200.3	200.9	200.7	201.21
207.0	204.9	202.3	200.6	200.6	200.1	_		_	—		}	205.15
201 0		_	_			207.5	208.0	209.2	210.3	209.6	209.6	
218.7	218.7	223.7	229.4	214.5	202.7	216.0	210.5	210.4	200.6	184.6	169°3 195°7	$211.67 \\ 212.64$
219.4	214.0	207.5	208.5	194.2	199.6	212.3	198.2	207.5	209.4	$207.4 \\ 201.3$	199.5	203.82
205.2	204.2	204.2	193.4	191.7	191.7	191.7	197.9 193.2	200.4 193.2	195.9	195.9	195.9	196.35
199.0	196.9	195.7	190.0	193.6	193.8	192 .9	200.5	200.5	200.9	201.7	204.0	198.52
197.1	196.4	198.2	198.9 195.4	198 · 9	197.5	190 9	200 2				- 7	199.56
194.6	194.6	195.4	130 4	131 0		204.8	207.3	205.9	205.6	205.1	205.2}	i
200.2	198.8	203.3	209.5	208.5	208.3	203.1	205.7	204.6	206.3	212.6	215.4	201.90
204.7	204.7	204.7	206.3	209.4	205.6	193.4	202.7	207.2	204.3	196.3	208.4	206.60
203.6	201.4	201.4	201.8	200.8	198.2	198.6	200.8	202.2	203'4	205.9	202.9	203.15 204.82
204.9	205.6	206.4	206.9	206.9	206.9	208.9	207:0	204.3	202.9 206.2	200°2 195°6	206.7	204 62
206.3	206.3	206.3	206.3	206.3	206.3	206.0	206.2	206.2	200 2	190 0	1 1	
197.2	196.6	196.6	204.6	210.3	209.7	192.2	191.2	197.4	196.9	199.3	196.4	200.92
104:6	100:0	100:0	190.1	190.9	190.9	190.3	190.3	190.2	191.1	192.7	192.3	192.63
194.6	192.6 181.9	190°2 182°4	182.7	182.3	181.0	183.1	182.9	182.9	182.9	182.7	186.8	184.02
177.5	177.0	177.0	177.0	177.9	177.3	177.6	180.0	180'9	179.4	180.0	178.7	179.25
180.3	180.3	180.3	180.5	180.3	181.7	182.5	183.4	184.2	183.9	185.2	187.7	181.12
182.2	182.7	182.9	179.9	174.3	177.1	174.4	179.2	182.1	180.6	174'3	176.1	179.99
185.6	185.2	185.7	190.9	167.9	167.6	170:0	180.0	185.0	180.4	181.9	180.9	181.35
						170.2		197.68	197.48	197.02	197 · 24	198:30
199.81	199.00	198.09	198.28	195.54	194.92	194.48	196.10	 	<u> </u>	131 02	101 21	130 00
							ICAL FORC			0	0	
61.2	61.3	61.3	6η1	6j.0	61.0	6 ì ·2	6η4	6i°3	61.3	6j.0	60.8	60 ⁵ 75
64.6	64.6	64.4	64.2	64.6	64.6				<u> </u>	60.2	$\begin{bmatrix} -59.6 \end{bmatrix}$	62.85
-						63.4	62.7	61.7	61.2 62.0	61.6	61.5	63.33
65.6	65.6	66.6	65.8	65.2	66.6	64.7	63.6	62.8 61.8	61.6	61.4	61.2	61.80
62.6	62.8	62.6	62.8	62.6 61.6	62.4 60.8	62.0 60.4	60.0	59.6	59.2	58.2	58.2	61.19
62°2 60°4	62°2 60°4	61.7 60.7	61.7 60.4	60.0	59.8	59.7	59.0	58.8	58.7	58.9	58.7	59.52
63.0	62.8	62.8	62.6	62.6	62.4	62.6	62.2	62.2	62.0	61.9	62.0	62.11
61.0	61.0	61.4	61.4	61.5	61.6						54.7}	59.92
	_			—		57.3	56.8	56.2	55.7	55.3	53.8	53.65
55.0	55.0	54.9	54.8	54.8	54.8	54.4	54.0	54.0	54.0 57.8	54°0 57°5	57.4	58.20
60.4	60.6	61.8	61.8	61.2	60.4	59.4 62.0	59°2 62°4	58.8 62.2	62.2	62.0	61.7	60.68
62.8 66.0	62.8	63.0	62.6 65.4	62'4 65'3	65.0	64.8	64.6	64.2	64.2	64.2	63.6	64.49
64.6	65.8 64.2	63.8 63.8	63.1	62.6	62.0	61.8	61.6	61.2	60.7	60.2	60.0	62.54
64.6	64.6	64.4	64.2	63.8	63.4				_		$\begin{bmatrix} -63 \cdot 3 \end{bmatrix}$	62.97
_						64.2	64.4	63.8	63.4	63.8		
60.4	60.0	59.7	59.5	59.0	58.8	58.2	57.4	56.7	56.0	55.8 57.5	55°3 56°0	59.76 58.02
59.7	59.5	59.5	59.2	58.5	58.2	57.8	57.5	57°3	57.6 59.3	57°5 58°8	57.5	59°96
62.2	62.0	61.8	61.8	61.6	61.2	60.6 57.5	60°2 57°0	59.7 56.4	55.8	55.4	54.8	58.43
59.8	59.6	59.4	58.6 58.9	58°3 58°7	58.0 58.7	58.6	58.2	57.8	57.6	57.4	57.7	58.47
63.6	59.6 63.6	59°3	63.6	63.2	63.3		_				$\frac{-}{61\cdot 2}$	61.68
_			_			62.6	62.4	62.2	62.0	61.6		
67.2	67.3	67.8	67.8	67.4	67.2	66.8	67.2	66.6	66.6	66'1	65.6 68.6	65°72 70°15
73.0	73.2	72.6	71.5	71.5	71.0	70.5	70.1	69°9 71°4	69 .6 71 . 0	$69^{\circ}2$ $70^{\circ}2$	69.4	70 13 72:31
74.5	74.7	74.3	74.2	73.6	73.6	73.1	72.0 70.4	70.4	70.0	69.4	68.3	70.99
71'8	71.9	72.1	72·1 70·9	71.6 72.3	71°1 72°3	70.8 72.3	72.3	70.8	70.2	71.2	71.2	71.02
72.6	70°8 72°6	70°5 72°2	72.3	72.0	71.2	71.2	71.2	71.2	70.2	70.5	69.4}	70.84
							62.70	62.27	61.95	$\frac{70.2}{61.71}$	61.51	62.76
64.24	64.17	64.12	63.95	63.74	63.23	63.01	02 70	02 21	01 90	01 /1	01 21	02 10

	0	ne Scale Div	rision = '00	00066 parts	of the V.F.		ICAL FOR in Scale Div		esponding to	1º decrease	of Tempera	ture, 1.64.	
Mean G gen T	öttin- ime.	Oh.	1h.	$2^{ ext{h}}.$	3 ^h .	4 ^h •	5 ^h .	6 ^h •	7 ^h •	8 ^h •	9 ^h .	10 ^h •	11 ^h .
	(1 2 3 4 5 6 5	sc. Div. 183 9 181 9 192 6 187 7 189 3 200 9	Sc. Div. 183 ° 0 184 ° 9 192 ° 1 187 ° 1 188 ° 2 200 ° 8	Sc. Div. 183 * 6 184 * 9 191 * 3 186 * 2 189 * 8 198 * 6	sc. Div. 185 * 5 184 * 9 190 * 4 186 * 2 190 * 2 195 * 8	sc. Div. 184'4 183'2 190'4 186'7 190'9 194'3	sc. Div. 184°2 182°9 188°7 185°7 193°5 195°0	Sc. Div. 182 4 184 4 187 3 185 7 195 7	sc. Div. 183°1 185°7 180°6 186°5 194°9 196°5	Sc. Div. 183 ° 0 189 ° 7 193 ° 7 190 ° 8 194 ° 8 199 ° 8	sc. Div. 183°3 195°1 193°4 190°1 194°3 194°4	Sc. Div. 182 '9 196 '7 192 '8 190 '1 196 '2 188 '7	Sc. Div. 184'0 198'0 194'1 189'9 196'2 190'3
	7 8 9 10 11 12 13	207.8 197.8 199.8 192.5 193.7 195.1	205 · 2 197 · 1 198 · 7 192 · 0 192 · 8 192 · 1	204.1 196.3 197.3 191.5 190.7 186.8	200°1 199°7 195°7 190°4 189°1 187°8	196.0 195.5 195.6 188.0 188.1 186.7	195.2 194.3 197.2 186.7 188.1 185.2	195.0 195.6 194.1 185.3 189.0 184.2	195.9 196.2 192.7 186.1 190.4 184.3	195 · 8 195 · 9 192 · 0 187 · 8 191 · 2 186 · 6	195.7 194.9 191.6 187.8 191.0 189.0	195.0 195.7 191.2 187.7 192.2 190.4	194.0 195.7 191.1 187.8 191.9 190.4
JUNE.	14 15 16 17 18 19 20	181.4 178.8 183.8 181.0 180.0 183.3	184.7 174.4 186.2 182.6 179.7 183.3	187.4 181.5 185.4 183.2 181.0 184.5	188'9 179'1 186'8 183'5 180'3 184'5	183.4 186.7 186.8 182.0 179.9 184.8	181'9 183'4 184'2 182'2 178'9 183'8	186°1 182°7 187°0 180°0 176°5 183°0	186°1 184°5 183°5 180°0 176°8 182°9	184'9 184'3 183'5 180'0 177'0 184'1	186.8 187.7 182.7 182.3 176.2 186.3	187.5 190.0 182.7 181.5 175.4 186.9	184.7 188.0 181.3 179.0 174.1 186.9
	21 22 23 24 25 26 27	201°2 199°2 185°7 179°8 182°4 180°4	203 '4 196 '0 187 '4 182 '5 182 '8 180 '4	202.5 196.7 187.4 181.8 181.7 180.6	201°8 194°1 187°4 178°3 181°0 178°9	197 · 4 193 · 9 186 · 7 179 · 4 178 · 2 175 · 8	198.4 193.0 184.0 175.7 175.0 172.5	196.7 192.5 182.6 175.2 173.3 171.4	195.4 191.2 182.2 176.5 171.1 170.0	194.8 192.9 184.3 174.8 171.9	195 · 5 192 · 3 183 · 9 173 · 5 173 · 7 175 · 5	196 · 2 193 · 2 184 · 5 174 · 7 173 · 7 177 · 5	199.0 190.0 182.6 174.7 174.2 179.6
	28 29 30	180.9	179°9 172°5	180°5 174°5	180°5 173°4	179·4 170·9	179.4 167.2	178·1 168·3	175.6 167.0	176°9 168°7	179.6 168.4	176·4 168·7	175°3 170°0
Hourly	Means	188.08	188.07	188.07	187.47	186.32	185.24	184.89	184.45	185.80	186.36	186.48	186.5
		1	1		TEMPERAT	ī -	E VERTICA	1	AGNET.		1		
	1 2 3 4 5 6	68.7 69.0 65.7 66.4 65.4 61.0	69.4 69.0 66.0 66.8 65.2 61.4	69.7 68.7 66.2 67.4 64.8 61.8	69°3 69°2 66°6 67°4 64°4 62°4	69.3 69.5 67.0 67.4 64.0 62.8	69.5 69.4 67.0 67.6 64.0 62.8	69.8 69.6 67.2 68.0 63.9 62.8	70°3 69°6 67°1 68°7 64°2 62°8	70°5 69°6 67°2 69°0 64°5 63°0	71°2 69°5 67°6 69°0 64°6 63°2	71°5 69°5 67°9 68°7 64°7 63°3	71.8 69.8 68.2 68.2 64.8 63.6
	7 8 9 10 11 12 13	59°3 61°0 63°4 65°6 63°6 63°4	59.5 61.0 63.6 65.5 64.3 63.5	59.7 61.1 64.3 66.0 64.6 64.0	60.6 61.8 64.6 66.6 65.1 64.0	61.6 63.6 65.3 67.3 65.4 64.4	62.8 64.2 65.8 67.6 65.7 66.0	63.7 64.6 66.3 67.8 66.0 66.4	63.4 65.0 66.6 68.0 66.0 66.8	63.7 65.4 67.4 67.7 66.0 67.0	64.3 66.0 68.6 68.0 66.0 67.2	64.8 66.6 69.2 68.2 66.0 67.4	65.5 66.6 69.5 68.4 66.4 67.2
JUNE.	14 15 16 17 18 19 20	66.6 69.4 67.6 69.3 71.5 70.6	66.6 69.6 67.6 69.1 71.5 70.6	66.6 69.5 68.0 69.0 71.5 70.0	67.4 70.3 68.5 69.2 71.4 70.5	68.8 70.5 69.3 70.0 71.5 69.8	69.5 70.6 69.5 70.7 71.8 69.7	70°0 70°5 69°5 71°5 72°5 69°6	70.5 70.5 70.4 72.1 73.3 69.7	70.9 70.5 71.0 72.5 74.0 69.5	71.6 70.7 72.0 73.0 74.7 69.4	72.2 70.7 72.5 73.2 75.2 69.2	72.6 71.0 72.6 73.5 75.5 68.6
	21 22 23 24 25 26 27	59.5 61.2 65.6 69.6 70.8 72.7	59°2 62°0 65°6 69°2 70°5 71°7	59.8 62.2 65.6 69.5 70.5 71.5	60°3 63°0 66°0 70°3 70°3 71°8	61.0 63.8 66.6 70.9 70.9 72.0	61.6 64.6 67.7 71.5 71.7 72.5	61 · 8 65 · 6 68 · 6 72 · 3 72 · 9	62.4 66.0 69.0 73.3 72.9 73.0	62.6 66.6 69.7 73.9 73.2 72.9	62.8 67.6 71.0 74.7 74.0 73.0	63.4 68.4 71.3 74.7 74.7 73.0	63.6 68.5 71.9 75.2 74.6 73.0
	28 29 30	71·2 74·4	71°1 74°0	71.0 74.6	71°4 74°6	71.6 75.6	72.6 76.0	72.8 76.0	73·4 77·0	74°0 77°0	74·4 77·2	74·7 77·5	75·2 77·9
Hourly	y Means	66.63	66.67	66.83	67:19	67.69	68.17	68.24	68.92	69.20	69.67	69.94	70.1

	0 0 1	D: :-!	.000066			RTICAL F			n to 10 doors	ogo of Tom	a amatuma 1°6	.4
	One Scale	Diaision =	-000066 pa	rts of the V	. r. Increa	se, in Scale	Divisions, c	orresponding	to 1° decre	ase of Tem	perature, 1°6	
12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18h.	19 ^h .	20 ^h .	21 ^h .	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
185.0	187.7	170.7	174.9	177.0	181.1	179.0	176.9	176.9	178.6	171.0	171.0	180.55
194'3	188.0	191'1	188.6	184.7	186.9	193.9	191.2	182.9	185 .8	193.3	195.2	188.73
194'1	191.7	191.7	189.6	189.2	185.8	186.7	186.7	186.7	185.3	188.2	188.3	189.65
189'2	188.9	188.8	189.6	189.3	189.6	188.3	188.5	188.0	187.4	192.6	190.2	188.48
196.2	196.4	193.9	195.0	191'4	188.9	196.7	193.7	194.1	199'3	201.5	201.5	194.28
190'4	204.0	203.0	200.8	202.1	202.7						207.7}	199.21
_						202.6	202.6	204.2	204.3	206.6		
197.4	198.9	198.4	204'1	199.0	178.8	195.3	193.6	195.0	169.2	199.1	194.2	195.96
196.8	198.2	193.9	193.8	196.8	194.5	195.9	196.8	196.9	196.8	198'4	199.9	196.39
189.5	187.8	187.8	185.2	186.3	186.1	186.1	190.0	191.9	191.8	191.8	191.5	191.78
187.7	187.8	188.9	188.9	189.1	189.1	187.5	190.8	190.4	193.1	193.7	195.7	189.43
191'8	191.8	191 .2	191.2	192.4	192.4	193.6	193 .1	192.5	195.9	194.2	196.9	191.90
191'4	192.2	192.0	193.6	193.6	193.7	10010	10010	105:0	105.7	170.0	176.9	188.43
				15040		189.0	189.0	187.8	185.7	178.6	1/6 9)	ļ
184.6	184.2	181.6	181.7	178.6	176.3	177.1	156.4	160.8	170.4	181.4	183.0	180.48
190.0	185.9	186.0	184'3	179.3	182.4	179.8	171.4	180.0	181.3	176.6	181.4	182.48
180.0	180.7	180.0	179.4	179.9	179.9	180.6	180'4	180'4	177.1	179'9	182.2	182.27
180.0	177.5	178'1	173.4	176.4	176.4	170.5	162.4	164.8	179.5	179.5	180.0	178.16
173.7	173.7	174.7	174.4	174.4	174.4	176.8	178.2	178.2	178.2	181.0	181.8	177:30
187.9	187.9	187'9	189.2	190.0	190.8	20212	1051	100.0	107.1	104.4	199.9	187.73
					l .	200.2	195.4	190.3	187.1	184.4		
202.2	204.2	203.5	191.9	192.8	195.4	194.0	194.7	191.6	190.7	194.9	199.2	197:39
187.4	187.4	188.0	187.6	187.9	188.0	183.1	187.0	188.8	188.8	177.5	184.2	190.03
180.6	182.0	179.1	176.3	177.0	174.8	174.5	176.4	178.7	176.6	172.8	175.3	180.95
175.9	176.9	174.4	174.5	175.5	175.5	175.5	176'3	176.6	178.1	180.5	181.3	176.98
174.2	174.7	174.7	175.8	175.8	176.6	159.7	166'9	169.8	174.2	172.6	178.9	174.70
182.4	182.4	182.4	181.8	178.7	178.4					150.0	179.6}	177.24
	-	. —			. —	170.6	173.9	177'9	178.9	173.6	179.63	
174'2	173.7	175.8	176.8	175.3	176.4	175.8	178.6	177.3	176.7	175.4	175.4	177.25
169.3	168.6	169.3	169.0	167.3	166.8	168.8	168.8	170.0	170.0	171.3	175.4	169.74
186.39	186.67	185.62	185.07	184.61	183.81	183.81	183.08	183.26	183.88	185.03	187:20	185.69
				TEMPER	ATURE OF	TUP VPDT	ICAL FORC	P MAGNET				
		l -	I	l	l .					^		
72°0	7i°8	71.7	7 i · 9	7η7	7 °5	71.2	70°5	7 0° 3	78°0	69°7	69°4	70°53
69.8	69.1	69.0	69.0	68.0	67.8	67.9	67.5	67.0	66.7	66.4	65.6	68.59
68.8	68.8	68.8	68.2	68.4	68.0	67.6	67.8	67.6	67.6	67.2	67.4	67.51
68.0	67.8	67.7	67.8	67 .2	67.3	67.0	66.7	66*4	66*2	65.8	65.8	67.44
64.9	64.9	64.8	64.6	64.0	63.8	63.2	62.6	62.1	61.8	61.6	61.4	63.92
63.6	63.2	63.4	63.6	63.0	62.2						— 1	61.99
			_			60.0	59.9	5 9.8	59.5	59.3	$\frac{-}{59\cdot 3}$	
65*4	65.6	65.6	65'1	64.8	64.4	63.7	62.8	62.5	61.6	61.0	60'6	63.00
67.1	67.5	67.4	67.2	66.6	66.0	65.2	64.8	64.4	64.0	63.6	62.8	64.74
69.2	69.5	69.5	69.0	68.8	68.6	68.4	67.6	67.2	66.7	66.6	65.4	67.14
68.6	68.6	68.0	68.2	68'1	67.7	67.6	66.6	65.8	65.0	64.6	63.6	67.05
66'4	66.6	66.4	66.0	65.6	65.4	64.9	64.6	64.4	63.7	63.1	63.0	65.22
67.0	66.6	66.6	66.1	65.7	65.2		-				— }	66'10
		-			_	68.0	67.5	67.1	66.9	66.2	66.0}	
72.6	72.9	72.6	72.8	72.0	71.6	71.2	71.0	70.7	70.2	69.7	69.0	70.40
71.2	71.3	70.8	70.8	70°3	70.2	70.2	69.2	68.2	68.0	67.8	68.2	70.02
73.0	73.0	72.7	72.5	72.5	72.0	71.6	71.0	70.6	70.4	70.2	69.5	70.73
73.7	74.2	74.2	$74^{\circ}2$	74.0	73.2	73.0	72.9	72.7	72.0	71.5	71.2	72.09
75.7	75.2	75.0	74.5	74.4	73.7	73.3	73.1	72.5	72.0	71.4	70.8	73.17
68.1	67.7	67.4	67.0	66.5	66.3						59 .6}	66.66
				_		60.0	60.0	60.0	60.0	60.0	59.6 ∫	
63.6	63.6	63.7	64.0	64.2	64.1	63.8	63.2	63 .2	62.6	61.8	61.2	62.40
69.2	69.6	68.8	68.6	68.2	68.0	67.4	66.8	66.6	66.4	65.6	65'1	66.27
72.3	72.4	72.7	73.5	73*3	72.9	73.0	72.5	71.5	71.1	70.7	69.9	70.18
75.5	75.3	75.1	75.1	74.6	74.4	73.6	73.0	72.4	71.9	71.3	71.0	72.82
74.6	75.0	74.9	74.5	74.4	74.2	74.0	73.7	73.7	73.2	73.3	73.0	73.13
73.0	72.8	72.6	72.4	72.4	72.3						$\frac{-}{71.5}$	72.47
						73*1	72.7	72.5	72.2	71.7	71.5	
75.2	75.7	75.6	75.5	75.0	74.9	74.5	74.3	73.9	73.7	73.2	73.0	73.67
78.0	78.1	78.1	77.7	77.5	77.1	76.9	76.6	75.8	75.0	74.8	74.5	76.33
70°30	70.26	70.12	70.00	69.68	69.35	68.87	68.43	68.05	67.64	67.25	66.85	68.60

	On	e Scale Div	ision = '00	0067 parts o	f the V. F.	VERTI Increase, in	CAL FOR	CE.	sponding to	1° decrease	of Temperat	ure, 1°64.	
Mean G	Göttin-}	Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h •	6 ^h •	7 ^h •	8h.	9h,	10 ^h .	11h.
	$egin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix}$	Sc. Div. 174'8 160'7 169'0 170'0	Sc. Div. 172 3 163 7 167 7 171 8	Sc. Div. 169 5 167 4 168 1 170 5	Sc. Div. 169 5 169 9 167 1 174 6	Sc. Div. 168 6 167 0 169 4 176 5	Sc. Div. 169 7 169 8 170 8 176 5	Sc .Div. 170'9 171'0 172'8 175'5	sc. Div. 163.8 172.5 174.3 174.7	Sc. Div. 165 7 174 3 176 3 175 0	Sc. Div. 165 ' 7 176 ' 0 175 ' 1 174 ' 6	Sc. Div. 167'9 176'0 179'5 173'0	Sc. Div. 171 ° 0 175 ° 1 178 ° 8 172 ° 5
	5 6 7 8 9 10 11	144.4 180.5 180.7 179.7 172.7 161.3	166.5 181.2 183.0 177.9 170.9 163.4	166°1 179°5 185°5 176°3 169°1 161°5	170.7 179.0 184.3 175.0 166.4 156.4	171°5 180°4 182°0 172°2 163°8 157°5	172.7 177.8 181.2 172.3 162.0 158.4	171.0 176.4 180.2 168.9 160.6 160.3	172.3 174.8 178.5 169.3 161.7 160.3	173 · 4 177 · 4 177 · 7 173 · 3 160 · 4 163 · 3	172.8 179.3 177.8 174.5 158.6 164.3	175°5 177°2 179°8 175°0 159°0 171°9	179°0 175°3 179°8 175°6 158°3 177°8
JULY.	12 13 14 15 16 17 18	172°3 182°7 185°3 190°5 191°4 182°8	168.0 186.2 188.8 185.2 191.4 183.7	167.2 181.4 185.0 187.5 190.1 184.6	169.7 181.4 188.0 187.5 188.0 184.7	168.7 180.6 189.1 188.1 186.9 184.6	170°8 181°5 190°1 189°6° 186°4 182°1	173.7 183.5 190.1 190.5 187.3 183.1	173.6 181.6 191.5 189.1 188.3 185.3	179 ° 8 184 ° 6 190 ° 3 191 ° 5 184 ° 3 186 ° 7	184.0 187.0 190.8 191.1 184.3 186.7	186'9 187'5 192'9 191'1 182'1 186'8	184'2 190'8 193'8 190'8 184'9 186'3
	19 20 21 22 23 24 25	180°4 177°2 176°8 170°2 175°3 182°9	178.5 176.0 177.2 172.9 175.9 180.5	177°3 175°0 177°2 173°0 175°5 180°5	176.0 174.5 176.2 171.0 174.9 175.6	175.0 172.9 178.0 169.7 172.3 172.1	175.0 169.1 177.9 169.8 173.6 171.4	176.0 168.4 177.0 168.9 173.3 171.6	173°5 168°4 175°2 167°9 176°5 174°4	175 · 4 167 · 4 174 · 2 169 · 9 179 · 8 180 · 2	175.5 168.3 174.0 173.1 178.7 178.7	173.9 168.8 168.3 173.4 183.5 178.4	172.7 170.0 172.7 174.1 183.2 176.4
	26 27 28 29 30 31	179°0 176°8 173°4 162°7 168°9	178.5 179.5 173.0 162.3 168.8	175 · 4 178 · 1 166 · 6 165 · 6 168 · 8	174.2 178.6 164.6 163.9 171.7	174 ° 2 176 ° 6 162 ° 8 162 ° 6 167 ° 9	170°4 173°6 161°6 163°1 168°6	169°2 172°2 164°1 162°6 168°7	169°2 171°5 174°1 161°8 169°9	171 · 4 173 · 2 167 · 9 160 · 5 173 · 9	173°5 171°4 167°6 164°7 171°5	174.5 171.4 163.4 166.0 172.4	176.4 174.3 164.9 171.7 176.6
Hourly	Means	174.90	175.73	174.90	174.57	173.74	173.55	173.62	173.85	175.10	175.54	176.15	177:30
		0	1 . 0 _		75.8	76.7	1 0	77.5	$\frac{1 \text{AGNET.}}{77.5}$	7 [°] 7.9	78°3	78°3	78°1
	$\left(egin{array}{c} 1 \\ 2 \\ 3 \\ 4 \end{array} ight)$	74·3 73·6 72·5 70·3	75.0 73.8 72.5 70.7	75.2 74.3 72.9 71.1	75.8 74.7 73.5 71.6	75.0 73.9 72.0	77.3 75.5 74.5 73.0	76.4 74.6 73.6	75.7 74.6 74.3	75.8 74.6 74.5	75 · 9 74 · 7 75 · 3	75.9 74.8 75.7	75·7 75·0 75·8
	5 6 7 8 9 10 11	73.7 73.0 70.2 72.1 76.1 77.5	74·1 72·6 70·0 72·5 76·3 78·0	74.5 72.2 69.6 73.0 76.6 78.2	74.6 72.7 69.8 73.7 77.5 78.3	75·1 73·5 70·0 74·3 78·3 79·0	75.2 73.8 70.5 74.2 79.7 80.0	75.4 73.8 70.7 74.3 81.2 80.5	75.6 74.0 71.1 74.1 82.0 80.8	75.8 74.2 71.5 74.1 81.6 80.9	76.8 74.3 72.8 74.5 82.6 80.7	77.3 74.9 73.5 74.2 83.7 80.3	77.9 75.2 74.0 75.0 83.2 80.3
JULY.	12 13 14 15 16 17 18	73.4 69.7 65.1 65.0 64.6 65.6	73·2 69·8 64·8 65·0 65·0 66·4	73·4 70·0 65·5 65·5 65·4 66·5	73.5 70.5 66.0 65.5 66.0 67.7	73.5 70.3 66.0 65.6 66.7 68.0	73.7 70.3 66.2 66.0 67.6 69.2	73.7 70.3 66.4 66.0 67.4 69.0	73.7 70.2 66.0 66.0 68.0 69.6	74·2 70·2 66·1 66·5 68·5 70·0	74·3 70·3 66·6 66·7 69·3 70·7	74.4 70.1 66.3 66.9 69.5 71.0	75.2 69.7 66.6 67.3 69.6 71.3
;	19 20 21 22 23 24 25	71·4 72·5 72·4 72·1 73·7 70·5	71.5 72.5 72.0 72.1 73.8 71.3	71.5 72.8 72.0 72.5 73.4 71.5	$ \begin{array}{c} - \\ 72.0 \\ 73.5 \\ 72.3 \\ 73.2 \\ 73.0 \\ 72.0 \end{array} $	72·5 74·0 72·5 73·7 73·0 72·8	73·1 74·0 72·7 74·0 73·0 73·3	73.7 75.5 73.0 74.3 72.5 73.5	74·2 75·6 73·5 74·5 72·5 74·0	74.4 75.9 73.7 75.4 72.3 74.8	74.7 76.5 74.3 75.8 72.5 75.1	75°3 76°5 74°5 76°1 72°5 75°5	75.5 76.5 74.7 76.3 72.5 76.0
	26 27 28 29 30 31	72·1 70·5 72·8 76·8 76·0	72'3 69'3 73'3 77'2 75'8	73.0 71.6 73.9 77.4 75.5	73.0 71.5 74.8 77.5 76.0	74.5 71.9 75.5 78.0 75.9	74.5 73.1 76.3 78.6 75.8	74.5 73.4 77.0 78.7 76.4	74·1 73·8 77·3 79·2 76·5	74·3 74·4 77·3 79·7 76·7	74.5 74.5 78.0 80.3 77.0	74.8 75.0 78.6 80.7 77.7	75.0 74.8 78.9 80.7 77.5
	Means	71.76	71.88	72.18	72.60	73.04	73.52	73.83	74.01	74.27	74.70	74.96	75.15

² Four minutes late.

b Fifteen minutes late.

	One Scale	Division =	•000067 par	rts of the V		RTICAL F		orrespondin	g to 1° decr	ease of Tem	perature, 1	64.
12 ^h .	13 ^h .	14h.	15h.	16 ^h .	17h.	18h.	19h.	20h.	21h.	22h.	23 ^h •	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 151'4	Sc. Div. 148 6	Sc. Div. 166.7	Sc. Div. 168.70
172.7 178.4	176°3 178°4	171°3 174°6	175°6 174°3	176°4 175°7	175.6 172.6	173°9	172°3 166°7	158.7 166.8	163.8	157.0	168.4	170.63
181.2	181.9	180.9	176.7	170.2	166.6	149.7	157.9	166.7	168.0	171.0	168.2	171.20
174.2	174.3	172.3	174.7	174.8	175.0		_			l —		172.37
l —	_	_				170.9	173.1	167.6	164.0	167.6	$\left \frac{-}{163\cdot 2}\right\}$	1
176.8	178.1	171.7	173.5	166.2	171.2	171.4	157.4	167.7	175°4 180°3	177°7 181°0	181.0 180.0	170°96 178°85
176.6	179°2 175°5	179°5 175°5	179°3 174°5	179°3 174°3	179°4 176°2	179'4 172'4	178.9 172.3	179.8 170.4	170.7	178.8	180.0	177.94
179°5 175°2	173.8	171.9	171.9	171.8	170.2	168.1	169.5	170.2	168.3	172.0	173.2	172.86
159.8	161.9	162.4	161.3	162.3	160.8	160.8	160.0	155.4	152.5	145.2	157.3	160.96
169.5	167.5	167.5	162.2	164.1	158.9						$ \frac{-}{169\cdot 9}\}$	163.94
						163.7	163.7	165.2	164.7 170.5	161°3 164°5	169.9	173.15
178.2	178.2	174.6	175.6	174 . 5 178.0	169°1 181°2	169 ' 1 172 ' 9	168°3 176°6	169 . 4	184.7	186.7	183.6	183.13
188 2	186.5 190.7	186 .2 190.0	184.9 188.2	187.8	184.7	179.4	181.8	189.1	192.2	193.2	194.8	189.12
189.8	190.7	188.9	189.6	190.2	190.0	190.4	189.7	176.1	178.6	183.3	188.0	188.24
184.9	185.1	183.2	184.4	185.0	184.4	185.9	189.2	187.5	186.9	180.3	182.8	186.07
186.4	185.1	181.9	180.4	180.0	180.0			15014	174:0	174.6	$\left\{ \frac{179\cdot 4}{179\cdot 4} \right\}$	180.73
172.9	172.9	173.2	171.8	172.6	165.2	170°1 165°7	169°8 153°7	158 ·4 160 ·4	174°0 165°0	165.6	165.9	171.42
170.4	170.4	170.4	171.5	170.9	170.6	163.3	164.4	165.7	166.0	172.0	171.3	170.12
172.7	172.8	172.2	170.4	173.5	180.1	180.4	173.0	168.5	170.6	162.4	166.1	173.64
173.2	173.3	170.1	170.7	170.2 р	170.4	169.7	171.2	171.7	171.7	173.0	175.0	171:47
183.5	183.8	184.7	179.6	178.5	180.6	177.7	173.7	175.0	177.6	174.2	182.1	178.06
173.1	172.3	171.3	170.3	171.0	170.9	173.5	170.6	168.0	168.3	166.7	$\frac{-}{170.4}$	173.71
173.8	173.8	174.8	174.4	171.0	164.9	163.8	166.4	163.4	161.7	178.5	178.2	172.25
171.6	170.8	169.0	169.1	168.9	170.9	171.6	170.9	171.9	170.2	170.7	171.2	172.67
167.2	171.3	171.1	165.2	165.2	165.7	163.7	160.6	160.9	161'1	161.1	166.1	165.97
173.4	169.8	163.5	155.7	154.6	154.6	156.2	156.5	165.4	166.5	166.5 169.5	167.7 174.3	163°25 169°00
171.9	171.9	177.4	169.4	170.3	170.3	158'4	162.6	157.3	154'9	170.49	173.70	173.72
176.23	176.53	175.25	173.89	173:39	172.68	170.26	169.30	168.64	169.61	170 49	175 10	110 12
								CE MAGNET		1 0	0 :	0
77.9	77.5	77.1	76°6	76°2	76°0	75°8	75.5	75.0	75.0	74.4	73.9	76.37
75.9	75.8	76.0	76.0	75.6	75.2	74.5	74.3	74.2	73.8	73.7 70.8	72·4 70·2	74 · 99 73 · 42
75°0 76°4	75°0 76°6	74.4	73.8 75.4	73°5 75°0	73°5 74°6	73.0	72.2	71.6	71.0	70 8	70 2	· ·
10 4	100	75'8	10 4	75 0		75.9	75.6	74.9	74.5	75.0	73.9	74.23
77.7	77.5	77.0	76.7	76.5	76.2	75.5	75.2	74.9	74.4	73.8	73.0	75.60
75.2	75.0	74.5	74.3	74.0	73.2	72.6	72.4	72.0	71.7	71.6	70.8	$73.40 \\ 72.31$
74·4 75·8	74.4	74.6	74.5	74.2	73·7 75·5	73.4	$73^{\circ}2$ $75^{\circ}0$	72.7 74.8	72.5 74.7	72°3 74°9	71.8 75.0	74.65
82.2	76°1 82°1	76°4 81°8	76.1 81.5	75.8 80.5	80.4	75.2 80.0	79.7	79.4	79.2	78.8	78.4	80.13
80.1	80.0	80.0	80.3	80.0	79.7	_					—)!	78:57
	.—					76.6	76.5	75.8	74.9	74.0	73.2}	73.65
75.2	75.0	74.9	74.9	74.3	74.0	73.7	73.0	72.4	71.7	71 . 2	71.2 65.3	68.88
69.7	69°2 67°0	69.0 67.0	68.6 67.0	68°2 66°6	67.8 66.6	67°5 66°3	67.0 65.3	67.0 65.0	66'4 64'5	64.4	63.8	65.92
68.0	68.0	67.6	67.3	67.0	66.7	66.5	65.8	65.4	65.0	64.6	64.0	66.12
69.8	69.7	69.5	69.2	69.0	68.6	68.0	67.1	66.6	66.2	66.4	65.6	67.65
71.2	71.5	71.5	71.0	70.7	70.0			71.0	71:6	71.0	$\frac{-}{70.5}$	69.98
75.8	75.0	7	7	75.4	75:0	72°0 74°5	71.6 74.3	71.6 74.0	71.6 73.6	73.0	70.3 7	73.95
76.3	75°6 76°0	75°5 75°7	75°5 75°3	75.4 75.2	75.0 74.8	75.0	74.5	74.0	74.0	73.2	72.8	74.71
74.7	74.5	74.7	74.1	73.7	73.0	72.9	73.0	73.1	72.7	72.5	71.5	73.25
76.4	76.4	76.3	75.9	75.6	75.2	74.9	75.1	74.8	74.5	74.0	74.0	74.71
72.5 76.0	72.5	72.5	72.7	72.7	72.5	72.3	72.0	71.6	71.2	71.2	70.2	72.45
70 0	76.2	76.2	76.2	76.0	75.8	74.6	74.0	73.2	73.0	73.0	$\{-72\cdot 5\}$	74.05
75.0	75.2	74.2	74.3	74.0	73.7	73.2	72.3	72.0	71.6	71.0	70.8	73.21
75.0	75.0	75.0	75.3	75'1	74.8	74.3	74.3	74.2	74.2	74.7	74.2	73.76
78.5	78.2	78.5	78.2	78.7	78.2	78.2	78°0 78°5	77.8	77:3	77.0	76.7 76.4	77°08 78°79
Q∩•►						1 70.7	1 7815	78.0	77.5	77.0	1 10 4: 1	10/9
80.7 77.5	80.5	80.1	80.0	79.5	79.3	78.7						
80.7 77.5 75.20	80.5 77.3 75.11	74.91	76.2	$\frac{79.5}{76.2}$	75.9	$\frac{75.4}{73.72}$	74.7	74.1	$\frac{73.6}{72.63}$	$\frac{73.4}{72.34}$	$\frac{72.5}{71.77}$	75.84

	Or	ne Scale Div	ision = '00	0067 parts o	of the V.F.		CAL FOR		sponding to	1° decrease	of Temperat	ture, 1°64.	
Mean (Göttin- }	0 ^h .	1 ^h .	2 ^h .	3h.	4h.	5 ^h •	6 ^h .	7 ^h .	8 ^h •	9 ^h .	10 ^h .	11 ^h .
	, 1	Sc. Div. 174.9	Sc. Div. 175 0	Sc. Div. 171°4	Sc. Div. 171 5	Sc. Div. 170°5	Sc. Div.	Sc. Div. 173.6	Sc. Div. 170°7	Sc. Dv. 171 7	Sc. Div. 174.5	Sc. Div. 175 9	Sc. Div.
	2 3 4 5 6 7 8	177'3 167'8 167'9 163'2 143'7 158'2	170.6 171.3 167.4 162.1 153.3 157.2	174.7 170.0 165.5 159.7 156.2 164.4	172.9 169.7 164.6 158.8 158.5 165.4	171.8 167.6 162.6 159.3 162.3 167.7	170.6 166.8 161.8 158.8 165.7 171.6	170.8 165.4 161.8 157.0 165.4 171.6	172.0 164.6 161.8 159.1 166.5 172.3	171 · 4 165 · 7 160 · 3 158 · 2 165 · 7 175 · 0	169.0 164.0 159.8 159.7 180.9 179.6	169 ° 0 162 ° 3 161 ° 7 159 ° 3 169 ° 2 175 ° 8	170.7 162.0 157.5 164.3 167.9 171.0
IST.	9 10 11 12 13 14 15	169.8 182.8 182.0 169.8 170.7 161.4	169.8 182.0 180.8 164.4 174.1 168.1	174.8 179.6 179.8 159.7 166.2 169.9	176.8 178.7 179.8 162.6 165.0 169.5	176°2 175°5 177°3 164°5 166°5 168°5	175 · 8 a 174 · 8 172 · 2 165 · 5 167 · 5 c 169 · 5	176°4 175°0 172°2 165°8 166°8 169°5	174.8 173.3 173.5 166.7 166.8 170.7	172.5 174.6 177.8 167.2 172.9 169.9	174.0 175.9 177.1 168.7 176.0 169.6	173 · 4 173 · 1 179 · 7 167 · 2 181 · 1 172 · 3	173 · 4 174 · 5 182 · 6 166 · 0 173 · 1 175 · 7
AUGUST.	16 17 18 19 20 21 22	174.5 181.2 182.2 184.4 186.1 178.1	176°5 182°7 186°2 184°1 185°0 176°2	176°2 183°1 186°2 184°9 183°7° 178°2	175°3 181°9 185°7 184°9 181°4 175°3	174.2 180.3 186.2 182.5 179.8 175.2	174.0 178.7 186.3 185.3 177.9 174.6	175.5 180.9 187.0 184.1 176.5 174.7	178°0 182°8 185°5 183°6 175°0 175°9	176.9 182.5 184.9 183.6 177.5	177.0 181.7 187.6 184.4 179.4	175°5 183°2 186°4 184°4 179°0 184°0	175.0 183.2 185.3 184.4 181.8 183.4
	23 24 25 26 27 28 29	182°1 174°7 182°6 181°5 176°2 175°0	178 · 9 184 · 6 181 · 6 179 · 2 178 · 3 171 · 7	179 · 9 183 · 8 179 · 8 178 · 9 175 · 9 170 · 5	177 · 2 181 · 0 176 · 9 177 · 7 174 · 7 169 · 2	174.4 179.2 174.9 175.3 174.4 169.0	173 · 2 178 · 1 174 · 0 172 · 7 173 · 3 167 · 0	173°5 176°8 172°1 169°5 175°3 168°6	175 ° 4 178 ° 3 172 ° 1 169 ° 1 177 ° 4 170 ° 9	170°3 179°7 173°0 174°5 176°9 170°6	177.5 177.8 171.9 179.3 174.2 172.2	182.1 176.7 171.4 183.7 189.3 176.7	190°8 180°8 171°8 199°6 188°8 175°4
	30 31	171.9	171.0	168.0	166.8	166.7	165.2	164.7	163.8	163.6	163.7	164.8	162.3
Hourly	y Means	173.85	174.31	173.88	173.15	172:39	171.93	171.94	172.33	172.76	174.42	175.28	176.1
	C 1	72.2	73.3	78.5	TEMPERAT	74.4	HE VERTICA	AL FORCE 1	75°0	7Š·5	76°1	76°0	76°3
	1 2 3 4 5 6 7 8 9 10 11	71'3 73'0 76'3 78'2 76'5 75'5 72'1 69'5	71.5 73.5 76.5 78.1 76.0 75.2 — 71.9 70.0	73°5 — 72°0 74°0 77°0 78°0 76°3 76°0 — 71°6 70°2	72.5 74.3 77.7 78.5 76.5 74.5 — 71.7 70.5	74.4 	74·9	75 1 74 7 76 5 80 2 80 6 78 3 74 7 74 0 72 8	75 0 75 3 77 5 80 5 80 7 79 0 75 5 — 74 2 73 0	75 5 76 0 78 0 81 0 80 8 79 3 75 5 74 3 73 2	77.0 79.0 81.6 81.0 79.5 75.8 — 74.8 73.5	77.0 79.5 82.0 81.4 80.0 75.7 — 75.5 74.0	77:2 80:0 82:2 81:4 80:4 75:7 75:7 74:2
AUGUST.	12 13 14 15 16	70.0 74.0 73.5 73.0	70°3 74°0 73°5 73°6	70°3 74°3 74°0 73°7	70.8 74.3 74.9 74.3	72:3 75:0 75:2 75:0	73.0 76.0 76.1 76.0	73.7 76.5 76.2 76.5	74.3 77.1 76.5 77.0	74.8 77.5 76.7 77.2	75.5 77.0 77.0 78.0	76°2 77°3 77°3 78°5 —	76:3 77:7 77:5 78:5
AUG	17 18 19 20 21 22	71.5 68.3 65.7 67.5 67.0 70.6	71.6 68.3 66.0 67.3 67.3 70.4	71.6 68.5 66.3 67.0 68.0 70.3	72·3 68·7 66·3 66·7 68·2 70·2	73.0 69.2 66.5 66.8 69.0 70.2	73.5 69.5 67.0 67.0 70.0 70.7	73.7 69.4 67.3 67.0 70.5 71.0	73.7 69.2 67.5 67.0 70.6 71.2	73.7 69.3 68.0 67.5 71.0 71.3	74.0 69.5 68.4 67.6 72.0 71.7	74.2 69.8 68.3 68.0 72.2 71.7	74·2 70·0 68·5 68·3 72·7 71·7
	23 24 25 26 27 28 29	68.5 66.7 69.5 69.5 70.8 71.7	68.7 67.4 69.5 69.8 70.5 71.9	68.8 68.2 70.5 70.3 70.5 72.3	69°4 69°0 70°7 71°1 70°7 72°7	70°5 69°7 71°0 71°8 71°0 73°5	70.8 70.0 71.6 73.0 71.7 74.4	71·1 70·5 72·0 73·5 72·0 75·1	71·1 71·0 72·5 74·0 72·7 75·2	72.4 71.3 73.0 74.2 73.3 74.8	72.5 72.0 73.5 75.0 74.3 74.7	71.7 72.3 73.7 75.0 74.5 74.4	71.6 72.8 73.5 74.5 74.6
	30	72.3	72.5	73.5	74.0	74.6	75.0	75.2	76.0	76.5	77.0	77.5	77:5
U anni	y Means	71.33	71.48	71.80	72.08	72.72	73.38	73.78	74.13	74.47	74.92	75.14	75.2

^a Fourteen minutes late.

	One Searc	Division =	000067 pa	its of the v	. F. Increa	se, in Scale	Divisions, co	rresponding	io i decre	ase or Temp	perature, 1.6	Daily an
12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^b .	18h.	19 ^h .	20h.	21 ^h .	22h.	23 ^h .	Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 170'9	Sc. Div. 171.5	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
78.2	173.6	172 0	170 9	171 0	1/1 9	157.8	156.1	161.0	161.6	164.9	$\left \frac{-}{172.9} \right\}$	170.4
70:0	174.8	169.3	166.5	168.0	168.0	169.4	165.2	169.1	170.4	169.7	168.9	170.4
70.9		161.3	162.4	160.3	161.9	162.7	162.2	162.2	162.2	163.6	167.0	164.4
63.5	160.3	158.7	158.6	158.6	158.6	159.0	159.6	157.8	157.8	158.9	159.0	160.6
60.2	156.7 168.1	159.0	140.3	114.8	91.9	151.4	152.5	150.6	80.0	106.4	143.8	147.4
59.9		160.4	161.7	139.9	149.6	144.6	90.8	128.7	150.2	140.4	150.8	154.4
55.5	167.5				165.8	144 0	30 0	120	100 0	-		
70.8	170.4	169'4	170.5	160.3	103 8	145.6	162.7	161'1	165.5	163.6	169.0}	166.8
70:0	170:0	177°3 b	176.9	179.7	160.2	161.8	162.0	169.9	169.6	177.8	180.7	172.7
72.0	176.6		176.3	173.7		176.1	161.0	168.7	175.2	179.3	179.8	174.5
70.1	170.6	175.2	169.1	169.3	175.0		160.8	154.9	147.7	145.3	162.0	170.2
77.8	170.5	171.3	171.3	168.4	166.7	155.4	129.3	162.6	162.0	165.3	170.8	162.8
66.0	166.0	166.2	167.0	167.0	152.5	146.4	151.3	140.0	149.3	162.9	161.3	163.7
69.7	167.8	169.8	161.8	147.8	164.6	136.7	101 0	140 0	143 0	102 3	l i	
71°4	167.9	169'4	163.1	163.6	134.3	144:7	136.1	158.7	158.9	154.0	$ \frac{-}{164\cdot 0}\} $	163.3
					170.0	144.7	150 1	178.7	180.1	180.1	179.8	175.9
75.9	173.0	174.7	170.0	176.2	176.6	175.0	175.0		182.4	183.3	185.0	182.4
32.3	183.2	185.0	184.0	183.3	177.0	183.1	184.0	183.0	182 4	182.9	184.7	184.3
85.3	183.8	184.2	184.8	185.2	184'6	183.8	173.8	178.4		182 9 176 9	184.7	183.7
34.4	183.7	183.8	183.4	184.6	183.9	183.9	184.3	183.5	182.5		170.0	
79.1	179.1	178.0	175.7	174.5	174.0	172.7	168.0	167.9	172.7	176.3	178.2	177.4
80.4	181.6	180.0	179.1	179.1	179.1		170.4	100:1	180.5	181.4	$_{181\cdot 7}$ }	178.7
-						178.3	179.4	180.1				170.0
86.5	186.5	184.6	174.1	187.0	183.2	171.7	176.2	176.2	178.3	179.6	177.9	179.0
78.9	179.2	178.5	181.5	182.8	176.7	175.0	170.2	177.9	177.6	170.9	174.9	178.1
71.5	171.8	172.4	175.3	169.6	169.3	171.3	169.9	173.4	169.6	173.1	173.1	173.4
93.3	176.7	173.1	173.0	174.5	171.6	164.8	168.5	168.5	172.3	172.4	176.4	176.0
76.2	171 1	170.0	155.7	155.6	167.9	169.7	162.5	162.9	168.6	167.7	166.8	172.0
76.9	182.7	180.7	179.9	177.6	172.1	l —					- J	172.1
		_				163.9	164.7	165.5	167.8	170.4	171.9	
63.2	165.2	161.8	162.4	164.8	165.1	165.6	167.8	166.9	166.8	168.8	168.6	165.8
74.23	173`40	172.58	169.93	167.62	165.47	164.25	161.32	165.71	165.15	166.77	171.30	170.8
						THE VERT	ICAL FORC	E MAGNET.	0	0	1 0 1	0
76°3	76°2	75.7	75°5	75.3	75°·3	-		_			$\left \begin{array}{c} \overline{}_{72\cdot 5} \end{array}\right\}$	74.5
_					. —	74.3	73.7	73.1	72.8	72.2	72.2	74.89
76.6	76.8	76.6	76.2	76.4	76.1	75.5	75.5	74.7	74.5	73.7	73.3	
80.5	80.7	80.0	79.5	79.3	79.2	78.7	78.5	78.4	78.0	77.2	76.5	77.6
82.3	82.2	82.3	82.0	81.8	81.2	81.0	81.0	80.6	80.2	79.8	79.2	80.3
81.4	81.2	81.4	81.2	82.2	81.8	81.0	80.7	78.8	79.5	79.5	79.0	80.2
80.4	80.3	79.7	79.5	79.5	79.0	78.7	78.5	79.0	77:9	76.5	76.5	78.4
75.6	75.4	76.0	75.7	75.5	75.2				70.7	70.7	$\{-72.0\}$	74.7
				_		73.3	73.5	73.2	72.7	72.5		
75.7	75.5	74.2	73.7	73.5	72.7	72.5	72.0	71.2	71.0	70.1	69.6	73.0
74.3	74.5	73.7	73.1	73.2	72.3	72.8	71.3	71.2	71.0	70.6	70.3	72.19
76.5	76.0	76.4	76.4	76.3	75.9	75.5	75.2	74.7	74.7	74.7	74.3	74.3
77.8	78.0	77.8	78.0	78.2	78.0	77.2	76.8	76.1	75.5	75.2	74.5	76.4
77.6	77.5	77.3	78.2	78.0	76.3	76.1	75.7	75.2	74.7	74.2	73.6	75.9
78.7	79.0	78.8	78.2	78.2	78.2				<u> </u>	——————————————————————————————————————	$\frac{-}{71.5}$	75.7
	_		_	<u> </u>		73.0	72.8	72.5	72.2	71.7		
74.3	74.0	73.6	73.0	72.4	71.5	71.1	70.8	70.4	70.0	69.6	69.2	72:3
70.0	69.8	69.6	69.5	69.3	68.6	68.2	67.8	67.6	67.5	66.9	66.2	68.7
68.2	68.2	68.2	68.5	68.3	68.2	68.3	68.0	67.6	67.7	67.9	67.8	67.6
68.4	68.2	68.2	68.2	68.3	68.3	68.0	68.0	68.0	67.6	67.5	67.1	67.6
$72 \cdot 7$	72.7	$72.\overline{7}$	72.6	72.5	72.5	72.5	71.9	71.4	71.2	71.2	71.2	70.9
71.7	71.7	71.3	71.3	71.1	71.0						$\frac{-}{69\cdot 2}$	70.8
	'-'		,,,,,	`		70.8	70.7	70.5	70.0	69.5		
72.0	72.3	72.2	71.8	71.6	71.0	70.2	69.5	69.3	69.0	68.2	67.5	70.5
72.6	73.0	73.0	72.7	$72 \cdot 2$	$72 \cdot 2$	72.5	71.3	71.2	70.7	70.5	70.0	70.9
73.5	73.7	73.3	73.5	72.7	72.1	71.7	71.5	71.1	70.7	70.5	70.2	71.90
74.5			74.4	74.1	73.9	72.5	71.9	71.7	71.6	71.5	71.5	72.8
74.7	74.5	74.2		75.5	75.2	75.0	74.9	74.7	73.9	73.8	73.1	73.5
73.8	74.8	76.1	76.0 73.4	73.0	72.8	75 0	—			~		
	73.2	73.2	104	100	12 8	74.4	74.0	73.3	73.3	73.3	$\{-72.8\}$	73.5
77.5	77.3	77.2	77.0	76.7	76.5	76.0	75.7	75.4	74.8	74.6	74.4	75.6
0	1	1	}	1								

	Or	ne Scale Div	ision = '000	0066 parts o	f the V.F.		ICAL FOR Scale Divi		sponding to	1° decrease	of Temperat	ure, 1°64.	
Mean Go gen Tir	öttin-}	O ^h •	1h.	2 ^h .	3h.	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8 ^h .	9 ^h .	10 ^h •	11 ^h .
	1 2 3 4 5 5 S	Sc. Div. 169°1 165°9 163°6 142°5 153°1	sc. Div. 165 * 5 165 * 9 163 * 6 141 * 7 152 * 4	sc. Div. 166'5 165'0 162'8 149'2 154'3	sc. Div. 165 '7 164 '1 162 '7 156 '2 157 '9	Sc. Div. 164 ° 0 160 ° 9 162 ° 0 161 ° 9 162 ° 5	sc. Div. 161 1 159 7 162 5 164 1 167 5	Sc. Div. 160 5 159 5 162 4 166 9 169 3	sc. Div. 160°5 159°2 163°4 167°3 192°5	Sc. Div. 161 1 159 7 165 9 168 2 180 6	Sc. Div. 161 1 159 6 165 3 168 6 193 6	Sc. Div. 161'1 158'0 165'5 169'7 182'4	Sc. Di 160 ' 157 ' 164 ' 172 ' 174 '
	6 7 8 9 10 11 12	170'4 155'4 176'9 183'6 139'2 164'9	168°1 156°1 179°0 182°1 156°5 169°2	166°1 157°7 178°1 182°1 159°8 167°0	164'3 157'5 177'3 180'5 168'1 165'7	163°5 161°8 174°7 178°3 174°6 169°8	163.5 168.8 178.8 179.2 173.6 167.0	163 · 5 176 · 4 180 · 8 178 · 0 179 · 8 168 · 4	161.5 178.9 181.2 179.7 184.6 169.1	161 · 2 186 · 5 183 · 2 182 · 7 179 · 3 171 · 6	159.8 189.0 186.4 184.0 178.4 169.7	159.8 177.3 185.4 184.6 180.9 176.1	159° 173° 184° 184° 177° 171°
MB.	13 14 15 16 17 18 19	164.3 165.0 183.4 176.4 184.6 186.6	163.4 165.0 184.1 178.1 184.2 186.1	164.2 166.8 182.9 178.6 185.3 186.1	166°3 167°2 180°4 179°5 184°4 183°8	166°3 169°6 179°1 181°0 183°7 182°9	166.3 h 170.3 178.7 181.2 183.3 181.9	167.8 170.3 179.6 182.0 182.4 181.9	168.6 174.4 180.2 183.3 181.7	166.7 176.6 180.9 184.4 182.7 181.9	165:3 177:7 181:4 185:4 182:2 183:8	165 '9 176 '6 180 '1 188 '0 181 '5 181 '7	166: 177: 180: 187: 180:
	20 21 22 23 24 25 26	183 °9 114 °6 193 °0 175 °8 179 °1 187 °5	182 1 134 8 194 9 178 9 187 3 189 3	182.0 147.2 193.3 177.5 187.7 190.9	182.5 172.8 191.8 177.4 185.5 188.8	182.8 194.2 189.9 177.6 188.0 189.6	182.8 198.9 188.4 180.0 187.4 189.3	184.4 212.8 186.4 178.8 189.5 188.3	188°3 236°0 185°3 182°3 191°2 187°4	189 °9 236 ° 5 187 ° 7 183 ° 8 188 ° 6 190 ° 2	196.6 227.7 184.4 183.7 188.6 189.6	189 '9 222 '6 184 '4 184 '1 189 '1 188 '5	187: 213: 185: 182: 188: 190:
	27 28 29 30	196°1 192°4 186°3	197°1 192°4 187°0	196'6 192'3 186'0	195.4 190.6 182.5	194.0 188.2 182.5	193 .5 185.4 180.6	194.4 184.8 180.2	196.4 184.9 180.2	196.8 184.8 180.1	194.5 185.0 181.4	193.5 184.4 182.5	191° 184° 182°
lourly	Means	171.29	173.38	174.08	174.96	176.28	176.68	178.04	180.76	181.55	181.62	180.52	179
		1			TEMPERAT	URE OF T	HE VERTICA	AL FORCE	MAGNET.				1
	1 2 3 4 5	73.7 75.5 76.8 74.5 75.5	74°0 75°9 76°6 75°0 75°7	74·3 75·7 76·4 75·2 76·0	75.0 76.0 76.2 75.4 76.4	75.7 76.5 76.3 75.3 77.2	76·3 77·3 76·5 75·9 77·2	77°0 77°8 76°5 76°1 77°4	77.6 78.5 76.5 76.2 77.1	78·3 79·0 76·5 76·5 77·4	78.5 79.3 76.5 76.9 77.5	79·0 79·5 76·5 77·0 77·7	79°0 79°0 76°0 77°0
~;	6 7 8 9 10 11 12	74.5 75.0 67.5 66.8 68.4 73.2	75.0 74.8 67.5 66.5 68.7 73.3	75.5 75.5 68.0 66.9 69.0 74.2	76.5 75.5 68.1 67.5 69.7 74.9	77.0 75.5 68.7 67.5 70.5 75.2	77.5 75.5 68.7 68.5 71.2 75.9	78.0 75.5 68.7 68.6 71.7 76.0	78.8 75.6 68.5 68.7 72.3 75.8	79°5 75°7 68°5 68°2 73°0 75°4	80.0 75.4 68.6 69.0 73.6 75.3	80°3 75°0 68°7 69°3 73°7 75°0	80 : 74 : 68 : 69 : 69 : 74 : 67 : 5
SEPTEMBER.	13 14 15 16 17 18 19	74.0 73.1 65.5 65.7 64.2 63.7	74.0 72.5 65.5 65.5 63.9 64.0	74·3 72·5 66·0 65·3 63·7 64·6	74.5 72.5 66.6 65.0 64.4 65.0	75.5 72.3 67.3 65.0 65.1 65.7	76.6 72.3 67.6 65.5 65.6 66.5	77.0 71.7 67.6 65.5 66.0 66.8	77°3 71°5 67°6 65°5 66°5 67°7	78.0 71.5 67.8 65.5 66.6 68.5	78°5 71°7 68°3 65°6 67°3 69°5	78°5 71°5 68°5 65°6 67°5 69°5	78° 71° 68° 65° 67° 69°
	20 21 22 23 24 25 26	65.5 66.0 61.8 69.3 63.7 60.2	65°1 64°8 61°8 68°2 63°0 60°3	64.6 63.7 62.6 68.0 63.0 60.3	64.4 63.4 63.1 67.7 62.5 60.7	64.5 63.5 63.6 67.7 62.5 61.2	64.3 63.7 64.6 67.7 62.3 61.8	64.2 64.0 65.2 68.1 62.3 62.0	64.6 64.0 66.1 68.0 62.0 62.5	64.7 64.5 66.6 68.0 62.0 62.4	65°2 65°4 67°3 67°6 62°3 62°5	65.4 65.7 67.9 67.6 62.5 62.7	65: 65: 67: 62: 62:
	27 28 29 30	56.9 60.3 62.5	56.7 60.5 62.9	57.0 60.9 63.7	57.2 61.0 64.6	58.0 61.6 64.6	58.5 62.7 65.4	58 · 9 63 · 4 65 · 6	59°3 63°6 65°7	59°4 64°0 66°5	60.0 64.5 67.0	60.5 64.5 67.3	60° 64° 67°
lourly	Means	68.22	68.14	68:34	68.61	68.88	69.44	69.68	69.90	70.12	70.21	70.65	70

^{*} Forty minutes late.

	One Scale	Division =	·000066 pa	rts of the V		RTICAL E		orresponding	g to 1° decr	ease of Tem	perature, 1°	54.
12h.	13h.	14 ^h .	15 ^h .	16h.	17h.	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 163 9	Sc. Div. 163*9	Sc. Div. 163'2	Sc. Div. 162.6	Sc. Div. 164'1	Sc. Div. 162°6	Sc. Div. 164°1	Sc. Div. 163 11
160°8 157°1	161.7 157.3	161.9 159.2	161.8 159.4	164°0 159°5	160.7	160.5	160.1	158.7	159.0	163.1	163.6	160.52
164'9	164.9	164.7	164.7	164.7	164.7	143.0	164.8	151.5	129.8	144.2	159.7	160.22
172.2	172.6	173.2	168.4	165.3	165.6	162.2	142.6	140.4	139.7	140'6	143.6	159.01
175.5	167.8	162.8	151.5	159.2	164.5						170.4	167.75
						166.2	165.5	167.1	168.2	167.1		
159.1	159.6	159.2	159.0	161.9	161.6	159.1	150.7	152.2	149'1	154.5	153.6	160.01
171.4	171.4	174.0	173.3	173.4	170.6	174.0	174.9	174'9	175.0	176.5	174.6	171.77
183.1	181.9	182.4	182.3	182.3	182.3	182'3	183.7	182.8	182.2	182°2 158°5	183.5 174.0	181 . 55
184.8	184.7	180.4		179.6	180.0	180.0	178.6	169.8	159 ' 9 133 ' 5	156.2	168.8	166.80
176:2	170.7	167.3	172.8	158.9	163.1	164.3	165 .2	153.0	100 0	100 0	, ,	
171.6	168.9	168.4	166.2	166.7	167.7	162.7 a	159.8	133.9	144.0	157.8	[159.5]	164.89
165.8	165.8	166.2	163.2	156.8	159.5	126.6	153.9	154.6	159.1	145.2	165.7	161.44
175.6	175.2	175.2	175.5	180.9	177.0	176.9	179.6	179.6	180.9	180.9	181.6	174.85
180.3	180.3	180.1	182.3	182.3	178.7	176.4	181.1	181.0	179.9	178.6	173.7	180.23
187.2	187.7	187.7	185.6	185.6 c	185.2	185.7	185.6	186.2	182.7	184.4	184'0	183.87
180.3	180.4	181.7	181.2	180.3	181.4	182.7	184.2	184'3	185.2	179.6	180.7	182.44
178.9	176.8	176.8	178.0	178.8	177.7						180.7	180.22
	_				-	177.5	167.8	176.1	177.0	180.7		
187.7	199.6	203.9	203.7	189.6	191.5	200.0	167.5	182.6	151.2	131.2	129.3	182.09
510.3	196.4	193.9	192.4	188.8	183.3	168.6	186.3	184.5	181.0	180.6	191.8 175.6	190°38 184°77
190.5	184.5	182.1	180.8	185.7	180.6	179.1	178.8	177'2	180.2	175 · 4 182 · 7	179.1	180.83
182.7	181.2	180.7	180.1	180.6	181'4	181.4	182.9	183.5	183°5 178°4	169.4	185.4	185.78
189.7	189.7	190'4	189.4	184.9	186.4	180.7	181.8	181.8	1/0 4	109 4	100 1	}
189.3	189.1	186.6	186.6	186.6	186.6	189.3	185.1	191.2	193.6	195.9	195.2	189'38
191.2	100:0	192.1	192.2	191.9	192.5	192.0	192.2	192.4	192.5	192.3	192.0	193.55
191 5 184 ° 4	192°2 184°5	184.2	183.8	184.2	186.0	185.9	186.7	187.4	187.1	185.9	186.0	186.21
180.2	184.2	184.4	186.6	183.4	182.1	183.0	176.3	177.0	180.3	182.0	181.3	182.22
178.90	178.02	177.72	176.84	176.01	175.95	173.24	173.05	171.77	169.11	169.55	172.98	175.88
176 90	178 03	111 12	170 04						100 22			
					ATURE OF		1		0		0	
79°0	78.8	78.5	78°5	78.1	77.8	76°5	77.0	76°8	76·7	76.7	76.7	77:06
79.5	79.7	79.5	79.0	78.8	78.5	78.3	78.1	77.6	77.2	77.2	77.3	77:97
76.0	76.0	76.2	76.0	75.5	75.3	75.5	75.5	75.5	75.5	75.5	74.8	76.03
76.7	76.5	76.5	76.5	76.5	76.4	76.3	76.1	76.2	76.2	76.0	76.0	76.12
78.0	78.5	78.2	78.2	78.2	77.0		-	77:0	74·8	74.6	$\frac{-}{74.5}$	76.70
-				70.0	70:0	75.4	75.3	75.0	76.3	76.0	75.8	78.05
80.0	80.5	80.0	80.0	79.3	79.0	78.4	77.6	77'3 69'4	69.0	68.2	68.1	73.15
73.7	73.7	73.3	72.6	72.0 68.2	71.0 67.8	71.0 67.6	70·0 67·3	67.1	67.0	67.0	66.7	68.02
68.6 69.5	68.5 69.6	68'3 69'7	68.3	69.5	69.4	69.0	69.0	69.0	69.0	68.7	68.2	68.61
74.4	74.5	73.3	74.0	74.5	74.5	73.7	73.5	73.2	73.1	72.5	72.5	72.45
75.0	75.2	75.2	74.7	74.2	74.3	-					$\frac{-}{74.5}$	75.03
				~		75.3	75.7	75.7	75.5	75.5		
78.7	78.8	78.8	78.6	78.6	78.4	77.7	77.0	76.3	75.5	74.7	73.8	76.82
71.7	71.0	70.6	70.3	70.0	69.5	69.1	68.8	68.2	68.0	67.3	67.4	70.71
68.1	68.1	67.7	68.0	67.8	67.5	67.4	67.0	67.0	66.6	66.0	65.7	67.23
65.2	66.0	65.6	65.5	65.0	65.0	64.7	64.5	64.5	64.5	64.4	64.0	65'18
67:7	67.5	67.7	67.4	67.2	67.0	67.0	65.2	65.4	65.0	64.7	64.4	66.04
69.7	70.0	70.2	69.5	69.4	69.0	60.0	60.0	68.0	67.8	67.4	$\frac{-}{66\cdot 5}$	67.70
65.5	05.5	65:0	C4:0	64.6	65.0	64.8 64.8	68°0 65°0	64.8	64.2	63.8	66.4	64.91
65.6	65.5	65.2	64.8	64.6	64.5	64.2	64.0	63.7	63.2	63.3	62.6	64.45
68.6	65°4 70°0	65.5 70.3	65°0 70°5	64.8	70.2	70.0	69.7	70.1	70.0	69.8	69.5	67.42
67.0	67.0	66.2	66.2	66.3	66.0	66.0	65.2	65.0	64.7	64.2	65.7	66.91
62.0	61.7	61.7	61.2	61.2	61.3	61.2	61.0	60.7	60.6	60.6	60.2	61.88
62.2	62.2	62.2	62.2	62.4	62.2						57·5 }	60.98
_			_			58.7	58.2	58.7	58.3	58.0		
61.0	61.2	60.8	60.8	61.0	60.6	60'4	60.5	60.8	60.5	60.4	60.5	59.65
64.6	64.6	64.7	64.6	64.5	63.8	63.7	63.2	63.2	63.0	63.5	62.9	63.24
67.3	67.0	66.8	66.8	66.2	66.4	66.5	65 .2	65.2	65.3	64.9	64.6	65.66
											- 11	69.54

c Four minutes late.

	On	e Scale Divi	sion = •000	0066 parts o	f the V. F.		CAL FORC		sponding to	1° decrease	of Temperat	ure, 1 • 64.	
Mean Gö gen Tir	ttin- }	Oh.	1 ^h .	2h.	3h.	4 ^h .	5 ^h .	6h.	7 ^h .	8 ^h .	9 ^h .	10 ^h .	11h.
	1 2 3	Sc. Div. 183 2 184 7 198 4	Sc. Div. 184 '7 184 '7 199 '2	Sc. Div. 185 2 189 0 198 9	Sc. Div. 189°5 191°6 196°4	Sc. Div. 186°5 191°6 194°7	Sc. Div. 186°7 191°0 194°5	Sc. Div. 186°3 193°1 195°7	Sc. Div. 187 4 198 3 191 7	Sc. Div. 181 9 198 3 193 8	Sc. Div. 189 5 208 5 192 3	Sc. Div. 189 8 204 4 191 3	sc. Div 189'8 205'5 191'2
	4 5 6 7 8 9	197 ' 4 192 ' 4 189 ' 3 159 ' 3 186 ' 7 174 ' 4	198.7 192.0 189.3 134.7 186.7 176.7	197.7 192.1 190.9 140.3 185.4 181.8	196°3 189°7 186°9 172°6 184°3 184°9	195 ° 2 190 ° 4 184 ° 9 182 ° 9 184 ° 5 191 ° 6	192°1 190°4 184°9 183°4 184°5 195°4	190'4 189'5 184'2 188'5 187'0 198'4	190°3 190°9 187°5 193°8 185°3 197°2	189 '9 190 '3 193 '0 186 '8 186 '7 198 '0	189.6 191.8 194.4 186.3 186.7	188°9 190°8 190°9 186°3 188°2 195°7	187.5 190.5 190.1 187.7 188.9 195.0
OCTOBER.	11 12 13 14 15 16 17	195.5 190.7 197.6 198.7 197.6 197.7	193 · 2 190 · 5 198 · 4 197 · 7 198 · 0 198 · 8	193 '4 191 '6 197 '7 200 '0 199 '1 201 '2	193 · 2 191 · 2 196 · 4 196 · 6 199 · 5 202 · 1	191.7 192.3 195.3 195.7 199.0 201.9	191.5 a 192.0 195.5 195.6 198.5 201.1	191.5 191.6 197.3 196.8 197.6 200.6	193 · 2 195 · 5 196 · 9 198 · 4 198 · 8 200 · 6	194.9 196.0 196.9 197.9 197.4 202.4	190 · 9 196 · 7 196 · 9 196 · 2 198 · 1 202 · 3	191.8 198.4 196.0 194.7 196.2 201.1	190 '7 197 '8 196 '2 194 '0 195 '1 198 '3
00	18 19 20 21 22 23 24	209 · 5 205 · 8 205 · 5 197 · 7 213 · 5 208 · 8	209 · 5 204 · 7 205 · 2 200 · 4 213 · 7 208 · 8	207'4 204'7 206'5 200'9 213'8 208'7	208·3 203·0 205·2 202·5 214·6 207·0	206 · 1 b 201 · 5 204 · 4 202 · 7 214 · 5 204 · 2	204 ° 0 201 ° 3 204 ° 0 201 ° 8 211 ° 0 203 ° 6	205.6 201.5 203.7 211.4 211.0 203.6	205 · 2 201 · 3 203 · 0 202 · 6 211 · 0 203 · 2	204.4 202.6 204.3 207.2 211.9 204.7	205 · 4 202 · 6 202 · 8 208 · 7 208 · 7 204 · 8	206.5 204.0 206.2 208.8 209.0 199.6	217°5 206°6 207°0 210°5 208°6 204°4
	25 26 27 28 29 30 31	209.0 196.3 201.4 204.2 203.0 207.5	208.5 197.7 204.2 204.7 200.9 208.6	208.5 198.3 200.9 203.9 202.8 208.8	209°2 198°5 202°2 204°2 202°1 208°8	207 · 4 197 · 8 202 · 8 202 · 8 204 · 5 208 · 9	206·3 197·2 201·5 202·8 204·5 208·2	205 · 1 197 · 2 202 · 1 201 · 4 204 · 2 208 · 2	203 · 3 196 · 7 202 · 1 201 · 5 204 · 2 208 · 2	203.6 197.2 202.5 202.5 204.8 209.4	201.7 198.8 200.5 202.5 205.3 209.4	200°1 197°3 200°5 202°5 205°6 209°4	201°3 198°5 201°7 200°6 206°2 209°4
		196.21	195.93	197:39	197.66	197.62	197:16	197:91	198.08	198.49	198.82	198:30	198.9
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	1 2 3	64.4 59.0 57.0	63.8 53.8 5.5	63°4 58°6 56°0	63°3 58°6 57°1	62°7 58°5 57°5	62.8 58.5 57.7	63.0 59.0 58.5	62°8 59°1 59°0	63°5 59°2 59°0	63°4 59°3 59°3	63.6 59.5 60.0	62°5 60°0 60°0
	4 5 6 7 8 9	57.0 58.6 60.8 66.4 64.0 59.5	57.0 58.6 60.9 65.6 64.0 59.3	57.8 58.8 61.5 65.8 64.0 59.1	57.6 60.5 62.5 65.6 64.3 59.6	57.6 60.3 63.5 66.0 65.3 59.3	58.7 61.0 64.0 66.3 66.0 59.3	59.6 61.4 64.5 66.3 66.3 59.0	60°1 62°3 65°1 66°3 66°6 59°2	60.6 62.5 65.5 66.2 66.1 59.4	61.5 63.0 65.7 66.0 65.6 59.3	62:0 63:3 66:0 66:0 65:0 59:5	62.5 63.2 66.5 65.6 64.3 59.5
OCTOBER.	11 12 13 14 15 16 17 18	56.5 61.0 56.0 57.0 56.4 56.7	56.9 60.8 56.3 57.0 56.5 56.2	66.5 60.6 56.3 57.0 56.5 55.7	58.8 60.5 56.8 57.8 57.2 55.2	59·2 60·2 57·2 58·2 56·4 55·0	60°0 60°3 57°7 58°2 57°1 55°2	60.0 60.3 58.0 58.2 57.5 55.3	60.5 60.0 58.2 58.3 57.9 55.4	60.6 59.6 58.2 58.2 57.9 55.4	61.5 59.2 58.6 58.7 58.3 55.3	61.7 59.0 59.0 59.1 58.7 55.4	61.8 58.7 58.8 59.0 59.0 55.2
0	18 19 20 21 22 23 24 25	48.9 53.1 51.4 55.7 48.4 50.1	49°1 53°0 51°6 55°0 48°3 50°2	52.0 52.7 52.2 53.3 48.0 50.2	50°2 52°6 51°6 53°4 47°6 50°6	51.0 53.2 52.2 53.3 47.6 51.6	51.5 53.5 52.4 53.8 48.1 52.0	51.9 54.2 53.0 53.2 48.4 52.0	52.0 54.4 53.1 53.0 49.0 52.6	52.4 54.4 53.1 52.6 49.0 52.8	53.0 54.5 53.6 52.4 49.5 53.4	53°2 54°5 53°5 52°3 50°0 53°8	53.6 54.3 53.2 52.2 50.2 54.2
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^a Twenty-five minutes late.

	One Scale 1	Division =	'000066 pai	ts of the V.		RTICAL Fo		orresponding	g to 1° decre	ase of Tem	perature, 1°6	54.
12h.	13 ^h •	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div-	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 188 1	Sc. Div. 188 1	Sc. Div. 189.6	Sc. Div. 184'4	Sc. Div. 186*83
190°3 214°3	188°3 224°4	$189.1 \\ 202.5$	188'9 184'7	190°0 187°9	180'4 190'0	178°3 184°4	176.8	176.8	194.7	192.6	192.4	194.26
191.7	192.2	192.5	193.7	194.0	193.4	195.8	196.1	196.4	196.6	198.1	$\frac{-}{198\cdot 1}$	194.87
187.2	188.1	188.6	188.7	189.1	189.1	190.1	191.1	191.1	190.4	187.8	1	
187.2	189.2	188.2	188'4	187.8	185.6	183.9	186.9	186.5	186.3	182.4	182.8	188.58
190.2	190.5	197.2	156.0	171.6	164.7	126.9	165.6	156.8 177.1	163.9 181.5	179 · 6 185 · 9	175.6 185.6	179°38 179°49
190 · 5	190°2 188°9	189°3	184.8 197.0	$180.2 \\ 190.3$	181.0	172 · 9	166°1 168°4	159.2	164.0	169.4	169.9	182:38
95.0	194.1	188.3	187.8	190.3	190.4	—					193.9	190.26
						199.5	201.2	191.0	176.6	172.3	193.9	
191.4	191.1	191.1	189.8	191.1	191'1	190°2 196°2	189.0 192.6	191°3 195°4	191.7 195.4	$188.5 \\ 197.5$	190'4 196'6	191°59 195°46
198.6	201°1 198°7	201.4 195.9	195 . 8	198 . 8	198 ° 0 196 ° 7	196.5	192 6	198.4	199.2	198.3	197.5	197.20
195.1	199.5	199.5	198.8	189.1	193.5	196.7	195.7	198'4	196.3	194.0	195.0	196.41
195.1	194.9	191.4	192.1	193.8	193.8	193.7	192.9	196.0	197.5	196.9	196.2	196.23
97.8	196.2	198.9	201.5	204.0	203.7	209.8	209.5	209.3	211.2	207.6	$\left[\begin{array}{c} -1 \\ 209 \\ 5 \end{array}\right]$	202.80
225.2	236.5	216.6	215.0	197.8	204.7	205.6	209 5	206.1	$\frac{211}{200.7}$	200.6	205.8	208.75
204.0	204.3	204.8	204.8	204.9	204.9	204.9	204.9	204.9	206.3	205.3	205.5	204.13
206.3	204.4	204.2	203.9	204.3	205 1	201.4	204.8	203.6	203.4	186.7	193.0	203.29
811.8	210.7	210.7	207.4	206.8	210.1	210.0	208.0	207:3	203.2	204·7 208·7	208.5 208.8	206 · 43 209 · 58
08.7 03.1	207:3 206:1	208·1 205·6	208.1	208.4 204.9	204.3	205.3	205.2	207.1	200 0	203 7	i ii	
		200 0				207.4	207.2	206.9	206.9	206.9	209.0}	205.40
201.2	200.5	198.9	199.5	199.5	198.9	198.6	199.6	198.9	198.1	196.3	196.2	202.10
98.2	198.2	195.4	199.2	198.9	198.2	191.9	195.0	197.6	199.0	199 . 2	201.8	$\frac{197.70}{202.12}$
201.8	202.6	204.2	203.2	$202.3 \\ 202.5$	202°2 195°2	204.1	202.1	202.1	200.3	204.5	202.9	202 12
206.9	201.6 206.9	202.5 208.5	210.2	202.5	208.7	205.5	200.1	201.5	206.2	206.2	207.0	205.18
510.9	209.3	210.2	210.3	210.3	210.4						206.6}	208.79
						208.8	208.4	208.0	207.0	205.7		
199.68	200.62	198.91	196.56	196.45	195.57	194.01	194.84	194.84	195*46	195.03	196.54	197.14
0 1					RATURE OF	0	i c			0	0 1	0
62.4	62.1	6j.8	61.2	6j.1	60.6	60.4	60.2	60°0	59.7	59.2	59.0	6Ĭ · 97 59 · 00
59.8	60.0 59.8	59°8 59°5	60°3 59°5	60.0	59°2 59°4	58.8	58.6	58.4	28.0	57·7 —	57.0	
- 09 6	99 8	59 5 			J9 4	56.7	57.0	57.2	57.2	57.0	56.8	58.17
62.6	62.6	62.4	61.8	61.4	61.4	61.0	60.7	60.4	60.0	59.7	59.2	60.22
63.2	63.0	62.8	62.7	62.7	62.7	62.5	62.0	61.8	61.7	61.2	61.0	61.71
66.5	66:5	66.3	66.8	67°0 64°9	66.6 64.7	66.6 64.6	66.4 64.6	66.5 64.5	66.4 64.2	$66\cdot2$ $64\cdot5$	64.6	$65.18 \\ 65.42$
63.8	$\begin{array}{c} 65.5 \\ 63.5 \end{array}$	65°1	63.0 63.0	63.1	62.6	62.1	61.9	61.7	61.4	60.8	60.0	63.69
59.8	90.0	60.0	59.7	59.0	58.9	_	_			_	56.7}	58.84
- 1			_			57.2	57.2	57.2	57.2	57.3		
61.8 58.5	62.0	62.0	61.9	61.7 57.3	61.5 57.2	$\begin{array}{c} 61.5 \\ 57.2 \end{array}$	61.5 57.1	61.5 56.9	61.2 56.9	$\frac{61\cdot0}{56\cdot7}$	61.0 56.0	60°94 58°63
58.3	58°0 58°2	57.8 58.1	57.4 58.0	57°6	57.4	57·1	57 1 57 4	57.3	57.3	57 · 5	57.4	57.61
59.0	58.3	58.0	57.8	57.8	57.5	57.2	56.9	57.0	57.0	57.0	56.8	57.79
59.2	59.2	59.5	59.8	60.0	59.8	59.7	59.5	59.0	58.2	$58^{\circ}2$	57.3	58.30
54.8	54.7	54.2	54.2	53.8	53.2	49.2	49.0	49.0	49.2	49.0	$\frac{-}{48.7}$	53.57
53.4	53.4	53.2	53.2	53.0	53.0	53.0	53.0	52.7	52.7	$\frac{13}{52} \cdot 7$	53.1	52.30
54.2	54.0	53.6	53.1	53.0	52.7	52.4	52.7	52.5	52.2	$52\cdot 2$	51.8	53.28
54.2	54.4	54.4	55.2	$55^{\circ}2$	55.0	54.5	54.2	54.6	54.4	54.6	54.7	53.60
51.7 50.2	51.4	51.5	51.0	50.8	50.3	50°5	49.5 50.6	49°2 50°3	49°2 50°2	$\frac{49\cdot2}{50\cdot2}$	48°4 50°0	51.76 49.57
54.0	50.6 53.8	50°8	51.0 53.2	53.2	50.2 53.0			_			50.0}	51.85
54.5						50.2	50.0	50.0	50.0	49.9	56.8 56.8	53.79
56.7	54.6 56.9	$\begin{array}{c} 55.2 \\ 56.3 \end{array}$	55°3 56°7	55°3	55°4 56°1	55°5 55°7	55°8 55°4	56°2 55°2	56°3 55°0	56.6 54.5	54.2	56°40
54.0	53.8	53.6	53.0	53.0	52.9	52.4	52.4	52.2	52.0	52.0	52.2	53.05
53.8	53.8	53.9	53.4	53.0	52.8	52.8	52.8	52.2	51.9	51.7	51.3	52.82
51.4 48.4	51.2	51.2	51.0	50.6	50.3	50.5	49.8	49.7	49.5	49.4	49.2	50.75
1	48'4	48.4	48.2	48.2	48.0	50.0	50.5	50.4	51.0	51.3	51.6}	49.07
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C 2 3 4 5 6 6 7 8 9 100 111 122 133 134 155 166 177 188 199 200 21 222 233 244 255 266 27 288 299 300 ourly Mea	196.7 194.8 197.7 203.6 203.3	Sc. Div. 206 2 196 4 195 6 201 5 203 6 201 1 196 9 189 0 189 3 192 7 191 5 195 1 196 3 195 1 193 6 204 1 202 4 211 2 204 6 207 2 219 2 220 1 202 4 212 5	sc. Div. 202 '7 195 '6 193 '9 202 '9 203 '6 202 '8 195 '0 189 '4 189 '3 194 '5 196 '0 196 '1 193 '3 195 '9 195 '2 204 '1 203 '9 209 '3 204 '7 212 '3 215 '5 219 '2 200 '5	sc. Div. 200'3 194'4 193'7 200'7 203'2 202'1 — 196'4 190'2 194'6 194'1 196'1 — 195'0 193'3 194'9 194'7 205'8 203'9 — 209'1 202'9 213'7 218'8 217'8	sc. Div. 200 '5 195 '7 193 '9 199 '3 200 '0 200 '8	sc. Div. 199'9 194'4 193'9 197'0 198'6 198'8 — 190'6 185'5 189'3 192'9 194'8 195'6 — 192'4 189'6 192'1 195'6 204'2 203'2 — 209'2 200'0 216'7	sc. Div. 201'5 194'7 194'4 196'8 197'9 199'5 191'2 185'5 188'7 191'8 195'0 195'9 192'9 189'6 190'2 197'1 204'0 203'2 209'2 201'4 218'3	sc. Div. 200 '5 194 '7 194 '9 195 '4 199 '0 199 '5 192 '1 184 '4 188 '6 192 '9 195 '0 195 '6 194 '6 196 '7 190 '6 198 '0 204 '0 202 '9 210 '9 203 '0	sc. Div. 202 *8 194 *7 194 *9 195 *0 199 *8 201 *3 192 *2 185 *3 192 *0 193 *7 194 *6 195 *9 194 *5 206 *4 190 *7 198 *6 202 *8 202 *7 210 *6	sc. Div. 204 1 194 9 193 7 194 6 198 8 203 9 — 192 4 185 3 191 1 198 7 194 6 195 8 — 194 5 201 5 190 5 198 1 202 7 202 7	Sc. Div. 206 '8 194 '9 193 '7 194 '0 198 '8 206 '1 191 '3 185 '3 191 '6 192 '7 193 '1 195 '8 194 '5 192 '7 191 '9 197 '1 201 '1 201 '5	Sc. Div 203 '9 193 '1 193 '7 194 '0 195 '9 205 '2
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 ourly Mea	206·5 196·7 194·8 197·7 203·6 203·3	206 2 196 4 195 6 201 5 203 6 201 1 — 196 9 189 0 189 3 192 7 191 5 195 1 — 196 3 195 3 196 1 193 6 204 1 202 4 — 211 2 2 204 6 207 2 219 2 220 1 202 4 —	202'7 195'6 193'9 202'9 203'6 202'8 — 195'0 189'4 189'3 194'3 194'5 196'1 193'3 195'9 195'2 204'1 203'9 — 209'3 204'7 212'3 215'5 219'2	200'3 194'4 193'7 200'7 203'2 202'1 — 196'4 190'4 190'2 194'6 194'1 196'1 — 195'0 193'3 194'9 194'7 205'8 203'9 — 209'1 202'9 213'7 218'8 217'8	200°5 195°7 193°9 199°3 200°0 200°8 — 193°9 189°0 190°9 194°9 195°0 196°3 — 193°7 190°7 195°4 202°7 202°8 — 209°2 203°8 213°4	199'9 194'4 193'9 197'0 198'6 198'8 — 190'6 185'5 189'3 192'9 194'8 195'6 — 192'4 189'6 192'1 195'6 204'2 203'2 — 209'2 200'0	201'5 194'7 194'4 196'8 197'9 199'5 191'2 185'5 188'7 191'8 195'0 195'9 192'9 189'6 190'2 197'1 204'0 203'2 209'2 201'4	200°5 194°7 194°9 195°4 199°0 199°5 — 192°1 184°4 188°6 192°9 195°0 — 194°6 196°7 190°6 198°0 204°0 202°9 — 210°9 203°0	202'8 194'7 194'9 195'0 199'8 201'3 — 192'2 185'3 192'0 193'7 194'6 195'9 — 194'5 206'4 190'7 198'6 202'8 202'7	204·1 194·9 193·7 194·6 198·8 203·9 — 192·4 185·3 191·1 198·7 194·6 195·8 — 194·5 201·5 190·5 190·5 190·7 202·7 202·7	206 · 8 194 · 9 193 · 7 194 · 0 198 · 8 206 · 1 — 191 · 3 185 · 3 191 · 6 192 · 7 193 · 1 195 · 8 — 194 · 5 192 · 7 191 · 9 197 · 1 201 · 1	203 · 9 193 · 1 193 · 7 194 · 0 195 · 9 205 · 2
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 ourly Mea	196.7 194.8 197.7 203.6 203.3	196 '4 195 '6 201 '5 203 '6 201 '1 196 '9 189 '0 189 '3 192 '7 191 '5 195 '1 196 '3 195 '3 196 '1 193 '6 204 '1 202 '4 211 '2 204 '6 207 '2 219 '2 220 '1 202 '4	195 ° 6 193 ° 9 202 ° 9 203 ° 6 202 ° 8 — 195 ° 0 189 ° 4 189 ° 3 194 ° 3 194 ° 5 196 ° 0 — 196 ° 1 193 ° 3 195 ° 9 195 ° 2 204 ° 1 203 ° 9 — 209 ° 3 204 ° 7 212 ° 3 215 ° 5 219 ° 2	194'4 193'7 200'7 203'2 202'1 — 196'4 190'4 190'2 194'6 194'1 196'1 — 195'0 193'3 194'9 194'7 205'8 203'9 209'1 202'9 213'7 218'8 217'8	195'7 193'9 199'3 200'0 200'8 — 193'9 189'0 190'9 194'9 195'0 196'3 — 193'7 190'7 193'7 195'4 202'7 202'8 — 209'2 203'8 213'4	194'4 193'9 197'0 198'6 198'8 — 190'6 185'5 189'3 192'9 194'8 195'6 — 192'4 189'6 192'1 195'6 204'2 203'2 — 209'2 200'0	194'7 194'4 196'8 197'9 199'5 191'2 185'5 188'7 191'8 195'0 195'9 192'9 189'6 190'2 197'1 204'0 203'2 209'2 201'4	194'7 194'9 195'4 199'0 199'5 — 192'1 184'4 188'6 192'9 195'0 195'6 — 194'6 196'7 190'6 198'0 204'0 202'9 — 210'9 203'0	194'7 194'9 195'0 199'8 201'3 — 192'2 185'3 192'0 193'7 194'6 195'9 — 194'5 206'4 190'7 198'6 202'8 202'7	194'9 193'7 194'6 198'8 203'9 — 192'4 185'3 191'1 198'7 194'6 195'8 — 194'5 201'5 190'5 198'1 202'7 202'7	194'9 193'7 194'0 198'8 206'1 — 191'3 185'3 191'6 192'7 193'1 195'8 — 194'5 192'7 191'9 197'1 201'1	193°1 193°7 194°0 195°9 205°2 ————————————————————————————————————
4 5 6 7 8 9 10 111 121 13 144 155 166 177 18 19 20 21 22 23 244 25 26 27 28 29 30 ourly Mea	194'8 197'7 203'6 203'3	195.6 201.5 203.6 201.1 196.9 189.0 189.3 192.7 191.5 195.1 196.3 195.3 196.1 193.6 204.1 202.4 211.2 204.6 207.2 219.2 220.1 202.4	193 '9 202 '9 203 '6 202 '8	193'7 200'7 203'2 202'1 ————————————————————————————————————	193'9 199'3 200'0 200'8 — 193'9 189'0 190'9 194'9 195'0 196'3 — 193'7 190'7 193'7 195'4 202'7 202'8 — 209'2 203'8 213'4	193'9 197'0 198'6 198'8 — 190'6 185'5 189'3 192'9 194'8 195'6 — 192'4 189'6 192'1 195'6 204'2 203'2 — 209'2 200'0	194'4 196'8 197'9 199'5 — 191'2 185'5 188'7 191'8 195'0 195'9 — 192'9 189'6 190'2 197'1 204'0 203'2 — 209'2 201'4	194'9 195'4 199'0 199'5 192'1 184'4 188'6 192'9 195'0 195'6 194'6 196'7 190'6 198'0 204'0 202'9 210'9 203'0	194'9 195'0 199'8 201'3 — 192'2 185'3 192'0 193'7 194'6 195'9 — 194'5 206'4 190'7 198'6 202'8 202'7	193.7 194.6 198.8 203.9 ————————————————————————————————————	193.7 194.0 198.8 206.1 ————————————————————————————————————	193.7 194.0 195.9 205.2 ————————————————————————————————————
5 6 7 8 9 100 111 122 13 144 155 166 177 18 20 21 222 234 255 27 28 29 30 ourly Mea	197'7 203'6 203'3	201 · 5 203 · 6 201 · 1 — 196 · 9 189 · 0 189 · 3 192 · 7 191 · 5 195 · 1 — 196 · 3 195 · 3 196 · 1 193 · 6 204 · 1 202 · 4 — 211 · 2 204 · 6 207 · 2 219 · 2 220 · 4 —	202'9 203'6 202'8 — 195'0 189'4 189'3 194'3 194'5 196'0 — 196'1 193'3 195'9 195'2 204'1 203'9 — 209'3 204'7 212'3 215'5 219'2	200 '7 203 '2 202 '1 — 196 '4 190 '4 190 '2 194 '6 194 '1 195 '0 193 '3 194 '9 194 '7 205 '8 203 '9 — 209 '1 202 '9 213 '7 218 '8 217 '8	199'3 200'0 200'8	198'6 198'8	197'9 199'5 191'2 185'5 188'7 191'8 195'0 195'9 192'9 189'6 190'2 197'1 204'0 203'2 209'2 201'4	199'0 199'5 ———————————————————————————————————	199'8 201'3	198'8 203'9 — 192'4 185'3 191'1 198'7 194'6 195'8 — 194'5 201'5 190'5 198'1 202'7 202'7	198 '8 206 '1 191 '3 185 '3 191 '6 192 '7 193 '1 195 '8 194 '5 192 '7 191 '9 197 '1 201 '1	195.9 205.2
6 7 8 9 10 11 12 13 144 155 66 7 8 9 10	203'3	201'1	202.8	202'1	200'8	198'8	199.5	199.5	201'3	203'9	206·1	205.2 189.7 186.7 190.5 192.9 193.1 196.8 195.0 194.8 199.8 205.6
NOVEMBER. 8 9 10 11 12 13 144 155 66 78 89 90 90 90 90 90 90 90 90 90 90 90 90 90	198'0 188'4 189'3 192'7 191'8 193'7	196'9 189'0 189'3 192'7 191'5 195'1	195 ° 0 189 ° 4 189 ° 3 194 ° 3 194 ° 5 196 ° 0 — 196 ° 1 193 ° 3 195 ° 9 195 ° 2 204 ° 1 209 ° 3 204 ° 7 212 ° 3 215 ° 5 219 ° 2	196'4 190'4 190'2 194'6 194'1 196'1 — 195'0 193'3 194'9 194'7 205'8 203'9 — 209'1 202'9 213'7 218'8 217'8	193'9 189'0 190'9 194'9 195'0 196'3 — 193'7 190'7 193'7 195'4 202'7 202'8 — 209'2 203'8 213'4	190 ° 6 185 ° 5 189 ° 3 192 ° 9 194 ° 8 195 ° 6 ———————————————————————————————————	191 2 185 5 188 7 191 8 195 0 195 9 192 9 189 6 190 2 197 1 204 0 203 2 209 2 201 4	192 1 184 4 188 6 192 9 195 0 195 6 — 194 6 196 7 190 6 198 0 204 0 202 9 — 210 9 203 0	192 · 2 185 · 3 192 · 0 193 · 7 194 · 6 195 · 9 — 194 · 5 206 · 4 190 · 7 198 · 6 202 · 8 202 · 7 —	192'4 185'3 191'1 198'7 194'6 195'8 194'5 201'5 190'5 198'1 202'7 202'7	191'3 185'3 191'6 192'7 193'1 195'8	189.7 186.7 190.5 192.9 193.1 196.8
9 10 11 12 13 14 15 16 177 188 19 20 21 22 23 24 25 26 27 28 29 30 ourly Mea	188'4 189'3 192'7 191'8 193'7 196'6 195'3 191'6 193'5 201'7 202'0 211'0 204'9 207'2 219'6 220'0 201'0	189.0 189.3 192.7 191.5 195.1	189'4 189'3 194'3 194'5 196'0 — 196'1 193'3 195'9 195'2 204'1 209'3 204'7 212'3 215'5 219'2	190'4 190'2 194'6 194'1 196'1 — 195'0 193'3 194'9 194'7 205'8 203'9 — 209'1 202'9 213'7 218'8 217'8	189'0 190'9 194'9 195'0 196'3 — 193'7 190'7 193'7 195'4 202'7 202'8 — 209'2 203'8 213'4	185.5 189.3 192.9 194.8 195.6 — 192.4 189.6 192.1 195.6 204.2 203.2 — 209.2 200.0	185.5 188.7 191.8 195.0 195.9 — 192.9 189.6 190.2 197.1 204.0 203.2 — 209.2 201.4	184'4 188'6 192'9 195'0 195'6 — 194'6 196'7 190'6 198'0 204'0 202'9 — 210'9 203'0	185'3 192'0 193'7 194'6 195'9 — 194'5 206'4 190'7 198'6 202'8 202'7	185'3 191'1 198'7 194'6 195'8 — 194'5 201'5 190'5 198'1 202'7 202'7	185'3 191'6 192'7 193'1 195'8	186.7 190.5 192.5 193.1 196.8 195.6 194.8 190.5 199.5
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 ourly Mea	189'3 192'7 191'8 193'7	189°3 192°7 191°5 195°1 196°3 195°3 196°1 193°6 204°1 202°4 211°2 204°6 207°2 219°2 220°1 202°4	189'3 194'3 194'5 196'0 —— 196'1 193'3 195'9 195'2 204'1 203'9 —— 209'3 204'7 212'3 215'5 219'2	190°2 194°6 194°1 196°1 — 195°0 193°3 194°9 194°7 205°8 209°1 202°9 213°7 218°8 217°8	190'9 194'9 195'0 196'3 — 193'7 190'7 193'7 195'4 202'7 202'8 — 209'2 203'8 213'4	189'3 192'9 194'8 195'6 — 192'4 189'6 192'1 195'6 204'2 203'2 — 209'2 200'0	188'7 191'8 195'0 195'9 — 192'9 189'6 190'2 197'1 204'0 203'2 — 209'2 201'4	188.6 192.9 195.0 195.6 ————————————————————————————————————	192.0 193.7 194.6 195.9 — 194.5 206.4 190.7 198.6 202.8 202.7	191°1 198°7 194°6 195°8 — 194°5 201°5 190°5 198°1 202°7 202°7	191 '6 192 '7 193 '1 195 '8 ————————————————————————————————————	190 · 5 192 · 9 193 · 1 196 · 8 195 · 6 194 · 8 199 · 5 205 · 6
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 ourly Mea	192.7 191.8 193.7 	192.7 191.5 195.1 ————————————————————————————————————	194'3 194'5 196'0 — 196'1 193'3 195'9 195'2 204'1 203'9 — 209'3 204'7 212'3 215'5 219'2	194.6 194.1 196.1 — 195.0 193.3 194.9 194.7 205.8 203.9 — 209.1 202.9 213.7 218.8 217.8	194'9 195'0 196'3 — 193'7 190'7 193'7 195'4 202'7 202'8 — 209'2 203'8 213'4	192'9 194'8 195'6 — 192'4 189'6 192'1 195'6 204'2 203'2 — 209'2 200'0	191'8 195'0 195'9 — 192'9 189'6 190'2 197'1 204'0 203'2 — 209'2 201'4	192'9 195'0 195'6 ————————————————————————————————————	193.7 194.6 195.9 ———————————————————————————————————	198.7 194.6 195.8 ————————————————————————————————————	192.7 193.1 195.8 ————————————————————————————————————	192.9 193.1 196.8 195.0 194.8 190.8 199.8
. WOVEMBER. 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 ourly Mea	191'8 193'7 	191.5 195.1 ————————————————————————————————————	194.5 196.0 ————————————————————————————————————	194'1 196'1 — 195'0 193'3 194'9 194'7 205'8 203'9 — 209'1 202'9 213'7 218'8 217'8	195°0 196°3 — 193°7 190°7 193°7 195°4 202°7 202°8 — 209°2 203°8 213°4	194'8 195'6 —— 192'4 189'6 192'1 195'6 204'2 203'2 —— 209'2 200'0	195'0 195'9 ———————————————————————————————————	195.0 195.6 ————————————————————————————————————	194.6 195.9 ———————————————————————————————————	194'6 195'8 — 194'5 201'5 190'5 198'1 202'7 202'7	193 · 1 195 · 8 — 194 · 5 192 · 7 191 · 9 197 · 1 201 · 1	193 1 196 8 195 0 194 8 190 8 199 8 205 0
HEAD AON 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 ourly Mea	193.7 196.6 195.3 191.6 193.5 201.7 202.0 	195°1	196.0 — 196.1 193.3 195.9 195.2 204.1 203.9 — 209.3 204.7 212.3 215.5 219.2	196'1 	196'3 193'7 190'7 193'7 195'4 202'7 202'8 209'2 203'8 213'4	195'6	195'9 192'9 189'6 190'2 197'1 204'0 203'2 209'2 201'4	195'6	195'9 194'5 206'4 190'7 198'6 202'8 202'7	195.8 	195.8 194.5 192.7 191.9 197.1 201.1	196.8 195.0 194.8 199.8 205.0
20 21 22 23 24 25 26 27 28 29 30 ourly Mea	196.6 195.3 191.6 193.5 201.7 202.0 211.0 204.9 207.2 219.6 220.0 201.0	195°3 196°1 193°6 204°1 202°4 — 211°2 204°6 207°2 219°2 220°1 202°4 —	193°3 195°9 195°2 204°1 203°9 — 209°3 204°7 212°3 215°5 219°2	193°3 194°9 194°7 205°8 203°9 — 209°1 202°9 213°7 218°8 217°8	190.7 193.7 195.4 202.7 202.8 ————————————————————————————————————	189.6 192.1 195.6 204.2 203.2 ————————————————————————————————————	189.6 190.2 197.1 204.0 203.2 ————————————————————————————————————	196.7 190.6 198.0 204.0 202.9 — 210.9 203.0	206'4 190'7 198'6 202'8 202'7	201.5 190.5 198.1 202.7 202.7	192.7 191.9 197.1 201.1	194.8 190.8 199.8 205.6
20 21 22 23 24 25 26 27 28 29 30 ourly Mea	195°3 191°6 193°5 201°7 202°0 211°0 204°9 207°2 219°6 220°0 201°0	195°3 196°1 193°6 204°1 202°4 — 211°2 204°6 207°2 219°2 220°1 202°4 —	193°3 195°9 195°2 204°1 203°9 — 209°3 204°7 212°3 215°5 219°2	194'9 194'7 205'8 203'9 ————————————————————————————————————	193.7 195.4 202.7 202.8 ————————————————————————————————————	192°1 195°6 204°2 203°2 ————————————————————————————————————	190°2 197°1 204°0 203°2 ————————————————————————————————————	190.6 198.0 204.0 202.9 ————————————————————————————————————	190.7 198.6 202.8 202.7	190°5 198°1 202°7 202°7	191.9 197.1 201.1	190°5 199°5 205°6
20 21 22 23 24 25 26 27 28 29 30 ourly Mea	193.5 201.7 202.0 211.0 204.9 207.2 219.6 220.0 201.0	193.6 204.1 202.4 — 211.2 204.6 207.2 219.2 220.1 202.4 —	195°2 204°1 203°9 ————————————————————————————————————	194.7 205.8 203.9 ————————————————————————————————————	195 · 4 202 · 7 202 · 8 209 · 2 203 · 8 213 · 4	195.6 204.2 203.2 209.2 200.0	197 · 1 204 · 0 203 · 2 	198.0 204.0 202.9 — 210.9 203.0	198.6 202.8 202.7	198°1 202°7 202°7 —	197°1 201°1	199°5 205°6
20 21 22 23 24 25 26 27 28 29 30 ourly Mea	201.7 202.0 211.0 204.9 207.2 219.6 220.0 3 201.0	204 1 202 4 — 211 2 204 6 207 2 219 2 220 1 202 4	204 · 1 203 · 9 ———————————————————————————————————	205.8 203.9 	202.7 202.8 	204.2 203.2 209.2 200.0	204.0 203.2 	204.0 202.9 210.9 203.0	202.8 202.7	202.7 202.7 —	201.1	205.6
21 22 23 24 25 26 27 28 29 30 ourly Mea	202'0 	202'4 	203 · 9 209 · 3 204 · 7 212 · 3 215 · 5 219 · 2	203.9 	202.8 209.2 203.8 213.4	200.0 200.2 203.5	203°2 209°2 201°4	202.9 210.9 203.0	202.7	202.7		
23 24 25 26 27 28 29 30 ourly Mea	211.0 204.9 207.2 219.6 220.0 201.0	204.6 207.2 219.2 220.1 202.4	204.7 212.3 215.5 219.2	202.9 213.7 218.8 217.8	203°8 213°4	200.0	201.4	203.0	210.6			20612
24 25 26 27 28 29 30 ourly Mea	204.9 207.2 219.6 220.0 201.0	204.6 207.2 219.2 220.1 202.4	204.7 212.3 215.5 219.2	202.9 213.7 218.8 217.8	203°8 213°4	200.0	201.4	203.0		209.0	207.7	207:9
25 26 27 28 29 30 ourly Mea	207 · 2 219 · 6 220 · 0 201 · 0	207°2 219°2 220°1 202°4	212·3 215·5 219·2	213.7 218.8 217.8	213.4				204.7	204.7	204.7	204
26 27 28 29 30 ourly Mea	219.6 220.0 201.0	220°1 202°4	219.2	217.8	990.0		210 0	219.6	219.7	221.0	221.7	221
28 29 30 ourly Mee	201.0	202.4				219.7	221.2	221.2	225.7	226.7	230.8	234
29 30 ourly Mea)		200 3		218.7	218.7 202.8	220.4	220°4 205°5	220.5 204.1	221.4 203.7	221·1 203·8	218.0
22 34 45 66 77 88			-	200.0	 —	_	_					_
2 3 4 5 6 7 8	213 8	412 0	211.8	210.7	212.7	212.6	212.7	213.6	215.6	214.2	214.2	214.
34 45 66 77 88	ans 200.59	200.96	200.87	200.67	200.37	199.52	199.85	200.54	201.22	201.26	201.09	201.2
34 45 66 77 88			,	TEMPERAT	TURE OF TH	HE VERTICA	AL FORCE M	MAGNET.				
34 45 66 77 88	51.6	51.9	52.2	52.2	52.7	53.3	53.6	°	• 54°4	55 · 0	。 55 · 4	55.6
44 5 6 7 8 9		26.0	56.0	56.5	57.4	57.1	57.5	54°2 57°7	57.8	58°4	58.2	58.4
5 6 7 8 9	. 11	56.2	56.0	57.3	57.3	57.3	57.6	58.0	58.5	58.2	58.2	58.0
8 9	54.0	53.5	54.2	54.4	55.2	55.2	56.0	56.4	57.0	57.4	58.2	58
8		52.2	52.2	52.2	52.6	52.7	53.4	53.8	54.2	54.7	55.0	55 3
9		53.4	52.2	52.2	52.6	53.4	53.2	53.8	54°0 —	54.3	54.3	54
	55.8	56.5	56.3	56.4	56.9	57.7	58.1	58.1	58.2	5 8'6	59.0	59
10		59°4 59°2	59.0	59.2	59.4	60.0	60.2	60.2	60.5	60.6	60.6	60.0
11 12		57.6	59°1 57°3	59°1 57°2	59.2	59°3 56°6	59°3 56°7	59°3 57°0	59°3	59°5 57°2	59.6 57.3	59°6
. 119		57.0	56.6	56.2	56.2	56.2	56.2	56.2	56.6	56.9	57.0	57.0
富 14	4 56°0	56.2	56.0	55.4	55.2	55.6	55.6	56.0	55'6	56.0	55.9	56
H 15		54.7	54.7	54.2	54.6	55.3	55.5	55.5	55.7	56.5	56.1	56.0
17	7 55.3	55.2	55.3	55.8	56.3	56.3	56.3	56.7	56.9	57.3	57.2	57.0
0 18		57.2	56.8	56.6	57.2	58.0	58.4	59:2	59.3	59.4	59.1	59
Z 19		57.2	56.8	56.6 50.4	56.1	56°2 51°4	56.3 51.5	55.6 51.2	55°2 52°0	55°2 52°2	55°1 52°0	54° 53°
21	1 52.0	52.0	51.3	50.7	20.8	51.1	51.3	51.4	51.4	51.7	51.8	51.
22 23		46.3	47.4	46.6	46.7	47.2	47.4	47.5	48.6	48.6	48.2	48.8
24	4 49.6	49.8	49.3	49.0	49'4	50.0	50.3	50.4	50.4	50.4	50.4	50
25	5 47.6	47.4	45.2	45.3	44'0	42.8	43.2	41.5	41.1	40.8	40.5	40'0
26		39·5 39·7	40.4	39'4	39'4	39.8	40.0	40.0	40.0	39.9	39.8	39
27 28			40.4	40°0 50°5	40.0	40.4	40.5	41.4 49.4	41.4 50.0	41.2 50.6	42.0 51.2	43°
29 30	7 39.9 49.3	49.2		43.0	43.4	43.6	43.6	43.6	43.4	43.3	43.2	43.4

	One Scale	Division =	*000065 pa	rts of the V.	VEI	RTICAL F se, in Scale	ORCE. Divisions, c	orresponding	g to 1° decre	ease of Tem	perature, 1°	34.
12h.	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18 ^h .	19 ^h •	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
203.9	204.0	200.0	198.3	198.3	197.4	193.8	194.3	193.4	192.5	191.3	192.5	199.81
						192.2	192.2	192.8	193.0	195.4	195.4	193.97
193.1	192.8	191.7	191.8	192.1	192.4	196.7	194.6	190.3	193.2	198.0	197.7	194.56
193.2	193.4	195.2	193.6	195.8	196.1		193.0	193.0	198.0	197.9	201.1	197.03
195.7	196.3	197°1	195.6	198 '9	199.2	193.9			199.2	203.2	203.2	200.36
196.8	197.8	199.0	202.2	202.1	201.1	201.1	200.6	198.9	199 0	200 2		
204.4	204.4	200.6	200'1	199.3	199.3		10010	100:5	197.7	197.8	$\left \frac{-}{198 \cdot 2} \right\}$	200.95
	_					199.0	199.2	198.5			188.9	191.15
189.7	189.2	189.2	188.9	189.0	188.0	188.2	189.5	189.4	189.2	189.0		
186.6	186.4	187.8	187.3	189.2	188.9	190.2	188.8	188.6	189.6	188.2	189.1	187.70
190.0	190.6	190.0	189.6	190.6	190.6	189.5	190.5	190.5	191.8	191.8	192.7	190.37
191.7	193.0	191.3	193.0	193.0	194.3	194.3	194.3	193.9	193.6	192.3	192.4	193.41
193.1	197.2	197.8	197.2	198.2	197.3	196.3	195.6	195.0	193.4	193.3	193.1	194.79
196.6	196.2	196.5	195.2	195.4	195.4						\	196.51
190 0	130 0	150 2	130 0	130 1	150 1	196.7	197.8	197.6	197.6	197.4	$ \frac{-}{197 \cdot 7} \} $	
193.9	193.2	193.6	194.0	195.7	196.4	196.4	195.2	196.3	196.3	196.3	196.3	195.00
						169.5	168.8	168.8	194.7	189.3	173.2	190.26
195.7	195.7	195.7	195.7	195.6	184.4	193.8	194.8	194.0	194.0	194.0	193.6	193.06
192.3	193.0	193'9	193.8	193.8	193.8			202.7	202.6	202.2	203.1	199.23
199.5	199.5	202.0	201.9	202.9	202.8	202.8	202.8		202.8	202.8	202.6	203.63
208.5	207.8	205.6	202.8	203.5	203.4	203.2	199.5	201.2	202 0	404 0	- 1	
206.3	206.1	206'1	204'1	204.1	204.3			010:-	212.1	211.0	$\frac{1}{211\cdot 0}$	205.59
_						211.0	210.0	210.7				907:00
207.8	207.8	207.1	207.8	205.2	206.6	204.8	207.2	207.0	206'1	205.2	204.8	207.99
205.8	205.8	204.5	205'1	205.1	205.1	206.9	208.7	208.7	208.7	209.7	209.6	205.33
221.5	221.6	221.8	221.2	222.8	222.4	221.8	221.4	221.2	221'3	221.3	219.4	218.74
238.1	233.0	228.3	228.2	214.3	220.5	220.4	215.0	203.7	210'4	216.0	220.0	221.71
216.2	218.2	215.4	212.8	201.4	205.4	207.4	205.7	204.6	200.3	198.8	198.4	213.37
						201 4	200 1					205.42
205.3	205.6	205.5	200.6	202.4	202.4	014:5	214.2	214.1	210.0	210.0	212·5	205 42
214.4	214.3	214.9	219.3	219.2	217.9	214.5 216.8	211.3	210.3	214.1	216.6	216.6	214.39
201.60	201.74	201.51	200.82	200.33	200.55	200.07	199.39	198.62	200.11	200.36	200.12	200.56
				TEMPER	ATURE OF	THE VERT	ICAL FORC	E MAGNET.		·	<u> </u>	
0		0		o IEMPER	0	0		0	0	0	0	0
	0				l	t	57.0	57.0	56.8	56.6	56.4	54.99
55.8	55.8	56.2	56.3	56.2	56.7	56.8		28.0	57.8	57.4	57.2	57.83
29.0	59.0	59.2	59.2	59.0	58.6	58.4	58.2		$55^{\circ}2$	54.6	54.2	56.94
58.3	58.3	57.8	57.4	57.0	56.7	56.5	56.0	55.3	53.2	5 3.0	52.7	55.43
57.5	57.0	56.6	56.5	56.7	55.2	54.5	54'1	53.7		53.3	53.1	53.72
55'3	55.1	54.7	54.3	54.0	54.0	53.9	53.8	53.5	53.2			
54.4	54.6	54.6	55.2	55.2	55.1					~~	55.3}	54.15
-	_					53.8	54.2	55.0	55.2	55.3		50.67
59.5	59.6	59.6	59.7	59.8	60.2	60.1	60.0	59.8	59.8	59.8	59.8	58.67
60.2	60.7	60.0	59.8	59.8	59.8	59.6	59.6	59.4	59.2	59.2	59.1	59.84
59.2	59.4	59.4	59.3	59.2	59.1	58.7	58.6	58.6	58.4	58.2	58.2	59.10
57.3	57.2	57.2	56.9	56.7	56.6	56.7	57.3	57.2	57.4	57.6	57.4	57.15
57.0	56.8	56.9	57.2	57.1	57.0	57.0	56.8	56.8	56.8	56.9	56.6	56.81
56.3	56.3	56°4	56.2	56.3	56.3	J. U				_	— \	55.62
-	00 0	JU 4	90 9	ì	000	54.8	54.3	54.2	54.5	54.5	$\frac{-}{54.5}$	
56.4	F7.0	F=-^		FC:C	FG: A	56.5	56.1	56.0	55.7	55.5	55.5	55.77
	57:0	57:0	57.0	56.6	56.4			57.2	57.2	57.3	57.4	56.75
57.0	57.0	57.2	57.1	57.2	57.2	57.3	57.2		58.0	58.0	57.6	58.05
58.6	58.5	58.0	57.9	57.9	57.8	57.7	58.1	58.0	51.2	51.3	51.3	54.27
54.7	54.2	53.0	52.7	52.4	52.2	52.1	52.4	52.3		5 1.6	51.6	51.85
52.7	52.6	52.8	52.4	52.5	52.4	52.5	52.0	51.7	51.7			
51.6	51.7	51.6	51.4	51.4	51.5		_		40.0	16:6	$\frac{-}{46.0}$	50.27
-			_		-	47.2	47.0	46.8	46.6	46.6		48.20
48.7	49.0	49.2	49.0	48.8	48.7	48.8	48.7	48.5	49.0	49.3	49.7	
50.2	49.6	49.3	49.0	48.8	48.0	47.8	47.7	47.7	47.5	47.5	47.6	49.17
39.8	39.6	39.2	39.3	39.3	39.3	39.4	39.6	39.6	39.7	39.8	39.6	41.41
40.4	40.4	40.4	40.4	40.4	40.3	40.0	40.0	40.0	40.1	40.3	40.2	40.00
43.6			1			47.2	47.3	47.5	48.4	49.0	49.2	43.75
21.0	44.0	44.7	45.2	46.4	47.3	t					1	48.20
	50.6	50.4	50.3	50.3	50.5	40:0	42.0	41.8	42.2	42.4	$\frac{-}{43.0}$	40 20
43.3	42.5	42.1	41.4	41.0	40.9	42.2 41.5	41.4	41.4	41.4	41.4	41.3	42.48
	53.46	53.35	53.24	53.50	53.09	52.43	52.38	52.58	52.27	52.26	52.18	52.82

Vol. III.

Mean (gen T	1		vision = '00										
	Göttin-}	Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h •	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .	10h.	11h
	1	Sc. Div. 216.6	Sc. Div. 216.6	Sc. Div. 215°0	Sc. Div. 218.3	Sc. Div. 218 3	Sc. Div. 218 7	Sc. Div. 219.5	Sc. Div. 221 '0	Sc. Div.	Sc. Div. 217.6	Sc. Div. 217 6	Sc. Di 218
- 1	2	213.7	214.0	214.0	213.7	212.2	209.0	209.7	209.3	208.0	206.8	205.8	204
. [3	203 1	202.2	203.2	203.2	204.4	204.4	204.7	205.5	206.1	205.7	205.7	206
- 1	4	210.0	210.0	208.0	208.8	208.9	210.3	210.8	211.8	211.3	210.3	211.0	211
1	5	206.9	206.6	207.7	208.3	205.4	206.2	205.5	205.0	205.6	205.5	204.2	205
1	6 7	213.5	213.3	$\frac{-}{212.4}$	210.7	210.4	210.0	209.3	209.9	210.3	210.1	209.1	208
1	8	203.6	203.9	206.2	204.5	203.5	202.3	202.3	204.2	205.0	205.2	204.4	204
	9	206.0	205.4	207.3	207.0	205.9	205.7	205.7	205.4	206.7	207.0	209.0	210
	10	208.1	208.5	209.3	210.1	209.2	210.5	208.7	208.7	210.2	208.2	208.1	206'
- 1	11	207.7	208.7	209.6	208.9	205.2	205.2	207:3	210.3	211.5	211.2	211.5	211
	$\frac{12}{13}$	212'1	214.2	215.7	217.2	218.2	217.2	218.7	217.4	220.0	220.0	219.7	220
DECEMBER.	14	227.6	230.5	226.1	227.8	226.0	225.1	225.1	225.1	225.2	224.8	224.4	222
BI	15	227.0	227.9	222.3	222.3	224.8	224.8	222.9	222.9	222.9	221.2	221.4	220
₹(16	216.1	216.1	218.4	217.8	215.6	215.6	213.8	212.1	212.1	211.3	211.8	211
5	17	214.2	214.2	214.2	213.2	212.1	209.8	208.6	208.6	210.4	209.6	209.0	209
8	18	210.3	212.4	210.8	214.1	211.8	211.5	212.4	211.3	209.7	209.3	208.8	209
_	19 20	207.6	207.4	210.8	209.3	207.8	206.6	207.7	207.7	207.7	207.0	207.0	208
	21	216.0	216.1	214.1	213.9	213.7	213.7	213.7	213.0	212.6	210.6	210.9	210
ł	22	213.7	213.7	214.0	214.1	214.3	214.3	214.5	217.7	218.5	218.3	218.3	218
}	23	215.2	215.7	215.9	213.1	213.4	214.5	214.5	217.9	216.0	214.9	219'6	218
	24 25 a	208.3	208.3	207.5	208.5	209.6	209.5	208.6	207.8	206.6	206.3	206.2	208
	26 27	213.0	213.0	213.6	213.7	214.7	213.3	211.8	211.5	211.3	211.4	211.7	211
}	28	200.3	200.3	200.7	201.9	201.0	201.1	202.8	204.1	204.1	203.9	205.1	204
}	29	205.1	205.7	208.0	208.0	208.1	207.5	209.9	210.1	210.1	209.8	209.1	208
İ	30	205.7	205.7	205.1	203.6	201.7	201.7	201.5	201.5	200.4	200.4	200.0	200
	\31	198.4	198.9	198.6	200.7	200.7	200.0	200.0	199.1	199.1	197.9	196.2	198
ourly	y Means	210.76	211.13	211.11	211.26	210.65	210.32	210.38	210.72	210.84	210.18	210.55	210
		11 0					HE VERTIC						
((1	41.3	41.2	40°9	40.4	40.0	40.2	40°2	40°2	40°4	40°9	4 i · 2	4i°
	2	43.4	43.5	43.5	43.6	44.1	45.4	45.5	46.0	46.4	47.4	47.6	48
ĺ	3 4	50°6 44°4	50°1 44°4	49°3 44°7	48°4 44°4	48.4	47.6 45.0	48.4	48'4	48'2	48.0	47.9	47
	5	47.3	47.2	46.9	46.6	46.8	47.5	45°2 47°5	45°0 47°9	45.2 48.0	45.6	46.2	46° 48°
ŀ	6							_		40 0	48.4	48.4	40
1	7	43.0	43.5	43.2	43.2	43.4	43.8	44.4	44.2	44.7	45.2	45.5	45
	8	48.7	48.8	48.4	48.2	48.2	49.1	48.7	48.6	48.4	48.6	48.6	48.
		47.2	47.2	46.8	46.4	46.0	46.1	46.4	47.1	47.3	47.4	47.4	47
	9					14							
	9 10	45.6	45.6	45.1	44.5	44.5	45.2	45.8	46.0	46.5	47.3	47.8	
	9					44.5 46.2 40.5	45°2 46°6	45.8 46.0	45.6	45.2	45.2	45.4	45
В.	9 10 11 12 13	45.6 45.8 43.0	45.6 45.4 42.6	45°1 45°2 41°8	44.5 45.4 41.2	46.2 40.5	45°2 46°6 40°5	45.8 46.0 40.4 —	45.6 40.4 —	45°2 40°0 —	45°2 40°0	45°4 40°0 —	45°
3ER.	9 10 11 12 13 14	45.6 45.8 43.0 — 32.0	45.6 45.4 42.6 — 32.3	45.1 45.2 41.8 — 32.6	44.5 45.4 41.2 — 33.1	46.2 40.5 — 33.2	45.2 46.6 40.5 — 33.4	45.8 46.0 40.4 — 33.8	45.6 40.4 — 34.1	45°2 40°0 — 34°8	45°2 40°0 — 35°2	45.4 40.0 — 35.9	45° 40° 36°
MBER.	9 10 11 12 13 14 15	45.6 45.8 43.0 32.0 34.6	45.6 45.4 42.6 — 32.3 34.2	45.1 45.2 41.8 — 32.6 33.9	44.5 45.4 41.2 — 33.1 34.4	46.2 40.5 - 33.2 34.9	45.2 46.6 40.5 — 33.4 36.0	45.8 46.0 40.4 — 33.8 36.4	45.6 40.4 — 34.1 36.9	45.2 40.0 — 34.8 37.4	45°2 40°0 — 35°2 38°4	45.4 40.0 — 35.9 39.0	45° 40° 36° 39°
CEMBER.	9 10 11 12 13 14 15 16	45.6 45.8 43.0 	45.6 45.4 42.6 — 32.3 34.2 38.0	45·1 45·2 41·8 ————————————————————————————————————	44.5 45.4 41.2 — 33.1 34.4 37.4	46.2 40.5 33.2 34.9 38.0	45.2 46.6 40.5 — 33.4 36.0 38.7	45.8 46.0 40.4 — 33.8 36.4 39.1	45.6 40.4 — 34.1 36.9 39.7	45.2 40.0 — 34.8 37.4 39.9	45 · 2 40 · 0 35 · 2 38 · 4 40 · 2	45.4 40.0 — 35.9 39.0 40.4	45° 40° 36° 39° 40°
ECEMBER.	9 10 11 12 13 14 15 16 17 18	45.6 45.8 43.0 32.0 34.6	45.6 45.4 42.6 ————————————————————————————————————	45.1 45.2 41.8 — 32.6 33.9	44.5 45.4 41.2 — 33.1 34.4	46.2 40.5 - 33.2 34.9	45.2 46.6 40.5 — 33.4 36.0	45.8 46.0 40.4 — 33.8 36.4	45.6 40.4 	45.2 40.0 — 34.8 37.4	45.2 40.0 35.2 38.4 40.2 41.8	45.4 40.0 35.9 39.0 40.4 41.8	45° 40° 36° 39° 40° 41°
DECEMBER.	9 10 11 12 13 14 15 16 17 18 19	45.6 45.8 43.0 ————————————————————————————————————	45.6 45.4 42.6 ————————————————————————————————————	45°1 45°2 41°8 ————————————————————————————————————	44.5 45.4 41.2 — 33.1 34.4 37.4 39.7 38.4 41.5	46·2 40·5 	45.2 46.6 40.5 — 33.4 36.0 38.7 40.8	45.8 46.0 40.4 — 33.8 36.4 39.1 41.5	45.6 40.4 — 34.1 36.9 39.7	45.2 40.0 	45 · 2 40 · 0 35 · 2 38 · 4 40 · 2	45.4 40.0 35.9 39.0 40.4 41.8 41.2 42.4	45° 40° 36° 39° 40° 41° 41° 42°
DECEMBER.	9 10 11 12 13 14 15 16 17 18 19 20 21	45.6 45.8 43.0 ————————————————————————————————————	45.6 45.4 42.6 ————————————————————————————————————	45.1 45.2 41.8 — 32.6 33.9 37.4 39.6 39.1 41.5	44.5 45.4 41.2 — 33.1 34.4 37.4 39.7 38.4 41.5	46.2 40.5 — 33.2 34.9 38.0 40.8 38.1 42.2	45.2 46.6 40.5 — 33.4 36.0 38.7 40.8 39.0 42.5	45.8 46.0 40.4 — 33.8 36.4 39.1 41.5 39.4 42.5	45.6 40.4 — 34.1 36.9 39.7 41.8 39.7 43.0	45.2 40.0 34.8 37.4 39.9 41.8 40.7 42.7	45.2 40.0 35.2 38.4 40.2 41.8 41.2 43.0	45.4 40.0 35.9 39.0 40.4 41.8 41.2 42.4	45° 40° 36° 39° 40° 41° 41° 42°
DECEMBER.	9 10 11 12 13 14 15 16 17 18 19 20 21 22	45.6 45.8 43.0 32.0 34.6 38.0 40.0 39.7 41.9 38.1 40.0	45.6 45.4 42.6 — 32.3 34.2 38.0 40.0 39.0 41.7 — 38.2 40.2	45.1 45.2 41.8 ————————————————————————————————————	44.5 45.4 41.2 — 33.1 34.4 37.4 39.7 38.4 41.5 — 38.2 39.1	46.2 40.5 	45.2 46.6 40.5 — 33.4 36.0 38.7 40.8 39.0 42.5 — 38.2 36.1	45.8 46.0 40.4 — 33.8 36.4 39.1 41.5 39.4 42.5 — 38.7 35.6	45.6 40.4 	45.2 40.0 	45°2 40°0 35°2 38°4 40°2 41°8 41°2 43°0 40°2	45.4 40.0 35.9 39.0 40.4 41.8 41.2 42.4 40.2	45° 40° 36° 39° 40° 41° 41° 42° 40°
DECEMBER.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	45.6 45.8 43.0 — 32.0 34.6 38.0 40.0 39.7 41.9 — 38.1 40.0 38.1	45.6 45.4 42.6 ————————————————————————————————————	45.1 45.2 41.8 — 32.6 33.9 37.4 39.6 39.1 41.5 — 38.2 39.4 37.4	44.5 45.4 41.2 — 33.1 34.4 37.4 39.7 38.4 41.5 — 38.2 39.1 37.4	46.2 40.5 	45.2 46.6 40.5 — 33.4 36.0 38.7 40.8 39.0 42.5 — 38.2 36.1 37.2	45.8 46.0 40.4 — 33.8 36.4 39.1 41.5 39.4 42.5 — 38.7 35.6 37.0	45.6 40.4 	45.2 40.0 	45.2 40.0 35.2 38.4 40.2 41.8 41.2 43.0	45.4 40.0 35.9 39.0 40.4 41.8 41.2 42.4	45° 40° 36° 39° 40° 41° 42° 40° 36° 41°
DECEMBER.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	45.6 45.8 43.0 32.0 34.6 38.0 40.0 39.7 41.9 38.1 40.0	45.6 45.4 42.6 — 32.3 34.2 38.0 40.0 39.0 41.7 — 38.2 40.2	45°1 45°2 41°8 ————————————————————————————————————	44.5 45.4 41.2 — 33.1 34.4 37.4 39.7 38.4 41.5 — 38.2 39.1	46.2 40.5 	45.2 46.6 40.5 — 33.4 36.0 38.7 40.8 39.0 42.5 — 38.2 36.1	45.8 46.0 40.4 — 33.8 36.4 39.1 41.5 39.4 42.5 — 38.7 35.6 37.0 43.4	45.6 40.4 	45.2 40.0 	45.2 40.0 35.2 38.4 40.2 41.8 41.2 43.0 	45.4 40.0 	45° 40° 36° 39° 40° 41° 42° 40° 36° 41° 44°
DECEMBER.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	45.6 45.8 43.0 — 32.0 34.6 38.0 40.0 39.7 41.9 — 38.1 40.0 38.1	45.6 45.4 42.6 ————————————————————————————————————	45.1 45.2 41.8 — 32.6 33.9 37.4 39.6 39.1 41.5 — 38.2 39.4 37.4 42.9 — 39.4	44.5 45.4 41.2 — 33.1 34.4 37.4 39.7 38.4 41.5 — 38.2 39.1 37.4	46.2 40.5 	45.2 46.6 40.5 — 33.4 36.0 38.7 40.8 39.0 42.5 — 38.2 36.1 37.2	45.8 46.0 40.4 — 33.8 36.4 39.1 41.5 39.4 42.5 — 38.7 35.6 37.0	45.6 40.4 	45.2 40.0 	45.2 40.0 35.2 38.4 40.2 41.8 41.2 43.0 	45.4 40.0 	45° 40° 36° 39° 40° 41° 42° 40° 36° 41° 44°
DECEMBER.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	45.6 45.8 43.0 	45.6 45.4 42.6 — 32.3 34.2 38.0 40.0 39.0 41.7 — 38.2 40.2 38.0 42.2 — 39.9 — 46.4	45·1 45·2 41·8 — 32·6 33·9 37·4 39·6 39·1 41·5 — 38·2 39·4 37·4 42·9 — 46·1	44.5 45.4 41.2 — 33.1 34.4 37.4 39.7 38.4 41.5 — 38.2 39.1 37.4 42.2	46.2 40.5 — 33.2 34.9 38.0 40.8 38.1 42.2 — 38.2 37.1 37.3 41.7	45.2 46.6 40.5 	45.8 46.0 40.4 — 33.8 36.4 39.1 41.5 39.4 42.5 — 38.7 35.6 37.0 43.4 —	45.6 40.4 	45.2 40.0 	45.2 40.0 	45.4 40.0 	48° 45° 40° 36° 39° 40° 41° 42° 40° 41° 41° 41° 45°
DECEMBER.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	45.6 45.8 43.0 	45.6 45.4 42.6 — 32.3 34.2 38.0 40.0 39.0 41.7 — 38.2 40.2 38.0 42.2 — 39.9 — 46.4 43.0	45·1 45·2 41·8 — 32·6 33·9 37·4 39·6 39·1 41·5 — 38·2 39·4 42·9 — 39·4 42·9 — 46·1 42·5	44.5 45.4 41.2 — 33.1 34.4 37.4 39.7 38.4 41.5 — 38.2 39.1 37.4 42.2 — 45.8 41.8	46.2 40.5 — 33.2 34.9 38.0 40.8 38.1 42.2 — 38.2 37.1 37.3 41.7 — 45.8 41.4	45.2 46.6 40.5 — 33.4 36.0 38.7 40.8 39.0 42.5 — 38.2 36.1 37.2 42.4 — 40.0 — 46.1 41.6	45.8 46.0 40.4 	45.6 40.4 	45.2 40.0 	45.2 40.0 	45.4 40.0 35.9 39.0 40.4 41.8 41.2 42.4 40.2 35.8 40.0 44.5 	45° 40° 36° 39° 40° 41° 42° 40° 36° 41° 44° 41° 45° 42° 42° 42° 42° 42° 42° 42° 42° 42° 42
DECEMBER.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 27 28 29 30	45.6 45.8 43.0 — 32.0 34.6 38.0 40.0 39.7 41.9 — 38.1 40.0 38.1 42.2 — 46.6 43.6 43.6	45.6 45.4 42.6 ————————————————————————————————————	45·1 45·2 41·8 — 32·6 33·9 37·4 39·6 39·1 41·5 — 38·2 39·4 42·9 — 46·1 42·5 44·2	44.5 45.4 41.2 — 33.1 34.4 37.4 39.7 38.2 39.1 37.4 42.2 — 38.7 41.8 41.8 44.2	46·2 40·5 — 33·2 34·9 38·0 40·8 38·1 42·2 — 38·2 37·1 37·3 41·7 — 45·8 41·4 45·0	45.2 46.6 40.5 	45.8 46.0 40.4 	45.6 40.4 34.1 36.9 39.7 41.8 39.7 43.0 	45.2 40.0 	45.2 40.0 	45.4 40.0 	45° 40° 36° 39° 40° 41° 42° 40° 36° 41° 44° 41° 45° 42° 47°
DECEMBER.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	45.6 45.8 43.0 	45.6 45.4 42.6 — 32.3 34.2 38.0 40.0 39.0 41.7 — 38.2 40.2 38.0 42.2 — 39.9 — 46.4 43.0	45·1 45·2 41·8 — 32·6 33·9 37·4 39·6 39·1 41·5 — 38·2 39·4 42·9 — 39·4 42·9 — 46·1 42·5	44.5 45.4 41.2 — 33.1 34.4 37.4 39.7 38.4 41.5 — 38.2 39.1 37.4 42.2 — 45.8 41.8	46.2 40.5 — 33.2 34.9 38.0 40.8 38.1 42.2 — 38.2 37.1 37.3 41.7 — 45.8 41.4	45.2 46.6 40.5 — 33.4 36.0 38.7 40.8 39.0 42.5 — 38.2 36.1 37.2 42.4 — 40.0 — 46.1 41.6	45.8 46.0 40.4 	45.6 40.4 	45.2 40.0 	45.2 40.0 	45.4 40.0 	45° 40° 36° 39° 40° 41° 42° 40° 36° 41° 44° 41° 45° 42° 42° 42° 42° 42° 42° 42° 42° 42° 42

^a Christmas Day.

	One Scale	Division =	: '000065 pa	irts of the V	F. Increa	ase, in Scale	Divisions, o	orrespondin	g to 1° decr	ease of Tem	perature, 1°	.1
12h.	13h.	14h.	15h.	16h.	17h.	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily an Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 216 75
218.4	218.4	220.1	218.6	217.7	213.0	213.0	214.7	214.2	213.2	213.2	209.7	
203.7	203.1	202.1	202.2	202.4	200.6	200.0	198.6	199.0	200.3	200.9	201.6	205.65
206.2	207.1	206.8	207.3	207.3	207.7	208.7	209.1	209.6	208.5	208.5	208.5	206.2
09.7	209.3	208.1	206.4	206.2	207.2	207.7	207.4	207.4	207.4	205.0	206.9	208.79
04*4	206.2	205.4	205.5	205.9	205.9		<u> </u>				- 7	208:40
	l —			l		217.6	217.1	216.8	215.5	214.2	$\{ \frac{1}{215\cdot 3} \}$	200 40
08.1	207.7	206.5	206.6	206.5	205.6	205.6	205.4	204.6	203.7	203.3	203.4	208.0
04.7	205.5	206.3	207.6	207.7	207.3	205.1	205.2	205.2	205.6	205.0	206.0	205.0
11.7	211.2	225.4	218.8	213.0	208.4	206.3	204.0	203.9	207.0	208.4	208.1	208.66
08.6	202.2	207.6	207.3	207.3	209.0	207.1	207.3	207.3	207.0	205.0	205.0	207.79
11.2	211.7	213.0								212.3	212.2	210.73
			215.3	214.4	214.4	214.4	212.6	208.5	208.2	212 3		210 /
20.4	220.1	220.2	221.6	220.3	219.1			205.5		007.4	$\left\{ \frac{-}{228\cdot 4}\right\}$	220.80
			<u>-</u>			228'1	227.7	227.5	227.2	227.4		
22.9	223.7	223.7	223.8	222.2	222.2	223.4	221.4	224.5	224'1	224.5	224.2	224.6
15.4	215.1	213.9	220.2	220.2	215.4	215.4	216.4	220.8	220.8	216.7	216.1	220.30
11.8	211.6	211.6	212.0	211.4	210.8	211.7	212.3	212.3	212.5	213.3	214.2	213.2
08.2	209.7	210.8	210.2	210.2	210.6	210.2	211.6	2 12.6	214.0	210.2	210.0	210.9
09.1	209.4	209.4	208.7	208.7	208.7	208.7	206.2	206.4	206.8	206.0	207.3	209.4
$08.\overline{2}$	208.2	208.2	208.2	208 1	207.4	200 1	200 2	200 1	200 0			
00 2	200 2	200 2	200 2	200 1	207 4	017:0	014:0	217.3	216.9	215.5	215.5	210.0
10.5	0100	-			-	217.2	214.6					010.4
10.7	213.5	213.0	214.3	211.4	213.5	214.6	214.5	214.7	214.4	214'4	214.1	213.4
17.8	217.8	217.3	214.7	216 1	216.0	214.5	214.2	214.2	213.9	213.7	214.0	215.5
17'4	222.9	215.8	215.2	213.0	198.9	208.0	209.1	206.9	207.0	205.3	205.4	213.08
08.2	207.8	204.0	203.5	202.0	200.0	_				_	— 1	208.28
- 09.6	209.6	208.7	_		<u> </u>	214.7	211.4	215.1	212.6	211.0	212.4	
-	209 0	200 1	207*4	203.3	201.2	200.0	200.2	200.2	200.6	200.2	200.3	208.00
04.1	205.4	203.5	000:7	004:0	204.0		1			203.2	204.1	203 29
			203.7	204.2	204.2	203.1	204.2	205.6	204.3			
08.2	209.0	209.0	209.0	208.8	208.3	207.7	205.7	205.6	205.4	205.1	205.4	207.8
00.0	201.0	201.2	200.8	200.3	200.2	200.0	201.3	201.3	199.5	199'6	198.3	201.30
05.0	205.2	205.0	196.7	197:3	197.4	197.0	197.2	196.7	197.7	196.7	197.0	199.0
10.18	210.20	210.63	210.23	209.47	208.20	210.00	209.60	209'94	209.78	209.20	209:36	210.50
				ТЕМРЕ	RATURE OF	THE VER	FICAL FOR	E MAGNET				
4î 6	4η2	41.2	42.0	42.0	42.2	42°2	42.3	42.3	42°6	43.3	43.4	4î·4
49'3	49.7	50.0	50.2	50.2	50.6	51.0	51.6	51.4	51.2	51.0	50.9	48.01
47.8	47.4	47.2	47.0	46.7	46.2	46.5	45.6	45.4	45.2	45'1	45.0	47.42
46.3	46.3	46.7	47.1	47.2					46.7	47.0	47.2	45 9
48'4				47.0	46.9	46.9	46.7	46.5	40 /		1 1 1	10 50
	48.3	48.2	48.0	47.9	47.7		10.0	41.0	41.6	42.3	$\left\{ \begin{array}{c} - \\ 42.7 \end{array} \right\}$	46.18
16:0	400.4	4000		45.0		40.4	40.9	41.3	41.6		42 ()	47.0
46.2	46.4	46.6	47.1	47.3	47.6	47.7	47.6	47.8	48.4	48.7	48.8	45.8
48.6	48'6	48.4	48.0	48.0	47.6	48.0	48.2	47.8	48.0	48.0	47.4	48.3
47.8	48.0	47.8	47.6	47.6	47.5	47.5	47.2	46.7	46.4	46.2	45.9	47.0
47.6	47.5	47.4	47.4	47.2	46.6	46.4	46.4	46.3	46.2	$46^{\circ}2$	46'3	46.38
44.7	44.4	44.3	44'0	44.0	43.6	43.4	43.6	43.4	43.4	43.4	43.2	44.69
40.0	39.8	40.0	39.7	40.0	40.2	_		_				90.5
_		-				32.3	32.2	32.4	32.6	32.3	$\frac{-}{32\cdot 1}$	38.5
36.3	36.1	35.9	36.0	36.5	36.4					35.4	35.5	34.89
39.4						36.0	35.8	35.6	35.4		37.0	37.40
40.2	39.3	39.1	39.3	39.2	39.3	38.8	38.7	38.3	38.1	37.2		
10.0	40.5	40.5	40.7	40.7	40.5	40.2	40.0	40.0	40.0	40.0	40.0	39.6
41.6	41.6	41.3	41.1	41.0	40.2	40.0	39.9	39.7	39.2	39.9	39.6	40.70
11.7	41.9	42.1	42.4	42.4	42.3	42.4	42.6	42.6	42.4	42.4	42.4	41'0
43.0	43.0	43.2	43.0	43.0	42.8		l			_	— \	41.0
_		1				36.6	37.2	37.3	37.8	38.1	$\frac{-}{38\cdot 1}\}$	41.2
40'4	39.9	40.0	40.0	40.2	40.0	39.7	39.7	39.8	39.8	39.8	39.9	39.48
37.0	37.6	38.0	38.1	37.9					$\frac{38\cdot2}{}$	38.4	38.4	37.55
41.6	41.5				38.1	38.3	38.2	38.2		43.0	43.0	40.2
		40.8	41.4	42.0	42.4	42.2	42.2	42.9	42.6	40 0		
	44.6	45.2	46.0	46.2	46.4	39.1	39.1	38.9	39.0	39'1	$\frac{-}{39\cdot 2}$	42.72
44.4	41.5	42.0	42.8	43.4	44.2	_	-				47.0}	42.10
44'4 - 41'2	l .					45.4	45.6	45.7	45.5	45.7		
41.2					1 49 4	43.4	43.4	43.5	43.6	43.8	43.7	44.70
44.4 	44.0	43.6	43.3	43.4	43.4	10 1	1 20 2					
44.4 41.2 - 44.9 42.2	44.0 42.2	43.6 42.2	$\begin{array}{c c} 43.3 \\ 42.3 \end{array}$						43*4	43.6	43.6	42.43
44.4 41.2 -44.9 42.2 47.0	44.0 42.2	43.6 42.2	42.3	42.4	42.5	42.6	43.0	43*2		43.6	43.6	
44.4 41.2 	44.0	43.6							43°4 47°6 48°4			$42^{\circ}4$

	o	ne Scale Div	vision = '00	00066 parts	of the V.F.	VERT	ICAL FOR in Scale Div	RCE.	esponding to	1º decrease	of Tempera	ture, 1 · 64.	
Mean (gen T	Föttin- }	0h.	1h.	$2^{ m h}.$	3h,	4 ^h .	5 ^h .	6 ^h •	7h.	8h.	9h.	10h.	11h.
	$\begin{bmatrix} 1 \\ 2 \end{bmatrix}$	Sc. Div. 197.0 197.8	sc. Div. 197 0 198 4	sc. Div. 196 5 199 3	sc. Div. 197 4 199 3	Sc. Div. 196.7 199.3	Sc. Div. 197 1 198 9	Sc. Div. 198.6 200.0	Sc. Div. 198 6 200 0	Sc. Div. 198 5 200 0	sc. Div. 199 ° 0 200 ° 0	Sc. Div. 198 6 200 0	Sc. Div 199'1 202'0
	3 4 5 6 7 8	207.5 199.7 203.2 200.0 212.0 223.4	208 0 199 1 203 2 200 0 215 7 223 4	207 · 5 199 · 5 201 · 3 200 · 7 216 · 6 220 · 0	205 · 4 200 · 0 201 · 4 200 · 7 215 · 0 220 · 0	205°9 198°4 200°6 200°5 215°6 220°0	206.6 199.7 201.7 201.7 218.7 220.0	206°2 203°9 201°5 201°7 220°0 220°6	206 · 2 203 · 9 202 · 6 201 · 9 222 · 5 217 · 7	205.5 200.6 202.0 202.3 221.0 217.4	205°3 200°0 201°0 195°7 220°0 218°5	203.6 200.6 199.8 196.3 219.2 218.8	204 · 2 200 · 5 198 · 5 203 · 7 220 · 3 219 · 3
JANUARY.	10 11 12 13 14 15 16	225 · 5 225 · 0 214 · 7 200 · 3 193 · 2 189 · 4	227 · 4 225 · 8 214 · 7 200 · 6 193 · 3 189 · 6	228 · 8 223 · 2 215 · 0 200 · 6 194 · 6 190 · 5	226.0 223.2 213.6 200.0 194.5 191.6	225 °3 220 °6 213 °6 198 °3 194 °5 192 °4	225·2 219·5 211·4 197·4 194·9 194·1	227°3 219°5 210°0 197°6 193°4 195°1	228·2 219·5 211·2 197·7 192·5 197·7	228·2 220·1 211·1 198·5 192·4 197·7	229°3 219°2 208°4 197°4 192°5 198°3	229°3 217°4 208°5 197°1 191°8 198°3	229 · 5 215 · 6 207 · 5 196 · 6 191 · 7 198 · 8
JA	17 18 19 20 21 22 23	213°0 213°4 215°1 208°9 220°1 221°7	212.6 213.1 215.1 210.5 220.1 220.1	212 · 1 213 · 4 215 · 1 210 · 1 219 · 9 218 · 7	212·1 211·9 215·1 210·0 216·5 217·1	211·1 213·3 215·2 213·7 218·2 216·0	211.1° 213.8 214.1 215.6 219.4 214.2	208·2 215·8 215·4 215·0 220·5 213·1	207.4 215.4 215.4 214.5 220.5 212.5	207 · 4 215 · 4 215 · 4 216 · 4 218 · 9 211 · 7	205°3 214°3 215°4 217°4 220°9 210°0	205°3 214°3 214°9 218°9 219°8 206°7	205 '4 214 '3 213 '9 219 '1 221 '1 208 '0
	24 25 26 27 28 29 30 31	214 · 5 206 · 6 206 · 6 214 · 7 208 · 6 207 · 2	214 · 5 206 · 6 207 · 4 216 · 7 206 · 7 207 · 2	214.5 206.6 205.7 216.5 203.8 208.6	212.8 204.0 207.1 215.3 202.6 206.8	210.6 203.1 208.1 216.3 206.3 205.7	210°0 201°2 208°4 214°9 205°0 203°5	210°0 200°9 208°8 214°0 205°0 206°9	210.6 198.5 208.1 213.1 205.0 207.8	210°3 199°9 209°1 211°0 202°8 218°1	209°1 199°9 209°4 209°3 203°4 255°2	207 '9 199 '9 209 '6 208 '1 205 '0 225 '8	208°3 200°4 210°3 209°2 207°1 225°3
Hourl	y Means	209.50	209.49	209.50	208.44	208.43	208.39	208.81	208.81	208.91	209.78	208.29	208.8
						URE OF TE				,			
	$\begin{pmatrix} 1 \\ 2 \\ 2 \end{pmatrix}$	48°4 46°7	48°3 46°6	48°0 46°3	48°1 46°0	48°1 45°8	48·2 46·2	47.5 46.2	47°9 46°3	47° 4 46° 6	47°4 47°0	47°0 47°0	47°2 47°1
	3 4 5 6 7 8 9	43.0 47.2 45.6 46.6 38.7 34.3	42.8 46.8 45.5 46.6 38.0 34.1	42.9 46.2 45.4 46.5 37.3 34.0	42.8 45.7 45.0 46.1 37.3 33.8	42.7 46.3 45.3 46.2 37.1 34.0	42.8 46.4 46.0 46.3 37.4 34.6	43°1 45°0 46°3 46°4 36°7 35°2	43.6 44.9 46.3 45.6 36.0 36.0	44.1 46.2 46.4 45.0 35.4 36.0	44.4 46.8 46.9 45.0 35.5 36.5	44.6 46.8 47.5 44.8 35.6 36.9	44.5 46.7 48.0 44.5 35.7 35.9
JANUARY.	10 11 12 13 14 15 16	29°3 30°1 36°2 45°0 49°8 50°8	29.5 29.7 36.3 45.0 49.4 50.4	29.8 30.1 36.1 45.0 49.0 50.0	29.8 30.5 36.2 45.1 48.6 49.4	30°1 31°1 37°1 45°4 48°4 48°8	30.8 32.1 38.6 46.6 48.8 48.6	30°1 32°8 40°0 47°0 49°4 47°6	29·1 33·4 39·7 47·6 50·0 46·9	29.0 33.9 40.7 47.7 50.3 46.5	28.8 35.0 42.0 47.8 50.4 45.9	28.7 35.8 42.4 47.8 50.5 45.4	29·5 36·3 42·6 47·8 50·2 44·8
JAN	17 18 19 20 21 22 23	37.8 39.2 34.0 39.1 31.2 32.8	38.0 38.7 34.0 39.1 31.2 33.0	38°1 38°7 34°0 39°1 31°3 33°4	38·1 38·1 34·3 38·4 31·9 33·9	38.4 37.7 34.6 37.4 31.6 34.6	39°1 37°2 35°3 37°1 31°6 35°5	39.7 37.1 35.9 36.9 32.1 36.2	40.0 37.1 35.9 36.6 31.5 37.8	40.2 36.9 36.2 36.9 31.9 38.1	40.4 36.8 36.4 36.6 32.1 39.0	41'2 36'5 36'8 36'2 32'4 39'3	41.6 36.4 38.1 35.5 33.0 39.5
	24 25 26 27 28 29 30 31	36·2 40·5 40·2 35·0 39·1 40·0	36°1 40°7 40°4 34°6 39°3 40°0	35.8 41.0 39.8 34.2 39.5 40.0	36.8 41.4 39.8 34.4 39.9 39.9	37.6 41.7 40.0 34.4 39.4 40.1	38·1 42·6 39·8 35·1 39·7 40·4	38·1 43·4 39·3 35·8 40·0 40·5	38·3 43·6 39·7 36·1 40·7 40·6	39°1 43°9 39°1 36°7 41°4 40°4	39.5 44.2 38.4 37.8 42.0 40.6	39.7 44.0 38.5 38.2 42.0 40.4	39.5 44.0 37.6 39.0 41.6 40.4
		i '										_	

^a Twenty minutes late.

b Twelve minutes late.

1					VI	ERTICAL	FORCE.					
	One Scale	Division =	: *000066 pa	rts of the V	. F. Increa	ase, in Scale	Divisions,	orrespondin	g to 1° decr	ease of Tem	perature, 1	
12 ^h .	13 ^h .	14 ^h .	15h.	16 ^h .	17h.	18h.	19 ^h •	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 199°2	Sc. Div. 195°0	Sc. Div.	Sc. Div. 198 26
198.8	198.8	199.3	199.2	199.2	198.8	199.2	199.4	199.4	199 4	130 0	l əl	
200.8	200.0	200.0	200.0	200.2	200.0	207.8	209.6	209.6	207.4	206.7	$ \ _{207} \cdot _{2} \} $	201.85
204.2	204.3	203.8	204.2	202.1	202.2	202.2	186.6	193.4	195.0	204.1	203.0	203.22
204.2	201.8	198.1	197.0	197.9	198.4	198.4	198.8	201.4	201.9	202.9	202.6	200.25
197.4	198.4	200.2	201.8	203.4	202.3	202.3	201.6	201.4	201.5	200.4	200.2	201.18
205.6	206.5	208.1	207.9	208.2	209.8	210.4	210.5	210.2	210.8	210.7	212.0	204.83
219.2	219.2	220.4	220.4	220.1	221.9	221.9	220.6	221.5	221.5	221.5	221.7	219.44
219.0	218.8	218.8	220.4	220.4	220'1	 					$\left \frac{-}{222\cdot 4} \right\}$	221.07
l —		_	_	_		225.0	225.8	225.5	225.2	225.1	222 4)	225.85
226.0	225.0	223.0	220.6	222.5	223.1		225°1°a	225.1	225.5	223.6 214.7	214.7	218.59
215.7	215.7	220.3	216.9	217.7	217.4	214.6	216°4°	216.4	217.0	202.9	200.7	208.16
205.7	205.7	205.7	206.1	205.6	204.9	204.6	204.7	204.7 192.6	194.1	194.1	193.3	196.45
195.4	197'1	196.1	196.0	195.5	195.5	190.3	192.6 190.4	192.6	190.4	190.1	190.1	191.97
194.9	191.0	190.6	190'1	189.9	189.9	189.9	190 4	190 0	130 1			
201.2	201.8	202.0	203.5	204.3	204.4	215.7	215.5	215.0	215.0	213.5	$\left\{ \frac{1}{214\cdot 5}\right\}$	201.66
205.3	204.3	203.6	203.8	205.1	206.1	206.1	207.5	206.6	208.2	207.6	207.3	207.62
205 3	214.5	203 6	205 8	$\frac{205}{215}$.3	215.9	216.6	216.6	216.4	216.4	215.1	215.1	214.77
214.3	210.1	209.0	208.8	210.5	209.1	208.4	207.6	207.5	209.2	212.8	210.1	212.30
218.9	218.1	218.1	218.2	218.1	218.7	220.0	219.0	220.5	220.7	220.0	221.1	216.73
221.1	220.4	221.3	218.3	220.3	223.2	223.2	222.4	222.6	222'1	221.0	221.7	220.56
207.1	207.7	207.8	207.8	208.0	208.0		_				}	212.72
_			_	-		213.7	215.3	215.4	215.5	214.2	214.7	208*89
208.3	208.5	207.0	206.3	205.9	205.9	206.1	205.8	206.6	206.6	206.6	206.6	208 89
201.4	202.5	204.0	204.0	204.2	204.8	204.5	204.5	205.7	205.7	206.0 213.5	206°3 213°7	203 38
210.3	210.1	211'4	212.1	212.1	213.2	212.3	212.3	213.2	213°1 203°9	207.7	209.7	210 23
208.0	208.0	210.0	209.5	210.6	210.4	210.3	205.5	205°1 206°8	207.3	207.4	207.1	206.36
210.7	210.8	207.7	206.2	205.7	206.1	207.9	207.7	200 8	201 5	207 1	- 1	
220.3	219.4	219.4	221.4	222.0	218.2	220.4	220.3	220.3	213.0	212.8	212.6}	216.29
208.28	208.39	208.48	208.30	208.63	208.78	209.27	209.31	209.76	209.67	209.63	209.67	208.96
	(ТЕМРЕЯ	ATURE OF	THE VERT	ICAL FORC	E MAGNET.				
47.4	47.4	47°3	46.6	46°3	46.0	46.0	46.0	46.4	46°6	46°7	46°6	47.20
47.4	47 4	47.4	47.0	47.0	46.6						- 1	45.24
	1, 0			_		40.6	41'4	42.0	42.5	43.0	42.7	
44.2	45.0	45.2	45.0	46.7	46.6	46.6	47.2	47.4	47.6	47.4	47.4	44'91
47 0	47.0	47.0	46.8	46.7	46.6	46.9	46'3	46.2	46.2	46.3	45.8	46.41
48.6	48.5	47.7	47.4	47.0	46.6	46.5	46.4	46.6	46.7	46.9	47.0	46.67 43.30
43.7	42.6	42.0	41.4	41.0	40.2	39.7	39.4	39.5	40.0	40.0	40°0 34°2	35.23
35.8	35.2	35.3	33.7	33.8	33.9	33.8	33.8	34.0	34.0	34.1	1 1	1
35.8	36.3	36.1	36.1	36.0	36.1	90.5		30.0	29.7	29.4	$\frac{-}{29\cdot 4}$	34.05
20:0	-	-		31.0	30.8	30.2	30.2	30.9	31.0	30.8	30.8	30.19
30.6	31.1	31.3	31.0	36.5	36.0	36.6	36.6	36.3	36.2	36.2	36.3	34.59
38.0 42.5	37.2 42.2	36.6 42.2	36.6 42.2	42.2	42.4	42.6	42.8	42.8	43.2	43.6	44.4	40.87
48.4	48.4	48.4	48.6	48.8	48.9	49.1	49.3	49.3	49.3	49.3	45.8	47.56
50.8	50.6	51.2	51.5	51.5	51.5	51.2	51.1	50.9	51.0	51.0	51.0	50.30
44.8	44.1	43.0	41.8	41.0	40.2	 					$\left \begin{array}{c} - \\ 37 \cdot 2 \end{array} \right\}$	43.64
		-				35.2	35.6	36.0	36.5	36.6		
42.2	41.8	42.2	42.2	41.7	41.5	41.1	40.7	40.6	40.5	40.1	40.0	40.30
36.4	36.3	36.5	36.5	36.0	35.1	34.9	34.2	34.0	34.4	34.3	34.0	36.35
39.5	40.0	39.9	39.9	39.7	39.4	39.6	40.0	40.0	39.5	39.3	31.3	37.55 35.61
36.0	35.8	34.8	34.6	34.7	34'1	33.9	33.6	32.8	32.3	$\begin{array}{c} 31.8 \\ 32.2 \end{array}$	32.2	32.53
33.5	33.6	33.2	33.1	32.7	32.3	32.5	32.4	32.3	32.1	04 2		1
40.0	39.7	39.7	39.8	40.0	40.0	95.0	35.2	35.3	35.7	35.9	${35.9}$	36. 90
39.7	-	20:0	40.5	40:0	10:0	35°2 40°0	40.0	40.0	40.0	40.0	40.4	38.98
44.0	39.6	39.8	40.5 42.5	40.6 42.3	40.2	41.8	42.0	41.4	40.8	40.4	40.0	42.29
37.8	43.8 37.4	43°3 37°1	37·2	37·1	37.3	37.3	37.3	37.3	36.6	36.3	35.1	38.18
39.4	39.6	39.8	39.9	39.7	39.2	39.3	39.1	38.9	38.8	38.9	38.9	37.63
41.9	42.1	42.4	42.2	42.0	41.9	41.4	40.6	40.4	40.5	40.2	40.0	40.83
41.3	40.6	40.5	39.2	39.3	39.3	35.6	35.6	35.7	36.0	36.2	37.1}	39.17
41'41	41.30	41.13	40.88	40.80	40.56	39.92	39.52	39.20	39.52	39.2	39.34	40.28
11	41 OO	47 10	1 10 00	10 00	10 00	00 0			l	l	<u> </u>	

^c Ten minutes late.

VERTICAL FORCE. One Scale Division = '000065 parts of the V. F. Increase, in Scale Divisions, corresponding to 1° decrease of Temperature, 1'64. Mean Göttin-gen Time. Oh. 1h. 3h. 4h. 5h. 6h. 9h. 10h. 11h. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. 214.2 212.5 214.2 210.1 209.4 210'6 212.3 211.2 208'0 205.8 205.8 203.7 2 198.7 200'4 200.1 199'2 198'6 197:3 196.7 195.6 195'2 196.1 195.5 195.5 3 192.6 196.3 192.9 191'2 192.8 194.7 193.2 194.6 193.6 194.7 194.7 197.7 4 208:0 211.3 215.2 213.2 212.4 211'1 214.4 213.4 212.3 209.7 210.0 a 208'6 5 211.0 210.4 214'4 213.2 212.1 211.9 210.2 209.5 208.0 206.6 205.0 204.8 6 202.0 203'1 200.0 200.3 202.3 203.2 205.4 206.9 209.9 214'0 212.8 212.8 7 8 203.1 202.8 202.2 198.5 199.7 198'6 199.8 199'9 199:3 200.3 199.2 199.2 9 197.1 198.7 195'3 193.9 194.5 193.7 194'5 195.0 1951 195.3 197.6 1991 10 197.9 197.6 197.6 198.1 197.9 195'9 195'0 195.8 195.8 195.8 195.8 195'8 11 200.7 200.6 203.3 202.9 201.6 202.2 202'1 201.3 202.4 202.4 204.3 204'3 FEBRUARY 12 205.0 205.7 206.0 201.7 203.4 201.8 201.8 200.2 199.8 199.2 199.5 199.7 13 204'1 203.9 203.3 204.3 203'1 201.5 200.0 201.1 201.8 203'4 202.8 201.7 14 203'9 15 204.2 202.2 202.3 202.2 200.6 202:2 200:5 201.7 203.2 202.5 201.0 206.7 16 206.7 208.7 211.5 210.1 210'3 210.1 212.0 211.2 210.3 р 210.2 210.1 c 17 207.0 206'6 206.6 205.1 204.7 203.8 202.2 201.4 200.8 199.5 198.7 198'9 18 204.5 204.5 202.1 203:2 200.7 200:3 198'3 198:3 199'0 198'2 197.5 196.4 19 198'4 198.0 198.8 198.8 199.0 198.2 197'1 197.1 197'1 195.8 194.9 194'9 20 195.6 197.5 197.6 196.6 1961 196'1 198.4 199.0 200'0 199.7 200.0 200.0 21 200.9 202.8 22 201.6 202.8 203.0 204.5 205.5 207.6 209'1 207.1 212.8 214'4 23 213'1 218.0 217.7 215'4 213.7 211.6 211'2a 210.0 212.3 24 207.6 213.4 218.1 207:6 208:1 211.4 211.2 210.3 210.9 214.9 213.6 214'3 25 204.3 211.6 209'4 207.2 206.0 205.4 204'3 208.1 205.5 203.7 203.7 201'0 26 208.7 214.1 213.8 212.8 210.3 208:3 206.8 206.5 208.7 205.3 204.5 207.9 27 201'1 203.6 204.7 204.2 203.4 204.5 203.3 201.9 200'8 201.0 201'4 201'4 28 203.58 205.17 205'32 204.03 Hourly Means 203'43 203'31 203'08 202.90 203.22 202.70 202.73 203'15 TEMPERATURE OF THE VERTICAL FORCE MAGNET. 37:3 37.8 38.5 38.1 38.3 38.7 39.3 39.6 40.6 41'4 42.0 42.2 2 44.7 44.3 45.4 45.4 45.5 46'4 47.0 47.3 47.6 47.7 48'2 48.2 3 49.2 49.0 49.0 48.7 48.9 48'9 48'9 48.7 48'3 48'2 46.2 46.9 4 37.9 37:1 36.6 37.1 36.4 36.5 36.9 37.6 38.1 38.9 39.3 39.1 5 36.3 36.2 36.3 36'2 37.0 37.2 38.0 38'5 39.3 39.8 40.2 40'4 6 39.1 39.0 39.7 39.5 39.8 40.3 39.8 40.2 40.8 41'4 42.0 42.6 7 8 42.8 43.0 43.8 43.5 43.7 44.2 44.6 44.9 45.0 45.4 45.4 45.5 9 46.2 46.2 48'8 47.5 47.2 47.2 47.2 47.2 47.1 47.1 47.1 47.2 10 45'6 45.8 45'9 45.0 45.2 45.8 46'3 46'6 46'6 47.0 47.4 47.2 11 43'4 43.0 42.2 42.3 42.6 42'4 42.6 43.2 42'9 43.0 42.6 42.6 12 41.4 41'4 41.7 42.7 FEBRUARY 42.6 43'4 43.8 44:3 44.7 45°0 45.1 45'3 41.7 13 41.7 40.8 40'8 41.0 42'3 41'8 42.8 42.5 42.5 42.5 42'4 14 15 41.8 41.6 41.2 41'4 41.3 42.2 42.4 42.3 42.3 42.4 42.2 42.3 16 38.9 38.5 37.8 36.6 36.7 36.9 36.7 37.0 37.2 38.0 38'4 38.2 17 40.0 40.0 40'6 40.4 40.8 41.4 42.4 43.0 43.6 44.4 44.9 45.0 18 41.6 41.4 41'4 41'4 41.8 42'4 43'1 43.8 44'1 44.5 45.2 45.8 19 45.2 45.6 45.9 45.0 45.0 45.2 45.6 45.5 46'3 46.6 46.8 46'5 20 46.0 46.0 45.6 45.2 45'4 45.3 44.9 44.5 44.0 43'8 43.9 44'4 21 22 37.1 36:9 37.1 36.9 37:1 40'0 38.6 38.7 40.1 40.0 40.0 39.7 23 35.8 36'3 35.3 37:3 37.1 37.4 37.9 38.1 39.4 24 33.3 33.5 34.0 38.0 35.1 35.336.3 37.7 38.8 39.8 40.0 40.0 25 39.9 39:3 39:3 39.6 42.0 42.4 40.5 41'3 42.9 43.9 44.4 44.8 26 39.1 38.8 38.8 40.5 42.7 40.3 42.1 41'3 42.6 43'4 42.9 42.7 2742.7 42.2 42.0 42'1 42.6 43.7 44.5 44.4 44.8 44.4 44.6 44.6 28 41.15 Hourly Means 40.97 41.14 41'20 41:35 41.87 42.26 42.80 42.85 43'42 43.55 43'44

^{*} Five minutes late.

b Two minutes late.

VERTICAL FORCE. One Scale Division = '000065 parts of the V. F. Increase, in Scale Divisions, corresponding to 1° decrease of Temperature, 1'64. Daily and 16h. 17h. 18h. 13h. 14h. 15h. 19h. 20h. 12h. 21h. 22h 23h Monthly Means. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. Sc. Div. 203.4 202.4 203.4 203.5 203.6 203.3 204.0 203'4 203.2 201.5 201.2 198'8 206.23 195.1 195.2 193.8 194.0 194.7 194.7 193.6 192.8 192.0 191.7 190.0 190.5 195.29 198.4 199'6 203'4 203.5 202.4 203.1 203.3 204.1 204'4 206.1 208.3 208.0 198.90 208.3 208.1 208.4 208.6 209.0 208.8 210.7 210.7 211.2 211.2 211.0 210.59 208:3 204.8 204.8 204.8 204.8 204.5 204.5 204.5 205.1 205.2 204.2 204.5 202.1 207.12 204.7 210.4 209.5 209.5 205.0 211.0 206'68 207.8 207.8 206.9 206.4 205:5 203.1 200.0 199'1 200.0 200:0 199'45 200.0 200.0 199.0 198'1 197.4 196'1 197:3 197.1 195.8 196.59 198.7 198'0 199.3 197.6 195.8 196.1 196.2 196.9 198.1 198:3 197.6 197.04 195.4 195.5 195.5 196.0 196.4 199.0 199'0 199.0 199'4 199.8 195.3 199.7 204.5 205.6 203.5 203.9 203.9 204.1 204'0 204.0 204.3 204.1 205.0 203:30 204.2 203.8 201.3 201.9 202.4 204.7 204.3 203'8 205.2 205.2 205'0 204.7 203.9 202.92 204.7 205.6 204.9 204.4 201.5 201.2 203.57 208:4 207.5 204'9 203.0 } 205.8 203.0 200.4 200'6 201.4 202.8 203'1 205.2 205.7 204'0 205.4 205.6 198.5 205.2 202.68 208.41 207.2 207.2 208.2 208.4 208.4 205.1 204.0 205'1 207.2 207.1 207:0 208.8 202'41 198:3 198.3 198.7 198'9 201.7 203.3 203.3 203.3 204'1 204'3 203.9 204.5 196.8 198.4 197:3 199.0 199.6 200.0 200.0 198.5 198.5 199'1 198'4 197.4 199'42 195.4 192.7 193.9 195.4 196.00 194.0 194.0 194.0 195.4 195'6 194.3 195.8 195.4 200.0 199.0 198.7 201.0 200.0 201'4 200:39 212.0 212.7 199.2 } 209'3 198.3 201.1 222.6 210.00 219.2 231.5 238'1 211.7 205.5 184.2 207.2 206.7 213.0 214.0 214.2 209'9 211'1 212.3 212.5 213.2 214.5 215'1 215.2 215.2 215.4 213'43 210:3 213.5 209.4 209.7 209.7 203.5 208.9 195.2 196.6 206.8 206.8 209'83 215'1 215'2 217:3 197.9 203:37 198.4 204.4 202:1 203'1 207.7 205.6 196.5 193.0 201.6 200.8 199.5 202'3 202'1 198.7 198.2 199.9 200.3 201.3 202.1 200.6 205.07 205.9 201.6 201.0 201'4 200.7 202.3 199.5 199.6 198.7 204.22 211.1} 210.7 212.9 211.4 210'4 211.3 203:07 203.68 204'29 203:27 202:35 202.66 202.73 203.77 203'32 203:13 203.33 203:37 203'40 TEMPERATURE OF THE VERTICAL FORCE MAGNET. 0 41.27 42'4 42.7 42.9 42.7 42.7 42.5 42.3 43.0 43'4 43'6 44'0 44.6 48.2 48.4 48'4 48.7 49.2 49'4 49'6 49.7 50.0 49'4 47.70 48.2 47:9 41.1 39.2 38.5 44.85 42.4 41.6 40.0 39.6 45.6 44.4 43.4 40.6 39.0 39'4 39.8 39.6 39.2 39.0 38.7 38.7 38.7 38.2 38.0 37.8 37.0 38.12 40.4 40.9 40.9 40.7 40.5 40'2 40'0 40.0 39.8 39.8 39.19 41.0 41.0 40.8 43.2 43.3 42.7 42.1 41.4 41.05 40.4 40.4 40.7 41'3 41.7 42.6 45'13 45.4 45.4 45.8 46.0 46.0 46.0 46.0 46.0 46.1 46.0 46.5 46.2 47.4 47.4 47.0 47.01 47.0 47.6 47.6 47.1 47.6 46.2 46.0 45'6 45'5 47.4 47.2 47.0 47.2 46.8 46.0 45.6 45.2 45'0 44.7 44.4 44.2 46.05 42.8 42.8 42.2 42'3 41.2 41'4 42.38 41.5 41.4 42.2 42.2 42.6 41'6 42.9645.0 44.4 43.8 43.2 43.0 41.9 41.3 41.4 41.3 41.4 41.4 41.6 42.4 41.7 42.2 42.3 41'4 41'5 41.65 39.8 39.7 40'8 41'2 41.9 42.0 } 43.0 41.7 41.2 39.9 39.1 41.57 42.4 41.5 40.6 43.0 43.0 39.5 39.5 39.4 39.7 39.7 39.8 40'4 40.1 40.0 39.7 38.71 40.0 39.6 39.7 40.3 45.0 43.4 43'1 41.7 41.4 42.85 45.4 44.3 43.6 42.2 41.5 45'4 44.9 44.2 45.2 45.8 45'1 45.6 45.4 44'9 44.7 44.4 44'6 45.2 45.2 44.03 47.3 46'8 47.4 47.1 46'6 46'8 46.7 46.33 46.6 46.9 47.4 46.6 46.6 44.4 44'4 43.2 44'0 44.5 44.6 42'61 37.1 } 36.3 36.3 36.4 36:3 36'8 39.8 37.0 40.4 40.7 40.8 40.8 40.2 39.0 39'18 40.6 40.8 39.5 38'6 39.5 35.6 36.90 39.2 39.2 37:0 36.8 35.0 34.3 34.0 33.6 38.7 37.8 40.1 38'10 39.8 39.8 39.1 39.1 39.1 39.5 39:3 39.1 39.1 39.1 39.7 45.1 45.0 44.7 44.7 44'1 43.7 43.5 42.6 41'9 41.0 40.0 39.5 42.34 43'4 42.82 45.0 44'9 44'8 44.0 44.4 44.2 43.8 45.0 43.9 44'6 44'6 44.9 44.8 44.7 44.6 44.5 44'6 42.39 37.8 37.8 37.9 37.9 38.0 37.5 43'62 41.82 41.70 41'38 42'33 43.63 43.53 43:31 43'12 42.81 42:02 41.56 41'55

[·] Three minutes late.

	On	e Scale Div	ision = '00	0065 parts o	of the V. F.		ICAL FOF in Scale Div		sponding to	1º decrease	of Tempera	ture, 1°64.	
Mean Göt gen Tim	ttin-)	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8h.	9h.	10h.	11h.
	1 2 3 4 5 6	Sc. Div. 211 3 211 0 201 5 199 4 204 4 197 1	Sc. Div. 210 ° 0 210 ° 4 201 ° 7 199 ° 6 205 ° 7 196 ° 6	Sc. Div. 210 '3 210 '3 201 '9 199 '0 206 '4 198 '9	Sc. Div. 208 * 5 203 * 5 201 * 3 195 * 7 a 194 * 9 196 * 8	sc. Div. 206 ° 0 203 ° 6 201 ° 3 194 ° 9 198 ° 7 194 ° 5	Sc. Div. 204 '9 203 '9 199 '7 194 '9 198 '6 193 '0	Sc. Div. 208 ' 3 202 ' 7 199 ' 1 195 ' 4 196 ' 6 193 ' 0	Sc. Div. 208 '2 201 '4 199 '6 196 '1 196 '2 191 '2	Sc. Div. 212 1 201 0 199 6 196 3 196 9 192 8	sc. Div. 221 ° 0 200 ° 4 197 ° 9 196 ° 3 196 ° 9 189 ° 7	224 1 199 9 196 7 197 2 196 1 193 0	sc. D 224 198 195 197 195 193
1 1 1 1 1	7 8 9 10 11 12	197'3 195'0 206'3 205'2 210'5 210'6	199°1 198°5 206°3 206°8 211°0 210°6	199°1 200°1 207°4 208°1 212°6 210°6	191 ° 2 204 ° 5 204 ° 2 205 ° 0 210 ° 8 208 ° 4	194.5 204.9 202.9 205.0 208.2 207.4	195°3 204°9 200°7 205°9 207°1 205°3	197.0 208.0 201.5 205.0 207.1 205.2	197'0 206'8 205'6 204'3 206'6 202'9	198'4 208'0 204'0 202'4 206'3 202'9	199.7 206.4 202.5 201.8 205.4 201.5	202.5 206.7 202.3 200.7 206.4 202.5	200° 206° 202° 201° 205° 209°
MARCI	14 15 16 17 18 19 ^d	206.6 211.2 213.1 198.7 190.4 195.8	208 · 4 214 · 3 214 · 1 201 · 3 175 · 7 195 · 9	208 · 2 213 · 9 213 · 5 200 · 0 171 · 8 197 · 2	209 · 2 209 · 5 207 · 9 198 · 4 176 · 9 197 · 0	205 · 9 209 · 8 207 · 6 196 · 0 186 · 4 196 · 2	205·2 208·0 205·6 193·5 203·6 194·6	203°3 206°9 205°1 190°7° 209°0 193°3	203°1 207°0 204°9 188°4 202°4 192°0	203 · 8 207 · 7 203 · 8 188 · 3 206 · 5 193 · 0	204.9 209.0 202.4 187.0 239.6 193.0	204.6 207.0 200.5 187.6 212.2 194.4	204 207 200 188 208 196
2 2 2 2 2 2 2 2	21 22 23 24 25 26	208 · 3 193 · 4 196 · 1 189 · 2 190 · 1 205 · 2	207 '9 195 '0 196 '1 191 '7 194 '6 207 '7	207 ° 0 197 ° 2 194 ° 9 190 ° 8 195 ° 3 208 ° 2	206.5 197.2 196.0 188.0 195.4 206.0	205.7 195.8 192.4 186.7 194.4 204.7	204.5 194.6 191.6 185.6 193.3 205.7	204°3 193°2 190°6 187°1 192°6 207°6	202.8 191.5 192.4 188.0 193.3 207.4	202.7 192.5 193.9 188.8 193.3 207.4	202.7 192.5 196.1 190.4 194.8 209.3	202.7 192.0 195.8 190.6 193.9 209.6	203 · 193 · 195 · 191 · 194 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 · 205 ·
3	28 29 30 31	203°4 196°8 205°1	202.8 200.6 204.3	200°4 200°0 200°5	197.6 198.9 202.1	194.9 198.2 201.9	194.9 198.8 202.6	194'1 198'2 202'1	194.0 198.8 198.2	194.8 199.1 199.3	194.8 199.2 198.8	198.6 198.1 198.6	193 202 199
Iourly M	Ieans	202.41	203.20	203.23	201.33	200.46	199.72	199.24	199'14	199.58	199.80	199.93	200
				,	FEMPERAT		E VERTICA		IAGNET.				. 0
	1 2 3 4 5 6	37·4 40·5 44·7 45·1 43·8 45·4	37·4 40·4 44·6 45·0 43·3 45·3	3 ⁷ ·9 41·0 44·2 45·8 43·4 45·4	39.0 43.0 44.4 47.0 48.0 46.3	39·3 42·9 44·7 47·1 44·9 47·4	39.9 42.8 45.2 47.5 45.8 48.0	39.6 43.4 46.0 47.8 46.4 48.4	40°0 44°4 46°4 47°9 47°0 48°6	40°4 45°0 46°8 48°2 47°4 48°7	40.6 45.6 47.4 48.9 48.2 49.6	40°6 46°1 48°0 49°3 48°4 49°0	40°0 46°2 48°2 49°4 48°0 49°0
1 1 1	7 8 9 10 11 12	44.5 42.2 40.4 41.4 37.0 38.1	44.1 41.6 40.3 40.9 36.6 38.0	45.4 40.9 40.6 40.8 37.0 38.7	47.2 40.6 41.8 41.2 38.2 39.0	46.4 40.6 42.2 40.6 39.3 39.3	46.6 40.6 43.3 40.6 40.0 39.8	46.7 40.8 43.7 41.4 40.0 40.7	47.0 41.0 44.2 41.7 39.9 41.2	47.0 41.0 44.4 42.2 40.2 41.8	46.7 41.0 45.8 42.3 41.6 42.8	47.0 41.1 44.9 43.4 41.5 43.4	47 '0 '40 '' 45 '' 42 '' 43 '' 43 ''
MARCH.	14 15 16 17 18 19 ^d 20	40°2 38°0 37°2 44°2 45°4 48°9	39.7 37.8 37.5 43.7 45.6 48.4	39.6 37.8 38.2 44.2 46.3 48.0	39.2 39.5 40.2 44.5 47.0 48.0	39.4 38.2 40.0 45.3 47.6 48.4	39.8 38.2 40.3 46.4 48.1 48.8	39.8 38.5 41.0 47.3 49.1 49.2	42.2 39.8 41.7 47.6 49.3 50.0	42.0 40.0 41.8 48.6 49.5 50.0	42·1 40·4 42·5 49·4 50·0 50·0	42·1 40·7 43·4 50·6 51·0 50·0	42: 41: 43: 51: 51: 49:
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^d Not included in the Means, on account of disturbance.

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	20 b 21 b	148'0 177'7	160.9	143.0 150.6	174.5 174.4	184.5 181.7	183.8	197.7 185.0	203.8	194.8	191.1	184.7	195
	$\frac{21}{22}$	170.6	170.6	171.0	172.8	173.3	175.3	179.2	178.6	186.9	179.6	178.0	178.8
	23	186.6	187.7 191.5	189.0	189°3 187°8	188°2 186°6	188.0 183.4	187.5 182.8	186.7 183.2	186.5 184.3	186.0 184.1	185.0	184.8 183.8
1	$\begin{bmatrix} 24 \\ 25 \end{bmatrix}$	193.1						-				_	
1	26	186.6	187.7 181.9	186.5 181.7	186°3 181°1	184.6 181.1	182.4 181.1	180.7 181.1	179.5 183.2	179°1 184°2	178.4 183.2	177°7 184°2	177°9
1	27 28	182.6 191.2	188.0	185.4	184.2	182.6	182.8	183.1	186.1	188.1	188.6	189.2	190'0
	29	188 4 175 6	190.4 174.9	190.6 183.5	189 . 9	188.7 187.3	188.0 188.1	188°0	188.7 190.8	188.7 190.8	190.8	196.3	197.6 197.7
Hourly	30 Means	189.81	189.55	188.74	188.12	187.33	186.87	186.80	187.55	189.07	189.33	190.85	190.5
			!		TEMPERAT	TURE OF TI	HE VERTIC	AL FORCE N	AGNET.	<u> </u>			<u></u>
		4i°0	4i°0	4i°·2	42.0	43.2	44.0	44.2	45.0	45.2	45° . 5	45°5	45°4
	$\begin{bmatrix} 1 \\ 2 \end{bmatrix}$												51.2
	3 4	44.3	44.6	45.4	46.5	47.3	48.3	49 ° 3	49.6		50·8 —	51·1 —	_
	5	46.0	46.5	48'1	49.4	50.0 50.0	51.0 50.4	51.3	51.5	51.6	51.8 52.2	51.8 52.5	51.8 52.5
	6 7 ь	$\begin{array}{c} 48.6 \\ 52.2 \end{array}$	48.8 51.8	49.6 52.0	49.5 52.0	52.2	52.5	51.0 52.8	51.4 53.2	51·9 53·7	54.4	55.2	56.2
1	8	56'1	54.4	54.4	54.5	55.0	55.5	56.1	56.5	57.4	58.2	59.0	59.2
ł	9 10	52°3 51°9	53°2 52°3	53.6 53.6	53°5 54°2	54.0 54.4	54°0 54°0	54°1 54°5	53.6 54.4	53 ·8 5 4·6	54°5 54°4	54.8 54.2	55°C
	11			48.4	49.0	49.6	50.2	50.5	50. 3	51.0	<u>-</u> 51·4	52.6	52°3
	$\frac{12}{13}$	48.0 49.8	47.9 50.4	50.9	52.0	52.0	50.2	52°0	50 5 51.5	51 · 4	51.8	52.2	52.5
ان	14	51.1	51.6	52.5	53.2	53.1	53.1	53 °0	53.0	53.2	53.5	54.2	54.3
APRIL.	15	49.5 46.3	50°1 46°6	50°2 46°9	50°1 47°4	50°0 47°6	49 . 8 48 . 2	49.6 48.2	50.0 48.7	50°3 48°5	50.4 47.8	50.6 48.0	51.2 48.2
AP	16 17	48.6	48.6	49.0	48.6	48.6	49.0	49.2	49.3	49.2	48.8	48.4	47.7
	18 19 b	41.6	41.6	41.8	42.2	42.6	42.8	43.5	44.2	44.5	44.6	46.0	47:2
-	20 b	50.3	49.5	49.4	49.1	49.4	49.6	50.2	50.7	51.0	51.2 57.0	51.0 58.2	51.5 58.8
	21 b 22	52.4 61.7	52.4 61.7	61.0 63.0	53°2 60°6	53°2 60°4	$\begin{array}{c} 53.2 \\ 60.3 \end{array}$	54.5 60.0	54.2 60.0	55.6 60.0	59.6	59.6	59.2
- 1	23	53.5	5 3°5	52.8	52.4	52.3	53.0	53.6	54.0	54.2	54.2	55.2	54°8
	$\begin{bmatrix} 24 \\ 25 \end{bmatrix}$	50.2	50.8	51.2	51.7	52.5	<u></u> 53.0	53.3	53 ° 6	53.4	54.5	54.7	55°0
		52.2	52.2	52.2	52.2	53.1	54.0	54.7	55.7	56.2	57.1	57.5	58.0
	26	55.3	55.4 50.2	55°3	55°7 50°9	55.5 51.3	$55^{\circ}2$	54.7 52.2	54.5 52.2	54°5 52°1	54.6 52.2	54.7 52.0	54.5 52.0
	27	40.0											
	27 28 29	49°2 49°5	49.5	49.2	49.2	49.2	49°2	49.6	49.8	50.1	51.0	51.2	50.7
	$\begin{bmatrix} 27 \\ 28 \end{bmatrix}$				49°2 50°6	49°2 51°0	51.1	21.1	51.5	21.6	52.1	52.4	52.5

^{*} Four minutes late.

b Not included in the Means, on account of disturbance.

[°] Seven minutes late.

129. 139. 144. 159. 169. 179. 189. 199. 209. 211. 229. 23. Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintain Maintai		One Scale	Division=	•000065 par	rts of the V.		RTICAL F		orresponding	; to 1° decre	ase of Temp	perature, 1·6	4.
2000 2004 2007 2007 10972 19972 19973 19974 1970 1984 1945 19375 18971 19976 22911 20272 19911 1736 18370 18370 18370 18371 18371 18371 18371 18371 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18373 18	12 ^h .	13h.	14h.	15h.	16h.	17 ^h .	18h.	19 ^h .	20h.	21h.	22h.	23.	Daily and Monthly Means.
223*1 202*2 193*1 173*6 183*0 185*9 195*4 197*0 195*4 197*0 195*8 195*1 195*0 185*9 195*1 195*0 185*9 195*3 195*3 195*2 195*0 195*9 195*3 195*3 195*2 195*0 185*9 185*4 185*6 185*5 185*7 185*7 185*7 185*7 185*8 185*9 185*2 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*9 185*0 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*9 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*8 185*0 185*7 185*6 185*2 185*5 185*7 185*6 185*7 185*6 185*1 185*3 185*3 185*0 185*7 185*6 185*2 185*5 185*7 185*8 185*3 185*0 185*7 185*6 185*4 185*5 185*3 185*3 185*0 185*7 185*6 185*4 185*5 185*3 185*3 185*0 185*7 185*6 185*4 185*5 185*6 185*7 185*6 185*4 185*5 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6 185*6		Sc. Div.					Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
192'6 193'2 191'3 191'2 191'2 190'5 191'5 193'6 180'7 190'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7 193'7							198.4	197.0	198.4	194.2	195.7	189.1	199'46
192°G 193°2 191°3 191°2 191°2 190°5 191°5 191°5 193°G 193°G 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T 193°T	228.1	202.2	198.1	173.6	183.0	185.9	184.4	184.6	189.5	189.7	199.0		196.11
18973 18973 18979 18970 18970 18974 18874 18379 18572 18970 18673 1871 18976 18978 18974 20411 18070 18299 14870 14875 18171 1877 1877 1877 1877 1877 1877	192.6	193.2	191.3	191.2	191.2	190.5			193.6	193.7	193.7	193.7	192.17
291 S 207 4 2041 1800 — 132'9 148'0 145'5 110'1 124'7 166'0 168'3 186'2 184'3 181'0 184'8 184'9 184'8 184'0 184'8 186'2 184'3 181'0 184'8 184'8 184'0 185'8 186'2 184'3 181'0 184'8 185'3 186'8 186'2 184'3 181'0 184'8 185'3 186'8 186'8 186'2 184'3 186'2 184'3 186'2 184'3 186'2 184'3 186'2 184'3 186'2 184'3 186'2 184'3 186'2 184'3 186'8 186'2 184'3 186'2 184'3 186'2 184'3 186'2 184'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3 186'3				188.0		189.4			188.2				189.69
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## TEMPERATURE OF THE VERTICAL FORCE MAGNET. ## 46'2	194.9	192.2	193.9	188.6	179.1	189.2	179'9	185.2	189.0	193.0	193.0	195 3	188 52
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	91.24	190:37	189.43	187.79	188*28	188.81	189*46	189.16	188.18	188:29	188.76	189.99	188.93
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a Five minutes late.

e Eight minutes late.

	Or	ne Scale Div	ision = '00	0066 parts o	f the V.F.		CAL FOR n Scale Div		sponding to	1º decrease	of Tempera	ture, 1.64.	
Mean G gen Ti	öttin-}	O ^h •	1 ^h .	2 ^h •	3h.	4 ^h .	5 ^h •	6 ^h .	7h.	8 ^h .	9 ^h .	10 ^h .	11h.
ſ	1	Sc. Div. 194'8	Sc. Div. 191.7	Sc. Div. 191.8	Sc. Div. 188 5	Sc. Div. 187 4	Sc. Div. 188 8	sc. Div. 190°1	Sc. Div. 190.6	Sc. Div. 190°5	Sc. Div. 191 9	Sc. Div. 191 9	Sc. Div 191 9
	2 3 4 5 6 7 8	194.7 189.6 185.9 183.7 176.5 121.5	191'1 187'4 184'9 183'7 176'5 143'6	188.2 185.0 182.8 181.5 174.1 160.9	186'3 182'5 180'2 179'4 170'3 164'2	185 · 4 180 · 9 176 · 2 176 · 6 167 · 2 164 · 2	184.4 180.3 174.9 174.8 166.8 170.7	185°0 180°5 176°2 171°7 165°7 175°5	186.4 181.2 175.0 171.0 164.6 177.5	187.2 181.1 175.0 171.4 166.2 175.5	188 · 2 181 · 5 176 · 3 171 · 4 167 · 3 176 · 4	188.8 180.9 175.7 172.5 168.5 175.4	188.7 181.4 175.6 171.8 168.9 174.2
	9 10 11 12 13 14 15	178°4 171°0 168°3 167°1 169°2 167°9	175 · 8 171 · 7 167 · 5 166 · 3 169 · 2 161 · 1	175 · 8 172 · 2 165 · 7 163 · 5 168 · 0 163 · 8	173 · 4 171 · 3 162 · 6 162 · 1 166 · 1 160 · 9	168 '9 167 '5 162 '6 162 '1 164 '8 160 '1	169 '9 164 '8 162 '1 162 '6 164 '8 162 '3	170.5 163.9 161.9 163.9 163.9 164.7	172·1 164·8 161·1 165·3 165·4 165·9	166.5 164.5 161.0 b 166.5 168.2 169.5	166.5 165.5 162.1 165.9 166.3 168.2	170°3 164°6 163°4 164°9 165°6 166°0	170°2 166°5 163°3 164°0 166°9 162°8
N N	16 17 18 19 20 21 22	174.7 174.4 169.4 169.6 170.1 172.6	173°1 171°8 166°5 169°5 172°4 172°0	170.8 169.9 167.1 169.1 171.8 171.2	169°3 169°3 167°1 166°5 173°1 171°8	169 · 2 167 · 0 163 · 3 165 · 3 171 · 1 171 · 3	169 ° 4 168 ° 3 161 ° 7 163 ° 8 171 ° 1 167 ° 3	170°5 166°4 161°7 164°4 171°1 165°8	173 · 5 166 · 4 161 · 0 168 · 8 170 · 3 165 · 4	173.0 166.4 162.0 169.8 d 172.3 165.4	173 ° 0 164 ° 9 161 ° 7 171 ° 6 173 ° 4 166 ° 2	173°0 164°0 161°7 171°3 172°0 166°2	172.7 165.3 164.4 173.8 172.9 166.2
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lourly	Means	58.42	58.64	58.99	59.45	59.89	60.33	60.57	60.85	61.11	61.49	61.75	61.8

^a Omitted in the Means, on account of disturbance.

b Seven minutes late.

	One Scale	Division =	*000066 pa	rts of the V		RTICAL E se, in Scale		orresponding	g to 1° decre	ease of Tem	perature, 1°6	34.
12h.	13 ^h .	14 ^h .	15 ^h .	16 ^h •	17h.	18h.	19 ^h .	20 ^h .	21h.	22h•	23h.	Daily ar Monthl Means
Sc. Div.	Sc. Div. 193 ° 0	Sc. Div.	Sc. Div. 189'0	Sc. Div. 189'1	Sc. Div. 188'9	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
193.1	190 0	131 0	103 0	109 1	100 9	194.3	194.7	194.7	193.4	193.4	193.2}	191.58
189.0	189.4	187.2	187.0	186.2	185.9	186.8	187.0	187.0	187.3	189.6	189.6	187.78
	181.4	182.0	182.2	182.2	182.5	183.5	184.0	182.8	183.8	185.4	186.0	182.9
181.4										178.6	183.7	178.1
175°6	175'9	176.7	177.9	177.9	178.1	178.1	177.8	178.6	178.5			
171.8	171.8	173.5	173.8	172.6	173.7	173.7	171.9	170.1	168.0	172.6	176.5	174.1
170.0	174.4	183.8	175.6	171.9	176.9	123.5		46.2	46'1	118.6	110.6	153.4
174°2	174.2	174.3	173.7	175.0	175.3				_	_	176.4}	169.0
						174.3	174.3	167.8	167.1	171.6	176.4	
170.2	170.2	169.0	170°2	170.2	170.3	170.3	166.9	170.3	171.3	171.3	171.7	170.8
166.8	166.8	166.8	167.2	167.2	167.8	167.8	167.4	167.8	169.0	162.5	168.4	167.2
163.3	164.6	163.8	163.6	162.2	164.0	164.7	164.2 c	165.8	165.2	166.5	166.5	164.0
163.0	162.4	167.5	163.7	163.7	163.7	165.1	165.1	168.1	168.4	168.9	168.6	165.1
164.9	165.2	165.1	165.7	165.7	165.7	165.7	168.8	169.3	169.3	161.2	158.5	165.9
	170.4	168.6	169.7		170.9	(1	105 0	100 0		1 1	
162.8	1104	100 0	109 /	170.0	110 8	168.8	171.1	171 1	172.2	173.1	$ \frac{174\cdot 4}{174\cdot 4}$	167.3
175.0	175.0	170.0	17010	170.4	170.0		171.1					171.5
175.0	175.0	170.0	176'0	170.4	173.6	168.8	173.4	163.7	163.1	170.5	176.1	
166.5	165.3	164.9	166'3	151.7	158.7	163.1	166'9	158.5	159.5	165.3	166.2	165.3
166.9	165.8	165.5	162.3	163.9	165.5	168.0	166.3	163.3	164.4	165.0	164.7	164.5
168.7	168.3	167 .2	165.1	166.8	165.4	161.0	162.5	167.6	168'4	169.3	168.6	167.6
172.2	172.6	171.5	173.1	173.1	172.2	169.5	171.2	171.2	170.9	172.2	173.2	171.8
166.2	166.3	163.7	166.7	166.3	166.4) i	167.5
						164.9	166.6	166.9	168.5	168.1	$ \frac{168.7}{168.7}$	107 5
167.1	167.1	167.1	166.6	166.8	168.3	168.6	168.2	168.7	171.6	171.6	172.9	168.3
166.7	169.0	168.7	168.7	168.7	168.4	169.4	170.8	172.0	172.4	173.4	174.9	168.1
									175.6	178 9	180.7	174.4
175.3	174.0	173.9	174.6	175.0	175.7	175.7	175.9	175.6				
178.1	174.8	174'8	174.9	174.8	161.0	164.2	173.4	174.9	171.4	170.0	167.6	172.6
170'4	164.6	162.3	161.8	150.2	161.1	159.7	141.2	98.8	130.0	132.0	151.8	159.6
164.1	164'1	164.2	164.9	164.7 °	164.7					150.0	$ \frac{1}{174 \cdot 4} \} $	165.9
- 181°5	179°1	178.8	181.0		178.5	173°9 177°7	171°4 177°7	171.7 179.0	172°6 178°7	172°6 179°0	174.4)	177.3
171.76	171.85	171.40	171.76	170.84	170.86	171.45	172.33	172'12	172.33	173.01	174.10	171.7
				TEMPER	ATURE OF	THE VERT	ICAL FORC	E MAGNET.				
52°·3	52°0	51°8	51°6	5 Î · 4	5η2	-	<u> </u>	<u> </u>	<u> </u>	0	$\left \begin{array}{c} \stackrel{\circ}{\underset{47\cdot7}{\cdot}} \end{array}\right\}$	50.2
-						47.2	47.4	47.4	47.5	47.6		(
53.0	53.0	5 3°1	53.2	53.1	52.5	52.3	52 ·2	51.6	51.2	50.8	50.2	51.2
55.9	55.6	55.4	55.2	54.8	54.4	54.0	53.8	53.2	53.7	53'1	52.8	54.2
58.6	58.4	58.0	57.8	57.3	57.0	56.8	56.8	56.8	56.3	56.2	54.6	56.6
60.6	60.4	60.0	60.5	60.0	60.0	59.8	59.8	59.0	58.2	57.8	57.2	58.6
62.6	62.0	62.5	61.1	60.9	61.3	61.3		61.7	61.6	61.0	61.3	61.0
61.7	61.2	61.3	60.8	60.2	60.4		_	1	—		- 1	l
	01.0	01.0	000		00 4	59.4	59.1	59.0	59.0	59.0	59.0	60.2
62.2	60.0	62.1	62.7	62.7	61:0				61.2	61.2	61.2	61.2
63.8	62.3				61.9	61.7	61.6	61.6			62.5	62.9
	63.8	63.6	63.5	63.5	63.3	63.0	63.2	63.4	63.8	63.9		
65.2	65.5	65.3	65.1	65.6	65.4	64.8	64.3	64.3	64.3	64.1	63.4	64.8
65.3	65.4	65.4	65.5	65'1	64.3	63.5	63.1	62.5	61.9	61.5	61.1	64.2
64'3	64°3	63.7	63.2	63.3	62.9	62.5	61.8	61.4	60.6	60.2	60.0	62.8
65'9	65.7	65.2	65.1	64.7	64.2		-				60.3	62.9
						62.4	61.7	61.3	60.7	60.5		
64.4	64.0	63.7	63.6	63.4	63.0	62.5	62.3	62.0	61.5	61.0	60.5	62.5
65.4	65.9	65.4	65.2	65.0	65.2	64.8	63.7	62.9	62.5	62.3	61.8	63.4
65.6	65.2	65.2	65.3	64.2	64.1	63.7	63.2	62.7	62.4	61.8	61.2	63.7
63.7	63.2	63.3	63.1	62.7	62.2	62.5	62.0	61.3	60.8	60.6	60.0	62.4
61.7									60.4	60.0	60.0	60.4
63.8	61.6	61.2	61.4	61.3	60.7	60.6	60.6	60'4	00 4			
ס טיט	63.8	63.6	63.7	63 °5	63.2		<u> </u>		60.0	60:0	$\{61.5\}$	62.4
60	-					62.3	62.3	62.0	62.2	62.0	01 9 1	
62.5	62.6	62.7	62.5	62.5	62.2	62.0	61.7	61.5	61'1	60.7	60.3	61.6
64.6	64.4	64.7	64.0	63.5	63.1	62.2	61.2	60.4	59.5	59.2	58.4	62.4
59.3	59.3	59.2	59.0	58.6	58.2	58.0	57.7	57.2	56.6	56.3	55.7	58.4
61.1	61.1	60.8	61.0	60.7	60.0	60.0	59.5	59.0	59.0	59.0	58.4	59.4
	64.2	66.2	66.2	66.7	66.7	66.7	66.7	66.3	65.7	65.5	64'9	63.2
	64.9	64.2	64.0	63.8	64.2						58.5}	
		~~ •		50 0	01.44	20.0	00.0	59.8		59.2	1 50.5	63.2
64.2 65.0	01 9	!		-		60.3	1 60 0 1	1 114 7	39 h	119 /	1 00 011	
	56.2	56 ° 0	55.2	55.0	54.7	60°3 54°6	55.3 60.0	55°4	59°6 55°4	55°4	55.2	56.4

d Five minutes late.

^{*} Four minutes late.

	Or	ne Scale Div	ision = '00	0066 parts o	of the V.F.		CAL FOR		sponding to	1° decrease	of Tempera	ture , 1 ⁶⁴ .	
Mean (gen T	Göttin- }	Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .	10 ^h .	11h.
	1 2 3 4 5 6	Sc. Div. 178 4 164 8 165 3 168 8 173 0	Sc. Div. 177'4 167'2 166'9 167'7 172'4	Sc. Div. 175 ° 6 169 ° 2 167 ° 0 166 ° 6 171 ° 8	Sc. Div. 174°0 169°5 165°9 166°6 171°8	Sc. Div. 171 ° 6 168 ° 6 164 ° 8 166 ° 3 172 ° 4	Sc. Div. 171 ° 6 166 ° 0 166 ° 0 165 ° 0 171 ° 1	sc. Div. 174'8 164'4 164'4 165'0 168'9	Sc. Div. 172°5 165°0 163°3 165°0 168°6	Sc. Div. 172°8 166°4 163°1 166°1 170°3	Sc. Div. 175°2 168°3 164°3 166°2 169°4	Sc. Div. 177 '7 166 '2 165 '7 166 '2 167 '7	Sc. Div. 178*4 165*8 167*9 166*3 166*6
	7 8 9 10 11 12 13	168 '7 169 '8 166 '6 157 '6 163 '3 168 '6	166 ' 4 168 ' 1 166 ' 1 154 ' 9 161 ' 6 168 ' 6	164.8 167.0 165.8 157.3 160.9 166.8	163°1 167°9 164°0 157°3 157°1 165°2	161.0 167.2 163.4 154.9 154.8 166.4	159.6 168.3 163.1 155.7 157.0 166.5	164.2 167.8 162.8 157.8 160.4 164.7	160°5 167°1 162°8 162°6 160°4 166°7	161.8 166.3 161.9 162.6 163.1 167.8	160°3 166°8 165°4 162°2 163°5 166°1	161'1 167'0 158'4 161'1 169'0 168'0	160°1 167°0 155°0 163°8 166°7 170°8
JUNE.	14 15 16 17 18 19	170°3 182°8 172°1 169°1 170°0 166°2	166.8 182.9 172.2 169.5 169.3 165.4	168.6 183.1 171.0 167.1 167.8 165.2	170.4 182.0 170.8 163.3 165.5 165.0	173.0 179.6 169.6 162.8 163.0 164.8	172.4 179.8 a 167.6 164.2 160.9 162.5	180.7 179.8 166.3 165.0 159.9 161.0	184.4 178.7 165.4 167.0 161.0 160.7	189°1 175°0 165°2 165°7 163°1 162°2	189.7 176.4 166.1 166.0 163.1 163.9	192.3 174.7 169.7 165.4 165.2 163.3	185.4 173.2 169.6 164.1 165.0 162.3
	20 21 22 23 24 25 26 27	163°1 163°0 161°8 158°9 156°4 151°8	162.5 162.5 161.3 158.3 155.2 151.6	161.4 162.5 159.4 156.3 155.8 148.6	163°9 161°8 158°1 155°6 155°6 148°6	157.8 161.8 157.4 154.9 151.8 147.5	155.8 159.5 ° 154.8 152.3 150.4 145.8	155°8 158°2 154°8 151°8 150°0 145°1	155.8 156.3 154.8 150.3 150.0 144.8	157.0 157.5 155.5 149.6 150.4 144.2	157.8 159.1 155.8 150.5 150.4 145.6	158°4 159°4 155°3 150°2 149°5 146°0	159.5 159.8 154.3 149.6 147.8 145.5
	28 29 30	149'9 152'8 154'4	149 '9 152 '8 154 '4	151°2 152°5 152°2	148°3 152°8 150°4	147.4 153.0 149.5	147.4 151.8 147.5	147.4 150.6 147.1	148'1 148'9 148'8	146.7 146.0 148.8	145°8 146°8 149°7	147.0 149.0 152.1	148.9 149.5 151.8
Hourly	Means	164.90	164.30	163.67	162.87	161.74	160.87	161.10	161.13	161.47	162.09	162.52	162.10
		0	0	1	EMPERATI	1			1			0	
	$egin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{bmatrix}$	55.3 59.2 60.0 61.3 58.4	55.3 59.2 61.0 61.0 58.4	55.3 59.2 61.4 61.6 58.2	56.0 59.5 61.3 61.6 58.6	56.5 60.1 61.3 62.3 59.1	56.5 61.0 61.6 63.0 59.2	57.4 61.4 62.1 62.6 59.4	59°0 61°6 62°5 62°7 60°2	59.6 61.5 62.8 62.6 60.2	59.8 61.8 63.5 63.1 60.8	60°2 62°3 63°6 63°1 61°4	60.0 63.6 63.1 61.4
	7 8 9 10 11 12	60.0 62.3 61.5 66.6 64.3 60.5	60.0 62.3 61.5 66.6 64.5 60.5	60°4 62°2 61°6 66°6 64°8 61°0	61.0 62.1 62.3 66.6 65.0 61.1	61.7 62.1 62.5 66.6 65.5 61.1	62.5 62.3 63.7 66.6 66.0 61.7	63.0 62.5 64.3 66.7 66.0 61.7	63.5 62.6 64.7 66.5 65.9 62.0	63.7 62.7 65.6 66.6 65.9 62.3	64.7 63.3 66.6 66.7 65.7 62.6	65.5 63.5 67.5 66.7 65.7 63.3	65.9 63.5 68.5 66.7 65.5 63.6
JUNE.	13 14 15 16 17 18 19	59.0 53.3 59.0 59.2 59.0 61.8	59.3 53.3 58.7 59.2 59.3 62.0	59·2 53·8 59·1 59·3 60·0 61·7	59.0 53.8 59.5 60.0 60.2 61.7	58.8 53.8 60.0 60.4 61.5 61.8	58.8 54.2 60.4 60.5 62.1 62.4	58.0 54.5 60.6 60.6 63.4 62.5	57.6 54.7 60.5 61.0 63.3 62.8	57.2 55.5 60.6 61.3 63.5 63.2	57.1 56.7 61.0 61.9 64.0 63.3	57.0 57.7 61.4 62.5 64.2 63.5	56'9 58'6 61'2 63'3 64'2 63'7
	20 21 22 23 24 25 26 27	62.4 62.6 63.0 65.5 65.8 68.5	62.5 62.5 63.5 65.7 66.4 68.2	62.7 62.1 63.9 66.3 66.6 69.7	63.4 62.7 64.8 66.6 66.9 70.4	64.2 63.2 65.7 67.5 67.4 71.0	64.5 63.5 66.3 68.2 68.0 71.5	64.6 63.7 66.5 68.5 68.5 72.0	64.9 64.4 66.5 68.7 69.3 72.4	65.2 64.7 66.8 69.3 69.7 72.5	65°3 65°5 67°3 70°6 70°6 73°0	65.5 65.5 68.3 70.3 71.2 73.5	65.5 65.7 68.5 70.4 71.5 73.7
	28 29 30	70°5 67°6 67°0	70°1 67°4 67°0	69.7 67.5 67.5	69.7 67.8 68.0	70°3 68°3 68°9	70°4 68°7 69°5	70.5 69.3 69.7	70.5 69.8 70.2	71·2 70·1 70·5	71.6 70.7 70.7	72.0 70.7 71.3	72:3 70:9 71:1
Hourly	Means	62.06	62.13	62.36	62.68	63°14	63.28	. 63*85	64.12	64.43	64.90	65.28	65.4

a Nine minutes late.

b Three minutes late.

	One Scale	Division = '	'000066 par	ts of the V.		RTICAL FO		rresponding	to 1º decrea	ase of Temp	erature, 1·6	1 .
12h.	13h.	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily an Monthl Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 167.7	Sc. Div.
182.6	175.8	174.6	171.7	169.6	170.4	170.4	170.2	170.2	170.4	170.4		173.50
165.8	165.1	165.8	165.6	165.6	166.2	166.2	165.6	164.3	160.3	161.7	163.4	165.71
167.9	167.3	165.7	165.0	167.3	167.3	166.6	162.0	164.1	164.5	167.8	168.9	165.79
166.3	166.3	166.3	167.8	167.8	168.6	167.5	168.9	170.4	171.8	173.1	173.1	167.68
166.2	166.4	166.6	166.0	166.9	167.7						— 1	168.7
						164.7	164.1	168.1	169.0	168.7	$\frac{-}{170.7}\}$	100 /
159.8	160.5	161.4	169.1	169.2	161.2	161.2	158.8	154.4	159.0	166.2	169.1	162.56
166.7	167.0	164.1	164.5	166.0	166.0	166.6	166.7	165.3	164.8	162.5	165.0	166.48
156.7	154'9	154.9	155.5	155.9	155.9	153.3	155.5	155.2	155.3	157.6	157.6	159.33
167.1	166.0	168.9	163.1	161.8	158.7	159.5	156.9	154.8	155.8	157.5	161.2	159.97
										164.5	168.6	164.40
166.7	167.3	171.7	167.9	166.7	166.4	166.4	166.9	167.1	167.7	104 9	11	104 40
173.1	173.3	181.9	170.0	180.9	167.7		1 (0.40		10010	172.1	$\left\{ \frac{1}{172}, \frac{1}{3} \right\}$	167.58
						149.3	148.3	157.2	169.0			
182.6	182.6	178.5	180.2	179.0	177.7	171.8	177.5	177.9	177.5	174.6	180.4	178 4
172.3	172.3	169.2	170.0	169.3	170.8	171.8	172.8	172.8	172.8	174.7	176.3	$175^{\circ}5$
169.6	168.6	168.9	168.6	168.0	165.9	167.7	169.4	166.6 р	166*2	170.5	170.5	168.59
164.5	164.2	162.8	163.6	163.6	159.4	163.8	164.9	165.0	165.0	169.3	169.2	165.2
165.8	164.4	164.6	162.0	162.1	161.2	161.2	162.8	162.8	164.2	165.4	165.6	164.0
162.5	161.3	161.3	161.3	163.6	163.6				_			
						164.5	164.7	164.3	164.3	166.6	$\frac{-}{167\cdot 1}$	163.6
159.9	159.9	158.0	156.2	159.2	159.7	158.2	159.4	161.3	160.7	162.9	162.9	159.4
160.5	160.5	158.2	158.2	158.2	158.2	158.5	158.7	158.7	159.0	161.7	163.1	159.8
										155·5	157.1	
153.1	153.1	153.1	148.6	148.6	151.0	152.2	153.2	154.4	155.1			154.9
149.6	148.9	148.9	148.9	149.9	151'1	151.9	151.6	152.4	154.2 g	155.7	156.4	152.4
147.8	148.1	149.0	149.5	149.6	150.2	150.6	151.3	152.6	152.6	152.2	152.0	151'2
145.7	145'1	144.6	144'6	144.2	144.5						146.6	146'1
_	_		<u> </u>		<u> </u>	144.5	144.5	145.5	146.6	146.6		
148.8	148.4	148.9	149.7	147.8	148.6	145.3	146.0	146.2	146 ·2	153.3	153.2	148.3
149.5	148.6	148.6	149'2	149.2	149.7	149.5	147.9	151.3	143.1	147.6	155.1	149.8
151.8	152.5	152.5	151'5	147.3	145.3	147.5	148°0d	152.7	154.7	156.9	158.7	151.0
162.41	161.86	161.88	161.10	161.45	160.21	159.65	159.87	160.61	161.16	162.91	164.31	161.9
				ТЕМРЕ	RATURE O	F THE VER	TICAL FOR	CE MAGNE	<u>. </u>	l	(
. 0					1						0	. 0
6 0. 1	60°2	60°2	60°3	60°3	60°0	60°0	60°0	60°.0	59°6	59°4	59°2	58.7
63.2	63.2	63.2	62.8	62.7	62.2	62.3	61.6	61.5	61.3	60.7	60.2	61.4
63.4	63.0	62.8	63.0	62.6	62.5	62.4	62.0	62.0	62.0	61.7	61.3	62.2
62.7	62.5	62.1	61.7	61.2	61.0	61.0	60.0	59.6	59.3	58.8	58.2	61.5
61.8	61.8	61.8	61.6	61.4	61.0							
		_			_	60.4	60.7	60.6	60.4	60.3	60.0}	60.3
65.7	65.5	65.4	64.8	64.4	63.9	63.7	63.2	63.2	63.2	63.0	62.6	63.3
63.2	63.1	63.1	63.0	62.8	62.5	62.4	62.4	62.8	62.4	62.0	61.2	62.6
68.2	68.2	68.7	68.2	68.2	68.3	68.0	67.9	67.7	67.5	67.4	67.2	66.1
67.2				66.0	65.5	65.2	65.0	64.9	64.7	64.6	$\frac{67.2}{64.5}$	66.1
65.3	67.0	66.6	66.2		62.3	61.7		60.6	60.4	60.1	60.0	63.7
63.9	64.3	63.7	63.4	62.7	63.0	01 (61.0	00 0	UU 4	ł		
00 g	64.2	64.0	63.6	63.3	00.0	50.5	50.5	50:0	<u></u>	59.2	59.0}	61.6
57.0				<u>-</u>		59.5	59.5	59.0	59.0			
57.2	57.0	56.5	56.7	56.2	56.1	56.0	55.4	55.6	55.6	55.4	54.2	57.0
59.1	59.2	60.0	60.5	59.7	59.0	59.0	58.5	58.4	58.0	57.8	57.4	56.9
61.4	61.2	61.0	60.6	60.4	60.4	60.0	59.8	59.2	58.5	58.2	57.4	60.0
63.5	63.2	63.2	63.3	62.7	62.5	61.8	61'4	60.7	60.2	59.8	59.0	61.3
64.0	63.7	63.2	63.2	63.2	63.0	63.0	63.0	6 3.0	62.6	62.5	62.4	62.5
63.9	64.1	64.0	64.4	63.2	63.2				}	_	- 1	i
					_	61.7	61.7	61.6	61.3	61.2	$\frac{-}{60.8}$	62.5
65.5	65.5	65.5	65.7	65.5	65.3	65.3	64.5	64.1	63.6	63.4	62.8	64.4
65.8	65.6	66.0	65.6	65.2	65.2	64.7	64.3	64.0	63.8	63.6	63.2	64.3
68.7	68.6	68.6	70.0	70.0	69.4	68.5	68.0	67.3	67.0	66.7	66.1	67.0
70.4	70.6	70.5	70.5	69.7	69.3	68.5	68.1	67.8	67.3	66.7	66.3	68.4
71.5												
73.6	71.4	70.7	70.3	69.8	69.6	69.3	68.7	68.6	68.5	68.2	68.3	69.0
	73.3	73.2	73.1	72.7	72.6		70	70	70.0	71.0	$\{71.0\}$	71.9
72.3						72.7	72.7	72.5	72.0	71.6		
	72.5	71.7	71.4	70.8	70.5	70.1	69.6	69.1	68.7	68'4	68.4	70.5
	71.0	70.6	70.1	69.9	69.6	69.0	68.3	67.5	67.0	67.0	66.7	69.0
70.9						20.00	00.4	0× • ×	07.0	00.5	00.0	00.11
	71.3	71.0	70.5	70.0	69.5	69.0	68.4	67.7	67.2	66.7	66.0	69.1,

^e Seven minutes late.

⁴ Five minutes late.

	One	Scale Divi	sion = .000	0066 parts o	f the V.F.		CAL FOR Scale Divis		ponding to	l° decrease	of Temperat	ture, 1 64.	
Mean Götti gen Time.	n-}	Oh.	1h.	2 ^h •	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7հ․	8 ^h .	9 ^h .	10 ^h .	11h.
	1 1 2 1 3 1	Sc. Div. 57°5 52°8 49°8	Sc. Div. 157°5 152°3 149°2	Sc. Div. 154.5 151.5 148.6	Sc. Div. 151'9 149'0 148'0	Sc. Div. 150°5 146°3 142°5	Sc. Div. 150°4 144°2 138°8	Sc. Div. 149'5 142'9 138'3	Sc. Div. 146 3 140 9 138 3	Sc. Div. 147°5 138°9 138°7	Sc. Div. 146 8 138 9 138 7	Sc. Div. 147.6 140.5 138.2	Sc. Div 147 7 141 8 139 5
10	6 1 7 1 8 1 9 a 1	45 · 4 42 · 5 34 · 4 39 · 7 39 · 9 43 · 0	146'1 143'5 138'3 138'6 139'1 143'0	144.0 144.5 138.3 137.6 138.6 139.9	144.0 143.9 138.7 137.6 135.2 139.9	140.6 143.9 139.8 135.0 132.1 139.2	139.6 143.2 139.6 133.0 130.7 137.0	137.0 142.2 137.1 133.3 132.6 139.1	138.5 141.6 137.1 131.6 136.2 138.9	138 · 1 141 · 9 140 · 0 133 · 7 138 · 5 143 · 6	137.0 141.9 140.0 134.5 144.7 143.6	136.2 142.3 138.3 135.3 155.4 143.6	136 ° 6 142 ° 3 136 ° 9 135 ° 3 161 ° 0 141 ° 1
11. 12. 12. 12. 12. 12. 12. 12. 12. 12.	2 I 3 1 4 I 5 I 6 I	39 3 38 4 40 3 53 4 148 6 139 4	138 ' 5 138 ' 4 140 ' 3 151 ' 8 147 ' 4 136 ' 3	140°1 139°2 142°9 151°1 145°5 135°6	136.7 138.4 143.2 150.1 143.1 138.3	135 · 8 133 · 8 141 · 1 149 · 2 141 · 0 136 · 5	134.5 132.9 141.6 147.3 139.8 135.2	136'9 132'0 142'7 147'0 139'1 134'2	136'9 131'3 142'7 146'0 136'7 133'4	139.9 130.6 144.5 145.1 137.6 134.1	138 · 9 131 · 4 145 · 5 145 · 2 137 · 6 135 · 5	137.7 134.1 145.2 144.6 138.5 140.1	137 '8 135 '7 148 '4 145 '7 137 '0 142 '7
19 20 21 22 23 24	9 1 1 1 2 1 3 1	136°7 131°3 138°3 133°5 143°6	134'9 131'6 138'3 135'3 142'9 148'7	135°3 131°3 138°3 134°8 142°9 147°4	133°5 132°4 138°3 136°4 142°1 145°8	129.0 132.4 135.8 138.7 142.1 145.3	128 · 2 132 · 2 134 · 8 137 · 8 142 · 1 146 · 3	125 ° 9 131 ° 7 134 ° 8 135 ° 9 139 ° 6 146 ° 3	124.9 131.7 133.7 134.2 140.6 145.5	127 '9 132 '5 134 '9 135 '1 140 '8 146 '3	127'9 135'1 134'9 134'7 144'1 147'6	127.5 135.1 134.6 135.6 144.2 147.6	129'1 135'7 135'0 136'5 146'3
20 20 21 22 22 3 3 3 Aug.	6 1 7 8 8 9 0 1	145.6 160.9 162.2 160.0 155.4 158.6	148 2 159 0 160 5 158 3 154 7 156 6	150°2 159°6 160°5 156°1 154°7 154°8	150°3 158°0 159°0 154°6 154°7 153°4	151.0 156.8 156.4 153.5 154.9 153.4	151°9 155°4 153°1 153°5 154°9 153°2	153.6 154.1 152.6 151.5 154.9 150.3	154 · 1 154 · 4 152 · 9 152 · 6 154 · 8 151 · 2	159 ° 0 155 ° 7 155 ° 2 153 ° 1 153 ° 8 151 ° 5	158°1 157°4 154°9 153°1 155°4 153°2	159.6 155.5 154.9 152.2 155.1 151.8	160°5 157°5 154°9 152°2 155°0 151°8
Hourly Me	-	146.13	145.78	145.35	144.67	143.25	142.33	141.63	141'18	142.31	142.77	142.92	143.4
							HE VERTIC						
(:	1 2 3	66.4 68.1 69.6	66.4 68.4 69.7	66.7 68.5 70.5	$67.3 \\ 69.5 \\ 71.3$	$\begin{array}{c c} 67.6 \\ 70.6 \\ 72.3 \end{array}$	$ \begin{array}{c c} 68.7 \\ 71.5 \\ 73.3 \end{array} $	69.6 72.3 73.7	$70.0 \\ 72.7 \\ 74.8$	70°5 73°4 75°3	71°3 74°0 75°9	71°5 74°5 76° 5	72°2 74°7 76°7
10		71.5 72.7 71.8 73.3 74.5 76.7	71.5 72.5 71.8 73.3 74.5 75.3	72.0 72.5 71.6 73.6 75.0 75.4	72·3 72·5 72·3 74·0 75·8 75·4	73·5 72·5 73·3 75·6 76·8 75·5	74·3 72·8 74·0 76·7 77·5 76·3	74.8 73.0 74.6 77.4 78.1 76.5	75.4 74.0 75.4 78.0 78.5 77.0	76.2 74.6 75.7 78.0 78.7 77.5	77·4 75·2 76·5 77·5 79·3 78·2	77.0 75.4 77.0 78.0 79.0 78.6	76.7 75.5 77.5 78.3 78.5 78.1
JULY.	2 3 4 5 6 7	75.5 75.8 72.0 68.5 70.9 73.8	75.7 76.3 71.9 68.5 71.1 74.2	76.3 76.5 72.0 68.5 71.3 74.0	77·1 77·0 72·4 69·3 72·0 74·3	77.2 77.8 72.7 69.5 73.0 75.4	77.5 78.4 73.2 70.3 73.7 76.5	77·1 78·9 73·3 70·7 74·5 77·3	77.3 79.7 73.2 71.5 75.4 79.0	77.7 80.0 73.4 72.0 75.6 79.0	78.5 79.6 73.4 73.1 75.5 79.0	79.0 79.5 73.2 73.5 76.6 79.0	79°0 79°3 73°6 73°5 76°5 78°6
1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	9 0 1 2 3 4	76.5 77.0 76.2 76.7 72.3 69.5	77.0 77.6 76.0 76.5 72.5 69.3	77.0 77.9 76.0 76.5 72.6 70.0	78.0 78.3 76.0 76.2 72.9 70.2	78·3 78·0 76·3 76·3 72·9 70·5	79.2 78.4 76.5 76.5 73.1 70.8	80.0 78.4 77.0 76.7 73.0 71.0	80°3 78°2 77°3 77°2 73°1 71°0	80.6 78.4 77.5 77.3 73.0 71.1	81.5 78.5 78.3 77.4 73.3 71.5	81.5 78.5 78.4 77.7 73.4 71.5	82:3 78:6 78:4 77:5 73:5 71:5
2 2 2 2 2 2 2 3 3	6 7 8 9 0 1	71.0 63.5 63.3 64.5 66.4 64.6	70°4 63°9 63°4 65°3 66°5 65°1	69.7 64.1 63.8 65.9 66.5 65.3	69.5 65.5 64.4 66.4 66.0 65.9	68.7 66.0 65.5 66.7 66.4 67.0	68°5 66°5 65°7 67°4 66°3 67°3	68·3 66·7 66·3 67·7 66·5 67·5	68.0 66.7 66.5 68.3 66.5 67.9	68°2 66°7 66°8 68°5 66°6 68°0	68°2 66°5 67°4 68°6 67°0 68°5	68°3 66°7 67°7 69°2 67°5 68°5	68:3 66:5 67:6 69:3 67:7 68:5
\mathbf{A} ug.					\ —		. —	,	,				

[•] Omitted in the Means, on account of disturbance.

					VE	RTICAL 1	FORCE.		· · · · · · · · · · · · · · · · · · ·		 	
	One Scale	Division =	000066 par	ts of the V.	F. Increas	e, in Scale I	Divisions, co	rresponding	to 1° decrea	ase of Temp	erature, 1·64	1.
12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18 ^h •	19 ^h .	20h.	21h.	22 ^h .	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
147.2	146 6	146.6	146.9	147.0	147'1	148.0	149.7	150.8	151.6	152.8	152°8 148°7	149.78
141.8	142.3	141.7	142.0	142.7	143.6	144.1	144.3	144'3	144.2	146.4	140 /	144.43
138.0	137.7	138.2	139'3	140.0	135.0				142:0	143.2	144.0	141.60
_						144.0	144'1	144'1	143.2	138.8	140.5	139.10
137.5	138.2	138.2	138.2	138.2	140.3	140.3	140.3	133.9	130.2	140.7	132.4	141.81
142.4	142.6	140.4	140.8	141.4	140.8	141.5	141'8	142.6	142'4	140.0	140.1	137.96
136.9	135.0	135'9	138.3	135.4	136.5	138.3	137.3	138.8	140.0	138.3	139.9	135.68
135.6	135.6	132.9	132.6	134.5	135.9	136.4	136.5	136.2	136.2	134.0	143.0	137.68
163.5	165.4	161.0	98.3	139.4	122.4	137.0	80.2	132.6	143'2	104 0		
140.9	141.2	133.7	134.5	134.3	134.3	106:0	122.0	128.0	130.5	133.0	138.7	137.94
				10514	70014	136.9	133.2	131.9	135.2	140.7	139.1	136.14
137.8	137.9	133.0	134.7	135.4	136.4	127.8	$124.2 \\ 137.2$	138.2	140.7	141.2	141.4	136.18
135.7	135.7	134.9	137.2	137.7	135.7	136.5		143.8	145.6	152.0	153.4	145.14
147.9	146.8	147.2	148.9	146.4	146.4	142.8	143.8	145.7	146.3	147.5	148.6	147.01
144.9	145.4	145.4	145.4	145.6	145.6	145.6	145.7		137.5	138.3	137.4	139.38
137.1	138.0	137.3	137.3	136.9	138.1	137.5	138.2	139.3	101 0		- 1	
144'1	145°1	143.2	138.0	136.1	136.1	10410	194.0	134.9	135.9	136.7	137.6	137.42
	_	_	1001	10010	1000	134.2	134.9	131.3	131.6	131.3	131.3	129.90
129.1	126.7	127.7	128.6	129.0	129.4	130.0	130.8	134.2	134.4	135.2	137.1	133.70
135.7	135.0	133.7	134.4	133.2	134.8	133.9	134.2	134 2	132.6	134.8	135.6	133.40
134.2	134.4	134.4	133.3	132.5	133.7	120.9	128.1		142.9	143.7	145.2	136.10
136.2	136.7	137.4	137.4	132.5	119.2	134.3	136.9	135.2		148.1	150.1	144.34
145'1	143.9	143.9	144'1	145.1	147.3	145.7	145.7	145.7	148.1	140 1	100 1	
146.7	146.7	146.7	146.7	145.5	140.2	7.40.7	1.40:0	142.5	142.5	144.3	144.5	145.65
		<u> </u>				142.7	143.0	155.3	159.9	158.3	158.8	154.97
157'1	156.6	155.1	155.6	155.0	155.4	154.8	155.3	154.3	157.4	159.2	162.2	156.77
156.9	155.6	155.6	155.5	155.6	156.4	156.6	152.8	155.7	153.8	158.2	159.8	155.92
155.0	155.0	155.0	154.0	154.2	154.2	154.1	155.7	150.4	151.6	151.3	153.1	152.55
151.4	151.1	150.8	151.5	150.6	148.3	150.1	150.4	1	155.0	155.9	156.2	154.37
154.3	153.3	152.5	154'1	153.2	149.7	153.6	153.6	154.8	155 0	100 0	100 2	1
151.3	151.3	151.3	151.8	149.7	151.1	152.6	152.9	154.8	154.6	154.8	156.5}	153.02
143.15	142.86	142.03	142.35	141.85	141.25	141.65	141.96	142.17	143.26	144.81	145.57	143.11
-10 12	-1-00											
	1			l	ATURE OF	THE VERT	CICAL FORCE	E MAGNET	·	<u>'</u>		
		1 . 0		TEMPER	ATURE OF					68.4	68.0	69.77
72°·5	72°5	72.2	7i°9	темрен 71°5	7 <u>1</u> °1	7ő·7	69°7	69.3	68.6	68.4 70.5	68.0	69.77 72.17
74.9	75.0	75.3	74.0	темрен 71°5 73°6	7 [°] 1 73 3					68.4 70.5	70.0	72.17
	72°.5 75°0 76°7			темрен 71°5	7 <u>1</u> °1	70°.7 72°8 —	69°7 72°1	69°3 71°5	68.6 70.9	70.5	70.0	
74·9 76·7	75°0 76°7	75°3 76°5	74.0 76.3	темрен 71°5 73°6 75°0	71°1 73°3 74°5	70°7 72°8 — 74°0	69.7 72.1 73.5	69°3 71°5 — 73°0	68.6 70.9 72.5	70.5	70.0	72°17 73°83
74·9 76·7 — 76·5	75°0 76°7 — 76°2	75·3 76·5 — 75·7	74.0 76.3 75.5	темрен 71°5 73°6 75°0 — 75°2	71°1 73°3 74°5 — 74°9	70°7 72°8 — 74°0 74°5	69.7 72.1 73.5 74.5	$\begin{array}{c c} 69.3 \\ 71.5 \\ \\ 73.0 \\ 74.5 \end{array}$	68.6 70.9 72.5 74.0	70.5 72.1 74.0	$\begin{bmatrix} 70.0 \\ -71.5 \\ 73.6 \end{bmatrix}$	72°17 73°83 74°65
74·9 76·7 — 76·5 75·4	75.0 76.7 — 76.2 75.2	75.3 76.5 — 75.7 74.9	74.0 76.3 — 75.5 75.3	71°5 73°6 75°0 75°2 74°7	71°1 73°3 74°5 — 74°9 74°5	70.7 72.8 74.0 74.5 74.5	69.7 72.1 73.5 74.5 74.2	69°3 71°5 73°0 74°5 73°8	68.6 70.9 - 72.5 74.0 72.8	70.5 	70.0 71.5 73.6 72.3	72.17 73.83 74.65 73.90
74.9 76.7 76.5 75.4 77.5	75.0 76.7 — 76.2 75.2 77.5	75.3 76.5 — 75.7 74.9 77.5	74.0 76.3 — 75.5 75.3 77.0	71°5 73°6 75°0	71°1 73°3 74°5 — 74°9 74°5 75°7	70.7 72.8 74.0 74.5 74.5 75.3	69.7 72.1 73.5 74.5 74.2 75.5	69°3 71°5 73°0 74°5 73°8 74°5	68.6 70.9 72.5 74.0 72.8 73.5	70.5 72.1 74.0 72.7 73.5	70.0 71.5 73.6 72.3 73.3	72.17 73.83 74.65 73.90 74.93
74.9 76.7 76.5 75.4 77.5 78.2	75.0 76.7 — 76.2 75.2 77.5 78.3	75°3 76°5 ————————————————————————————————————	74.0 76.3 — 75.5 75.3 77.0 77.6	71°·5 73°6 75°0	71°1 73°3 74°5 — 74°9 74°5 75°7 77°1	70.7 72.8 74.0 74.5 74.5 75.3 76.8	69.7 72.1 73.5 74.5 74.2 75.5 76.5	69°3 71°5 73°0 74°5 73°8 74°5 75°8	68.6 70.9 72.5 74.0 72.8 73.5 75.5	70.5 	$ \begin{bmatrix} 70.0 \\ -1 \\ 71.5 \\ 73.6 \\ 72.3 \\ 73.3 \\ 74.6 $	72.17 73.83 74.65 73.90 74.93 76.45
74.9 76.7 76.5 75.4 77.5 78.2 78.5	75.0 76.7 — 76.2 75.2 77.5 78.3 78.5	75·3 76·5 ————————————————————————————————————	74.0 76.3 —— 75.5 75.3 77.0 77.6 78.5	71°·5 73°6 75°0 — 75°2 74°7 76°1 77°5 79°5	71°1 73°3 74°5 74°9 74°5 75°7 77°1 79°5	70.7 72.8 74.0 74.5 74.5 75.3	69.7 72.1 73.5 74.5 74.2 75.5	69°3 71°5 73°0 74°5 73°8 74°5	68.6 70.9 72.5 74.0 72.8 73.5	70.5 72.1 74.0 72.7 73.5	70.0 71.5 73.6 72.3 73.3 74.6 76.8	72:17 73:83 74:65 73:90 74:93 76:45 78:58
74.9 76.7 76.5 75.4 77.5 78.2	75.0 76.7 — 76.2 75.2 77.5 78.3	75°3 76°5 ————————————————————————————————————	74.0 76.3 — 75.5 75.3 77.0 77.6	71°·5 73°6 75°0	71°1 73°3 74°5 — 74°9 74°5 75°7 77°1	70°.7 72°.8 — 74°.0 74°.5 74°.5 76°.8 79°.4 —	69°.7 72°.1	69°·3 71°·5 73°·0 74°·5 73°·8 74°·5 75°·8 78°·2	68.6 70.9 72.5 74.0 72.8 73.5 75.5 77.7	70.5 	70.0 71.5 73.6 72.3 73.3 74.6 76.8	72:17 73:83 74:65 73:90 74:93 76:45 78:58 76:71
74·9 76·7 76·5 75·4 77·5 78·2 78·5 78·0	75.0 76.7 — 76.2 75.2 77.5 78.3 78.5 77.7	75·3 76·5 — 75·7 74·9 77·5 78·1 78·5 77·5	74.0 76.3 — 75.5 75.3 77.0 77.6 78.5 77.3	71°.5 73°.6 75°.0	71°1 73°3 74°5 — 74°9 74°5 75°7 77°1 79°5 77°0	70°.7 72°.8 — 74°.0 74°.5 74°.5 75°.3 76°.8 79°.4 — 76°.7	69°.7 72°.1	69°·3 71°·5 73°·0 74°·5 73°·8 74°·5 75°·8 78°·2 76°·2	68.6 70.9 72.5 74.0 72.8 73.5 75.5 77.7 76.0	70.5 72.1 74.0 72.7 73.5 75.0 77.0	$ \begin{bmatrix} 70.0 \\ -1 \\ 71.5 \\ 73.6 \\ 72.3 \\ 73.3 \\ 74.6 $	72:17 73:83 74:65 73:90 74:93 76:45 78:58
74.9 76.7 76.5 75.4 77.5 78.2 78.5 78.0	75.0 76.7 ——————————————————————————————————	75·3 76·5 —— 75·7 74·9 77·5 78·1 78·5 77·5 —— 79·0	74.0 76.3 	71°.5 73°.6 75°.0	71°1 73°3 74°5 — 74°9 74°5 75°7 77°1 79°5 77°0 — 78°3	70°.7 72°.8 — 74°.0 74°.5 74°.5 75°.3 76°.8 79°.4 — 76°.7 78°.6	69°.7 72°.1	69°·3 71°·5 73°·0 74°·5 73°·8 74°·5 75°·8 78°·2 76°·2 77°·1	68.6 70.9 72.5 74.0 72.8 73.5 75.5 77.7 — 76.0 76.6	70.5 	$ \begin{bmatrix} 70.0 \\ \hline 71.5 \\ 73.6 \\ 72.3 \\ 73.3 \\ 74.6 \\ 76.8 \\ \hline 75.0 \\ 75.7 $	72:17 73:83 74:65 73:90 74:93 76:45 78:58 76:71 77:61 76:97
74.9 76.7 76.5 75.4 77.5 78.2 78.5 78.0 78.9 78.7	75.0 76.7 ——————————————————————————————————	75·3 76·5 — 75·7 74·9 77·5 78·1 78·5 77·5 — 79·0 78·0	74.0 76.3 — 75.5 75.3 77.0 77.6 78.5 77.3 — 79.3 77.2	71°.5 73°.6 75°.0 — 75°.2 74°.7 76°.1 77°.5 79°.5 77°.1 — 78°.7 76°.8	71°1 73°3 74°5 74°9 74°5 75°7 77°1 79°5 77°0 — 78°3 76°3	70°.7 72°.8 — 74°.0 74°.5 74°.5 75°.3 76°.8 79°.4 — 76°.7 78°.6 75°.7	69°.7 72°.1	69°·3 71°·5	68.6 70.9 72.5 74.0 72.8 73.5 75.5 77.7 76.0 76.6 73.6	70.5 	$egin{array}{c} 70.0 \\$	72:17 73:83 74:65 73:90 74:93 76:45 78:58 76:71
74.9 76.7 76.5 75.4 77.5 78.2 78.5 78.0 78.9 78.7 72.7	75.0 76.7 ——————————————————————————————————	75·3 76·5 — 75·7 74·9 77·5 78·1 78·5 77·5 — 79·0 78·0 72·3	74.0 76.3 — 75.5 75.3 77.0 77.6 78.5 77.3 — 79.3 77.2 71.6	71°5 73°6 75°0 — 75°2 74°7 76°1 77°5 79°5 77°1 — 78°7 76°8 71°5	71°1 73°3 74°5 74°9 74°5 75°7 77°1 79°5 77°0 78°3 76°3 71°0	70°.7 72°.8 — 74°.0 74°.5 74°.5 75°.3 76°.8 79°.4 — 76°.7 78°.6 75°.7 70°.5	69°.7 72°.1	69°·3 71°·5	68.6 70.9 72.5 74.0 72.8 73.5 75.5 77.7 76.0 76.6 73.6 69.3	70.5 	$\left\{ egin{array}{c} 70.0 \\$	72:17 73:83 74:65 73:90 74:93 76:45 78:58 76:71 77:61 76:97
74.9 76.7 76.5 75.4 77.5 78.2 78.5 78.9 78.7 72.7 73.5	75.0 76.7 	75·3 76·5 — 75·7 74·9 77·5 78·1 78·5 77·5 — 79·0 78·0 72·3 73·1	74.0 76.3 — 75.5 75.3 77.0 77.6 78.5 77.3 — 79.3 77.2 71.6 73.0	71°5 73°6 75°0 — 75°2 74°7 76°1 77°5 79°5 77°1 — 78°7 76°8 71°5 72°6	71°1 73°3 74°5 74°9 74°5 75°7 77°1 79°5 77°0 78°3 76°3 71°0 72°1	70°.7 72°.8 — 74°.0 74°.5 74°.5 75°.3 76°.8 79°.4 — 76°.7 78°.6 75°.7 70°.5 72°.0	69°.7 72°.1 — 73°.5 74°.5 74°.5 76°.5 77°.6 — 76°.5 74°.8 70°.1 72°.3	69°·3 71°·5	68.6 70.9 72.5 74.0 72.8 73.5 75.5 77.7 76.0 76.6 73.6 69.3 71.5	70.5 	$ \begin{bmatrix} 70.0 \\ \hline 71.5 \\ 73.6 \\ 72.3 \\ 73.3 \\ 74.6 \\ 75.0 \\ \hline 75.7 \\ 72.4 \\ 68.5 \end{bmatrix} $	72:17 73:83 74:65 73:90 74:93 76:45 78:58 76:71 77:61 76:97 71:79
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74.9 76.7 76.5 75.4 77.5 78.2 78.5 78.7 72.7 73.5 76.3 78.6 82.5	75.0 76.7 76.2 75.2 77.5 78.3 78.5 77.7 78.7 78.4 72.5 73.3 76.1 78.6 82.3	75°3 76°5 — 75°7 74°9 77°5 78°1 78°5 77°5 — 79°0 72°3 73°1 76°1 79°0 — 80°9	74.0 76.3 — 75.5 75.3 77.0 77.6 78.5 77.3 — 79.3 77.2 71.6 73.0 76.5 78.6 — 81.0	71° 5 73° 6 75° 0 75° 2 74° 7 76° 1 77° 5 79° 5 77° 1 — 78° 7 76° 8 71° 5 72° 6 76° 7 78° 4 — 80° 5	71°1 73°3 74°5 74°9 74°5 75°7 77°1 79°5 77°0 ——————————————————————————————————	70°·7 72·8 — 74·0 74·5 74·5 75·3 76·8 79·4 — 76·7 78·6 75·7 70·5 72·0 76·0 — 77·8 80·0	69°·7 72°·1	69°·3 71··5 73·0 74··5 73·8 74··5 75·8 78·2 76··2 77··1 73·8 69··6 72··0 74··5 78··6	68.6 70.9 72.5 74.0 72.8 73.5 75.5 77.7 76.0 76.6 69.3 71.5 74.4 77.0 78.3	70.5 	70.0 71.5 73.6 72.3 73.3 74.6 76.8 75.0 75.7 72.4 68.5 70.7 73.7 76.7 78.1 76.5	72:17 73:83 74:65 73:90 74:93 76:45 78:58 76:71 77:61 76:97 71:79 71:51 74:67 77:29 79:67 77:83
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	$\begin{pmatrix} 2\\3\\4\\5\\6\\7 \end{pmatrix}$	Sc. Div. 156°5 156°0 141°4 152°0 151°9 147°4	Sc. Div. 155'0 155'0 146'5 156'0 151'9 147'2	Sc. Div. 152°5 154°4 144°1 145°0 145°8 147°9	sc. Div. 151'9 154'5 142'0 144'3 143'2 147'9	Sc. Div. 155°1 151°3 140°6 148°2 143°9 146°8	Sc. Div. 154.9 148.8 139.3 147.1 136.9 146.7	Sc. Div. 154 1 149 6 139 3 146 1 137 4 145 6	sc. Div. 148 * 8 151 * 1 140 * 1 151 * 5 138 * 5 144 * 9	Sc. Div. 149 ° 6 149 ° 8 141 ° 8 148 ° 2 140 ° 1 146 ° 8	Sc. Div. 149°6 150°2 140°7 153°5 139°8 149°1	sc. Div. 148 · 6 149 · 3 141 · 9 154 · 7 137 · 9 153 · 7	Sc. Div. 147 ' 4 149 ' 6 140 ' 0 148 ' 8 145 ' 4 151 ' 7
T.	8 9 10 11 12 13 14 15	150.7 147.1 143.3 149.4 146.0 141.5	151'5 146'4 143'9 148'5 145'0 140'8	150.7 147.4 143.9 148.2 142.8 140.1	151.6 145.6 143.7 146.8 141.2 139.8	151.6 143.5 144.2 145.1 139.6 136.2	148°2 142°6 144°1 143°3 138°2 139°0	146.6 139.6 143.2 143.1 135.5 139.2	147 · 2 139 · 4 141 · 5 142 · 9 135 · 7 139 · 2	145 1 139 5 141 4 142 9 135 8 138 1	144.0 138.2 141.4 142.1 137.7 138.1	146.8 138.5 142.3 141.8 140.0 138.1	146°1 138°6 142°4 144°2 139°7 138°7
AUGUST.	16 17 18 19 20 21 22	138.0 137.2 145.0 159.5 155.1 155.4	137.1 135.3 145.0 159.5 153.7 155.4	131'9 133'2 144'8 157'1 153'3 152'4	133°5 132°4 142°7 157°0 153°3 151°0	132·1 131·2 141·7 157·9 151·8 150·2	132.9 130.3 145.3 158.4 150.6 150.9	131.7 131.7 144.7 157.7 152.0 150.9	129'9 131'9 145'7 157'7 151'7	131'1 133'8 148'1 157'7 151'4 151'8	132.8 134.3 149.9 157.0 150.4 149.5	134.4 136.0 148.9 155.9 150.4 151.7	133'3 138'5 153'1 155'4 150'4 149'7
	23 24 25 26 27 28 29	159.4 154.7 154.4 142.2 147.6 140.1	156'4 154'6 150'1 147'4 148'6 148'8	155°2 153°3 148°3 153°0 148°6 148°5	154.6 151.5 148.3 153.5 148.0 148.2	153°3 151°3 147°8 151°2 147°5 145°9	152.3 152.1 147.8 148.5 147.5 145.7	153°5 150°8 155°8 148°3 150°0 148°6	154.6 151.6 160.1 147.8 150.2 148.2	154.5 152.9 155.3 146.8 152.2 149.1	155.8 155.4 150.2 146.3 150.4 149.0	155.4 153.0 150.0 144.8 149.9 149.5	152.7 152.3 150.9 144.8 149.5 149.3
	30 a 31 a	149°5 151°0	148°1 150°3	148°1 148°5	143°7 148°5	143°5 148°5	143.4 149.0	142.7 149.0	141.9 150.0	143°5 152°0	144.5 153.8	145°1 152°7	147.8 152.0
Hourly	Means	148.82	149.15	147.60	146.94	146.17	145.47	145.62	145.88	145.99	146.06	146.40	146.3
							VERTICAL					· · · · · · · · · · · · · · · · · · ·	
	2 3 4 5 6 7	65.3 66.2 66.7 68.3 68.7 69.5	65.0 66.2 67.4 68.8 68.7 69.3	65.0 66.5 67.9 69.6 70.4 69.0	66.0 67.3 68.8 70.5 70.5 69.5	67.5 68.3 69.5 71.3 73.0 70.0	67.7 68.5 70.1 71.5 73.5 70.5	68.0 68.6 70.5 72.0 73.8 71.4	68.5 68.6 70.7 72.3 73.7 71.7	68.8 69.0 71.0 73.0 73.7 72.0	69·4 69·5 71·9 73·5 74·5 72·5	70°0 69°7 73°0 73°2 75°5 72°3	69.9 69.5 72.5 74.2 72.1
ľ.	8 9 10 11 12 13 14	67.2 70.5 71.9 69.0 71.2 72.5	67.0 70.6 71.7 69.6 71.5 72.5	67.0 70.6 72.0 69.4 72.1 72.7	67.3 70.6 71.8 69.4 73.2 73.4	67.5 71.6 71.7 70.5 73.5 74.3	68.5 72.6 71.8 71.5 74.4 74.5	69°1 73°3 72°2 72°0 74°7 74°7	69.6 73.4 72.4 72.5 74.5 75.4	70.6 73.7 72.5 72.8 75.0 75.6	71.5 74.5 72.5 73.5 75.0 76.0	72.0 74.5 72.5 73.8 74.7 76.3	72.5 74.5 72.6 73.7 74.5 76.5
AUGUST.	15 16 17 18 19 20 21 22	74.5 74.5 69.5 64.4 63.5 64.7	74.5 75.0 69.4 64.0 64.1 65.0	75°3 75°3 69°5 64°1 63°8 65°8	76.7 75.4 69.5 63.5 64.3 66.5	76°5 75°3 69°3 64°3 65°5 66°7	77.0 75.5 69.5 64.4 66.0 66.8	77.4 75.5 69.5 64.5 66.5 66.9	78.0 75.5 69.5 64.7 66.9 67.3	78.0 75.7 69.5 64.7 67.4 67.5	78°5 75°5 69°5 65°3 68°0 68°1	78.6 75.5 69.7 65.4 68.3 69.0	79.5 75.4 69.6 65.7 68.5 70.0
	23 24 25 26 27 28 29	65.5 65.5 66.0 66.6 69.3 67.3	66.5 66.0 65.8 66.6 68.8 67.2	67.3 66.0 66.4 66.8 68.8 67.5	68°1 66°5 67°5 67°3 68°6 67°0	68.6 67.2 69.0 68.3 68.6 69.0	68.7 68.5 69.5 68.6 69.0	68.7 68.5 70.0 69.3 68.5 69.3	69.0 68.7 70.5 69.6 68.3 69.0	69°3 69°0 71°7 70°4 68°5 69°3	69.5 69.8 72.5 71.5 68.7 69.5	69.7 70.1 71.6 72.0 69.4 70.2	70.0 70.5 71.6 71.6 69.5 70.3
	30 a 31 a	67.0 66.3	67.0 66.3	68.0 68.0	69°0 66°4	69.8 66.2	70°3 66°6	70°5 67°0	70°7 67°0	70·8 66·7	71·3 66·8	71.0 66.8	71.5 66.7
Hourly	y Means	68.26	68.38	68.40	69.13	69.87	70.30	70.62	70.85	71.50	71.70	71.96	71.9

The observations on the 30th and 31st days are omitted from the Means, the readings having been affected to an uncertain amount by the induced magnetism of the vertical iron shafts of Robinson's anemometer.

	One Scale	Division =	•000066 pa	ts of the V		RTICAL F		orresponding	r to 1° decre	ease of Tem	perature, 1·6	64.
12 ^h .	13h.	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18 ^h .	19h.	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
149.5	147.9	147.6	146.6	146.7	146.7	147.0	147.6	147.7	150.1	152.8	156.7	150°45 149°11
149.0	148.5	148.0	146.5	145.6	144.2	143.2	143.1	146.0	151.9	147.5	145.6	138.30
140.0	139.9	141.8	146.8	142.5	112.0	114.6	137.2 148.2	133.7 143.7	124 ·1 139 ·3	143°0 142°6	146°0 142°8	147.15
148.8	147.2	147.2	146.0	143.2	139.8	147.3	151.2	151.2	151.2	142 6	144.4	143.91
151°1 150°8	148°5 146°7	144 · 9 146 · 7	144'3 137'0	141.8 137.5	132.6 137.5	135'9						146.40
	-					142.8	144'3	149'4	145'4	149.5	150.3	
146'1	146.4	143.9	144.0	143.6	135.5	138.7	140.4	143.0	144.8	145'9	147.9	145.85
138.6	137.6	139.7	138.8	138.8	139.4	138.8	139.8	141.1	141.3	141'1	142.3	140.99
142.6	142.0	142.1	142'7	143.0	143.9	142.2	140.4	141.0	146.3	146.3	146'1	143.08
142.1	146'1	140.6	140.3	140.3	140.3	141.1	141'1	142.7	145.2	143.4	145.0	143.60
138.3	138.3	138.3	138'8	139.0	139.0	139.1	140.5	141.2	140.0	141.2	140'1	139.65
135.5	136.5	135.6	136.6	137.6	141.6	19911	134.4	135.0	135.8	134.8	137.5	137.60
	10110	101.1	100.0	100:1	100:0	133.1		116.3	127.0	131.3	135.2	131.30
131.3	131.3	131.1	129.6	130.1	129 . 9	130°2 137°3	128 · 9	140.0	140.0	141.5	141.1	135.96
136.8	136.1	135.3	135.3	135.7		155.0	155.4	155.4	155.1	155.1	159.2	149.96
152.1	152.0	152.7	146.0	150.9	155°3 155°2	155.2	156.0	154.6	154.2	150.8	155.7	156.10
155'1	153.8	155.2	154.6	155.2			152.8	152.8	153.6	153.2	155.7	152.00
150.6	150.6	150.6	150.6	151°1 147°8	151°1 122°9	151.0	102 0	102 0	100 0		1 ()	
145.7	145.6	145.6	147.8	141 9	122 9	147.3	140.6	148.2	149.1	150.3	159.4	148.77
150.0	150.0	151.2	152.7	153.1	151.6	152.2	152.0	145.7	144.7	147.6	147.9	152.35
150.7	150.7	150.2	152.2	152.2	151.4	146.3	135.4	134.8	135.3	131.5	142.7	148.62
153.6		151.8	151.8	151.8	146'1	146.2	141.6	145.2	144.3	145.2	143.7	149.73
144.8	152.9	143.6	142.6	144.8	143.6	143.0	145.6	145.6	146.6	147.4	147.4	146.41
142.8	144°2 143°0		142 0	148.0	146.6	146.7	147.4	145.8	135.0	134.0	133.2	145.91
147.1		143°8 147°1	145 2	147.9	148.5	140 /	111	110 0	100 0			
14/ 1	147.1	14/ 1	147 0	147 9	140 0	148.9	148.9	148.6	147.0	145'0	145.1	147.46
148.3	148.3	144.4	146.0	145.8	145.8	145.8	145.4	146.1	146.1	149:3	149.3	145.93
			149'1	149.3	149.3	149.5	152.0	154.2	154.5	155.8	156.2	151.14
151.4	151.7	149.4	149 1	143 3	<u> </u>							
145.24	145.11	144.79	144.32	144.21	141.40	142.63	143.85	143.73	143.65	144.36	146.32	145.44
				TEMPE	RATURE OF	THE VERT	CICAL FORCE	E MAGNET			ı	
69°9	70°0	69°7	70°1	70°1	7ő·0	68°4	67°9	67°9	66°8	$6\overset{\circ}{6}$.5	66.0	68.10
70.2	70.2	70.2	70.5	70.5	70.4	70.3	70.3	70.0	68.0	67.4	66.2	68.89
72.7	72.5	72.5	72.5	73.2	73.4	72.9	72.7	71.7	71.0	70.5	70.0	71.07
72.5	72.4	72.4	72.3	71.5	71.0	70.7	69.8	69.5	69.3	69.0	68.6	71.06
72.8	72.5	72.7	72.2	72.0	71.7	71.5	71.0	70.4	70.2	70.3	70.3	71.99
71.8	71.6	71.5	71.3	71.0	70.8						67.7	70.07
	· —	_				67.3	67.3	67.1	67.3	67.3		-0-01
72.2	72.4	72.5	72.3	72.3	72.0	72.5	72.3	72.0	72.0	71.5	71.5	70.64
74.5	74.3	74.2	74.5	74.1	74.0	73'6	73.5	73.3	73.0	72.7	72.0	73.09
72.7	72.5	72.5	72.0	71.7	71.2	70.7	70.4	69.9	69.5	69.4	69.2	71.55
73.9	73.7	73.3	73.1	72.8	72.5	72.4	72:2	72.0	72.0	71.6	71.6	72.03
74.6	74.5	74.4	74.2	74.2	74.0	73.8	73.3	73.3	73.3	73.0	73.0	73.75
76.2	76.3	75.7	75.7	75.7	75.6	77.0	70	F0.7	-	7010	$\left\{\begin{array}{c} \overline{75\cdot5} \end{array}\right\}$	75.29
70:-						77.3	76.5	76.1	75.7	76.0	74.7	77.22
79.5	79.2	79.0	79.2	78.3	77.6	77:1	76.7	76.3	76.0	75.3	74.7 71.0	71 22
75.5	75.3	75.5	75.2	75.2	74.4	73.5	72.8	72.3	71.7	71.3		
69.3	68.5	67.7	66.8	66.5	65.5	64.9	64.4	64.3	64.5	64.4 64.3	64.4 63.7	67°72 64°76
66.0	65.5	65.5	65.5	65.4	65.0	64.8	64.5	64.5	64°5 65°5	65.3	64.7	66.45
68.5 70.5	68.3	68.5	67.5	67.3	66.8	66.8	66.2	66.2	00 0	00 0		
-	70.2	69.7	69.5	69.5	69.5	68.5	67.7	67.4	66.7	66.3	$\overline{65\cdot7}$	67.74
70.2	70:0	70:0	60.8	60:5	69.1	68.2	67.7	67.5	66.8	66.2	65.8	68.42
70.7	70.0	70·0 70·0	69.0 69.8	69.5	68.5	68.1	67.9	67.5	67.2	66.2	66.2	68.23
71.6	70'7 71'4	70.8	70.6	69.8 68.6	69.8	69.2	69.5	69.0	69.0	68.8	67.4	69.24
71.5	71.5	71.4	71.3	71.3	71.0	71.0	71.4	71.0	70.6	70.4	70.3	70.02
72.2	71.5	71.4	70.8	70.7	70.5	70.0	69.7	69.7	70.1	69.7	69.7	69.68
70.4	72.2	70.1	69.6	69.4	69.0	100	-	55				
	10 4	10.1	05.0	03 4	09 0	68.4	68.3	68.3	68.3	67.7	$\frac{-}{67\cdot 4}$	68.83
71.2	70.6	71.0	69.6	69.2	69.0	68.6	68.4	68.2	67.5	67.0	67.0	69°35
_	66.4	66.0	66.0	65.8	65.6	65.4	64.3	63.8	63.2	63.1	63.0	65.80
66.2	00 4	00 0			1		1				11	

	Or	ne Scale Div	ision = '00	0066 parts o	f the V.F.		CAL FOR		sponding to	l° decrease	of Temperat	cure, 1.64.	
Mean (Göttin-}	Oh.	1 ^h •	2 ^h .	3h.	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8 ^h .	9հ.	10 ^h .	11h.
	/ 1ª	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.					
	$\begin{bmatrix} 2 \\ 3 \\ 4 \end{bmatrix}$	151°3 153°8	152.7 151.7	151.8 152.2	151.8 123.8	149.6 154.2	151.6 148.2 154.9	149 .3 145.8 157.8	149°3 144°9 157°7	149°3 146°7 157°8	148°3 146°4 157°8	146°3 146°3 160°9	147°2 150°2 159°1
	5 6 7 8 9 10	160°1 158°4 153°1 152°8 163°9 161°1	161'4 157'0 152'3 151'4 164'1 164'8	157.5 156.4 151.9 151.4 158.9 161.5	156.4 157.8 151.4 151.4 158.7 160.2	155°3 152°7 149°5 151°9 156°9 158°8	155.9 b 152.6 147.4 151.9 154.9 158.1	154'9 150'0 144'9 155'3 154'9 158'1	154.0 148.7 144.9 155.3 155.9 159.0	154.5 151.0 144.9 152.9 155.9	155°0 152°3 144°8 163°8 155°9 158°5	154'3 151'3 143'5 164'7 154'0 162'1	153.9 150.2 143.6 165.0 154.6 155.6
SEPTEMBER.	12 13 14 15 16 17 18	143.8 170.8 174.6 170.9 163.8 161.9	148.5 173.3 173.4 170.5 163.8 161.9	131'4 172'2 171'5 167'9 164'4 161'2	131.7 169.6 170.0 165.4 163.1 159.3	150.0 169.6 167.8 163.9 160.3 159.5	153 · 2 169 · 6 167 · 8 163 · 5 162 · 7 159 · 5	162.7 169.6 168.7 166.5 163.8 158.5	165 ' 4 169 ' 6 169 ' 6 162 ' 8 163 ' 6 159 ' 6	169.7 170.3 169.6 164.1 162.0 161.2	173.8 170.3 166.8 163.4 161.3 159.7	175°1 168°3 165°7 163°4 160°4 159°8	173 · 5 168 · 2 164 · 4 163 · 4 159 · 0 162 · 2
	19 20 21 22 23 24 e 25	162.1 164.5 166.1 155.3 143.6 175.0	163°3 163°8 164°9 158°9 f 175°0	163°3 162°5 162°2 160°3 138°8 174°5	162.5 161.3 160.6 155.6 154.0 173.5	162.0 161.1 161.6 156.1 150.5 172.6	162.0 161.1 159.4 156.4 172.5 172.5	161.6 159.4 159.5 157.6 197.6 171.1	160.7 159.4 162.8 160.6 195.7 171.9	162.8 159.3 167.2 161.7 184.1 171.4	164.9 159.5 166.9 157.0 191.7 171.4	165.4 159.2 163.1 154.8 190.4 169.7	166.0 158.7 162.0 157.1 182.7 170.7
	26 27 ° 28 29 30	165.3 173.3 178.2	121°3 166°3 175°7 180°3	138°3 167°6 174°6 178°9	154.5 162.6 173.5 178.3	164.7 162.4 171.5 177.9	160°2 163°1 171°3 176°2	164'3 165'1 175'9 176'2	169'7 168'5 193'2 174'9	169.7 169.6 198.7 173.1	169°7 170°6 200°5 175°6	162'3 176'9 199'5 173'5	159.5 177.6 191.1 171.9
Hourly	y Means	162.73	163.41	161.26	160.39	160.24	160.10	160.81	161.95	162.88	163.46	163.27	162.64
		1 _	<u> </u>	1	TEMPERAT		1		1				
	1 a 2 a 3 4	62°5 63°3 66°1 65°5	62°3 63°4 66°5 65°0	62°5 64°3 66°4 64°9	62°5 65°0 66°3 64°7	63°3 65°6 67°0 64°7	63.5 66.2 68.0 64.9	63°7 66°5 68°4 64°9	63°9 67°0 68°7 65°0	64.5 67.7 69.2 64.6	65°3 68°4 69°9 64°6	66°3 68°8 70°2 64°5	65.7 69.3 70.4 64.6
	5 6 7 8 9 10	62.7 63.5 66.0 65.7 60.5 60.7	62.5 64.0 66.2 65.3 61.0 61.0	63.5 64.5 66.7 64.9 61.7 61.5	63.8 64.7 66.7 64.7 62.5 61.7	64.4 66.6 67.6 64.9 63.0 62.5	64.5 67.3 68.7 65.0 63.3 63.3	64.5 67.2 69.5 64.7 63.5 63.3	64.7 67.2 70.0 65.0 64.0 63.7	65°3 67°3 70°2 65°2 64°3 63°8	65.7 67.5 70.5 65.4 64.5 64.5	66°1 67°6 70°7 65°5 64°7 64°5	66.3 67.5 70.5 65.5 65.1 64.5
SEPTEMBER.	12 13 14 15 16 17 18	62.7 56.5 55.1 57.4 59.9 62.5	62.4 56.3 56.0 57.8 59.5 62.4	62:3 56:3 57:1 58:2 60:2 62:5	62°1 56°3 57°2 58°5 60°5 62°5	62:3 56:5 58:0 59:0 61:5 62:7	62:3 56:5 58:3 59:8 62:1 62:9	62°3 56°6 58°5 60°2 62°4 63°3	62.0 57.1 58.8 60.5 62.9 63.5	61.7 57.7 59.0 60.7 63.3 63.5	61.5 58.0 59.5 61.5 63.6 63.5	61'8 58'2 60'0 61'7 63'9 63'6	60.6 58.5 60.5 62.4 63.6 63.5
	19 20 21 22 23 24 e 25	60°8 60°0 58°8 62°5 66°0 60°0	60.7 60.0 59.2 61.3 — f 59.6	60.7 60.8 59.0 61.7 63.5 59.2	60.7 61.3 60.0 62.5 63.1 59.0	60.7 61.5 61.0 62.6 63.0 59.5	60'9 61'4 61'0 63'0 63'1 59'6	61.0 61.9 61.1 63.4 63.1 60.0	61'4 62'5 61'4 63'7 63'3 60'2	61.5 62.5 61.5 64.5 63.1 60.1	61.5 63.0 62.1 65.5 63.0 60.0	61.6 63.5 62.6 65.8 62.9 60.5	61.5 63.5 63.1 65.8 62.8 60.5
	26 27 ° 28 29 30		63°7 61°7 57°4 56°0	64.7 61.5 57.2 57.1	62.5 62.7 57.2 57.6	62.5 62.7 57.7 58.0	63 · 2 62 · 5 58 · 0 58 · 4	63°5 62°5 58°2 58°6	64.2 62.2 58.4 59.0	64.5 62.3 58.5 59.1	65.5 62.5 58.5 59.1	66'4 62'4 59'0 59'0	66.5 61.5 58.5 58.5
Hourly	Means	60.97	60.99	61.27	61.21	62.02	62.35	62.55	62.81	62.99	63.29	63.2	63.47

^a The observations on the 1st and 2nd days are omitted from the Means, the readings having been affected to an uncertain amount (up to 4^h on the 2nd) by the induced magnetism of the vertical iron shafts of Robinson's anemometer.

^b Eight minutes late.

	One Scale	Division =	: •000066 pa	arts of the V	VE.	RTICAL F ase, in Scale	ORCE. Divisions, c	orrespondin	g to 1º decre	ease of Tem	perature, 1.6	4.
12h.	13h.	14 ^h .	15 ^h •	16 ^h .	17 ^h .	18h.	19 ^h .	20h.	21 ^h .	22 ^h .	23 ^h •	Daily and Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
147:2	147.3	147°3	147.3	147.3	147.9	147.9	147.9	148.9	148.9	150.3	151.4	148.47
151.1	151.1	146.1	147.3	147.7	149.4	149.4	150.0	151.0	152.6	149'8	150.1	149.22
157.1	157.8	153.9	156.0	158.6	156.7	_				-	157.8}	156:35
	'					155.6	156.1	156'1	156.9	157.8		
153.8	152.0	151.1	151.6	151.6	151.0	151.0	155.2	155.3	155.6	155.2	157.8 152.1	154.78 151.85
150.4	148.4	148.4	152.1	151.7	152.4	151.5	149'1	149°5 149°7	149°5 149°7	150°8 149°0	151.9	147.17
143.0	143.9	144.6	143.7	143.9	145.0	146.5 158.6	148 '9 159 ' 9	159.7	160.8	160.3	160.3	158.36
163°1 154°6	162°2 154°6	166°8 155°1	162 . 8	159°8 156°8	158°5 156°8	156.6	156.6	156.8	155.2	156.6	164.6	157.02
155.6	156.0	156.0	156.2	156.7	156.7	105 0			_		- 11	155.08
_		_				155.0	153.5	150.8	148.5	125.4	134.4	
173.3	169.8	169.9	169.2 c	170.0	170.1	165.1	162.4	164'6	168.5	168.5	170.8	162.55
168 2	168.2	169.8	168.3	169.2	169.6	169'6	170.2	171.5 q	172.0	172.0	172.8 168.2	170°12 167°49
163.4	162.7	164.2	164.9	165.5	165.8	164.8	166'8	166.8	168.7 162.3	167°8 158°8	160.7	163.58
164.4	162.5	163.8	166.3	152.6	154.9	162.0	162'3	162°3 156°8	159.4	160.3	160.3	160.20
159.7	157.5	156.5	158.3	158.8	159°2 158°3	158*4	158.7	100.0	103 4.			
162.5	162.5	159.3	161.3	159.3	155 5	162.3	162.6	162.6	160.6	158.9	161·3 164·9	160.66
167.9	167.1	165.9	162.3	161.4	159.6	160.1	160.6	161.3	161.3	163.6	101 0	163.05
158.7	158.3	159.2	159.5	159.2	160.9	160.6	161.8	161.8	163.0	163.0	163.7	160.80
160.5	156.5	157.8	158.1	157.7	153 6	157.8	154.9	158.8	158.2	158.9	157.8	160.26
157.7	166.2	158.4	159'1	158.1	158.1	153.8	139'3	122.7	132.3	129.3	107.5	151.41
190.8	186.5	182.3	174'1	174.1	171.9	162.2	160.2	164.2	171.0	171.7	171.9	173.17
168.2	168.5	167.8	166.6	168.0	169.0				755.0	141:4	106.9	162.50
	l	_				156.4	134.4	128.3	155°0 164°5	141 4 164 5	164.8	160.02
159.5	159.2	160.8	160.7	163.9	168.8	153.6	163.0	162 · 9	170.6	166.4	170.6	170.13
177.6	177.3	186.8	174.9	170.4	172.0	167°2 177°4	166 '7 170'5	170.3	175.6	175.6	176.7	180.70
181°8 171°9	202.0	$\begin{array}{c} 173 \cdot 1 \\ 172 \cdot 2 \end{array}$	180.4	177°1 172°0	177.4 172.3	172.3	171.2	172.7	172.7	172.5	172.5	174.20
	171.9		171'5				157.82	157.10	159.21	157:37	156.23	160.79
162.02	162.28	161 23	161.18	160.28	160.33	159.64			103 01	10, 0,	.00	
	1	1	1	TEMPER	1	THE VERT	1 .	ı	<u> </u>		1 0 1	
65.5	67.0	66.3	65.8	65.6	65.5	65.3	65.0	65.0	64.5	64.2	63.2	64.55
69.5	69.2	69.0	69.3	69.2	68.8	68.2	68.3	68.0	67.6	67.3	66.6	67:37
69.7	69.5	69.2	68.7	68.2	68.2	67.7	66.8	66.6	66.3	65.8	65.3	67.90
64.4	64'3	64.6	64.2	64.4	64.3	_	 -				$\frac{-}{63 \cdot 1}$	64.42
						64.3	64'1	63.6	63.4	63·2 64·5	64.2	64.95
66.4	66.3	66.4	66.2	66.0	65.2	65.2	64.8	64.8	64 . 5 66.5	66.7	66.2	66.48
67.4	67:0	66.9	66.9	66.7	66.5	69.0 66.6	66.5 68.5	66.2 68.0	67.8	67.2	66.3	68.90
70°5 65°5	71.0	70.5	70.9	70°7 64°5	70.0 64.3	63.7	63.1	62.6	62.0	61.6	61.3	64.40
65.0	65.4	65.0 64.8	64.7 64.0	63.6	63.2	62.8	62.2	62.0	61.2	61.1	61.1	63.11
64.2	64.2	64.0	63.8	63.6	63.3		_			_	—)	63.27
	~~~				<b>-</b>	63.2	63.2	63.2	63.0	63.5	63.5	
60.1	60.0	59.6	59.0	58.8	58.2	58.2	58.0	58.0	58.0	57.6	57.1	60.30
<b>5</b> 8.8	58.6	58.2	58.5	58.0	57.6	57.2	56.8	56.2	56.3	56.0	55°3	57·18
61.0	61.3	60.8	60.4	60.0	59.8	59.9	59.2	59.0	58.7	58.2	57.9 60.0	58 <b>·</b> 93
62.5	62.3	62.0	61.5	61.0	60.7	60.2	60.3	60.1	60.1	60°0	62.7	62.38
63.5	63.0	63.3	63.3	63.0	62.5	62.3	62.5	62.2	62.6			
63.3	63.9	63.7	63.7	63.6	63.6	61.2	61.0	61.0	61.0	60.7	60.5	62.66
61.2	61.5	61.3	61.8	61.2	61.2	60.7	60.2	60.3	60.5	60.1	60.0	60.98
63.6	63.6	63.2	62.5	62.4	62.2	61.4	60.7	60.4	60.0	59.2	59.1	61.69
64.0	64.2	64.2	63.7	63.4	62.7	62.2	62.2	62.7	62.4	62.0	62.3	62.00
65.7	65.6	65.2	65.3	65.2	65.4	64.6	64.5	64.6	64.4	64.4	64.5	64'26
62.8	62.5	62.8	62.8	62.1	62.0	61.8	61.6	61.2	61.3	61.3	61.2	62.63
60.2	61.0	61.0	61.0	61.0	60.7				<u></u>		$\frac{-}{61\cdot 3}$	60.37
-		_		-		60.9	60.2	60.2	60.8	61.5	62.1	64.47
66.5	66.5	66'4	65.7	65.5	65.0	64.7	63.9	63°6 57°7	63°0 57°5	62 <b>°</b> 6 57 <b>°</b> 2	57.3	60.65
61.3	60.9	60.7	60.2	59.7	59.4	59.0	58°3	57 · 4	57.2	56.7	56.3	58.12
50.0	59.5	59.5	59.8	59.8	58.2	58.1	57.5	58.8	58.7	59.0	58.2	58.33
59°2 58°2	58.6	59.0	59.0	58.5	58.6	58.2	58.4	000	00 ,	00 0		_

^e Fifteen minutes late.

d Three minutes late.

^e Omitted in the Means, on account of disturbance.

	Oı	ne Scale Div	ision = '00	0066 parts o	f the V. F.		ICAL FOR n Scale Divi		ponding to	1° decrease (	of Temperat	ure, 1°64.	
Mean G gen T	öttin-}	0 ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h •	10h.	11 ^h .
	$\begin{pmatrix} 1 \\ 2 \\ 2 \end{pmatrix}$	Sc. Div. 174 1 175 5	Sc. Div. 173 7 175 5	Sc. Div. 174.7 174.9	Sc. Div. 170°5 172°9	Sc. Div. 169°4 171°3	sc. Div. 169°7 169°7	sc. Div. 168.6 169.6	Sc. Div. 168 6 169 6	sc. Div. 169°5 166°6	sc. Div. 169°5 164°1	sc. Div. 172°6 164°5	Sc. Div. 174'4 165'0
	3 4 5 6	174°1 164°0 163°0	173 · 4 165 · 3 163 · 0	171 '4 165 '2 163 '0	166°1 165°3 164°8	167.5 165.0 164.6	166.8 163.1 163.3	167.5 161.6 164.6	165.7 161.5 166.0	164.5 161.5 165.7	163°1 161°5 164°2	162.5 161.7 163.9	163.4 159.6 163.9
	7 8 9 10	163°1 161°2 167°3	162.0 161.2 167.3	164°0 161°2 167°1	164°0 158°6 165°9	163.8 157.9 163.7	161°9 157°1 161°8	162.5 158.4 161.8	162°5 158°4 163°7	163°2 162°8 163°7	163°2 166°9 164°2	163°2 165°3 163°3	163°3 167°4 163°3
	11 12 13 a	173°3 173°2 46°3	173°3 173°2 163°5	172°3 173°2 153°8	172°3 173°2 145°8	170°7 170°9 167°4	170.7 170.0 173.3	170°7 170°0 180°0	169°8 173°0 185°7	172°2 174°9 192°9	171 · 8 176 · 7 187 · 4	170'9 173'7 183'7	170°1 173°8 176°4
OCTOBER	14 15 16 17	181°2 178°9 176°2	180°6 176°1 175°0	179°7 176°1 175°0	172°0 177°1 173°3	179.0 180.8 172.7	178°3 180°8 172°7	179°4 184°7 172°4	179°5 187°5 175°5	181.7 187.5 175.4	181.4 184.2 173.1	179'8 183'6 170'8	178.7 181.0 170.5
00	18 19 20	161.4 163.6 172.6	165.5 165.4 175.0	165°5 167°2 171°8	164.3 162.5 169.4	162.9 163.7 169.4	164.3 163.0 169.4	165.4 164.4 169.4	167°1 168°1 171°8	166.5 164.7 171.8	166 <b>·</b> 9 165 <b>·</b> 5 168 <b>·</b> 7	165.6 166.4 168.7	166.5 168.8
	21 22 a 23 a 24	169°9 174°1 137°3	170°8 174°2 — b	174 <b>.1</b> 176.4 213.2	174.4 176.3 152.0	173°2 176°6 184°9	171°2 176°6 188°5	170°8 176°6 219°8	172°4 177°6 209°3	172.2 179.0 199.0	172.6 182.2 181.9	172°5 184°4 174°2	172°2 182°7 204°2
	25 a 26 27 28	180°4 187°1 194°7 193°4	180.7 189.0 197.2 194.2	161:3 183:0 195:7 197:1	188'8 185'6 193'9 192'3	200.6 185.7 195.2	189.5 188.4 194.4 187.4	186.9 187.9 195.3	191 · 9 188 · 2 193 · 3	203.5 188.9 193.3	196.2 188.8 190.6	190.9 188.0 190.9	187'9 188'9 191'7
	29 30 31	183 · 1 181 · 4	181.8 183.1 184.5	183°1 182°2	182.8 12.8	189°4 177°6 177°3	175.4 173.4	187.4 181.3 173.4	187°7 180°4 173°4	188°1 181°2 173°4	184.2 180.0 174.4	183·9 178·5 174·4	183°9 179°6 174°4
Hourly	Means	174.20	174.62	174.43	172.77	172.35	171.49	172'14	172.90	173.16	172.57	172.02	172.18
			1 _0 _				HE VERTICA			0		1 0	
. {	1 2 3	58°0 55°2	58.8 55.2 —	59°.7 55°0	59°4 56°8 —	59°0 57°6	59.0 58.0	59°0 58°2	59°1 58°5 —	59°0 59°2 —	59°0 60°0	59°0 60°5	59°0
	4 5 6	55.3 59.8 61.5	56.0 59.7 61.3	56.4 59.7 61.2	58.8 60.0 61.0	58.2 60.0 60.7	59.0 60.5 60.7	59°3 61°4 60°9	60.0 61.2 61.0	60.4 62.3 60.9	60.6 62.9 61.2	61.0 63.5 61.2	61.2 63.5 61.1
	7 8 9 10	61.5 61.5 59.8	61.4 60.0	61.3 61.5 60.2	60.8 61.3 60.2	60.7 61.5 60.4	60.8 61.7 60.4	60°8 62°1 60°4	61.0 62.3 60.5	60°8 62°3 60°5	60°9 62°3 60°5	61.0 62.4 60.7	61.0 62.5 60.7
	11 12 13 a	55°2 55°4 53°8	55.5 55.0 54.0	56.0 55.0 55.0	56.8 55.0 56.5	57.0 55.2 54.6	56.7 55.4 54.5	56°6 55°6 54°4	56.7 55.2 54.3	56.5 55.0 54.4	56.5 55.1 54.7	56.6 55.2 54.5	56.7 54.7 55.0
OCTOBER.	14 15 16 17	51°5 48°2 51°3	51'3 48'2 51'5	51°3 50°0 52°0	53.7 49.5 53.4	52.7 49.8 53.7	52.6 50.5 54.2	53°0 50°9 54°4	53°3 50°9 55°0	53°3 51°2 55°4	53°3 51°5 56°3	53°3 51°6 57°0	53°3 51°8 57°3
100	18 19 20 21	56°7 60°0 55°3 57°2	56.2 59.4 55.0 56.5	56.5 59.6 59.0	57°2 59°6 56°7	57.8 59.5 56.3	58.6 59.8 56.8	59°0 59°8 57°0	59.0 60.0 57.0	59°5 60°2 57°4	60.2 60.3 58.0	61.0 60.5 58.7	61.2 60.4 58.8
	22 a 23 <b>a</b> 24	52.7 54.2 —	52.7 — ь	55°2 52°4 54°0	55°2 52°2 53°7 —	55°4 52°2 54°7	55.5 52.2 54.9	55°4 52°2 55°2 —	55°2 52°2 55°4	55°5 52°5 56°4 —	56.0 53.0 57.2	55°5 53°2 58°1 —	55.4 53.0 58.2
	25 a 26 27 28	57.2 50.1 44.8 46.4	56.2 50.0 44.2 46.6	56.0 53.1 44.8 47.6	56.2 50.8 45.0 47.4	56.5 50.6 45.4 48.0	56.6 50.2 46.1 48.4	56.7 50.2 46.1 48.9	56.6 50.5 46.5 49.0	56.0 49.2 47.2 49.5	56.2 50.1 48.0 50.5	55.8 50.2 48.0 50.7	55°2 49°6 48°4 50°4
	29 30 31	49.0 52.0	49°2 51°5 —	49°2 51°5 —	49°5 52°0 —	51°0 52°5	51.4 53.5 —	52°0 54°2 —	52°1 54°9 —	52°2 55°2 —	53°2 55°3 —	54°1 55°9 —	53°3 55°5 —
rr	Means	54.80	54.73	55.26	55.46	55.59	55.90	56.12	56.33	56.49	56.91	57.16	57.10

^a Omitted in the Means, on account of disturbance.

12h.   Sc. Div. 174'4   166'0	13h.	14 ^h .		1		oc, in Douge						
174.4	1	14	15 ^h .	16 ^h .	17 ^h .	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
100 0	Sc. Div. 170°1 166°0	Sc. Div. 170°1 166°7	Sc. Div. 170°8 168°7	Sc. Div. 171 2 168 7	Sc. Div. 172°3 168°9	Sc. Div. 172.3	Sc. Div. 168'8	Sc. Div. 169°9	Sc. Div. 172°9	Sc. Div. 172°9	Sc. Div. 172°9	Sc. Div. 171'41
i i	_	_	-			170.8	170.8	172.0	172.2	172.0	172·3 }	169.76
163.4	163.4	163.2	163.5	163.5	163.2	163.9	164.0	164.0	164.2	164.0		165.45
163°5 164°0	162.5 163.9	162 <b>.</b> 2	162°2 163°7	162.4 163.7	162°2	162°2	162°2	162°2	162°1 163°1	162°0 163°1	16 <b>2</b> °0 163°1	162.62 163.80
163.2	164'1	163.2	162.5	161.6	162.2	162.2	162.1	155.8	157.9	161.2	162.6	162.32
	176°3 165°7	173'4	164.5	164.0	164.5	140.6	155.7	155.7	163.6	163.6	163.7	162.17
_	105 /	165.6	165.6	165.6	165.3	169.5	169.5	169.9	169.5	169.6	169.8	165.96
	170.1	171.8	171.8	172.0	171.8	171'8	171.8	171.6	171.6	171.8	171.4	171.49
	173.4	173.4	173.4	176.9	173.6	169'4	169.4	169'4	156.1	149.6	139.5	169.74
	178 <b>.</b> 7	184'4 182'1	180 <b>·</b> 5 182 <b>·</b> 7	180°5 182°7	178 <b>·</b> 2 182 <b>·</b> 7	179 <b>°</b> 4 179 <b>°</b> 5	179°8 179°7	178 <b>.</b> 4 184.1	180'4 182'1	178°8 178°7	180°1 178°7	175°59 180°25
181.0	182.3	182.4	181.9	181.0	180.7	180.7	180.1	180.5	179.9	180.7	179.6	181.51
	172.4	174.3	174.5	174.5	174.7	_					— )	169.99
166.9	163.1	165.1	163.0	162.9	162.9	166°2 162°3	165°2 161°8	167.6 160.1	152°0 160°1	147°1 161°4	158·2 } 161·7	163.82
	166.4	166.4	166.7	166.7	168.2	168.8	170.4	170.8	171.3	170.6	171.0	166.87
	166.5	166.7	167.5	169'1	168.5	164'1	159.0	164.2	166.1	167.8	168.9	168.42
	172.7	173.0	173.0	173.9	175.1	174'1	174.2	174.2	174'6	174.8	174.8	173.07
180.8	184 <b>°</b> 9 195°5	184 <b>.</b> 5 195 <b>.</b> 9	184°2 186°7	184 <b>°</b> 2 176 <b>°</b> 4	176 <b>·2</b> 174 <b>·</b> 5	176.2	177.7	152.8	152.8	108.0	107.0	171.08
		-		_		b	<b></b> -b	—ъ	139.4	138.1	139.6}	180.17
	185.0	186.1	183.9	183.3	184.2	184.5	183'0	185.8	186.6	188.4	187:3	186.63
	190.0	190.1	190.1	190'8	190°5	188.7 184.0	192.0 184.3	192 <b>°</b> 0 184 <b>°</b> 3	194 <b>.</b> 4 190 <b>.</b> 6	194.5 190.9	194.7 193.2	189 <b>.</b> 52 191 <b>.</b> 49
183.9	185.7	185.7	185.7	186.0	182.8	182.7	188.6	188.6	186.4	185.8	185.7	187.37
179'6	180.4	180.6	184.3	182.4	182.6	180'4	179.2	179.6	180.6	182.2	182.8	180.88
175.6	174.5	174.6	176.3	175.6	175.6	180.6	 180°4	 179°7	 179 <b>·</b> 4	 174°3	$\frac{-}{169\cdot 8}$	176.49
172.64	172.86	172.85	172.84	172.97	172.82	170.85	171.47	171.77	171.40	170.87	170.93	172.46
		2,- 00							· · · · · · · · · · · · · · · · · · ·	110 01	1,0 30	1,2 10
	0 1	0 1	. 0					E MAGNET		0	0 1	•
59°5 60°5	59°0 60°5	58.7 60.0	58°8 59°8	58°4 59°6	58°2 59°4	58°0	57°4	57°1	56°8	56°4	55°6	58°41
_	_		—		—	57.4	57.4	57.0	56.4	56 <b>·2</b>	56.0	58.12
60.8	60.7	60.2	60.2	60.4	60.3	60.3	60.1	60.0	60.0	60.0	60.0	59.58
63.2	63.3	62.8 61.0	$62.5 \\ 61.0$	$62.3 \\ 61.0$	62°3 61°5	62'1 61'5	62°1 61°5	62.0	61.9	61.9	61.7	61.79
61.0	61·1	61.1	61.1	61.2	61.4	61.4	61.4	61.5 61.4	61.5 61.4	61.2 61.2	61.3 61.5	61°17 61°17
62.5	63.0	62.5	62.3	61.5	61.2	61.3	62.5	62.3	60.2	60.0	59.8	61.76
60.7	60.7	60.6	60.2	60.2	60.5	FC: F					55.8	59'34
56.9	57.0	57°0	56.9	56.7	56.4	56.5 56.2	56°2 56°0	56.0 56.0	56°0 55°4	$\begin{array}{c} 55.9 \\ 55.2 \end{array}$	55.8 J 55.1	56.32
54.6	55.0	54.8	54.6	54.8	54.8	54.7	54.7	54.6	54.4	54.5	54.2	54.88
55.0	55.0	54'2	54.2	53.8	54.1	53.4	53.2	53.0	52.8	52.8	52.1	54°14
53.2	52·3 52·2	52°0 52°0	51.7 51.5	51·2 51·3	51'2 51'3	50°6 51°3	50.2	49.5	49.2	48.7	48.7	51.71
57.2	56.9	56.6	56.4	56.5	26.0	JI J	51.3	51.3	51.2	51.1	51.4	50.92
-		_	_	_		57.8	57.6	57.5	57.2	57.1	5 <del>7</del> .0}	55.62
61.2	61.5	61.4	61.0	61.1	60.9	60.8	61.0	61.0	61.0	61.0	60.2	59.80
59.0	59°5	59°5	59'0 59'4	59°2 59°2	59.0 59.0	58.6 59.2	58°5 59°2	57.6 58.9	57°3 58°4	56°6 57°4	55°9 57°2	59°13
55.4	55°2	55.0	54.3	53.2	53.3	53.2	53.0	52.7	52.9	52.9	52.9	54.68
52.5	52.4	52.2	52.2	52.0	52.4	52.2	52.5	52.2	52.5	52.5	52.5	52.47
58.4	58.4	58 <b>·2</b>	57°5	56.9 —	56.2	b	b	b	55.2	56.4	57.5	56.35
54.5	54.0	53.7	53.7	53.7	53.0	52.4	52.0	51.8	51.5	51.2	50.4	54.46
49°2 48°5	49.0	48.6	48.4	48.4	48.0	47.4	46.6	46.1	45.6	45.4	44'8	48.84
50.2	48.5 49.8	48°2 49°5	47.7 50.0	47°4 49°9	47°2 50°0	47°3 49°8	47.2 49.2	47.0 49.2	47.0 49.2	47.0 49.3	47.0 49.2	46°85 49°11
53.4	53.7	53.4	53.5	53.4	53.2	53.1	53.0	52.6	52.6	52°4	52.2	52.50
55 to 1	56.0	55.2	55°4	55.2	55 <b>`</b> 2	 53 <b>·</b> 4	53.3	<u>-</u>	 53 <b>°</b> 9	<del>-</del>	<del></del> 53·7}	54.12
55.8			i									

	One	e Scale Divi	sion = •000	0066 parts o	f the <b>V. F.</b>		CAL FORC n Scale Divi		ponding to	l° decrease	of Temperat	ure, 1 • 64.	
Mean Göt gen Tim	tin-)	0h.	1 ^h .	2 ^h .	3h.	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9h.	10 ^h .	11h.
	1 2 3 4 5 6	Sc. Div. 173'9 171'7 164'4 166'6 172'7 177'7	Sc. Div. 173 '9 175 '0 164 '9 170 '2 173 '3 180 '2	Sc. Div. 172 6 175 0 161 5 165 0 172 2 173 7	Sc. Div. 166°7 173°3 162°6 167°4 171°7 176°2	sc. Div. 164 8 171 0 162 0 167 1 171 7 176 2	Sc. Div. 167 ° 0 171 ° 2 165 ° 7 165 ° 5 171 ° 7 176 ° 2	sc. Div. 169 8 170 8 166 8 166 2 171 7 176 2	Sc. Div. 169 8 169 8 166 8 167 9 172 1 175 4	Sc. Div. 171 *8 166 *9 170 *6 169 *6 173 *6 179 *2	sc. Div. 171 '8 166 '5 169 '3 169 '4 171 '6 178 '6	sc. Div. 172 7 165 1 167 9 166 6 172 5 176 9	Sc. Div 181'3 165'5 167'9 166'3 172'7
	7 8 9 10 11 12 13	179'9 172'6 173'5 180'2 180'8 180'5	179 '9 171 '6 175 '6 180 '2 184 '4 180 '5	178°1 171°5 175°5 184°0 184°4 180°3	177.4 171.5 175.3 182.5 179.0 180.3	177'9 171'2' 177'0 182'0 179'0 180'1	176.5 170.3 176.4 182.8 179.0 188.7	178 1 169 5 178 5 183 7 181 1 181 6	179°1 170°4 178°5 183°7 181°0 180°7	179.0 170.4 180.6 183.7 182.2 180.7	179 1 170 4 182 2 183 2 182 1 179 8	178 1 168 7 183 7 183 2 181 3 182 2	178.7 169.3 178.5 183.1 180.9 180.8
NOVEME	14 15 16 17 18 19 20 c	184.8 179.8 176.5 172.8 172.7 188.6	184.7 181.1 176.6 173.7 172.8 168.8	185.0 181.6 176.8 173.9 178.9 181.1	183°1 180°9 176°6 173°9 178°9 184°9	180°9 183°7 175°7 172°8 178°9 186°0	180.4 182.7 174.7 171.9 180.8 187.3	181.7 182.7 174.5 171.9 181.5 187.3	182.6 184.4 174.9 173.3 183.5 188.3	182.6 185.3 174.9 173.6 184.4 190.5	182.9 187.7 174.9 173.6 188.3 185.5	182.6 184.9 174.7 175.6 216.6 188.5	181.7 184.9 174.6 174.8 194.6 189.8
	21 22° 23 24 25° 26 27	188.4 185.7 175.6 174.1 179.2 186.5	187.0 185.4 175.6 174.0 177.2 187.1	187.0 185.5 175.7 174.0 184.5 188.0	187.4 183.7 175.2 172.4 185.7	185°5 183°4 171°4 170°6 186°4 190°4	185 · 2 181 · 5 173 · 5 172 · 2 187 · 5 193 · 0	185 '4 181 '5 176 '1 182 '1 191 '0 191 '3	180°0 181°6 178°1 185°3 189°7 190°7	183.7 181.6 179.4 189.6 189.7 193.9	180°2 178°3 179°4 193°3 191°9 193°8	225 · 4 178 · 3 176 · 9 204 · 5 193 · 4 195 · 0	224 4 178 2 175 7 201 7 192 7 198 4
- 1	28 29 30	205.2	205.3	202°4 196°6	205°7 198°1	205.2	205°2 199°0	205.3	204.0	202.8 198.8	201.6	200·5 197·8	200°8 197°8
lourly I	Means	178.97	179.67	179.25	178.89	178.61	179.18	179.59	179.90	180.67	180.62	181.23	180
					TEMPERAT	TURE OF TH	HE VERTICA	L FORCE N	MAGNET.		ı		
	1 2 3 4 5 6	53.6 57.2 59.0 58.4 56.0 51.5	53.8 57.2 59.0 58.0 54.4 52.1	54.0 57.2 59.0 58.0 55.0 59.2	54·1 57·7 59·0 58·8 54·5 52·2	54.8 58.7 59.0 59.0 54.5 52.2	55°2 59°2 59°2 59°2 54°6 52°4	55.7 59.3 59.6 59.3 55.0 52.0	56°2 59°6 59°8 59°4 54°7 52°3	56.8 59.8 59.8 60.0 54.9 52.4	57·2 60·2 59·9 59·8 55·2 53·2	57°7 60°5 59°8 60°0 55°6 53°6	57.8 60.6 59.8 60.0 55.8 53.4
	7 8 9 10 11 12 13	49.2 55.5 53.8 51.2 49.8 49.8	49.4 55.9 53.1 50.8 49.4 49.9	49.4 56.0 53.0 50.6 49.6 50.2	49.7 56.0 53.0 50.5 50.6 50.0	50.0 56.1 53.0 50.2 50.5 50.1	50°5 56°7 53°0 50°4 50°2 50°6	51.0 57.2 53.0 50.8 50.7 50.8	51.4 57.4 53.0 51.2 51.0 51.2	52.1 58.0 52.8 51.2 51.2 51.2	52°3 58°5 52°5 51°1 51°2 51°8	53°1 59°0 52°4 51°2 50°9 51°7	53.8 58.8 53.0 51.2 51.0 51.8
NOVEMI	14 15 16 17 18 19 20 °	47.5 47.5 53.0 54.3 52.7 43.7	47.6 47.4 53.0 54.2 52.4 43.6	47.8 47.4 52.9 54.1 51.2 44.0	48.0 47.8 52.7 53.3 50.5 44.2	48.4 48.0 52.7 53.6 49.8 44.6	49.0 48.2 53.4 53.9 49.8 44.9	49.2 48.6 53.8 54.0 49.2 46.2	49.3 49.4 54.0 54.0 49.0 46.0	49.4 49.6 54.5 53.8 48.8 46.4	49.4 50.2 54.4 54.2 48.6 46.6	49.4 50.4 54.6 54.2 48.4 47.0	49.2 50.4 55.1 54.4 49.4 46.4
	21 22 ° 23 24 25 ° 26 27	46.2 51.8 55.5 54.2 50.1 47.4	46.4 51.4 55.3 54.2 49.3 47.2	46.4 51.0 55.2 54.2 48.6 47.0	46.6 50.7 55.2 54.4 48.4 46.7	47.0 51.0 55.2 55.1 47.8 46.0	48.0 51.3 55.5 55.1 48.2 46.4	49°2 51°6 55°6 55°1 48°3 46°7	49.7 52.4 55.9 55.0 48.2 46.6	50°5 52°7 56°0 54°6 47°8 46°8	51 · 2 53 · 4 56 · 2 54 · 4 47 · 4 47 · 0	51.7 54.0 56.2 54.8 47.4 47.2	53.8 54.2 56.4 54.4 47.8 46.4
	28 29 30	35.8 37.1	35.8 32.1	35.9 38.5	35°9 37°6	35°4 38°1	36.1 —	36.3 36.3	36.8 39.6	37.5 40.0	38.1 -	38.6 40.0	38.8
Iourly I	Means	51.50	51.03	51.33	51.00	51.05	51.39	51.60	51.84	52.02	52.24	52.43	52.5

^{*} Fifteen minutes late.

	One Seele	Division —	•000066 pa	rts of the V		RTICAL F		orresponding	r to 1º decre	ease of Tem	perature, 1°	34.
12h.	13h.	14h.	15h.	16h.	17h.	18h.	19h.	20h.	21h.	22h.	23h.	Daily and Monthly Means.
sc. Div. 189 5 166 2 166 1 166 2 172 9	Sc. Div. 211 ° 2 166 ° 0 166 ° 0 166 ° 2 173 ° 6	sc. Div. 194.4 166.4 166.0 166.3 173.6	Sc. Div. 164 6 167 4 163 1 166 3 173 2	Sc. Div. 166 3 167 4 163 3 166 9 173 2	Sc. Div. 175 ' 7 165 ' 1 164 ' 5 167 ' 6 173 ' 2	Sc. Div. 177 8 163 5 164 5 167 9 174 4	sc. Div. 171'4 164'0 149'5 170'3 174'3	Sc. Div. 164'2 164'3 153'1 171'2 174'4	sc. Div. 169 '9 164 '3 160 '8 171 '2 175 '8	Sc. Div. 169 '9 156 '5 162 '4 171 '2 165 '3	Sc. Div. 169 ' 7 156 ' 3 166 ' 6 171 ' 7 174 ' 8	Sc. Div. 174°20 167°05 164°01 167°95 172°76
177.6 174.2 172.3	177.6  174.8 177.0	178·2  175·9 177·0	178'3  175'8 173'6	178°3 175°8 173°6	178°8 	178°9 165°2 173°6	183°3 170°3° 173°7	178°9 170°3 173°8	181·2 171·7 176·0	179°3 171°5 175°9	$\begin{bmatrix} -7 \\ 179.9 \\ 171.7 \\ 174.8 \end{bmatrix}$	178°11 175°54 172°58
179°2 183°1 180°2 182°9	181.6 183.1 180.2 181.6	181.6 183.1 180.2 181.2	181.8 182.9 179.4 181.2	179°1 182°5 177°3 181°2	179°1 180°7 176°1 180°9	174.5 182.1 173.6	172.3 182.1 173.5	177.7 182.2 177.2	179.4 182.7 177.2	179.4 181.8 179.2 —	179.8 180.0 179.5 	178°37 182°44 179°53 181°18
181.7 185.0 173.0 174.2 189.8	182.8 185.0 173.0 175.0 198.4	184.2 184.5 175.6 172.6 190.5	184.2 183.4 174.7 173.7 193.4	184.5 183.3 174.3 173.2 199.2	184.7 181.4 172.6 173.2 191.0	184.4 184.7 180.5 173.0 171.4 191.0	184.4 182.7 178.8 172.8 172.5 191.0	177.6 182.3 177.8 172.8 173.6 191.0	178 · 1 182 · 3 176 · 1 172 · 8 172 · 0 191 · 0	178 · 1 182 · 3 176 · 1 171 · 8 175 · 3 191 · 0	182.8 176.6 171.3 172.8 191.0	183.01 182.01 174.30 173.39 188.34
189 · 8 190 · 8 178 · 0 176 · 8 204 · 8	192°3 	191 · 2 	191°2 	191.4 	191.4 	188.5 171.5 176.4 181.8 177.7	187.8 184.3 176.3 176.2 177.7 188.6	187.8 181.2 176.1 177.8 176.8 185.8	188.4 177.4 176.4 182.4 178.6 185.4	188.4 179.7 175.6 178.6 179.9 185.3	188.4 179.7 175.6 178.7 179.2 185.8	187.76 184.28 179.46 176.43 184.57 187.89
187 · 2 196 · 7 201 · 1 196 · 0	196.8 193.1 202.1 196.0	197.6 193.1 202.1 196.4	184'3 192'9 202'6 196'4	186.7 192.9 ———————————————————————————————————	188.1 193.0 203.0 197.4	188'8 	204.7 202.2 197.5	204.7 202.2 195.3	204·3 202·5 195·2	206 '4 203 '1 190 '7	205.8 203.1 194.6	195°38 203°04 197°43
180*43	182.41	181.20	179.56	179.13	179.28	179.66	178.80	178.45	179.51	178.55	179.27	179.76
				TEMPER.	ATURE OF	THE VERTI	CAL FORCE	MAGNET.				I.
58·2 60·2 59·8 60·0 55·1 53·2	58°2 60°2 59°8 60°0 54°9	58.2 60.1 59.8 59.4 54.8 52.6	58.0 60.0 60.0 59.0 55.0 52.4	58.5 60.0 60.0 58.9 54.7 52.0	58.8 60.0 59.9 58.4 54.4 51.7	58.8 59.8 59.8 58.0 54.2	58.0 59.6 59.7 57.3 54.0	57.4 59.5 61.0 57.1 53.8	57·3 59·2 60·0 56·8 53·6	57·2 59·2 59·3 56·5 53·0	57.0 59.2 59.0 56.2 52.2	56.77 59.34 59.63 58.65 54.56
53.4 58.2 53.0 51.2 51.1	53.0  53.4 57.5 52.9 51.0 51.0	53.7 57.2 52.5 50.9 51.0	54·2 57·2 52·1 50·8 50·8	54°1 57°0 52°1 50°6 51°4	54.0 57.0 52.1 50.6 52.0	48.4 54.1 56.5 52.1 50.5 52.0	48.4 54.2 54.9 52.2 50.8 50.7	48°4 54°1 54°7 52°2 50°7 50°4	48.4 54.2 54.2 52.0 50.2 50.1	48.5 54.2 53.8 51.7 50.2 49.6	49.0 } 55.0 54.0 51.5 50.2 49.6	51.77 52.51 56.54 52.58 50.75 50.66
51'4 49'2 50'4 55'6 54'6 50'0	51.4 	51.0 48.5 51.2 55.7 55.6 47.5	50°3 48°2 51°4 55°5 55°0 47°4	50°2 48°0 51°5 55°4 54°8 46°6	49.8 48.0 52.0 55.4 54.8 46.2	47.3 47.8 52.5 55.3 54.5 45.7	47.2 47.8 52.3 55.2 54.3 45.4	47.8 47.8 52.5 55.2 54.1 45.0	47.5 47.7 52.6 55.2 53.6 44.4	47.5 47.6 52.8 55.0 53.1 44.2	$\left\{ \begin{array}{c} - \\ 47.5 \\ 47.5 \\ 52.9 \\ 54.7 \\ 52.7 \\ 44.2 \end{array} \right\}$	49:92 48:37 50:32 54:50 54:16 48:12
45.8 54.8 54.4 57.0 55.0	45.4 54.5 54.7 56.5	45.4 54.2 55.0 56.3	45.4 54.0 55.2 56.0	45°2 54°8 55°4 55°9	45°1 55°0 55°4 55°7	45°1 55°0 55°4 55°5	45.0 55.0 55.3 55.2 54.0	45.0 54.0 55.2 55.2 53.7	44.9 53.6 55.0 54.6 52.8	45.1 53.0 55.3 54.2 51.6	45.6 52.2 55.5 54.0 50.5	45°27 51°53 53°64 55°60 54°28
38.8 41.1	55.7 47.8 45.4 — 38.4 41.2	55°2 47°9 45°5 — 38°1 41°2	55°1 47°4 45°4 — 38°6 41°2	55.0 47.8 45.4 ——————————————————————————————————	54.4 48.2 45.0 — 38.3 40.6	54.2 47.7 — 36.1 38.3 40.6	36.0 38.3 39.7	35 4 35 4 38 1 39 6	35·3 37·9 40·6	35.5 37.7 40.4	30 5 46 8 — 35 6 37 2 40 3	37 47 37 47 59 72
52.63	52.42	52.33	25.55	52.16	52.10	51.34	51.04	50.95	50.74	50.28	50.21	51.61

	On	e Scale Divi	ision = •00	0066 parts o	f the V.F.		CAL FOR in Scale Div		esponding to	1º decrease	of Tempera	iture, 1°64.	
Mean (	Göttin-}	0 ^h .	1 ^h .	$2^{ m h}$ .	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7h.	8 ^h •	9 ^h .	10h.	11h.
	( 1 2 3 4 5 5	sc. Div. 195 ° 7 185 ° 9 184 ° 5 189 ° 2	Sc. Div. 195 '7 184 '8 184 '5 189 '2	Sc. Div. 195 '7 186 '7 186 '8 186 '2	Sc. Div. 196°8 184°3 185°8 189°1	Sc. Div. 195°2 184°3 185°1 189°1	Sc. Div. 193°2 184°3 185°1 190°4	Sc. Div. 193°2 182°7 185°1 190°4	Sc. Div. 193°2 185°8 187°0 192°5	8c. Div. 191.5 185.8 188.7 192.5	:sc. Div. 189 5 187 5 189 7 192 5	sc. Div. 188°2 194°2 189°7 192°5	Sc. Div. 187'8 192'9 189'7 192'7
	6 7 8 9 10 11	194.6 190.6 174.5 176.6 171.2 167.9	194.6 190.6 179.1 176.6 171.0 169.0	194.6 189.9 182.2 178.5 172.4 169.2	194.6 189.7 183.3 178.5 173.2 171.8	191.6 189.4 183.3 179.6 172.8 170.7	191.6 188.7 184.7 180.1 172.8 173.6	190.6 188.2 183.7 180.4 171.8 175.5	190.6 186.0 183.7 181.3 172.1 176.5	190°2 184°5 184°4 183°0 170°3 180°3	189 · 4 183 · 3 183 · 9 181 · 9 176 · 7 179 · 4	189.4 182.4 182.2 179.8 176.7 179.4	187.7 182.2 182.2 179.3 178.9 180.2
DECEMBER.	12 13 14 15 16 17 18 ^b	182°3 180°8 183°1 191°1 183°7 196°5	182°3 181°9 182°4 189°7 181°5 194°9	181 '4 184 '1 182 '5 191 '6 193 '0 194 '5	181'3 184'4 183'5 192'8 188'7 195'4	179 ° 9 183 ° 5 181 ° 7 193 ° 1 190 ° 7 197 ° 1	180°4 183°5°a 180°7 191°4 186°5 196°2	181 · 3 182 · 5 181 · 8 191 · 4 194 · 9 197 · 1	181 · 2 182 · 5 183 · 1 191 · 4 207 · 9 197 · 7	181.6 182.5 183.6 191.4 216.2 200.1	181.0 184.5 183.8 191.4 203.1 201.6	180°9 183°8 183°6 191°9 206°4 197°6	179'9 185'8 183'4 190'8 195'6 197'6
	19 20 ^b 21 22 23 24 25 ^d	85.0 214.1 203.9 192.9 197.9	76°3 213°5 204°1 193°3 197°9	160°9 212°0 203°0 194°4 201°1	156°4 211°6 200°7 198°6 200°5	209.7 211.8 201.5 198.3 198.4	234.0 211.8 202.7 198.4 198.3	234·5 212·3 201·7 197·5 198·3	221°3 212°2 203°5 200°5 199°1	246°1 210°8 203°0 202°8 200°7	237·8 209·6 201·4 203·4 199·3	239·1 209·6 201·7 203·7 199·3	235.7 209.6 198.5 200.6 199.0
	26 27 28 29 30 31	206°1 198°1 185°8 180°6 173°8	206·1 196·4 185·8 180·0 172·4	206.0 196.4 185.8 179.6 173.9	206.0 196.7 183.7 178.6 173.7	204.0 195.0 178.0 176.5 172.4	203.0 194.8 181.3 175.4 172.4	203·1 193·7 181·3 176·2 173·2	204·3 193·7 181·3 177·4 173·2	205 ° 6 195 ° 0 196 ° 0 178 ° 0 174 ° 8	205 · 6 192 · 7 185 · 8 176 · 9 173 · 5	205·2 192·7 182·8 176·9 172·6	205.0 192.3 180.9 174.5 172.6
Hourly	Means	187.71	187.60	188.62	188.66	187.75	187.71	187.95	189:17	190.55	189.41	189.40	188.42
	$\left( egin{array}{c c} 1 \\ 2 \\ 3 \\ 4 \end{array} \right)$	40°4 46°8 47°3 45°0	40°2 47°0 47°2 44°6	40°4 46°5 46°4 44°3	40°9 46°4 46°4 44°3	41°5 46°4 46°4 43°9	42°2 46°4 46°5	42.6 46.8 46.6	42°7 47°4 46°5 44°2	43.2 47.6 46.4	44.0 48.2 46.3	44·2 48·2 46·2	45°0 48°1 45°7
	5 6 7 8 9 10 11	41.5 43.4 47.0 51.1 53.8 52.0	41.7 43.7 46.9 51.4 54.1 51.5	41.4 43.5 46.6 50.6 53.6 51.5	41°4 44°3 46°7 50°3 53°6 51°7	42·2 44·5 47·2 50·2 53·5 51·3	44.3 42.9 45.0 47.7 50.3 54.2 51.6	44.3 44.1 45.3 48.0 50.4 54.4 51.8	44 2 44 4 46 0 48 4 50 4 54 8 52 1	44.1 44.5 46.4 48.6 50.0 54.7 51.9	44.4 44.6 47.6 49.2 50.2 55.0 52.0	44.6 44.6 48.2 49.4 50.4 55.0 52.0	44.4 45.1 48.4 49.4 51.0 55.0 52.0
DECEMBER.	12 13 14 15 16 17 18 b	48.4 47.6 47.6 42.2 39.8 40.2	48.5 47.4 47.4 42.4 39.8 40.0	48.4 46.9 47.2 42.3 39.1 39.8	48°3 46°6 47°2 40°8 39°0 39°6	48·3 46·8 47·4 40·0 39·0 39·6	48.5 47.4 47.8 39.8 39.0 39.8	48.6 47.6 48.0 39.8 39.3 40.3	48.7 47.8 47.7 40.1 39.5 40.8	48.7 48.0 47.4 40.3 40.2 41.2	48.7 48.0 47.5 40.5 40.2 41.7	49.4 47.5 47.6 41.2 42.0 42.2	49.2 47.2 47.4 41.0 43.9 42.1
	20 b 21 22 23 24 25 d 26	42.2 35.4 38.8 42.4 40.0	42.2 36.1 38.7 42.6 39.8	41·2 35·9 38·8 41·7 39·8	40.6 35.7 38.5 40.9 40.0	40.0 36.0 38.9 40.4 40.1	39.4 36.3 39.1 40.4 40.2	39°3 36°3 40°0 40°4 40°1 —	39.8 36.8 40.0 40.0 40.3	40.0 37.0 40.4 39.7 40.3	39.8 37.3 40.9 40.3 40.6	39.7 37.5 41.6 40.3 41.0	39.0 37.3 42.7 41.0 41.4
	27 28 29 30 31	33·1 38·0 44·5 49·4 52·4	33.5 38.1 44.5 49.4 52.4	33.6 38.3 44.4 50.0 53.0	33.4 38.8 44.9 50.0 53.0	33.4 39.1 45.9 50.1 52.8	33.8 39.3 46.5 50.9 52.7	34.0 39.6 47.2 50.8 52.5	34.1 40.0 47.6 51.0 52.5	34.2 40.4 47.9 51.2 52.5	34°3 41°0 48°4 51°2 53°0	34.0 41.4 48.4 51.3 53.2	34·2 41·5 48·5 51·6 53·2
Hourly	Means	44.20	44.24	44.34	44.30	44.39	44.70	44.94	45.12	45.23	45.26	45.80	46.01

^a Two minutes late.

b Omitted in the Means, on account of disturbance.

	One Scale	Division =	: '000066 pa	arts of the V		RTICAL I se, in Scale		orresponding	g to 1° decre	ase of Tem	perature, 1·6	4.
12 ^h .	13 ^h .	14 ^h .	15h.	16 ^h •	17h.	18h.	19 ^h .	20h.	21 ^h .	22h.	23 ^h .	Daily an Monthly Means.
Sc. Div.	Sc. Div. 188'8	Sc. Div. 190.5	Sc. Div. 187.1	Sc. Div. 189°1	Sc. Div. 189'1	Sc. Div. 189'1	Sc. Div. 189'4	Sc. Div. 182 4	Sc. Div. 189'8	Sc. Div. 189°2	Sc. Div. 185 9	Sc. Div. 190.56
198.8	200.0	196.2	202.6	202.4	195.7	195.7	188.8	168.2	181.6	184.8	185.0	189.14
189.7	191.5	191.6	193.6	193.6	193.8	192.9	190.4	190.4	190.0	189.6	190.1	189.15
192.8	192.4	192.4	193.3	191.8	191.8					10710	194.6}	192.09
-	100.1	100:1	-	107:0	107:0	195.4	192.8	194.4	196°7 189°4	$195.3 \\ 189.2$	194.6 )	189.89
186'9 181'5	188'1 181'5	188'1 183'6	187.8 187.0	187.8 185.3	187.8 185.3	185°1 183°5	188.7 187.8	189 <b>.</b> 4 187.7	183.4	180.7	179.1	185.21
180.4	180.4	182.3	183.4	183.4	180.8	181.1	175.7	178.6	178.0	177.8	174.8	181.00
179.3	177.0	177.0	178.7	177.6	177.6	176.2	174.7	169.5	170.0	172.1	171.2	177:37
78.9	181.6	184.4	183.8	176.3	175.0	170.6	173.8	176.4	177.7	172.9	168.1	174.97
179'4	180.8	182.1	182.3	182.3	182.3						183.1	178.42
						183.3	183.3	183.3	183.3	183.1		
79'9	181.2	182.0	182.7	182.7	182.7	182.7	182.9	182.9	180.7 182.2	180°8 182°9	183.1 180.8	181.48 183.07
84.2	184.5	182 <b>·</b> 8 179 <b>·</b> 9	182 <b>.</b> 8 182 <b>.</b> 5	183°1 183°7	182°0 184°0	182°0 184°0	182 <b>.</b> 6	181.6 186.4	184.6	186.8	189.1	183 49
83.4 90.5	179 <b>·</b> 9	193.7	192.9	192.9	192.9	192.9	192.9	192.2	187.8	182.9	187.9	191.5
97.8	194.8	196.2	192 9	192 9	196.3	192.4	198.2	196.2	197.5	191.1	191.1	195.6
96.7	195.2	195.3	193.2	192.7	190.7		_	-			1 13	170.39
					_	62.0	109.2	139.8	— с	22.0	55.0}	
51.1	264.5	258.2	255'1	225.8	225.5	224.6	220.3	214.2	215.5	214.5	214.5	213.3
09.3	209.6	209.6	210.0	210.0	210.0	208.3	208.7	207.6	206.5	204.4	203.9	209.8
99.4	199.0	198.8	198.2	199.4	198.4	198.0	195.6	192.3	193.4	192.1	192.9	199.3
99.0	200.8	200.8	198.8	198.4	199.5	199.4	197.7	197.7	197.7	196.6	197.2	198.6
99.3	197.5	196.0	196.2	197.6	197.6	_		_		_		201.02
_	•	_	_			$\frac{-}{208.7}$	209.4	209.4	208.7	207.9	206.2	
05.1	204.9	205.0	205.3	204.7	204.7	$\frac{203}{204} \cdot 7$	203.5	203.5	201.6	199.4	199.3	204.2
92.2	190.8	189.6	189.6	189.6	188.9	188.1	186.8	186.7	186.7	184.9	184.9	191.5
81.4	182.3	183.6	182.6	182.1	182.3	181.1	178.5	180.6	180.6	180.6	180.6	182.70
74.5	174.6	175.7	175.0	175.0	175.0	175.0	174.7	174.7	174.4	174.4	173.6	176.13
73.9	173.3	173.3	173.3	173.3	173.4	173.4	173.3	173.3	173.3	171.0	169.8	173.0
88.24	188.61	188.98	189.52	189.13	188.62	188.20	188.18	186.93	187:33	186.27	185.92	188.3
					ATURE OF	THE VERT		E MAGNET.				0
45.2	45°4	45.5	45°4	45°7	46°4	46.5	$4\r{6}$ .0	46.5	46.2	46°0	46°6	44°11
47.9	47.7	47.5	48'0	47.8	47.3	47.0	47.2	47.4	47.4	47.2	47.3	47.31
45.4	45.4	45.2	45.2	$45^{\circ}2$	45.0	45.0	45.3	45.0	45.0	45.0	44.8	45.8
44.4	43.8	43.8	44.0	43.7	43.6		41.0	40:0	40:6	41.0	$\{\frac{-}{41\cdot7}\}$	43.4
10:0	45.0	- I	45:0	45.3	45.4	41.0 45.6	41.0 44.5	$\begin{array}{c} 40.8 \\ 44.2 \end{array}$	40.6 43.7	43.5	43.4	44.0
46°3 48°2	45.6 48.3	45.6 48.2	45°6 47°6	45 3	47.2	46.8	46.4	46.7	47.0	47.0	47.0	46.4
49.8	20.0	49.8	50.0	20.0	50.0	20.0	50.5	50.4	50.7	51.0	51.1	49.0
51.2	51.4	51.2	51.6	51.9	52.0	52.3	53.0	53.7	54.0	54.0	53.8	51.5
55.0	55.1	55.2	54.6	54.3	54.1	54'1	54.0	53.2	53'0	52.7	52.3	54'1
51.7	51.2	50.8	50.2	50.0	49.5						47.9}	50.4
_						47.4	47.4	47.4	47.5	47.6		48.2
49.2	49.0	48.5	48.2	48.0	47.6	47.5	46.7	46.5	47.4	47.6	47.4 47.6	47.43
47.1	47.3	47.4	47.4	47.3	47.6	47.6 45.0	47.6 44.0	47°4 44°3	47.6 44.0	47°6 43°4	42.8	46.4
47°3 41°4	47.2	47.4	$\begin{array}{c} 47.4 \\ 42.2 \end{array}$	46.5 41.7	45'9 41'6	43 0	41.6	40.8	40.3	40.2	40.0	41.0
43.6	41.6 43.5	41.6 42.8	41.8	41.4	41.3	41.5	40.4	40.4	40.3	40.0	39.8	40.7
42.2	42.3	42.8	42.7	42.8	43.0						— 1	41.3
_ '		l —				39.8	40.6	42.3	— с	42.6	42.6	
38.1	38.0	38.4	38.0	38.0	37.1	36.6	35.9	35.7	35.0	34.3	34.6	38'4
37.0	36.6	36.4	36.6	36.3	36.1	35.7	36.1	36.9	37.7	38.1	38.4	36.6
43.4	43*3	42.4	42.2	42.2	42.2	42.2	42.2	42.5	42.4	42.7	42°2 39°7	41°1 40°7
41.6	41.2	41.2	41.0	40.8	40.8	40.5	40.5	40.3	40.3	40.0		40 /
41.8	41.6	41.4	40.8	40.3	40.0		_	_	_		$=$ $\}$	38.3
_	_	_		_	_	31.1	31.4	31.6	32.0	32.6	33.1	
34.5	34.0	33.9	34.1	34.1	34.0	34.0	34.3	34.9	36.1	37.1	37.3	34.3
41.7	41.9	42.2	43.3	43.6	44.0	44.3	44.5	44.6	44.6	44.8	44.3	41.6
	49.3	49.3	49.2	49.0	48.7	48.6	48.9	48.8	49.1	49.0	49'1	47.7
49.0		20.0	1 70.0	52.2	52.2	52.2	52.2	52.4	52.6	52.7	52.7	51.4
49°0 52°0	52.3	52.2	52.2									
49.0	52·3 53·2	52.7	52.8	52.8	52.6	52.6	53.5	53.1	53.0	53.5	54.2	52.9

	Or	ne Scale Div	ision = ·00	0066 parts o	of the V. F.		CAL FOR n Scale Div		sponding to	1° decrease	of Tempera	ture, 1°64.	
Mean G gen Ti	öttin-}	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8 ^h •	9 ^h .	10 ^h .	11h.
(	1	Sc. Div. 169*8	Sc. Div. 169.8	Sc. Div. 170°9	sc. Div.	Sc. Div. 168*8	Sc. Div. 168*8	Sc. Div. 169°7	Sc. Div. 170°4	Sc. Div. 170°4	Sc. Div. 170°4	Sc. Div. 170°4	Sc. Div 170°4
	2 3 4 5 6 7	183.5 176.7 190.8 192.3 198.4	182.8 181.5 190.8 194.2 198.2	174.7 182.9 191.6 196.4 197.2	181°1 185°3 191°5 195°1 195°3	178°2 184°5 190°3 195°1 195°0	179'4 181'7 190'3 194'2 197'2	181.9 183.0 192.5 195.6 198.0	182.4 184.0 190.5 195.6 198.4	182.7 186.3 187.9 195.3 197.7	184.5 186.0 186.7 194.6 196.9	185.6 186.0 185.0 194.6 197.7	184°3 185°8 184°9 194°6 199°5
	8 9 10 11 12 13	194.1 209.8 207.3 189.6 190.2 177.9	193.8 212.1 207.3 193.1 188.3 179.8	195.6 212.1 210.0 196.4 186.9 180.9	192.6 210.4 209.1 189.6 186.2 181.1	190°9 207°0 210°0 190°7 188°8 180°9	191'4 209'4 210'0 193'6 189'2 180'8	190'8 209'4 209'1 201'3 188'7 180'8	190°3 209°1 205°1 196°9 188°3 180°8	189'4 209'3 203'3 203'2 193'1 183'6	188.8 209.3 203.3 199.2 208.7 184.8	188.8 	187.8 208.3 202.8 197.8 200.2 184.2
JANUARY.	15 16 17 18 19 20 21	177 · 2 186 · 5 188 · 8 198 · 7 186 · 9 179 · 8	177.2 186.5 188.8 198.7 186.7 180.3	177.2 189.7 189.8 198.7 185.4 181.3	177.2 185.9 187.6 197.6 186.3 178.0	174.7 186.9 188.7 193.5 186.3 178.0	175 · 9 188 · 3 188 · 8 196 · 7 185 · 9 178 · 0	175 '9 — 190 '0 192 '2 197 '9 186 '6 177 '3	175 · 2 190 · 8 193 · 9 195 · 9 185 · 5 178 · 2	174.8 189.2 192.6 196.8 184.5 178.5	174 · 2 189 · 2 191 · 4 196 · 0 184 · 2 180 · 0	172.2  188.2 193.2 196.2 181.5 179.8	172.2 185.3 192.3 198.6 182.5 181.1
	22 23 24 25 26 27 28 29	186.4 	186.5 	189'1 184'6 186'8 175'0 175'3 175'5 184'8	188.6 	188.4 ————————————————————————————————————	187.5 186.4 182.8 178.1 174.4 172.4 181.8	187.9 	187.8 190.0 184.2 179.4 174.5 177.4 186.7	188.8 	188.8 	187.7 189.4 183.9 181.8 173.8 178.1 182.5	186.5 189.6 182.9 179.2 173.6 178.1 182.5
	30 31	187.2	187.2	186.9	187.1	 184°4	183.2	185.4	185.4	184.2	182.4	179.7	179.7
lourly	Means	186.11	186.54	187.53	186.73	186.13	186.40	187.64	187.57	187.90	188.11	187.58	187.1
					TEMPERAT								
	$\begin{bmatrix} 1 \\ 0 \end{bmatrix}$	54.4	55.0	54.2	54.3	54.2	54.6	54.6	54°6	54.5	54.5	54.3	54°4
	2 3 4 5 6 7 8	45.8 47.6 42.2 39.9 36.9 39.9	46.0 47.3 42.0 39.5 37.1 39.5	46.5 46.5 42.0 39.0 37.1 39.8	46.4 46.5 41.7 39.0 37.2 40.0	46.4 46.4 41.6 39.1 37.1 40.0	46.2 47.0 41.9 39.4 37.3 40.6	46.4 46.4 42.1 39.7 37.8 41.0	46.4 46.5 42.7 39.6 38.1 41.5	46°3 46°4 43°7 39°6 38°1 41°5	46.3 46.3 44.4 39.5 38.1 42.4	46.7 46.4 45.6 39.5 38.1 43.0	47.2 46.0 45.7 39.8 37.3 43.4
RY.	9 10 11 12 13 14 15	28·1 25·6 35·0 41·6 47·4 49·6	27·2 25·7 34·7 42·3 47·4 49·7	27·1 27·0 36·0 42·0 47·4 49·7	26.9 27.0 35.4 42.0 47.2 49.6	26·3 27·1 36·1 42·3 47·4 50·0	27·2 27·3 37·1 42·6 47·6 49·8	27.7 28.0 38.0 43.0 47.8 50.2	28·2 29·2 38·8 43·4 48·0 50·5	28·3 30·0 39·3 43·4 47·7 50·9	28.7 31.0 39.5 43.6 48.4 51.4	29.0 31.7 40.0 44.2 48.4 52.1	29.2 32.0 40.0 44.5 49.0 52.2
JANUARY.	16 17 18 19 20 21 22	43.8 43.1 36.2 42.9 46.7 42.4	43.8 42.9 36.1 43.5 46.5 42.6	45.0 42.6 36.1 43.0 46.5 41.9	44.4 42.4 37.2 43.1 47.2 41.6	43.9 41.6 37.8 43.4 47.4 41.4	43.7 41.5 38.3 44.4 47.8 41.7	43.7 41.2 38.3 44.7 48.4 42.1	43.5 40.9 38.5 44.8 48.7 42.2	43.5 40.9 38.8 45.3 48.9 42.0	44.0 41.1 38.8 46.5 49.3 42.3	44.4 41.4 39.1 47.2 49.2 43.0	45 ( 40 '4 39 '1 47 '3 48 '4 43 '3
	23 24 25 26 27 28 29	37·9 43·4 49·4 50·2 48·0 47·4	38·1 43·6 49·5 50·0 48·0 47·4	38·3 43·5 48·8 50·0 48·0 46·7	38.0 43.8 48.3 50.2 48.4 46.4	38.8 44.3 47.7 49.8 48.8 46.6	40°0 45°0 48°3 50°0 49°5 46°6	40°4 45°2 48°6 50°9 49°6 46°7	40.6 45.7 48.5 51.2 49.7 47.2	41.0 46.2 48.4 51.2 49.5 47.3	42.4 46.6 48.5 51.7 49.5 47.2	43.0 47.3 49.2 51.7 49.5 47.4	43:3 47:4 49:2 51:8 49:2 47:6
l	30 31	43.4	43.5	43.5	43.6	43.7	44.6	44.6	44.7	45.2	46.0	46.9	47.2
<del></del>	Means	42.65	42.65	42.62	42.61	42.66	43.08	43.35	43.60	43.77	44.12	44.55	44'(

	One Scale	Division =	·000066 pa	rts of the V		RTICAL I se, in Scale		orrespondin	g to 1° decre	ease of Tem	perature, 1°	34.
12h.	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17h.	18h.	19 ^h .	20h.	21h.	22h.	23h.	Daily and Monthly Means.
Sc. Div. 70.5	Sc. Div.	Sc. Div. 170'9	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
_						183.4	183.4	182.8	182.8	182.8	183.5	173.68
84.3	188.8	184.9	189.8	187.8	186.3	182.9	179.5	169.9	167.7	170.4	169.3	180.95
85.8	187.8	187.2	186.9	186.8	187.8	188.6	189.8	189.8	189.8	189.5	189.5	185.96
84.9	187.4	187.4	188.9	191.3	191 3	191.3	191.7	191.7	191.8	191 4	191.3	189.72
94.7	195.2	195.7	195.7	196.1	195.7	195.7	196.5	198.4	198.4	199.3	197.7	195.70
99.5	198.9	198.9	199.5	199.3	199.3	197.3	195.2	196.1	195.2	192.1	192.8	197:26
88.0	187.6	188.2	188.1	188.2	188.2						. 1	
_						207.4	207.6	207.8	209.3	204.9	$_{205\cdot 2}\}$	194.37
207:3	207:3	208.7	208.7	208.3	206.6	207.3	208.9	211.5	212.2	211.7	211.7	209.42
6.10	200.9	210.2	217.2	$227 \cdot 2$	209.4	203.5	203.2	178.4	177.0	179.6	188.8	203.24
97.5	194.8	194.8	194.7	195.1	195.1	195.2	189.5	189.0	185.1	185.0	189.4	193.93
200.5	189.3	189.2	184.4	183.4	184.0	182.7	182.0	181.2	180.2	180.3	180.2	188.85
89.1	188.3	183.5	179.0	175.9	175.6	175.6	177.2	176.6	176.8	173.1	176.2	180.29
72.2	173.0	173.0	172.8	173.1	173.6						1	
		1.00				185.4	185.4	183.9	183.6	186.2	$\frac{-}{186\cdot 2}\}$	177.18
84.0	186.8	185.8	186.2	187.7	187.7	188.0	188.4	188.3	188.3	188.3	189.6	187.73
93.2	195.7	195.7	195.8	195.8	195.7	195.8	197.2	198.6	198.6	199.6	198.7	193.70
4	193 7	193 7	195.1	194.0	194.2	192.3	$\frac{197.2}{189.1}$	182.3	180.8	183.3	185.0	193.49
94.0			180.8	179.8	179.8	175.6	$\begin{array}{c} 189.1 \\ 177.2 \end{array}$	182 3 177 6	178.0	179.2	179.8	182.26
82.6	180.8	180.8							186.3	186.3	186.5	181.80
82.5	184'3	182.9	182.3	183.0	184.3	184.7	186.3	186.3	100 9	100 0	100 4	
87.3	188.9	189'9	191.3	190.2	191.7	107.7	197.7	197.7	193.9	193.9	188.2	190.10
			10010	100:0	10010	197.5						188.57
92.7	192.1	191.2	190.8	190.8	190.8	190.6	188'8	188.7	188.7	188.7	187.8	
82.9	182.6	183.8	178.5	178.5	178.5	177.9	177.1	177.1	175.6	175.6	174.3	181.57
78.7	179.2	180.8	180.5	178.4	177.4	177.4	177'3	174.6	174.2	173.4	173.4	177.59
73.2	173.0	173.0	173.0	173.0	165.8	164.5	170.6	173.0	162.4	175'1	176.2	172.66
97.2	211.3	219.2	187.8	189.8	172.2	183.6	189.6	167.1	169.9	169.3	154.0	180.27
82.5	182.3	182.3	182.3	182.5	182.6						185.8	183:14
			_			186.4	186.8	181.9	188.9	188.2		
79.7	179.5	179.5	183.1	184.0	184.0	183.7	184.3	184.3	184.3	183.7	185.0	183.69
87.95	188.20	188.91	187.93	188.12	186.2	188.24	188.48	185.96	185.41	185.82	185.61	187.20
		- 0		TEMPER		THE VERT	ICAL FORC	E MAGNET.		0	1 0 1	0
54.2	$5\mathring{4}^{\circ}0$	54°0	53°8	53.7	<b>5</b> 3°6						- 7 l	52.25
				_		46.0	46.0	46.0	46.2	46.4	46.4	
47.4	47.9	47.4	47.8	47.8	48.0	48.2	48.0	48'1	48.3	48.6	48.4	47.19
45.3	45.0	44.6	44.6	44.2	44.2	43.3	42.6	42.1	42.1	42.2	42.3	45.07
45.0	44.4	43.2	42.4	41.5	41.1	41.1	41.0	40.5	40.5	40.4	40.0	42.36
39.2	39.0	38.2	38.0	37.8	37.8	37.6	37.1	36.4	36.0	36.2	36.6	38.49
37.2	$\frac{38.0}{0}$	37.8	38.1	37.0	37.1	37.3	38.1	39.0	$\frac{39.2}{39}$	$\frac{39.7}{39.7}$	39.8	37.88
43.6	43.8	43.9	44.0	43.6	43.4				- 33 2			
-0	10 0	100				30.3	29.8	29.3	29.0	29.0	$\frac{-}{28.8}$	38.80
29.3	29.8	29.6	29.2	29.2	29.4	29.0	28.1	26.4	26.1	$25\cdot 2$	25.3	27.94
32.8	33.2	34.3	34.2	34.8	34.9	34.6	34.4	34.7	$\frac{20.1}{34.7}$	35.0	35.1	31.40
40.4	40.0	40.0	39.7	39.5	39.1	$\frac{38.9}{94.9}$	39.1	39.9	40.0	40.5	41.2	38.66
44.7		45.0	45.4	45.7	45.7	45.2				40.2	47.4	44.48
	44.9		49.5	50.0	50.1		46.4	46.5	47.3		49.6	48.8
49.4	49.2	49.2	51.8		1	50.5	20.0	50.5	50.3	20.0		
52.3	52.1	52.1	010	51.4	51.0	44.2	11:1	4410	44.0	44.2	$\frac{-}{44\cdot 4}$	49.20
15:0	40.0	44:0	11.9	44.0	42.0		44.4	44.2	44.2		42.6	43.77
45.0	43.8	44.2	44.3	44.2	43.8	43.5	43.2	42.6	42.2	42.1		
40.0	39.8	39.3	38.8	38.4	37.9	37.6	37.0	37.0	36.9	36.7	36.6	39.88
39.5	40.0	40'1	39.9	40.4	39.6	40.2	40.6	41.4	41.5	41.5	42.3	39.22
47.3	47.4	47.4	47.6	48.1	47.8	47.6	47.6	47.6	47.8	47.6	47.3	46.13
48'4	47.6	47.2	46.7	46.0	45.6	44.7	44.2	43.7	43.6	43.5	43.0	46.63
43.2	43.4	43.0	42.7	42.4	41.8						$\overline{37\cdot 5}$	41.12
						37.3	37.1	37.0	37.4	37.4		
43.3	43.3	42.6	42.6	42.4	42.6	42.4	42.4	42.0	42.3	42.7	43.2	41.40
47.6	47.6	47.4	47.8	47.8	47.7	48.3	48*4	48.5	49.0	49.3	49.3	46.70
49.7	49.6	49.8	50.4	50.4	50.6	50.8	51.0	50.8	50.8	50.6	50.3	49.53
$52^{\circ}2$	52.1	52.0	51.4	51.2	50°8	50.4	50.2	50.0	49.6	49.5	49.2	50.72
49.2	49.2	49'4	50.6	51.2	47.5	49.4	49.0	49.0	48.2	47.4	47.4	48.97
47.3	47.0	46.8	46.8	46.6	46.2			_				45.71
						41.7	41.6	41.7	41.7	41.9	43:3	
47.2	47.0	46.7	46.7	45.3	44.5	44.3	44.2	44.2	44.0	44.0	43.7	44*98

	0	ne Scale Di	vision = '00	00065 parts	of the V. F.		ICAL FOF in Scale Div		esponding to	1° decrease	of Tempera	iture, 1'64.	
Mean gen T	Göttin-}	O ^h .	1 ^h .	$2^{ m h}$ .	3h.	4 ^h •	5 ^h •	6 ^h .	7 ^h .	8h.	9 ^h .	10h.	11h.
	( 1 2 3 4 5 5	Sc. Div. 187°3 184°3 178°9 178°0 179°5	Sc. Div. 186°0 184°3 178°9 178°2 179°5	sc. Div. 187 ' 4 183 ' 0 179 ' 2 181 ' 0 179 ' 4	Sc. Div.  186°9 178°0 179°2 180°3 178°6	sc. Div. 186.7 182.7 177.6 178.1 178.3	sc. Div.  185°8 183°4 177°0 177°8° 176°1	sc. Div. 187.4 183.6 177.0 177.8 177.7	Sc. Div. 187.4 183.4 176.9 177.3	Sc. Div.  187.4  182.9  176.9  177.5  179.4	Sc. Div.  184.4 180.5 175.7 178.2 178.8	sc. Div. 184.4 179.0 174.1 176.9 180.4	Sc. Div. 184.4 178.0 173.1 176.9 180.9
Υ.	6 7 8 9 10 11 12	193°1 192°9 178°4 187°5 199°3 198°2	192.8 193.6 189.2 191.1 202.5 198.2	194.7 193.6 189.2 191.9 201.5 198.7	193°5 195°3 185°3 189°3 200°5 196°3	192°3 191°1 186°0 186°2 197°0 194°9	191.0 190.6 186.1 187.9 196.8 192.7	192.7 195.3 189.2 190.7 198.7 194.4	193 '9 194 '4 189 '2 193 '5 198 '9 192 '3	195.6 194.0 193.6 194.1 199.7 191.4	194.0 193.7 197.5 194.8 198.9 191.1	191 · 2 187 · 7 192 · 2 194 · 3 196 · 7 189 · 6	194.7 187.8 195.4 194.3 196.7 189.4
FEBRUARY.	13 14 15 16 17 18 19	191 · 7 183 · 7 185 · 2 182 · 4 178 · 7 173 · 3	194.3 183.9 187.1 182.3 180.0 178.0	198.7 188.6 185.9 182.1 178.9 179.5	181.1 180.0 178.6 179.4 178.1 176.5	182.6 180.9 175.3 177.3 176.0 176.5	182.9 181.9 175.3 175.9 175.3 176.3	183°1 185°1 176°5 176°4 173°4 173°3	183°3 185°5 177°5 177°8 173°4 175°3	181.8 185.5 178.1 177.8 173.3 175.2	181.8 185.5 178.1 177.1 173.1 173.8	184.8 182.2 176.7 174.6 170.5 172.2	187:1 180:9 176:7 174:9 171:7 173:4
	20 21 b 22 b 23 24 25 26	147.8 172.5 174.3 129.9 178.4 184.5	100°4 170°5 177°9 127°9 173°9 183°5	161.0 179.1 177.2 156.9 183.3 186.1	193.4 179.8 172.6 175.7 189.4 181.8	190·1 179·8 172·8 180·0 188·5 177·9	185.0 179.8 174.9 186.3 188.5 180.6	192.0 179.8 174.7 184.8 188.5 181.5	194'3 184'4 181'1 183'9 189'5 180'9	193 ° 9 176 ° 3 182 ° 4 188 ° 9 191 ° 5 183 ° 4	180.0 185.7 180.8 192.6 188.9 180.9	250°2 184°2 182°6 199°0 190°7 180°2	243.7 182.5 181.8 192.6 189.7 180.2
	27 28 29	181·2 179·8	179°8 182°6	181·7 182·6	181.7 182.0	184°1 180°2	184°1 178°6	181°2 178°6	183°1 180°1	180°4 180°9	180.6 181.4	181·4 182·6	180·4 182·9
Hourl	y Means	181.76	182.85	185.27	183*48	182.74	182.86	183.55	184.19	184.86	184.46	183.65	183.65
		<u> </u>	1	<u> </u>			HE VERTIC				<u> </u>		
	$\left(\begin{array}{c}1\\2\\3\\4\\5\\6\end{array}\right)$	43·4 41·6 46·4 45·4 46·5	43.6 41.6 45.9 45.2 46.6	43.0 42.0 46.3 45.2 46.3	42.4 44.0 46.4 45.3 46.0	42·4 43·2 47·3 46·3 46·2	42.4 43.4 47.6 46.8 46.6	42.6 43.5 47.9 47.0 46.6	42.6 44.3 48.4 47.2 46.4	42.5 44.8 48.6 47.2 45.7	43.2 45.9 49.3 47.5 45.6	43.4 46.6 49.7 47.7 45.4	43.5 47.4 50.2 48.2 45.2
Y.	$egin{array}{c c} 7 & 8 & 9 & \\ 9 & 10 & \\ 11 & 12 & \\ \end{array}$	39.0 39.9 41.3 40.8 33.1 36.1	39.0 39.5 41.3 40.6 32.8 35.6	38.8 39.3 43.0 40.1 33.3 35.2	38·2 38·2 42·4 41·0 34·9 35·5	38.1 38.8 42.4 40.0 34.3 36.2	38·2 39·3 42·3 39·8 34·6 37·0	38·2 40·0 42·0 39·8 34·6 37·0	38.6 40.3 42.0 39.8 34.4 87.8	39°1 40°6 42°3 39°8 35°1 38°3	39.6 41.3 42.4 39.9 36.0 39.4	40.2 42.0 43.0 39.9 36.8 40.0	41.4 42.2 43.0 39.9 37.4 40.6
FEBRUARY.	13 14 15 16 17 18 19	38.8 43.2 42.7 44.2 45.8 46.2	38.4 42.5 42.4 43.5 45.8 45.6	38.8 42.3 42.9 44.0 45.7 45.5	42.4 42.6 45.4 44.5 46.4 46.2	41.0 42.7 45.6 45.5 46.6 45.8	41·3 42·9 46·2 46·4 47·4 46·3	41.4 42.4 46.5 46.7 47.5 47.0	42.4 42.8 46.8 46.6 48.2 47.9	43.0 43.5 47.4 47.1 49.2 48.3	43.4 44.5 47.8 47.9 49.6 48.8	43.9 45.7 48.2 48.6 50.0 49.2	44.0 46.5 48.3 49.4 50.2 49.2
	20 21 b 22 b 23 24 25 26 27	45°3 50°2 49°4 46°2 43°2 46°4	45.4 50.0 49.0 46.2 41.5 44.3	46.0 49.5 49.0 44.9 41.3 44.0	47.0 49.4 49.4 44.7 42.0 46.3	47.0 49.3 49.5 44.1 42.0 46.2	47.4 49.4 49.5 44.3 42.3 46.5	47.7 49.6 49.3 44.4 42.4 46.3	48.1 49.9 48.8 45.0 42.8 46.4	48.5 49.9 48.4 44.4 42.8 46.4	49.0 50.0 48.7 45.5 43.3 47.1	49.5 50.2 48.8 45.8 43.8 47.4	50.6 50.4 48.8 46.1 44.3 47.4
	28 29	43.0	42.5 44.6	42.1	42.0	42.0 44.6	42.5 45.0	43.6 45.3	44°5 45°2	45°2 44°6	45.2 44.6	46.0 44.4	46°2 44°0
Lfanni.	y Means	42.95	42.52	42.49	43.07	43 08	43.42	43.57	43.88	44.10	44.64	45.07	45.3

^{*} Three minutes late.

^b Omitted in the Means, on account of disturbance.

	One Scale	Division =	·000065 pa	rts of the V		RTICAL F se, in Scale		orresponding	g to 1° decre	ease of Tem	perature, 1.6	54.
12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17h.	18 ^h .	19 ^h .	20h.	21h.	22 ^h .	23 ^h .	Daily an Monthly Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc, Div.	Sc, Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
184.9	184.6	185.1	184.7	184.7	184.7	183.4	183.9	184.2	184.4	181.5	184.3	185.25
		178.0	178.2			180.1	180.0	180.0	178.9	178.9	178.9	180.38
176.9	178.0			179'1	179.0		177.7		177.9	178.2	179.0	176.82
172.8	172.8	174.6	174.6	178.2	178.2	177.4	170.7	177.9		178.8	179.5	177.85
176.9	175.5	175.5	175.5	176.9	176.9	176.7	178.7	179.7	179.8	170 0		l
180.9	180.9	180.8	184.2	184.2	184.3		10011	170.0	170:0	100:5	$\left  {193\cdot 5} \right\}$	180.15
-						180.1	180.1	172.6	172.3	182.2		100.76
95.3	195.7	196.2	198.8	198.8	195.5	190.8	191.5	192.6	193.0	192.6	189.2	193.72
190'9	192.6	195.5	192.2	194.6	190.9	178.3	185.9	179.7	177 3	176.3	177.8	189.23
90.3	190.6	192.1	187.7	186.9	189.2	187.7	187.9	187.2	187.2	187.5	187.5	188.88
194'3	195.0	196.6	196.6	196.8	196.8	196.8	197.3	197.3	197.3	201.5	203.5	194:39
96.4	196.4	196.4	197.4	197.4	197.4	197.3	196.9	197.3	198.0	198.0	198.0	198.08
89.1	187.4	187.4	188.7	188.0	186.9						— 1	192.58
				_		196.8	195.6	195.0	194.6	192.3	191.7	192 56
82.0	182.0	180.0	181.5	185.8	184.2	181.6	177.6	171.1	180.6	183.0	182.7	183.55
80.9	181.8	183.4	183.4	184.2	185.3	186.5	186.1	184.1	184.3	184.1	183.0	183.80
			178.0				176.2	177.5	179.4	181.2	182.4	179.10
76.7	176.7	177.8	170.5	178.0	181.4	181.6			177.2	177.9	177.7	176.9
75.9	175.9	176.1	173.5	173.5	174.5	174.8	174.8	175.9				
72.7	172.0	172.0	173.6	173.2	173.7	175'3	174.7	177.2	172.8	172.8	172.8	174.3
73.4	174.8	176.1	178.1	179.4	179.8	_		_		1400	156.6}	174.3
		_				190.1	189.8	166.4	168.3	148.4	156.63	
94.5	197.6	224.3	141'8	210.0	179.2	193.6	163.8	176.8	178.8	179.3	167.5	184.9
85.3	184.1	184.7	184'1	184.3	172.8	184.2	135.2	143.9	148.7	152.4	163.0	174.0
81.8	185.8	169.7	182.6	170.1	168.7	159.5	140.9	124.9	150.0	147.5	123.0	168.2
88.5	190.9	193.3	186'1	161.0	163.8	159.9	151'9	149.1	137.2	139.2	164.6	170 1
89.1	182.8	181.6	180.6	178.4	180.6	182.1	181.4	181.4	181.6	181.4	180.6	184.2
78.9		181.4	178.6	182.2	183.4	102 1	IUI I					
10 9	180'4	101 4	1100	104 4	100 4	104.0	184.0	184.4	184.2	184.0	184.2}	182.1
70.0	170.0	150.0	170.0	150.0	150.0	184.0					178.0	179.9
79.9	179.2	179.0	178.9	178.8	179.0	178.9	177.8	177.6	176.9	174.9		
82.9	182.9	182.6	187.2	178.7	181.1	185.1	185.8	186.7	186.7	186.7	186.0	182.7
183.09	183.25	183.10	183.23	182.14	182.40	181.93	180.72	178.25	179.14	178.67	179.76	182.47
				ТЕМРЕІ	RATURE OF	THE VERT	CICAL FORCE	E MAGNET				
	0	0	0	0	0	0	0	0	C	0		0
43.7	44.0	43.4	44.0	44.0	44.0	44.0	43*4	43.2	43.1	42.8	42.4	43.21
47.5	47.3	47.3	47.0	46.6	46.4	46.3	46.3	46.2	46.2	46.3	46.2	45.3
50.3	49.8	49.5	48.9	47.7	47.6	46.6	46.5	46.0	45.7	$45^{\circ}4$	45.9	47.6
48.4	48.3	48.3	48.1	47.2	47.0	46.8	46.6	46.4	46.4	46.3	46.4	46.8
45.0	44.0	43.6	43.0	42.5	42.3					_		
_	1 11 0	10.0				38.8	39.0	39.0	39.1	39.3	$\frac{38.9}{-}$	43.6
41.4	41.4	41.4	41.6	41.4	41.0	40.6	40.2	40.0	39.8	39.7	40.0	39.8
42.6									42.3	42.1	41.9	41.3
	42.6	42.7	42.8	42'9	42.8	42.6	42.6	42.5	1			$\frac{41}{42}$ .5
43.2	43.3	43.2	43.3	43.1	43.2	42.7	42.4	42.4	42.4	42.5	41.8	
39.2	39.0	38.3	37.9	37.7	36.8	36.4	36.0	35.1	34'1	34.0	33.7	38.3
37.6	37.3	37.3	37.0	37.0	36.4	36.2	36.6	36.4	36.5	36.5	36.1	35.7
40.6	40.9	41.3	41.2	41.2	41'2	_		_			38.7	<b>3</b> 8*3:
	l —		_		-	36.9	<b>36.</b> 9	37.1	37.2	37.7		
44.6	45.0	45.4	45.4	45.0	44'9	44.9	45.2	44.6	44.4	44.5	44.2	43.2
46.6	46.0	45.6	45°4	45.0	44.4	43.8	43'4	43.7	43.7	43.6	43.2	44.0
47.7	47.7	47.2	45.8	45.9	45.6	45.2	44.8	44.7	44.4	44'0	44.2	45.73
49.6	49.8	49.4	49.0	49.0	48.7	48.5	47.5	47.0	47.0	46.7	46'1	47.2
49.6	49.4	49.3	49.3	49.3	49.3	49.3	48.3	47.6	47.4	47.0	46.6	48.1
49.3			1				<del></del>	1	— I	_		
	49.3	49.3	49.1	48.6	48.2	44.7	44.6	44.5	44.6	$\frac{-}{44.5}$	$\frac{-}{44.6}$	46.9
21.8	50.0		54:0	<u> </u>	55:0				53.4	51.0	50.5	50.5
	53.0	53.8	54.2	54.4	55.0	54.8	54.8	54.3			49.3	
49.8	49.6	49.5	49.0	48.7	48.5	48.4	49.0	51.2	51.9	49.5		49.6
48.7	48.2	48.0	47.9	49.6	49.6	49.4	48.6	48.6	47.5	47.3	46.5	48.69
45.9	45.4	45.0	44.8	44.5	44.7	44.5	44*4	44.4	45.0	46'6	46'4	45.13
44.4	46.4	47.6	48.2	48.0	46.7	46.6	46.6	45.4	45.4	45.5	46'4	44.24
47.2	47.0	46.8	46.4	45.7	45.5						$\frac{-}{43\cdot 4}$	45.48
	-	_				43.3	43.2	42.8	42.6	43.0		
	1 40.0	46.4	46.2	46.4	46.3	46.2	46.2	45'4	45.0	44'9	45.0	44.81 43.79
46.0	46.3		49.6	40.0	10.0	19.0	49.4	49 5		49 4	4/11	
	45.29	43.2	42.6	42.8	43.2	43.2	42.6	42.6	42.6	42.4	43.09	43.9

Mean Gött gen Time	tin-}	O ^h .	1 ^h .	$2^{ m h}$ .	3h.	4 ^h •	5 ^h .	6 ^h •	7 ^h .	8h.	9հ.	10 ^h •	11h.
	1 2 3 4	Sc. Div. 184 ' 9 186 ' 3 188 ' 7 186 ' 4	Sc. Div. 186°0 187°2 188°7 188°0	Sc. Div. 184'5 188'5 190'1 188'0	Sc. Div. 182 ° 0 188 ° 9 189 ° 8 183 ° 8	Sc. Div. 182 ° 0 188 ° 9 188 ° 0 179 ° 5	Sc. Div. 179°1 187°8 186°0 178°9	Sc. Div. 179 0 187 3 185 7 178 9	Sc. Div. 179°2 187°0 183°8 179°4	Sc. Div. 179°4 186°8 182°8 179°7	Sc. Div. 179°3 186°2 181°6 181°4	Sc. Div. 180'4 186'2 180'8 183'2	sc. Div 182°4 186°1 180°8 184°6
1 1	5 6 7 8 9 0 1	192 · 2 184 · 6 174 · 8 178 · 7 186 · 8 181 · 0	193.5 185.2 172.4 180.4 187.0 182.2	192'4 183'3 171'2 179'5 186'4 180'4	189 '9 181 '8 171 '2 178 '8 183 '8 176 '3	187 · 2 180 · 5 169 · 5 177 · 8 180 · 3 172 · 9	186.5 180.1 169.3 176.0 177.6 166.4	184.5 179.8 169.9 177.4 177.6 172.7	184.5 178.3 170.6 177.7 178.3 173.2	186°3 177°0 170°2 177°0 178°3 174°2	186.7 175.7 170.2 176.4 176.2 174.2	185.6 175.0 174.5 176.3 175.0 174.2	185.6 175.8 170.3 175.9 175.8 174.5
MARCH.	2 3 4 5 6 7	178.6 184.3 189.4 194.3 157.6 188.8	181 · 3 184 · 3 186 · 0 195 · 8 163 · 7 187 · 9	182°1 184°3 187°3 195°0 175°4 189°3	177.8 177.8 188.5 193.4 180.8 185.2	177.6 181.5 187.3 193.4 188.3 183.8	176.4 181.8 192.0 192.1 197.7 182.6	177.0 182.8 196.1 190.8 205.1 182.6	179°3 183°8 199°8 191°8 204°8 182°7	179 · 8 185 · 7 203 · 3 190 · 9 216 · 0 185 · 4	180°3 185°5 203°3 189°3 203°0 186°6	180°1 185°3 205°1 188°5 197°9 184°6	181.0 185.3 202.5 188.6 197.9 186.7
2 2 2 2 2 2 2 2	19    20    21    22    23    24    25	136.8 170.8 176.3 165.0 166.0 166.3	146.4 176.2 176.1 170.3 169.0 173.1	167.0 173.9 174.9 171.1 168.3 170.4	172.7 169.5 173.3 172.0 166.8 170.3	180.6 169.4 172.6 173.0 166.5 172.8	186.5 169.1 172.6 171.0 168.1 170.2	188'8 169'1 173'5 169'5 169'2 171'6	209 '9 169 '4 174 '8 170 '6 171 '8 174 '4	225 · 5 169 · 4 174 · 8 171 · 4 171 · 6 177 · 4	224 · 9 168 · 4 174 · 2 168 · 5 168 · 6 180 · 7	209 · 5 168 · 4 175 · 2 168 · 9 168 · 1 179 · 0	207 '7 168 '4 175 '5 169 '0 168 '3 179 '0
2 2 2 3	26   27   28   29   30   31	173°0 176°4 168°4 163°8 155°9	173 · 4 176 · 8 168 · 4 165 · 1 162 · 9	176°3 176°7 167°7 164°2 160°9	176 · 8 174 · 9 164 · 5 162 · 2 163 · 9	176°9 173°1 163°1 161°3 164°2	176'9 172'0 163'4 161'3 161'1	175°3 173°3 165°3 161°3 163°7	175 · 5 173 · 4 164 · 3 162 · 1 161 · 8	175.5 171.2 163.9 163.2 160.7	175 ° 0 170 ° 6 162 ° 5 163 ° 9 164 ° 2	174.3 170.5 160.8 163.7 164.2	175°8 168°1 159°8 163°9 163°9
Hourly M	leans	176.15	178.05	178.86	177.66	177.48	177:13	178.07	179.34	180.64	179.90	179.09	179.0
	h	0	1 0	1 0			HE VERTIC			1 0	0	0 1	. 0
	1 2 3 4	42°4 42°2 39°7 40°6	41°6 40°7 39°7 40°3	42.4 40.0 39.6 40.4	42.7 40.0 39.0 41.4	43°0 40°0 39°4 43°7	43.7 40.0 40.6 44.4	44.3 40.3 41.3 44.4	44.1 41.1 41.9 44.6	45°0 41°3 42°7 44°2	44.9 41.9 43.4 43.8	45°3 41°7 44°0 43°2	45°3 41°4 44°0 42°4
]	5 6 7 8 9 10	38.7 43.6 48.5 47.1 42.4 44.4	38.5 43.6 48.3 46.5 42.1 44.0	38.7 43.8 48.6 46.4 41.7 45.0	38·2 44·5 48·4 46·0 42·2 46·0	39·2 44·4 48·9 46·3 43·2 46·8	39·9 44·5 49·8 46·6 44·3 47·4	41.0 45.4 50.2 46.7 45.0 47.6	41.0 45.9 51.2 47.0 45.0 47.6	41.8 47.1 51.4 47.3 45.4 48.0	42.8 48.1 52.0 48.2 45.8 48.3	44.1 48.2 52.2 48.5 47.0 48.8	44.2 48.2 52.1 48.6 47.5 48.4
MARCH.	12 13 14 15 16 17 18	45.4 40.8 35.3 35.1 40.5 41.0	44.4 40.5 35.1 35.3 40.5 41.2	44.4 40.8 35.3 35.9 40.8 41.2	44.8 42.6 36.0 36.4 40.6 42.6	44.4 41.2 36.1 37.0 40.6 43.9	44.5 41.0 36.3 37.8 41.2 44.9	44.4 41.3 36.4 38.3 41.6 45.4	43.9 41.4 36.4 39.1 41.8 45.6	43.7 41.3 37.2 39.2 42.4 45.9	44.1 41.2 37.2 39.8 42.5 46.4	44'3 41'2 38'0 39'8 42'6 46'4	44.5 41.0 38.0 40.0 43.7 46.6
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44	26 27 28 29 30 31	47 · 3 47 · 5 52 · 2 52 · 5 53 · 0	47.1 47.6 52.4 53.0 52.3	47.2 48.0 53.2 53.0 52.3	47·1 48·5 54·0 54·2 52·2	47.3 49.2 54.8 54.4 52.9	48.2 50.3 55.0 54.4 54.0	49.2 51.1 55.0 54.3 54.7	50°2 51°5 55°2 54°4 55°2	50°4 51°8 55°6 54°4 55°4	51 · 2 52 · 3 56 · 4 54 · 6 56 · 2	51.4 52.6 57.3 54.9 57.2	51.4 53.1 58.2 55.0 57.2
Hourly M		45.11	44.86	44.98	45.36	45.73	46.58	46.69	46.98	47.28	47.74	48.12	

190		One Scale	Division =	*000066 pa	rts of the V		RTICAL I		orrespondin	g to 1° decr	ease of Tem	perature, 1°	64.
1867   18673   18673   1877   18679   1872   1891   1887   1887   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897	12h.					4			1	1			Daily and Monthly Means.
1867   18673   18673   1877   18679   1872   1891   1887   1887   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897   1897		Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.		Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.		Sc. Div.
181											188.2		
18476   18672   18679   18772   18772   18772   18773   19770   19475   19178   1928   19274   18656   18676   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18876   18776   17777   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779   1779													
185'8 185'7 185'6 185'6 185'0 187'1 185'2 185'0 180'8 189'2 8 192'4 1 175'3 176'9 175'0 175'4 175'3 176'9 175'9 175'9 175'7 175'9 175'0 175'9 175'0 175'9 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 175'0 17			186.0			187.2	100 0	100 4	100 0	100 1	100 0	!	
1851   1857   18576   18576   18576   18576   18570   1871   1859   18570   18670   18670   18670   1871   1871   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771	104 0	100 2	100 3	107 2	10; 2	101 2	197:5	197:0	194.5	191.8	192.8	192.4	186 55
1737   1754   1753   1769   1759   1759   1757   1759   1756   1757   1759   1740   1776   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771   1771	185'8	185.7	185.6	185.6	188.0	187.1							186.21
177-96   177-76   178-1   177-0   174-75   174-75   174-75   172-3   173-6   175-8   178-13   178-7   177-176-9   177-14   179-0   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   177-9   1													177.62
173.5   177.4   179.0   178.3   179.3   189.7   180.5   180.8   180.8   180.4   181.0   181.0   178.7   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.5   174.													173.29
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		177.4	179.0			179.3	180.7		180.8				178.76
13477   174*5   174*5   175*6   175*6   175*8   175*8   175*6   175*8   175*6   175*8   175*6   175*8   175*6   175*8   175*8   181*9   182*4   182*4   183*5   183*0   182*5   183*4   184*1   184*3   184*3   181*3   181*0   185*2   185*5   190*6   194*5   195*9   195*5   195*4   185*6   185*4   184*1   184*3   184*3   181*3   181*0   185*2   185*4   185*0   195*4   185*0   195*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*2   185*4   185*0   185*2   185*4   185*0   185*4   185*0   185*3   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*4   185*0   185*5   185*4   185*0   185*5   185*4   185*0   185*4   185*0   185*5   185*4   185*0   185*5   185*4   185*0   185*4   185*0   185*5   185*4   185*0   185*5   185*4   185*0   185*4   185*0   185*5   185*4   185*0   185*5   185*4   185*0   185*4   185*0   185*5   185*4   185*0   185*5   185*4   185*0   185*4   185*0   185*5   185*4   185*0   185*5   185*4   185*0   185*4   185*0   185*5   185*4   185*0   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*5   185*6   185*6   185*5   185*6   185*5   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*6   185*						177.9							179.64
181'0						176.3							
181'0   181'9   181'9   181'9   182'4   183'5   183'0   182'5   183'0   181'1   184'3   181'0   181'0   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'1   181'							176.4	176.4	177.5	176.7	176.7	178.7}	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	181.0	181.9	181.9	182.4	182.4	183.5					184.3	184.3	181.08
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							189.5				195.1		187.27
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										196.2	196.2		195.45
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										175.8	159.2	160.2	184.75
$ \begin{array}{c}$											189.0	188.2	190.36
202:9 296:4 208:6 205:5 164:7 177:2 176:2 168:3 159:8 166'4 177:1 177:2 185'27 170:2 169:0 167:8 169:2 169:2 169:2 169:7 169:8 170:3 170:3 170:3 170:1 177:8 170:0 170:7 173:8 173:3 173:1 173:2 171:7 166:9 166:9 166:2 164:7 165:0 164:9 164:4 177:1 173:8 173:3 173:1 173:2 171:7 169:0 169:9 157:7 156:0 162'8 164:9 168:6 168:5 169:6 172:1 176:7 176:7 176:7 169:0 168:2 172:4 174:4 175:3 168:8 157:0 169:0 168:5 169:6 172:1 176:7 176:7 176:7 169:0 168:2 172:4 174:4 175:3 168:8 157:0 169:0 174:1 175:3 173:5 173:5 174:3 168:3 173:9 174:1 174:1 169:0 166:0 166:1 171:0 174:1 175:3 173:5 173:5 174:3 168:3 173:9 174:1 174:1 169:0 166:0 166:1 171:0 174:1 175:3 173:5 173:5 174:3 168:3 173:9 174:1 174:1 169:0 169:1 175:4 174:4 178:8 168:7 168:7 168:5 168:6 168:6 171:0 171:0 171:0 169:1 175:4 174:4 174:1 169:0 169:1 175:1 175:1 169:0 166:0 166:1 171:0 171:0 170:1 169:1 175:1 175:1 169:1 175:1 169:0 160:0 166:1 164:3 154:4 155:1 160:3 163:5 161:9 148:2 159:1 159:5 161:0 160:0 166:1 164:3 154:4 155:1 160:3 163:5 161:9 148:2 159:1 159:5 161:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0 179:0													זליללן
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										175.3	168.8	157.0	169.62
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		_		_			172.7	169.7	169.6	160.9	166.0	166.1 }	
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			168.7				168.6			169.5		169.5	171.16
185'0   174'0   170'1   164'7   162'9   159'2   155'7   153'9   157'3   157'4   148'8   148'8   148'8   161'57   169'0   179'03   179'57   179'46   177'77   176'94   177'01   175'11   175'01   174'21   175'03   174'14   177'68   179'03   179'57   179'46   177'77   176'94   177'01   175'11   175'01   174'21   175'03   174'14   177'68   185'0   44'4   44'4   44'4   44'2   44'0   43'4   43'4   43'4   43'4   43'4   43'8   43'0   43'0   42'0   41'7   41'4   40'8   40'0   40'0   40'0   40'0   40'0   40'0   40'0   40'0   40'0   40'0   40'0   40'0   40'0   40'0   40'0   40'0   40'5   40'3   41'4   41'0   40'6   40'7   40'9   41'1   40'9   41'48   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0   44'0											160.9	161.9	162.79
165*0 160*4 166*1 164*3 154*4 155*1 160*3 163*5 161*9 148*2 159*1 159*5 161*05*  179*03 179*59 179*57 179*46 177*77 176*94 177*01 175*11 175*01 174*21 175*03 174*14 177*68*  ***TEMPERATURE OF THE VERTICAL FORCE MAGNET.**  45*0 44*4 44*3 44*4 44*4 44*2 44*0 48*4 43*4 43*4 43*4 43*4 43*5 43*5 43*5 43										157.4			
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## TEMPERATURE OF THE VERTICAL FORCE MAGNET  ## A				<u> </u>					<u> </u>	174.21	175.03	174.14	177.68
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48:4       47:8       46:8       46:3       46:3       45:6       45:3       45:0       44:6       44:5       44:1       43:0       46:37         47:4       46:5       46:0       45:8       45:4       45:0       44:8       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4       44:4													
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51.2     50.8     50.4     50.2     49.9     49.6     49.4     48.6     48.4     48.4     48.2     48.0     49.21       53.2     53.0     52.5     52.6     52.4     52.4     52.4     51.9     51.8     51.8     51.6     52.2     51.30       58.4     58.2     58.0     56.8     56.2     55.8     55.7     55.7     55.4     55.0     54.1     54.1     54.1     55.53       54.8     54.4     54.5     54.4     54.4     54.2     54.0     53.7     53.3     53.1     53.2     53.1     54.01       58.0     58.1     58.1     57.6     59.4     59.6     57.0     56.1     55.1     54.3     54.3     54.3     54.1     55.60	53'2						54.8	53.9			1		
51·2     50·8     50·4     50·2     49·9     49·6     49·4     48·6     48·4     48·4     48·2     48·0     49·21       53·2     53·0     52·5     52·6     52·4     52·4     52·4     51·9     51·8     51·8     51·6     52·2     51·30       58·4     58·2     58·0     56·8     56·2     55·8     55·7     55·7     55·4     55·0     54·1     54·1     55·53       54·8     54·4     54·5     54·4     54·4     54·2     54·0     53·7     53·3     53·1     53·2     53·1     54·0       58·0     58·1     58·1     57·6     59·4     59·6     57·0     56·1     55·1     54·3     54·3     54·1     55·60		53.4	i .	i		1	40.0	40.0			40.1	17.0}	51.21
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	Or	ne Scale Div	vision = '00	00065 parts	of the V. F.	Increase,	in Scale Div	isions, corre	sponding to	1º decrease	of Tempera	ture, 1 • 64.	
Mean Göt gen Tin	ttin-}	Oh.	1h.	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h •	7 ^h .	8 ^h .	9 ^h .	10 ^h •	11h.
(	1 2	sc. Div. 164°8	Sc. Div. 164.8	Sc. Div. 169°4	sc. Div. 169°7	Sc. Div. 169.8	Sc. Div. 167.6	Sc. Div. 168°1	Sc. Div. 170°8	Sc. Div. 170°9	Sc. Div. 171 0	Sc. Div. 171.7	Sc. Div 171°9
	3	151.6	163.7	168.4	171.9	175.6	177:3	180.6	186.8	183.6	181.3	187:1	178.5
	$\begin{bmatrix} 4 \\ 5 \end{bmatrix}$	$\frac{169.5}{172.2}$	168°0 171°8	167°5 169°3	168.0 168.0	165.6 166.6	165°0 166°5	168°3 166°5	167 <b>·</b> 9 166 <b>·</b> 5	168'9 167'7	170°4 171°4	171.1 171.7	173°1 173°5
	6 a	171.7	174.5	168.5	166.1	165.8	164.6	164.6	164.7	168.9	168.0	165.5	163
	7 8	149°4 172°5	151 <b>·</b> 9 171·5	150°8 172°0	149°7 170°0	166°1	170°4 168°3	174.8 166.5	180.4 166.1	188.7 165.9	182 <b>.</b> 8	186.6 162.6	174° 161°
t t	9	166.2	164.9	164.9	161.8	158.8	 157`1	 155 <b>·</b> 7	 155 <b>·</b> 7	155.7	154 <b>·</b> 9	154.1	152
	$\begin{vmatrix} 11 \\ 12 \end{vmatrix}$	155.7	155.9	157°2 161°3	157.2	157.2	155.9	155.9	157.5	158.5	159°4 159°0	159°4 157°6	158°
	13	164.0 163.0	$162.7 \\ 163.3$	163.0	160°6	157.4 164.0	158.0 163.9	158.0 163.6	159 <b>·</b> 4 163 <b>·</b> 0	159 <b>·</b> 4 163 <b>·</b> 6	163.6	164.4	164.
ا انر	14	173.4	171.7	172.0	170.0	168.9	167.4	167.4	166.6	167.2	167.0	166.5	164
Æ ( 1	15 16	169.6	166.9	166.0	163 <b>.</b> 0	— 161.8	161.8	162.4	162.2	166.8	169.4	170.2	173
1 1 -	$\begin{vmatrix} 17 \\ 18 \end{vmatrix}$	169°3 174°5	167 <b>·</b> 8 174 <b>·</b> 2	165°7 174°2	163.4 174.2	159°8 172°0	161°5 167°9	161 <b>·</b> 5 167·9	162.8 171.7	165°7 175°7	173°3 177°3	177°1 176°4	182° 178°
1	19	181.4	181.3	177.5	175.7	175.5	174.8	174.0	171.7	172.9	172.3	172.1	172
2	20 21 ь	175°4 —	173 <b>·</b> 9	171.3	169.9	170.1	169.0	169·5	169.9	169·5 —	169.6	169.6	168.
	$\begin{bmatrix} 22 \\ 23 \end{bmatrix}$	171.3	169.4	164.6	164.6	165.2	165.2	165.0	162.9	165.4	165.4	165.4	164
2	24	171.8	171.8	171.9	171.8	171.9	168.3	166.1	169.7	169.7	169.3	171.6	170
	$\begin{vmatrix} 25 \\ 26 \end{vmatrix}$	174.9 170.4	174 <b>.</b> 4 168.9	170°5 166°5	170°5 166°2	170°5 165°6	169 <b>.</b> 4 166 <b>.</b> 2	169'4 167'7	167°5 166°7	167°5 167°0	167.5 166.8	167.5 166.8	167°
{ 2	27	171.1	168.8	167.6	165.4	164'3	163.0	163.0	163.0	163.0	162.7	162.2	161.
	28 29	165°5 159°8	165.2 159.0	166.6 159.7	165°7 165°5	164 <b>'9</b> 157 <b>'</b> 7	163.7 160.0	163°7 160°0	166°3	164'9 165'2	164.9 171.2	165.6 173.1	165°
	30		-				_						
lourly M	<b>Ie</b> ans	167.71	167.48	166.87	166.37	166.00	165.59	165.90	167.04	167.97	168.50	169.13	168
	H				TEMPERAT	URE OF TH	IE VERTICA	L FORCE M	IAGNET.	i i			
(	$\begin{bmatrix} 1 \\ 2 \end{bmatrix}$	52.7	52·7	52.6	51°5	51°3	5 <u>1</u> .6	51°5	5 <u>1</u> °2	50°8	50°8	50°8	50°
	3	45.2	46.0	46.9	47.4	48.5	49.4	50.5	50.8	51.0	51.2	51.6	52
	$\begin{bmatrix} 4 \\ 5 \end{bmatrix}$	$53^{\circ}2$ $51^{\circ}2$	53°1 51°8	53.0 52.2	53°2 52°3	53°3 52°4	53.4 52.6	53.4 53.2	53°5 53°4	53.4 54.0	53.6 54.2	53.7 54.2	53. 54.
	6 a	50.8	51.2	52.0	54.2	53.1	53.8	54.2	54.2	54.7	55.2	56.0	56
	$\begin{bmatrix} 7 \\ 8 \end{bmatrix}$	54°0 51°2	54°2 51°5	55.0 52.3	55°3 53°6	55 · 7 54 · 2	56°0 54°7	56.1 55.0	56°2 55°4	56°2 56°0	56°3	56.8 57.4	56. 57.
١,	9	55.0	<u> </u>	56.2	57.4	 58.6	59·0	59.2	59.2	60.0 —	60.6	61.2	60.
1	11	59.8	59.6	59.2	59.2	58.7	59.0	59.2	59.0	59.0	59.0	59.0	59
	$\begin{vmatrix} 12 \\ 13 \end{vmatrix}$	55°2 55°3	56°2 55°3	56°2 55°1	56.4 54.5	$57.1 \\ 54.2$	57°4 54°2	57.5 54.2	57.8 $54.2$	58'1 54'2	58°5 54°2	59°2 54°2	$59 \cdot 54$
1 7	14 15	50°2 51°4	50°4 53°0	50°5 54°0	51.0 54.3	51.2 54.8	51°4 55°4	52°0 55°4	52°3 55°6	52.8 56.2	53°2 56°5	53.8 57.2	54° 57°
PR (	16			54.4	54.2	54·5	 54·5	54.4	54·7	55.5	 55°4	55.5	55
	17 18	53°2 -50°8	53.8 50.3	50.3	50.1	50.0	50°1	50.1	49.8	49.2	49.2	49'1	48
1:	19 20	44.4 48.5	45°0 48°6	45°8 49°8	46.8 50.2	47°2 50°4	48°0 50°7	48.4 51.0	48.8 51.4	49'1 51'8	49.6 52.3	50°2 53°0	50°
	21 ^b 22	54·0	53.4	53.2	53.2	53.5	53.4	23.8	54.7	55.1	55.2	56.5	56.
	11	47.7	47.5	48.0	48.0	48.0	49.0	49.4	49.6	50.3	50.4	50.4	50.
	23	41 1	47.5	48 0	48 0	48 0 49.5	49 0	50.1	50.2	50.8	51.4	51.6	51.
	23 24 25	46.8	414		52.2	52.3	52.5	52°2 53°2	52°1 53°3	52.2	52.4	52.6	53.
	24 25 26	46.8 50.2	51.0	52.1		£0.0							22.
	24 25 26 27	46.8		52°1 50°4 51°5	51.9 51.4	$52^{\circ}2$ $51^{\circ}4$	52.6 51.9	52.0	52.2	53.7 52.2	54.4 52.8	55°0 53°2	53.
	24 25 26	46.8 50.2 49.4	51.0 50.0	50.4	51.9								25° 53° 56°

	One Scale	Division =	· 000065 par	ts of the V.		RTICAL F se, in Scale		orresponding	to 1° decre	ase of Temp	erature, 1°6	4.
12h.	13 ^h .	14 ^h .	15h.	16 ^h .	17h.	18h.	19 ^h .	20h.	21 ^h .	22h.	23h.	Daily an Monthl Means.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
172.9	173.3	173.6	172.9	163.5	169.0	10710	107.0	,			$\frac{-}{162 \cdot 5} \}$	168.0
-						167.0	167.3	161.1	161.9	157.0		
180.4	177.0	177.9	174.7	168.6	167.0	160.6	155.7	160.3	168.2	169.8	169.5	172.3
173.1	171.2	171.2	170.8	169.9	167.4	167.4	167.4	165.8	159.6	167.4	169.5	168.4
169.9	168.4	168.4	168.4	164.9	91.8	124.2	140.9	144.0	161.0	160.6	168.7	160.9
163'6	165.4	171.9	183.0	173.9	124.5	119.0	96.1	193.0	70.7	126.5	116.2	154.5
169.7	173.4	170.2	168.4	168.6	160.8	160.8	169.9	169.8	169.8	160.9	165.6	168.0
160.6	160.6	160.6	163.5	163.5	163.8							10110
						166.7	166.7	155.5	158.2	164.4	$\frac{-}{164\cdot 7}$	164.9
152.6	152.6	152.6	151.8	152.7	152.7	147.0	151.2	154.5	155.3	155.3	155.6	155.6
158.7	158.7	158.6	158.4	158.4	158.4	158.4	158.9	159.1	159.4	160.0	162.1	158.2
		156.6	157.0	157.4	157.0	158.1	158.8	158.8	160.0	160.0	160.0	158.8
157.1	156.6											
164.4	164.2	164.5	166.2	167.4	168.9	169.7	169.7	169.9	169.7	169.7	171.2	165.8
165.6	165'6	165.6	165.6	165.4	164.7	164.7	166.5	167.0	168.6	168.2	169.6	167.5
$173^{\circ}2$	175.3	182.9	179.8	172.8	154.4	l —	<del></del>		_	_	— \	167.3
	·	_				163.0	161.0	163.3	165.3	165.3	$_{167\cdot _{2}}\}$	
188.5	186.8	173.7	168.0	166.0	164.2	145.4	160.7	167.0	168.9	169.4	171.9	168.3
177:5	176'9	179.4	173.4	177.1	176.7	176.0	176.0	176.0	178.7	180.2	182.1	175.6
173.5	174.5	170.4	169.2	168.8	169.6	169.8	169.7	171.3	171.9	171.3	172.5	173.0
169.2	170.7	170.7	168.0	168.0	168.1	100 0	100	111		111 0		
109 2	170		100 0	100 0	-	166.3	120.4	112.5	125.1	149.2	$\frac{-}{152 \cdot 2}$	161.9
162.7	163.0	163.1	163.0	162.9	162.7							105.0
102 1	100 0	100 1	1 200	1020	102	168.0	168.0	168.0	169.6	169.6	169.9}	165.8
169.9	170.0	169.8	172.3	168.6	173.0	173.0	173.0	173.7	173.7	173.3	173.2	171.1
												169.4
167.5	167.5	167.5	168.6	168.6	169.2	169.4	170.2	170.2	170.4	170.4	170.4	
166.5	166.0	167.4	167'4	166.2	167.1	167.1	167.5	168.2	168.5	168.9	168.6	167:3
161:3	161.2	161.8	161.8	161.8	161.8	162.9	163.8	163.8	164.0	164.1	165.5	163.7
165°2	163.5	162.7	161.6	163.1	149.3	142.9	148.2	144.2	141.5	153.8	154.0	159.6
180.8	164.7	170.7	169.6	166.4	150.0						<b>-</b> )	162.8
						143.2	145'4	159.4	159.4	164.4	162'1}	102 0
168.73	167.91	167.82	166.97	165.68	160.33	160.52	160.73	161.05	162.99	164.93	166.46	165.8
	1	1		ТЕМРЕК	ATURE OF	THE VERT	ICAL FORC	E MAGNET.				l
. 0	2	0	48.0	49°4	49°3	0	0	0	۰	•	0	٥
50°3	50°0	49.6	49.6	49*4	49.3						- J	49.7
						46.7	46.4	46.2	46.0	45.9	45'9 }	
52.0	52.0	52.0	52.2	52.0	52.2	<b>52.</b> 0	52.1	52.3	52.7	53.1	53.4	50.7
53.4	53.2	53.2	53.0	52.5	52.0	51.8	51.7	51.8	51.8	51.8	51'4	52.8
54.8	54.8	54.6	54.3	54.4	55.1	56.2	56.2	55.6	55.4	55.0	52.1	53.9
56.3	56.4	56.2	55.6	<b>56.</b> 8	57.0	56.4	56.4	56.7	57.3	56.4	55.5	55.1
57.2	57.4	57.0	56.5	55.6	54.9	54.2	53.8	53.3	53.0	52.6	52.2	55.2
58.5	58.2	58.0	58.2	58.0	28.0	014	1	00 0				
00 Z	1	1	}	}	l	56.7	56:4	56:1	56:1	55.4	$\frac{-}{55\cdot 4}$	55.8
CO: "	CO:0	61.0	62:0	62:9	61:7		56.4	56.1	56'1	55.4		
60.5	62.0	61.8	63.0	62.2	61.7	61.8	61.0	60.6	60.4	60.5	60.3	59.9
58.9	58.7	58.4	58.4	58.3	58.2	58.2	58.0	57.4	56.8	56.2	56.1	58.4
59.2	59.3	59.1	58.6	58.4	58.4	58.5	58.0	57.6	57.2	56.5	55.9	57.7
54.2	54.0	53.6	52.7	52.2	51.9	51.3	51.1	50.9	50.4	50.0	50.1	53.1
53.4	53.2	53°1	53.0	53.0	52.9	52.7	52.5	52.3	51.9	51.4	51.2	52.2
57.0	57.4	57.1	57.2	57.5	58.0		-			_		
					_	55.7	55.3	54.6	54.2	54.1	$\frac{-}{53\cdot 4}$	55.5
56.1	55.8	55.5	55.7	55.3	55.2	55.0	54.5	54.0	53.7	52.7	51.6	54.6
		48.3	48.4	48.2	48.2	48.2	47.8	46.7	46.4		45.3	
48.4	48.3									45.7		48.6
51.0	51.2	52.2	52.2	51.7	51.0	50.5	50.0	49.5	49.5	49.5	49.3	49.2
54.0	53.6	53.2	53.2	23.0	52.7	54.2	54.2	55.4	56.5	56.6	$\overline{_{55}\cdot_2}\}$	52.6
	57.0	56.2	56.0	55.8	55.5	50.3	49.6	49.4	48.7	48.4	$\frac{352}{48.0}$	53.2
56.7	50.5	50.0	49.8	49.4	49.0	48.5	48.3	47.8	47.4	47.0	46.6	48.8
_			50.8		1		1					
50.4		51.2		50.6	50.6	50.5	50.2	49'9	49.9	49.8	50.0	50.1
50°4 51°6	51.3	. 5.7.7	52.0	51.9	51.6	51.4	51.3	50.8	50.4	50.2	49.6	51.7
50°4 51°6 53°1	52.6	52.4		54.4	54.2	54.1	53.8	53.2	53.2	52.8	52.6	53.3
50°4 51°6 53°1 55°0	52°6 55°0	54.7	54.6	,					=0.0			
50.4 51.6 53.1 55.0 54.0	52.6		54.6 54.5	54.5	54.4	54.4	54.4	54'1	53.8	53.9	54.0	53.2
50.4 51.6 53.1 55.0 54.0 56.0	52.6 55.0 54.4 56.2	54.7 54.7 55.4	54°5 55°1	54.2 54.3	54.4 53.6	<b> </b>						
50.4 51.6 53.1 55.0 54.0	52.6 55.0 54.4	54.7 54.7	54.5	54.5	54.4	1	i			53·9 51·2	$\frac{54.0}{51.6}$	53·2 53·9

0	ne Scale Div	ision = '00	0066 parts o	of the V.F.		CAL FOR n Scale Div		sponding to	1° decrease	of Tempera	ture, 1°64.	
Mean Göttin-} gen Time.}	O ^h •	1 ^h •	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7h.	8 ^h .	9 ^h .	10 ^h .	11 ^h .
$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{pmatrix}$	Sc. Div. 169°0 166°8 158°1 155°4 154°3 148°5	Sc. Div. 168 6 167 5 158 2 155 4 152 1 146 5	Sc. Div. 168 6 167 9 155 5 155 4 149 7 144 5	sc. Div. 166 5 165 7 154 7 153 9 147 9 143 1	Sc. Div. 165 ' 4 162 ' 4 153 ' 6 151 ' 2 145 ' 8 143 ' 1	Sc. Div. 164 ' 9 159 ' 5 151 ' 9 148 ' 2 146 ' 0 139 ' 1	Sc. Div. 164 ' 3 160 ' 5 151 ' 3 149 ' 2 143 ' 4 139 ' 4	sc. Div. 166'6 159'7 154'1 149'2 141'7 139'0	Sc. Div. 169 ' 7 160 ' 2 155 ' 0 152 ' 3 141 ' 2 139 ' 0	Sc. Div. 170 ' 7 158 ' 3 155 ' 7 151 ' 8 141 ' 2 139 ' 7	sc. Div. 173 '9 157 '8 155 '3 153 '3 140 '7 140 '2	Sc. Di 169 0 157 8 156 4 153 4 140 8 138 0
7 8 9 10 11 12 13	130°4 155°6 126°6 154°3 163°3 165°0	130°8 153°8 128°3 154°3 162°0 164°3	137 · 5 150 · 8 134 · 2 158 · 4 160 · 9 163 · 0	141°2 150°8 135°7 160°0 159°3 163°1	149°2 150°8 148°3 160°0 156°9 162°9	149.7 150.7 152.4 159.9 155.0 160.8	153°8 150°7 150°4 159°0 155°0 163°4	157.8 153.2 152.8 157.7 156.3 164.7	165 · 8 162 · 6 153 · 3 159 · 4 158 · 0 164 · 9	171.5 161.2 155.5 159.4 160.9 165.3	166°2 153°9 159°5 158°5 161°7 162°7	164 4 152 9 163 4 158 1 160 1 163 0
XVW 15 16 17 18 19 20 21	165.3 156.2 155.4 131.3 151.0 130.9	163 · 1 159 · 8 152 · 6 137 · 3 151 · 3 134 · 2	160°5 152°2 152°6 149°2 149°7 137°9	158.5 145.8 151.6 149.8 145.2 137.9	157 · 2 149 · 7 149 · 6 148 · 9 140 · 4 139 · 0	155.7 150.5 147.9 151.2 139.4 139.0	155°2 149°7 149°1 150°6 144°1 137°2	155.2 149.7 152.5 160.8 141.6 137.2	155°2 153°3 157°9 154°9 142°6 133°8	155 · 2 155 · 4 153 · 3 148 · 5 141 · 1 137 · 9	157.6 156.9 152.2 146.4 143.8 137.5	155° 6 156° 6 150° 8 143° 6 143° 6
21 22 23 24 25 26 27	147.0 147.9 149.2 144.9 143.4 142.8	146.3 147.9 148.8 144.2 142.8 140.2	146.3 146.5 148.8 144.3 145.2 137.1	145.6 147.1 144.1 143.9 140.2 138.0	142.9 147.1 142.0 142.6 138.0 143.1	141.5 145.9 140.5 140.8 137.7 140.0	140°5 145°4 139°3 140°1 137°1 142°7	143°3 145°9 140°4 140°1 137°3 147°2	143°3 147°2 143°1 142°2 138°0 149°5	144.9 147.9 140.1 142.5 138.0 148.2	144.6 147.9 140.1 140.7 138.0 148.4	144': 147': 139': 141': 138': 152':
28 29 30 31	140°0 138°7 148°6	140°0 138°1 147°5	140°0 135°8 146°4	135.8 135.2 142.4	135.8 133.9 142.1	135 · 2 133 · 9 145 · 0	137.2 134.3 143.9	137.0 135.4 144.4	137.6 133.1 146.1	137.6 136.2 150.5	135.7 136.9 152.1	135° 137° 154°
Hourly Means	149.63	149'48	149.59	148.26	148.22	147.49	147.66	148.92	150.34	150.69	150.46	150
	11 0	1 0	l c				AL FORCE		1 0	1 0	. 0	1 0
$\left(\begin{array}{c}1\\2\\3\\4\\5\\6\end{array}\right)$	51°0 52°2 56°3 58°1 59°6 63°2	50.7 52.2 57.0 58.3 60.8 63.7	50°7 52°4 57°3 58°4 61°8 64°1	51.2 53.0 58.2 58.8 61.5 64.3	51.7 54.0 59.2 59.2 62.5 65.0	52.6 54.8 59.7 59.5 63.5 65.5	53.0 55.2 60.0 60.0 64.0 65.8	53·2 56·1 60·0 59·4 64·5 66·5	53.2 56.8 60.0 60.2 65.4 67.0	53.4 57.5 60.5 60.2 66.0 67.7	53.8 58.2 61.0 60.0 66.4 68.3	54°1 58°2 61°4 59°6 66°3 69°2
7 8 9 10 11 12 13	60°0 58°8 59°3 57°2 54°3 51°2	60°0 59°1 60°0 57°0 54°4 54°1	60°0 59°2 60°3 57°0 55°0 54°0	60°4 60°4 60°3 57°0 55°6 54°5	60.0 60.7 60.9 57.1 56.4 54.5	60.5 61.0 60.7 57.4 57.1 53.7	60°6 61°2 61°0 57°5 57°2 53°4	61 · 3 61 · 0 61 · 5 57 · 5 57 · 6 53 · 5	60°4 61°2 61°9 57°2 58°0 54°1	61.7 61.0 62.0 57.2 58.6 54.5	62·2 61·0 62·2 57·4 59·2 55·2	62 ° 61 ° 61 ° 61 ° 61 ° 65 ° 65 ° 65 ° 65
XAM 15 16 17 18 19 20 20	53°2 56°6 57°2 60°2 62°4 64°7	53.8 57.0 57.4 60.3 62.4 64.5	54.7 57.2 58.2 61.0 62.5 64.7	55°2 57°4 58°2 61°0 63°7 65°4	55.6 58.0 59.2 61.5 64.8 65.7	56°2 58°4 60°2 62°0 65°7 66°5	57°1 58°8 60°4 62°4 66°7 67°3	57.2 59.2 60.2 63.1 68.1 67.7	57.7 59.4 60.5 63.5 68.5 68.0	57.7 59.8 61.5 64.1 69.3 68.5	57'9 60'0 62'0 65'0 69'3 68'5	58.0 60.0 62.3 66.2 69.0 68.3
21 22 23 24 25 26 27	63.0 62.0 60.3 63.5 64.7 63.5	62.9 62.0 60.5 63.5 64.8 63.5	62.7 62.2 60.7 63.5 65.5 63.6	63.4 61.8 61.2 63.5 65.4 64.4	63.6 61.7 61.8 63.9 65.6 64.5	64.0 61.8 62.5 64.8 65.7 64.9	64.5 61.7 63.0 65.3 65.7 65.3	64.3 61.6 63.8 66.0 65.9 65.5	64.4 61.5 64.7 66.5 66.5	64.6 61.7 65.5 67.2 67.0 66.5	64.8 62.4 66.3 68.5 67.3 67.0	65 ° 66 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 67 ° 68 ° 8 ° 67 ° 68 ° 8 ° 67 ° 68 ° 8 ° 67 ° 68 ° 8 ° 67 ° 68 ° 8 ° 67 ° 68 ° 8 ° 67 ° 68 ° 8 ° 67 ° 68 ° 8 ° 67 ° 68 ° 8 ° 67 ° 68 ° 68
28 29 30 31	65.5 65.7 60.0	65°8 66°5 60°0	66.0 62.0 60.0	65°8 67°0 60°0	66°3 67°5 60°3	66°5 67°5 60°1	67°0 67°5 60°1	67.6 67.7 60.0	68°0 67°9 60°0	68.6 67.9 60.4	69.4 68.5 60.5	69 · 5 67 · 5 60 · 7
Hourly Means	59.21	59.71	59.99	60.32	60.79	61.51	61.24	61.85	62.12	62.61	63.02	63.1

	One 81:	Division -	.000086 **	rts of the V	VEI F Incres	RTICAL F	ORCE.	orresponding	r to 1° decre	ease of Tem	perature, 1 · 6	5 <b>4.</b>
12h.	13h.	$\frac{\text{Division} = }{14^{\text{h}}}.$	15 ^h .	16 ^h •	17h.	18h.	19h.	20h.	21h.	22h.	23h.	Daily ar Monthl Means
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Se. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 166°1	Sc. Div 164*89
70.0	169.7	161.1	161.1	161.2	157.6	157.8	157.8	157.5	161.4	158.9	156.3	159.38
57.8	159.7	161.4	155.3	158'9	158.2	157.9	160.2	157.7	149.3	147.9		
54.7	152.8	153.4	148.3	151.1	151.1	152.8	152.3	153*1	154.1	141.4	151.0	153.10
53.6	152.8	153.5	152.3	153.3	154.4	154.3	154.3	154.4	154.8	154.3	154.3	153 1
43.2	144'3	142.2	145.4	144.6	144.6	142.2	140.5	140.5	140.6	145.8	147.5	144.4
38.0	136.8	138.6	138.8	138.8	139.3						- i	139.7
_				_		154.5	137.5	134.0	131.0	134.5	$132 \cdot 3$	
64.4	161.2	159.6	159.3	155.9	151.3	149.3	144.9	149.4	151.6	154.6	155.2	153.1
50.9	150.6	150.7	150.2	150.5	150.5	150.2	149.9	150.9	151.1	1511	140.8	151.8
	157.9	155.2	159.0	140.9	152.7	151.5	140.6	142.2	141.6	153'4	153.4	148.7
61.4						159.4	159.6	159.6	159.8	161.0	163.0	158.6
58.0	157.5	158.3	157:3	157.3	157.3			159.8	161.8	161.2	163.9	158.9
60.1	157.8	157.8	157.8	158.0	154.4	154.7	158.8	109 6	101 0	101 0	1 . 1	
63.0	163.2	166.2	166.2	166.2	164.2			70415	10414	102.0	166.5	164 1
			_			162.3	163.9	164.5	164.4	165.8		1.5010
55.4	156.1	155.8	156.2	156.2	155.4	155.4	156.5	155.9	155.9	157.1	157.1	156.9
53.9	150.5	149.9	151.5	151.5	153.2	153.2	153.8	154.7	156.2	157.4	157.5	153.2
50.3	150.3	153.3	158.7	161.1	164.1	150.3	133.6	129.5	122.3	144.2	144.5	149.4
51.9	208.2	190.1	151.8	166.8	154.7	153.2	148.2	148.2	149.2	150.7	151.0	154.0
40.2	140.3	139.4	139.4	137.4	137.7	132.9	125.0	134.1	130.3	133.5	130.9	139.7
97.6		137.6	138.6	137 4	138.2	1020		^				
37.6	137.6	191 0	190 0	101 9	100 0	140.7	130.0	139.9	141.0	144.2	146.6}	137.9
10.0	140:	149.1	142.4	142.4	143.7	143.5	144.6	145.2	145.2	145.2	145.5	144.2
43.6	143.5	143.1	143.4	143.4					149.3	149.5	148.2	147.7
47:3	146.7	148.0	148.8	148.8	148.8	148.8	149.0	149.0			143.9	142.7
42.7	147.4	144.6	144.5	144.5	144.2	144.7	140.2	134.6	135.6	143.9		
41.8	140.2	140.2	140.0	145.0	136.4	128.4	138.3	141.2	143.5	144.6	144'8	141.3
38.0	138.0	135.3	133.7	137.6	139.3	122.4	119.0	117.1	133.2	143.7	140'6	136.3
47.6	143.7	141.5	140.8	139.8	138.8						$\left\{\begin{array}{c} -138\cdot7 \end{array}\right\}$	141.9
_						141.0	138.4	133.9	132.7	138.7	138.7 /	
33.9	133.5	133.3	133.8	133.8	131.6	132.6	133.7	133.7	133.7	133.9	139.3	135.6
	138.9	140.5	140.0	140.0	140.4	142.9	140.6	141.0	141.0	148.5	149.9	138.78
38:2				159.9	131.8	135.9	132.1	151.1	154.3	156.1	157.8	149'1
54.2	153.7	155.8	172.3									
50.07	151.60	150.60	149.79	149.62	147.93	147.13	144.57	145.67	146.12	148.94	149.89	148.8
					ATURE OF						1 0 1	. 0
54.3	54°2	$5\overset{\circ}{4}$ ·2	54°5	54.3	53.8	53.4	52.8	52.2	52°3	52°4	52.4	52°8
58.0	58.0	57.8	57.6	57.4	57.2	56.6	56.8	57.0	57.0	56.8	56.2	56.1
		61.5	61.3	60.7	60.2	90.0	59.7	59.2	58.9	58.6	57.6	59.6
61.5	61.4		59.0	59.0	59.0	59.0	58.8	58.9	59.0	59.0	59.2	59.1
59.6	59.2	59.0		65.2	64.7	64.2	64.3	64.0	63.7	63.2	$63 \cdot 2$	64.0
66.0	65.6	65.5	65.5			04.0	0.4.0	0.70	00 1	00 4		
69.1	68.7	68.4	68.3	68.1	68.0	0010	-	6110	61.0	61.0	61.0}	65.2
	<b>—</b>				-	63.0	62.5	61.9	61.2	61.8	58.2	60.6
61.2	61.3	61.3	61.5	61.2	61.0	60.5	60.5	60.0	59.5	59.2		
61.4	61.2	61.0	60.5	60.3	60.3	60.3	60.0	59.8	59.7	59.2	59.2	60.3
61.2	61.1	60.6	60'3	60.0	59.6	59.2	59.5	59.0	58.2	$58^{\circ}2$	58.0	60.2
58.1	57.8	57.6	57.4	57.2	56.7	56.3	56.0	55.7	55.5	55.0	54'4	56.8
59.4	29.0	58.9	58.9	58.7	57.8	57.4	56.5	55.4	55.2	55.0	54.6	57.0
54.5	53.4	53.5	53.0	53.0	52.8			_			— 1	53.6
- 1	00 I				_	53.6	53.2	53.0	52.8	52.7	52.8	
57:0	57.0	57·5	57.4	57.5	57.2	57.3	57.2	57.0	57.0	57.0	57.0	56.7
57.9	57.8		59.8	59.2	59.0	58.2	58.1	57.5	57.2	56.7	56.5	58.5
60.0	60.0	60.2		62.0	61.3	61.1	61.2	62.0	62.2	60.2	59.7	60.6
62.4	62.3	62.3	62.2						63.0	62.6	62.5	63.8
66.4	66.5	67.3	67.4	67:2	65.8	65.4	64.7	63.5		65.4	65.2	66.4
69.0	68.8	68.0	67.5	67.0	67.2	66.2	66.2	66.1	65.7	UU 4		
68.3	68.2	68.0	68.0	67.5	67.3			_	-	<u> </u>	$\{63.5\}$	66.1
			<del></del>	_		63.3	63.3	63.3	63.2	63.4	03.27	
65.0	65.0	65.0	64.6	64.4	64.0	63.5	63.0	62.5	62.5	62.3	62.1	63.8
62.4	62.3	62.0	61.5	60.8	60.7	60.6	60.4	60.5	60.2	60.2	60.4	61.4
67.6	67.6	67.3	66.8	66.7	66.5	66.3	65.2	64.8	64.2	64.0	63.2	64.5
68.8	68.8	68.1	67.6	67.2	66.6	66.4	66.0	65.2	65.0	64.5	64.4	66.0
		68.2	69.0	68.2	67.4	67.0	66.1	65.2	64.6	64.0	63.2	66.2
67.7	67.5				66.6	0, 0						
67.5	67.5	67.4	67.3	67.0	t .	65.9	65.2	65.2	65.0	64.8	$\{-64.5\}$	65.6
			70.0	-	60:0					66.2	65.8	67.8
69.9	69.9	70.1	70.0	69.6	69.0	68.5	68.3	68.0	67.0		59.5	65.5
66.8	66.4	66.5	66.4	66.0	65.2	63.8	62.1	61.2	60.6	60.0		
		61.0	60.5	60.3	61.2	61.2	60.0	59.2	59.0	58.5	58.0	60.1
60.6	60.4	01.0	1 00 0	000	) ""							

	O	ne Scale Div	vision = •00	0066 parts o	of the V.F.		ICAL FOR n Scale Divi		sponding to	1° decrease	of Tempera	ture, 1 ° 64.	
Mean ( gen T	Göttin- }	Oh.	1 ^h .	2 ^h •	<b>3</b> ʰ.	4 ^h .	5 ^h .	6 ^h •	7 ^h •	8 ^h .	9 ^h .	10 ^h .	11 ^h .
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	sc. Div. 156°4 152°7 142°9	Sc. Div. 154°9 149°7 143°1	Sc. Div. 152°6 147°9 143°0	Sc. Div. 150°2 147°6 139°6	Sc. Div. 148°7 144°8 137°6	Sc. Div. 145°7 143°5 136°3	sc. Div. 144'6 141'0 135'8	sc. Div. 146'6 142'2 136'2	Sc. Div. 146'6 142'5 135'1	Sc. Div. 146.6 141.9 135.0	Sc. Div. 146°6 141°4 135°0	Sc. Div 146°5 141°4 135°0
	4 5 6 7 8 9	136.8 145.9 150.6 146.9 144.2 138.5	136.8 144.4 150.9 146.1 142.9 138.7	134°3 145°2 146°7 143°1 142°9 137°1	133.6 145.4 144.7 143.1 141.2 135.0	134°1 146°4 145°8 141°9 141°0 132°2	134°2 146°4 145°8 140°4 138°0 131°2	135.7 146.4 144.6 138.0 135.0 131.2	136.9 147.7 144.3 138.0 132.9 132.3	137.3 147.7 144.3 139.8 132.9 134.2	140°4 148°5 145°3 141°3 131°6 133°7	143.8 148.5 144.0 141.1 132.5 137.2	143 · 8 148 · 8 143 · 8 140 · 7 132 · 7 140 · 8
JUNE.	11 12 13 14 15 16 17	143.5 148.5 152.8 146.4 123.3 122.0	143 ° 9 151 ° 0 152 ° 4 144 ° 7 122 ° 6 121 ° 0	143°1 147°7 151°3 138°8 120°4 120°5	141.7 144.8 151.3 136.7 118.7	141.8 143.0 150.9 132.6 117.7 117.4	140°5 143°8 148°6 130°1 115°2 115°3	140.7 144.7 148.6 125.3 114.9 115.1	141 · 1 144 · 9 148 · 1 123 · 3 113 · 4 114 · 0	143.6 144.9 149.2 123.3 111.5 115.3	145.7 144.9 152.9 123.6 112.8 116.1	145.7 144.9 153.8 119.2 113.0 116.0	145.7 144.9 160.4 119.2 114.0
	18 19 20 21 22 23 24	126°3 123°7 130°8 128°4 144°1 138°5	125°5 123°7 132°8 131°8 147°8 138°5	122 ° 9 125 ° 0 133 ° 1 136 ° 7 137 ° 1 138 ° 0	116.4 124.9 131.5 134.5 137.1 129.3	119.5 124.1 132.4 131.5 136.4 129.5	118·3 124·1 129·8 132·6 136·4 136·3	119.0 123.5 125.0 136.0 132.1 135.7	117.6 123.1 125.0 139.2 131.8 133.2	119°0 125°7 129°4 141°2 128°7 134°6	118 · 8 125 · 7 135 · 9 146 · 1 129 · 3 132 · 7	118 · 8 128 · 2 138 · 1 150 · 8 129 · 3 130 · 9	121°1 129°4 137°2 145°1 133°5
	25 26 27 28 29 30	129.6 132.0 126.3 132.2 131.9	128°3 131°8 125°4 130°2 131°9	126.7 129.3 125.4 127.0 129.3	121.5 126.4 123.3 124.4 128.1	121 ° 0 125 ° 7 121 ° 0 123 ° 4 126 ° 8	120.0 122.6 119.9 121.9 126.6	121.0 120.3 117.8 123.8 126.4	119 '8 120 '3 117 '8 123 '8 124 '2	119.8 121.6 119.0 123.8 124.1	119.8 120.5 121.7 121.6 124.2	121.8 120.9 123.3 121.6 125.4	121 · 3 122 · 7 124 · 4 121 · 8 125 · 4
ourly	Means	138.28	138.11	136.35	134.52	133.35	132.44	131.62	131.45	132.15	132.95	133.23	134'1
				1	TEMPERA	TURE OF T	HE VERTIC	AL FORCE	MAGNET.				
	$\left( egin{array}{c} 1 \\ 2 \\ 3 \\ 4 \end{array} \right)$	58.4 59.3 64.0	59.0 59.7 64.8	59.6 60.3 65.0	59.6 61.0 65.5	59.6 62.0 66.0	60°1 62°7 66°8	60°4 63°1 67°8	60°5 63°5 68°5	61°0 64°0 68°5	61.5 64.5 69.0	63.0 69.2	62·4 65·5 69·7
	5 6 7 8 9	66.5 62.0 59.8 60.5 62.5 65.9	66.4 62.0 59.7 60.4 63.2 66.2	66.5 62.0 59.8 60.8 63.5 66.5	66.7 62.1 60.3 61.2 63.8 67.1	67:3 61:5 60:5 62:2 64:6 68:0	67:4 61:5 60:5 63:0 65:5 68:3	67.5 61.5 60.6 63.3 66.0 68.5	67.5 61.8 61.0 63.5 66.5 68.7	67.4 62.0 61.5 64.1 67.1 69.0	67:3 62:4 62:1 64:6 68:0 69:3	67.3 62.7 62.8 65.4 68.4 69.7	67 · 4 62 · 7 63 · 1 65 · 5 68 · 5 69 · 7
JUNE.	11 12 13 14 15 16 17	62.0 59.4 58.8 61.0 74.3 74.7	62.0 59.5 58.8 62.0 74.4 74.9	62°2 59°6 58°4 63°0 75°4 75°1	62:3 59:7 58:2 63:5 76:2 75:3	62:5 59:8 58:5 65:6 77:0 77:2	62:4 60:2 59:2 67:5 78:0 77:1	61.9 60.4 59.4 70.0 78.5 77.6	61.7 60.3 59.4 71.6 79.5 78.4	61.9 60.3 59.7 73.4 79.8 78.0	61.8 61.0 60.2 75.0 80.7 78.4	62.6 61.5 60.8 76.4 81.0 78.9	62.8 62.0 61.0 76.7 80.5 78.5
	18 19 20 21 22 23 24	72.5 72.0 69.8 67.3 67.5 67.0	72.5 72.0 69.5 67.3 67.5 67.6	73.0 72.5 69.0 67.7 67.5 67.6	73.5 72.8 69.2 68.5 68.4 68.0	73.5 73.0 69.5 68.8 67.6 68.5	74·1 73·1 69·5 69·3 68·4 69·0	74.5 73.5 69.5 69.5 69.5 69.0	75·1 73·5 69·5 70·1 70·3 69·3	75.5 73.7 69.7 70.4 71.5 69.5	75°4 73°8 70°0 70°8 71°6 69°7	75.5 74.0 70.6 71.0 71.5 70.5	75°5 74°0 71°3 70°6 71°3 70°5
	25 26 27 28 29 30	69.6 70.7 72.6 69.1 68.6	70°0 70°5 72°5 69°5 68°8	70°9 71°1 72°5 70°5 69°8	72.0 72.0 72.7 71.0 70.3	72.5 72.1 72.9 71.5 70.5	73°3 72°7 72°9 72°0 71°3	74.0 73.1 72.9 71.6 71.6	75°5 73°5 72°9 72°0 72°3	75°9 74°5 72°9 72°5 72°5	76°3 75°0 73°0 73°1 73°2	76.7 75.5 73.5 73.5 73.5	76.7 75.5 73.5 73.6 73.5
	Means	65.99	66.18	66.23	66.96	67.41	67.92	68.28	68.71	69.09			70.0

	One Seels	Division -	•000066 ***	rts of the W		ERTICAL I		orresponding	z to 1° decre	ease of Tem	perature, 1·6	
12h.	13h.	14h.	15h.	16h.	17 ^h .	18h.	19h.	20h.	21h.	22h.	23 ^h .	Daily and Monthly Means.
sc. Div. 146.6 141.4	Sc. Div. 146 7 141 1	Sc. Div. 146 7 140 6	Sc. Div. 147 4 138 8	Sc. Div. 147.8	Sc. Div. 148'4 140'3	Sc. Div. 148 4 141 3	Sc. Div. 148 4 141 3	Sc. Div. 149 3 141 3	Sc. Div. 150 5 142 6	Sc. Div. 151'8 142'6	Sc. Div. 153 3 142 6	Sc. Div. 148.80 142.95
134'1	140.4	136.1	135.4	135.9	121.7	138.6	138.6	137.5	137.5	139.1	139.3	137.03
142.8 148.5	140 · 9 148 · 6	139°9 146°8	138'9 146'8	139.6 147.4	140°0 147°4	138.4 150.3	140°2 148°5	141.9 149.3	141.9 150.6	147.5 151.6	148.0 153.5	139·49 147·93
143.6 140.7	143.6 140.7	143.7 141.5	144.6 140.0	145.7 141.3	147°2 138°4	146.5 139.2	148.7 140.2	149.6 142.4	150°5 144°1	150°5 144°7	151.5 144.9	146.52 141.60
132.8	139.6	134·1 136·0	134'1 136'0	134.3 136.0	136.3 139.3	137.0	137.0	137.9	136.3	136.3	136.3	136.41
145 8	145.8	145.7	145.8	146.5	146.2	140.6 146.8	140°6 149°3	143.4 150.5	143.6 150.5	144.5 150.5	$\begin{bmatrix} - \\ 142 \cdot 1 \\ 152 \cdot 0 \end{bmatrix}$	137·37 145·53
145.4	145.4	145'4	145.6	145.6	146.0	142.5	139.4	147'1	149.2	150.7	150°7 149°7	145.88 148.91
154°2 118°8	149'0 118'8	147°2 118°7	145'8 118'1	144°4 118°1	145°7 119°5	144°3 119°5	141.4 120.8	141'4 120'8	140°9 120°8	149°5 125°0	123.3	125.22
113.0	113.0 114.0	111.8	113.4 122.0	113.6 122.0	113.8 122.0	116.0	117.3	117.8	118.2	119.7	120.7	116.09
						121.5	121.5	120.8	122.8	123.8 120.9	$\left  \frac{-}{126 \cdot 3} \right\}$	119°45 121°57
121°1 131°7	126.2 131.2	122 <b>·3</b> 124 <b>·</b> 9	123 <b>·</b> 2 128 <b>·</b> 9	124.6 128.6	124.6 130.3	124°0 130°3	123°0 130°6	122.4 130.3	122 <b>.</b> 1 130.3	132.7	134'1	127.72
130.7 142.0	132.1	133 <b>·2</b> 134 <b>·</b> 6	131.5 133.5	127 <b>.</b> 4 130 <b>.</b> 8	127 <b>.</b> 9 130.0	119.8 130.0	124.0 124.3	123.6 117.5	114.8 127.8	105 <b>.</b> 4 134 <b>.</b> 6	111°7 144°1	127.63 135.18
133.2	141.3 133.7	133.7	131.8	131.8	132.3	132.3	125.6	126.2	131.4	133.9	133.9	133.20
132.5	132.2	134.3	131.6	129'3	129'3	127.5	124.8	121.6	127.5	128.9	$_{129}$ .0 $\}$	131.54
121·3 122·7	123°0 123°2	122 <b>.</b> 1 122 <b>.</b> 6	122.0 122.6	123 <b>°</b> 0	123°3 122°0	123.5 122.6	123.5 123.8	124°4 123°8	124°4 124°1	128.5 126.8	128 <b>.</b> 8 126 <b>.</b> 3	123.27 124.05
124.4	124.0	124.3	125'9	127.8	127.8	127.8	124.0	125.3	128'4	130.1	131.8	124.45
121.9 123.2	122 <b>°</b> 0 123 <b>°</b> 5	121.5 127.5	123 <b>·</b> 9	123 <b>·</b> 9	$124^{\circ}8$ $123^{\circ}4$	125.5 123.4	123.5 123.8	119.7 123.8	121'1 121'4	125.2 125.1	125.4 123.7	123°92 125°32
133'46	133.60	132.96	132.73	132.78	132.21	132.98	132.47	132.69	133.60	135.58	136.27	133.74
			' <u>'</u>	ТЕМРЕ	RATURE OF	THE VERT	ICAL FORC	E MAGNET				
62.5	62°5	62.4	62.2	61.9	6 <u>1</u> °5	6°12	6Î.0	60.4	60°.0	59°·8	58°8	60°76
65.5 69.5	65.6 69.6	65°7 68°9	65°2 68°7	65°2 68°5	65°3	65.1	65.0	64.7	64.6	64.5	64.2	63°80 67°25
67.0	66.7	66.4	66.0	65.8	65.5	66.2 64.8	66°0 63°7	66.0 63.1	66°0 62°5	65.7 62.0	65.6 } 61.7	65.85
62.5	62.2	62.3	62.1	62.0	61.8	61.6	60.5	60.3	60.0	59.5	59.0	61.28
63°3 65°5	63°0 65°5	62.7 65.1	62.5 64.7	62.0 64.5	61.4 64.5	60°5 64°1	$\begin{array}{c} 60.2 \\ 63.6 \end{array}$	60°0 63°4	59.6 62.9	59·4 62·6	59°0 62°4	61.05 63.47
68·7 69·7	68.7 69.9	68.6 69.7	68.2 69.6	68.0 69.2	67.6 68.6	67.4	67.2	66.7	66.2	<u>-</u>	66.0	66.55
		_				64.0	63.6	62.7	62.5	62.1	$\frac{-}{61.9}$	67°10 61°44
62.6 62.3	62.0 62.0	61.6 63.0	61.5 61.5	61'2 61'4	$60.2 \\ 60.2$	60°2 60°6	60.3 60.0	59 <b>.</b> 6	59 <b>·</b> 2 59 <b>·</b> 7	59°0 59°4	59.1	60.23
61.5	61.6 77.5	62°0 77°5	62.4 77.0	61.7 76.6	61°5 75°7	61.5 75.0	61°5 74°7	60°9 74°6	60°4 74°4	60°1 74°0	60°3 74°0	$60.32 \\ 72.26$
80.8	81.0	81.0	79.8	79.3	78.6	77.7	77.5	77.1	76.6	76.1	75.3	78.17
78.3	77·5 —	76°0	76°5 —	76°5	76°4 —	75.0	74.5	74.3	73.7	73.5	$\frac{-}{73.0}$	76.22
75°0 73°4	74.7 73.0	74.7 72.5	74.5 72.4	74·3 71·6	73.7 71.3	73.7 70.9	73°5 70°0	73°3 69°6	73°0 69°2	72.6 69.0	72.4 69.5	74.00 72.10
71.3	71.3	70.5	70.8	70.8	70.5	70.5	70.5	70.0	69.5	69.4	68.3	70.02
70.2	70°5 70°8	70°0 70°5	69.8 70.5	69.6 70.2	69°5 69°7	69.3 69.5	69°1 68°7	69.0 68.2	68°5 67°9	68°5 67°5	68°2 67°2	69:35 69:35
70.6	70.2	69.6	69.8	70.0	69.4	71.7	71·5	71.2	70.7	70°5	$\frac{-}{70.4}$	69.67
76.7 75.0	76.0	75.6	75.0	74.3	73.7	73.3	73.0	72.7	$72.5 \\ 72.7$	$72.0 \\ 72.7$	71.5 73.0	73.74 73.55
73.2	74.8 73.0	74.8 73.0	75.0 72.5	75°0 72°3	74.6 71.6	74.4	73.7 71.5	73°4 71°0	70.6	70.0	69.3	72.25
73°5 74°0	73°5 74°0	73°3 73°5	73°3 73°7	72.6 73.8	72·3 73·6	71.5 73.5	71°1 73°3	70°8 72°7	70°5 72°5	69.6 72.0	69°4 71°0	$71.72 \\ 72.23$
70.02	69.93	69.65	69.44	69.15	68.77	68.25	67.89	67.53	67.15	66.83	66.21	68.24
	1	!	l	I	I	1	1	1	}	ł	Į l	1 .

January 21st and	$22_{\mathrm{nd.}}$			MAGNET	ICAL C	BSERVATIO	ONS.			,	
Mean Göttingen	Angu	lar Value of	one Scale I	Division =	0′′721.				DECLINAT	ion.	
Time.	10h.	11h.	12h.	13h.	14h.	15h.	16h.	17 ^h .	18h.	19h.	20h.
M. S.	Sc. Div.	Sc. Div.	Sc. Div. 114.2	Sc. Div.	Sc. Div 116*2		Sc. Div. 117.8	Sc. Div. 113*8	Sc. Div.	Sc. Div.	Sc. Div.
0 0	113.0	114.1	114.8	116.0	116.2		116.0	114.0	115.5	115.7	116.3
5 0		114.2	114.8	116.0	116.1		115.3	114.0	115.0	115.6	116.3
10 0	113.1	114.3	112.0	116.0	116.1		114.5	114.0	115.0	115.6	114.4
15 0	113.3	114.3	115.1	116.5	116.1		114.2	114.0	115.2	119.0	116.4
20 0	113.7	114.2	115.0	116.0	116.0		114.0	114.5	$\frac{115.2}{115.2}$	116.0	116.5
25 0	113.8			116.1	116.0		114.2	114.2	115.2	115.9	
30 0	114.0	114'1	115.0				113.8	114.4	115.2	116.0	116.5
35 O	113.9	114.7	115.0	116.2	116.0	122 2					116.5
40 0	113.8	114.8	115.0	116.9	116.0		113.2	114.4	115.2	116.1	116.0
45 0	113.9	114.5	115.0	116.7	116.1		114.0	114.2	115.3	116.5	115.8
<b>50</b> 0	114.0	114'1	115.0	116.2	116.0		113.8	114.5	115.5	116.5	115.8
55 0	114'1	114.2	115.3	116.3	115.8	118.8	114.0	114.7	115.4	116.5	116.0
M. S.	One S	Scale Divisio	on = '0000	087 parts o	f the II.	F.			Horizont	AL FORCE.	
2 0	625.0	621.3	622.0	621.0	620.0	618.0	621.2	621.2	620.7	620.4	620.8
Z U	625.3	621.8	622.0	620.5	620.0		620.0	619.4	620.6	620.4	621.0
$\begin{array}{ccc} 7 & 0 \\ 10 & 0 \end{array}$	-			620.0	620.0		620.0	619.8	620.2	620.6	621.0
12 0	625.1	622.0	621.0	620.0	620.0		619.2	619.7	620.6	620.8	620.8
17 0	625.0	622.0	621.4	-			617.4	620.0	620.5		
22 0	625.0	621.8	622.0	620.0	619.0	1	618.2	620.2	620.8	620.6	621.8
27 0	625.0	621.8	622.0	620.0	619.0					620.4	622.1
32 0	624.2	621.8	622.0	619.0	619.0		618.2	620.0	620.4	620.4	622.8
37 O	624.2	621.5	622.0	619.0	618.8		619.4	620.2	620.0	620.0	620.5
42 0	624.0	622.0	622.0	620.0	619.0		619.2	620.4	620.4	620.6	621.5
47 0	623.2	622.0	622.0	620.0	619.0		619.0	620.0	620.6	620.6	622.8
<b>52</b> 0	623.0	622.2	621.0	620.0	619.0		620.0	621.2	620.4	620.4	623'4
57 0	622.1	622.2	620.6	620.0	618.0	622.0	621.4	620.8	620.6	620.4	622.7
Thermometer	43.8	43.9	44.2	45.0	45°C	44.5	43.5	42.0	41°6	41°3	39.6
	One S	cale Divisio	n = .0000	63 parts of	the V. I	F.		,	VERTICAL	Force.	
M. S.		1	. <b>-</b>		1.5046	1,51.0	1500	15.0	1	1 .	1
3 0	176.5	175.9	171.9	170.1	173.2		172.9	174.2	174.5	175.5	178.0
8 0	176.5	175.7	171.9	170.1	173.8		173.1	174.2	174.5	175.3	178.0
13 0	176.5	175.7	171'4	170.5	173.8		173.6	174.2	174.5	176.8	177.8
18 0	176.5	175.7	171'4	171.1	173.8		173.6	174.0	174.5	176.8	177.8
23  0	176.5	174.9	171.4	171.1	173.8		173.6	174.1	174.5	176.8	177.8
28 0	176.5	174.9	171.4	171.8	173.0	172.0	173.8	$174  ^{\circ} 1$	174.3	177.8	177.8
33 0	176.5	174.9	171.4	171.8	172.6		173.6	$174 \cdot 1$	174.3	177.9	177.8
38 0	176.5	173.1	171'1	171.8	172.6		173.9	$174^{\circ}1$	174.3	178.0	178.0
43 0	176.5	173.1	171.1	171.8	172.6	3   172.0	173.8	174.6	175.2	178.0	178.3
48 0	176.5	173.1	171'1	172.5	172.6	172.6	173.6	174.4	175.2	178.0	178.3
<b>5</b> 3 0	176.5	172.5	170.6	172.5	172.6	172.6	173.6	174.4	175.4	178.0	178.3
58 0	176.5	172.5	170.6	172.5	171.9		174.3	174.4	175.4	178.0	178.3
Thermometer	42.6	42°8	44.6	45°6	44.6	44.8	44.1	42°·8	4i°8	41°2	40.2
							T				Deslination
· · · · · · · · · · · · · · · · · · ·			ME	TEOROLO	GICAT	OBSERVAT	····	creasing N	umpers deno	te decreasin	g Declination
		Ther	nometers.		JUAL	Wind.	±0±160+	1			
Mean Göttingen Time.	Barometer at 32°.	Dry.	Wet.	Direc	tion.	Fore	ce.	-	W	eather.	
р, н. м.	In.										
		95.6	94.0	NT 1	. 337	T:-1	h+	Close	in	1 1	
	29.545		24.9	N. by		Ligh Modes		Clear;	circum. and	i haze.	
11 0	29.554		24.5	N. by		Mode:			ircum. and		
12 0	29.598		22.6	N. by		Ligh			ircum. and	naze.	
13 0	29.616		21.1	N		Ligl Ero			circum.		
14 0	29.653		18.9	N		Free			with haze.		
	29.690		16.9	N. by		Brisk, wit		Clear; o			
15 0	29.712		13.4	N. by		Fres		Clear;			
15 0 16 0	00.755		11.8	N.N		Brisk, wit		Clear;			
15 0 16 0 17 0	29.755		1 0.40	N.N.	W	Bris	sk.	! Cloudy.	with haze.		
15 0 16 0 17 0 18 0	29.812		9.2								
15 0 16 0 17 0 18 0 19 0	29.812 29.839	6.0	6.2	N. by	r W.	Brisk, wit	th gusts.	Cloudy,	with haze.		
15 0 16 0 17 0 18 0 19 0 20 0	29.812 29.839 29.928	3.3 6.0	6.2 3.8	N. by	w.	Brisk, wit Moderate, w	th gusts.	Cloudy, Cloudy;	with haze.	ir.	
15 0 16 0 17 0 18 0 19 0	29.812 29.839	3.3 6.0	6.2	N. by	w.	Brisk, wit	th gusts.	Cloudy, Cloudy;	with haze.	ir.	

^{*} At 22^d 10^h, Thermometer of H. F., 39° 5; of V. F., 39° 0.

)			·			MAGNE	FICAL (	OBSERVATI	ONS.		Ja	nuary 21st	and 22nd.
			DECLINAT	ION.						ıla <b>r</b> Value o		Division= (	
	21h.	22h.	23h.	Oh.	1h.	2h.	3h.	. 4h.	5h.	61.	71.	8h.	9h.
	Sc. Div. 116'0 115'8 115'8	Sc. Div. 116.6 116.9 117.0	Sc. Div. 117 ° 0 116 ° 7 116 ° 2	Sc. Div. 118°3 118°4 118°8	Sc. Div. 119.6 119.2 119.9	Sc. Div. 120°2 120°8 120°8	Sc. Di 120*8 120*6	v. Sc. Div. 3119°1 119°0	Sc. Div. 116°2 116°0 116°0	Sc. Div. 112.7 112.0 111.7	Sc. Div. 108 * 8 108 * 8 108 * 6	Sc. Div. 108 0 108 2 108 7	sc. Div. 110 '4 110 '8 111 '0
	116.1 116.0 116.2 116.4 116.6	116.9 116.8 116.4 116.5 116.5	116.4 116.1 116.2 116.8 117.2	119.0 119.0 119.2 119.0 119.4	119.8 120.0 120.0 120.2 120.2	120°8 120°4 121°0 121°0 120°6	120°4 120°4 120°2 120°3 120°1	1 118°2 1 118°1 2 117°9 117°5	116 · 4 115 · 2 115 · 0 115 · 2 114 · 7	111.0 111.0 110.7 110.2 110.0	108:4 108:0 108:1 108:0 108:0	108.9 109.1 109.3 109.5	111.2 111.7 111.8 112.0 112.1
	116.8 117.0 116.8 116.7	116.9 117.0 117.0 117.0	117.4 117.8 117.8 117.9	119°3 119°8 120°1 119°9	120°3 120°7 120°3 120°3	120°8 120°8 120°8 120°4	120°1 120°0 119°5 119°5	117.0 117.0 116.8	114.2 114.0 113.2 112.7	109.7 109.4 109.2 109.0	108.0 108.0 107.9 108.2	109.8 110.0 110.2 110.3	112:2 112:3 112:8 113:0
			Horizonta	L Force.		1	ncrease,	in Scale Divisi	ons, correspo	onding to 1°	decrease of	f temperatur	e, 1 <b>°</b> 63.
	622.6 621.8 621.8 621.6 623.2 622.8 622.2	622.8 622.4 622.0 622.4 622.5 622.4 622.0	624·1 624·4 624·9 624·6 625·0 625·2 625·7	624'9 625'0 624'7 625'2 625'6 625'7 625'4	624·3 624·0 625·0 625·0 625·0 625·0 625·0	624.0 623.2 623.2 623.0 622.4 621.1 621.0	618.5 616.2 617.5 616.5 617.5 615.5	613.5 612.0 611.5 611.4 610.9	608·2 607·2 607·6 607·4 607·0 607·2 606·5	608 '4 609 '2 610 '0 609 '7 610 '3 610 '3 614 '0	616.0 616.8 617.0 618.7 619.7 620.1 621.2	624.8 625.8 625.9 626.7 627.9 628.5 630.0	634.5 636.0 635.1 635.0 635.4 636.3 637.2
	622 2 622 2 621 4 621 4 622 1 622 1	623 · 4 623 · 6 623 · 8 623 · 0 623 · 5	625 7 625 8 626 4 625 3 624 9	625 · 5 626 · 0 626 · 0 625 · 7 625 · 5	625 ° 0 624 ° 8 624 ° 8 624 ° 8 624 ° 5	620 ° 0 620 ° 8 620 ° 0 620 ° 0 618 ° 5	614.5 615.0 614.5 613.9 613.0	610°3 608°5 609°5 608°4	607 °0 606 °7 607 °2 608 °0 608 °2	615 1 614 0 613 2 614 5 615 6	621 · 2 621 · 9 622 · 0 622 · 8 623 · 1	630°8 631°3 631°6 632°8 633°9	637.7 638.0 638.0 637.7 638.7
	38.4				37.1	36°6	37.5	38.0	37.5	3 [°] 7.0	37.2	37.6	38°7ª
-								in Scale Divisi				I	
	179 · 1 179 · 1 179 · 1 180 · 4 180 · 4 180 · 4 180 · 4 179 · 3 179 · 3 178 · 6 178 · 6	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		180°2 180°2 180°3 180°3 180°3 180°3 180°7 180°7 183°2 183°2 182°2	183.0 183.7 183.7 183.2 183.2 182.8 182.8 182.3 182.3 182.3 182.3	182'3 182'3 182'3 182'3 182'3 182'3 182'3 182'3 182'3 182'8	182*8 182*8 182*8 183*4 183*4 183*8 183*8	184.6 184.6 184.8 185.3 185.3 185.4 185.4 185.8 185.8 187.2 186.8 187.0	187.5 187.5 187.5 187.6 187.6 187.6 187.6 187.6 186.5 187.4 187.3 188.1	188°1 187°4 187°4 188°1 188°1 187°7 188°1 187°0 187°0 187°0 187°4 186°3	187 · 2 187 · 3 187 · 0 187 · 0 187 · 7 186 · 0 186 · 5 186 · 2 186 · 4 186 · 0 186 · 0 186 · 0 186 · 2	186.2 186.0 185.8 185.5 185.5 185.5 185.5 185.4 185.1 184.9 184.7	
	39°·7	39°·3	38.8	38°·3	3 [°] 7	39°1	38.6	39°1	38.1	37°6	37.7	37.9	38.6ª
-	and increas	ing Horizon	ntal and Vert	ical Force.		The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s					
					ME'	TEOROLO	GICAL	OBSERVAT	IONS.				
-	Mean Gö Tim		Barometer at 32°.	Ther	wet.	Direc	tion.	Wind.	ce.	-	W	eather.	
	D. H 21 22 23 22 0 1 24 4 5 6 7 8	2 0 3 0 0 0 0 0 0 0 0 0 0 0	In. 29 993 30 039 30 078 30 120 30 144 30 154 30 167 30 157 30 135 30 147 30 184	1.0 -1.2 -0.7 -1.4 0.0 2.7 6.4 9.5 12.4 16.6 18.8 18.9	0'6 -0'7 -1'1 -1'9 -1'1 2'8 5'7 9'1 12'4 15'8 16'2 16'7	N N.N. N.N. N.N. N.N. N.N. N.N. N.N. N	.W. .W. .W. .W. .W. .W. .W. .W. .by N. .by N.	Moderate, w Mode Moderate, w Brisk, wit Brisk, wit Brisk, wit Brisk, wit Brisk, wit	rate. rate. rith gusts. ch gusts. ch gusts. ch gusts. ch gusts. ch gusts. ch gusts. ch gusts.	Clear; ci Clear; cu Clear; ci Cloudy, v Cloudy, w Clear; ci Clear; ci	th haze. th cum. ircum and rcum. tmstrat. rcum. vith haze. vith haze. rcum.		,

February 27th a	nd 28th.			MAGNET	TICAL OB	SERVATIO	ONS.				
Mean Göttingen	Angu	lar Value of	one Scale I	Division =	0′′721.				DECLINAT	ion.	
Time.	10 ^h .	11 ^h .	12h.	13h.	14 ^h .	15h.	16 ^h .	17h.	18h.	19h.	20h.
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Se. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
0 0	110.8	112.8	113.0	113.4	117.4	113.8	114.0	114.4	113.7	112.4	112.0
5 ()	111.0	112.6	113.0	113.8	117.0	113.8	114.0	114.9	114.6	112.9	112.0
10 0	111.0	112.8	113.5	114.0	116.6	113.8	114.2	115.1	114.8	113.0	112.4
15 0	111.0	113.0	113.4	115.0	115.0	114.0	115.0	115.8	114.0	113.9	112.4
20 0	111.5	113.0	113.7	114.8	113.4	113.2	115.3	116.1	114.0	114.5	113.1
25 0	111.5	113.5	113.8	114.4	115.2	114.2	115.2	116.1	114.0	113.0	113.5
30 0	111'2	112.8	114.0	114.6	115.4	113.8	116.9	115.7	114.0	112.2	114.3
35 0	111.7	113.0	113.8	114.4	115.0	113.4	115.8	115.9	113.7	112.2	114.8
40 0	111.8	113.2	113.7	114.4	115.6	113.6	115.0	116.0	113.0	111.9	114.7
45 0	112.2	113.4	113.5	118.6	115.4	113.8	114.2	115.8	111.0	111.2	114.7
50 0	112.3	113.8	114.0	122.0	115.0	113.4	114.3	114.2	110.8	111'5	114.5
55 O	112.8	113.4	114.2	119.9	114.0	113.9	114.3	113.1	111.5	111.8	114.8
M. S.	One S	Scale Divisio	on = .0000	087 parts of	the H. F.				Horizon	ral Force	
	C00:0	C02.0	699.0	609.4	694.0	605.4	610.0	610.6	616.4	600:4	699:1
2 0	622.0	623.2	623.0	623.4	624.2	625.4	619.8	619.6	618.4	622.4	622.1
7 0	622.4	623.4	623.2	624.2	625.0	625.2	620.4	619.0	610.0	622.2	622.8
12 0	622.0	623.0	623.4	623'4	626.0	624.0	620.3	618.4	619.8	623.0	622.8
17 0	623.2	622.6	623.4	622.6	625.8	625.4	620.6	618.2	621.0	623.0	623.0
22 0	623.6	623.0	623.6	622.6	625.4	625.2	620.1	618.0	621.8	623.0	623.0
27 0	622.2	622.8	623.8	622.5	623.8	623.8	619.0	618.8	621.3	622.7	623.2
32 0	621.8	623.0	624.0	624.0	624.2	623.0	619.9	617.0	621.9	622.9	623.0
37 0	622.0	623.2	621.0	623*2	624.2	622.2	620.8	616.4	622.4	621.9	623.0
42 0	621.2	623.2	621.8	623.2	625.8	621.4	620.6	617.4	622.4	621.2	622.0
47 0	621.2	624.0	622.0	625.0	626.0	620.8	621.0	618.8	621.4	621.9	621.8
52 O	622.0	623.8	624.0	627.4	625.8	620.2	620.0	618.6	621.0	622.0	621.0
57 0	621.8	623.8	625.2	627.2	625.2	619.0	619.0	618.7	621.2	622.2	621.0
Thermometer	38.8	38.2	3 <b>?</b> ·8	38.8	40°0	40.2	40°0	40°1	40°1	39°·8	38.9
M. S.	One S	Scale Divisio	on = .0000	063 parts of	the V.F.				VERTICAL	Force.	
	105:0	107:0	105.0	100.5	1100.0	150.5	101.4	1,00.2	1,00.0	1	150.0
3 0	185.9	185.2	185.0	182.7	180.5	179.7	181.4	180.5	180.3	179.4	179.0
8 0	185.9	185.3	183.9	182.7	180.2	179.7	181.4	179.7	181.3	179.4	178.9
13 0	186.0	185.1	183.9	182.7	180.2	179.7	180.9	179.7	181.1	179.3	178.9
18 0	185.6	185.0	183.7 183.6	182.7	180.5	179.7	181.6	180.3	180.9	179'3	178.9
23 0	185.7	184.9		182°2 182°2	180.5	179.7	181.3	180.3	180.8	178.8	178.9
28 0	185.6	185.0	184.6 183.6		180.2	179.7	180.7	180.5	180.8	178.6	178.9
33 0	185.5	185.0	ļ	182.5	180.2	179.9	181.5	180.3	180'4	178.7	179.0
38 0	185.3	185'0	182.8	181.9	180.7	179.4	181.5	179'4	180.0	178.9	179.0
43 0	185.5	185.0	182.7	181.9	180.7	180.4	180.3	179.7	180'4	178.9	179.4
48 0	185.0	185.0	182.7	181.9	180.4	180.5	180.3	180.8	179'8	179.1	179.5
53 0	185.0	185.0	182.7	181.9	180.4	180.4	180.5	180.8	179.8	179.1	179.7
58 0	185.0	185.0	182.7	181.4	180.4	180.4	180.2	180.3	179.4	179.1	179.7
Thermometer	38.3	38.1	38.3	39.0	40.0	40.0	40.0	40°2	40.3	40°4	4°0.0
							Increasing	Numbers de	note decreas	ing Westerl	y Declination
1	1		ME	TEOROLO	GICAL O	BSERVAT	IONS.				
Mean Göttingen	Barometer	r Ther	mometers.		Wind				117 ·*		
Time.	at 32°.	Dry.	Wet.	Direc	tion.	Force.			Weath	er.	
D. н. м.	In.										
27 10 0	1	1	-	~	_		- 1				
- 24 IU U 1	30.008		13.7			ery light.		; circum.			
	30.008 29.997					ery light.	Cloudy	; circum. a	and haze.		
11 0	3 29 997		11.7			ery light.		; slight sno	w.		
$\begin{array}{ccc} 11 & 0 \\ 12 & 0 \end{array}$			12.0			ery light.		; circum.			
$egin{array}{ccc} 11 & 0 & \ 12 & 0 & \ 13 & 0 & \ \end{array}$	29.971		70.₽		w i V	ery light.	Cloudy,	with haze.			
$egin{array}{cccc} 11 & 0 & & \ 12 & 0 & & \ 13 & 0 & & \ 14 & 0 & & \ \end{array}$	29°971 29°909	11.1	10.7			7.	1 ~-		_		
$\begin{array}{ccc} 11 & 0 \\ 12 & 0 \\ 13 & 0 \\ 14 & 0 \\ 15 & 0 \end{array}$	29.971 29.909 29.903	11.0	10.7	N. by	W.   V	ery light.		; circum. a			
11 0 12 0 13 0 14 0 15 0 16 0	29.971 29.909 29.903 29.883	11.1 11.0 10.7	10.7 10.2	N. by N.N.	W. V.	ery light.	Cloudy	; haze and s			
11 0 12 0 13 0 14 0 15 0 16 0 17 0	29.971 29.909 29.903 29.883 29.851	11.1 11.0 10.7 10.5	10.7 10.2 10.5	N. by N.N. N.N.	W.   Vo E.   Vo E.   Vo	ery light.	Cloudy Cloudy	; haze and s ; circum.	snow.		
11 0 12 0 13 0 14 0 15 0 16 0 17 0 18 0	29.971 29.909 29.903 29.883 29.851 29.827	11.1 11.0 10.7 10.5 10.7	10.7 10.2 10.5 10.5	N. by N.N. N.N. N.E. b	W. Vo E. Vo E. Vo y N. Vo	ery light. ery light. ery light.	Cloudy Cloudy Hazy;	; haze and s ; circum. occasional s	now.		
11 0 12 0 13 0 14 0 15 0 16 0 17 0 18 0 19 0	29.971 29.909 29.883 29.851 29.827 29.801	11.1 11.0 10.7 10.5 10.7 11.0	10.7 10.2 10.5 10.5 10.5	N. by N.N. N.N. N.E. b N.N.	W. Vo E. Vo y N. Vo E. Vo	ery light. ery light. ery light. ery light.	Cloudy Cloudy Hazy; Hazy;	; haze and s ; circum. occasional s occasional s	now.		
11 0 12 0 13 0 14 0 15 0 16 0 17 0 18 0	29.971 29.909 29.903 29.883 29.851 29.827	11.1 11.0 10.7 10.5 10.7 11.0	10.7 10.2 10.5 10.5 10.5	N. by N.N. N.N. N.E. b N.N. N.N.	W. Vo E. Vo y N. Vo E. Vo E. E.	ery light. ery light. ery light.	Cloudy Cloudy Hazy; Hazy; Hazy;	; haze and s ; circum. occasional s	now.		

^a At 28^d 10^h, Thermometer of H. F., 41° 4; of V. F., 40° 8.

1						MAGNET	ICAL C	BSERVA	TIONS.			Feb	ruary 27th	and 28th.
Ī			DECLINATION	ON.						Angu	lar Value	of one Scale	Division =	0'`721.
ľ	21h.	22h.	23h.	0h.	1 h.	2h.	3h.	4h		5 ^h .	6h.	7 ^h .	8h.	9h.
	sc. Div. 115 '4 115 '8 115 '0 114 '2 114 '0 113 '8 113 '6 113 '4 113 '0 113 '1 114 '0 114 '1	sc. Div. 114 2 114 6 114 7 114 8 115 0 114 8 115 0 116 0 116 0 116 0 116 0 116 0	Sc. Div. 116:0 115:5 115:9 116:0 115:6 115:4 115:9 116:0 116:0 116:0 116:2	sc. Div. 116.6 116.6 117.0 117.0 117.1 117.8 118.0 118.3 118.8 118.8 119.0	Sc. Div. 119.0 119.0 119.2 119.3 119.7 119.2 119.8 119.7 120.0 120.2 120.4 121.0	Sc. Div. 121 ° 0 121 ° 0 121 ° 0 120 ° 8 120 ° 6 121 ° 0 121 ° 2 121 ° 0 121 ° 0 121 ° 0 121 ° 0 121 ° 0 120 ° 6	sc. Di 120' 120' 120' 120' 120' 119' 119' 119' 119' 119' 119' 119' 11	66   117. 117. 116. 116. 116. 115. 115. 114. 114. 113. 113.	2   11 0   11 8   11 4   11 2   10 9   11 1   11 2   10 4   10 5   10 0   10	. Div 1 · 2 · 1 · 0 · 0 · 9 · 0 · 3 · 9 · 8 · 0 · 0 · 0 · 9 · 2 · 8 · 4 · 8 · 0 · 8 · 0 · 7 · 8	sc. Div. 108 ° 0 108 ° 0 108 ° 1 107 ° 9 108 ° 0 107 ° 4 107 ° 7 108 ° 0 107 ° 3 107 ° 0 107 ° 2 107 ° 1	Sc. Div. 107 °0 107 °0 107 °4 107 °1 106 °9 107 °0 107 °0 107 °1 107 °2 107 °2 107 °2 107 °3	Sc. Div. 107 * 5 107 * 8 108 * 0 107 * 9 108 * 2 108 * 6 108 * 8 108 * 3 108 * 7 109 * 0 109 * 2	sc. Div. 109 3 109 7 109 8 110 0 110 0 110 5 111 0 111 1 111 8 112 0
ŀ		<u> </u>	Horizonta					1	11			decrease of		1
	621 · 0 621 · 0 621 · 4 621 · 8 621 · 9 621 · 5 621 · 0 620 · 8 620 · 9 620 · 1 620 · 1 621 · 0	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				616.6 616.4 616.4 616.3 615.6 615.0 615.2 614.4 614.3 613.8 613.4	613 '2 '612 '2 '612 '3 '610 '4 '610 '4 '610 '4 '610 '6 '609 '8 '609 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '608 '8 '8 '608 '8 '8 '8 '8 '8 '8 '8 '8 '8 '8 '8 '8 '8	2   607 · 607 · 607 · 607 · 606 · 606 · 605 · 605 · 605 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 604 · 60	6   60 1   60 0   60 4   60 0   60 0   60 0   60 3   60 2   60	4.8 3.0 5.0 6.0 5.8 4.6 4.6 5.0 6.7 7.0 6.4 6.6	606.3 606.4 607.0 608.1 608.0 607.8 609.0 608.4 608.8 608.2 609.2 609.6	610.0 610.8 610.6 610.2 610.0 611.9 611.8 612.0 613.7 613.6 613.4	613.8 614.0 614.4 612.0 613.0 613.6 615.0 617.0 617.0 617.0 618.0	618.0 618.0 617.0 617.5 617.0 616.8 617.0 617.0 617.0 617.0 617.0
-	39°2	39°5	39°·5	39°0	39.0	38.0	37.8	38.	0 3	°.0	40°0	4°°4	40°·8	41°0°a
-			VERTICAL ]	Force.		I	ncrease,	in Scale Di	visions, c	orrespor	iding to 1°	decrease of	Temperatur	e, 1 · 80.
	179.7 179.7 179.7 181.0 181.1 181.2 181.2 181.5 181.5 181.5	181.5 181.7 181.4 181.4 181.4 181.6 181.4 181.3 181.3 181.3	182'1 182'1 182'1 182'1 182'1 182'1 182'1 182'1 182'1 182'5 182'5 182'5	183.0 183.0 183.0 183.6 183.6 183.6 183.6 183.6 183.6 183.6	184.7 184.7 184.8 184.6 184.8 184.7 184.7 184.9 184.9 185.0 185.2	185·2 185·1 184·9 185·2 185·1 185·5 185·6 185·6 185·6 185·6	185.6 185.2 185.4 185.4 185.1 185.5 184.9 184.9 185.2	185° 184° 184° 184° 184° 185° 185° 185° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184° 184°	5   18 9   18 9   18 6   18 4   18 0   18 0   18 5   18 6   18	4.7 4.3 4.3 4.5 4.8 4.5 4.5 4.5 4.7 4.3 4.3 4.3 4.3	183.7 183.7 183.7 183.7 183.7 183.5 183.5 183.5 183.5 183.5 183.3	183°3 183°0 183°0 183°0 183°0 183°0 183°0 182°8 182°8 182°8 182°4	182'4 182'7 182'7 182'2 182'2 182'2 182'2 182'2 182'6 182'5 182'5	182.7 182.7 182.7 182.7 182.3 182.3 182.3 182.3 182.3 182.3 182.3
-	40°0	40°0	40°0	40°0	39°5	38.4	38.3	38.	5 3	Ď·4	40.0	40°0	40°1	40°6 a
-	and increas	sing Horizo	ntal and Vert	ical Force.										
-		1	1			TEOROLO	GICAL		ATIONS	S.				
	Mean Go Tir		Barometer at 32°.	The Dry.	wet.	Direc	ction.	Wind.	Force.			w	eather.	
		2 0	In. 29.757 29.731 29.727 29.727 29.740 29.720 29.724 29.714 29.708 29.695 29.692 29.694	11.8 11.6 11.3 11.8 12.4 14.9 16.7 18.3 18.5 17.7 18.1 19.4	10.5 10.8 11.4 14.1 15.8 17.3 17.5 17.1	N.E. N.E. N.E. N.E. N.E. N.E. E.N	E. E. by N. by N. E. by E. E. by E. by E. by E. by E. by E. l. by E. l. l. E.	M Moderat M M Moderat Moderat M Moderat Moderat Moderat Moderat	oderate oderate e, with e, with oderate e, with e, with e, with	gusts. gusts. gusts. gusts. gusts. gusts. gusts.	Cloudy, Cloudy; Cloudy; Cloudy; Fair, wit Fair, wit Cloudy, Cloudy; Cloudy; Cloudy;		d haze. um.	

March 18th and						BSERVATIO					
Mean Göttingen	Angu	la <b>r V</b> alue of	one Scale I	Division =	0''721.			-	Declinati	ON.	
Time.	10h.	11h.	12h.	13b.	14h.	15h.	16h	. 17 ^h .	18h.	19h.	20h.
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. D'v.	Sc. Div.	Sc. Div.	Sc. Di		Sc. Div.	Sc. Div.	Sc. Div
0 0	108.9	111.5	112.2	126.6	110.1	112.8	113.0		113.9	114.0 113.9	114.0 114.2
5 0	109.0	111.4	112.4 113.8	124°0 120°3	110.8	113.0	113.0		114.0	114.9	114.6
10 0	109.8	111.8 112.0	118.8	116.8	111.6	113.0	113.0		114.0	114.1	115.1
$\begin{array}{ccc} 15 & 0 \\ 20 & 0 \end{array}$	111.6	112.0	125.4	115.0	1112.0	112.9	113		114.0	114.1	114.1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	111.0	112.0	125.6	114.6	112.0	112.9	113		114.0	114.2	113.1
30 0	110.4	112.0	124.8	113.7	112.5	112.8	113		114.0	114.3	113.2
35 0	110.8	111.6	126.4	112.0	112.1	113.0	113:5		114.0	114.3	113.9
40 0	111'4	111'4	128.6	111.5	112.3	113.0	113.2		114.0	114.5	114.1
45 0	111.0	112.5	128.8	110.7	112.2	113.0	113.5		114.0	113.3	114.6 115.3
50 0	111.5	112.0	128.9	110.5	112.7	113.2	113.2		114.0	113.8	115.3
55 0	111.5	112.6	128.6	110.5	112.6	113.0	113.	110 0	114 0	110 0	110 0
N 6	One S	cale Divisio	n = .0000	987 parts o	f the II.F.			H	ORIZONTA	L FORCE.	
м. s. 2 0	600.9	607.0	600.8	595.0	602.8	603.4	603		602.0	602.0	600.0
7 0	601.8	607.2	599.6	595.0	603.0	603.0	603.0		602.0	602.0	601.5
12 0	601.6	608.8	600.0	594.2	602.8	603.7	602.9		602.0	601.5	601.2
17 0	603.2	607.2	597.6	593.1	602.4	604.0	603.0		602.2	601.0	601.0
22 0	606.6	606.8	597.6	593 <b>°</b> 0	602.4	603.8	602.8		601.4	601.0	601.2
27 6	607.0	607:5 606:8	597.8 595.2	595 6 597 2	603.0	603.4	$\frac{602}{602}$		601.4	601.0	601.0
$\begin{array}{ccc} 32 & 0 \\ 37 & 0 \end{array}$	607.0	606.8	590.7	599°6	603.0	603.0	602		601.0	601.0	602.0
42 0	607.4	606.8	592.0	601.8	603.6	603.2	602		600.9	602.0	602.0
47 0	606.8	602.7	593.0	602.0	603.0	603.2	602		600.8	601.0	602.0
52 0	607.2	601.8	592.8	601.9	603.2	603.4	602.0		600.8	600.0	602.0
57 0	605.4	602.0	594.2	603.0	603.4	604.0	602.0	901.6	601.8	601.5	601.0
Thermometer	52.4	52°·2	52.0	52°7	53.0	53°3	53.8	54.0	54.0	53°·6	53.2
	One S	cale Divisio	n = .00000	6.				7	FERTCAL F	orce.	
м. s. 3 0	163.4	164.4	164.7	161.2	156.5	155.9	156:2	2   156.2	156.2	153.8	154.4
8 0	164.5	164.6	165.1	159.1	156.2	156.4	158		156.2	153.7	154.4
13 0	164.2	164.6	165.1	158.1	156.0	156.5	158.8		156.2	153.7	154.4
18 0	164.2	164.7	165.5	158.3	156.0	156.2	155.8	3 155.1	156.3	153.7	154.4
23 0	164.3	164.7	164.2	158.7	156.0	155.6	155.8		156.3	153.9	154.4
28 0	164.8	164.7	164.2	158.6	156.4	155.6	156.9		154.4	153.9	154.4
33 0	164.8	164.7	163.3	158.0	156.3	156.5	156.9		154.6	153.9	155.0
38 0	164.1	165.5	161.9	158.0	156.1	156°2 155°7	156°2		154°1 154°1	153°9 153°9	$\begin{array}{c} 155.2 \\ 155.2 \end{array}$
43 0 48 0	164°1 164°1	$\frac{165.2}{165.2}$	161.7 161.9	$\begin{array}{c} 158.0 \\ 157.5 \end{array}$	156.4	155.7	156 2		154 1	154.4	155.8
$\frac{48}{53} = 0$	164 1	164.8	160.9	157.5	156.0	156.3	156.2		154.1	154.4	155.8
58 0	164.4	164.8	161.2	156.9	155.9	156.3	156.5		153.8	154.4	156.5
Thermometer	5 <u>1</u> .1	5 l° 1	5 Î · 1	53.2	54.1	54.0	54.5	3 54.1	53.9	54°4	54.3
<u> </u>	1				The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon		Increasi	ng Numbers de	note decreas	ing Westerl	y Declinatio
			MI	ETEOROI	OGICAL	OBSERVA	TIONS.				
Mean Göttingen	Barometer		mometers.			Wind.			Wes	ather.	
Time.	at 32°.	Dry.	Wet.	Dire	ction.	Force.					
D. H. M.	In.	٥	0								
18 10 0	29.752	39.5	35.3		C.	Very lig		Cloudy; cir			
11 0	29.754	37.6	34.0	E E		Very lig		Cloudy; cir			
$\begin{array}{ccc} 12 & 0 \\ 12 & 0 \end{array}$	29.750	35.1	$\frac{32.1}{30.4}$		y N. y N.	Very lig Very lig	ht.	Cloudy; circ			
$\begin{array}{ccc} 13 & 0 \\ 14 & 0 \end{array}$	29.735 29.736	32.4	29.3	E.N		Very lig		Generally clo			
15 0	29.716	33.2	30.5	N.		Very lig	ht.	Cloudy; circ			
16 0	29.715	33.9	30.1	N.		Very lig	ht.	Cloudy; circ			
17 0	29.720	33.3	29.4	N.E.	by N.	Very lig	ht.	Cloudy; cir			
18 0	29.722	32.9	29.2	N.E.	by N.	Very lig		Cloudy; cir			
19 0	29.715	34.6	31.5	N.N	V.E.	Very lig		Cloudy; circ			
				1	- 1	71 1		Ol 1			
20 0 21 0	29.690 29.681	34.1	30.7	-	-	Calm. Calm.		Cloudy; circ			

^a At 19^d 10^h, Thermometer of H.F., 56° '3; of V.F., 56° '2.

T					354 037000				· · · · · · · · · · · · · · · · · · ·		10.	. 10.
		<b>T</b>			MAGNET	ICAL O.	BSERVAT				March 18th	
		DECLINAT		1				T	<u> </u>		e Division =	1
211.	22h.	23h.	0h.	1h.	2h.	3 ^h .	4 ^h .	5h.	6 ^h .	7h.	8h.	9h.
Sc. Div. 114.8	Sc. Div. 115.0	114.5	Sc. Div. 115.0	Sc. Div. 117.6		Sc. Div. 118 ²	Sc. Div.	Sc. Div. 114 O	Sc. Div.	Sc. Div. 108*2	Sc. Div. 107.0	Sc. Div. 107 3
114.6	114.8	114.5	115.2	117.8		118.2	117.7	114.1	110.5	108.0	107.0	107.2
114.1	114.2	114.6	115.3	118.6		118.2	117.2	115.6	110.0	109.0	107.2	107.4
114.1	114.2	114.7	115.4	118.2		119.9	116.2	114.3	109.8	108.0	107.2	107.8
114.1	114.3	114.3	116.0	118.4	120.2	119.7	116.3	114.0	109.5	107.0	107.0	107.0
115.0	114.8	114.4	116.0	119.6		119.6	115.9	114.0	109.0	107.0	107.4	107.8
114.8	114.8	114.4	117.2	119.6		119.8	116.2	112.9	108.3	107.0	107.0	107.8
115.0	114.2	114.6	116.8	119.4		119.2	116.0	112.0	108.0	107:2	107.4	107.8
114.8	114.2	114.4	117.2	119.0		118.9	116.6	111.8	108.1	107.2	107.8	108.8
115.0	114.0	114.3	118.0	119.8		119.0	116.0	111'4	108.0	106.8	107.6	109.2
115.0 114.7	114.5	114.6	117.8	119.8		118.2 $118.2$	116·1 115·0	110.8	108.0	107.0	107.8	109.0
	111 0	1	1		1			<u> </u>	<u> </u>	!	<u> </u>	
		Horizont	AL FORCE		Inc	rease, in	Scale Divisi	ons, corresp	onding to 1	decrease of	f Temperatui	e, 1.63.
600.0	600.0	601.0	600.0	598.0		585.0	583.4	581.8	578.0	578.5	583.4	589.8
600.0	601.5	601.4	600.3	597.0		583.8	585.2	581.8	577.0	579.5	583.4	591.3
600.0	601.7	600.6	600.4	597.4	593.7	$585^{\circ}6$	585.0	581.0	577.2	580.0	584.7	592.4
600.8	601.4	600.8	600.6	597.2	593.2	584.5	585.0	578.2	574.5	581.0	585.0	593.2
601.0	601.4	600.4	601.6	597.0		586.4	584.0	579.0	573.6	582.0	585.4	599.2
601.0	600.6	600.8	601.8	598.2	592.0	585.6	582.1	578.0	575 5	582.5	587.0	596.8
601.0	600.4	600.6	600.0	595.4		584.0	581.5	578.0	574.5	583.0	584.8	595*8
600.0	601.6	601.0	600.6	596.0		584.0	582.0	578.2	575.5	583.0	587.4	596.0
600.0	601.4	600.2	599.2	595.4		582.0	582.4	578.0	576.0	581.3	587.2	594.7
600.5	601.6	599.8	601.0	595.2		583.8	582.2	577.0	578'3	580.2	585.7	590.0
601.0	601.6	600.0	597.7	594.2		583.8	579.9	578.2	577.0	581.4	587.4	590.7
600.0	601.8	600.3	598.8	593.4	586.6	285.0	580.2	577.8	577.0	581.6	588.2	591.2
53°2	53.0	53.2	53.5	53.0	52°·6	53°•4	54.0	55.0	$5\mathring{5}^{*}2$	56.0	56.4	56°5°
_		VERTICAL	Force.		Incre	ase, in Sc	cale Division	ıs, correspon	ding to 1°	decrease of '	Гетреrature,	1.80.
156.2	156.2	155.2	156.7	155.5	159.7	59.3	158.6	156.3	155.0	154.9	153.9	154.3
156.9	156.5	155.3	156.6	156.1	159.6	58.7	158.6	156.2	155.0	154.9	153.9	154.4
156.9	156.5	155.4	156.5	156.1	159.9	59.2	158.3	156.5	154.5	154.9	154.0	154.3
156'9	156.5	155.4	156.5	157.6		$.59^{•}2$	158.3	155.8	154.5	154.9	154.5	154.5
156.9	156.5	155.4	156.5	157.6		.59 <b>°</b> 6	158.3	156.0	154.5	154.9	154.2	156.0
156.9	156.4	155.4	156.5	158.3		59.3	157.3	156.0	154.8	154.9	154.2	156.0
156.9	156.4	155.7	156.2	158.8		59.3	157.1	155.6	154.8	154.9	154.2	155.1
156.9	156.6	155.5	156.0	158.8		58.8	157.1	156.0	154.8	154.6	154.2	155.2
156.9	156.6	155.4	156.0	159.3		58.7	157.1	155.2	154.8	153.7	154.2	154.9
156.9	156.5	156.5	156.1	159.3		58.7	156.3	155.2	154'9	153.8	154.3	154.9
156.9	156.5	156.5	154.8	159.3		58.6	156.3	155.5	154.9	153.8	154.3	156.0
156.9	156·5	156.7	155.5	159.6	159.3 1	58.6	156.3	155.2	154.9	153.9	154.3	154.7
53.8	53°5	53.5	53°3	53°3	53°1	$5\mathring{3}\cdot 4$	5 <b>4°</b> 1	54°3	5 <b>4</b> °9	5а5	55°6	56.1ª
and increasi	ing Horizo	ntal and Ver	tical Force.									
				ME	TEOROLOGI	CAL OI	BSERVATI	ONS.				
Mean Gö	ittinger	Barometer	Thern	nometers.	]	Wind.						
Tin		at 32°.	Dry.	Wet.	Direction.		Force.	-		Weatho	er.	
р. н.	. м.	In.	0									
18 22	i i	29.675	34.6	91.7			Calm.	CI.		3.1.		
$\frac{16}{23}$		29 691	35.3	$\begin{vmatrix} 31.7 \\ 32.5 \end{vmatrix}$			Calm. Calm.		circum. an			1
19 0		29.691	35.1	32.9			Jaim. Jaim.		circum. ar			Į.
13 0	I:	29.691	$\begin{array}{c c} & 36.9 \\ \hline & 39.1 \end{array}$	33.6	N.E.		y light.		circum. ar			i
$\frac{1}{2}$	f!	29.654	38.3	33.5	E.N.E.	Ver	y light. y light.		strat. and h			
$\frac{2}{3}$		29 657	43.0						strat. and h			1
	- 19	29.654	45.0	37.0	E. by N.		y light.		strat. and h			1
4 5	0	29.639	46.5	36.7	E. by N. E. by S.		y light.		cirstrat. a			1
6	0	29.610	47.8	39.4	E. by S.	Ver	y light. y light.		cirstrat. a			ļ
7	0	29.611	49.5	41.9	12.		y ngm. Calm.		circum. an circum. an			I
8	o l	29.602	46.7	40.2			Calm.			nd strat. nd cirstrat.		1
9		29.606	45.3	39.6	_		Calm.			id cirstrat.		1
	-		100			1	~	J.oudy ,	cuille di			1
	1		1	1	1	1		1				

April 22nd and 23	3rd.			MAGN	ETICAL	OBSERVAT	YONS.				
Mean Göttingen	Angula	r Value of	one Scale D	ivision = 0	oʻ·721.				DECLINAT	TION.	
Time.	10h.	11h.	12h.	13 ^h .	14h.	15h.	16 ^h .	17h.	18h.	19h.	20h.
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.		Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
0 0	108.9	111.9	111.9	113.0	110.7	112.6	112.8	111.9	113.0	113.6	114.0
$\begin{array}{ccc} 5 & 0 \\ 10 & 0 \end{array}$	109.8	112.0	111.8	113.8	110.9	112.2	112.8	111.5	113.0	113.6	114.2
10 0	110.0	112.2	112.5	114.7 114.4	110.4	112.1	$\frac{112.7}{112.9}$	111.8	113.0	113.8	114.8 114.8
$\begin{array}{ccc} 15 & 0 \\ 20 & 0 \end{array}$	110.0	112.6 112.8	112.0 115.0	113.8	111.0	112.0	112.9	111.7	113.0	114.0	114.7
$\begin{array}{ccc} 20 & 0 \\ 25 & 0 \end{array}$	110.3	112.6	111.5	112.2	111.9	112.4	112.8	112.2	112.3	113.6	114.3
30 0	110.3	112.4	110.8	111.8	112.0	112.6	112.1	112.2	113.0	113.4	114.2
35 O	110.9	112.4	110.3	111.8	111.8	112.8	112.1	112.0	113.0	113.8	114.3
40 0	111.0	112.2	111.5	112.2	112.0	113.0	112.0	112.0	112.8	114.0	114.3
45 O	111.0	112°3	114.0	112.9	112.8	113.0	112.1	112.0	113.0	114.2	114.3
50 O	111.8	112.2	115.9	112.1	112.3	113.0	112.2	112.3	113.4	114.0	114.7
55 0	111.8	111.8	113.8	111.1	112.5	113.0	112.1	112.7	113.3	114.0	114.8
M. S.	One Se	cale Divisio	n = .000	087 parts <b>o</b>	f the II. F	•			Horizon	AL FORCE	. ·
	588.5	593.2	592.0	566.8	587.0	585.8	585.9	586.9	585.2	586.0	587.0
$7  {0 \atop O}$	$\begin{bmatrix} 589.0 \\ 589.0 \end{bmatrix}$	593 2 596.0	590 <b>·</b> 9	567*9	587.4	585.6	586.0	585.5	585 2	585.9	587 0
12  0	589.8	599.8	588.5	570°5	583.0	586.0	586 <b>.</b> 0	585.8	585.0	586.2	588.0
17 0	587.0	600.8	588.6	575.0	583.0	586.0	586.5	586.0	585.0	586.4	588.2
$\begin{array}{ccc} 17 & 0 \\ 22 & 0 \end{array}$	590.2	601.0	585.6	578.0	582.0	586.0	587.0	585.0	586.0	586.6	588.2
$\begin{array}{ccc} 22 & 0 \\ 27 & 0 \end{array}$	590.3	600.0	585.8	379.2	581.2	585.9	587.0	586.0	585.9	586.6	588.0
32  0	592.9	598.8	584.8	579.2	584 4	586.0	587.0	586.0	586.0	586.8	587.6
37 O	595.5	599.4	585.0	579.0	584.0	586.1	586.0	586.0	586.8	586.2	587.5
42  0	595.0	596.0	584.8	581.2	584.2	586.2	586.5	586.0	586.0	586.2	587.5
47 0	595.0	594.2	580.0	585.8	585.0	586.2	586.1	586.0	585.0	586.3	588.0
$ \begin{array}{ccc} 52 & 0 \\ 57 & 0 \end{array} $	593.2	591.0 591.2	581.2 $573.8$	588.2 589.0	585.8	586°2 586°0	586°5	586°0 585°5	585°3	586.4	587.8 588.3
	60.5	60.3	60.0	60°1	60.3			·	-		59.4
Thermometer	11			!	1	!	59°0	59.2	59.4	59°1	59*4
M. S.	One S	cale Divisio	n = 000	063 parts o	f the V. F	·			VERTICAL	Force.	
3 0	206.4	207.6	209.4	209.1	202.5	200.3	200.6	203.1	203.3	203.7	204.2
8 0	206.6	208.1	209.6	209.1	202.5	200.5	201.4	203 1	203.1	203.7	204.0
13 0	206.6	208.9	210.3	207.5	202.1	200.4	201.4	203 1	203.1	204.3	204.0
18 0	206.4	208.6	210.3	207.0	201.9		201.4	203.1	203.4	204.2	204.1
23 0	206.4	208.6	210.7	205.7	200.9		202.4	203.3	203.4	204.4	204.1
28 0	206.7	209:3	210.7	205.7	200.9	200.1	202.4	203.3	203.4	204.4	204.2
33 O	207.6	209.3	210.7	205.1	201.3		$202 \cdot 4$	203.3	203.4	204.3	204.2
38 0	207.6	209.5	211'1	205.1	200.5		202.4	203.3	203.5	204.2	204.2
43 0	207.5	209:3	211.0	204.4	200.5	1 :	203.3	203.3	203.6	204.2	204.2
48 0	208.6	210.5	211.0	204.4	200.0		203.0	203.3	203.7	204.2	204.4
53 0 58 0	207.5	210'4 209'4	210°7 210°7	203.6	200.0		203.0	203.3	203.7	204.2	204.4
58 0	207.4	200 4 	210 /	200 0	200 3	200.2	203.1	203.3	203.7	204.5	204.4
Thermometer	59·4	59°.6	60.0	60.0	6η1	6η1	60°6	60°2	60°.0	60°0	59.2
							Increasing	Numbers de	enote decreas	ing Westerl	y Declinati
			M	ETEOROL	OGICAL	OBSERVAT	ions.				
Mean Göttingen	Barometer	. The	rmometers.		Win	nd.			***		
Time.	at 32°.	Dry.	Wet	. Dire	ection.	Force.	_		Weath	er.	
D. H. M.	In.	0	•								
22  10  0	29.704	52.0			by S.	Very light.	Cloudy	; circum.	, cirstrat.,	and haze.	
11 0	29.700	48.7	45.9	-	-	Calm.		; circum.	, cirstrat., a	and haze.	
$\frac{12}{10} = 0$	29.672	46.8			-	Calm.	Cloudy	; circum.	and haze.	•	
13 0	29.668	44.8			_	Calm.	Cloudy	; circum.	and haze.		
14 0	29.680	43.8			W.	Very light.		; circum.	, cirstrat.,	and haze.	
$\begin{array}{cc} 15 & 0 \\ 16 & 0 \end{array}$	29.668 29.656	44.2			-	Calm.		; circum.			
10 0	29.644	44.6			_	Calm. Calm.		; circum.			
17 0					-	Calm.	Cloudy	; circum.	and haze.		
$\begin{array}{cc} 17 & 0 \\ 18 & 0 \end{array}$	29 645	40.0	1								
$\begin{array}{cc} 18 & 0 \\ 19 & 0 \end{array}$	29.645 29.645	46°3			_	Calm.	Cloudy	; circum.,	, strat., and	haze.	
18 0			45.5	_	_		Cloudy	; rain.	, strat., and	haze.	

^a At 23^d 10^h, Thermometer of H. F., 61° '3; of V. F., 61° '0.

					MAGNET	ICAL OB	SERVATIO	NS.				April 22nd	and 23rd.
		DECLINAT	ion.						An	igular Value	of one Scal	e Division =	
21 ^h .	22h.	23h.	Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5		6 ^h .	7 ^h .	8 ^h .	9 ^h .
Sc. Div.	sc. Div. 115 2 115 6	sc. Div.	Sc. Div. 118 '8	Sc. Div.	Sc. Div. 120.8	sc. Div.	Sc. Div.	105		Se. Div.	Sc. Div. 101 2 101 2	Sc. Div. 103 2	Sc. Div. 104.9
115°2 115°2	115 6	116.4 117.8	119.0	120.2	119.8	116.7	111.0	105 105		102.0	101.4	103.4	105.0
115.2	115.4	118.0	118.8	121.1	119.0	116.0	110.8	104	.0	102.0	101.4	103.6	105.4
115.0	116.2	118.0	118.8	120°4 120°7	118.8	115.8	109.8	104 103		102.0	101.6	103.8	104°3 104°2
115.0	116.5	118.2	119.8	120.5	118.8	115.2	108.5	103		102.0	102.0	104.2	104.8
115.2	116.0	118.0	119.2	121.0	118.3	114.8	108.0	103	٠1	102.0	102.0	104.4	105.0
115.2	116.2	118.5	119.2	122.0	118.2	114.2	107.7	103		101.6	102.0	104.4	105.8
115.2	116.0	118.6 118.2	118.3	122.4 121.0	118 <b>°</b> 0	113.1	107.1	102		101.0	102.3	104.4	106.3
112.3	116.0	119.0	110.0	120.7	117.0	112.8	106.6	102		101.5	102.8	104.4	107.0
		Horizont.	al Force		I	ncrease, in	Scale Division	ons, cor	rresp	onding to 1°	decrease of	f Temperatur	e, 1 <b>6</b> 3.
588.2	589.4	592.2	593.8	592.6	588.0	574.2	570.5	571		576.1	580.8	585.0	597:8
588.3	590.2	592.8 593.2	594.0 595.4	592.8 591.2	585.8 586.0	573.4	569.8	572 572		576.0 577.0	580.6 581.0	586°2 588°2	596 <b>·</b> 4 595 <b>·2</b>
588.2	589.2	593.2	593.6	591.8	584.7	573.5	568.7	571		578.0	581.4	589.0	605.6
588.6	589.0	593.2	593.8	590.4	582.2	572.0	569.2	571	.0	578.0	581.6	589.4	610.2
588.4	588.4	593.2	594.2	592.0	581.0	571.6	569.6	571		578.6	582.2	589.0	611.8
588.3	588°2 588°4	592.0 592.2	594.0 593.4	590 <b>.</b> 8	578°8 578°4	571.3 571.0	569.4	571		578.8	583°2 584°0	588°2 588°2	$\begin{array}{c} 612 \cdot 2 \\ 608 \cdot 4 \end{array}$
588.2	590.2	592.2	593.6	589.8	577.2	571.0	569.0	573		579.0	583.6	591.8	604.8
588.2	591.0	592.4	593.0	591.0	576.8	571.4	570.0	574	0	579.7	586.0	598.4	597.4
588.7	592.2	590.0	594.7	589.0	575.8	571.2	570.8	574		580.6	583.0	600.0	595 <b>.</b> 5
588.2	593.4	593.4	593.3	589.0	575.0	570.3	571.0	575		580.3	582.8	598.5	593.8
59.6	59°7	59.8	59°6	59.5	59.7	60.0	60°.8	6°.	7	eg.0	61.5	61.2	6j.3 a
		VERTICAL	Force.		In	crease, in S	Scale Division	ns, cori	respo	nding to 1°	decrease of	Temperatur	e, 1·64.
204.4	204.5	201.7	202.8	202.7	203.8	202.7	202.1	200		199.6	199°4	200.6	202.7
204.4	205.2	202.1	202.8	204.2	203.8	202.8	201.7	$\frac{200}{200}$ .		199.6	199.4	200.6	202.7
204.4 204.7	205°2 205°2	202.3	202.8	203.4	204.6 203.3	202 6	201.3	199		199.6 199.6	199 <b>.</b> 1	200.6	202°0 204°4
204.7	$205 \cdot 2$	202.3	202.5	204.1	203.2	203.4	201'1	199		199.6	199.2	201.2	204.9
204.7	205 4	202.3	202.5	204.1	203.3	202.7	201.1	199		199.6	199.8	201.4	205.1
204.7 204.9	203.4	202.0	202.5	204.1	203·3 203·3	$202.7 \\ 201.9$	201.0	199.		199 <b>.</b> 6	199 <b>·</b> 8 199 <b>·</b> 7	201 4 201 4	$205.1 \\ 204.7$
204.8	201.0	202.0	202 1	203.8	203.3	$201.9 \\ 202.7$	200.5	199		199 1	200.3	201 4	204 7 204 <b>4</b>
204.8	201.2	202.0	202.5	204'1	202.7	202.6	200.5	199	6	198.8	200.2	202.2	202.6
204.8	201.2	202.0	202.5	204.2	202.7	202.1	200.2	199		198.8	200.1	202.7	202.6
204.7	201.7	202.8	202.8	204.0	202.7	202.1	200.5	199		199.4	200.7	202.7	202.0
59.4	60°.6	60.6	60°1	59°7	59.0	59.2	<u>60.0</u>	60°.	0	60°4	60.4	60.3	60°.5 a
and increas	sing Horizo	ontal and Ver	tical Force.										
		II.			TEOROLO		BSERVATI	ONS.	1				
Mean Go		Barometer		mometers.	_		ind.				Weat	her.	
Tim	ie.	at 32°.	Dry.	Wet.	Direct	tion.	Force.				<del></del>	***************************************	
D. н. 22 22		In.	0	0		. I	W 1		~				
22 23 22 23	2 0	29.653 29.651	47.5	47.0	N. by	E.	Very ligl Calm.	nt.		oudy; rain. oudy; rain.			
23 (	0	29.639	49.5	47.7	N.N.	.E.	Very ligh	nt.		oudy; rain.			
1	0	29.650	51.3	49.8			Calm.		Clo	oudy; rain.			
2		29.646	51.2	51.1	N.E. b		Very ligh			oudy; rain.	and also	rat	
4		29.654 29.648	47.7 50.7	47.0 48.7	E.S. E.	E.	Very ligh Very ligh			zy; circun zy; circun			
5	0	29.635	52.2	49.2	E.N.		Moderate			zy ; circun zy ; circun			
6	0	29.617	54.2	50.1	N.E. b	y E.	Moderate	е.	Ha	zy; circun	a. and cirs	trat.	
7 8	0	29.605	55.0	50.8	E.N.	E.	Moderate Moderate			zy ; circun zy ; circun			
9		29 · 597 29 · 565	55°8	50.7 50.8	E.N. E.N.		Moderate			zy; circun zy; circun			
_		20 000	1 000	30 0	12,11.	<b>~</b> . }	maduci abt	•	] ~~~	_, , ocum			

May 29th and 30th	ch.		-	MAGNETI	CAL OB	SERVATIO	NS.				
Mean Göttingen	Λngula	r Value of	one Scale D	vision =0'	7.721.				DECLINAT	ion.	
Time.	10 ^h .	11 ^h .	12h.	13h.	14h.	15h.	16h.	17".	18 ^h .	19 ^h .	20 ^h .
M. S. 0	Sc. Div. 106.8	Sc. Div. 109 2	Sc. Div. 108*2	Sc. Div.	sc. Div. 109 8 109 8	sc. Div. 110°4 109°8	sc. Div. 125 6 127 8	Sc. Div. 126°0 124°5	Sc. Div. 117 0 118 2	Sc. Div. 115°2 114°8	Sc. Div 115 4 116 2
$\begin{bmatrix} 5 & 0 \\ 10 & 0 \end{bmatrix}$	107.0 107.2	109.0	108.0	109.3	109.6	110.2	128.0	123.6	119.1	114.8	115.8
15 0	107.8	109.3	106.0	108.8	109.7	110.6	126.6	123.2	119.6 119.2	114.9 115.0	115.0 114.3
20 0	108.2	109.0 109.1	106.3	$109.0 \\ 109.2$	109.8	112°2 114°4	124.8 125.0	123.4 $123.6$	119.0	114.7	114.5
$\begin{array}{ccc} 25 & 0 \\ 30 & 0 \end{array}$	109.0 109.1	108.8	107.6	109.0	110.4	118.0	127.8	123.6	119.0	114.8	114.4
35 0	109.8	108.8	108.0	109.0	110.0	122.2	129.6	121.4	117.8	115°8	115.0 112.4
40 0	110.0	108.8	108.5	$\frac{109.2}{109.0}$	109.4	128.0 125.8	127.6 124.8	121.2 120.1	117.2 117.0	115.0	112.2
45 0 50 0	110.0 110.0	$\frac{108.3}{108.2}$	109°0 109°7	109.0	109.4	$\frac{123}{124.6}$	124.2	118.8	117.0	115.1	112.0
55 0	110.0	108.6	110.0	109.2	109.7	124.0	125.0	118.0	116.5	115.0	111.1
м. s.	One Se	ale Divisior	i = .0000	87 parts of	the H. F.					FAL FORCE	
2 0	582.2	58810	576.5	575.2	578:0	578.2	580.0		569.4	570°4 571°5	$\begin{array}{c} 571.0 \\ 572.2 \end{array}$
7 0	583.8	590.0	574.0 572.5	575°0 575°4	579°2 577°3	578.4 578.0	581.6 581.0		572.2	573.2	574.0
$\begin{array}{ccc} 12 & 0 \\ 17 & 0 \end{array}$	583°8 589°5	591 °0 591 °0	572.0	575.7	578.0	$578 \cdot 2$	581.6	570.0	573.2	573.0	573.8
22 0	595.0	589.0	572.0	576.2	577.2	580.2	577.2	569.0	572.8	573.5	576°2 577°0
27 0	597:0	588.0	573.4	576.3	577.0	581.0 581.4	572.8 572.2		570.5 570.6	575°0 574°0	578.2
$\begin{array}{ccc} 32 & 0 \\ 37 & 0 \end{array}$	597.5 598.5	588 <b>°</b> 0 586 <b>°</b> 0	569°8 570°4	$577.0 \\ 577.2$	$\begin{array}{c} 578.2 \\ 578.4 \end{array}$	584.5	$\frac{572.2}{572.8}$		568.4	573.4	575.8
42 0	596.2	583.0	571.0	577.4	578.0	584.0	571.2	567.2	567.5	573.4	575.0
47 0	599.0	582.0	571.8	578.0	577.2	582.0	566.8		568.0	$572 \cdot 0$ $572 \cdot 0$	$\begin{array}{c} 574.4 \\ 573.6 \end{array}$
52 0 57 0	598.0 591.0	580°0 576°5	573°0 576°2	578°2 578°4	577°0 577°4	584.2 584.0	565.4		569°0 570°0	571.8	573.2
Thermometer	73.2	73.2	72.1	72.0	71.4	71.4	71.0	70.8	70°6	70°4	70.2
м. s.	One Sc	ale Division	= .0000	63 parts of	the V. F.				VERTICAL	Force.	
3 0	179.1	181.4	182.5	182.7	182.9	179.9	174.3	177:1	174.4	179.2	1821
8 0	179.1	183.0	183.0	182.7	182.4	179.9	174.3	176.7	174.7	177.7	182.1
13 0	179.1	183'1	182.5	182.7	182.2	179.9	174.1	174.6	175.4 175.4	178.6 177.8	182°3 182°6
$\begin{array}{ccc} 18 & 0 \\ 23 & 0 \end{array}$	181 1 181 8	183°1	182.5 182.5	182.8 182.8	181.8	179°9 179°9	173°0	174.6 174.3	174.7	177.8	182.7
$\begin{array}{ccc} 23 & 0 \\ 28 & 0 \end{array}$	181.8	183.1	182.5	182.9	180.4	179.9	171.3	172.9	175.0	179.4	182.7
33 0	182.7	183.1	182.5	182.9	180.4	179.6	171.5	172.9	175.0	179°4 179°4	182°2 181°8
38 0 43 0	182.7 182.7	183°1	182.5 182.5	182 <b>.</b> 9 182.6	179.9	179°5 175°5	171.5 172.0	172°1 174°4	173°4 173°4	179 4	181.2
48 0	182.8	183.1	182.2	182.6	179.9	175.5	174.2	174.4	173.4	181.4	181.5
53 0	182.8	183.1	182.5	182.6	179.9	175.5	174.6		175.0	181.4	181.3 181.2
58 0	181.8	183.1	182.2	182.6	179.9	175.0	177.1	174.4	177 1	182.1	·
Thermometer	71.9	7 η5	71°3	70.8	70°5	70.9	72.3	72.3	72.3	72°3	70.8
							Increasin	g Numbers de	enote decrea	sing Westerl	y Declination
l.			MI	ETEOROL	OGICAL	OBSERVAT	TONS.				
Mean Gottingen	Barometer	· Ther	mometers.		Win	nd.			Weat	her.	
Time.	at 32°.	Dry.	Wet.	Direc	ction,	Force.					
D. H. M.	In.	0	0								
29 10 0 11 0	29.275	69.2		E. b		Very ligh Very ligh	t. Cl	oudy; circui			
$\begin{array}{c c} 11 & 0 \\ 12 & 0 \end{array}$	29°263 29°255	64.8	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	E. b	y 15.	Calm.		oudy; circur oudy; circur			
13 0	29.262	64.0	60.0	_	_	Calm.	Cle	oudy; cir. cur	n., cumstra	it., and haze.	
14 0	29.252	61.7	58.2	E. b	y N.	Very ligh		oudy; circur			
$\begin{array}{ccc} 15 & 0 \\ 16 & 0 \end{array}$	29°258 29°240	61.7	57°3 57°4	_	_	Calm. Calm.	Cle	oudy; circur vercast; rain, l	n., cumstra	it., and haze. id thunder.	
17 0	29 240	62.1	57.5		_	Calm.	Ov	ercast; rain,	lightning, ar	d thunder.	
	29.227	62.6	58.2	_	_	Calm.	0.7	ercast : rain. l	lightning, ar	d thunder.	
18 0		1									
19 0	29.241	61.8	59.2	E. b		Very light	it. Or	rereast; lightn	ing and thu	nder; occasi	onal rain. onal rain.
	29°241 29°203 29°199	61.8 60.5	58.0		V.E.	Very light Very light Very ligh	it. Ov	rercast; lightn rercast; lightn rercast; rain,	ing, thunder	nder; occasi r, and occasio	mai ram.

^a At 30^d 10^h Thermometer of H. F., 73° · 5; of V. F., 72° · 0.

					MAGNET	ICAL OB	SERVATIO	ons.			May 29th	and 30th.
		DECLINAT	TION.					A	ngular <b>V</b> alu	e of one Sca	ale Division	= 0°721.
21h.	22h.	23h.	Ob.	1 ^h .	2h.	3h.	4 ^h .	5 ^h .	6h.	7 ^h .	8h.	9h.
Sc. Div. 110°2 109°6 108°8 107°8	Sc. Div. 109°2 109°1 110°2 111°7	Sc. Div. 115 '9 117 '0 118 '5	Sc. Div. 125.0 124.8 126.0 126.8	Sc. Div. 130°0 131°0 130°0 127°5	Sc. Div. 126'0 126'0 126'0 127'0	sc. Div. 120°2 119°0 118°2 117°6	sc. Div. 117 0 117 0 116 2 114 4	sc. Div. 109°2 108°4 108°3 110°0	sc. Div. 106 2 105 8 105 8	Sc. Div. 97.6 98.7 99.8 100.2	Sc. Div. 100 6 101 0 101 8 103 3	sc. Div. 104 '2 104 '1 104 '3 104 '7
107.5 106.8 106.0 107.2 106.2 106.5	112.6 113.8 115.0 114.7 114.8 115.9	120°9 121°2 121°9 122°6 121°7 122°0	127.0 127.0 126.2 126.0 126.8 127.8	127.0 127.8 128.0 128.0 128.0 127.0	127.4 128.8 129.4 129.0 129.4 125.7	118.0 117.4 117.0 117.2 117.4 116.6	114.2 114.8 114.8 115.0 117.2 113.6	111.2 111.4 111.2 110.8 109.4 107.0	104.6 102.8 98.6 98.7 97.7 97.4	100'3 100'8 100'8 100'2 100'0 100'8	103 ° 4 104 ° 0 103 ° 9 103 ° 9 104 ° 0 104 ° 4	105.0 105.3 105.4 105.8 105.8 105.0
107.0	117.0	123°0 124°0	128.7 129.7	127.0 126.0	121.3 153.0	117.0 117.4	112.0	105°4 106°0	96.5 96.8	100.3	104.0	106°2 106°4
	,	Horizont	AL FORCE.			Increase, in	Scale Divis	ions, corresp	onding to 1	° decrease o	of temperatur	re, 1.63.
572.6 573.7 571.6 571.0 567.4 566.2 568.2 567.4 566.2 565.0 565.2	567.0 566.0 565.9 568.8 572.0 569.0 570.9 572.0 571.0 571.0 574.8 574.7	573.0 573.4 578.0 578.0 578.0 579.4 578.5 578.0 578.8 579.0 578.8 578.0	578.0 579.0 576.5 579.4 580.9 581.0 580.0 578.0 577.0 574.0 572.0 569.9	567 · 2 567 · 2 568 · 0 568 · 5 571 · 0 572 · 0 569 · 0 567 · 5 568 · 0 567 · 0 567 · 0	566.0 565.0 562.5 561.0 562.2 566.0 560.6 560.4 557.2 557.6 554.0 554.0	554·2 555·0 556·6 556·4 555·8 554·2 554·0 553·2 557·3 560·0 557·2 557·4	560°2 559°0 558°2 556°Q 554°8 555°0 556°2 557°0 552°2 551°4 551°6 554°4	555·2 546·8 554·6 556·2 551·4 550·0 547·6 552·5 545·4 543·4 551·8 554·6	551·2 550·6 556·6 556·4 557·4 554·8 550·6 546·2 541·5 543·0 546·8 551·5	551·2 553·5 560·0 567·0 568·4 569·0 567·8 565·0 564·0 564·0 564·0 562·0	562·2 560·8 564·1 573·0 578·8 578·0 580·0 579·6 576·6 571·0 571·1 571·0	575.0 577.0 578.0 581.2 580.0 579.8 580.0 577.0 576.2 583.0 584.0 584.0
70°0	70°·0	69°5	69.0	69°.0	69°0	68°7	69°4	70°2	70°·8	71°7	72.4	73°0ª
		VERTICAL :	Force.		·	Increase, i	n Scale Divi	sions, corres	ponding to	l° decrease (	of temperatu	re, 1 · 64.
180.6 180.0 179.2 178.3 177.8 176.1 176.0 175.4 174.7 174.3 174.3	174'3 173'9 173'9 174'0 174'0 176'3 177'3 176'8 176'8 176'4 176'1	176°1 176°1 176°0 176°1 176°1 176°4 178°6 178°6 178°6 180°3 180°3	181.5 181.5 182.1 182.1 182.2 183.7 183.7 183.1 182.8 182.8 182.9	183.0 183.3 183.3 183.8 183.8 183.1 183.1 183.1 183.1 183.1 183.1	184.5 184.3 184.3 183.8 183.8 183.8 183.1 183.1 183.1 183.1 183.2 184.3	184'3 184'3 183'9 183'9 183'8 183'4 183'4 183'4 183'4 183'3 182'6 182'6	182.6 181.9 181.9 181.9 181.6 180.9 180.9 179.9 179.9 179.1	179°1 178°6 178°2 177°2 177°9 176°6 176°6 176°6 176°6 176°6 176°5	177.2 177.2 177.2 178.7 178.4 177.7 179.2 177.4 178.2 177.3 177.6	177.7 177.9 178.8 179.1 179.2 180.0 179.0 179.0 179.1 179.1 179.1 180.3	179 °6 179 °9 180 °4 182 °2 182 °2 182 °8 183 °0 183 °0 183 °0 183 °0 183 °0 183 °0	183.2 183.7 183.8 183.8 184.7 184.7 184.7 184.7 184.7 186.0 186.0
7.5	7ΰ5	71.2	70°0	69°0	68°5.	68.7	68.9	69°5	69°9	7°°7	7ΰ3	71°5 a
and incre	easing Horizo	ntal and Ver	tical Force.									
		1	1	ME	TEOROLO	GICAL C	BSERVAT	YONS.				
	Göttingen ime.	Barometer at 32°.	Ther	wet.	Direct	Wind.	Force.			Weather.	•	
29	H. M. 22 0 23 0 0 0 1 0 2 0 3 0 4 0 5 0 6 0 7 0 8 0 9 0	In. 29 ' 201 29 ' 192 29 ' 207 29 ' 213 29 ' 215 29 ' 225 29 ' 225 29 ' 221 29 ' 210 29 ' 201 29 ' 201 29 ' 195	60°4 60°4 60°2 58°7 61°5 63°7 70°3 71°9 72°5 73°5 72°1 73°0	59°2 59°3 58°8 57°8 60°2 62°2 68°0 69°0 69°7 69°7 68°7	N.N.	E. Ve	ery light. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm.	Cloudy; c Cloudy; c Cloudy; c Cloudy; c Cloudy; c Cloudy; c Cloudy; c Cloudy; c Cloudy; c Cloudy; c	aia, lightninircum. and ircum. and ircum. ircum. irstratircum. and ircum. and ircum. and ircum. and	l strat. l strat. cirstrat. l cirstrat.		

Vol. III.

June 24th and 25	th.		I	MAGNETI	CAL OI	BSERVATIO	NS.					
Mean Göttingen	Angu	lar Value o	f one Scale	Division =	: 0' · 721	•			-	DECLINAT	ion.	
Time.	10 ^h .	11 ^h .	12 ^h .	13 ^h .	14 ^h .	15 ^h .	16	6 ^h .	17 ^h .	18 ^h .	19 ^h .	20 ^h .
M. s. 0 0 0 5 0 10 0 0 15 0 0 20 0 25 0 30 0 35 0 40 0 45 0 55 0 0 55 0	110'4 111'2 111'2 111'0 111'4 112'0 112'6 112'8	Sc. Div. 113·2 113·6 114·7 115·0 115·2 115·4 115·4 115·0 115·2 114·8 114·8 114·6	Sc. Div. 114 '4 114 '2 114 '0 114 '2 114 '4 114 '8 115 '0 115 '4 115 '0 114 '8 115 '0 114 '2	sc. Div. 114'4 114'3 114'5 114'0 114'5 114'4 114'0 113'8 113'9 113'2 113'0 112'8	Sc. Div 112'7 113'0 113'0 114'4 114'8 114'2 113'8 113'2 113'0 113'2 113'0	113·1 113·4 113·2 113·9 113·8 113·8 113·8 112·8 112·2 112·2 112·0	sc. 112 112 112 112 112 112 112 112 112 11	2.8 2.6 2.7 2.6 2.7 2.0 2.0 2.1 2.1	Sc. Div. 112.5 112.2 112.2 112.2 112.2 112.2 112.5 111.5 111.6 111.6 111.8 111.9	Sc. Div. 111 '9 112 '0 112 '0 111 '9 112 '0 111 '9 112 '0 112 '2 112 '0 111 '8 111 '9 111 '9 112 '2	Sc. Div. 112.6 112.1 112.0 112.1 112.1 112.1 112.1 112.0 112.0 112.0 112.3 111.9 111.7	Sc. Div. 111 2 112 1 112 0 111 9 111 8 111 0 111 6 112 0 112 0 112 1 112 1
M. s.	One S	Scale Divisio	on = '000	087 parts	of the H.	F.				Horizont	AL FORCE	
2 0 7 0 12 0 17 0 22 0 27 0 32 0 37 0 42 0 47 0 52 0 57 0	583 '8 582 '4 580 '2 579 '6 578 '8 577 '0 580 '0 582 '2	584.6 585.4 585.0 584.6 584.8 585.0 582.2 576.0 574.8 573.6 573.8 570.5	571 °0 571 °2 575 °0 575 °4 575 °0 574 °8 574 °2 577 °2 577 °4 575 °8 575 °2	575.6 576.0 575.0 575.0 574.8 574.0 574.4 574.0 574.5 574.5 574.2 575.8	575.8 575.6 576.8 577.0 577.2 575.2 576.4 575.5 575.0 574.8 575.2	576.8 576.7 576.0 575.2 576.0 576.6 575.8 576.0 576.0 576.8	577 577 578 578 578 577 576 576 576 576 577	2 3.5 3.0 3.4 3.9 3.6 3.4	578.5 576.2 576.0 577.0 576.2 576.0 577.5 577.5 578.6 579.0 578.0 577.7	577.8 577.8 578.0 578.1 578.8 579.0 577.9 577.3 578.0 578.0 578.0 578.0	579.0 578.0 581.2 578.8 579.0 579.5 579.5 579.1 581.0 580.0 581.0	581.0 582.0 581.3 581.1 582.0 581.4 580.0 582.0 582.0 581.0 581.0
Thermometer	73°3	73.8	73°9	73.8	73°0	72°5	$7\mathring{2}$	1	7η9	71°4	70°6	7°0.4
M. s.  3 0 8 0 13 0 18 0 23 0 28 0 33 0 38 0 43 0 48 0 53 0 58 0	184'5 183'2 183'3 183'3 183'3 181'7 181'8 181'6 181'6 181'6	182.6   181.9   182.3   182.6   182.4   181.1   181.5   180.6	180.6 180.6 180.6 180.6 180.6 180.8 181.8 180.9 180.9 181.2 181.1 182.2 182.0	182.0 181.7 181.9 181.6 181.6 181.9 181.9 181.9 181.9 181.9 181.7 181.7	of the V.  179 1 178 4 178 7 177 7 177 7 177 7 177 6 176 3 176 3 176 3 176 3	176°3 176°3 175°9 175°9 176°2 176°2 176°5 176°2 176°5 177°0 177°0	177 177 177 177 177 177 177 177 177 177	·0 ·0 ·0 ·1 ·1 ·1 ·6 ·6 ·6 ·1	174'8 174'7 174'4 174'3 174'2 174'2 174'2 174'2 174'3 174'3 174'3	Vertical 174.5 174.5 174.8 174.8 174.8 174.8 174.8 174.8 174.8 174.9 175.1 175.7	FORCE.  176.4 176.4 176.4 177.2 178.4 178.7 178.7 178.7 178.7 178.7	178.7 178.7 178.7 178.7 178.7 178.7 178.7 178.2 178.2 177.4 177.4
Thermometer	71.3	7i°9	72°3	72°•4	72°.7	73.5	7 3	.3	72°9	73°0	72°5	7î·5
							Increas	sing N	umbers den	ote decreasi	ng Westerly	Declination,
li di				TEOROLO	OGICAL	OBSERVAT	ions.	•				
Mean Göttingen Time.	Barometer at 32°.	Thern Dry.	Wet.	Direc		ind. Force.				Weath	er.	
D. H. M.  24 10 0  11 0  12 0  13 0  14 0  15 0  16 0  17 0  18 0  19 0  20 0  21 0	In. 29.739 29.719 29.713 29.721 29.735 29.731 29.722 29.726 29.720 29.703	80°1 79°5 77°8 74°0 68°7 67°3 65°3 66°2 65°5 65°3 64°4 64°4	59.4 61.9 62.1 63.5 58.4 56.2 55.7 55.3 54.5 54.6 53.6 53.4	N.W. N.N N.N N.N 	.W. .W. .W. .W.	Moderate. Moderate. Moderate. Moderate. Light. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. C						
		<u> </u>	1	<u> </u>		¥ 760 · 5 · .						

 $^{^{}a}$  At 25d 10h, Thermometer of H. F., 76°  $^{\circ}$  5 ; of V. F., 74°  $^{\circ}$  7.

				MAC	ONETICAL	OBSERV	ATIONS.			ė	June 24th a	nd 25th.
,		DECLINA	ATION.					A	ngular Value o	f one Scale	Division =	0' 721.
21 ^h .	22 ^h .	23 ^h .	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8 ^h .	9 ^h .
Sc. Div.	Sc. Div. 101 6	Sc. Div.	Sc. Div. 121 0	Sc. Div. 121.3	Sc. Div.	Sc. Div.	Sc. Div.	Sc. D 114		Sc. Div.	Sc. Div.	Sc. Div
111.4	102.0	118.0	121.6	121.6	120.0	118.3	116.0	113.		104.0	102.2	103 2
11.3	103.0	124.8	121.4	121.0	119.8	119.7	115.2	112.		103.0	102.0	103.7
11.3	103.8	122.0	121.3	120.8	118.2	119.9	115.3	111.		101.9	102.6	103 2
11.4	104.0	121.7	121.0	120.6	118.0	119.7	115.8	110		101.2	103.0	103.7
11.9	113.0	122.2	120.4	120.6	117.6	119.6	115.2	109		102.0	103.6	104.0
11.9	115.2	122.0	120.4	120.6	116.8	119.4	115.0	109		102.0	102.2	103.8
10.3	116.3	121.7	121.2	120.8	117.8	118.2	113.8	109		102.1	105.0	104.2
09.8	117.2	121.7	122.2	121.8	118.6	117.0	112.9	108		102.4	104.3	105.2
07.9	119.0	122.0	123.0	122.0	118.8	116.2	113.4	108		102.0	104.0	105.0
06.9	119.0	121.2	123.2	122.2	119.2	116.3	114.7	108		102.6	104.2	105.1
03.0	119.7	121.0	123.0	120.2	117.8	116.0	114.4	108	0 105.3	102.2	103.0	105.2
		Horizon	TAL FOR	CE.	]	Increase, in	Scale Division	ons, cort	responding to 1°	decrease of	f Temperatur	e, 1.63.
79.0	584.0	585.6	578.6	576.0	566.6	569.0	575.0	569		583.2	580.2	579.2
79.0	586.0	584.7	579.0	577.2	565.8	570.0	574.8	572	0 578.0	579.5	581.0	576.8
78.5	589.2	584.0	579.4	576.2	568.2	567.4	573.4	572		575.4	583.2	576.2
79.0	589.4	582.6	582.0	573.6	567.0	567.2	572.8	573		575.0	588.2	574 (
78 <b>·5</b>	587.0	580.5	582.2	571.8	567.0	568.8	574.0	571		577.0	589.0	574.2
77.0	586.2	580.3	581.6	571.0	566.8	571.0	572.0	573		577.4	597.2	573.0
77.0	585.0	580.2	582.0	568.4	567.0	572.8	571.0	573		578.0	577.8	572.2
77.0	582*2	580.3	579.2	567.8	568.8	572.2	571.5	574		580.0	595.4	574.6
77.5	581.6	580.3	579.5	567.2	566.6	572.0	572.5	576		578.6	594.2	577.4
78.8	580 4	580.8	578.3	566.8	566.5	574.2	574.3	576		576.6	590.8	578.2
83.2	583 0	581.0	577.2	567.2	567.2	573.4	572.5	577		579.2	588.8	577.4
33.3	585 3	582.8	576°3	567.2	568.2	573.0	571.5	578	581.2	578.0	585.3	577 2
69.6	69·3	68.7	- 68°7	69°0	69°8	70°8	71.7	73.	2 73.8	75°0	75°7	76·4
		VERTICA	L Force.		I	ncrease, in	Scale Divisio	ons, corr	esponding to $1^\circ$	decrease of	f Temperatu	re, 1°64.
76.6	172.8	175.3	179.8	182.5	181.8	178.3	179.4	175	7   175.2	176.5	174.8	173.5
76 <b>·6</b>	172.0	175.5	180.5	182.6	181.8	180.0	179.6	175		175.7	175.2	173.5
76.6	170.9	177.3	181.2	182.6	181.8	178.8	179.2	175		174.8	175.0	173 5
76.7	170.8	177.7	181.9	183.1	181.5	181.2	178.9	175		174.8	175.6	174.0
75.5	170.7	177.7	181.9	182.8	180.7	179.1	178.9	175		175.3	176.4	174.0
76.5	170.0	177.2	181.9	181.4	180.7	179.1	178.5	174		175.3	176.9	174.0
76.3	171.2	177.4	182.3	181.2	180.6	181.7	177.7	175		175.3	176.3	174:3
76.8	171.3	177.9	181.9	181.1	181.2	179.3	177.7	175	2 176.5	175.3	175.6	174.2
76.9	171.8	178.0	182.2	181.1	180'6	179.2	178.0	174		175.0	176.1	174.7
76.9	173.5	177.7	182.2	181.1	179.8	179.2	177.6	174		173.8	176.1	174.8
75.2	174.2	178.7	182.0	182.2	181.0	179.9	176.9	175		174.2	175.4	174.8
73.8	175.4	179.7	182.3	182.6	178.3	179.7	176.3	175	2 176.5	174.4	175.0	174.8
7η1	70°7	69°9	69.6	69°2	69°5	70°3	70°9	71°	5 72°·3	73°3	73.9	74.7
d increas	sing Horizo	ntal and Ver	tical Force		<u>'</u>			<u>'                                    </u>				
				МЕ	ETEOROL(	OGICAL C	BSERVAT	ions.				
	öttingen	Barometer	Ther	mometers.	_	W	ind.			Wear	ther.	
Ti	me.	at 32°.	Dry.	Wet.	Direc	etion.	Force.					
D. H	. м.	In.		۰								
24 2		29.699	63.9	52.9	N.W.	by N.	Very lig	ht.	Clear and fine	_		
	3 0	29.725	64.4	53.4			Very lig		Clear and fine			
	0 0	29.723	66.7	55.7	_	_	Calm.		Fine; circur			
	1 0	29.730	69.0	56.9	_	_	Calm.		Fine; circu			
	2 0	29.722	72.5	60.5	N.N	.W.	Very lig	ht.	Fine ; circur			
	3 0	29.710	76.4	63.0	N.N		Moderat	te.	Fine; cir.			
	4 0	29.704	79.3	62.4	N.N	w.	Moderat		Fine; cir.			
	5 0	29.693	81.7	64.1	N.N	.w.	Moderat		Fine; cir. and			
	6 0	29.674	82.7	64.3	N.N	.W.	Moderat		Fine; cir. and			
		00.000	84.1	66.1	N.	w.	Moderat		Fine; circur			
	7 0	29.658										
	7 0 8 0	29.647	82.0	69.7	S. by	· W.	Very lig		Fine; circur	n.		
	7 0					· W.	Very lig Very lig		Fine; circur Fine; clear.	n.		

July $22\mathrm{nd}$ and $23$	Brd.		1	MAGNET	ICAL OI	BSERVATIO	NS.				
Mean Göttingen	Angu	lar Value of	one Scale I	Division =	0'.721.		· ·		DECLINAT	ion.	
Time.	10h.	11 ^h .	12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18 ^h .	19 ^h .	20 ^h .
M. S. O O O O O O O O O O O O O O O O O O	Sc. Div. 108 · 2 107 · 8 107 · 8 107 · 8 107 · 8 108 · 0 108 · 2 108 · 6 108 · 8 109 · 0 109 · 2 109 · 0	109.0 109.2 109.4 109.7 109.2 109.2	109'4 109'0 110'2 110'0 109'6 110'2	sc. Div. 110 '4 111 '0 110 '8 111 '2 111 '0 110 '8 110 '8 110 '8 111 '2 111 '0 111 '0 111 '0 111 '2 111 '4	Sc. Div. 111'4 112'0 111'8 112'0 112'4 112'6 111'4 111'8 111'6 111'0 110'8 111'4	Sc. Div. 111 '7 111 '6 111 '6 111 '5 111 '4 111 '8 112 '0 113 '2 113 '6 113 '2 112 '8 112 '4	sc. Div. 112 '4 112 '8 113 '2 113 '0 112 '5 112 '8 112 '4 112 '2 113 '0 112 '9 112 '4 112 '0	Sc. Div. 112.0 112.2 112.6 112.8 112.8 112.8 112.4 113.7 113.2 113.0 113.2	Sc. Div. 113 2 113 8 114 0 114 1 115 2 116 0 117 2 118 2 117 0 116 3 116 0 116 4	Sc. Div. 116.0 116.2 117.0 116.3 114.9 114.0 113.8 114.0 114.3 116.0 117.0 118.0	sc. Div. 118.0 117.3 116.0 115.8 115.8 115.7 116.0 115.3 115.0 114.1 114.0
м. s.	One	Scale Divisi	on = '000	0087 parts	of the II.	F.			Horizont	al Force.	
M. s.  2 0  7 0  12 0  17 0  22 0  27 0  32 0  37 0  42 0  47 0  52 0  57 0	584.8 582.0 578.8 579.2 578.6 579.3 580.6 581.2 581.4 581.6 581.0 581.0	581°2 581°4 581°2 581°0 580°6 583°2 582°6 582°7 582°7 582°2 580°6 580°6	579.8 577.7 578.3 578.0 577.4 577.0 577.4 578.0 578.0 578.2 578.2 579.4	577.8 578.4 579.2 579.4 578.8 577.2 577.2 578.8 580.0 579.8 580.0 581.4	579.6 579.8 580.8 581.4 579.8 578.8 578.0 580.2 578.5 576.6 577.5 578.8	578 '8 578 '2 578 '4 578 '6 576 '8 579 '2 579 '2 579 '8 580 '4 580 '6 580 '4 580 '2	581.8 581.4 581.6 581.8 579.8 580.0 580.0 580.4 581.0 581.2 580.4 580.2	580'9 581'0 581'4 581'6 581'6 581'6 581'6 581'6 582'0 583'2 583'6 582'0	582.0 582.0 582.2 582.0 583.9 584.1 584.0 584.0 581.4 581.0 581.0	581.0 579.2 580.7 580.0 578.6 582.0 586.0 588.7 587.0 585.0 582.8 581.5	582.0 579.8 579.8 579.4 579.9 578.6 577.8 577.8 577.5 577.5
Thermometer	75°5	75°6	75°5	75°2	74.8	74.5	73.6	73.0	73.0	73.0	72°5
M. s.  3 0 8 0 13 0 18 0 23 0 28 0 33 0 38 0 43 0 48 0 53 0 58 0	One  168.3 167.9 168.8 170.0 172.4 173.2 173.2 173.5 173.4 173.3 173.3 172.8	Scale Divisi 172.7 172.7 172.8 173.2 173.2 173.2 173.3 173.3 173.3 173.1 173.2 173.3 173.3 173.3	on = '000 172.7 172.9 173.0 173.0 173.1 173.1 173.0 172.7 172.7 172.7 172.7 172.8	0063 parts  172 *8 172 *8 172 *9 172 *9 172 *7 172 *7 173 *1 173 *3 173 *3 173 *5	of the V.  172 · 2  172 · 0  172 · 0  171 · 3  171 · 3  171 · 0  170 · 6  170 · 7  170 · 7  170 · 7  170 · 4	F.    170°4   170°4   170°4   170°4   170°5   170°5   170°5   170°3   170°1   170°2   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3	173.5 174.5 173.4 174.1 174.1 174.1 173.9 173.9 173.9 173.9 173.9	175·1 175·6 175·6 175·6 175·6 175·6 175·6 175·6 175·6 175·4 175·4	VERTICAL  175 * 4 175 * 4 175 * 4 175 * 1 175 * 1 173 * 2 173 * 2 173 * 2 173 * 2 173 * 2 173 * 2	173.0 173.1 172.7 172.7 172.7 171.8 171.8 170.2 169.5 168.0 168.0	168.5 169.1 169.1 169.1 169.1 169.4 169.4 170.5 170.6
Thermometer	74°5	74.7	74.7	74.5	³74°.7	74.1	73.7	73.0	72°9	73.0	7å·1
						]	Increasing 1	Numbers de	note decreas	ing Westerly	Declination,
	11		ME	TEOROLO		OBSERVATI	IONS.				
Mean Göttingen Time.	Barometer at 32°.	Thern Dry.	Wet.	Direc	Win	Force.			Weathe	er.	
D. H. M.  22 10 0  11 0  12 0  13 0  14 0  15 0  16 0  17 0  18 0  19 0  20 0  21 0	1n. 29 · 534 29 · 533 29 · 505 29 · 506 29 · 515 29 · 508 29 · 518 29 · 511 29 · 509 29 · 486 29 · 467 29 · 465	74·1 73·1 73·1 69·1 63·3 61·9 59·9 59·5 59·1 58·5 56·9 55·8	74'1         67'4         —         Calm.         Cloudy; cirstrat. and circum.           73'1         66'9         —         Calm.         Cloudy; cumstrat. and circum.           69'1         64'7         —         Calm.         Cloudy; cumstrat.           63'3         60'7         —         Calm.         Cloudy; cirstrat. and circum.           61'9         60'1         —         Calm.         Cloudy; cirstrat. and circum.           59'9         58'6         —         Calm.         Cloudy; cirstrat. and circum.           59'5         57'1         —         Calm.         Cloudy; cumstrat.           59'1         57'1         —         Calm.         Cloudy; cumstrat.           58'5         57'1         —         Calm.         Cloudy; circum. and cirstrat.           56'9         55'5         —         Calm.         Cloudy; cirstrat.								

^a At 23^d 10^d, Thermometer of H. F., 77° · 3; of V. F., 76° · 1.

					MAGNET	ICAL OI	BSERVATIO	NS.			July 22 _{nd}	and 23rd.
		DECLINA	TION.					Ang	gula <b>r V</b> alue	of one Scale	Division =	0'.721.
21h	22h	23 ^h	$O_{\rm p}$	1 ^h	2 ^h	3 ^h	4 ^h	5 ^h	6h	7 ^h	8 ^h	9 ^h
Sc. D'v. 115 0 115 0	Sc. Div. 107.6 104.8	Sc. Div. 115*4 115*0	Sc. Div. 120°2 119°8	Sc. Div. 124.4 124.2	Sc. Div. 123 5 124 0	Sc. Div. 116.4 114.6	Sc. Div. 114 1 112 2	Sc. Div. 106 9 107 0	Sc. Div. 107 0 106 1	Sc. Div. 105 2 104 9	Sc. Div. 104°0 104°2	Sc. Div. 105 5 105 5
116°5 117°0	101.0	114.2 114.6	119.0 121.2	124.7 125.0	$124.0 \\ 124.2$	113.8	111.5	107.4 107.6	106.6 107.0	104.4	104.0 104.5	106.0 106.2
117°0 117°2	102°0	114.0 114.7	120.8 120.7	127.4 127.0	124°4 124°6	113°2 112°0	110°3	108.0	106°2	104.0 104.0	105.0	106°3 108°2
116.8 116.2	108.0	114.7 114.0	121°2 122°0	126 2 124 2	124 ° 4 123 ° 0	112°2 112°4	108.3	107°0 106°0	106.0 102.8	104.7 104.8	105.0	109°2 109°2
116·2 117·0	114.8	114.8 112.0	122.0 121.8	124 ° 0 125 ° 0	122.4 121.2	111.8 112.2	108.0	105.6 106.2	106 <b>.0</b>	104.8	105°8	111.0
115.2	116.3	117.8	122.2 124.0	124.4	119.0 117.8	113.0 113.0	107.9	107.0	105.4 105.4	104.3	106.0	109.3
		Horizon	tal Forc	Е.	I	ncrease, it	n Scale Divisio	ons, correspo	onding to 1°	decrease of	Temperatui	е, 1 63.
578°0 577°5	559 <b>.</b> 7 561.0	577.0 577.0	585.4 584.8	587°2 588°2	580°4 577°0	559°5 560°0	564°5 566°8	565°5 565°0	574°0 573°0	572.0 571.0	571°5 572°0	572.0 573.2
576°9 577°5	565.4 566.2	578.6 579.0	584.2 586.0	590°2 588°8	576 4 574 2	560°0 557°6	564°3 564°0	564.7 565.0	574.0 571.5	571.0	571.0 573.7	575°0 577°5
577°0 576°1	570°0 571°4	579°4 579°2	586.6 587.0	587.8 587.2	573°4 573°4	561.8 559.0	564°0 565°0	565°0 567°2	571 · 9 573 · 0	572.0 572.6	579°0 579°3	584.5 584.0
575°5 573°5	573°0 573°2	579°0 579°2	587.2 587.3	586.0 584.2	573°4 572°0	560°2 561°8	564.0 564.8	569.8 570.0	571.5 571.0	572°2 571°3	578°0 574°5	597.0 594.0
573.0 570.5	573.6 574.5	579°4 580°8	587.6 587.4	584.0 585.4	571°2 570°8	562.8 562.0	563·1 563·0	568.8 571.0	571.0	573°2 572°0	576.5	588.0 587.5
569.0	575°0 575°4	581°3 581°4	586.8 588.4	586.8 585.4	567°2 566°2	461.6 561.8	564.5 566.0	571.4 573.0	572°0 571°2	572.5 571.5	576°5 574°6	581°5 578°0
72°·3	72.0	7η5	7 Î · 5	72°2	7å·0	73.8	74.6	75.0	75°5	76°0	76°5	77°0 a
		VERTICA	L FORCE.		I	ncrease, in	Scale Division	ons, correspo	onding to 1°	decrease of	Temperatu	re, 1.64.
170°6 170°6	162.4 163.6	166.3	170°2 170°3	172.9 173.2	173°0 173°3	171.0 170.7	169°7 169°7	169°8 168°9	168.9 168.9	167.9 167.9	169°9 170°3	173°1 173°1
170°0 170°0	164.9 163.6	166·3	170°3 172°0	173°2 173°2	172 <b>·</b> 9 173 <b>·</b> 2	170°7 170°2	169.5 169.7	168.3	168.9 168.9	167°9 168°7	170.9	173°3 173°9
169.6 169.6	162 <b>.</b> 9 161.8	166.4 166.5	171.5 172.5	174°3 174°3	173°2 173°3	171.0 169.6	169·7 169·7	168°3	168.9	168.7 168.7	172°2 172°2	174.9 174.5
169.6 168.9	161.8 162.2	166°4 166°5	172.4 172.4	174°5 174°5	173°3 173°3	168.6 168.4	169·7 170·1	169.8 169.8	168.9 168.9	169.6	172.8 172.8	176°3 175°0
168.0	162.0	166.2	172.3	173.6	173.3	168.4	170.1	169.3	168.2	169.6	172.8	174.2
166.2 166.2	163°2 163°3	166.4 166.3	$171.9 \\ 172.7$	173.6 173.6	173°3 173°4	168.4 168.3	169.8	169°3	$168.2 \\ 168.2$	169.9	173.1	174°2 174°2
164.2	163.5	167.2	172.9	173.8	172.8	168.9	169.8	169.3	167.9	169.9	173.1	173.1
72.7	72.5	71.5	72°1	72°1	72°5	73.2	73.7	74.0	74.3	74.5	75°4	75.8 a
and increa	sing Horizo	ntal and Ver	tical Force.									
		1	Thom	·	TEOROL		OBSERVATI	ions.			and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
	öttingen me.	Barometer at 32°.	Dry.	Wet.	Direc	Win etion.	Force.			Weathe	er.	
1	н. м.	In.	0	0			<b>C</b> .					
23	3 0 0 0 1 0 2 0	29 * 445 29 * 465 29 * 492 29 * 501 29 * 492	56.7 57.9 61.5 66.7 70.8	55.9 56.9 59.7 63.7 64.5		-	Calm. Calm. Calm. Calm. Calm.	Cloudy; Cloudy; Cloudy; Cloudy;	; fine. ; fine.	nd strat.		
	3 0 4 0 5 0 6 0 7 0	29 '471 29 '460 29 '456 29 '438 29 '431	74.6 79.1 76.7 78.8 79.9	65°2 69°3 69°4 70°4 70°7		- - - -	Calm. Calm. Calm. Calm. Calm.	Fine; c	ircum. and circum. and ircum. and fine, with fine.	l strat l cirstr <b>at.</b>		
1	8 0 9 0	29·425 29·406	80°9 79°5	68.5 67.8		-	Calm. Calm.	Cloudy	; circum. 2	and strat. and cirstrat	•	٠

August 28th and	29th.			MAGNET	ICAL OB	SERVATIO	NS.				
Mean Göttingen	Angula	ır Value of	one Scale D	oivision = C	721.				DECLINAT	ION.	
Time.	10 ^h .	11 ^h .	12 ^h .	13 ^h .	14 ^h .	15.	16 ^h .	17 ^h .	18 ^h .	19 ^h .	20 ^h .
M. S. O O	Sc. Div. 119 0	Sc. Div. 118'3	Sc. Div. 105 2	Sc. Div. 107 ° 0	Sc. Div. 109'9	Sc. Div. 120°0	Sc. Div	112.5	Sc. Div.	sc. Div.	Sc. Div. 106 6
5 0	119.6	119.1	106.0	107.5	111.0	124.5	128.0		110.3	108.0	107.0
10 0	128.2	114.0	106.7	107.4	113.2	126.7	120.9		109.5	108.7	106.2
15 0	132.8	110.5	106.9	107.0	114.2	133.8	119.0		109.7	109.0	107°0 106°4
20 0	128.1	113.2	107.0	107.2	123.8	138.0	119.7		108.3	109.6	108.2
25 0	127.2	108.0	107.3	106.7	129.0	142.0	115.3			111.5	108.0
30 0	123.0	106.5	107.2	107.8	131.5	148.4	116.0		109.3	109.2	106.5
35 0	119.0	104.8	106.0	107.3	144.0	147.9	119.6		104.6	114.0	108.2
40 0	119.9	104.2	106.0	107.0	137.8	139.7	1		104.1	113.8	108.2
45 0	117.2	103.0	106.2	107.2	131.0	142.8	116.0	1	105.0	113.2	108.7
50 0	116.6 113.1	103.6	106.5	106.5	126.8	147.0	112.3		107.5	112.6	108.3
55 0	110 0	104.2	107.0	108.5	125.4	141 0	112 0	111 4	10, 0	112 0	100 0
M. S.	One S	cale Division	m = '0000	87.	<del></del>				Horizont	AL FORCE	
0 0	614.8	577.8	560.4	574.0	578.0	587.5	561.0	564.0	571.0	575.0	567:4
5 0	612.2	575.3	554.0	574.0	578.0	580.2	547.0		574.0	572.2	567.2
10 0	621.4	572.0	561.0	574.0	570.0	580.9	540.0		576.7	564.0	566.8
15 0	621.2	570.6	561.4	575.9	568.0	586.6	538.5		577 <b>.</b> 5	562.2	572 2
20 0	614.2	566'2	$566^{\circ}2$	576.0	570.8	586.2	547.0		573.5	561.4	575 (
25 0	603.8	571.0	576.7	575.8	578.0	589.0	541.0		572.5	561.2	575 4
30 0	598.2	562.2	573.0	574.5	586.5	586.5	543.5		576.5	566.6	576.2
35 O	595.2	566.0	569.5	574.0	588.4	585.8	552.5		576.5	567.0	574.4
40 0	593.8	561.4	570.0	571.5	591.6	577.0	559.0		571.0	567.4	575
45  0	591.0	563.4	<b>5</b> 69.0	571.0	589.9	569.4	564.0		571.5	567.2	573.6
50 O	582.3	564.0	566.0	572.0	590.0	569.0	564.0		571.5	567.6	577.0
55 0	582.4	561.5	570.0	577.5	594.2	573.0	564.0	569.0	573.5	568.4	576°2
Thermometer	76°0	75°8	75°·8	75°6	75.6	75.4	75°0	74.5	74.1	74.0	73°7
	One S	cale Divisio	n= .0000	63.					VERTICAL	Force.	
M. S.	189.3	188.8	176.2	1 1 1 1 1	170.0	155.7	155.6	167.9	169.7	162.5	162.6
$\begin{array}{ccc} 0 & 0 \\ 5 & 0 \end{array}$	188.6	187.0	174.5	171°1 171°1	170.0	155.7	153.3		168.4	158.5	162.0
10 0	189.0	185.7	174.4	171.1	169.6	155.6	153.3		167.2	160.2	162.5
15 0	184.6	185.3	174.3	171.6	169.6	149.5	156.4		165.3	158 1	164'2
20 0	182.9	183.1	175.4	171.6	164.8	147.6	158.0		164.0	157.9	164'
$\begin{array}{ccc} 20 & 0 \\ 25 & 0 \end{array}$	182.9	182.2	175.1	171.6	160.5	147.2	158.0		164.4	158.6	163 4
30 O	184.0	179.5	173.8	171.2	162.2	148.7	162.2		165.1	157.0	165
35 0	184.7	179.3	173.4	171.5	159.1	148.7	165.8		164.1	158.1	166''
40 0	185.4	178.4	172.9	171.5	153.1	148.0	165.8		163.3	157.8	166
45 0	186.9	177.8	171.9	171.5	151.4	148.0	166.5	168.9	162.2	159.5	166'2
50 O	187.7	178.0	171.0	171.5	151.4	149.3	166.5		162.2	1.9.7	166
<i>5</i> 5 0	189.1	176.9	171.1	171.5	154.6	149.7	166.2		162.2	162.2	167
Thermometer	74°5	74.5	74°7	74°8	76°1	76°0	75°5	75°2	75.0	74.9	74''
							Increasi	ng Numbers de	enote decrea	sing westerl	Declination
			MI	ETEOROL	OGICAL	OBSERVAT	TONS.				
	1										
Mean Göttingen	Barometer	Ther	mometers.		W	Vind.			Wea	ther.	
Mean Göttingen Time.	Barometer at 32°.	Ther	mometers.	Direc	etion.	Force.			Wea	ther.	
D. H. M.		.			etion.				Wea	ther.	
D. H. M. 28 10 0	at 32°.	Dry. 0 74.6	Wet	E.S	etion.	Force.	ght.	Cloudy; cum.	-strat. and c	eircum.	
D. H. M. 28 10 0 - 28 11 0	In. 29.709 29.705	Dry.	Wet. 70.1 69.7	E.S N.1	etion.	Force.  Very lig	ght.	Cloudy; cum.	-strat. and c	eircum.	
D. H. M. 28 10 0 - 28 11 0 28 12 0	In. 29.709 29.705 29.713	Dry.	Wet. 70°1 69°7 68°3	E.S N.1	etion.	Force.  Very lig Very lig Calm	ght. ght.	Cloudy; cum. Cloudy; cum.	-strat. and c	eircum. eircum. eircum.	
D. H. M. 28 10 0 28 11 0 28 12 0 28 13 0	In. 29.709 29.705 29.713 29.709	Dry.	Wet. 70°1 69°7 68°3 67°3	E.S N.1	etion.	Very lig Very lig Calm Calm	ght.	Cloudy; cum. Cloudy; cum. Clear, with str	-strat, and c -strat, and c -strat, and c rat, and cir	eircum. eircum. eircum.	
D. H. M. 28 10 0 28 11 0 28 12 0 28 13 0 28 14 0	In. 29.709 29.705 29.713 29.709 29.703	Dry.	Wet. 70°1 69°7 68°3 67°3 66°3	E.S N.1	etion.	Very lig Very lig Calm Calm	ght.	Cloudy; cum. Cloudy; cum. Clear, with str Clear; circu	-strat. and c -strat. and c -strat. and c rat. and cir m.	eircum. eircum. eircum.	
Time.  D. H. M.  28 10 0  28 11 0  28 12 0  28 13 0  28 14 0  28 15 0	In. 29 '709 29 '705 29 '713 29 '709 29 '703 29 '703	Dry.  74.6 72.1 71.7 69.3 67.9 65.9	Wet. 70°1 69°7 68°3 67°3 66°3 64°7	E.S N.1	etion.	Very lig Very lig Calm Calm Calm	ght.	Cloudy; cum. Cloudy; cum. Clear, with str Clear; circu Clear; circu	-strat. and c -strat. and c -strat. and c rat. and cir m.	circum. circum. circum. cum.	wia:bla
Time.  D. H. M.  28 10 0  28 11 0  28 12 0  28 13 0  28 14 0  28 15 0  28 16 0	In. 29 '709 29 '705 29 '709 29 '709 29 '709 29 '703 29 '703 29 '697	74.6 72.1 71.7 69.3 67.9 65.9 65.6	Wet. 70°1 69°7 68°3 67°3 66°3 64°7 64°1	E.S. N.2	etion.	Very lig Very lig Calm Calm Calm Calm Calm	ght.	Cloudy; cum. Clear, with str Clear; circu Clear; circu Clear; circu	-strat. and c -strat. and c -strat. and c rat. and cir m. m. and cirs	circum. circum. ircum. -cum.	ı visible.
Time.  D. H. M.  28 10 0  28 11 0  28 12 0  28 13 0  28 14 0  28 15 0  28 16 0  28 17 0	In. 29 '709 29 '705 29 '709 29 '703 29 '703 29 '697 29 '694	Dry.  74.6 72.1 71.7 69.3 67.9 65.6 65.5	Wet.  70°1 69°7 68°3 67°3 66°3 64°7 64°1 64°2	E.S N.2	etion.	Very lig Very lig Calm Calm Calm Calm Calm	ght. ght.	Cloudy; cum. Cloudy; cum. Clear, with str Clear; circu Clear; circu Clear; circu Cloudy; sheet	-strat. and c -strat. and c -strat. and c rat. and cir m. m. and cirs	circum. circum. ircum. -cum.	ı visible.
Time.  D. H. M.  28 10 0 -  28 11 0 28 12 0  28 13 0 28 14 0  28 15 0 28 16 0  28 17 0 28 18 0	at 32°.  In. 29 '709 29 '705 29 '713 29 '709 29 '703 29 '697 29 '694 29 '686	Dry.  74.6 72.1 71.7 69.3 67.9 65.9 65.6 65.5 63.9	Wet.  70°1 69°7 68°3 67°3 66°3 64°7 64°1 64°2 62°9	E.S N.2	etion.	Very lig Very lig Calm Calm Calm Calm Calm Calm	ght. ght.	Cloudy; cum. Cloudy; cum. Clear, with str Clear; circu Clear; circu Cloudy; sheet Cloudy; fine.	-strat. and co-strat. and cirstrat. and cirm. m. and cirstrat. and cirstrat.	circum. circum. ircum. -cum.	ı visible.
Time.  D. H. M.  28 10 0 -  28 11 0 28 12 0  28 13 0 28 14 0  28 15 0 28 16 0  28 17 0 28 18 0  28 19 0	at 32°.  In. 29 '709 29 '705 29 '713 29 '709 29 '703 29 '697 29 '694 29 '686 29 '694	Dry.  74.6 72.1 71.7 69.3 67.9 65.6 65.5 63.9 62.9	Wet.  70°1 69°7 68°3 67°3 66°3 64°7 64°1 64°2 62°9 62°0	E.S N.2	etion.	Very lig Very lig Calm Calm Calm Calm Calm Calm Calm Calm	ght. ght.	Cloudy; cum. Cloudy; cum. Clear, with str Clear; circu Clear; circu Cloudy; sheet Cloudy; fine. Cloudy; fine;	-strat. and co-strat. It is a co-strat. It is a co-strat. It is a co-strat.	circum. circum. ircum. -cum.	ı visible.
Time.  D. H. M.  28 10 0 -  28 11 0 28 12 0  28 13 0 28 14 0  28 15 0 28 16 0  28 17 0 28 18 0	at 32°.  In. 29 '709 29 '705 29 '713 29 '709 29 '703 29 '697 29 '694 29 '686	Dry.  74.6 72.1 71.7 69.3 67.9 65.6 65.5 63.9 62.9 61.7	Wet.  70'1 69'7 68'3 67'3 66'3 64'7 64'1 64'2 62'9 62'0 60'9	E.S N.2	etion.	Very lig Very lig Calm Calm Calm Calm Calm Calm	yht.	Cloudy; cum. Cloudy; cum. Clear, with str Clear; circu Clear; circu Cloudy; sheet Cloudy; fine.	-strat. and co-strat. and co-strat. and corat.	circum. circum. ircum. -cum.	ı visible.

^a At 29^d 10^h, Thermometer of H. F., 75° · 3; of V. F., 74° · 4.

					MAGNE	TICAL O	BSERVATIO	ONS.				August 28th	and 29th.
		DECLI	NATION.						Ang	gula <b>r V</b> alue	of one Scale	Division =	= 0''721.
21h.	22h.	23h.	Oh.	1 ^h .	2h.	3h.	4 ^h .		5 ^h .	6h.	7 ^h .	8h.	9 ^h .
Sc. Div. 110 '2 110 '2 111 '2 111 '2 110 '0 108 '8 109 '2 109 '4 108 '0 106 '2 103 '8	Sc. Div. 104 '2 103 '0 101 '2 101 '2 101 '4 102 '8 103 '2 104 '0 105 '0 107 '8	Sc. Div. 110 '0 111 '2 112 '0 113 '0 114 '4 113 '2 114 '4 115 '4 115 '4	Sc. Div. 117 *2 118 *8 120 *0 120 *6 121 *0 122 *0 122 *6 121 *5 122 *8	Sc. Div. 124 '2 124 '3 123 '2 124 '8 122 '0 122 '0 120 '2 122 '4 122 '0 122 '0	Sc. Div. 121 '4 121 '8 121 '0 118 '4 117 '0 117 '8 118 '0 118 '7 119 '0 118 '8	Sc. Div. 116 0 116 4 112 0 113 0 113 2 112 0 113 1 113 8 115 2 115 8	116.0 119.0	Sc.   116   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117   117	3.0 1.8 1.5 1.8 1.8 2.0	Sc. Div. 113 '3 113 '0 112 '3 110 '0 107 '5 108 '6 106 '2 107 '8 109 '2 108 '6	sc. Div. 107 ° 0 107 ° 2 106 ° 6 105 ° 2 104 ° 2 104 ° 0 103 ° 2 103 ° 0 103 ° 2 102 ° 4	sc. Div. 102 '8 103 '2 102 '8 103 '0 102 '6 101 '8 102 '8 103 '0 103 '8 103 '8	sc. Div. 104 '0 103 '5 104 '2 103 '4 104 '5 105 '2 105 '8 106 '6 106 '6
103.0	108.0	113.4	124.0 123.2	122.6 121.9	117·7 116·1	114.8	116°0 114°6	110		108.8	103.0	104.0	106.8
	<u>'</u>	Horizonta	L Force.	·		Increase, i	n Scale Divisi	ons, c	orresp	onding to 1°	decrease of	Temperatur	re, 1.63.
579.6 578.0 579.2 577.0 574.8 575.2 576.0 570.2 567.4 567.3 570.2 567.2	567.4 566.7 563.6 564.2 565.4 568.0 571.2 569.4 568.8 570.0 570.8 565.8	567.8 568.2 568.4 571.2 572.8 571.6 570.4 570.8 571.0 573.4 575.0 574.4	576·2 577·4 579·2 579·2 581·4 581·4 581·4 580·6 576·8 575·6 575·2 577·6	573°2   572°3   571°4   575°6   578°6   576°6   576°6   577°3   571°0   568°2   563°8	561.0 561.6 566.1 567.8 566.2 565.0 558.4 555.6 557.0 557.2 559.0 554.5	554.5 556.5 560.0 562.2 564.8 563.5 565.5 566.7 566.0 567.5 565.5 566.9	568.5 568.2 568.2 571.0 571.1 572.4 571.3 573.0 571.1 577.5 572.5 573.5	574 578 578 571 570 574 570 568 567 567 567	5.0 5.8 6.0 6.0 7.0 7.0 7.0 7.5 7.5	570°0 568°0 566°5 567°5 568°0 566°4 560°8 563°2 565°3 564°2 563°6 562°4	568·2 568·6 568·4 566·0 560·2 554·4 556·6 562·4 562·0 570·0 566·2 569·5	578°1 573°4 571°2 569°0 570°5 568°6 571°0 572°6 571°4 569°6 571°8 580°6	589.6 590.2 590.0 591.2 589.2 590.5 588.8 581.4 581.5 584.2 581.9
73.2	73.0	72.6	7 <u>°</u> 1°9	72°0	72°5	73.2	74.0	75	g.0	76.2	76°2	75.7	75.8ª
	-	Vertical 1	Force.		1	Increase, ir	n Scale Divisio	ons, co	rresp	onding to 1°	decrease of	'Temperatu	re, 1°64.
168.6 168.8 168.6 169.2 169.4 169.3 168.8 167.8 168.4 170.1 169.1 168.1	167.7 166.3 165.3 165.4 165.4 166.1 167.9 167.9 167.8 167.8	166.8 166.7 168.3 168.3 170.0 170.0 170.3 170.5 172.8 173.9 173.6 173.6	175.0 175.0 175.4 175.9 175.9 175.9 175.9 175.6 175.6 175.6 175.6 175.6	171.7 172.0 173.0 173.0 172.4 171.5 171.5 170.9 170.8 170.4 170.1	170°5 170°4 171°3 171°5 170°9 169°5 169°4 169°3 168°7 170°5 170°5	169 · 2 169 · 7 169 · 7 170 · 4 170 · 4 169 · 7 169 · 4 169 · 2 168 · 4 168 · 4 168 · 1	169°0 169°0 167°0 167°8 167°5 165°5 167°1 166°5 165°4 167°2 164°8 164°8	167 167 166 165 165 167 167 167 167	· 0 · 5 · 1 · 4 · 4 · 4 · 2 · 2 · 1 · 6	168.6 168.6 169.1 168.7 168.7 168.3 168.7 168.3 169.7 169.3 169.6 170.2	170.9 170.9 171.2 171.4 168.4 168.5 170.0 167.4 167.3 169.1 170.2 169.5	170.6 170.2 169.7 169.7 169.7 169.6 169.8 168.8 169.8 170.0 170.6	172°2 172°2 172°2 172°5 172°8 172°9 173°1 173°1 173°1 173°5 173°5
73.9	7å·8	73.1	7°1.7	71.9	72°3	72°7	73.5	$7\overset{\circ}{4}$	•4	75.1	75°2	74.8	74·7 a
and increas	sing Horizo	ntal and Vert	ical Force										
		1			reorolo		OBSERVAT	IONS					
<b>M</b> ean G Tin		Barometer at 32°.	Thern Dry.	Wet.	Direc	wi	rd. Force.				Weath	er.	
	2 0 3 0 0 0 1 0 2 0 3 0 4 0 5 0 6 0 7 0	In. ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °		59.9 59.3 61.0 64.9 69.1 70.9 71.0 72.3 72.3 71.4 74.5 75.2	E. by E. S. S. S. N. N. N. N. N. N. N. N. N. N. N. N. N.	y S. y S. .E. E.	Calm. Calm. Calm. Calm. Calm. Very light Very light Very light Very light Moderate.		Clear Cloud Cloud Cloud Cloud Cloud Cloud Cloud Overc	• .	rcumstrat., and h -strat., and h t. and haze and haze and haze and rain and rain.		

15 0 20 0 25 0 30 0 35 0 40 0 45 0 50 0 55 0 M. s. 0 0 5 0 10 0 15 0 20 0 25 0 30 0 40 0 45 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 60 0 6	10h.  sc. Div. 103 * 5 103 * 0 104 * 0 104 * 2 104 * 8 104 * 8 105 * 0 105 * 0 105 * 0 105 * 0	sc. Div. 104 '6 104 '0 103 '0 102 '0 101 '6 102 '0 102 '0 102 '0 104 '1 102 '8  Scale Divisi 612 '4 612 '4 611 '4 615 '4 612 '2	12 ^h .  Sc. Div. 99°3 101°0 106°8 116°0 120°0 119°2 116°0 112°1 108°2 105°0 104°8 106°8  Son = '000 587°6 580°4 577°4	13h.  Sc. Div. 107 ° 0 107 ° 0 106 ° 6 106 ° 4 105 ° 7 106 ° 0 106 ° 2 105 ° 8 108 ° 0 108 ° 2 109 ° 0 109 ° 2	Sc. Div. 198° 5 108° 6 108° 2 108° 4 109° 0 109° 2 108° 0 107° 0 106° 2 106° 3 106° 2 106° 5	1	16h.   Sc. Div.   118 '8   118 '3   124 '0   129 '8   126 '2   118 '6   111 '6   109 '4   107 '5   109 '8   113 '0   111 '9	17h.    Sc. Div.     112.7     111.0     108.8     109.0     109.2     109.2     109.3     109.8     110.4     109.8     109.8	DECLINAT    18h.     sc. Div.     109 0     108 2     107 7     108 5     106 4     105 3     107 0     108 2     108 8     110 0     110 2     111 8     HORIZONT	19h.  19h.  112'0 112'2 113'3 114'1 113'3 114'0 115'0 114'8 114'2 115'0 115'3 115'4	20h.  Sc. Div. 117 1 116 2 115 6 116 8 116 8 115 2 118 2 118 2 118 9 118 6 117 8 117 6		
M. S. 0 0 0 15 0 20 0 25 0 30 0 45 0 0 15 0 20 0 25 0 0 35 0 40 0 45 0 25 0 0 35 0 40 0 45 0 45 0 45 0 45 0 45 0	Sc. Div. 103 '5 103 '0 103 '8 104 '0 104 '2 104 '8 104 '8 105 '0 105 '0 105 '0 105 '0	Sc. Div. 104 '6 104 '0 104 '0 103 '0 102 '0 101 '6 102 '0 102 '0 102 '0 104 '1 102 '8  Scale Divisi 612 '4 612 '4 611 '4 615 '4 612 '2	Sc. Div. 99°3 101°0 106°8 116°0 120°0 119°2 116°0 112°1 108°2 105°0 104°8 106°8	Sc. Div. 107 ° 0 107 ° 0 106 ° 6 106 ° 4 105 ° 7 106 ° 0 106 ° 2 105 ° 8 108 ° 0 108 ° 2 109 ° 0 109 ° 2 2087 parts	Se. Div. 108 5 108 6 108 2 108 4 109 0 109 2 108 0 107 0 106 2 106 3 106 2 106 5	Sc. Div. 107 *8 107 *7 107 *2 106 *8 106 *2 107 *2 109 *2 110 *0 110 *0 117 *0 118 *8 118 *2	Sc. Div. 118 '8 118 '3 124 '0 129 '8 126 '2 118 '6 111 '6 109 '4 107 '5 109 '8 113 '0	Sc. Div.   112.7   111.0   108.8   108.8   109.0   109.2   109.2   109.3   109.8   110.4   109.8	Sc. Div. 109°0 108°2 107°7 108°5 106°4 105°3 107°0 108°2 108°8 110°0 110°2 111°8	Sc. Div. 112.0 112.2 113.3 114.1 113.3 114.0 115.0 114.8 114.2 115.0 115.3 115.4	Sc. Div. 117 1 116 2 115 6 116 8 116 8 115 2 118 2 118 9 118 2 118 6 117 8 117 6		
0 0 0 5 0 10 0 0 15 0 20 0 25 0 0 35 0 0 0 0 25 0 0 25 0 0 25 0 0 35 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	103 · 5 103 · 0 103 · 8 104 · 0 104 · 2 104 · 8 104 · 8 105 · 0 105 · 0 105 · 0 105 · 0 One	104.6 104.0 104.0 103.0 102.0 101.6 102.0 102.0 102.0 104.1 102.8 Scale Divisi 612.4 612.4 611.4 615.4 612.2	99°3 101°0 106°8 116°0 120°0 119°2 116°0 112°1 108°2 105°0 104°8 106°8	107.0 107.0 106.6 106.4 105.7 106.0 106.2 105.8 108.0 108.2 109.0 109.2	108 5 108 6 108 2 108 4 109 0 109 2 108 0 107 0 106 2 106 3 106 2 106 5	107°8 107°7 107°2 106°8 106°2 107°2 110°0 110°0 117°0 118°8 118°2	118.8 118.3 124.0 129.8 126.2 118.6 111.6 109.4 107.5 109.8 113.0	112.7 111.0 108.8 108.8 109.0 109.2 109.2 109.3 109.8 110.4 109.8	109.0 108.2 107.7 108.5 106.4 105.3 107.0 108.2 108.8 110.0 110.2 111.8	112.0 112.2 113.3 114.1 113.3 114.0 115.0 114.8 114.2 115.0 115.3 115.4	117 1 116 2 115 6 116 8 116 8 115 2 118 2 118 9 118 2 118 6 117 8 117 6		
5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0 50 0 55 0 M. s. 0 0 5 0 10 0 15 0 20 0 25 0 30 0 40 0 45 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50 0 50	103 ° 0 103 ° 8 104 ° 0 104 ° 2 104 ° 8 104 ° 8 105 ° 0 105 ° 0 105 ° 0 105 ° 0 Tope 105 ° 0	104 ° 0 104 ° 0 103 ° 0 102 ° 0 101 ° 6 102 ° 0 102 ° 0 104 ° 1 102 ° 8 Scale Divisi 612 ° 4 612 ° 4 611 ° 4 615 ° 4 612 ° 2	101'0 106'8 116'0 120'0 119'2 116'0 112'1 108'2 105'0 104'8 106'8	107.0 106.6 106.4 105.7 106.0 106.2 105.8 108.0 108.2 109.0 109.2	108 6 108 2 108 4 109 0 109 2 108 0 107 0 106 2 106 3 106 2 106 5	107.7 107.2 106.8 106.2 107.2 109.2 110.0 110.0 117.0 118.8 118.2	118.3 124.0 129.8 126.2 118.6 111.6 109.4 107.5 109.8 113.0	111.0 108.8 108.8 109.0 109.2 109.2 109.3 109.8 110.4 109.8	108.2 107.7 108.5 106.4 105.3 107.0 108.2 108.8 110.0 110.2 111.8	112.2 113.3 114.1 113.3 114.0 115.0 114.8 114.2 115.0 115.3 115.4	116°2 115°6 116°8 116°8 115°2 118°2 118°9 118°2 118°6 117°8		
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20 0 25 0 30 0 35 0 40 0 45 0 50 0 55 0   M. s. 0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0	104 · 2 104 · 8 104 · 8 105 · 0 105 · 0 105 · 0 105 · 0 105 · 0	102 ° 0 101 ° 6 102 ° 0 102 ° 0 102 ° 0 104 ° 0 104 ° 1 102 ° 8 Scale Divisi 612 ° 4 611 ° 4 615 ° 4 612 ° 2	$   \begin{array}{c}     120.0 \\     119.2 \\     116.0 \\     112.1 \\     108.2 \\     105.0 \\     104.8 \\     106.8 \\     \hline                               $	105.7 106.0 106.2 105.8 108.0 108.2 109.0 109.2 590.0	109 ° 0 109 ° 2 108 ° 0 107 ° 0 106 ° 2 106 ° 3 106 ° 2 106 ° 5	106.2 107.2 109.2 110.0 110.0 117.0 118.8 118.2	126.2 118.6 111.6 109.4 107.5 109.8 113.0	109.0 109.2 109.3 109.8 110.4 109.8	106.4 105.3 107.0 108.2 108.8 110.0 110.2 111.8	113°3 114°0 115°0 114°8 114°2 115°0 115°3 115°4	116.8 115.2 118.2 118.9 118.2 118.6 117.8 117.6		
25 0 30 0 35 0 40 0 45 0 50 0 55 0 M. s. 0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 40 0	104 *8 104 *8 105 *0 105 *0 105 *0 105 *0 105 *0 0ne	101.6 102.0 102.0 102.0 104.0 104.1 102.8 Scale Divisi 612.4 611.4 615.4 612.2	$   \begin{array}{c}     119^{\circ}2 \\     116^{\circ}0 \\     112^{\circ}1 \\     108^{\circ}2 \\     105^{\circ}0 \\     104^{\circ}8 \\     \hline     106^{\circ}8 \\     \hline     6587^{\circ}6 \\     580^{\circ}4 \\     577^{\circ}4   \end{array} $	106.0 106.2 105.8 108.0 108.2 109.0 109.2 590.0	109 '2 108 '0 107 '0 106 '2 106 '3 106 '2 106 '5	107.2 109.2 110.0 110.0 117.0 118.8 118.2	118.6 111.6 109.4 107.5 109.8 113.0	109.2 109.2 109.3 109.8 110.4 109.8	105.3 107.0 108.2 108.8 110.0 110.2 111.8	114.0 115.0 114.8 114.2 115.0 115.3 115.4	115°2 118°2 118°9 118°2 118°6 117°8 117°6		
30 0 35 0 40 0 45 0 50 0 55 0   M. s. 0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0	104 '8 105 '0 105 '0 105 '0 105 '0 105 '0 0ne	102.0 102.0 102.0 104.0 104.1 102.8 Scale Divisi 612.4 612.4 611.4 615.4 612.2	$   \begin{array}{c}     116.0 \\     112.1 \\     108.2 \\     105.0 \\     104.8 \\     106.8 \\     \hline                               $	106°2 105°8 108°0 108°2 109°0 109°2 20087 parts	108.0 107.0 106.2 106.3 106.2 106.5	109°2 110°0 110°0 117°0 118°8 118°2	111.6 109.4 107.5 109.8 113.0	109:2 109:3 109:8 110:4 109:8	107.0 108.2 108.8 110.0 110.2 111.8	115.0 114.8 114.2 115.0 115.3 115.4	118 · 2 118 · 9 118 · 2 118 · 6 117 · 8 117 · 6		
35 0 40 0 45 0 50 0 55 0 M. s. 0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0	105 ° 0 105 ° 0 105 ° 0 105 ° 0 105 ° 0 00e	102.0 102.0 104.0 104.1 102.8 Scale Divisi 612.4 612.4 611.4 615.4 612.2	$   \begin{array}{c}     112 \cdot 1 \\     108 \cdot 2 \\     105 \cdot 0 \\     104 \cdot 8 \\     106 \cdot 8 \\     \hline                              $	105 '8 108 '0 108 '2 109 '0 109 '2 0087 parts	107 ° 0 106 ° 2 106 ° 3 106 ° 2 106 ° 5 of the II. F	110.0 110.0 117.0 118.8 118.2	109'4 107'5 109'8 113'0	109:3 109:8 110:4 109:8	108.2 108.8 110.0 110.2 111.8	114.8 114.2 115.0 115.3 115.4	118.9 118.2 118.6 117.8 117.6		
M. s. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	105 ° 0 105 ° 0 105 ° 0 105 ° 0 One	102.0 104.0 104.1 102.8 Scale Divisi 612.4 612.4 611.4 615.4 612.2	$   \begin{array}{c}     108.2 \\     105.0 \\     104.8 \\     106.8 \\     \hline     000 = `000 \\     \hline     0587.6 \\     580.4 \\     577.4 \\   \end{array} $	108.0 108.2 109.0 109.2 0087 parts	106°2 106°3 106°2 106°5	110.0 117.0 118.8 118.2	107.5 109.8 113.0	109.8 110.4 109.8	108.8 110.0 110.5 111.8	114.2 115.0 115.3 115.4	118.2 118.6 117.8 117.6		
M. s. 0 50 0 55 0  M. s. 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0	105 ° 0 105 ° 0 105 ° 0 One	104.0 104.1 102.8 Scale Divisi 612.4 612.4 611.4 615.4 612.2	$   \begin{array}{c}     105.0 \\     104.8 \\     106.8 \\     \hline     600 = .000 \\     \hline     587.6 \\     580.4 \\     577.4 \\   \end{array} $	108.2 109.0 109.2 0087 parts	106°3 106°2 106°5 of the II. F	117.0 118.8 118.2	109°8 113°0	110.4 109.8	110.0 110.5 111.8	115.0 115.3 115.4	118.6 117.8 117.6		
50 0 55 0 M. s. 0 0 0 5 0 10 0 0 15 0 20 0 0 25 0 0 35 0 40 0 45 0	105 ° 0 105 ° 0 One	104.1 102.8 Scale Divisi 612.4 612.4 611.4 615.4 612.2	104.8 106.8 ion = .000 587.6 580.4 577.4	109°0 109°2 0087 parts	106°2 106°5 of the II. F	118.8	113.0	109.8	110°2 111°8	115.3 115.4	117.8		
55 0  M. s. 0  0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0	One 590'4	Scale Divisi 612.4 612.4 611.4 615.4 612.2	106.8 ion = .000 587.6 580.4 577.4	109.2 0087 parts 590.0	of the II. F	. 118.2			111.8	115.4	117.6		
0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0	590.4	612.4 612.4 611.4 615.4 612.2	587.6 580.4 577.4	590.0		1			Horizont	AL FORCE	•		
0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0	590.4	612.4 612.4 611.4 615.4 612.2	587.6 580.4 577.4	590.0		1							
5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0	_	612.4 611.4 615.4 612.2	580°4 577°4		1 001 4	593.4	571.4	584.4	586.0	593.2	587.8		
10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0		611.4 615.4 612.2	577.4	ひいひ て	592.8	594.2	574.0	588.2	588.2	591.6	588.6		
15 0 20 0 25 0 30 0 35 0 40 0 45 0		615 <b>.</b> 4 612 <b>.</b> 2		589.3	593.1	593.8	584.4	587.4	589.6	590.6	590.6		
20 0 25 0 30 0 35 0 40 0 45 0		612.2	$578^{\circ}4$	590.4	593.4	594.2	588.8	586.6	591.9	592.3	595.4		
25 0 30 0 35 0 40 0 45 0	1		584.4	588.6	594.8	593.8	590.9	590.2	595.4	590.4	593.8		
30 0 35 0 40 0 45 0	_	611.6	588.4	588.7	597.4	593.6	590.2	589.7	595.2	590.3	587.4		
35 0 40 0 45 0		610.9	586.9	589.0	597.0	593.6	589.4	592.2	594.7	590.6	583.4		
40 0 45 0	i	604.4	584.4	587.6	598.6	597.1	589.2	590.7	596.2	589.2	584.4		
45 0		594.9	584.4	586.8	596.4	593.4	583.8	590.4	597.6	588.6	582.6		
50 0		594.9	585.0	585.6	596.6	585.4	583.0	590.9	595.2	591.7	585.2		
	610.9	594.1	584.8	588.4	594.0	581.8	586.9	591.4	595.2	591.4	586.0		
55 0	614.6	593.9	586.6	590.4	593.4	578.4	586.4	589.2	596.9	589.6	584.6		
Thermometer	69°4	70°2	70°2	70°2	70°0	69°7	69°5	69°6	69°6	69°4	69°0		
<b>X</b> 6	One	Scale Divisi	on = .000	063 parts	of the V. F		<u>' </u>		VERTICAL FORCE.				
M. S.					1,00.1	100.0	1000	1.00.0					
0 0	184.4	185.0	190.5	184.2	182.1	180.8	185.7	180.6	179'1	178.8	177.2		
	182.6	184.9	190.3	184.2	181.4	180.8	185.3	181.0	178.4	176.0	176.8		
	182.6	184.9	190.2	184.5	180.5	182.5	186.3	181.0	180.7	176.0	176.7		
15 0 20 0	182.6 182.6	186.0 186.3	188.8 180.0	184.6 184.8	180.3	182.4	185.8 183.7	182°2 181°4	179°3 179°1	177:3	176°4 176°9		
	182.6	186.7	187.4	184.6	180.2	184.3	181.8	180.3	178.4	176.5	$170.9 \\ 177.2$		
	183.1	187.6	186.6	184.8	180.7	185.8	183.4	180.3	178.4	177.0 177.5	180.5		
35 0	183.1	186.8	185.4	184.8	180.6	188.2	182.4	179.4	179.6	177.1	179.8		
	183.1	186.3	185.4	184.1	180.7	188.2	181.8	179.4	179.4	176.9	178.7		
	183.8	187.0	185.4	184.3	180.6	185.8	181.2	179.4	179.4	177.4	180.4		
50 0	183.8	187.9	183.9	182.8	180.6	186.4	182.2	179.4	179.2	176.8	178.6		
	185.0	189.1	183.9	182.3	180.8	184.5	180.6	179.1	178.8	177.2	178.4		
Thermometer	6 [°] 7.9	68°5	68°6	70°0	70°·3	70°5	70°0	70°5	70°0	69.7	70°1		
Ţł.					 	1	Ingressing 1	Vumbow do	note decrees	na Wastarle	Declination,		
			ME	TEOROLC	GICAL O	BSERVAT			Lote decreas	ms in esterny	Decimation,		
i!		Them	mometers.		Wind								
Mean Göttingen Time.	Barometer at 32°.	Dry.	Wet.	Direc		Force.	-		Weather	•			
							-						
D. H. M.	In.	0	0			a •							
23 10 0	29.543	72.2	66.8	-	-	Calm.	General						
$\begin{array}{ccc} 11 & 0 \\ 12 & 0 \end{array}$	29.528	69.9	65.8	-	-	Calm.	Generall						
13 0	29.527 $29.555$	67.3	64.2	_	,	Calm. Calm.	General						
14 0	29 562	65.9	64.3		L L	Calm.	Generall	y clear; she	et lightning	nearly round	the horizon.		
15 0	29.543	65.7	63.7		_	Calm.					the horizon		
16 0	29.552	64.8	63.2			Calm.		y clear; she heet lightnir		nearly round	the horizon		
17 0	29.554	62.6	61.7			Calm.		neet Hghtnir heet lightnir					
18 0	29.562	63.1	62.3		_	Calm.		neet lightnir heet lightnir					
19 0	29.554	64.1	63.1		_	Calm.	Clear . s	heet lightnir	.e. .e.				
20 0	29.553	63.3	62.6	_	_	Calm.	Generall		·o·				
21 0	29.565	61.1	60.5	-	-	Calm.	Generall						
				1									

^a At 24^d 10^h, Thermometer of H. F.,  $68^{\circ}$  · 0; of V. F.,  $67^{\circ}$  · 6.

					MAGNET	CICAL O	BSERVATIO	NS.		Sep	tember 23rd	l and 24th.
		DECLINATI	ION.					Α	ngular Value	of one Scale	Division =	= 0' · 721.
21 ^h .	22ª.	23 ^h .	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	Gh.	7 h.	8h.	9 ^h .
Sc. Div. 117.8 120.6	Sc. Div. 116.8 117.3	Sc. Div. 117.7 117.2	Sc. Div. 116'8 116'2	Sc. Div. 121 0 119 2	Sc. Div. 119°0 118°1	Sc. Div 116 3 118 0	3   111.0	sc. Div 106 2 106 0	103.8	Sc. Div. 101.5 100.8	Sc. Div. 101°2 101°1	Sc. Div. 106.5 106.2
118.4 118.0 117.5	117.5 117.7 117.6	116.2 115.8 116.0	116.4 116.5	118°8 120°2	119.4 117.8	116.4	111.5	105.3	103°2 103°2	99.5	102.0 103.2	105.8 102.0
117.8 118.7	117°2 117°2	116.2 115.8	116.1 117.2 118.0	120.0 119.0 120.0	117.8 118.0 117.8	118°0 117°2 113°8	110.0	105.5 105.3 105.4	103°0 102°9 102°6	99.8	105.0 102.0	104.7 104.3 104.8
117.2 115.3 116.0	117.0 116.6 116.7	116.2 116.2 116.8	118.3 118.0 118.0	119°2 117°9 119°0	119.3 118.0 118.2	112°2 111°8 111°3	107.8	105°2 104°8 104°0	102.6 102.2 102.4	101.8 100.7 101.2	105.0 102.0	104.2 105.0 104.0
116.0 117.8	116.8	116.2 116.1	115.6 112.6	120.0 117.0	117.6 117.0	111.0	107.1	103.8 104.7	102°5 102°6	101.8 102.0	106.0 102.0	105°0 104°0
		Horizonta	L Force.			Increase,	in Scale Divisi	ons, corre	sponding to 1°	decrease of	Temperatur	re, 1.63.
581.4 580.8 580.0 580.8	587.4 588.6 591.4 591.5	590'4 589'4 588'4 583'6	588°9 589°4 588°9 588°9	585.8 582.9 580.9 577.9	573°9 571°4 575°9 574°4	566°2 566°7 565°0 563°4	565°2 566°4 564°2	563.8 563.6 565.2 566.4	571.6 573.4	574.4 573.6 571.6 573.6	586.4 589.4 590.8 591.4	603'4 608'2 609'4 605'6
584.6 584.4 581.8 589.2	590°4 590°4 588°6 590°4	584.8 585.4 588.0 588.4	586°9 587°4 585°4 584°9	577.4 577.9 578.4 578.4	574.9 571.4 570.9 565.4	564.8 564.4 563.8 561.8	565*9 562*2 563*9	564°3 563°6 564°7 564°0	574°2 575°2 575°0 574°2	576 ° 4 575 ° 4 581 ° 2 582 ° 6	591.8 592.4 594.6 595.4	607.4 604.8 601.2 601.0
587°4 586°7 585°0 585°0	590°2 589°8 589°2 589°4	589'4 587'4 589'5 588'9	585`1 584`4 585`4 585`4	577'9 577'9 575'4 576'9	566.4 567.4 567.9 568.2	564.0 562.4 564.6 565.6	565°1 564°1	564°9 565°6 567°5 568°8	573 '8 575 '2 574 '4 574 '6	582.8 585.6 586.8 587.4	596°2 596°2 597°2 601°4	598 '4 597 '2 599 '8 595 '4
69.0	69°0	68.4	68°0	68°.0	68.0	68.0	68.0	68°1	68.3	68.4	68°2	68.5 a
		VERTICAL :	Force.	· · · · · · · · · · · · · · · · · · ·	1	ncrease, i	n Scale Divisio	ns, corres	ponding to 1°	decrease of	Temperatur	e, 1°64.
180°2 181°7 181°0 179°9 179°2 177°3 177°0 177°7 177°4 174°2 174°2 174°2	175.4 175.3 175.4 175.5 175.4 175.4 175.6 175.6 175.6 175.6 175.6	175.6 175.6 175.8 175.8 175.8 175.8 175.8 175.8 175.8 175.8 175.6 175.6	175.8 175.8 175.8 175.8 176.8 176.8 176.9 177.1 177.1 178.9 178.9 178.9	178 · 9 178 · 9 178 · 9 177 · 9 178 · 6 178 · 6 178 · 7 178 · 4 178 · 4 178 · 8 178 · 8	177.5 177.3 178.5 177.9 177.0 177.2 177.8 177.0 177.0 177.4 177.7 177.4	177 · 4 177 · 4 176 · 9 176 · 8 176 · 9 177 · 8 177 · 6 177 · 6 177 · 6 177 · 1 177 · 2	176.6 177.7 177.4 177.8 177.1 177.4 178.7 178.7 178.7 178.3	180.0 177.5 177.5 177.5 179.1 179.4 179.4 178.0 177.9 179.7	178 '8 178 '8 178 '9 181 '3 181 '3 181 '0 181 '2 181 '1 180 '7 181 '0 181 '5 181 '7	182'3 181'5 181'4 181'8 181'2 181'3 182'6 183'1 183'0 183'6 184'4 183'8	183.8 184.0 184.0 184.0 184.0 184.0 183.9 183.6 183.6 183.6 183.7	183 7 183 9 183 9 184 7 185 0 185 0 184 8 184 8 184 8 184 8
70.0	69.8	69°.5	6 <b>9</b> .3	68°2	68.0	67.7	67.7	67.7	68.1	68.0	68.0	67.6 a
and increas	sing Horizon	ntal and Vert	ical Force.	<u> </u>	mpopor	ogia : r	Operation	IONG.				
Mean G	ottin ~~~	Pa	Ther	mometers.	TEOROLO		OBSERVAT	ions.				
Tin		Barometer at 32°.	Dry.	Wet.	Direc	etion.	Force.	_		Weath	er.	
	2 0 3 0 0 0 1 0 2 0 3 0 4 0 5 0	1n. 29.557 29.577 29.599 29.641 29.609 29.646 29.648 29.611 29.619 29.627 29.629	59.9 59.8 59.9 63.9 64.8 64.6 64.8 66.1 65.6 61.7 62.1	59'3 59'0 58'8 62'4 62'4 63'5 63'5 64'0 65'1 64'5 59'9 59'4	N.W. N.W. N.W. S W. b W. b N. by N. by N. by	by N.  I.  W.  y S.  y S.  w W.	Calm. Calm. Very light Very light Very light Very light Very light Calm. Light. Moderate. Very light	Ger Clo	nerally clear. nerally clear. ndy, udy; occasion udy; circum ndy; occasion ndy; occasion ndy; and rainy, ndy with rain. ndy; circum ndy; ccasion	. and cirstr . and cirstr al rain. al rain. . and cirstr	rat.	

Vol. III.

October 21st and	122nd.			MAGNET	ICAL OF	SERVATI	ONS.			-	
Mean Göttingen	Ang	ular Value	of One Scal	e Division =	=0'.721.				DECLINAT	HON.	
Time.	10h.	11 ^h .	12h.	13h.	14h.	15h.	16h.	17h.	18h.	19h·	20h.
M. s 0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0 50 0 55 0	Sc. Div. 108'9 108'0 109'2 109'8 109'8 110'5 111'0 111'0 111'7 112'8 114'1	Sc. Div. 114'0 113'1 112'0 111'0 110'3 109'9 112'0 106'0 103'8 104'2 109'8 112'4	Sc. Div. 113 '9 114 '0 114 '2 113 '1 111 '0 110 '2 111 '0 111 '2 111 '2 111 '3 111 '1 111 '4	Sc. Div. 112'0 112'0 112'3 112'0 112'2 112'7 113'1 113'2 113'6 113'6 113'0 113'3	Sc. Div. 113 '9 113 '2 113 '1 113 '5 113 '9 114 '0 113 '1 112 '2 111 '7 111 '0 110 '9 111 '1	Sc. Div. 113°3 115°0 115°0 116°3 117°2 117°1 119°0 119°7 123°8 124°8 128°0 131°0	sc. Div. 133.6 131.0 128.0 124.1 122.0 121.4 121.0 120.0 123.2 124.6 125.0 125.7	Sc. Div. 124 ' 2 123 ' 0 120 ' 2 119 ' 2 117 ' 4 115 ' 6 115 ' 8 116 ' 2 117 ' 0 116 ' 0 113 ' 3 112 ' 0	Sc. Div. 111 ' 0 112 ' 7 113 ' 0 113 ' 4 112 ' 8 112 ' 2 112 ' 7 113 ' 0 113 ' 2 112 ' 7 112 ' 4 112 ' 0	sc. Div. 111'2 111'3 111'2 111'8 112'0 112'8 113'2 113'2 113'2 113'4 113'4 113'4	Sc. Div. 113 '2 111 '2 111 '2 111 '0 111 '4 111 '8 113 '0 113 '4 114 '2 114 '5 113 '8 114 '5
м. s.	One	Scale Divis	sion = '000	087.					Horizon	TAL FORCE	
0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0 50 0 55 0	629°0 626°0 625°0 618°0 614°8 613°0 614°5 617°8 620°0 616°0 618°4 616°5	613.0 615.0 617.0 614.0 614.0 611.0 611.8 612.0 606.0 606.0 601.8 601.2	605.0 607.0 611.0 614.4 616.6 616.8 616.8 617.7 618.8 620.0 620.1	619.0 619.0 619.0 619.0 619.0 617.0 618.0 617.1 617.0 616.1 616.9 618.0	619 ° 0 618 ° 0 618 ° 0 619 ° 0 619 ° 0 620 ° 0 615 ° 0 612 ° 3 610 ° 0 608 ° 0	604.5 601.0 597.5 594.0 591.0 588.2 591.0 595.0 592.0 592.0	590°0 599°5 598°0 598°0 596°2 593°3 587°6 585°8 588°0 591°2 591°6	591'4 596'0 598'8 602'0 602'6 602'8 603'0 602'8 607'2 610'0 612'0 612'4	611.0 611.7 610.2 610.4 611.2 611.7 612.3 610.2 612.0 612.4 611.0 611.4	610°0 610°3 609°4 610°0 608°0 607°4 607°4 607°4 610°2 612°2 612°8 610°5	614.2 616.2 614.4 612.0 612.4 611.8 612.0 613.2 612.4 611.8 612.2 612.2
Thermometer	53°5	53°7	54°0	54°1	54°5	55°0	5 <b>4</b> ·7	54.3	54.0	53.7	54°0
М. s.	One		ion = '000					,	VERTICAL		
0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0 50 0 55 0	206°2 205°9 205°7 205°0 205°0 204°3 204°3 204°7 204°7 204°7 204°7 206°5 206°5	207 ° 0 207 ° 0 207 ° 6 207 ° 6 207 ° 6 206 ° 7 206 ° 7 206 ° 7 206 ° 7 207 ° 7 207 ° 7	206'3 206'3 206'8 206'8 206'8 205'5 205'5 205'3 204'7 204'7 204'7	204·4 204·5 204·7 204·7 204·2 204·2 204·2 204·2 204·2 204·2 204·2 204·2 204·2 204·2	204.2 204.2 204.2 204.2 204.2 204.2 204.8 204.8 204.8 204.8 204.8	203 '9 204 '7 204 '7 205 '5 206 '2 206 '2 206 '2 206 '5 204 '6 205 '4 205 '4	204'3 204'3 202'4 201'7 201'6 201'3 201'3 201'6 203'9 203'8 205'0	205°1 205°0 205°3 206°1 205°4 205°5 203°1 202°3 201°7 201°4 201°5	201'4 201'5 202'1 202'2 204'6 204'1 204'0 205'1 205'0 205'0 204'8 204'7	204.8 204.7 205.7 205.1 204.1 203.2 203.4 203.4 203.4 203.4 203.4 203.4	203.6 203.6 203.6 203.6 303.3 203.3 203.1 203.1 203.9 203.9 203.9
Thermometer	53.2	53.2	54.2	54.4	54.4	55.2	55°2	55°0	54°5	54.2	54°6
						=	Increasing	Numbers de	note decreas	sing westerly	Declination,
			ME	TEOROLO	GICAL (	BSERVAT	rions.				
Mean Göttingen Time.	Barometer at 32°.	Ther	wet.	Direction	Wind.	Force.			Weather.		
D. H. M.  21 10 0  11 0  12 0  13 0  14 0  15 0  16 0  17 0  18 0  19 0  20 0  21 0	In. 29.756 29.754 29.770 29.773 29.772 29.779 29.765 29.783 29.760 29.752 29.712 29.676	0 40·2 39·7 38·9 38·1 35·5 36·1 36·9 36·5 36·5 36·9 37·3	37·2 37·0 36·5 35·3 33·4 33·9 34·6 34·0 34·0 34·4 35·0	W. by W. by W. by W.S.W W.S.W W.S.W W.S.W W.S.W W.S.W	S. Ve S. Ve Ve V. Ve V. Ve V. Ve V. Ve V. Ve V. Ve V. Ve	Light. Calm. ry light, ry light. ry light. ry light. ry light. ry light. ry light. ry light. ry light. ry light. ry light.	Generally of Clouded; of	clouded; cir ircum. and rcum. and rcum. and ee. cum. and ce; circum cum. and ce-cum. and ce-cum. and	strat. cirstrat. strat and haze. cirstrat. cirstrat. strat.	cirstrat. cirstrat.	

					MAGNET	ICAL OB	SERVATIO	NS.		October 21st and 22nd.			
		DECLI	INATION.					Λng	gular Value	of one Scale	e Division =	=0'`721.	
21 ^h .	22 ^h .	23 ^h .	Oh.	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .	
sc. Div. 115 '2 116 '0 118 '2 119 '4 118 '8 119 '0 119 '0 118 '8 116 '5	Sc. Div. 106 '2 105 '6 105 '8 105 '0 105 '2 103 '5 103 '8 102 '1 103 '4	Sc, Div. 110°2 110°8 113°7 113°9 115°3 115°9 115°0 117°1 121°3	sc. Div. 116·3 117·4 119·1 117·4 118·8 117·9 120·3 116·8 119·0	Sc. Div. 119°1 117°7 117°7 117°0 117°8 117°9 115°0 113°8 113°9	Sc. Div. 114'0 113'0 114'2 113'8 113'6 112'0 112'2 113'9 112'7	sc. Div. 108 '7 108 '0 110 '0 110 '6 109 '7 115 '0 114 '2 110 '0 110 '0	Sc. Div. 114 '0 111 '4 111 '2 112 '0 110 '0 110 '2 110 '2 108 '8 109 '2	Sc. Div. 110 '2 109 '4 110 '4 111 '0 109 '4 108 '8 108 '8 107 '7 109 '0	sc. Div. 108 '8 107 '2 107 '0 108 '0 110 '2 107 '2 106 '0 108 '4 107 '5	Sc. Div.   103 ° 0   102 ° 8   103 ° 5   106 ° 2   107 ° 0   107 ° 5   102 ° 2   105 ° 4   104 ° 0	Sc. Div. 103 ' 5 103 ' 0 104 ' 2 104 ' 1 104 ' 8 104 ' 2 104 ' 4 104 ' 0 106 ' 1	c. Div. 107.6 109.0 108.0 109.0 108.7 108.8 111.8 112.0 114.3	
112.4 109.8 106.8	106.0 107.4 108.7	119.4 119.1 118.7	118.1 117.8 118.3	114.7 114.2 114.0	112.0 110.5 110.5	112.0 113.0 113.3	107.6 109.3 111.0	110.5 110.8 111.8	105.5 103.2 103.5	104.8 103.0	106.5 107.1 108.5	114°1 114°9 114°4	
		Horiz	ONTAL I	orce.		Increase, in	Scale Divisi	ons, correspo	onding to 1°	decrease of	f Temperatu	re, 1.63.	
610.4 610.0 607.2 604.8 606.0 606.6 606.8 604.2 600.8 594.6 600.0 599.2	594.6 595.8 593.4 596.8 596.2 601.0 597.5 611.2 613.4 616.1 619.8 620.2	620.6 618.8 620.7 618.2 618.5 620.3 616.2 620.0 624.2 622.2 622.6 621.8	620·2 618·0 619·4 616·2 618·0 616·8 619·1 619·8 618·7 619·1 617·5	618 · 2 614 · 0 615 · 5 613 · 8 612 · 8 612 · 0 611 · 0 610 · 2 606 · 5 601 · 2 601 · 0	599.0 597.1 595.8 600.0 602.0 603.0 603.4 600.0 595.0 597.0 595.0 596.0	591.0 588.0 587.5 590.0 585.5 577.5 583.0 581.2 585.6 591.5 593.6 589.2	584.0 579.0 584.0 590.4 590.2 589.2 592.0 591.0 593.8 589.4 587.0 587.4	584 '3 581 '3 581 '0 582 '2 580 '3 576 '8 572 '0 569 '2 571 '0 573 '2 575 '8 577 '4	587.0 580.2 578.0 576.8 574.0 578.2 578.0 580.5 583.8 586.0 585.6 583.4	585.6 591.2 591.2 603.8 601.2 611.8 599.6 598.2 596.5 594.7 599.5 597.2	595:3 598:0 599:2 601:5 603:0 608:8 604:8 605:0 608:2 611:2 616:2 618:8	618.8 619.1 621.4 611.5 611.8 607.1 610.2 614.2 614.0 611.8 616.4 616.5	
54.0	5 <b>4</b> °2	54°2	54°0	53.6	52.7	53.0	53.0	53.0	52°·8	52.6	52.4	52°1 a	
		Vert	ICAL FOR	CE.	I	Increase, in	Scale Divisi	o <b>ns, corr</b> espo	onding to 1°	° decrease of Temperature, 1.64.			
203'4 201'9 200'9 200'9 200'5 200'1 200'1 198'5 196'9 194'0 189'7	186.7 184.9 184.2 185.1 184.2 187.7 189.7 191.5 190.9 193.0 193.0	193.0 193.9 194.8 194.1 195.4 196.2 196.2 197.0 197.3 197.3 196.6 197.5	197'7 198'0 198'5 197'7 198'9 199'5 200'9 200'5 201'9 203'2 203'0 200'6	200'4 200'6 199'0 199'0 199'0 201'1 201'3 201'3 201'4 201'4	200 · 9 200 · 9 200 · 7 200 · 7 201 · 1 203 · 9 204 · 0 203 · 5 203 · 5 204 · 2 203 · 2 204 · 1	202 · 5 202 · 5 203 · 2 203 · 2 202 · 4 201 · 0 202 · 9 204 · 0 203 · 9 204 · 8 203 · 1 202 · 7	202.7 202.7 203.4 204.6 204.4 203.2 202.7 202.6 203.1 202.6 202.6 202.0	201.8 202.0 202.2 201.6 203.1 203.9 203.5 204.6 206.5 207.4 208.5 209.4	211.4 211.6 212.4 211.0 210.3 211.3 211.3 210.1 210.1 209.5 209.1 207.5	202.6 202.6 205.2 208.9 208.8 209.8 209.6 207.5 207.5 207.5 208.3 208.3	207 · 2 208 · 5 207 · 4 208 · 3 207 · 5 209 · 1 207 · 8 208 · 4 208 · 0 208 · 8 208 · 7 210 · 0	208.7 209.7 209.0 209.0 208.7 210.2 211.7 210.8 209.9 210.5 210.1	
5 <b>4</b> °4	5 <b>4</b> .6	54°7	5Š·7	$5\overset{\circ}{5}.0$	53.3	53.4	53.3	53.8	53.2	53.0	52°·6	52°4a	
and increas	sing Horizon	ntal and Ver	tical Force.										
	-				TEOROLO	OGICAL	OBSERVAT	TIONS.					
Mean G Tir		Barometer at 32°.	Ther Dry.	Wet.	Direc	etion.	Wind. For	ce.	-	w	eather.		
	2 0	In. 29 644 29 617 29 587 29 581 29 557 29 538 29 538 29 587 29 609 29 638 29 674	38°1 38°1 37°9 37°7 37°9 38°1 38°1 37°3 38°3 35°5	35.7 35.9 36.1 35.9 36.3 36.8 36.2 35.5 34.6 33.8 33.8 32.6	S.S S.S S.S S.S V.S N. b	W W W W W W	Mode Mode Nearly Nearly Nearly Mode Brisk, wit Brisk, wit Brisk, wit Brisk, wit	calm. calm. calm. calm. rate. th gusts. th gusts. th gusts. th gusts.	Cloudy; Generall Cloudy; Cloudy; Cloudy; Generall Cloudy, Cloudy, Cloudy; Cloudy;	Weather.  udy; fine, with haze.  udy; fine, with haze.  nerally cloudy.  udy, but fine.  udy; fine; circum. and haze.  udy; fine; circum. and haze.  nerally clouded.  udy, with haze.  udy, with cir. and haze.  udy; circum. and haze.  udy; circum. and haze.  udy; circum. and haze.			

November 27th	and 28th.			MAGNE	rical o	BSERVATIO	ONS.					
Mean Göttingen	Ang	gular Value	of one Scale	Division =	= 0' .721.	•			DECLINAT	TION.		
Time.	10h.	11h.	12h.	13h.	14h.	15h.	16h.	17 ^h .	18h.	19h.	20h.	
M. s.	Sc. Div.	Sc. Div.	Sc. Div. 109 2	Sc. Div.	Sc. Div	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div	
$\begin{array}{ccc} 0 & 0 \\ 5 & 0 \end{array}$	112.0	110.0	111.5	140.0	118°2		120.0	116.5	116.2	110.1	109.2	
10 0	112.2	108.8	110.3	135.6	116.0		118.4	115.3	114.6	110.8	109.0	
15 0	111.4	110.3	113.3	132.4	117.1		115.9	115.0	115.0	112.0	109.5	
20 0	110.0	109.8	112.6	132.0	116.7		115.3	114.7	114.1	113.8	111.1	
$\begin{array}{ccc} 20 & 0 & \bullet \\ 25 & 0 & \bullet \end{array}$	111.5	110.0	113.0	126.8	115.2	120.2	115.4	114.1	113.6	113.2	110.9	
30 0	110.3	110.0	111.3	124.8	113.8		115.2	113.9	113.5	113.8	108.0	
35 O	111.0	110.0	112.0	125.4	113.5		115.7	114.6	112.8	112.7	109.0	
40 0	111.5	111.7	115.0	126.5	113.3		115.1	114.4	111.3	112.5	109.6	
45 0	111.0	112.4	117.2	127.0	115.0		114.9	115.0	110.0	112.8	107.8	
50 0	110.5	112.2	121.2	124.3	115.0		115.0	115.2	109.6	112.1	108.7	
55 O	110.0	110.7	127.2	122.0	116.3		115.3	115.9	110.4	111.5	109.0	
м. s.	One	Scale Divi	sion = '00	0087 parts	s of the H.	F.		·····	Horizoni	AL FORCE	<u>'</u>	
	637.0	636.0	619.0	622.2	628.4	620.1	641.4	699.9	606.0	1 (0110	200.0	
$\begin{array}{ccc} 0 & 0 \\ 5 & 0 \end{array}$	637.2	636.2	619.8	634.2	625.8		643.4	$622.2 \\ 623.5$	626.2	624.0	628.0	
10 0	637.0	632.0	619.7	638.4	623.8		646.0	625.2	625 2	623.2	627.5	
15 0	641.2	631.2	617.0	637.0	624.0		641.0	625.2	626.6	623 ° 0 624 ° 0	624.5	
20 0	642.0	631.6	618.3	637.2	622.2	620.4	640.8	626.2	626.1	624 0	622.0	
$\begin{array}{ccc} 20 & 0 \\ 25 & 0 \end{array}$	641.2	629.2	616.4	636.2	624.8	632.6	635.0	627.8	625.2	623.0	620°0 618°0	
30 0	638.6	627.4	615.3	635.0	625.7	642.8	632.2	626.0	626.0	625.0	618.2	
35 0	638.0	624.8	615.0	635.4	626.0	645.8	631.0	625.2	627.2	625.0	624.8	
40 0	638.3	623.0	617.5	632.2	625.6	640.5	628.5	625.0	628.0	626.8	625.0	
<b>45</b> 0	639.4	622.2	618.2	630.8	620.2	640.8	624.0	623.2	625.2	628.8	623.0	
50 0	637.0	$622 \cdot 2$	616.2	631.1	620.8	638.2	621.6	623.2	624.2	630.0	622.0	
<b>5</b> 5 0	635.2	620.8	616.0	630.0	620.0	634.2	620.8	623.5	624.0	631.2	621.8	
Thermometer	42.7	43.0	44.0	44.2	44.4	44.8	45°6	46.4	46.8	46.2	46.5	
	One	Scale Divis	ion = '000	0063 parts	of the V.	F.			VERTICAL	FORCE.		
M. S.	00111	010:0	216.2	218.2	215.4	212.8	001:4	00514		005.5		
0 0	221.1 220.6	$218.0 \\ 218.4$	216.2	217.4	215.4	212.0	201.4	205.4	207.4	205.7	204.6	
5 0	220.4	218.6	214.2	216.7	215.6	210.8	202.3	205.8	207.4	204.9	204.6	
$\begin{array}{ccc} 10 & 0 \\ 15 & 0 \end{array}$	220.3	216.4	215.1	216.7	215.7	209.6	201.2	206.8 206.7	$207.5 \\ 208.2$	204.7	204.6	
20 0	220.4	216.3	215.4	218.1	215.7	208.2	$\frac{201}{201} \cdot \frac{2}{2}$	206.6	$\frac{205}{206.7}$	204.6 204.6	204.6 204.6	
$\frac{20}{25}$ 0	220.4	216.3	216.6	215.3	215.3	209.6	200.7	206.6	$\frac{206}{206} \cdot 7$	204.6	203.1	
30 0	220.5	216.5	216.4	$\frac{215.3}{215}$	215.3	205.0	201.1	206.2	208.0	204.6	203.1	
35 0	220.8	215.7	218.1	215.0	215.3	205.3	201.8	206.5	208.9	204.9	203.3	
40 0	220.2	215.6	218.3	215.0	214.6	200.9	202.2	206.0	206.9	204.9	203.2	
45 0	221.4	216.5	218.7	215.0	214.6	200.8	202.9	206.0	207.1	204.9	202.6	
50 0	221.1	216.2	218.0	215.4	214.1	200.8	204.0	205.6	206.5	205.6	202.6	
55 0	218.1	217.4	218.0	215.4	213.3	198.2	204.8	206.4	206.4	205.5	202.6	
Thermometer	42.0	43.1	43.6	44.0	4 <u>å</u> ·7	45.2	46.4	47.3	47°2	47°3	47.5	
							Increasing 1					
			ME	TEOROLO	OGICAL	OBSERVA <b>T</b>		vambers der	Tote decreasi	ng westeriy	Decimation	
		Ther	mometers.			Wind.						
Mean Göttingen Time.	Barometer at 32°.	Dry.	Wet.	Direc		Forc	e.		We	eather.		
р. н. м.	In.	0			Ì							
27 10 0	29.429	33.4	30.7	S.E. t	ov S	Ligh	ıt.	Cloudy	cumstrat. 2	nd alm		
11 0	29.395	34.7	31.7	S.E. i		Moderate, w		Cloudy	cumstrat. 2 cumstrat.	mu circum	•	
12 0	29.367	36.1	31.8	S.S.		Bris		Cloudy;				
13 0	29.373	36.1	32.7	S.S.		Fres		Cloudy;				
14 0	29.364	35.5	32.9	S.S.		Brisk, wit		Cloudy;				
	29.359	35.2	33.0	s.v	v.	Bris	k.	Cloudy, w				
15 0	29.356	34.1	32.9	S.V		Moderate, w		Cloudy:	nist and rain	1.		
15 0 16 0		34.9	34.0	S.V		$\mathbf{L}$ igh	ıt.					
16 0 17 0	29.334		1 01 0						, with rain. ; mist and rain.			
16 0 17 0 18 0	29.337	35.7	34.7	S.V		<b>V</b> ery li						
16 0 17 0 18 0 19 0	29°337 29°326	35.7 35.6	34.7 34.6			Caln	n.	Cloudy; r				
16 0 17 0 18 0	29.337	35.7	34.7				n. n.	Cloudy; r Mist, and	nist and rain	ain.		

					M AGNET	ICAL O	BSERVATIO	NS.		No	vember 27tl	and 28th.
		DECLINATI	on.					Ang	ular <b>V</b> alue	of one Scal	e Division =	= 0' · 721.
21 ^h .	22h.	23 ^h .	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^ћ .	6h.	7 h.	8h.	9 ^h .
Sc. Div. 110.5 112.0	Sc. Div. 107.8	Sc. Div. 106°1 106°8	Sc. Div. 111 ° 0 113 ° 0	Sc. Div. 113°1 113°2	Sc. Div. 114.4 115.0	Sc. Div 118 8 118 0	117.1	Sc. Div. 115 * 5 113 * 9	Sc. Div. 109°1 110°1	Sc. Div.	Sc. Div. 105°2 105°0	Sc. Div. 108 ° 0 108 ° 0
112.8	105.8	108.0	113.0	114.5	115.0	118.4		113.6	111.5	110.0	109.0	108.2
113.0	107.0	108.2	112.8	114.2	115.2	118.0	117.8	112.6	112.0	109.9	106.0	108.8
111.1	107.0	109.3	112.0	116.0	115.0	117.6		112.0	115.5	108.9	107.0	108.4
111.5	106.0	110.0	111.0	114.4	113.8	118.8	117.8	111.0	112.5	108.4	107.0	108.0
111°3 111°7	106.0 102.8	109.8	111.7 109.0	114.0 114.6	116.0 112.4	118.8		112.8 113.5	$\frac{110.9}{112.8}$	107.4	107.5 107.6	108.8 108.0
111.7	107.2	109.0	113.0	114.0	116.0	118.0	116.4	111.8	114.1	107.2	107.9	108.2
111.1	108.0	108.8	114.0	113.2	116.0	118.7	117.2	110.0	112.8	105.0	107.8	108.8
109.8	107.5	111.1	114.8	114.0	117.2	117.6		109.4	113.0	106.0	108.0	108.7
110.0	106.3	111.0	114.0	113.8	118.6	118.4	115.1	109.5	112.0	105.5	107.8	109.7
		Horizonta		,			in Scale Divisio	1 :	nding to 1	decrease of		
621 5	620.0	631.1	634.5	631.0	626.0	621.2	617.9	614.0	604.0	611.2	614.0	607:5
625.0	614.0	629.5	637.0	632.5	623.2	623.3		611.5	604.5	614.0	610.4	612.0
629°2	616'8 620'4	631.0	633°0 634°2	631.6 632.0	$623^4 622^2$	$622.0 \\ 621.5$	619.6	609.0 610.2	605*0 608*0	610.8	606.0	613°0 614°0
630.0	623.0	628.2	634.2	632.6	621.4	620.5		603.5	607.2	609.0	609.8	612.0
631.0	624.0	631.0	632.5	631.3	620.3	621.2	617.2	606.5	606.3	609.4	612.0	612.2
631.0	621.0	634.2	634.0	628.2	624.2	621.4	619.3	608.2	603.0	609.0	612.0	616.1
630.8	620.0	633.0	638.5	628.7	620.2	620.3		604.0	603.5	609.0	611.0	614.5
630.8	623.0	634.0	630.0	628.0	625.0	620.0		607.0	603.5	612.0	609*2	615.0
631°2 626°0	626.0	634.0 635.0	630.0	626°2 623°0	$623.2 \\ 622.3$	620.4		606.2	609*2 610*0	$\begin{vmatrix} 611.4 \\ 608.2 \end{vmatrix}$	608.0	615.2 618.0
625.8	630.0	637.0	631.0	623.6	623.0	618.2		606.5	608.0	611.0	610.3	620.0
46°8	48°4	48.9	49°4	49.4	49°4	49°6	49°6	49.6	49°·8	49.9	50°·5	5 i · 2 a
		VERTICAL 1	Force.		]	ncrease,	in Scale Divisi	ons, correspo	nding to 1	decrease o	f Temperatu	re 1.64.
200.3	198.8	198.4	201.0	202.4	200.2	200.0	202.2	202.8	203.1	205.5	204.1	203.7
199.7	198.1	198.4	201.0	203.0	200.4	201.5		203.4	203.4	206.9	204.1	203.7
199.7	197:3	198.4	201.0	203.0	200.4	201.5		202.5	203.1	206.9	203.7	204.7
199.6	197.3	199.4	201.0	201.5	201.1	201.5		202.2	203.2	206.9	203.7	204.7
$200.2 \\ 200.2$	197°3 196°6	199:8	201.0	201.6	200°7 200°2	201.5		202.0	204.8 204.4	205.9	203.7	204.7
200.5	196.5	200.3	201.6	200.2	200.1	201.2		203 1	204.5	205.9	204.8	204.4 205.1
200.6	196.2	200.2	200.4	200.7	200.6	201.9		203.5	204.2	205.1	203.7	205 1
200.6	195.4	200.3	201.8	200.8	200.1	201.9		203.7	205.1	205.1	203.9	205.1
200.7	196.2	200.1	201.8	201.2	200.3	201.9		202.8	205.5	204.2	203.7	204.5
200.2	198.2	201.0	202.4	200'2	200.7	201.9		202.8	205.5	203 9	203.7	204.5
<b>200.</b> 5	198.4	201.0	202.4	200.9	200.0	201.9	203.4	202.8	205.5	203.9	203.4	204.2
48.4	49.0	49.2	49.3	49.2	50°5	50°5	49.5	49.4	49°8	49.4	50.0	50°6°
and increa	sing Horizo	ntal and Vert	ical Force.		<u> </u>							
			1		TEOROLO	GICAL	OBSERVAT	IONS.	1			
Mean G Tir	öttingen ne.	Barometer at 32°	i	mometers.		1	Wind.		-	W	Veather.	
	шс.	at U2	Dry.	Wet.	- Direc	ction.	For	ce.	-			
D. 1 27 2	H. M.	In. 29:327	26.7	25:0			Λ-1	•••				
$\frac{2i}{2}$	- 1	29 327	36.7 37.3	35.9 36.2	_	_	Cal Cal				and circu	m.
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	29 329	37.3	36.2		_	Cal			with haze.	nd strat	
	1 0	29.366	36.9	35.7	-	_	Cal	m.		Cloudy; circum. and strat. Cloudy; circum. and strat. Cloudy; cirstrat.		
	2  0	29.394	38.3	36.0	S.V		$\operatorname{Lig}$	ht.				
	3 0	29.437   38.0   35.8   S.W. by W.   Very lig				cirstrat. a	ind haze.					
	4 0	29.475 29.483	38.5 40.3	36.5	S.W.	by W.	Very l			with haze.	.1.4.4	
	5 0   29 483   40 3   37 7   S.W. by W.   Light.   Cloudy; circum. and strat.   Cloudy, with circum.											
	7 0	29.506	43.0	38.6	w.s		Ligh	ht	1	with circu irstrat.	ш.	
	8 0	29.514	43.7	39.1	W.S	.W.	Bris	sk.	Clear; c	irstrat.		
;	9 0	29.521	42.6	38.1	W.S	.W.	Moderate, v	with gusts.	1 '	cirstrat.		
	i	1	1	l	1	į			1			

December 23rd an	d 24th.			MAGNI	ETICAL (	OBSERVAT	ions.				
Mean Göttingen	$oldsymbol{\Lambda}$ ngula	r Value of c	me Scale di	vision = 0	7721.				DECLINATI	ON.	
Time.	10 ^h .	11 ^h .	12 ^h .	13 ^h .	14h.	15 ^h .	16 ^h .	17 ^h .	18 ^h .	19 ^h .	20h.
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
0 0	107.0	107.5	110.1	134.0	123 9	123.8	122.7	118.2	114.0	113.2	116.7
5 0	109.2	109.2	110.3	138.0	123.8	122.0	121.7	118.0	113.2	113.3	116.4
10 0	113.8	108.4	111.1	132.0	126.8	122.2	120.0	119.0	113.4	114.0	116.6
15 0	117.6	107.0	113.8	131.2	127.1	123.6	120.2	117.3	113.9	114.5	116.0
20 0	120.1	104.7	115.2	134.5	125.8	128.0	123.0	115.0	113.9	114.3	116.5
25 - 0	122.9	10513	115.7	140.9	124.8	130.0	123.0	115.4	113.2	114.4	116'4
30 0	125.1	105.8	116.1	144.1	124.0	128.8	121.2	115.2	114.0	115.2	116.4
35 0	127:3	105.3	115.4	138.7	124.0	129.4	119.0	115.0	113.9	115.2	116.3
40 0	128.0	107.1	114.2	131.3	125.8	131.2	123.8	114.3	113.8	115.2	116.0
$\frac{10}{45}$ 0	119.8	109.0	116.3	126.2	126.0	131.8	123.2	114.8	114.1	115.8	116.5
50 0	112.9	109.0	119.9	123.7	126.1	131.0	120.3	114.0	113.9	115.4	116.5
$\begin{array}{ccc}  & 0 & 0 \\  & 55 & 0 \end{array}$	110.0	108.8	127.0	122.0	126.3	125.0	120.3	113.9	113.5	116.5	115.8
00	<u> </u>	<u> </u>	!	:	120 0	120 0	1200	<u> </u>	-	1	· · · · · · · · · · · · · · · · · · ·
M. s.	One Sc	eale Division	= .0000	87.					Horizoni	AL FORCE	,
0 0	623.0	631.1	629.0	587.0	611.0	617.5	623.0	635.0	636.5	636.5	633.0
5 0	623.0	629.7	627.6	592.0	611.0	615.2	619.5	631.5	636.0	636.1	633.4
10 0	620.8	635.0	628.0	588.0	614.1	615.0	616.0	633.0	634.0	626.2	633.6
15 0	620.0	635 · I	627.9	585.2	615.0	616.0	620.0	637.0	636.2	636.0	633.8
20 0	622.8	634.0	627.8	593.7	618.4	614.8	626.0	638.0	638.0	635.2	633.7
$\frac{20}{25} = 0$	628.8	634.8	627.0	604.9	620.0	617.0	634.0	637.0	637.0	634.6	635.0
30 0	626.4	635.6	626.9	619.0	625.0	618.0	636.2	635.0	638.0	634.4	634.6
35 0	626.2	631.6	626.8	620.0	627.2	619.0	631.0	636:0	637.0	635.0	635.0
40 0	628.2	631.1	621.6	618.4	623.0	621.0	636.0	637.0	636.0	635.2	633.2
	631.1	$\begin{bmatrix} 631.5 \\ 631.5 \end{bmatrix}$	610.5	616.0	622.2	$\frac{621.0}{621.4}$	640.0		637.0	635.0	633.0
,45 0	629.0	631.7						638.0			
50 0	629.0	630.0	601.0	617.2	621.8	623.0	637.5	637.0	637.2	635.0	634.2
55 0	020 0	600 0	591.0	615.0	618.2	625.0	641.0	636.2	637.0	634.7	634.2
Thermometer	41.3	41°3	42.0	41.8	41.4	41.6	42.0	42.1	42.0	42.0	42.3
M. S.	One Sc	cale Division	= 0.000	063.					VERTICAL	Force.	
0 0	219.6	218.4	217.4	222.9	215.8	215.2	213.0	198.9	208.0	209.1	206.9
5 0	220.2	$\frac{218 \cdot 2}{218 \cdot 2}$	$\frac{217}{217 \cdot 2}$	$\frac{222 \cdot 3}{222 \cdot 7}$	215.6	$\frac{215}{215} \cdot \frac{2}{3}$	211.4	200.1	208.0	209 1	207.1
10 0	219.8	218.0	216.9	219.1	219.7	215.5	210.2	200.8	208.2	207.8	207.3
$\begin{array}{ccc} 10 & 0 \\ 15 & 0 \end{array}$	219.8	218.0	216.6	218.6	219.7	215.5	208.0	201.3	209.2	207.7	207.2
20 0	219.1	218.3	216.5	$\frac{219.0}{219.0}$	220.6	215.3	204.8	201 3	209.2	207.6	207.3
25 0	219.9	218.3	216.0	$\frac{219}{219}$ .3	220.9						207.3
$\frac{25}{30} = 0$	219.0	217.4	216.0	220.8		215°3 214°0	204.6	302.8	209.2	207.8	207.4
					219.9		201.8	203.0	209.2		
35 0	218.4	218.6	216.0	219.4	219.9	214.1	203.4	205.3	209.2	207.4	207.4
40 0	218.6	218.3	216.3	215.9	219.9	214.0	202.7	206.0	209.2	207.5	207:0
45 0	218.6	217.7	217:4	215.8	216.2	214.0	201.1	206.8	209.4	207.6	207.0
50 0	218.5	218.0	220.1	215.8	215.5	214.0	200.2	206.8	209.2	207.5	207.1
55 0	218 5	217:3	221.0	215.8	215.2	214°1	200.5	208.0	209.2	207.3	207.0
Thermometer	40.0	41.0	4î·6	4 <b>î</b> °5	40.8	41.4	42.0	42.4	42.2	42.2	42°9
		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	*	and a minute of a t	e valid te etti (v. 1000		Increasing	numbers de	note dec <b>r</b> eas	ing Westerly	Declinati
			МІ	ETEOROLO	OGICAL	OBSERVAT	YONS.				
Mean Göttingen	Ranomat	Ther	mometers.	P OR PLANTAGE AND A STATE OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF TH	Win						<del>-</del>
Time.	Baromete at 32°.	Dry.	Wet.	Dire	etion.	Force.			Weathe	er.	
р. н. м.	Ir.	0	0								
23 10 0	30.184	1 .	i	İ	ĺ	C-1	1	1 -2	11		
11 0	30.148		1		-	Calm.		l; circum.	and haze.		
12  0	30.122		15.7			Calm.	, ,	; circum.			
- ·	30 157		13.4		-	Calm.		; circum.	•		
13 0	30.146	, , ,			-	Calm.		, with haze.			
13 0 14 0	00 140		16:4		-	Calm.		; circum.	and haze.		
14 0	20.100				-	Calm.	Calm. Cloudy, with haze. Calm. Cloudy; circum.; aurora.				
$\begin{array}{cc} 14 & 0 \\ 15 & 0 \end{array}$	30.126		1			Calm.					
14 0 15 0 16 0	30.092	16.2									
14 0 15 0 16 0 17 0	30.097 30.069	16.2 12.6	12.6	-	_	${ m Calm.}$	Cloudy	; circnm.	and haze; a	urora visible	e <b>.</b>
14 0 15 0 16 0 17 0 18 0	30.097 30.069 30.035	$ \begin{array}{c c} 16.2 \\ 12.6 \\ 13.7 \end{array} $	12.6 13.6	-		Calm. Calm.	Cloudy		and haze; a	urora visibl	e <b>.</b>
14 0 15 0 16 0 17 0 18 0 19 0	30.097 30.069 30.035 30.021	16.2 12.6 13.7 15.6	12.6 13.6 15.0	-		Calm. Calm. Calm.	Cloudy Cloudy	; circnm.	and haze; a	urora visible	e <b>.</b>
14 0 15 0 16 0 17 0 18 0	30.097 30.069 30.035	16.2 12.6 13.7 15.6 15.5	12.6 13.6 15.0 15.2	-		Calm. Calm.	Cloudy Cloudy, Cloudy,	; circum. ;	and haze; a	urora visibl	e <b>.</b>

^a At 24^d 10^h, Thermometer of H. F., 44° 8; of V. F., 44° 5.

					MAGNET	FICAL (	OBSERVATIO	ONS.		De	cember 23rd	1 and 24th.
		DECLINAT	ION.					Ang	ular Value	of One Scale	Division =	= 0'`721.
21h.	22h.	231.	Oh.	1h.	2h.	3h.	. 4 ^h .	5h.	6 ^h ⋅	7 ^h .	8h.	Sp.
sc. Div. 115 ° 0 115 ° 2 115 ° 0 115 ° 0 115 ° 4	Sc. Div. 111 '0 110 '0 109 '2 110 '0 110 '8	Sc. Div. 109 2 109 4 111 0 110 7 110 5	sc. Div. 111'2 111'8 111'9 111'8 112'0	Sc. Div. 116°5 116°8 116°0 115°1 114°7	Sc. Div. 118°1 115°4 117°1 117°0 118°2	Sc. Di 117 117 118 116 116	4   120°0 8   120°1 7   118°0 0   116°8 2   116°6	Sc. Div. 115 ° 0 113 ° 9 113 ° 7 113 ° 6 113 ° 8	Sc. Div. 112 0 111 8 111 5 110 4 110 8	Sc. Div. 110°0 110°3 109°4 111°0 109°4	Sc. Div. 109 * 2 110 * 2 109 * 7 108 * 6 108 * 2	Sc. Div. 110 ' 4 111 ' 2 112 ' 0 111 ' 8 112 ' 0
115.6 116.0 113.7 112.0 110.8 110.0 110.3	110°8 111°0 111°2 111°5 110°8 110°2 110°0	110°2 109°1 109°0 111°0 111°8 110°2 110°2	112.0   111.8   112.0   111.5   113.1   113.6   115.2	114.2 114.8 117.0 117.0 117.4 117.8 118.0	118°1 116°2 117°8 118°7 119°1 118°3 118°0	119 119 119 119 118 117 115	4   117.0 0   116.9 0   111.2 1   113.8 0   116.0	113.0 113.4 114.3 112.6 113.0 113.0 112.4	109°2 108°6 108°8 109°0 110°6 111°2 111°0	108.0 108.0 110.2 109.8 110.0 109.1 109.7	108.0 107.4 107.2 107.0 108.0 110.0	112.0 111.5 112.4 112.8 113.2 113.0 113.5
		Horizont	AL FORCE	•		Increase	, in Scale Divis	ions, corresp	onding to I	decrease o	of Temperatu	are, 1.63.
634'0 634'0 631'4 630'0 630'6 631'0 631'4 631'0 630'2 629'4 633'2 633'0	632.6 633.0 634.0 631.2 632.0 632.5 633.0 631.5 631.8 632.3 632.2 632.5	632 3 630 5 634 0 637 5 638 6 636 5 636 8 636 5 637 2 638 0 638 8 639 2	640.0 640.8 641.6 640.2 642.0 642.0 641.0 643.2 640.4 639.8 643.2 642.8	642.5 644.3 643.1 643.7 638.0 641.5 640.0 641.6 640.5 641.0 640.2 641.0	640°2 639°0 638°0 639°5 641°2 638°1 633°0 636°0 638°4 640°5 634°2 636°8	635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 ° 635 °	2 624.8 625.0 625.0 625.0 624.0 621.5 619.0 619.4 619.4 624.0 624.0	620°0 622°0 625°0 622°5 619°5 620°0 620°0 621°2 621°5 620°5 623°0 625°0	622·2 618·5 615·5 616·0 613·5 613·0 613·0 612·5 617·0 617·4 617·2	616°6 617°2 620°0 623°2 623°0 622°4 622°8 624°0 630°0 633°2 629°8 630°6	632*2 632*3 630*0 631*5 638*0 635*6 631*5 632*5 633*0 630*0 628*6 626*5	633.4 635.0 634.2 634.9 637.5 634.8 638.5 638.8 637.5 639.8 642.0 641.2
42.3	42.2	42.2	41.8	41.7	41.6	41°-4	42.0	43.0	44.0	44.2	44.6	4 1.8 a
		VERTICAL	Force.			Increase,	in Scale Divisi	ons, corresp	onding to 1	° decrease o	f Temperatu	re, 1.64.
207 · 0 207 · 1 207 · 3 207 · 3 207 · 2 207 · 3 207 · 6 207 · 3 207 · 4 207 · 5 205 · 9 205 · 4	205°3 205°0 205°2 205°2 205°2 205°2 205°2 205°8 205°8 205°6 205°2	205 ' 4 205 ' 4 205 ' 4 207 ' 1 207 ' 1 207 ' 1 207 ' 3 207 ' 3 207 ' 3 208 ' 3 208 ' 3 208 ' 3	208'3 209'2 208'9 208'9 208'9 208'5 208'5 208'5 208'5 208'1 208'3 208'2	208'3 208'3 208'9 208'2 208'5 208'5 208'5 208'5 208'1 207'5 206'4 208'0	207.5 207.4 207.4 207.4 207.9 207.9 208.0 208.1 208.1 208.5 208.5	208 6 208 8 208 8 208 8 208 8 209 7 209 6 209 7 209 7 209 7	5   209.1 209.6 3   209.4 3   209.4 7   209.4 6   209.5 6   209.3 7   209.7 7   209.7	209.5 309.5 209.1 208.9 208.9 208.6 208.3 207.6 207.6 207.6 208.6	208.6 207.2 207.2 207.2 207.2 207.2 207.2 207.2 207.2 208.2 208.1 207.8	207 · 8 207 · 7 208 · 4 208 · 4 208 · 1 207 · 9 207 · 9 207 · 9 208 · 1 208 · 1 207 · 1	206.6 206.5 208.1 207.7 207.7 208.1 207.4 206.2 205.5 205.0 205.0	206°3 206°3 206°0 206°0 206°0 206°1 206°1 206°1 206°1 206°1 206°1
42.6	43.0	43.0	42°2	42°2	42°9	42.2	4 l° 7	42°4	43.4	43.7	44.2	44°4 a
and increas	sing Horizo	ntal and Ver	tical Force.						2		2	
	Í	1		ME	TEOROLO	OGICAL	OBSERVAT	ions.				
Mean Ge Tin	öttingen ne.	Barometer at 30°.	Ther	mometers. Wet.	Direc	etion.	Force.			Weather	·.	
D. H. 23 22 24 ( )	2 0 3 0 0 0 1 0 2 0 3 0 4 0 5 0 6 0 7 0	In. 29 978 29 897 29 873 29 841 29 811 29 800 29 759 29 711 29 660 29 654 29 596	0 16.6 21.7 27.5 28.1 28.8 29.9 31.2 33.9 34.1 33.9 34.4 34.6	0 16:2 20:5 25:6 27:1 27:1 28:3 28:8 31:1 31:4 31:3 31:5 31:9	S.S. S. S. S. S. S. S. S. S. S. S. S. S.	.E. .E. y E. y E. y E. y E. by W. by W.	Calm. Calm. Very light. Very light. Very light. Very light. Very light. Very light. Very light. Very light. Very light. Very light. Very light.	Cloudy; Clouded, Clouded, Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy;	with haze. with circum., cwith haze. circum. a circum. a	cirstrat., an nm. and haze cirstrat., an and haze. nd cirstrat.	e. d haze.	

January 20th and	21st.			MAGN	ETICAL	OBSERVA'	TIONS.						
Mean Göttengen	$\Lambda$ ngula $f r$	Value of on	e Seale Div	rision = 0"	721.				DECLINAT	tion.			
Time.	10h.	11 ^h .	12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18 ^h .	19 ^h .	20 ^h .		
M. s. 0 0 0 5 0 10 0 0 15 0 0 20 0 25 0 0 35 0 40 0 45 0 50 0 55 0	Sc. Div. 113 '7 114 '6 112 '5 112 '1 113 '2 113 '1 113 '2 112 '9 112 '5 112 '0 112 '4 112 '8	113°1 112°9 112°9 113°2 114°1 115°0 115°4 115°0 116°2	Sc. Div. 117 1 115 0 114 9 115 0 114 8 115 2 115 5 115 7 116 0 115 6 115 2 115 9	Sc. Div. 116 0 115 3 115 0 114 2 116 0 117 0 119 8 126 2 129 6 131 0 130 5 129 0	Sc. Div. 126°3 125°0 123°3 121°2 119°0 117°0 115°8 114°8 114°6 114°0 114°0	sc. Div. 114'1 114'0 113'9 114'1 114'3 114'4 114'8 114'1 114'2 114'2 114'0 114'0	114.2 114.4 114.1	Sc. Div. 115 6 115 8 116 0 116 9 117 3 115 1 114 6 114 1 114 1 112 0 111 0 108 0	Sc. Div. 106'8 108'8 107'0 108'8 111'0 113'2 114'7 114'0 112'8 114'7 115'1 115'3	Sc. Div. 115 1 115 0 114 7 115 9 116 0 112 0 110 2 117 4 116 7 117 3 117 4 117 8	Sc. Div. 118'0 119'2 120'0 120'6 120'4 120'7 120'5 120'7 120'6 120'8 121'0 121'8		
	One Se	ale Division	= .00008	87 parts of	the <b>H</b> . F.		<u> </u>		Horizoni	AL FORCE			
M. s.  2 0  7 0  12 0  17 0  22 0  27 0  32 0  37 0  42 0  47 0  52 0  57 0	642.0 641.5 643.0 637.0 638.0 636.3 637.0 634.2 632.3 634.0 637.1 638.2	640°0 642°0 646°0 646°1 646°1 644°6 646°1 645°9 650°0 650°1 649°1 648°0	646.5 646.0 644.2 643.0 644.0 644.8 645.1 645.0 644.6 644.7 643.9 643.1	643°1 643°9 644°5 643°8 641°0 639°2 638°6 640°0 641°0 642°8 644°0 643°5	645.0 644.8 647.2 648.0 648.0 649.2 649.2 647.0 646.8 647.0 647.0	646.4 646.2 646.2 646.0 646.0 646.2 647.4 648.0 648.0 647.5 647.3	645.0 645.0 645.0 646.0 645.0 645.0 644.0 643.5 643.0 642.0 643.0 643.0	642°0 642°0 642°0 640°0 638°0 637°5 637°0 637°5 635°0 640°0 641°5 645°0	643.0 644.5 645.0 645.9 646.8 637.5 650.0 649.0 648.0 647.9 648.0 647.5	647.0 647.8 645.9 647.0 648.2 647.0 647.4 647.4 647.2 649.3 649.7 648.2	647.0 647.4 648.0 648.2 649.0 649.3 649.0 648.7 648.9 649.2 649.3		
Thermometer	37.0	38°0	38°6	38°5	38°5	38.2	38.4	3 <b>8</b> °0	38.4	39.0	38.6		
M. s.  3 0 8 0 13 0 18 0 23 0 28 0 33 0 38 0 43 0 43 0 48 0 53 0 58 0	One Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution Solution	213 '9 213 '3 213 '3 213 '6 213 '4 212 '4 212 '1 212 '1 212 '1 212 '1 212 '1 211 '4 211 '8 211 '8	212·3 212·5 212·6 212·1 210·7 211·2 210·8 210·7 210·7 210·3 210·3	210°1 210°4 210°5 210°5 210°5 210°2 210°3 210°0 210°6 210°8 210°4 210°4	the V. F.  209 0 209 1 209 1 209 1 208 8 208 8 208 8 208 7 208 7	208 '8 208 '8 208 '8 208 '8	210°2 210°3 210°4 210°4 210°4 210°4 210°4 209°4 209°4 209°4 209°4	209'4 209'1 209'1 208'9 208'9 208'9 209'6 209'6 209'6 209'6 209'4 208'4	208 '4 208 '4 208 '4 208 '4 208 '0 208 '0 208 '0 208 '0 207 '6 207 '6 207 '6	FORCE.  207 · 6 207 · 6 207 · 6 207 · 6 206 · 5 207 · 4 207 · 2 209 · 5 209 · 3 209 · 5 209 · 6	207.5 207.6 208.0 208.3 208.3 208.3 208.4 208.4 208.4 208.7 207.7		
Thermometer	36°·8	38.1	$39^{\circ}2$	40.0	39.9	39.9	39.7	39°4	39.6	40.0	40.0		
Mean Göttingen Time.	Barometer at 32°.	Ther	ME mometers.	TEOROLO Direc		OBSERVA' Wind.		Sumbers de	umbers denote decreasing Westerly Declination  Weather.				
D. H. M.  20 10 0  11 0  12 0  13 0  14 0  15 0  16 0  17 0  18 0  19 0  20 0  21 0	In. 29 '948 29 '922 29 '919 29 '917 29 '905 29 '887 29 '865 29 '849 29 '830 29 '810	21:3 20:0 19:4 18:9 18:1 16:9 16:9 15:3 14:4 13:5 14:5	17.8 17.4 17.2 16.7 16.4 15.6 15.7 14.4 13.3 12.6 13.3	W.S W.S W.S W.S W.S W.S W.S W.S	S.W. S.W. S.W. S.W. S.W. S.W. S.W. S.W.	Lig Moderate, Mode Mode Lig Lig Lig Very light (		Clear; cir. Clear; cir. Clear; halo round the moon. Clear; halo round the moon. Clear. Clear; cir. Clear; cir. Clear; cir. Clear. Clear. Cloudy; cir. Cloudy; cir.					

^a At 21^d 16^h, Thermometer of H. F., 35° '4; of V. F., 36° '2.

					MAGNE	rical oi	BSERVATIO	ONS.			January 20t	and 21st.
		DECLINAT	CION.					<b>A</b> ng	ular Value	of one Scale	Division =	0'.721.
21h.	22h.	23h.	Oh.	1h.	2h.	3h.	4 ^h .	5 ^h .	6h.	7 ^h .	8 ^h .	9h.
Sc. Div. 118 4 117 5	Sc. Div. 117.6	Sc. Div. 110.8 112.4	Sc. Div. 117.0 117.0	Sc. Div. 118.8 119.0	Sc. Div. 118'1 119'2	Sc. Div. 115 6 114 1	113.8	Sc. Div. 110°0 110°0	Sc. Div. 107 ° 0 107 ° 7	Se. Div. 109 ° 0 109 ° 2	Sc. Div. 112.0 112.0	Se. Div. 113 ° 0 113 ° 0
116·2 116·4 116·8	117.4 117.2 117.4 117.6	112.0 112.8 113.8	117.2 116.8 116.4	119.6 120.6 120.0	120.0 119.2 118.0	114.7 114.0 112.5	112.0 113.1 114.0	108.6 108.1 108.3	106.4 107.0 107.3	109°0 109°2 109°4	112.0	114.0 114.8 116.2
116.6 117.0 117.4	114.0 114.0 113.4	115.0 115.6 115.4 115.4	115.6 115.4 115.6 116.0	119.9 119.8 118.9 118.4	117.0 118.0 118.8 118.1	111.8 111.8 111.3	109.0 109.0 108.0	108.0 108.2 108.0 106.0	107.0 107.4 108.0 108.2	109.8 110.0 109.7 110.8	112.0 111.6 112.0 111.5	117.8 118.8 119.0 118.8
117.4 117.0 117.4	113.2 112.4 111.2	116.5 116.4 116.4	115.0 117.4 118.6	117.8 118.2 118.1	116.3 115.8 117.8	111.1	108.0 110.2 109.2	108.0 107.0 107.1	108.8 108.6	111.0 111.1 112.0	112.0 112.2 113.0	118.4 118.4 117.8
	<u>-</u>	Horizonta	L Force.	1	! I	ncrease, in	Scale Division	ons, correspo	nding to 1°	decrease of	Temperatur	<u> </u>
647 ' 4 647 ' 6 648 ' 0	645.8 645.7 645.7	642.6 643.0 644.4	650°4 650°2 648°8	649 <b>.</b> 5 650.0 650.0	642.5 641.0 640.8	628.0 626.4 624.0	620.4 618.0 615.9	629 '8 628 '0 628 '0	631.0 631.0 628.3	630.6 630.6 630.6	635°0 635°2 639°2	634.5 632.7 632.5
648 4 647 2 647 0	645.8 645.6 645.4	646.4 647.8 647.5	649°2 649°8 649°2	650°4 649°2 648°9	640°2 637°0 634°1	628.0 627.2 625.5	$617.2 \\ 622.5 \\ 624.1$	$\begin{bmatrix} 626.0 \\ 628.2 \\ 627.5 \end{bmatrix}$	629.7 629.8 630.8	631.4 631.6 633.0	640°0 639°8 640°2	631.4 634.5 638.4
644.8 645.0 645.4 645.4	645.0 644.4 640.5	650.4 650.0 648.0 650.0	650°2 650°0 651°2 650°8	647.6 647.6 646.2	634.0 632.2 632.5 630.0	624.0 623.0 624.0	626.6 625.0 626.5 627.8	627.6 630.0 632.0 632.2	630.6 630.7 631.4 630.8	632.6 633.7 630.0 632.0	638*5 637*2 637*8 636*2	639°0 642°2 642°3 642°8
645.6	641.8 639.2	651°2 650°4	652.0 652.4	644.8 644.5	628.0 631.1	624.0 623.0	632.0	632.2	630.6 630.4	632·5 635·5	635°0 633°2	642.5 644.4
38.0	3 ⁷ ·6	37.6	37.4	38.0	37.4	37°0	36°2	36.4	3 <b>Š</b> °5	35.7	36.0	35°9 a
	1	VERTICAL	Force.		1	ncrease, in	Scale Divisio		nding to 1°	decrease of	Temperatur	e, 1 64.
209 · 2 209 · 7 210 · 2 210 · 1 210 · 2 210 · 5 210 · 0 212 · 3 212 · 3 212 · 4 212 · 5 212 · 8	212.8 212.5 212.5 212.0 212.3 212.1 212.2 212.4 212.3 212.4 212.7 209.9	210·1 210·0 210·0 210·0 209·8 209·6 209·1 209·1 209·1 209·1 209·9	208 '9 208 '9 208 '7 208 '8 208 '9 209 '2 209 '6 209 '8 210 '0 210 '3 210 '5	210 · 5 210 · 4 210 · 4 209 · 7 210 · 3 209 · 5 209 · 5 209 · 5 209 · 5 209 · 7 210 · 4 210 · 1	210°1 210°1 209°0 209°0 209°0 204°7 206°2 206°8 207°9 208°4 208°8 209°5	210.0 210.2 210.2 210.2 211.5 211.7 211.7 212.4 212.5 213.3 213.3 213.3	213.7 213.7 214.3 214.3 215.0 215.0 215.4 215.2 215.2 215.6 215.6	215.6 215.6 215.6 215.6 215.6 215.0 215.0 215.0 215.0 215.0 215.0	215.0 215.0 215.0 214.3 214.7 214.7 214.7 214.7 214.7 214.7 214.7 214.7	214.5 214.5 214.5 214.5 214.7 214.7 214.6 215.6 215.6 216.4 216.4	216'4 216'4 216'8 216'8 216'8 216'8 216'8 216'8 216'8 216'8 216'8 216'8	217·4 217·4 217·6 217·7 217·7 218·1 219·2 219·2 219·3 219·3
39°5	39.3	39°1	39.1	39.1	39°1	38.4	37°4	3 ⁷ ·1	36°9	3 <b>6</b> .6	36°9	36.6 a
and increa	sing Horizo	ntal and Ver	tical Force.		TIPODOT O	CICAT C	Derbit in	IONS				
	j		Ther	mE'	TEOROLO		BSERVAT: Wind.	IONS.	1	the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s		-
Mean G	ne.	Barometer at 32°.	Dry.	Wet.	Direc		Fore	e.			eather.	
1 2	2 0 3 0 0 0 1 0 2 0 3 0 4 0 5 0 6 0 7 0 8 0	In. 29.820 29.822 29.824 29.822 29.836 29.840 29.820 29.816 29.816 29.818 29.854	14.4 14.2 14.0 13.5 12.9 13.3 13.8 13.3 9.8 9.8 8.7 6.5	13.0 13.2 12.8 12.4 11.3 11.6 11.6 10.9 8.9 8.9 7.8 5.6	W. by W. by W. by W. by W. by N. W. by N.W. I	y N.	Very light (no Very light (no Very light (no Very light (no Very light (no Very light (no Very light (no Moder Fres Brisk, wit Ioderate, w Moder Moder	early calm).  arry calm).  at.  ate.  h.  h.  h.  gusts.  ith gusts.  ate.  ith gusts.	Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy;	ir. eireum. an eireum., ei eireum., ei eireum., ei eireum., ei eireum. an eireum. an eireum. an	d cirstrat. r-strat., and l d cirstrat. rstrat., and d cirstrat. d cirstrat. rstrat. rstrat., and	haze.

	II											
Mean Göttingen	Angu	ılar Value o	f one Scale l	Division :=	0' 721.			<del></del>	DECLINAT	TION.	V-1	
Time.	10h.	11հ.	12հ.	13h.	14h.	15h.	16 ^h .	17 ^h .	18h.	19 ^h .	20h.	
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div	
0 0	110.0	116.0	117.0	110.8	112.5	113.2	114.0	110.2	110.2	109.8	107.0	
5 0	110.9	117.0	116.0	110.8	112.0		114.0	109.8	110.5	110.2	107.9	
10 0	110.8	116.0	114.5	111.5	112.5	112.2	114.2	110.4	111.0	110.8	108.5	
15  0	111.0	118.0	112.9	111.8	116.7	113.0	114.8	110.8	111.4	110.8	109.2	
20 0	111.0	119.2	112.0	112.7	118.8	113.5	114.2	110.8	111.0	110.0	110.0	
25  0	110.9	118.0	111.2	113.0	118.5		114.5	111.0	110.8	109.2	110.8	
30 0	110.4	118.8	111.1	113.8	115.5	111.9	114.8	111.6	110.4	109.0	110.4	
35 - 0	110.2	119.0	111.6	113.7	116.0		114.4	111.5	110.5	108.6	110.6	
40 0	110.5	121.0	111.7	113.0	119.2		113.2	111.8	110.0	109.0	111.0	
45  0	111.0	119.2	111.1	112.5	124.0		114.0	110.7	109.6	108.4	112.1	
50 0	112.0	118.2	111.2	112.5	124.2		113.2	110.8	110.0	107.2	112.3	
55 0	114.2	$117^{2}$	111.1	112.5	117.5		112.0	111.0	110.6	107.1	112.0	
	11				1	1			<u> </u>	1	1	
M. S.	One S	cale Divisio	n = '0000	987 parts o	f the H. F	·.			Horizont	AL FORCE.		
M. S. 2 0	636.0	624.5	630.0	626.4	627.0	646.6	632.8	634.8	634.5	634.2	632.1	
$\tilde{7}$ $\tilde{0}$	638.0	619.5	629.0	626.7	626.4	645.0	632.2	634.0	634.0	633.8	632.9	
12 0	640.0	617.5	630.0	624.8	625.2	643.8	632.8	635.0	634.2	634.2	633.0	
17 0	641.0	618.0	630.2	623.7	627.8	639.0	632.0	634.8	634.8	634.0	633.9	
22 0	641.0	620.0	629.0	624.3	631.0	638.4	633.2	635.0	634.8	633.2	633.8	
$\begin{array}{ccc} 22 & 0 \\ 27 & 0 \end{array}$	641.0	616.2	628.0	622.2	634.4	635.2	633.2	634.8	636.8	633.2	634.4	
$\begin{array}{ccc} 27 & 0 \\ 32 & 0 \end{array}$	638.0	614.5	627.5	622.6	632.2	633.0	633.9	634.0	637.0	634.0	633.2	
$\begin{array}{ccc} 32 & 0 \\ 37 & 0 \end{array}$	637.5	617.5	626.0	622.7	632.2	631.2	634.8	633.8	636.4	633.8	633.0	
42 0	635.0	620.5	625.5	623.0	635.0	631.2	635.0	634.2	635.8	633.8	633.0	
47 0	633.0	626.5	624.0	624.7	635.2	631.3	635.0	634.4	634.2	633.9	633.1	
52 0	631.0	628.0	625.5	625.2	645.4	633.0	635.2	635.2	634.4	633.0	632.9	
57 O	626.0	631.0	626.2	625.2	646.7	633.2	635.0	635.0	635.8	632.6	631.4	
										052 0		
Thermometer	43.9	43.4	43.5	43°9	43.6	43.4	43.3	43.5	43.5	43.4	43°6	
	One S	cale Divisio	n = .00000	63 parts of	the V.F.			•	VERTICAL	Force.		
M. S.	204.5	007:0	007:0	00010	000.1	100.7	10010	100.0	1 22212	1 202.0	00140	
$\begin{array}{ccc} 3 & 0 \\ 0 & 0 \end{array}$	204.5	207.9	205.9	202.3	202:1	198.7	198.2	199.9	200.3	201.6	201.0	
8 0	205.5	208.1	205.9	201.6	202.2	197.9	198.2	199.9	200.3	201.6	201.1	
13 0	205.5	208.1	205.2	201.4	202.2	197.9	198.8	199.9	200.3	201.5	201.0	
18 0	207.1	208.0	205.2	200.6	201.8	197.2	198.8	199.9	200.8	201.5	200.6	
23 0	206.9	208.0	205.2	200.5	201.8	196.6	198.8	199.9	201.1	201.5	201.2	
28 0	206.9	208.0	204.0	200.5	201.3	196.4	199.2	200.1	201.1	201.1	200.9	
33 0	206.9	208.0	204.0	200.9	200.9		199.7	200'1	201.1	201 1	200.9	
38 0	206.9	207:2	203.2	200.9	200.9		199.7	200'1	201.1	201.1	200.3	
43 0	206.9	207.2	203.2	201.1	200.4		199'9	200 1	201.3	201.1	200.3	
48 0	206.9	208.1	202.9	201.1	200.3	198.0	199.9	200.2	201.6	202.2	201.0	
53 0	206.9	208.1	202.9	201.6	201.4		199.9	200.2	201.6	202.5	201.1	
58 0	206.9	207.3	202.8	201.4	200.6	198.0	199.7	200.3	201.6	200'9	200.9	
Thermometer	42.9	42°·7	43.4	45°0	44.9	44.6	44.6	45°0	44.8	44.0	44.4	
							Increasing N	umbers de	note decreas	ing Westerl	y Declinati	
			M	ETEOROI.	OGICAL	OBSERVA'	rions.					
Mean Göttingen	Barometer	Ther	momete <b>rs.</b>			Wind.	—		77	Veather,		
Time.	at 32°.	Dry.	Wet.	Dire	etion.	For	ce.		,	eather.		
р. н. м.	In.	0	0									
26 10 0	29.837	25.3	23.3	E. h	y N.	Moderate, v	vith gusts.	Cloudy :	eireum. a	nd haze		
11 0	29.813	25.1	22.2		y N.	Brisk, wi		Cloudy	circum. a	nd haze		
12  0	29.774	1	$\frac{23.7}{23.7}$		y N.	Brisk, wi		Cloudy; circum. and haze.				
13 0	29.742	25.9	23.5	E		Brisk, wi	th gusts.		Cloudy; circum. and haze.			
14 0	29.741	26.3	24.5	Ē		Fre		Cloudy; circum. and haze. Cloudy; circum. and haze.				
15 0	29.700	27.6	25.7	Ē		$\mathbf{Fre}$	sh.					
16 0	29.676	27.9	26.2	Ē		Fre			circum. ar			
17 0	29.600	27.7	26.7	E		$\mathbf{Fre}$				aze, and sno	w.	
18 0	29.584			E		$\mathbf{Fre}$				naze, and sno		
	29.558	27.9	$\frac{27}{27} \cdot \frac{1}{3}$	E		Fre						
19 O			, -, 0					Cloudy; circum, haze, and snow.				
$\begin{array}{ccc} 19 & 0 \\ 20 & 0 \end{array}$	11			TF	]. 1	$\mathbf{Fre}_{i}$	sh.	Cloudv:	loudy; circum., haze, and snow.			
$ \begin{array}{ccc} 19 & 0 \\ 20 & 0 \\ 21 & 0 \end{array} $	29·494 29·466		27·1 27·2	E		Free Free						

 a  At 27d 10h, Thermometer of H.F., 45° '4; of V.F., 44° '6.

				7.1	MAGNET	ICAL O	BSERVATIO	ONS.		February 26th and 27th.					
		DECLINAT	ION.					$oldsymbol{\Lambda}$ ng	ular Value	of one Scale	Division =	0'.721.			
21h.	22h.	23h.	Oh.	1h.	2h.	3h.	4h.	5h.	6h.	7 ^h ·	8h.	9h.			
sc. Div. 112'0 112'2 112'1 111'6 111'5 111'1 110'8 111'3 111'4 111'3	Sc. Div. 112 '4 113 '0 113 '2 113 '4 113 '9 114 '0 113 '1 113 '0 113 '2 114 '0 113 '2 114 '0	Sc. Div. 113 '0 112 '2 112 '5 113 '0 113 '0 112 '9 113 '0 113 '0 113 '0 113 '2	Sc. Div. 112 '9 112 '5 112 '4 113 '0 113 '0 113 '0 112 '8 112 '7 112 '9 113 '1	Sc. Div. 113 1 113 4 113 8 113 4 114 0 115 0 115 2 116 0 115 3 115 3 116 0	Sc. Div. 116.0 116.0 115.9 115.2 116.2 117.0 117.3 117.0 116.8 116.2 116.0	Sc. Div 116 0 115 7 116 2 114 6 114 2 114 7 115 0 115 0 114 5 114 2 113 4	115.4 113.0 112.2 111.2 111.0 110.8 111.2 110.2 110.2 110.3	Sc. Div. 108 '4 107 '8 107 '0 107 '0 106 '2 105 '1 104 '8 104 '0 103 '4 103 '4	Sc. Div. 102 '8 102 '2 103 '0 103 '2 102 '6 103 '0 103 '2 102 '4 102 '2 101 '8 102 '0	Sc. Div. 102 '5 101 '4 101 '2 101 '8 102 '1 102 '9 102 '6 103 '2 103 '3	Sc. Div. 104 1 104 1 104 2 105 1 105 6 105 7 106 0 106 4 106 8	Sc. Div. 106 '7 107 '0 107 '7 107 '6 108 '0 108 '1 108 '2 108 '8 110 '0 109 '4 110 '0			
112.0	114.5	113.2	113.8	115.6	116.0	114.2		103 4	101.8	103.8	106.5	110.2			
		Horizonta	AL FORCE.		I	ncrease, i	n Scale Divisi	ons, correspo	nding to 1°	decrease of	Temperatur	e, 1 · 63.			
631.4 632.8 633.1 633.8 633.0 633.9 634.0 633.2 634.8 634.8 633.1 634.3	633 · 8 634 · 0 633 · 2 633 · 5 633 · 7 633 · 8 633 · 9 634 · 0 633 · 9 634 · 6 635 · 0	634.6 634.7 633.0 632.6 633.0 631.2 631.0 630.0 629.5 629.4 629.7 630.0	628.0 628.4 627.8 628.0 628.0 627.0 627.0 624.0 622.8 624.4 624.8 625.8	626·2 626·2 627·5 626·5 625·5 625·0 626·5 627·5 626·0 626·0 626·5 626·0	626.0 626.0 625.0 625.0 624.0 623.0 624.0 623.0 622.2 621.4 621.0 620.3	620 · 2 620 · 3 620 · 2 620 · 0 621 · 2 620 · 0 618 · 2 617 · 4 615 · 2 613 · 6	610°2 610°0 610°2 609°2 611°0 610°4 610°0 610°4 611°5	616.5 616.2 616.8 617.0 617.8 616.5 616.5 616.0 613.2 614.2 615.4	613.8 612.2 613.5 614.2 616.0 616.5 618.8 618.2 618.7 618.8 621.2 621.0	622.5 621.8 621.2 621.9 621.8 621.6 621.4 623.0 623.0 624.0 623.0 623.1	623 1 624 0 625 8 626 2 625 1 626 9 629 0 630 6 630 6 629 0 629 0	629 · 9 630 · 0 628 · 8 629 · 0 628 · 1 631 · 5 630 · 9 631 · 5 632 · 0 631 · 0 631 · 5			
43.3	42.8	4η6	42.0	42.0	42.0	42.2	42.9	44.4	44.4	44.8	45°4	45° · 2 a			
		VERTICAL	Force.		I	nerease, i	n Scale Divisi	ons, correspo	nding to $1^\circ$	decrease of	Temperatur	e, 1 <b>6</b> 4.			
201 · 3 201 · 9 201 · 6 201 · 1 201 · 5 202 · 0 203 · 0 202 · 8 203 · 1 202 · 4 202 · 0 201 · 8	202'1 201'7 201'7 201'9 201'9 202'0 202'0 202'0 202'0 201'0 201'0	200.6 200.6 200.5 200.6 200.6 200.5 200.5 201.0 201.0 201.0 201.0	201 1 201 1 201 1 201 1 201 0 201 0 201 0 201 5 203 1 203 1 203 1 203 1	203.6 203.8 203.8 204.7 204.7 204.7 204.7 204.7 204.7 204.7 204.7 204.7	204.7 204.7 204.7 204.7 204.2 204.2 204.2 204.2 204.2 204.2 204.2 204.2 204.2	204·2 203·8 203·8 203·8 203·8 203·5 203·3 203·3 203·5 203·5	203.4 203.8 204.3 204.1 204.1 204.2 203.7 203.9 203.9 203.9 203.8 204.5	204.5 204.5 204.8 204.8 204.6 204.6 203.1 203.6 203.6 203.3 203.3	203°3 202°5 202°3 202°3 202°3 202°2 202°2 202°2 201°3 201°9 202°2 202°1	201.9 201.9 201.6 201.6 201.4 201.1 201.1 201.1 201.1 201.1 200.9 200.9	200°8 200°8 200°7 200°7 200°9 200°9 200°9 200°9 200°9 200°9 200°9 201°0	201.0 201.0 201.1 201.1 201.1 201.7 201.3 201.3 201.5 201.5			
44.2	43.9	43.8	42°.7	42°2	42°0	42°1	42°6	43.7	44.2	44.4	4 <b>4</b> °8	44.4 a			
and increa	sing Horizo	ntal and Ver	tical Force.												
				ME	TEOROLO	GICAL	OBSERVAT	IONS.							
	öttingen me.	Barometer at 32°.	·	mometers.	Dines	tion	Wind.	00	-	w	eather.				
D. 1 26 2 27	H. M. 122 0 133 0 0 0 1 0 1 0 1 0 1 0 1 1 0 1 1 1 1	In. 29 '448 29 '392 29 '355 29 '301 29 '229 29 '217 29 '167 29 '073 28 '954 28 '925 28 '866 28 '838	27.5 27.5 26.3 26.5 27.9 27.0 27.7 28.9 29.3 29.9 30.7 30.8	Wet.  27.2 27.2 26.0 26.2 27.6 26.9 27.7 28.7 28.7 29.3 30.4 30.4	Direc E E E E E E E E E E E E E E E E E E E		Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh, with Fresh,	sh. sh. sh. h squalls. h squalls. h squalls. h squalls. h squalls. h squalls. h squalls.	Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy; Cloudy;	ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow. ady; circum., haze, and snow.					

March 24th and	25th.			MAGNET	TICAL O	BSERVATIO	ons.				
Mean Göttingen	Angula	ar Value of	one Scale I	ivision =	0′ 721.				DECLINA	TION.	
Time.	10h.	11h.	12h.	13 ^h .	14h	15h.	16h.	17h.	18h.	19h.	20h.
M. s. 0 0 0 5 0 10 0 0 15 0 0 0 0 0 0 0 0 0 0	Sc. Div. 104 ' 2 103 ' 8 102 ' 7 102 ' 0 102 ' 0 102 ' 0 102 ' 2 102 ' 2 102 ' 8 102 ' 6 103 ' 1 103 ' 1	Sc. Div. 103 ° 0 102 ° 8 103 ° 6 106 ° 2 111 ° 2 120 ° 7 125 ° 4 124 ° 8 123 ° 6 122 ° 5 120 ° 5 119 ° 5	Sc. Div. 117 ° 0 112 ° 2 109 ° 2 107 ° 8 108 ° 8 108 ° 4 109 ° 2 109 ° 0 109 ° 0 108 ° 8 107 ° 5	Sc. Div. 108 0 107 1 106 3 106 5 106 2 107 0 107 4 107 0 107 2 107 3 107 8	Sc. Div. 109 '3 110 '0 110 '0 110 '0 110 '0 110 '0 112 '4 112 '3 110 '0 107 '9 106 '9 107 '9 108 '9 108 '9	109.0 109.0 109.2 108.2 108.4 110.9 111.4 111.8 110.4 109.9 109.4	Sc. Div. 109 '2 109 '4 110 '0 111 '0 111 '1 110 '6 110 '2 108 '2 108 '3 108 '3 108 '0 106 '7	sc. Div. 107 ' 5 108 ' 0 107 ' 5 105 ' 0 104 ' 8 106 ' 8 107 ' 0 104 ' 0 102 ' 5 101 ' 0 100 ' 0 97 ' 8	sc. Div. 94 '4 93 '8 95 '3 99 '0 101 '2 101 '0 101 '2 99 '1 96 '5 94 '5 95 '8 99 '2	Sc.Div. 104'2 107'8 112'0 114'8 117'3 119'1 120'0 118'7 116'2 114'1 113'8	Sc. Div. 113 '8 113 '8 114 '0 113 '5 112 '2 112 '0 113 '0 113 '2 113 '8 114 '1 114 '0 113 '6
м. s.	One S	Scale Divisio	on = '000	087 parts o	of the H.	<b>г.</b>			Horizon	TAL FORC	Е.
2 0 7 0 12 0 17 0 22 0 27 0 32 0 37 0 42 0 47 0 52 0 57 0	628.7 626.0 626.0 626.5 626.2 628.5 628.8 629.0 631.2 630.6 631.4	630°2 622°8 612°7 604°2 601°8 609°3 612°2 615°8 619°0 618°5 618°0 620°0	617:5 619:6 617:5 614:2 613:0 612:5 614:5 617:4 621:8 619:8 621:2 622:8	622.8 622.5 620.5 617.8 617.1 618.6 620.0 619.4 617.6 616.0 614.7 615.6	615 · 8 616 · 0 616 · 3 617 · 3 617 · 0 615 · 6 618 · 0 619 · 0 616 · 9 618 · 0	618.0 618.3 618.0 617.0 619.1 619.0 620.8 623.0 620.5 619.0	619.1 617.8 618.2 617.0 618.0 618.0 622.0 621.0 621.0 620.9 620.9 620.4	621 '9 622 '0 622 '0 622 '0 622 '0 622 '0 618 '6 625 '2 622 '5 619 '0 616 '0 613 '2 612 '0	607 ° 0 604 ° 0 606 ° 0 607 ° 2 607 ° 7 607 ° 9 615 ° 0 614 ° 0 605 ° 0 603 ° 9 604 ° 3	607 5 605 0 608 0 610 2 616 0 617 5 621 5 622 0 623 0 622 0 620 0	619 ° 0 620 ° 0 620 ° 0 621 ° 2 622 ° 0 621 ° 9 622 ° 0 622 ° 0 620 ° 5 620 ° 5 621 ° 5 623 ° 0
Thermometer	5Î'8	52°6	52°·8	52°2	51.5	5ΰ0	50.4	50.1	50.0	49.8	49.6
M. s.  3 0 8 0 13 0 18 0 23 0 28 0 33 0 38 0 43 0 48 0 53 0 58 0	One S  195.8 195.2 195.0 195.0 194.9 194.8 194.8 195.2 195.6 195.7	195.7 195.7 195.5 195.5 196.4 196.7 196.7 196.2 196.2 195.5 195.2	$\begin{array}{c} 194.7 \\ 194.1 \\ 193.4 \\ 192.9 \\ 192.9 \\ 192.8 \\ 192.8 \\ 192.8 \\ 192.8 \\ 192.9 \\ 191.9 \\ 191.9 \\ 191.7 \end{array}$	191°1 191°1 190°9 190°1 190°1 190°3 190°4 190°5 190°5 190°5	191'2 191'2 191'2 191'2 190'9 190'5 190'5 190'5 191'6 191'6 191'6	192.0 192.0 192.0 192.0 192.0 192.0 192.0 192.0 192.0 192.0	191'4 191'1 191'1 191'2 191'2 191'1 191'2 190'8 191'1 191'1 191'1	190°7 190°7 190°7 190°7 187°0 186°0 184°3 184°0 183°2 179°7 179°6 177°1	VERTICAL  175.8 175.7 172.0 172.0 167.8 167.5 167.8 167.8 167.8 170.5 170.5 172.5	174.0 174.0 174.2 175.6 178.2 178.5 180.4 182.0 183.6 184.9 185.4 186.3	187·2 187·8 188·7 188·7 189·7 189·7 189·7 190·1 190·6 190·6
Thermometer	51.2	5Î.8	5η8	52.4	52.9	52.0	5 Å·3	5°1.2	5°12	5°1.4	50°8
							Increasing	Numbers de	note decreas	ing Westerl	y Declination,
			MI	ETEOROL	OGICAL	OBSERVAT	IONS.				
Mean Göttingen Time.	Barometer at 32°.	Ther Dry.	mometers. Wet.	Dire	Wir	Force.			Weathe	r.	
D. H. M.  24 10 0  11 0  12 0  13 0  14 0  15 0  16 0  17 0  18 0  19 0  20 0  21 0	In. 29:583 29:576 29:561 29:565 29:565 29:551 29:520 29:454 29:412 29:357 29:284	37'9 36'7 35'0 33'1 32'8 32'2 32'6 30'7 30'7 31'2 32'9 34'1	32 '9 31 '4 30 '8 29 '5 29 '2 28 '8 29 '3 27 '8 27 '8 28 '4 29 '7 30 '7	W.S.S.W. S. by S.S. S.S. S.S. S.E. 1 E. b E	by S. y W	Light. Light. Light. Very light. Very light. Very light. Very light. Very light. Very light. Light. Very light. Very light. Very light. Very light.	Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy; Cloudy; Cloudy;	; circum., ; circum., ; circum., ; circum., moon, diame ; circum., ; circum., ; circum., ; circum.,	cirstrat., a cirstrat., a	nd haze, and haze, and haze, and haze, and haze, and haze, and haze, and haze, and haze, and haze, and haze, and haze, and haze, and haze, and haze,	Halo round

² At 25^d 10^h, Thermometer of H. F., 52° · 6; of V. F., 52° · 5.

						MAGNETI	CAL OB	SERVATIO	NS.			March 24th	and 25th.
			DECLINAT	TION.					Aı	ngular Value	of one Scal	e Division =	= 0′′721.
	21h.	22h.	23h.	0h.	1h.	2h.	3h.	4 ^h .	5h.	6h.	7h.	8h.	9h.
	sc. Div. 112 '2 113 '7 115 '2 113 '0 112 '2 113 '0 112 '2 113 '0 112 '3 112 '0 112 '0 111 '9 112 '0	Sc. Div. 112.6 111.7 111.0 110.2 110.3 110.5 110.2 110.0 110.2 111.0 111.0		sc. Div. 110 ' 4 111 ' 2 110 ' 4 111 ' 2 111 ' 0 111 ' 3 111 ' 3 111 ' 7 111 ' 2 111 ' 3 111 ' 8	sc. Div. 111 '2 110 '0 110 '1 110 '8 111 '4 112 '2 112 '2 112 '0 112 '6 113 '6 113 '2 113 '8	115.8	sc. Div. 115°1 115°9 115°9 115°0 114°0 114°2 116°0 116°2 115°0 114°0 114°0 114°0	sc. Div. 113 '9 113 '4 113 '0 112 '4 111 '9 111 '0 111 '0 110 '9 110 '7 110 '0 110 '0 110 '0	sc. Div. 109°2 108°2 108°0 108°0 107°9 107°0 106°6 106°1 105°8 105°6 105°0	sc. Div. 105 ' 4	Se. Div. 101 '9 102 '0 101 '8 101 '6 101 '4 101 '2 101 '0 101 '0 101 '3 101 '6 101 '8 101 '0	Se. Div. 101 '0 101 '0 101 '6 102 '0 102 '8 103 '0 103 '0 103 '2 103 '0 103 '0 102 '7 102 '6	Sc. Div. 102*4 103*0 102*4 103*2 104*0 103*0 103*0 103*0 103*2 103*0 103*4 103*8
			Horizont	AL FORCE		Inc	erease, in	Scale Divisio	ons, corresp	onding to 1°	decrease of	Temperatur	e, 1.63.
	622 ° 0 622 ° 9 626 ° 4 623 ° 9 622 ° 0 622 ° 0 623 ° 0 622 ° 0 622 ° 0 622 ° 0 622 ° 0 622 ° 0 621 ° 0	621 '6 623 '2 623 '0 623 '9 624 '0 624 '2 624 '3 625 '0 624 '2 623 '6 623 '8 623 '7	624·2 624·8 625·6 624·8 623·2 623·6 624·2 623·8 623·7 623·6 623·8 623·8 622·0	621°3 622°8 622°2 621°0 621°0 621°0 619°8 619°0 618°2 618°8 618°6 616°3	616.0 612.4 616.0 616.2 616.8 617.0 616.6 619.2 617.8 616.5 616.8 617.8	618.6 618.2 619.0 620.4 617.8 619.0 616.2 615.0 616.4 615.0	612.6 612.1 613.0 613.8 612.1 609.8 607.4 606.5 608.0 608.0 606.2 605.8	606°0 606°0 604°6 601°0 602°2 600°7 600°0 601°1 600°8 600°0 599°0	596.0 596.0 596.0 599.0 599.0 599.8 600.0 601.9 602.5 604.8 605.0	603 '2 604 '0 604 '0 604 '0 605 '0 605 '0 606 '0 606 '0 607 '0 607 '0 607 '0	607:5 607:2 608:0 608:5 608:0 606:2 606:8 608:0 610:0 608:2 609:8	610°0 609°2 609°6 610°0 613°8 614°2 616°6 616°0 615°7 615°8 615°4 614°6	615 2 614 8 614 8 615 0 614 2 610 0 609 6 610 0 609 8 609 7 612 7
-	49°3	49.4	50°·0	50°·0	48°7	50°·5	51.4	52°0	52°·4	52.4	52.1	52.2	52°6°
-			VERTICAL	Force.		Inc	rease, in S	cale Division	ns, correspo	onding to 1°	decrease of	Temperature	e, 1 °64.
	189°4 189°4 189°4 189°1 188°9 188°9 188°9 188°9 188°9 188°9 188°9 188°9	188 '9 188 '9 188 '9 188 '9 188 '9 188 '9 188 '9 188 '7 188 '0 187 '8 188 '6	188.5 188.9 188.9 188.8 188.5 188.5 188.5 188.6 188.5 189.0 188.7 189.2	189°2 190°0 190°0 191°1 191°1 191°1 191°1 191°3 191°6 191°7 191°7	191.7 191.4 192.5 192.5 192.5 192.5 192.2 192.2 192.2 191.7 191.7	190°7   190°5   190°2   190°2   190°2   189°5   189°5   189°5   189°6   189°0   1	188°0 188°0 188°0 188°0 187°9 187°9 187°3 186°7 86°7 86°7 86°7 86°7	186.7 186.8 187.1 186.5 186.0 186.0 186.0 186.0 186.0 186.0 186.0	185.6 185.6 185.6 186.3 186.3 186.3 186.5 186.5 186.7 186.9 186.9	187°1 187°1 187°1 187°1 187°1 187°1 187°1 187°1 187°1 187°7 187°8 187°8	188.0 188.0 188.0 188.0 188.0 188.5 188.5 188.5 188.8 188.8 188.8	188 *8 188 *8 188 *8 190 *0 190 *0 190 *6 190 *6 190 *5 190 *5 190 *3 190 *4	190.4 190.6 190.6 190.4 190.3 189.8 190.1 189.8 189.7 189.7 190.5
	50°·3	5 Å . O	51.4	50°.6	49°8	5Î.0	52.0	52.2	52°1	52°0	52.5	52°4	52°5°a
a	nd increasi	ng Horizo	ntal and Ver	tical Force.						<u>-</u>		and the same of	NAME OF THE OWNER.
					ME	reorolog:	ICAL OI	SERVATI	ONS.				
	Mean Göt Time		Barometer at 32°.	Thern Dry.	wet.	Direction.	Wind.	Force.			Weather	r.	
	D. H. 24 22 23 25 0 1 2 3 4 5 6 7 8 9	M. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	In. 29 · 272 29 · 278 29 · 299 29 · 331 29 · 318 29 · 329 29 · 352 29 · 373 29 · 402 29 · 445 29 · 461 29 · 481	34·1 33·7 34·5 33·5 38·6 44·2 44·1 42·5 42·1 41·2 42·5 42·4	30.6 30.4 30.4 30.1 35.0 38.4 37.9 38.0 37.7 35.1 35.5 35.5	E. N.N.E. W.N.W. W.N.W. W.S.W. W. W. W. W. W. W. W. W. W. W. by N. W. W. W.	Ve Brisk,	ry light. Light. Light. Light. Light. Brisk. Brisk. Brisk. with gust oderate.	Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy	; circum., ; circum., ; circum., ; circum., ; circum., ; circum., ; circum., ; circum., ; circum., ; circum., ; circum.,	cirstrat., a cumstrat., cumstrat., cumstrat., cumstrat., cumstrat., cumstrat., cumstrat., cumstrat., cumstrat., cumstrat.,	nd haze. and haze. and haze. and haze. and haze. and haze. and haze. and haze. and haze. and haze. and haze.	

Mean Göttingen	Angula	. 37.1 . 0	~ • •								
	Tingula	r value of	one Scale 12	pivision = 0'	`721.				DECLINAT	ION.	
Time.	10h.	11h.	12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18 ^h .	19 ^h .	20 ^h .
м. s.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div		Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
0 0	101.6	128.4	126.4	107.4	113.4	111.3		107.0	106.9	108.4	109.8
5 0	102.2	119.6	121.6 115.4	107.5	113.8	111.2 113.3		109.3	106.2	109.2	109.8
10 0	102.4 102.4	114.5 112.6	112.4	111.4	$\frac{111.6}{112.4}$	112.3		107.9	106.7 107.5	109.4	109.8
$\begin{array}{ccc} 15 & 0 \\ 20 & 0 \end{array}$	102 4	$\frac{112}{125.4}$	110.8	113.3	113.4	110.3		106.2	107.3	110.0	109.6
$\begin{array}{ccc} 20 & 0 \\ 25 & 0 \end{array}$	103.0	$\frac{125 \cdot 4}{125 \cdot 2}$	110.3	116.6	113.9	107.1	102.8	106.4	108.4	110.0	109.8
$\frac{25}{30} = 0$	103.0	123.2	109.2	128.8	112.3	106.0		107.4	108.6	110.0	110.0
35 0	104.2	$\frac{123}{123} \cdot 0$	108.2	127.8	111.6	106.6		109.4	108.0	110.0	109.5
40 0	103.6	134.8	108.4	124.2	113.2	107.3		108.9	108.4	110.5	109.1
45 0	108.4	136.8	108.6	120.8	113.4	107.4		107.6	109.2	110.5	109.6
$\begin{array}{ccc} 10 & 0 \\ 50 & 0 \end{array}$	116.0	134.6	108.4	117.4	110.8	105.3		107.4	109.0	110.0	110.5
55 0	124.5	132.6	109.9	114.2	111.4	107.0		107.8	109.0	110.0	110.4
	One Se	ale Divisior	· = .0000	087 parts of t	he H. F.	I		ı	Horizoni	AL FORCE	•
M. s.	007.4	C10.5	610:5	1 500 to 1	500.0		1 (01+1	604.0	£00.0	600.	FORM
$\begin{array}{ccc} 2 & 0 \\ 7 & 0 \end{array}$	607.4	640.5	619.5	596.8	599.0	590.9		604.2	598.0	600.5	597.1
7 0	610.5	645.4	611.0	595.3	601.6	592°2   594°1		606.1	598.2	600.0	597.9
12 0	613.2	631.5	614.0	591.8	600.2			605.2	598 <b>.</b> 9	600.0	598.1
17 0	618.6	631.5	607:0	595.0	600.4	595.0		602.7			598.5
$\begin{array}{ccc} 22 & 0 \\ 27 & 0 \end{array}$	621.5	626.8	$606.5 \\ 606.2$	593.7 581.8	599°1 598°1	596°2		598.4	599.0	600.0	597.0
$\begin{array}{ccc} 27 & 0 \\ 29 & 0 \end{array}$	620.0	631.0 623.5	603.5	$\frac{581.8}{598.2}$	596°5	596-8   597 <b>-</b> 6		596 <b>·</b> 9	599.0	599.0	598°0
$\begin{array}{ccc} 32 & 0 \\ 37 & 0 \end{array}$	615.8 619.7	$623.5 \\ 607.5$	600.3	$\frac{598 \cdot 2}{605 \cdot 1}$	593.0 596 5	$\frac{597.6}{597.2}$		597 <b>·</b> 2 598 <b>·</b> 0	599 <b>·</b> 2	598.8	598 9
$\begin{array}{ccc} 37 & 0 \\ 42 & 0 \end{array}$	618.2	613.0	598 <b>.</b> 4	606.0	594 <b>°</b> 0	$\begin{array}{c} 1.597.2 \\ 1.597.8 \end{array}$		598.9	$\frac{599.0}{598.9}$	598.5	598 2
$\begin{array}{ccc} 42 & 0 \\ 47 & 0 \end{array}$	618 2	621.7	598 4 597 4	607.1	594 0 594 0	599.0		599.0	598.9	599.0	597.8
52 0	607.5	$\frac{621}{617.8}$	597 <del>4</del> 597 5	610.2	591.3	596.2		597.5	598.5	597.5	599.0
57 0	617.6	617.1	596.3	604.3	590.3	596.8		597.0	598.4	599.3	999.0
Thermometer	59°-4	59°9	60°.6	61.4	62°1	62°5	62°5	62.0	62°0	61.0	6 <u>1</u> .2
	One Sea	ıle Division	= .0000	63 parts of th	ne V. F.	·			VERTICAL	Force.	1
M. S.	2011	200.5	10440	150.0	7.001.1	10515	1.2000	1	1	1.25.0	171.0
$\begin{array}{ccc} 3 & 0 \\ 0 & 0 \end{array}$	184.7	195.7	184.2	178.9	166.4	167.5		159.3	164.7	167.0	171.0
8 0	186.0	191.6	183.6	177.4	166.4	166.4		159.8	164.7	167.0	171.2
13 0	187.5 188.2	186°5 189°1	182.8	176.7 175.4	166 <b>.</b> 4	165°0		159°8	164.7	167.0 168.7	171.2
$\begin{array}{ccc} 18 & 0 \\ 23 & 0 \end{array}$	189.5	189.1	$184.7 \\ 184.7$	175.0	166.1	164.6			164.8	168.7	170°8
	189.5	187.2	184.7	173.0	166.7	165.4		160.6	164.8 164.8	168.7	170.8
$\begin{array}{ccc} 28 & 0 \\ 33 & 0 \end{array}$	188.9	184.1	182.1	$\begin{vmatrix} 173.2 \\ 172.7 \end{vmatrix}$	166.7	165 1	161.3	160.8	164.8	169.5	170.8
	191.7	184.1	182.2	171.3	167.2	164.1	161.3	160.8	165.0	169.8	170.8
$\begin{array}{ccc} 38 & 0 \\ 43 & 0 \end{array}$	191.8	185.7	181.5	169.6	167.0	164.1	161.3	160.8	165.0	169.8	170.8
48 0	192.0	186.4	181.5	168.7	167.0	163.7	161.3	160.8	165.0	170.2	170.8
53 0	192.8	185.2	181.5	168.2	167.0	163.9		164.9	165.3	170.2	170.8
58 <b>0</b>	197.8	185.2	179.8	166.2	167.0	164.6		164.9	165.6	170.5	170.8
				-							
Thermometer	58.2	58°·8	59°3	60.0	62°5	63.6	63.7	62.7	62.7	62.6	6 [°] 1.7
<b></b>							Increasing 1	Numbers de	note decreas	ing Westerly	y Declinati
	- A STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE S			TEOROLOG		BSERVA	ATIONS.				
Mean Göttingen	Barometer	Therm	iometers.		Wind.				Weather.		
Time.	at 32°.	Dry.	Wet.	Direction.	For	ce.					
D. Н. М.	In.										
21 10 0	29.478	65.0	0	W.S.W.	Lig	ht	Cloudy; circ	um eis ets	egt and ha-	Δ	
11 0	29.481	62.7		W.S.W.	Very 1		Cloudy; circ				
12 0	29.492	59.8	_	W.S.W.	Very	light.	Cloudy; circ		,		
13 0	29.509	58.2		w.s.w.	Very		Cloudy; circ				
14 0	29.510	60.2	_	W. by S.	Very	light.	Cloudy; circ				
15 0	29 522	59.7		N. by is.	Very		Cloudy; circ				
16 0	29.522	59.5		Ň.	Very		Cloudy; circ		•		nder and r
17 0	29.524	58.1		S.S.E.	Very		Cloudy; circ				
18 0	29.544	55.6		E.N.E.	Very		Cloudy; circ				
			1 1		Very						
19 0	29.542	52.0	· !	E.N.E.	Yery.	ngnt. t	Cioudy: circ	um., cir -str	at., and naze	e; ngnt thii	ider and i
19 0 20 0	29 542 29 540	53.8		E.N.E. N. by E.	Very		Cloudy; circ Cloudy; circ	um., cirstr um., cirstr	at., and haze	e; light thur e; light thur	ider and ra

^a At 22^d 10^h, Thermometer of H. F., 59° · 5; of V.F., 59° · 6.

				-	MAGNET	ICAL OI	BSERVATIO	NS.				April 21st	and 22nd.
		DECLINATI	ON.						Angular	Value	of one Scale	Division =	0.721.
21 ^h .	22h.	23 ^h .	Oh.	1 ^h .	2 ^h .	3h.	4 ^h .	$5^{ m h}$		6 ^h .	7 ^h .	8h.	9 ^h .
sc. Div. 109 '3 109 '5 110 '2 109 '6 109 '2 109 '6	sc. Div. 109 '6 110 '3 109 '6 108 '7 109 '2 108 '8 109 '2	Sc. Div. 110°0 111°2 112°5 112°6 112°6 112°6 112°2	Sc. Div. 112 ' 7 113 ' 2 113 ' 4 113 ' 6 113 ' 8 113 ' 7	Sc. Div. 113 · 2 113 · 2 114 · 0 114 · 4 114 · 8 115 · 2	Sc. Div. 113 '9 113 '6 112 '5 109 '8 109 '7 110 '4	Sc. Div. 110 ' 5 109 ' 6 110 ' 4 110 ' 7 111 ' 0	110°2 109°5 109°4 109°0 110°3 108°6	sc, 1 107 107 107 108 108 108	4   10 0   10 2   10 8   10 0   10	c. Div. 03.7 03.9 03.0 03.4 03.3 02.6	Sc. Div. 100 '6 100 '0 100 '4 99 '5 99 '6 100 '6 100 '5	Sc. Div. 106*5 107*4 106*4 105*4 105*3 104*0	Sc. Div. 102 ' 4 102 ' 0 102 ' 0 102 ' 0 102 ' 3 102 ' 5 102 ' 2
108.6 108.4 109.5 109.3 109.7	109 2 110 0 110 4 110 3 110 4	112 2 112 0 112 2 112 7 112 6 113 4	113.7 112.8 113.6 113.9 114.4 114.6	115 · 4 114 · 6 114 · 4 115 · 0 115 · 4 114 · 8	110°4 110°6 110°4 110°0 110°8 110°5	114.2 113.4 112.5 111.0 110.8 110.6	108*3 108*4 107*3 106*8 105*8 106*9	107 106 105 105 105 104	6 10 0 10 6 10 4 10	02.1 02.4 02.0 01.0 00.4 01.4	100 3 100 4 99 4 98 8 97 4 104 4	104 0 103 8 103 2 102 6 102 4	102 2 102 2 102 8 102 2 103 2 103 0
		Horizonta	L Force.		I	nc <b>r</b> ease, ir	Scale Division	ous, cor	respondin	g to 1°	decrease of	Temperatur	re, 1 °63.
599.0 599.5 600.0 600.0 600.0 600.9 600.0 600.5 601.0 600.2 600.2	599.0   600.5   599.0   597.2   598.0   598.2   598.2   598.3   598.4   601.4   601.3	601 · 2 601 · 8 602 · 2 602 · 0 602 · 2 602 · 3 601 · 8 601 · 6 601 · 4 602 · 8 602 · 6 602 · 0	600.7 600.0 599.3 598.0 598.0 598.6 600.0 599.2 598.2 598.4 598.0 598.2	598:0 598:4 597:8 596:0 596:0 594:7 594:0 593:2 592:3 590:1 588:2 587:8	584.0 583.8 584.2 585.0 585.3 585.4 585.0 583.2 583.2 583.2 584.8 584.7	585.6 584.6 585.0 586.1 585.9 585.1 584.7 584.0 581.8 579.0	582.8 579.0 581.2 578.0 576.2 579.0 576.1 580.0 578.5 577.0 576.0 578.0	575° 576° 574° 574° 577° 576° 576° 576° 577° 581°	$\begin{array}{c cccc} 2 & 58 \\ 0 & 58 \\ 6 & 58 \\ 0 & 58 \\ 0 & 58 \\ 0 & 58 \\ 4 & 58 \\ 58 & 58 \\ 5 & 59 \end{array}$	86°2 86°9 86°0 88°0 8°0 66°5 66°8 66°5 7°0 8°0 41°0	587.0 588.5 589.0 590.0 592.2 593.5 590.3 590.2 584.4 583.0 590.2	602.0 610.0 604.0 601.5 601.0 600.0 606.0 604.7 603.0 604.2 603.0	604.0 603.8 603.0 603.4 602.0 601.6 601.6 601.0 602.0 600.7 598.0 598.3
6°1.5	61°5	61.6	6η5	61°5	61.0	60°.8	60°5	60°.	4 6		60.0	59.2	5°°5 °
		VERTICAL	Force.		In	ncrease, in	Scale Divisio	ns, corr	esponding	g to 1°	decrease of	Temperature	e, 1°64.
170 ° 0 170 ° 0 170 ° 3 170 ° 6 170 ° 6 170 ° 6 170 ° 6 170 ° 4 170 ° 4 170 ° 5 171 ° 2	170.4 170.4 170.4 170.6 171.0 171.0 170.4 169.9 170.1 170.1	170°3 170°7 171°2 171°3 171°3 171°5 171°1 171°1 171°1 171°1 171°1 170°6	170.6 170.6 170.2 169.7 169.8 169.7 170.4 170.3 169.8 169.8 169.8	170.6 170.5 169.8 170.3 170.3 170.8 171.1 171.1 171.8 172.0 171.6 171.9	171°0 171°0 171°2 171°8 171°8 171°8 171°8 171°8 171°9 172°9 173°0 172°8	172.8   172.8   172.8   172.6   172.9   172.6   172.6   173.4   173.2   173.0   172.6	173°3 173°3 173°5 173°5 173°5 173°9 174°6 175°3 175°5 175°5	175° 175° 175° 175° 175° 175° 175° 178° 178° 178°	$egin{array}{cccccccccccccccccccccccccccccccccccc$	9.2 9.2 9.0 8.6 9.2 9.2 9.2 9.2 9.2 9.5 9.5	178°6 179°1 179°1 179°1 180°0 180°0 180°0 179°7 179°8 181°6 184°5	186'9 186'0 184'2 183'3 183'3 182'5 182'1 181'5 180'9 180'6 180'5 179'6	179°6 179°6 179°6 179°7 179°5 179°5 179°5 179°4 178°7 178°5 178°5
6Î:7	61°7	61.8	6°1.7	6η7	61.0	60.6	60°4	60°.	3 6	°.0	60°0	60.0	59.6 °
and increa	sing Horizo	ntal and Ver	ical Force.										
		1		ME	reorolo		OBSERVAT	IONS.					
Mean Gö Tin	öttingen ne.	Barometer at 32°.	There	mometers. Wet.	- Direc		Vind. Force.				Weat	her.	
	2 0 3 0 0 0 1 0 2 0 3 0 4 0 5 0 6 0 7 0	In. 29 · 534 29 · 542 29 · 574 29 · 592 29 · 603 29 · 632 29 · 641 29 · 653 29 · 667 29 · 684 29 · 684	54·4 52·2 49·3 49·9 52·4 51·2 49·3 47·9 46·9 45·5	0	E.S. S.I. S.I. S.I. N.E. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. N. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S. I. S.	E. E. by N. [. y E. I.E. I.E.	Very lig Very lig Very lig Very lig Very lig Very lig Very lig Very lig Very lig Light. Light.	ht. ht. ht. ht. ht. ht. ht. ht. ht. ht.	Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Cloudy	; circ; cirs; cirs; cirs; cirs; cirs; cirs; cirs; cirs; cirs; cirs; cirs	eum., cirstr trat., cir., an trat., cir., an trat., cir., an trat., cir., an strat., cir., an strat., cir., an trat., cir., an trat., cir., an	at., and haze at., and haze d circum.; d circum.; d circum.; d circum.; d circum.; d circum.; d circum.;	rain. rain. rain. rain. rain. rain. rain. rain. ; rain. rain. ; rain.

	th.			MAGNE	TIONII OB		JNO.				
Mean Göttingen	Angu	ılar Value o	f one Scale	Division =	0'`721.				Declinat	ION.	
Time.	10h.	11h.	12h.	13h.	14h.	15h.	16 ^h .	17h.	18h.	19h.	201
м. s.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Di
0 0	105.9	108.0	111.9	112.2	113.4	115.4	111.2	111.4	111.4	124.0	81.8
5 0	106.1	108.1	112.7	112.9	114.4	119.9	108.6	111.2	111.0	123.6	80.2
10 0	106.1	108.6	114.6	113.1	115.2	122.6	109.8	110.8	111.7	122.5	81.5
15 0	105.5	108.4	113.4	116.9	115.0	127.2	112.2	110.6	112.2	123.2	88.4
20 0	105.9	108.4	112.9	117.8	115.6	126.9	115.2	111'4	112.4	126.5	100.0
25 0	105.9	108.4	112.7	115.8	114.9	126.4	115.7	112.0	114.5	129.8	104.4
30 0	105.6	108.4	110.4	115.6	114.4	125.0	115.2	111.2	114.5	132 4	108.5
35 <b>0</b>	106.1	108.9	112.1	115.4	113.2	114.6	114.2	111.0	113.0	134.8	108.8
40 0	106.3	108.4	114.0	114.2	113.4	112.3	113.8	112.3	115.0	129.9	114.4
<b>45</b> 0	106.9	109.4	113.0	113.4	112.0	112.9	113.4	112.8	115.0	109.6	112.5
50  0	107.4	110.5	110.0	112.9	111.9	113.3	112.4	112.4	115.4	97.6	108.5
55 0	107.5	110.4	108.4	112.9	113.0	112.6	111.6	112.4	117.2	82.4	108.4
	ll One !	Scale Division	- :0000	187	0 A) XI IS	1	1	1	Hopigova	ral Force	
M. S.	II	1	· · · · · · · · · · · · · · · · · · ·		1		ī	1	1	1	
2  0	608.0	608.2	612.2	611.2	604.0	601.0	604.2	611.0	616.0	602.0	553.5
7 0	608.0	607.2	613.0	614.4	604.0	597.0	598.4	614.6	612.4	604.2	537.8
12 0	608.6	608.0	613.0	608.0	604.0	597.0	596.0	625.4	612.6	604.3	529.0
17 0	608.0	609.0	613.0	611.0	604.2	598.0	593.2	620.0	606.2	623.0	535.7
22  0	607.5	610.0	614.0	613.8	604.2	600.0	596.2	622.2	606.6	626.0	551 6
$\frac{-2}{27}$ 0	606.2	607.5	614.2	613.7	603.2	602.5	601.4	623.2	609.2	625.2	562.7
$\frac{21}{32}$ 0	606.0	608.2	614.0	613.1	603.0	605.0	603.5	623.4	609.4	620.3	575.5
$\begin{array}{ccc} 32 & 0 \\ 37 & 0 \end{array}$	606.0	609.0	614.2	611.8	604.1	601.0	603.8	616.2	603.0	608.8	587.3
42 0	604.8	607.2	617.0	611.0	604.0	598.5	617.0	616.8	602.2	597.5	592.8
47 0	606.0	607.0	620.0	611.0	603.0	603.0	604.0	614.5	602.6	563.4	592.0
$\begin{array}{ccc} 52 & 0 \end{array}$	608.0	608.0	620.0	607.0	601.0	602.6	605.2	614.8	594.6	557.6	590.8
57 O	608.2	608.2	616.0	605.0	598.0	604.0	605.4	616.6	590.2	549.2	588.7
					<u> </u>		<u> </u>	ļ		ļ	
Thermometer	65°6	66.0	66°4	66.4	66.2	66.2	66°.0	65.8	65.6	65.4	65.4
M. S.	One S	Scale Divisio	n = .0000	63 parts of	the V. F.				VERTICAL	Force.	
	100:4	100.5	150.4	10110	1 10010	101.0	1,50.0	1 , , , , ,	1.50.5	141:0	00.6
3 0	168.4	169.5	170.4	164'6	162.3	161.8	150.2	161.1	159.7	141.2	98.8
8 0	168.4	169.5	170.4	164.2	162.6	161.8	151.4	161.5	159.7	134.1	96.4
13 0	168.6	169.5	170.2	164.2	162.6	159.6	154.2	160.9	159.1	134.1	98.5
18 0	168.6	169.7	170.5	163.9	162.6	157.4	157.7	159.5	159.3	133.9	104.5
23  0	168.5	169.7	170.2	163.9	162.6	155.2	158.8	159.6	156.7	133.9	112.2
28 0	168.2	169.7	170.6	163.9	161.8	153.2	161.7	159.4	157.0	131.5	116.2
33 O	168.5	169.7	170.6	163.5	161.8	149.0	161.8	159.4	157.4	129.7	115.2
38 0	168.6	169.7	167.4	161.9	161.8	149.1	164.2	158.4	155.0	124.9	115.3
43 0	168.6	169.7	167.3	162.0	161.8	149.1	160.7	158.8	152.7	121.2	121'7
48 0	169.3	169.7	167.1	162.3	161.8	150.0	160.4	159.5	152.9	108.2	123.5
53 0	169.3	169.7	167.1	162.3	161.8	150.0	161.1	159.8	152.8	104.5	128.0
58 0	169.3	169.7	164.9	162.3	161.8				153.1	102.4	130.0
	1000		)			150.4	160.2 - 1	159.8		1	
			0	0			160.2			0	
Thermometer	63.7	64°3	64.2	64·5	66°5	66°5	$\frac{160.2}{6\mathring{6}.7}$	66.7	66·7	66°7	66.3
Thermomet <b>e</b> r			64.2	6 ⁴ ·5		66°·5	6 ⁶ ·7	66°7	66·7	66°7	
Thermometer						66°5	66.7	66°7	66·7		
	63.7	64°3			66.2	66°5	66.7	66°7	66.7	ing Westerly	
Thermometer  Mean Göttingen Time.		64°3	ME		GICAL OI	66°5	66.7	66°7	66·7	ing Westerly	
Mean Göttingen Time.	Baromete at 32°.	r Ther	ME mometers.	TEOROLO	GICAL OI	66°5	66.7	66°7	66.7	ing Westerly	
Mean Göttingen Time. D. н. м.	Barometer at 32°.	r Ther Dry.	ME mometers.	Direct	GICAL OI Wind tion.	66°5  SSERVAT	66.7 Increasing N	66°7	66°7	ing Westerly	Declination
Mean Göttingen Time. D. н. м. 28 10 0	Baromete at 32°.  In. 29°632	r Ther Dry.	ME mometers.  Wet.	Direct E.S.	GICAL OI Wind tion.	66°5  BSERVATI  Force.	66.7  Increasing N  IONS.	66°7 Numbers der	66°7  note decreasi  Weather	ing Westerly	Declination
Mean Göttingen Time.  D. H. M. 28 10 0 11 0	Barometer at 32°.  In. 29 °632 29 °624	r Ther Dry. 67.8 66.9	ME mometers.   Wet.   60°2 61°0	Direct E.S.	GICAL OI Wind tion.  E. Ve	66°5  BSERVATI  Force.  ery light. Calm.	66.7  Increasing N  IONS.  Partially Partially	66°7  Numbers der	Weather ith cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir.,	rstrat., and c	Declination
Mean Göttingen Time.  D. H. M. 28 10 0 11 0 12 0	Barometer at 32°.  In. 29°632 29°624 29°624	r Ther Dry. 67.8 66.9 66.9	ME mometers.    Wet.   60°2   61°0   61°0	Direct E.S. E.S.	GICAL OI  Wind tion.  E. Ve	66°5  BSERVATI  Force.  ery light. Calm. ery light.	66.7  Increasing N  IONS.  Partially Partially Partially Partially	66°7  Numbers der  7 clouded, we clouded, we clouded, we	Weather the cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir.,	rstrat., and costrat., and costrat., and costrat., and costrat., and costrat., and costrat.	Declination
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Mean Göttingen Time.  D. H. M. 28 10 0 11 0 12 0 13 0 14 0 15 0	Baromete at 32°. In. 29 · 632 29 · 624 29 · 638 29 · 654 29 · 664	r Ther Dry. 66.9 66.9 63.1 60.3 64.1	ME mometers.    Wet.   60°2   61°0   61°0   57°2	Direct E.S. E.S. E.S.	GICAL OI  Wind  tion.  E. Ve E. Ve E. Ve E. Ve E. Ve E. Ve	66°5  BSERVATION  Force.  Calm.  cry light.  cry light.  cry light.  cry light.	66°7  Increasing N ONS.  Partially Partially Partially Partially Cloudy,	y clouded, we clouded, we clouded, we clouded, we clouded, we clouded, we with cir., ci	Weather the cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir.,	rstrat., and c -strat., and c -strat., and c -strat., and c	Declination
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Mean Göttingen Time.  D. H. M. 28 10 0 11 0 12 0 13 0 14 0 15 0	Baromete at 32°. In. 29 · 632 29 · 624 29 · 638 29 · 654 29 · 664	r Ther Dry. 667'8 666'9 63'1 60'3 64'1 63'7	ME mometers.    Wet.   0 60.2 61.0 61.0 57.2 56.5 57.3 57.6	Direct E.S. E.S. E.S. N.F. N.N. N.N.	GICAL OI  Wind  tion.  E. Ve  E. Ve  C. Ve  E. Ve  E. Ve  E. Ve  E. Ve	66°5  BSERVATION  Force.  Every light.  Every light.  Every light.  Every light.  Every light.  Every light.	Partially Partially Partially Partially Cloudy, Cloudy, Cloudy,	y clouded, we clouded, we clouded, we clouded, we clouded, we with cir., ci with cir., ci with cir., ci	Weather the cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir.,	rstrat., and c -strat., and c	Declination
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Mean Göttingen Time.  D. H. M. 28 10 0 11 0 12 0 13 0 14 0 15 0 16 0 17 0 18 0	Baromete: at 32°.  In. 29 '632 29 '624 29 '624 29 '638 29 '664 29 '682 29 '688	64.3  Ther Dry. 67.8 66.9 66.9 63.1 60.3 64.1 63.7 62.7 61.1 60.9	ME mometers.    Wet.   0 60.2 61.0 61.0 57.2 56.5 57.3 57.6 56.3 56.1 56.1	E.S. E.S. E.S. N.N. N.N. N. by E. by E. by	GICAL OI  Wind  tion.  E. Ve  E. Ve  C. Ve  E. Ve  Ve  N. N.	Force.  Force.  Pry light.  Calm.  Pry light.  Pry light.  Pry light.  Pry light.  Light.  Light.  Light.  Light.  Light.	Partially Partially Partially Partially Ploudy, Cloudy,  7 clouded, we clouded, we clouded, we clouded, we with cir., ci with cir., ci with cir., ci with cir., ci with cir., ci with cir., ci with cir., ci with cir., ci	Weather the cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., cir., strat., and rstrat., and	rstrat., and co-strat.,  Declination		
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 $^{^{\}texttt{a}}$  At 29  $^{\texttt{d}}$  10  $^{\texttt{h}},$  Thermometer of H. F., 65  $^{\circ}$  · 9 ; of V. F., 65  $^{\circ}$  · 3.

					MAGNET	ICAL (	OBSERVAT	ions.			May 28th	and 29th.
		DECLINATI	ON.					Ang	ular Value	of one Scale	Division =	0''721.
21h.	22h.	23h.	Oh.	1 ^h .	2 ^h .	3h.	4 ^h .	5h.	6 ^h .	7 ^h .	8h.	9h.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. D			Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
110.6	115.4	125.5	124.7	121.9	122.2	119			102.8	103.0	104.8	106.0
113.7	113.4	124.7	124.4	121.8	123.0	119.			103.0	101.8	105.4	105.9
117.2	111.2	124.0	125.0	121.7	121.6	119	2 105.9		102.7	102.6	105.4	106.2
121.4	119.4	123.6	124.4	121.4	123.1	118.			101.6	102.6	105.2	106.3
127.5	124.8	123.4	125.5	121.0	122.0	116.			101.4	103.5	104.6	106.4
129.2	132.4	127.5	124.4	121.0	123.6	113.			101.5	101.4	105.5	106.2
130.4	133.3	129.4	125.3	121.9	123.8	114		103'4	101.8	102.4	106.4	106.2
134.8	133.5	130.8	126.8	122.4	122.4	117	2 104.4	103.8	102.5	102.6	105.9	106.3
137.5	132.1	130.3	122.6	123.6	121.5	115	6   104 4	103.7	101.8	103.6	106.0	106.4
138.8	129.7	127.7	123.8	122.7	121.5	114	4   104.9	103.2	101.5	104.2	105.6	106.2
130.4	127.4	128.3	124.2	123.4	119.0	109			102.8	104.0	106.0	105.6
121.2	126.6	126.6	122.3	123.6	118.6	107			102.6	105.2	106.4	106.0
	!	Horizonta	L Force.	***	<u>'                                     </u>	ncrease,	in Scale Div	isions, corresp	onding to 1	decrease of	Temperatui	re, 1.63.
· ·		1 1		<b>500.0</b>					1		1	1
583.7	576.5	604'1	599.8	593.9	592.0	570			608.4	605.8	612.4	597.8
583.5	577.6	603.0	600.9	597.0	591.8	566			608.8	604.2	604.2	599.2
585.5	587.1	599.6	602.1	598.0	591.9	562			608:2	604.8	603.5	601.0
588.4	593.8	599.6	604.4	598.2	590.0	559			605.6	606.0	600.2	598.7
584.8	593.1	596.6	601.0	598.8	587.0	557			605.8	603.2	601.0	599.0
581.0	596.2	595.1	602.0	599.0	585.4	559			608.0	595.8	598.2	599.1
577.5	594.7	594.2	602.0	598.8	585.0	557			608.8	598.3	599.0	600.3
563.7	596.0	591.0	606.8	599.0	581.9	551			609.2	601.0	599.2	599.6
560.8	597.2	591.0	601.1	597.2	581.0	556	0   592°5	606.0	608.0	603.3	600.1	600.5
566.5	600.8	591.1	600.9	597.0	578.2	558	5   594°5	605.3	607.8	602.6	601.0	601.0
575.0	600.1	594.0	594.4	594.0	577.8	559			604.8	604.0	601.0	601.9
576.4	603.2	599.9	592.9	593.4	575.8	564		608.8	605.0	604.5	600.8	604.2
65°2	65.0	64.5	64°5	64.1	63.6	64.	0 64.5	65.3	65.3	65.4	65.2	65.6 a
	l	VERTICAL	1			1	1	isions, corresp	onding to 1	decrease of	Temperatu	re 1.64.
		VERTICAL	TORCE.			merease,	III Beale Div	Isions, corresp	· · · ·		· · · · · · · · · · · · · · · · · · ·	
130.0	132.0	151.8	162.6	165.7	164.4	161	0   163.5	164.4	161.9	162.3	163.5	162.1
129.9	134.5	153.0	163.3	166.5	164.4	161			162.0	162.3	162.6	163.2
129.2	139.8	153.2	164.1	166.3	164.3	161			161.3	162.7	162.3	163.8
121.0	137.2	154.0	163.7	166.3	164.5	160			161.4	162.2	162.9	162.5
117.8	137.6	154.0	163.6	166.3	163.8	161			161.1	162.3	162.6	163.6
116.2			163.2	166.3	163.8	161			161.2	161.9	162.7	163.6
114.7	143.3	154.0		165.9		161			161.2	162.3	162.4	162.9
	145.4	154.6	163.5		163.8				162.3	162.6	162.4	162.9
109.6	148.7	154.6	164.7	165.9	163.8	160			162.2	163.0	163.5	163.6
109.6	151.8	155.7	164.2	165.9	163.0	161					163.0	163.8
115.7	155.1	156.6	164.8	165.9	163.0	163			162.3	163.3		
116.5	154.0	158.8	164.6	165.3	163.0	163			162.3	162.7	162.3	163.4
121.9	151.0	161.9	165.2	165.3	161.9	163	5   164.9	162.8	162.2	162.7	162.3	163.4
65.7	65°5	<b>64</b> .9	64°5	64.2	63.4	63.	8 64.5	64.7	64.8	64.7	64.8	65°1 a
and increa	sing Horizo	ontal and Ver	rtical Force.							-		
					TEOROLO	GICAL	OBSERVA	ATIONS.	<del></del>			
		1	The	rmometers.	i	Wine	d.					
Mean G	öttingen me.	Baromete at 32°.	Dry.	Wet.	Direc		Force.			Weather.		
		II			_	-						
28 2	и. м. 3 О	29.613	56°6	54.6	N.E. b	v E.	Light.	Cloudy, with	cir., cirstr	at., and cir	cum.	
	0 0	29.591		54.1			Light.	Cloudy, with	circum., c	irstrat., and	l haze; shov	wery.
	1 0	29.584		52.3			Calm.	Cloudy, with	ci <mark>rcum.,</mark> cir	rstrat., and	haze; thunde	er and lightni
	$egin{array}{cccc} 1 & 0 & \ 2 & 0 & \end{array}$	29.580		53.1		.	Calm.	Cloudy, with	circum., c	irstrat., and	l haze.	
		H	i	58.4	1	E	Very light.	Cloudy, with	circum.,			ınder and lig
	3 0	29.548	i	- 1	1	i	•	ining; show	very.	in etrat and	l haze	
	4 0	29.524		56.4			Very light.					
	5 0	29.210		56.9		.E.   \	Very light.	Cloudy, with				
	~ ~	29.521		55.3	_	-	Calm.	Cloudy, with	cırcum., c	irstrat., and	i naze.	mand Hala.
		29 521				- 1 -	7 1: 1.4	Cloudy with	cırcum cii	rstrat and	naze: tnunde	er and lightni
		29.583		55.8	N.E. b	у Е. [ \	Very light.	Oldudy, "Till			d bozo 41	ndom and 1:-
	6 0 7 0	29.583	58.3	1	1	• 1	Very light.	Cloudy, with	h cir-cum., c	cirstrat., an	d haze; thu	nder and lig
	6 0		58°3	58.3	N.E. b	• 1	-	Cloudy, with ning; sho Cloudy, with ning; sho	h cir-cum., o wery. h cir-cum., o	cirstrat., an	d haze; thu	nder and lig

Mean Gittlepon	June 23rd and 24	l _{th} .			MAGNE	FICAL	OBSERVAT	IONS.				
Time		Angula	r Value of	one Scale D	ivision = 0	··721.	· · · · · · · · · · · · · · · · · · ·	The Manager of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Co	~	DECLINA	TION.	
0 0 0 105:5 106:9 109:4 109:3 109:4 109:3 109:4 109:0 108:0 108:6 108:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:6 109:8 109:8 109:6 109:8 109:8 109:6 109:8 109:8 109:6 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8 109:8					1	1	15 ^h .	16 ^h .	17 ^h .	·	1	20h.
15	0 0	105.2	106.9 107.6	109.4	109.3	109	4   109.0 4   108.4	108.0	108.6	108.8	109.4	110.0
25	<b>15</b> 0	105.4	107.8	109.3	110.0	109	4 108.6	108.3	108.6	108.8	109.6	108.8
40	25 0 30 0	105°2 106°2	108°3 108°7	109 <b>.</b> 3	109.6	109	$\begin{bmatrix} 6 & 108.4 \\ 3 & 108.2 \end{bmatrix}$	108.4	108.6 108.6	108.8	109.6 109.5	108.8 109.4
M.   S.	40 <b>0</b> 45 0 50 0	106.1 106.4 106.4	109 <b>.2</b> 109 <b>.3</b>	109°4 109°1	109.6	109. 109.	4   108°2 0   108°2 2   108°0	108.7	108.6	109°2 109°2 109°4	110.0 110.0 110.0	109.4 109.4 110.0
2 0 604-1 606-1 604-0 604-0 603-1 603-2 602-0 601-5 601-5 601-5 601-0 602-4 12 0 604-0 607-4 604-1 603-9 603-0 602-3 601-5 601-5 601-0 601-0 602-4 604-0 603-0 603-0 602-0 601-5 601-0 601-0 602-4 604-0 603-0 603-2 602-0 601-5 601-0 601-0 602-2 602-0 601-0 603-5 601-0 601-0 602-2 602-0 601-0 603-5 601-0 601-0 602-2 602-0 601-0 603-5 601-0 601-0 602-2 602-0 601-0 603-5 601-0 601-0 602-2 602-0 601-0 603-5 601-0 601-0 602-2 602-0 601-0 603-5 601-0 601-0 602-2 602-0 601-0 603-5 601-0 601-0 602-2 602-0 601-0 603-5 601-0 602-2 602-0 601-0 603-5 601-0 602-2 602-0 602-0 602-0 601-5 601-0 602-2 602-0 602-0 602-0 601-5 601-0 602-2 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 602-0 60		 	1	!	<u> </u>	1		108 8	108 0	!	<u>!</u>	<u> </u>
7 0 604·0 606·0 604·1 603·9 603·0 602·3 601·5 601·5 601·5 601·0 601·0 602·6 17 0 606·0 602·6 602·0 602·0 601·5 601·0 601·0 601·0 602·8 17 0 606·0 602·0 602·0 601·5 601·0 601·0 601·0 602·8 17 0 606·0 600·0 601·0 602·0 602·0 601·0 601·5 601·0 601·0 602·0 602·0 601·0 601·0 602·0 602·0 601·0 601·0 602·0 602·0 601·0 601·0 602·0 602·0 601·0 601·0 602·0 602·0 601·0 601·0 602·0 602·0 601·0 601·0 602·0 602·0 601·0 601·0 602·0 602·0 601·0 601·0 602·0 601·0 602·0 602·0 601·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·0 602·	· ·	604.1	606.1	604.0	604.0	603	5 602'0	602.0	601.2	601.2	600.0	601.8
22	$\begin{array}{ccc} 7 & 0 \\ 12 & 0 \end{array}$	604.0	607.4	604.0	604.0	603.0	0 602.0	602.0	601.5	601.0	601.0	602.4 602.8
37	$\begin{array}{cc}22&0\\27&0\end{array}$	604°3	607°1 608°0	603.7 604.0	604°0 604°1	603	602.2	601.0 601.2	601.5	600.8	600.8	602.0
Second Color	$\begin{array}{ccc} 37 & 0 \\ 42 & 0 \end{array}$	606.3	605 <b>.</b> 4 603 <b>.</b> 7	604.5 604.1	603.0 603.0	602.6	601.6	601.8	601.5	600.2	600.8	602.4 602.5
M.   S.   One Scale Division = '000063 parts of the V.F.   VERTICAL FORCE.	<b>52 0</b>	606.8	603.1	604.3	603.9	602	601.2	601.2	601.5	600.0	601.0	602.8
No.	Thermometer	69°6	69°8	70°0	69.9	69°-	4 69°3	69°0	68.6	68.2	67.6	6 ⁷ ·1
8 0	M. S.	One S	cale Division	u = .0000	063 parts of	the V. I	r.		-	VERTICAL	Force.	
13												
23	13 0	155.5	154'3	153'1	153.2	151.8	148.5	147.6	151.0	152.2	153.2	154.6
28	$\begin{array}{ccc} 18 & 0 \\ 23 & 0 \end{array}$	,										
38												
Hean Göttingen Time.   Barometer at 32°.   Thermometers.   Dry.   Wet.   Direction.   Force.   Weather.												
Thermometer	43 0	154.4	153'6	153.5		151.0	148.3	149.3	151.4	152.7	153.3	
Thermometer												
Mean Göttingen   Barometer   at 32°.   Dry.   Wet.   Direction.   Force.   Weather.												
Mean Göttingen Time.   Barometer at 32°.   Thermometers.   Direction.   Direction.   Force.   Weather.	Thermometer	68.3	68.2	68.7	68.6	68°·6	70.0	70.0	69.4	68.2	68.0	67:3
Mean Göttingen Time.         Barometer at 32°.         Thermometers.         Wind.         Weather.           D. H. M.         In.         °         °           23 10 0         29.722         70.7         64.1         S.W. by S.         Very light.         Clear.           11 0         29.723         67.6         62.1         S.W. by S.         Very light.         Clear.           12 0         29.722         67.5         62.2         S.W.         Very light.         Clear.           13 0         29.736         64.4         60.0         S.W.         Very light.         Clear.           14 0         29.753         61.1         58.3         —         Calm.         Clear.           15 0         29.753         59.1         57.1         —         Calm.         Clear.           16 0         29.765         58.3         56.4         —         Calm.         Clear.           17 0         29.777         58.1         56.3         —         Calm.         Clear.           18 0         29.776         55.8         53.7         —         Calm.         Clear.           19 0         29.776         55.8         52.9         —         Calm.				ME.	TEOROLO	GICAL	OBSERVAT		Numbers dei	note decreas	ing Westerly	Declination,
Dry.   Direction.   Force.   Weather.	11		Thom		1				1			
23 10 0				<del></del>	Direct	ion.		ce.	_	w	eather.	
11 0       29 '723       67 '6       62 '1       S.W. by S.       Very light.       Clear.         12 0       29 '722       67 '5       62 '2       S.W.       Very light.       Clear.         13 0       29 '736       64 '4       60 '0       S.W.       Very light.       Clear.         14 0       29 '753       61 '1       58 '3       —       Calm.       Clear.         15 0       29 '753       59 '1       57 '1       —       Calm.       Clear.         16 0       29 '765       58 '3       56 '4       —       Calm.       Clear.         17 0       29 '777       58 '1       56 '3       —       Calm.       Clear.         18 0       29 '775       55 '8       53 '7       —       Calm.       Clear.         19 0       29 '776       55 '8       52 '9       —       Calm.       Clear.         20 0       29 '789       53 '2       51 '2       N.W. by N.       Very light.       Clear.	11		i	4	C 1117 1	0	<b>17</b>	liah+	(C)			
12 0       29 ° 722       67 ° 5       62 ° 2       S.W.       Very light.       Clear.         13 0       29 ° 736       64 ° 4       60 ° 0       S.W.       Very light.       Clear.         14 0       29 ° 753       61 ° 1       58 ° 3       —       Calm.       Clear.         15 0       29 ° 753       59 ° 1       57 ° 1       —       Calm.       Clear.         16 0       29 ° 765       58 ° 3       56 ° 4       —       Calm.       Clear.         17 0       29 ° 777       58 ° 1       56 ° 3       —       Calm.       Clear.         18 0       29 ° 775       55 ° 8       53 ° 7       —       Calm.       Clear.         19 0       29 ° 776       55 ° 8       52 ° 9       —       Calm.       Clear.         20 0       29 ° 789       53 ° 2       51 ° 2       N.W. by N.       Very light.       Clear.	11											
14 0     29 '733     61 '1     58 '3     —     Calm.     Clear.       15 0     29 '753     59 '1     57 '1     —     Calm.     Clear.       16 0     29 '765     58 '3     56 '4     —     Calm.     Clear.       17 0     29 '777     58 '1     56 '3     —     Calm.     Clear.       18 0     29 '775     55 '8     53 '7     —     Calm.     Clear.       19 0     29 '776     55 '8     52 '9     —     Calm.     Clear.       20 0     29 '789     53 '2     51 '2     N.W. by N.     Very light.     Clear.	12 0	29.722	67.5	62.2	S.V	ν.	Very	light.	Clear.			
15 0					S.V	٧.	Very Cel	ngnt. m.	1			
16 0     29 '765   58 '3   56 '4   —     —     Calm. Calm. Calm.     Clear. Clear.       17 0     29 '777   58 '1   56 '3   —     —     Calm. Calm.     Clear. Clear.       18 0     29 '775   55 '8   53 '7   —     —     Calm. Calm.     Clear.       19 0     29 '776   55 '8   52 '9   —     —     Calm. Calm.     Clear.       20 0     29 '789   53 '2   51 '2   N.W. by N.     Very light.     Clear. Clear.						.	Cal	lm.	Clear.			
18 0   29 · 775   55 · 8   53 · 7   — Calm. Clear. 19 0   29 · 776   55 · 8   52 · 9   — Calm. Clear. 20 0   29 · 789   53 · 2   51 · 2   N.W. by N. Very light. Clear.	16 0	29.765	58.3	56.4	-	.			1			
19 0 29 776 55 8 52 9 — Calm. Very light. Clear. Clear.						: l						
20 0   29.789   53.2   51.2   N.W. by N.   Very light.   Clear.	19 0	29 776	55.8	52.9		.	Cal	m.	Clear.			
21 0   29 (93   52 0   50 ±     Comm.   Clear.	20 0	29.789			N.W. 1	y N.						
	21 0	29 793	02 8	30 4	_		Cal	mi.	Clear.			

^a At 24^d 10^h, Thermometer of H. F., 71° '6; of V. F., 70° '3.

						MAGNET	ICAL O	BSERVATIO	NS.			June 23rd	and 24th.
			DECLINATI	on.					Ang	gular Value	of one Scale	Division =	0′.721.
2	1 ^h .	22h.	23h.	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6h.	7h.	8h.	9 ^h .
110 110 110 110 110	0.0	Sc. Div. 110'4 110'8 110'8 111'2 111'2 111'2	Sc. Div. 112 · 3 112 · 4 112 · 6 113 · 3 113 · 4 113 · 8	Sc. Div. 115.5 115.9 116.2 116.3 116.4 116.4	Sc. Div. 117 '4 117 '0 118 '2 118 '4 118 '4 118 '4	Sc. Div. 117.8 117.4 117.5 117.5 117.4 117.4	Sc. Div 115 6 115 4 115 4 115 1 115 1 114 6	5   111.4 111.3 1   110.9 1   110.0 1   109.7	sc. Div. 106 '4 106 '2 105 '6 105 '4 105 '0 104 '5	sc. Div. 102 ' 5 102 ' 5 102 ' 2 102 ' 4 102 ' 4 102 ' 2	sc. Div. 102 ' 4 102 ' 5 102 ' 9 102 ' 9 102 ' 9 103 ' 2	Sc. Div. 103 '4 103 '4 103 '4 103 '6 103 '2 103 '8	Sc. Div. 105 '4 105 '6 105 '8 106 '0 105 '8 105 '8
	).0 ).0	111.4   111.4   111.7   112.0   111.8   111.7	114.2 114.6 114.5 114.6 115.2 115.4	116.5 116.8 116.8 117.2 117.3 117.4	118.0 118.2 118.4 118.2 118.0 118.0	117.4 116.8 116.6 116.4 116.3 116.2	114.4 113.5 113.5 112.4 112.3 111.7	5   109·2 108·4 1   108·2 107·5	104.4 104.0 103.4 103.3 103.0	102°2 102°2 102°2 102°2 102°4	103 · 2 103 · 4 103 · 4 103 · 4 103 · 2 103 · 4	104.0 104.2 104.8 105.2 105.4 105.4	106.0 106.4 106.6 106.8 107.0 107.4
		· · · · · · · · · · · · · · · · · · ·	HORIZONTA		i		Increase, i	in Scale Divisi	ons, correspo	onding to 1°	decrease of	Temperatui	1
604 605 604 603 604 604 605 605	03.4         606.0         609.5         612.8         610.0           04.2         606.2         610.1         613.0         609.5           05.0         606.4         611.1         613.0         609.5           04.4         606.8         611.2         613.5         608.5           03.8         607.4         611.1         613.0         608.5           04.5         607.6         611.6         613.1         607.5           04.8         607.2         611.2         612.2         607.5           04.8         607.3         612.0         611.8         607.5           05.0         607.4         612.1         611.3         606.5           05.8         607.9         612.1         610.7         606.5           05.8         608.1         612.1         610.7         605.5					604.6 604.0 604.0 603.0 603.0 601.8 601.0 601.2 600.2 600.0 600.0 598.9	598.0 598.0 597.4 596.6 596.0 594.5 594.1 593.8 593.5 593.5 593.5	593.0 593.0 593.0 593.0 593.0 593.0 593.0 593.0 593.0 593.0 593.0	593.5 593.5 593.0 593.0 593.8 594.8 593.8 593.5 593.1 593.0 593.5 594.0	595.0 595.7 596.0 597.2 598.0 598.3 599.0 599.2 599.8 600.0 601.0 601.9	602.0 602.8 603.0 604.2 604.2 605.0 604.2 607.8 606.2 607.0 607.4 608.0	607.8 608.2 609.8 610.8 610.4 610.2 610.8 611.2 611.4 613.0 613.2	613.8 613.5 614.4 615.2 613.5 614.0 614.2 614.2 614.5 614.2 614.8
66°	8 608.1 612.1 610.7 60			66.1	67.2	67°9	68.2	69°2	69°4	70.0	70°·3	7 [°] 1·1ª	
			VERTICAL 1	Force.	<del>-</del>	I	ncrease, i	in Scale Divisi	ons, correspo	onding to 1°	decrease of	Temperatu	re 1.64.
155 154 154 154 154 154 154 154 155 155	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		158 · 9 158 · 9 158 · 9 158 · 9 158 · 9 158 · 9 158 · 9 158 · 9 158 · 9 158 · 9 158 · 7 158 · 4	158'3 158'3 157'5 157'5 157'4 157'4 157'4 157'4 157'4 157'4 157'5	156·3 156·3 156·2 156·2 156·2 156·2 156·2 156·2 156·2 155·9 155·6	155.6 155.6 155.6 155.7 155.1 155.1 155.1 154.9 154.9 154.9	154.6 154.6 154.6 154.6 153.9 153.9 153.9 153.1	152·3 151·9 151·6 151·8 151·3 151·3 151·3 151·3 151·3 151·3 151·3	151.8 151.8 151.8 151.8 151.5 151.3 151.3 150.8 150.8 150.8	150°3 150°0 150°0 150°0 150°0 149°1 149°1 150°0 149°8 149°6	149.6 149.6 149.9 149.9 149.9 149.4 149.4 151.1 150.2 150.2 150.7	150.5 150.5 149.9 150.6 150.1 150.1 150.1 150.1 150.1 150.1 150.1	
67	.0	66°7	66.1	65°5	65°7	66.3	66.6	67°5	68.2	68°5	68°7	69°3	70°0°
and i	ncreas	ing Horizon	otal and Verti	ical Force.									
	<del></del>	II.	<u> </u>	ſ		TEOROLO	GICAL	OBSERVAT	IONS.	<del></del>			
Me	an Gö Tim	ttingen e.	Barometer at 32°	Dry.	wet.	Direc	etion.	Wind.	ce.	-	w	eather.	
25	23		In. 29.809 29.824 29.862 29.869 29.862 29.849 29.844 29.831 29.827 29.817 29.804	51·4 51·4 57·4 64·1 66·7 69·1 71·7 72·7 72·3 72·3 73·4 73·7	60.6 60.6 60.6 60.6 60.6 60.6 60.6 60.6 60.6 60.6 60.6	S.V S.V S.V S.W. S.W.	W. W. W. W. by S. by S.	Cal Cal Cal Cal Nearly Very l Very l Very l Very l Very l Very l	m. m. m. calm. ight. ight. ight. ight. ight.	Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear.			

July 21st and 22	nd.			MAGNET	ICAL OBS	ERVATIO	NS.				
Mean Göttingen	Ang	ular Value o	of one Scale	division =	= 0' .721.				DECLINAT	10N.	
Time.	10 ^h .	11 ^h .	12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18h.	19 ^h .	20 ^h .
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
0 0	106.8	110.3	111.8	110.0	108.4	108.0	108.9	110.4	127.6	117.6	116.4
5 0	106.8	110.4	111.9	109.7	108.4	108.0	109.0	111.4	127.4	116.4	116.5
10 0	107.2	110.6	111.4	109.4	108.2	108.4	108.6	114.0	124 2	115.7	115.4
15 0	107.4	110.8	111.4	109.4	107.6	107.9	109.4	119.2	120.4	114.4	115.8
20 0	107.4	110.8	111.1	109.4	107.7	108.0	110.0	123.4	116.4	114.5	115.4
25  0	107.8	111.4	110.6	109.4	108.0	108.0	109.6	127.7	114.4	113.4	114.0
30 0	108.2	110.9	110.5	109.2	108.2	108.4	109.8	130.0	113.6	113.4	113.2
35 0	108.6	110.5	110.4	109.4	109.0	108.6	109.6	128.4	113.6	113.2	112.8
40 0	109.2	111.0	110.4	109.2	109.6	108.4	109.6	128.4	115.4	112.6	111.6
45 0	109.5	111.2	110.4	108.4	109.7	108.9	109.9	130.2	117.4	112.4	112.2
50 0	109.8	111.3	110.4	108.6	108.4	108.9	110.0	127.6	118.4	112.4	112.6
55 O	110.1	111.4	110.4	108.6	108.2	109.0	110.3	127.0	118.4	114.5	112.8
_	One	Scale Divis	ion = '00	0087 parts	of the H. I	?.		1	Horizon	ral Force	•
M. S.	593.8	593.2	589.7		1		504.5	507:0	586.2	585.0	594.0
$\frac{2}{7}$ 0	592.0	$\begin{bmatrix} 593.2 \\ 593.9 \end{bmatrix}$	589 7 589 5	583.0	587.5	590.8	594.5	597.0	589.0	585 1	595.2
7 0				584.0	587.6	590.4	588.5				
12 0	592.0	593.2	588.0	584.2	587.0	590.2	588.0	600.0	591.0	585.0	592.8
17 0	592.0	593.6	586.0	583.2	587.0	591.0	592.0	595.8	592.0	584.2	588.8
22 0	591.9	593.8	584.0	583.0	588.0	591.0	594.0	598.0	587.0	585.0	587.6
27 0	593.5	595.0	585.0	583.0	589.0	590.8	597.0	597.0	584.0	585.4	590.2
32 0	594.2	593 2	586.0	582.8	589.5	591.0	597.8	594.0	578.0	586.0	588.2
37 O	596.1	593.0	$583^{\circ}2$	586.0	589.0	589.8	598.5	586.5	577.5	587.5	587.2
42 0	596.4	592.2	583.0	585.8	593.0	589.4	599.0	583.0	577.5	588.2	586.2
47 0	596.4	591.8	582.4	586.5	593.2	591.0	598.0	581.5	579.0	588.4	586.0
52  0	596.6	589.0	584.6	587.0	593.4	591.4	597:0	582.0	581.5	588.0	585.8
57 O	595.0	589'1	584.1	587.2	592.1	591.0	597.0	583.0	584.0	592.0	584.2
Thermometer	79.7	79°2	79°0	78°5	78°0	77.5	77.4	77°3	76.9	76°6	76°4
d	One	Scale Divis	ion = '00	0063 parts	of the V. H	`.			VERTICAL	Force.	<u>,                                      </u>
M. S.		10510	104.0		1	1	1	1	1	1,,,,,	300.5
3 0	134.6	135.0	134.2	134.4	134.4	133.3	132.5	133.7	120.9	128.1	129.5
8 0	134.6	134.5	134.4	134.4	133.7	133.3	132.2	132.7	120.6	128.1	129.5
13 0	134.3	134.2	134.4	134.4	133.7	133.3	132.2	130.4	119.3	128'1	128.6
18 0	134.3	134.5	134.4	134.4	133.7	133.3	132.5	129.0	119.3	129.2	128.6
23 0	134.3	134.6	134.4	134.4	133.7	133.3	133.1	129.0	119.3	129.2	128.7
28 0	134.9	134.6	134.4	134.4	134.0	133.3	133.7	126.7	120.4	129.5	129.5
<b>3</b> 3 <b>0</b>	134.9	134.6	134.4	134.4	134.0	133.2	133.7	124.8	122.8	129.5	129.5
38 0	135.4	134.6	134.4	134.4	134.2	133.5	133.7	123.6	124.3	129.7	130.7
43 0	135.4	134.6	134.4	134.6	133 4	133.5	133.7	123.6	125.6	129.7	131.0
48 0	135.4	134.6	134.4	134.6	133 4	132.5	133.7	125.3	127.8	130.1	131.0
53 0	135.4	134.0	134.4	134.6	133.4	132.2	133.7	124.4	128.1	130.1	131.0
<b>5</b> 8 0	135.0	134.4	134.4	134.6	133.3	132.2	133.7	122.1	128.1	130.1	131.4
	<b> </b>		<del></del>		ļ		<u> </u>			<del></del>	
Thermometer	78.4	78.4	78.0	77.7	78.0	78.1	77.9	78.0	78.0	77.5	7 ³ ·3
								numbers de	note decreas	ing Westerly	Declination
	li .			TEOROLO		BSERVAT	rions.				
Mean Göttingen Time.	Baromete at 32°.	Dry.	Wet.	Direct	Wind.	Force.			Weather		
D. H. M.	In.	0	0		1						
21 10 0	29.406	80.3	72.8	S.W	7.	Light.	Cloudy, w	ith circum.	, and strat		
-1 10 0	29.426	78.2	72.0			Calm.			n circum. a	nd strat.	
11 0	29.419	75.1	69.6			Calm.			ı circum. a		
11 0 12 0	29 427	73.3	68.2			Calm.			ı circum. a		
11 0	29.422	70.9	66.8		i	Calm.		th circum.			
11 0 12 0	1 23 322		64.9		1	Calm.		th circum.			
11 0 12 0 13 0 14 0		1 00 3		1		Calm.		th circum.			
11 0 12 0 13 0 14 0 15 0	29·424 29·440		64.0				i cicuuy, wi		anu Still.		
11 0 12 0 13 0 14 0 15 0 16 0	29.424 29.440	67.7	64.9				Pantialler al	landed -: A		nd strat	
11 0 12 0 13 0 14 0 15 0 16 0 17 0	29.424 29.440 29.432	67.7 65.7	63.9			Calm.			ı circum. a		tning
11 0 12 0 13 0 14 0 15 0 16 0 17 0 18 0	29.424 29.440 29.432 29.432	67.7 65.7 67.3	63.9 64.5	=		Calm. Calm.	Cloudy, wi	th circum.	and strat.;	constant ligh	itning.
11 0 12 0 13 0 14 0 15 0 16 0 17 0 18 0 19 0	29.424 29.440 29.432 29.432 29.438	67.7 65.7 67.3 66.3	63.9 64.5 64.6			Calm. Calm. Calm.	Cloudy, wi	th circum. th circum.	and strat.; and strat.;	constant ligh constant ligh	tning.
11 0 12 0 13 0 14 0 15 0 16 0 17 0 18 0	29.424 29.440 29.432 29.432	67.7 65.7 67.3	63.9 64.5	=		Calm. Calm.	Cloudy, wir Cloudy, wir Cloudy, wir	th circum. th circum. th circum.	and strat.; and strat.; and strat.; and strat;	constant ligh	ntning. ntning.

^a At 22^d 10^h, Thermometer of H. F., 79° 0; of V. F., 77° 7.

Process							MAGNE	FICAL (	OBSERVAT	IONS.			July 21st	and 22nd.
Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sect				DECLINATI	ON.					Ang	gular Value	of one Scal	e Division =	= 0' `721.
112*  110*  110*  113*  123*  123*  123*  110*  113*  110*  110*  10*  13*  10*  10*  10*  10*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*  110*		21h.	22 ^h .	23 ^h .	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8 ^h .	9 ^h .
1114   1107   11819   12376   12375   12375   12374   11679   11274   10772   10174   9770   10114   10475   11179   11179   11275   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375   12375		Sc. Div.			Sc. Div.		Sc. Div.							Sc. Div.
1116   110.77   118.44   125.75   123.75   123.74   115.44   112.33   105.74   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4   107.4														
111   111   117   117   123   118   119   117   124   117   124   114   114   110   103   101   103   101   103   101   103   101   103   101   103   101   103   101   103   101   103   101   103   101   103   103   101   103   103   101   103   103   101   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103   103														
1110							124.2							105.4
111   113   117   117   123   123   125   123   125   123   125   123   125   123   125   123   125   123   125   123   125   123   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125   125														
111'2   114'2   117'2   123'4   125'4   123'3   114'4   111'4   101'5   100'4   99'4   102'4   106'4   111'4   111'4   101'5   100'4   99'4   102'1   106'5   106'6   111'2   115'5   120'4   123'2   122'4   121'5   114'5   112'4   104'2   98'4   100'2   106'6   111'0   116'3   123'4   123'6   121'4   120'3   115'0   111'4   103'3   97'4   100'3   103'4   106'6   111'0   116'3   123'2   123'6   121'4   120'3   115'0   111'4   103'3   97'4   100'3   103'4   106'6   111'0   116'4   133'2   123'6   121'4   120'3   115'0   111'4   101'3   97'4   100'3   103'4   106'2   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   107'2   100'3   103'4   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   100'3   10			113.2	117.9	123.8	126.4	124.4						102.4	
111   11   11   11   11   10   10   1														
111   2														
111														
110											97:7			
10.0   117.9   123.5   124.6   122.3   119.9   114.5   110.4   101.6   97.4   100.8   101.7   107.4														
S84'2   585'8   589'0   592'1   592'0   583'4   589'0   591'8   590'0   588'5   589'0   595'8   598'8   584'0   586'2   590'9   592'1   589'8   586'0   591'3   590'0   588'5   589'0   595'8   690'0   588'6   591'2   596'2   601'4   582'0   588'1   588'1   592'9   590'8   588'5   593'0   590'0   588'0   590'0   588'7   590'0   588'1   588'1   592'9   590'8   588'0   592'0   591'3   587'0   591'0   593'2   597'2   591'4   582'0   588'1   588'1   592'9   590'8   588'0   592'0   591'3   587'0   591'0   593'2   597'2   591'4   583'3   588'3   592'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'0   593'		110.8	117.9	123.2		122.3				101.6	97.4	100.8		
584'0   586'2   590'9   592'1   589'8   586'0   591'5   591'1   590'0   589'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'				Horizonta	L Force.			Increase,	in Scale Divi	sion <b>s, cor</b> respo	onding to 1	° decrease o	f Temperatui	re, 1.63.
584'0   586'2   590'9   592'1   589'8   586'0   591'5   591'1   590'0   589'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'0   590'		584.2	585.8	589.0	592.1	592.0	583.4	589	591.8	590.0	589.5	589.0	595.8	598.8
5832   5866   59070   59370   5909   58578   59310   59070   59910   59570   59110   59370   59170   5912   5970   69014     58270   5881   5881   5929   5909   58570   5920   5970   5870   5867   5955   59510   59114   5978   5952     58314   5890   58870   5928   59114   5820   5870   5867   5857   5857   59114   5978   5954     5832   5990   5890   5890   5920   5774   58876   58678   5872   5930   5914   5978   5956     58412   5990   5890   5990   5920   5774   58876   58678   5872   5930   5960   59672   59814     58412   5990   5990   5929   59411   57678   58675   58575   59578   59672   59878     58412   5990   5990   5929   59411   57678   58575   58570   58575   59100     5848   5990   5918   59378   5850   57574   58678   58770   58675   59100     5847   5990   5918   5938   58570   58574   58670   58575   59100     5848   5990   5918   5938   58570   58574   58670   58575   59100     5847   5990   5918   5938   5850   58574   58675   58870   58670   58978     5848   5990   5918   5938   58570   58870   58870   58870   58870   58970     5848   5891   5918   5918   5918   5918     5851   58910   58370   5820   5820   5890   58870   58870   58870   58910     5857   58571   59270   5930   5820   58476   5890   58890   58870   58870     5851   58571   59270   59370   58870   58870   58870   58870   58870     5858   5871   59270   59370   58870   58870   58870   58870   58870     5851   58571   59270   59370   58870   58870   58870   58870     58520   58578   58571   59270   58870   58870   58870   58870     5851   58570   58750   58870   58870   58870   58870     5851   58570   58750   58870   58870   58870   58870     5851   58570   58750   58870   58870   58870     5851   58570   58750   58870   58870   58870     5851   58570   58750   58870   58870   58870     5851   58570   58750   58870   58870     5851   58570   58750   58870   58870     5851   58570   58750   58750   58870     5851   58570   58750   58870     5851   58570   58750   58750     5851   58570   58750     5851   58570   58750     585														
582   0   588   1   588   1   592   9   590   8   582   0   592   0   591   5   587   0   591   5   591   5   591   5   591   5   591   5   591   5   5   5   5   5   5   5   5   5		583.2		590.0		590.9		593.0	590.0			591.2		
583'   589'   589'   592'   588'   592'   592'   573'   589'   586'   586'   586'   586'   586'   595'   595'   596'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'   586'		582.0		588.1		590.8								
583   2   590   0   598   0   599   4   592   0   577   4   588   6   586   587   2   593   0   593   596   596   600   0     585   5   590   0   590   0   593   0   593   0   593   576   0   587   585   585   587   585   596   0   596   0   596   597     584   8   590   0   590   0   592   0   573   587   585   587   585   596   0   596   0   599   597     584   8   590   0   590   0   592   0   578   8   587   585   587   585   596   0   596   0   599   8   597     585   589   0   593   0   591   8   595   0   585   587   585   587   0   586   0   590   0   593   8   590   595     585   587   1   592   0   593   0   582   0   579   0   588   587   0   585   587   0   593   8   590   2   596     585   587   1   592   0   593   0   582   0   579   0   588   0   587   587   587   587   587   0     585   585   587   1   592   0   583   0   582   0   584   0   585   0   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587   587		583.4		588.0		591.4	582.0			586.7				
S85'   5   590'   590'   590'   593'   592'   573'   2   588'   586'   588'   590'   590'   590'   590'   590'   590'   593'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'   590'		583.2		588.0		592.0		588.6			593.0			
584'8   590'0   590'0   590'0   590'0   590'0   590'0   590'1   595'8   587'5   585'0   587'5   580'0   590'0   590'0   590'8   595'8   585'8   589'0   591'8   593'8   586'8   587'0   586'8   587'0   586'0   590'0   593'8   596'4   595'4   588'8   587'0   586'0   580'0   593'8   596'4   595'4   588'8   587'1   590'0   593'8   590'2   593'8   590'2   595'8   585'8   587'1   592'0   593'0   582'0   578'0   588'7   587'5   590'0   593'8   590'2   596'8   585'8   587'1   592'0   593'0   582'0   588'7   587'5   590'0   594'8   600'0   594'6		585.5	590.0	590.0	593.0	592.0	573.2	588.9	586.5	588.8	590.8			598.4
585'8   589'0   593'8   596'0   575'4   586'8   587'0   586'5   590'0   593'8   596'4   595'6   585'8   587'1   592'0   593'0   582'0   584'6   589'0   589'0   585'5   590'0   594'8   600'0   594'6     76'3   76'0   76'0   76'2   76'6   76'8   76'6   77'2   77'5   78'0   78'0   78'5   78'8	İ	584.2	590.1	589.3	593.0	593.9	576.0	587.8	585.0	587.5	591.0	594.0		
S85   S87   S87   S97   S92   S92   S92   S92   S82   S85   S85   S85   S85   S90   S85   S90   S95   S90   S95   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S90   S94   S96   S94   S96   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95   S95			590.0		592.9		575.8			586.0	590.0	594.0	598.8	596.8
SS-8   SS7-1   S92.0   S93.0   S82.0   S84.6   S89.0   S89.0   S85.5   S90.0   S94.8   G00.0   S94.6		585.8	589.9	591.8	593.8	586.0	$575 \cdot 4$	586.8	3   587.0	586.0	589.0	593.8	596.4	595.4
Vertical Force   Increase, in Scale Divisions, corresponding to \$1^2\$ decrease of Temperature, \$1^* 64\$.				593.0	591.2	582.0	579.0	588.9	588.7	587.5	590.0	593.8	599.2	
Vertical Force   Increase, in Scale Divisions, corresponding to 1° decrease of Temperature, 1°64.		585.8	587.1	592.0	593.0	582.0	584.6	589.0	) 589.0	585.2	590.0	594.8	600.0	594.6
132   134   135   135   135   135   135   135   135   135   134   136   138   136   138   137   137   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135   135		76°3	76°0	76°0	76°2	76°6	76°8	76.0	5 7 [°] 7°2	77.5	78.0	78.0	78°·5	78°8ª
132'9   134'8   135'6   133'5   135'3   134'8   136'4   138'8   137'8   135'9   134'2   135'7   134'7   132'9   134'1   135'6   135'2   135'3   134'8   136'4   138'4   138'8   137'8   135'7   134'2   135'4   134'7   134'2   135'4   135'3   134'6   136'4   138'9   137'8   135'7   134'2   135'4   134'3   134'5   134'6   133'9   135'4   135'3   134'6   136'4   138'0   137'0   135'7   134'2   135'4   135'3   134'6   136'4   138'0   137'0   135'7   134'2   135'4   136'2   134'5   136'7   133'9   135'4   135'3   134'4   136'9   138'0   136'5   135'0   134'2   135'4   136'2   135'6   133'9   135'0   135'1   134'4   136'9   138'0   136'5   135'0   134'2   135'4   136'0   135'9   136'6   133'9   135'0   135'1   135'2   137'1   138'0   135'7   135'0   134'2   135'4   136'0   135'9   136'6   133'9   135'5   134'6   135'2   137'7   138'0   135'7   135'0   134'1   134'7   136'0   135'9   136'6   133'9   135'3   134'6   135'2   137'7   138'0   135'9   135'0   134'1   134'7   136'0   135'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'2   135'3   134'7   135'6   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'9   135'0   135'9   135'0   134'1   134'7   135'6   134'8   135'9   135'0   135'9   135'0   135'9   135'0   135'1   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'				VERTICAL	Force.		1	ncrease,	in Scale Divi	sions <b>, corr</b> espo	onding to 1°	decrease of	Temperatur	e, 1 64.
132'9   134'8   135'6   133'5   135'3   134'8   136'4   138'8   137'8   135'9   134'2   135'7   134'7   132'9   134'1   135'6   135'2   135'3   134'8   136'4   138'4   138'8   137'8   135'7   134'2   135'4   134'7   134'2   135'4   135'3   134'6   136'4   138'9   137'8   135'7   134'2   135'4   134'3   134'5   134'6   133'9   135'4   135'3   134'6   136'4   138'0   137'0   135'7   134'2   135'4   135'3   134'6   136'4   138'0   137'0   135'7   134'2   135'4   136'2   134'5   136'7   133'9   135'4   135'3   134'4   136'9   138'0   136'5   135'0   134'2   135'4   136'2   135'6   133'9   135'0   135'1   134'4   136'9   138'0   136'5   135'0   134'2   135'4   136'0   135'9   136'6   133'9   135'0   135'1   135'2   137'1   138'0   135'7   135'0   134'2   135'4   136'0   135'9   136'6   133'9   135'5   134'6   135'2   137'7   138'0   135'9   135'0   134'1   134'7   136'0   135'9   137'6   133'9   135'3   134'6   135'2   137'7   138'0   135'9   135'0   134'1   134'7   136'0   135'9   135'6   133'5   134'6   135'2   137'7   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'6   133'5   134'6   136'4   138'5   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'6   133'5   134'6   136'4   138'5   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'6   133'5   134'6   136'4   138'5   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'6   133'5   134'6   136'4   138'5   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'6   133'5   136'6   133'5   136'6   133'5   134'6   136'4   138'5   138'0   135'9   135'0   134'2   135'3   134'7   135'6   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'2   135'3   134'7   135'6   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'2   135'3   134'7   135'6   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'2   135'3   134'7   135'6   134'8   135'0   135'1   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'4   135'	1	132.6	134.8	135.6	133.2	135.3	134.8	136.4	138.7	137.8	135.9	134.2	135.1	134.7
132.9	- 1													
134+2   134+6   135+5   135+4   135+3   134+6   136+4   138+9   137+8   135+7   134+2   135+4   135+3   134+6   136+4   138+0   137+0   135+7   134+2   135+4   135+0   134+5   134+6   133+9   135+4   135+3   134+6   136+4   138+0   136+5   135+7   134+2   135+4   136+2   135+5   136+7   133+9   136+0   135+1   134+4   136+9   138+0   136+5   135+7   134+2   135+4   136+2   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+6   135+														
134+5   134+6   133+9   135+4   135+3   134+6   136+4   138+0   137+0   135+7   134+2   135+4   135+0   134+5   136+7   133+9   136+0   135+1   134+4   136+9   138+0   136+5   135+0   134+2   135+4   136+2   135+6   135+6   135+7   133+9   135+0   135+1   134+4   136+9   138+0   136+5   135+0   134+2   135+4   136+2   135+6   133+9   135+0   135+1   134+4   136+9   138+0   136+5   135+0   134+2   135+4   136+0   135+9   135+6   133+9   135+0   134+6   135+2   137+7   138+0   135+7   135+0   134+2   135+4   136+0   135+9   137+6   133+9   135+5   134+6   135+2   137+7   138+0   135+7   135+0   134+1   134+7   136+0   134+8   135+6   133+5   135+3   134+6   135+2   137+7   138+0   135+9   135+0   134+7   135+6   134+8   135+6   133+5   135+3   134+6   136+4   138+5   138+0   135+9   135+0   134+7   135+6   134+8   135+6   133+5   135+3   134+6   136+4   138+5   138+0   135+9   135+2   134+7   135+6   134+8   135+6   133+5   135+3   134+6   136+4   138+5   138+0   135+9   134+2   135+3   134+7   135+6   134+8   135+6   133+5   135+3   134+7   135+6   134+8   135+6   133+5   135+3   134+6   136+4   138+5   138+0   135+9   134+2   135+3   134+7   135+6   134+8   135+6   133+5   135+3   134+6   135+4   138+5   138+0   135+9   134+2   135+3   134+7   135+6   134+8   135+6   133+5   135+3   134+6   135+2   135+3   134+7   135+6   134+8   135+6   133+5   135+3   134+7   135+6   134+8   135+6   133+5   133+6   135+4   138+5   138+0   135+9   134+2   135+3   134+7   135+6   134+8   135+6   133+6   135+3   134+7   135+6   134+8   135+6   133+5   133+7   138+7   135+6   135+9   134+7   135+6   134+8   135+6   133+5   133+7   138+7   135+6   135+9   134+6   134+7   135+6   134+8   135+6   133+6   135+4   136+2   135+4   136+0   135+9   135+0   134+1   134+7   135+6   134+8   135+6   133+9   135+6   133+9   135+6   135+9   136+0   134+9   135+9   136+0   134+9   135+9   136+0   134+9   135+9   136+0   134+9   135+9   136+0   134+9   135+9   136+0   134+9   134+9   135+9   136+0   134+9   134+9   135+9   136+0   134+9   134+	- 1	134.2				135.3				137.8				
134 '5					135.4									
134 + 5	]			133.9	135.4			136.4	138.0					
135 6   135 78   133 19   135 70   135 11   134 14   136 69   138 70   135 70   135 14   136 70   135 79   135 6   133 9   135 70   134 16   135 12   137 71   138 70   135 77   135 70   134 12   135 14   136 70   135 79   136 6   133 19   135 75   134 6   135 12   137 77   138 70   135 79   136 70   134 17   136 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70   134 79   135 70			136.7						138.0					
135'9   135'6   133'9   135'0   135'1   135'2   137'7   138'0   135'7   135'0   134'1   134'7   136'0   135'9   136'6   133'9   135'0   134'6   135'2   137'7   138'0   135'7   135'0   134'1   134'7   136'0   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'1   134'7   135'6   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   135'0   134'2   135'3   134'7   135'6   134'8   135'6   133'5   135'3   134'6   136'4   138'5   138'0   135'9   134'2   135'3   134'7   135'6   134'8   135'3   134'7   135'6   138'0   135'9   134'2   135'3   134'7   135'6   134'8   135'3   134'7   135'6   138'0   135'9   134'2   135'3   134'7   135'6   134'8   135'3   134'7   135'6   136'4   136'4   138'5   138'0   135'9   134'2   135'3   134'7   135'6   134'8   135'3   134'7   135'6   136'4   135'9   135'0   134'2   135'3   134'7   135'6   134'8   135'3   134'7   135'6   136'4   135'9   135'0   134'2   135'3   134'7   135'6   136'4   135'9   135'0   134'2   135'3   134'7   135'6   134'8   135'0   134'2   135'3   134'7   135'6   136'4   135'9   135'0   134'2   135'3   134'7   135'6   136'4   135'9   135'0   134'2   135'3   134'7   135'6   134'8   135'0   134'6   134'7   135'6   134'6   134'7   135'6   134'8   135'0   134'2   135'3   134'7   135'6   136'0   135'9   135'0   134'1   134'7   135'6   135'0   134'1   134'7   135'6   135'0   134'1   134'7   135'6   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'0   135'	ı	135.6		133.9			134.4	136.9						
135   137   137   138   135   135   134   6   135   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136	- 1			133.9	135.0	135.1	135.2				135.0			
135   137   138   135   135   135   135   134   6   136   136   137   138   135   135   134   6   136   136   138   135   138   135   134   7   135   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136   136	- 1	135.9			135'0	134.6	135.2				135.0			
Thermometers   Wind.   Weather.   Weather.	ŀ	135.9	137.6	133.9	135.5	134.6	135.2	137.7	138.0	135.9	135.0	134.6		135.6
Mean Göttingen   Barometer at 32°.   Thermometers.   Direction.   Dry.   Wet.   Direction.   Force.		134.8	135.6	133.2	135.3	134.6	136.4	138.2	138.0	135.9	134.2	135.3		135.6
Mean Göttingen   Time.   Barometer   at 32°.   Dry.   Wet.   Direction.   Force.   Wind.   Weather.		76·7	76°4	76.6	76°7	76°5	76°5	76.2	76.3	76°5	76°7	77.2	77.3	77°4ª
Mean Göttingen   Barometer at 32°.   Dry.   Wet.   Direction.   Force.	İ	and increas	sing Horizo	ntal and Vert	ical Force.									
Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Dire						MET	reorolo	GICAL	OBSERVA	TIONS.				
Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Direction   Dire	1	15		_	Therm	nometers.			Wind.		1			
D. H. M. 21 22 0 29 469 68 7 66 0 — Calm. { Cloudy, with circum. and strat.; constant lightning; heavy rain. Cloudy, with circum. and strat.; constant lightning; heavy rain. Cloudy, with circum. and strat.; constant lightning; rain. Cloudy, with circum. and strat.; constant lightning; rain. Clear. Very light. Clear. Clear. 3 0 29 526 72 0 65 7 N.N.W. Very light. Clear. 3 0 29 572 72 9 64 0 N.N.W. Light. Clear. 4 0 29 576 74 7 64 1 N. Light. Clear. 5 0 29 594 75 7 64 1 N.N.W. Light. Clear. 6 0 29 599 77 8 65 8 N.W. Light. Clear. Clear. 7 0 29 610 78 2 67 4 N.W. Moderate with gusts. 8 0 29 608 79 3 65 1 N.W. Moderate. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear.	1						Direc	tion.		rce.	-	W	eather.	
21 22 0   29 469   68 7   66 0   —   Calm.   {   Cloudy, with circum. and strat.; constant lightning; heavy rain.   Cloudy, with circum. and strat.; constant lightning; heavy rain.   Cloudy, with circum. and strat.; constant lightning; rain.   Cloudy, with circum. and strat.; constant lightning; rain.   Cloudy, with circum. and strat.; constant lightning; rain.   Cloudy, with circum. and strat.; constant lightning; rain.   Cloudy, with circum. and strat.; constant lightning; rain.   Cloudy, with circum. and strat.; constant lightning; rain.   Cloudy, with circum. and strat.; constant lightning; rain.   Cloudy, with circum. and strat.; constant lightning; heavy rain.   Cloudy, with circum. and strat.; constant lightning; rain.   Cloar.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.   Clear.	1	р. н		In.		-	-		20		-			
22					1		-	-	Ca	lm. {				at.; constant
22         0         0         29.507         69.7         67.6         —         Calm.         Clear.           1         0         29.526         72.0         65.7         N. by W.         Very light.         Clear.           2         0         29.550         71.7         65.7         N.N.W.         Very light.         Clear.           3         0         29.572         72.9         64.0         N.N.W.         Light.         Clear.           4         0         29.576         74.7         64.1         N.N.W.         Light.         Clear.           5         0         29.594         75.7         64.1         N.N.W.         Light.         Clear.           6         0         29.599         77.8         65.8         N.W.         Light.         Clear.           7         0         29.610         78.2         67.4         N.W.         Moderate with gusts.         Clear.           8         0         29.608         79.3         65.1         N.W.         Moderate.         Clear.		28	23 0 29.495 68.5 66.8		66.8	_	-	Ca	lm. {			m. and stra	t.; constant	
1 0       29.526       72.0       65.7       N. by W.       Very light.       Clear.         2 0       29.550       71.7       65.7       N.N.W.       Very light.       Clear.         3 0       29.572       72.9       64.0       N.N.W.       Light.       Clear.         4 0       29.576       74.7       64.1       N.       Light.       Clear.         5 0       29.594       75.7       64.1       N.N.W.       Light.       Clear.         6 0       29.599       77.8       65.8       N.W.       Light.       Clear.         7 0       29.610       78.2       67.4       N.W.       Moderate with gusts.       Clear.         8 0       29.608       79.3       65.1       N.W.       Moderate.       Clear.	1	22 (	22 0 0 29.507 69.7 67.0				_	_	Ca	lm.	_	0,		i
2 0       29.550       71.7       65.7       N.N.W.       Very light.       Clear.         3 0       29.572       72.9       64.0       N.N.W.       Light.       Clear.         4 0       29.576       74.7       64.1       N.       Light.       Clear.         5 0       29.594       75.7       64.1       N.N.W.       Light.       Clear.         6 0       29.599       77.8       65.8       N.W.       Light.       Clear.         7 0       29.610       78.2       67.4       N.W.       Moderate with gusts.       Clear.         8 0       29.608       79.3       65.1       N.W.       Moderate.       Clear.		-	20 001 00 1				N. by	w.			1			j
3 0 29.572 72.9 64.0 N.N.W. Light. Clear. 4 0 29.576 74.7 64.1 N. Light. Clear. 5 0 29.594 75.7 64.1 N.N.W. Light. Clear. 6 0 29.599 77.8 65.8 N.W. Light. Clear. 7 0 29.610 78.2 67.4 N.W. Moderate with gusts. 8 0 29.608 79.3 65.1 N.W. Moderate. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear.	1										1			
4 0       29.576       74.7       64.1       N.       Light.       Clear.         5 0       29.594       75.7       64.1       N.N.W.       Light.       Clear.         6 0       29.599       77.8       65.8       N.W.       Light.       Clear.         7 0       29.610       78.2       67.4       N.W.       Moderate with gusts.       Clear.         8 0       29.608       79.3       65.1       N.W.       Moderate.       Clear.	1										1			ł
5 0 29.594 75.7 64.1 N.N.W. Light. Clear. 6 0 29.599 77.8 65.8 N.W. Light. Light. 7 0 29.610 78.2 67.4 N.W. Moderate with gusts. Clear. 8 0 29.608 79.3 65.1 N.W. Moderate. Clear.	1						N		$\overset{-1}{\text{Lig}}$	ht.				i
6 0 29.599 77.8 65.8 N.W. Light. Clear. 7 0 29.610 78.2 67.4 N.W. Moderate with gusts. Clear. 8 0 29.608 79.3 65.1 N.W. Moderate. Clear.				1		1			Lie	ht.	1			1
7 0 29.610 78.2 67.4 N.W. Moderate with gusts. Clear. 8 0 29.608 79.3 65.1 N.W. Moderate. Clear.						1								ı
8 0 29.608 79.3 65.1 N.W. Moderate. Clear.														j
		8	3 0								1			j
		9		29.605	78.9	65.3					Clear.			i

	i						<del></del>				
Mean Göttingen	Angul	ar Value of (	One Scale D	ivision = 0	7.721.		·	]	DECLINATI	on.	
Time.	10h.	11h.	12h.	13h.	14h.	15 ^h .	16h.	17h.	18h.	19հ․	20h.
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
0 0	107.5	108.9	110.4	107.9	109.5	117.4	111.6	109.4	108.4	110.4	111.2
5 0	107.9	109.6	110.4	108.4	109.4	116.2	110.2	109.4	108.4	110.4	109.3
10 0	108.4	110.1	110.4	109.3	109.4	115.9	110.3	110.4	108.8	110.4	106.4
15 0	109.2	110.2	110.4	109.4	109.8	115.8	110.4	109.8	108.8	110.3	103.4
20 0	108.9	110.3	110.3	109.6	110.4	117.4	109.2	108.8	108.6	109.9	104.3
25 0	108.9	110.4	110.3	109.4	109.8	118.4	109.2	109.4	109.6	109.6	106.4
30 0	108.8	110.4	110.4	109.4	110.5	118.3	109.6	109.4	109.5	110.5	108.3
35 0	109.0	110.5	110.0	109.0	110.4	116.4	109.6	109.4	108.8	110.6	110.4
40 0	108.9	110.5	108.9	109.4	110.6	113.0	109.6	109.6	110.0	111.0	111.6
45  0	108.9	110.1	108.2	109.4	113.7	111.4	109.6	109.4	110.4	111.4	114.4
50 0	109.5	110.5	107.9	109.5	118.4	111.4	109.5	109.0	111.4	112.0	116.2
<b>55</b> 0	109.0	110.4	107.9	109.2	117.8	111.4	109.6	108.4	111.4	111.8	117.4
	One S	cale Division	- :00008	37 parts of	the H. F.				Hopizova	TAL FORCE	
M. S.	One S		1		7	1	1	1	1	T	<u> </u>
2  0	615.0	617.0	599.0	599.0	603.0	598.5	587.2	600.0	601.6	600.0	598.0
7 0	612.0	615.0	598*2	598.5	601.2	596.0	583.1	598.8	601.8	601.2	596.0
12 0	611.0	615.0	597.2	604.0	602.0	594.0	589.2	599.6	602.2	601.0	594.0
17 0	610.2	615.0	598.0	606.0	600.2	589.5	590.8	601.8	602.2	601.7	593.9
22  0	609.2	614.2	601.0	608.0	598.0	587.0	591.8	602.8	600.0	600.0	596.9
27  0	609.2	611.0	600.0	607.0	596.0	587.5	592.8	602.4	602.0	599.0	598.1
32  0	610.0	609.8	602.0	605.0	595.0	587.0	595.8	602.8	600.8	600.0	598.4
37 0	609.8	608.5	601.5	603.0	593.9	584.0	595.0	601.2	599.4	600.0	600.0
42 - 0	611.4	608.4	600.0	603.8	593.0	582.0	596.0	599.8	600.0	600.0	600.2
47 0	611.0	605.0	600.0	603.0	593.0	583.0	597.8	600.2	599.8	599.0	600.0
52  0	613.0	602.0	600.0	602.9	598.0	584.0	598.8	600.5	600.8	599.0	598.0
57 0	614.5	299.0	299.0	603.0	599.0	584.2	599.8	601.2	600.6	599.1	594.0
Thermometer	70°·5	70°•4	70°7	71.0	7Î:0	70°5	70°2	7°00	69.4	69°0	68°5
	One S	Scale Division	n= '0000	63 parts of	the V. F.				VERTICAL	L FORCE.	
<b>M</b> . s.	ļ	1	1	1	1	<u> </u>	1	1	<del></del>	· · · · · · · · · · · · · · · · · · ·	<u> </u>
3  0	149'9	149.5	147.8	143.0	143.8	145.2	148.0	146.6	146.7	147.4	145.8
8 0	149.9	149.5	147.8	143.0	143.8	144.6	148.0	146.6	146.7	147.8	144.7
13 0	149.8	149.5	147.7	143.0	143.8	144.6	148.0	146.6	146.7	147.8	144.5
18 0	149.8	149.5	147.7	143.4	143.8	144.6	148.0	146.6	146.7	147.9	142.4
23 0	149.8	149.5	147.7	143.8	144.4	144.6	148.0	146.6	146.7	147.5	139.2
28 0	149.8	148'9	147.7	143.8	144'4	144.6	148.0	145.9	146.7	147.5	139.0
<b>3</b> 3 0	149.6	148.6	147.7	143.8	145.0	144.6	148.0	145.9	146.7	147.5	138.7
<b>3</b> 8 <b>0</b>	149.6	148.6	147.7	143.8	145.6	145.0	148.0	145.9	147.4	147.5	136.9
43 0	149.3	148.4	146.9	143.8	145.8	146.3	147.3	145.9	147.4	147'4	137:3
48 0	149.3	147.9	146.5	143.8	145.8	147.2	147.3	145.9	147.4	146.2	136.2
53 0	149.3	147.9	144.1	143.8	145.8	147.2	147.3	146.3	147.4	146.2	135.4
<b>5</b> 8 <b>0</b>	149.3	147.8	144.1	143.8	145.8	148.0	146.7	146.3	147.4	146.5	135.0
Thermometer	69.4	69°5	72.2	72.2	71.4	70°8	70°7	70°5	7ở· <b>o</b>	69°7	69°7
							Increasing	Numbers d	enote decrea	sing Westerl	y Declinati
			M	ETEOROL	OGICAL (	OBSERVA?	rions.				
M. Greet	1	The	rmometers.	<u> </u>	Wind.		Ī				
Mean Göttingen Time.	Baromet at 32°.	er	Wet.	Direct		Force.			Weather	•	
D. Н. М.	In.										
27 10 0	29.61	64.6	58.6	S.S.	$\mathbf{w}_{\cdot} \perp \mathbf{v}_{\cdot}$	ery light,	Nearly cle	ar, with cir	cum. and o	eirstrat	
11 0	29.61					ery light.			cum. and cir		
12 0	29.61					ery light.			-cum. and c		
13 0	29.61				-	Calm.			cum. and c		
14 0	29.62				-	Calm.			cum. and cir		
15 0	29.62				-	Calm.			um. and cir.		
16 0	29.62				.	Calm.			cum. and cir		
17 0	29.64				-	Calm.			cum, and cir		
18 0	29.65	- 1			- 1	Calm.	Clear, with	n light circ	cum. and cir	strat.	
19 0	29.64				.	Calm.	Clear, with	h light circ	cum. and cir	strat.	
20 0	29.64		47.8		-	Calm.	Clear, with	light circ	cum. and cir	strat.	
	29.650				_	Calm.			eum. and cir		
21 0	23 000	, , ., 0	1 10 0	1	- 1		, 01002, 1110	6			

*At 28^d 10^h, Thermometer of H. F., 71° · 0; of V. F., 70° · 2.

				Ŋ	MAGNET	ICAL OI	BSERVATIO	NS.		1	August 27th	and 28th.
		DECLINATI	ON.					Angı	ılar Value o	of One Scale	Division =	0'`721.
21 ^h .	22h.	23h.	Ob.	1 ^h .	2 ^h .	3h.	4h.	5h.	6 ^h .	7h.	8h.	9h.
sc. Div. 118' 4 119' 8 119' 9 118' 3 116' 4 115' 5 114' 7 112' 3 111' 3	Sc. Div. 115 '2 116 '4 116 '4 118 '0 118 '8 118 '4 118 '3 119 '5 119 '5	sc. Div. 119°3 119°2 117°8 117°2 117°0 116°4 116°0 114°4 115°1	Sc. Div. 118 * 5 118 * 5 118 * 7 120 * 4 120 * 6 121 * 2 123 * 2 124 * 4 124 * 4	126.0 126.0 126.6 127.0 127.0 126.4 126.6	Sc. Dv. 124 ' 6 124 ' 6 124 ' 5 124 ' 4 124 ' 9 122 ' 9 122 ' 9 122 ' 5 121 ' 7	sc. Div. 118'8 118'2 118'2 117'4 117'4 116'4 116'4 116'7 116'4	sc. Div. 111'4 110'2 107'8 106'6 105'4 105'4 106'2 106'4 105'5	Sc. Div. 104.6 103.8 103.0 102.4 101.6 100.5 100.0 99.6 99.4	Sc. Div.   95 * 4   94 * 2   95 * 4   95 * 4   95 * 2   95 * 4   95 * 4   95 * 4   95 * 4   95 * 4   95 * 4	sc. Div. 97 * 4 97 * 4 96 * 9 97 * 0 96 * 8 96 * 7 96 * 9 97 * 0 96 * 9 97 * 0	Sc. Div. 98.2 97.6 97.6 97.8 97.9 98.0 98.4 98.8 99.0	Sc. Div. 101 '4 102 '0 102 '8 103 '0 102 '8 104 '3 105 '0 105 '2 105 '5
111.6 111.4	119°2 118°6 118°7	115.5 116.4 116.2	124.4 124.9 125.4	125.4	120.6 119.6 119.2	114.8 113.6 112.4	105.6 105.6 104.7	99.4 99.0 97.8	96.4 97.3 98.4	97.2 97.8 97.3	100.3 100.0	105 '9 106 '4 106 '4
	·	Horizonta				!	n Scale Divisi	1	1	!	1	
590°0 587°0 587°8 584°2 583°6 582°0 585°0 585°0 585°0 589°0 587°9 591°1	87.0         595.0         599.0         596.8         594.2         593.5         596.8         593.5         593.5         596.8         593.5         596.8         593.5         596.8         593.5         596.8         593.5         596.8         593.5         596.8         593.5         596.8         592.0         598.0         592.0         592.0         598.0         592.0         593.0         598.2         593.0         593.0         592.5         592.5         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0         593.0					580.0 578.2 580.0 579.0 580.0 576.0 571.0 571.0 570.0 571.5 569.6	570.0 572.0 573.0 574.5 573.5 574.1 572.0 570.0 568.0 568.6 570.0 570.0	571.8 570.2 571.8 572.0 571.2 571.2 569.6 572.8 572.0 572.8 571.0 571.8	571 · 2 569 · 2 576 · 2 575 · 8 576 · 0 579 · 2 578 · 2 577 · 2 577 · 0 580 · 0 584 · 2 581 · 2	582°8 583°2 584°1 585°9 585°0 585°0 594°0 594°0 593°5 593°9 593°0 591°4	591.5 593.0 595.0 593.0 593.8 596.0 597.0 596.0 595.5 594.2 596.0 598.0	598.8 600.0 600.0 600.0 601.0 604.0 605.2 606.0 604.0 604.0 604.0
68.0	67.5	66.6	66.3	66.8	581°5 68°5	68.8	69.2	69°7	69.8	69°7	70.0	70°7 a
	-	VERTICAL ]	Force.		······	Increase, i	n Scale Divisi	ons, corresp	onding to 1	° decrease o	of Temperatu	re, 1.64.
135.0 135.0 135.0 135.0 135.8 135.8 137.2 136.1 136.1 136.1 134.2 134.2	134.0 134.5 134.5 134.2 134.2 134.2 134.0 134.0 134.0 133.9 133.9	133.5 133.5 133.5 133.7 133.7 133.7 133.7 136.6 136.6 136.6 138.3 139.0	140 · 1 140 · 2 140 · 2 141 · 1 141 · 5 145 · 1 146 · 2 146 · 4 146 · 4 148 · 3 148 · 3 148 · 8	148.8 148.9 148.9 148.9 148.9 148.9 148.7 148.7 148.7 148.7	148.5 148.5 148.5 148.5 148.5 148.6 148.6 148.6 148.6 148.6 148.6	148 2 148 2 148 2 148 2 148 2 147 1 146 6 146 2 146 2 146 2 146 2 145 9	145'9 146'4 146'8 146'8 146'6 146'6 146'0 146'7 145'7 145'7	145.7 145.7 145.7 145.7 146.6 146.3 146.3 146.3 146.3 146.3 146.3 146.3	148.6 147.7 147.7 148.1 148.1 149.3 148.7 148.7 148.0 148.0 149.0 148.2	148 · 2 148 · 2 148 · 2 148 · 2 148 · 2 148 · 2 148 · 2 148 · 3 149 · 4 149 · 4 149 · 5 149 · 5	149.1 149.7 149.7 149.7 149.7 149.7 149.7 149.7 149.7 149.0	149.0 149.0 149.0 149.0 149.0 149.0 149.0 149.0 149.5 149.5
70°·1	69°7	69°7	67°3	67°2	67.5	67.0	69·0	69.0	69.3	69°0	69°3	69°5 a
and increa	sing Horizo	ntal and Ver	tical Force.						A CONTRACTOR OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O			
		,		ME	TEOROL	OGICAL	OBSERVAT	ions.				
	öttingen me.	Barometer at 32°.	Therr	wet.	Dire	Win	d. Force.	_		Weathe	er.	
27 2 28	1. M. 2 0 3 0 0 0 1 0 2 0 3 0 4 0 5 0 6 0 7 0 8 0 9 0	In. 29.653 29.658 29.658 29.666 29.665 29.667 29.663 29.653 29.647 29.630 29.618	68.1 68.1 68.1 68.1	61 1 46 8 45 6 51 4 57 8 60 1 61 1 60 7 59 3 60 2 59 3			Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm. Calm.	Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear.				

September 22nd a	nd 23rd.			MAGNET	CICAL (	)BSERVATI	ONS.				
<b>M</b> ean Göttingen	Angul	ar Value o	f one Scale	Di <b>v</b> ision =	0'*721.	•			DECLINAT	ION.	
Time.	10 ^h .	11h.	12h.	13h.	14".	15h.	161	. 17h.	18h.	19h.	20h.
M. s. 0 0 0 10 0 15 0 0 20 0 25 0 30 0 35 0 40 0 45 0 55 0	112.6 113.2 113.4 113.4 113.6 113.6 113.8 114.2 114.2	Sc. Div. 113 '4 113 '4 113 '4 113 '4 113 '4 113 '4 112 '8 112 '6 112 '4 112 '4	Sc. Div. 112.8 112.5 112.6 112.4 112.4 112.8 112.8 112.8 112.8 112.8 112.6 112.4	Sc. Div. 112.4 112.4 112.7 112.5 112.5 112.5 113.4 112.2 111.4 111.1 111.4	Sc. Div. 111.5 111.5 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111.6 111	4     110.6       5     110.5       6     110.4       110.4     110.4       6     109.9       0     109.7       10     109.7       110.2     110.4	Sc. I   109'   108'   109'   109'   109'   110'   111'   106'   108'	14   110°1   110°0   110°2   111°5   111°5   112°6   4   113°0   4   113°8   115°4   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   116°2   110°0   110°0   110°0   110°0   110°0   110°0   110°0   110°0   110°0   110°2   111°5   110°0   110°0   110°2   110°0   110°2   110°0   110°2   110°0   110°2   110°0   110°2   110°0   110°2   110°0   110°2   110°0   110°2   110°0   110°2   110°0   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   110°2   1	Sc. Div. 114 '6 114 '3 113 '8 114 '4 114 '6 115 '4 115 '2 118 '4 119 '6 119 '5 120 '0	Sc. Div. 120°0 119°3 117°9 117°8 117°0 114°9 114°3 113°6 112°6 111°9 111°7 113°5	Sc. Div. 112:0 119:0 119:3 117:9 117:5 119:6 119:6 118:4 117:9 117:3 116:8 117:4
M. S.	One S	Scale Divisi	on = '000	0087 parts	of the H.	F.			Horizont	AL FORCE.	
2 0 7 0 12 0 17 0 22 0 27 0 32 0 37 0 42 0 47 0 52 0 57 0	7         0         606.8         613.8         613.6           12         0         607.0         613.0         614.0           17         0         609.2         613.8         614.2           22         0         611.2         615.0         613.2           32         0         612.2         616.5         613.3           37         0         612.6         616.0         613.3           42         0         612.8         616.2         613.3           47         0         612.8         616.2         613.3           47         0         612.8         617.8         612.3           57         0         615.0         617.0         610.0				608 : 610 : 6 610 : 6 610 : 6 610 : 6 610 : 6 610 : 6 611 : 6 612 : 6 613 : 1	0 613.6 2 614.0 2 614.1 0 615.7 1 616.4 4 616.7 0 616.0 5 617.0 0 617.0	616; 616; 616; 616; 616; 616; 616; 614; 613;	5   611.2 0   612.0 1   609.8 9   609.0 0   609.0 7   609.8 0   609.6 4   609.4 8   609.4 2   609.4	611.0 611.4 611.0 610.0 610.0 611.0 611.2 611.4 610.8 610.4 610.0	608.0 608.0 608.0 606.5 607.2 604.0 603.0 603.0 607.1 609.5 610.2 612.5	611.5 609.0 606.0 603.0 603.0 605.0 604.5 604.7 606.5 606.0 607.5
Thermometer	64.2	6 <b>4</b> .8	64.8	64.8	64.3	63.2	63°	0 62°·8	62.4	62° <b>2</b>	6j.8
M. s.  3 0 8 0 13 0 18 0 23 0 28 0 33 0 38 0 48 0 48 0 53 0	163°1 162°5 162°5 162°5 162°5 162°5 163°3 162°5 163°0	162.0 161.4 161.6 161.6 161.6 161.6 161.6 161.6 161.8 161.3 161.3	ion = '000  160'2 160'2 159'2 157'9 157'8 157'8 157'8 157'4 157'4 157'2 157'2	156°2 156°7 156°7 156°7 156°7 156°7 156°9 157°1 157°1 157°7 157°7	of the V.    157.8   157.8   157.7   157.7   157.7   157.7   157.7   157.7   158.5   158.4	158°1 158°1 158°0 157°5 157°5 157°7 157°7 157°7 157°7	157° 158° 158° 158° 158° 158° 158° 158° 158	9   157.5 3   157.5 3   157.7 3   157.7 4   157.7 7   157.7 7   157.9 7   157.9 5   157.9	VERTICAL  157.8 157.8 158.1 158.0 158.0 158.0 157.8 157.8 157.4 157.2 154.9	154'9 154'9 154'4 154'2 154'1 154'0 153'8 159'2 159'2 159'1	158.8 155.9 156.1 156.1 154.4 154.3 154.2 154.5 154.6 156.2 156.2
58 0	-	161.3	157.2	157.8	158.2		157		154.9	158.9	156.3
Thermometer	62.6	63.1	64.0	64.2	64.2	63.7	63°	$\begin{array}{c c}4 & 62.7\end{array}$	62.2	62°5	62.7
			<del></del>					ng Numbers der	note decreas	ing Westerly	Declination,
		l m		TEOROLO		OBSERVAT	TONS.				
Mean Göttingen Time.	Barometer at 32°.	Dry.	Wet.	Direc	1	Force			Weat	her.	
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				·	MAGNET	ICAL OI	BSERVATIO	NS.			Septe	mber 22nd	and 23rd.
		DECLINATI	ON.						Ang	gular Value o	of one Scale	Division =	0' 721.
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115.4	114.2	114.0	113.0	115.2	94.0	94.4	98.4	93		95.8	102.6	105.6	110.4
113.2	114.4	112.4	113.6	115.4	92.2	93.6	99.2	92	.8	96.0	102.3	106.4	109.9
113.4	114.3	112.2	114.2	114.8	93.4	93.2	99.3	91	•4	95.6	100.6	106.6	110.7
113.9	114.2	112.2	114.3	114.4	97.4	96.5	99.4	90		95*9	99.0	106.2	110.2
113.9	115.4	111.4	114.0	114.2	97.8	96.2	98.3	90		96.6	100.0	107.5	111.1
113.9	115.7	110.4	115.4	112.9	98.0	97.4	95.6	90		96.6	100.4	107.5	110.2
113.9	116.2	109.4	118.3	110.4	98.0	97.6	96.4	89		97:3	101.2	108.0	112.0
113.9	117.0	109.4	114.3	109.2	99.2	95.3	95.4		.3	97.6	102.4	108.0	112.3
113.9	117.2	108.8	114.4	106.8	98.6	95.4	96.0	92	-8	98.3	103.5	108.4	112.4
		HORIZONT.				1	n Scale Divisio	T		1	r	1	
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612.5	618.0	615.2	608.5	610.0	598·2	607.0	606.4	602		612.0	620.0	613.2	617.0
613.0	617.5	614.1	607.1	610.2	<b>598.0</b>	604.8	603.6	604		612.5	605.8	614.0	621.0
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613.2	618.0	614.0	605.0	610.4	596.0	604.7	604.0	607		615.2	602.5	608.8	620.0
613.0	620.0	613.0	604.0	608.2	600.0	608.0	603.6	607	6	616.0	602.2	614.2	614.0
613.0	621.0	613.0	605.0	606.2	597.8	609.0	603.0	605		616.0	603.0	615.0	614.0
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158.2	158.9	157.8	155.3	158.9	160.3	155.6	156.1	156		157.6	161.9	161.2	157.0
158.2	158.9	157.8	156.1	158.9	159.7	156.0		156		157.6	162.7	161.2	156.2
158.2	158.9	157.8	156.1	160.5	159.7	156.1	156.1	156		157.6	162.6	160.7	157.5
158.2	158.9	157.8	156.8	161.2	157.6	155.8	156.1	157		159.6	163.3	159.6	157.5
158°2 158°5	158'9 158'9	157.8 157.8	157°3 157°8	161°2 161°2	155°8 155°8	155°7	156°1 156°1	157 157		159.6 159.6	163°3 161°7	159°6 159°4	156.7 156.7
158.5	158.9	157.4	158.3	160.3	154.8	156.1	156.1	157		159.9	162.0	157.9	156.1
158.6	158.9	157.4	158.3	160.3	154.5	156.1	158.0	15		159.9	161.7	157.9	156.1
158.6	158.9	155.8	158.4	160.3	155.6	156.1	156.9	156		160.3	161.7	157.9	156.1
158.8	158.9	155.8	158.9	160.4	154.7	156.1	156.9	156		160.5	161.7	157.9	155.3
158.8	158.9	155.6	158.9	160.4	155.6	156.1	156.9	156	5.2	160.5	161.7	157.9	154.8
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and incre	easing Horizo	ntal and Ver	tical Force.										
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Vol. III.

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	M	ETEOROLO	GICAL (	BSERVAT	ions.									
arometer		Direc		Force.			Weath	er.						
In. 629.785 5529.797 44529.821 4429.837 44629.887 329.887 329.8887 329.898 3629.902 329.909 3	2.8 42.0 3.5 38.6 3.3 36.6 3.4 35.0 3.0 35.6 3.0 35	W. b W. k W. k W. b N.W.	by S. by S. by S. by W.  y W.	Light. Very ligh Very ligh Very ligh Very ligh Calm. Very ligh Calm. Calm. Calm.	t. Clear t. Clear t. Clear t. Clear Clear Clear t. Clear Clear Clear Clear Clear Clear Ligh	r. r. r. r. r. r. r. r. r. r. r. r. r. r								
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Thermometers.   Thermometers.   Thermometers	168.8   166.7   166.5     168.8   166.5   166.5     168.8   166.5   166.6     168.8   166.5   166.6     168.8   166.5   166.9     168.8   166.5   166.9     168.8   166.5   166.9     168.8   166.5   166.9     168.8   168.3   167.7   166.9     168.8   168.3   167.7   166.9     168.8   168.3   167.7   166.9     168.8   168.3   167.7   166.9     168.8   167.5   167.3   167.1     168.8   167.5   166.5   167.0     168.8   167.5   166.5   167.0     168.8   167.5   166.5   167.0     168.9   168.3   167.7     168.9   168.3   167.7     168.9   168.3   167.7     168.9   168.3   167.7     168.9   168.3   167.7     168.9   168.9   166.9     168.8   168.3   167.7   166.9     168.9   168.3   167.7   166.9     168.9   168.3   167.7   166.9     168.9   167.5   167.3   167.1     168.8   168.8   166.5   167.7     168.9   167.7   166.9     167.7   166.9   167.0     168.8   168.8   166.5   167.7     168.9   167.7   166.9     167.7   166.9     168.9   167.7   166.9     167.7   166.9     168.8   168.8   167.7   166.9     168.9   167.7   166.9     168.9   167.7   166.9     168.9   167.7   166.9     167.7   166.9     168.9   167.7   166.9     168.9   167.7   166.9     168.9   167.7   166.9     167.7   166.9     168.9   167.7   166.9     168.9   167.7   166.9     167.7   166.9     168.9   167.7   166.9     168.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   167.7   166.9     169.9   169.9   169.9     169.9   169.9   169.9     169.9   169.9   169.9     169.9   169.9   169.9     169.9   169.9     169.9   169.9   169.9     169.9   169.9     169.9   169.9     169.9   169.9     169.9   169.9     169.9   169.9     169.9   16	168   8   166   7   166   5   166   5     1	168   8   166   7   166   5   166   5   167   5	168   166   7   166   5   166   5   167   5   169   1     168   168   166   5   166   5   166   5   167   5   168   5     1	168 * 8   166 * 7   166 * 5   166 * 5   167 * 5   169 * 1   168 * 5     168 * 8   166 * 5   166 * 5   166 * 5   167 * 5   168 * 5   167 * 5     1	168 *8   166 *7   166 *5   166 *5   167 *5   169 *1   168 *5   163 *8     168 *8   166 *5   166 *5   166 *5   167 *5   168 *5   167 *5   163 *8     168 *8   166 *5   166 *6   166 *5   167 *5   168 *5   167 *5   163 *6     188 *8   166 *5   166 *6   166 *5   167 *5   168 *5   167 *5   163 *6     188 *8   168 *8   166 *5   166 *9   166 *5   167 *5   168 *5   167 *0   163 *5     188 *8   168 *8   166 *5   166 *9   166 *5   167 *5   168 *5   167 *0   163 *5     188 *8   168 *8   166 *5   166 *9   166 *5   167 *5   168 *5   167 *0   163 *5     188 *8   168 *8   167 *7   166 *9   167 *0   167 *7   168 *5   167 *0   162 *9     188 *8   168 *3   167 *7   166 *9   167 *0   168 *3   168 *5   165 *1   162 *9     188 *8   168 *3   167 *7   166 *9   167 *0   168 *1   168 *5   165 *1   162 *9     188 *8   167 *5   167 *3   167 *1   167 *0   168 *1   168 *5   165 *2   162 *9     188 *8   167 *5   166 *5   167 *0   167 *0   168 *4   168 *5   165 *3   161 *0     189 *7   58 *8   59 *0   59 *5   59 *5   59 *4   59 *2   59 *0   59 *2      Sample	168   8   166   7   166   5   166   5   167   5   169   1   168   5   163   8   158   2					

• At 21d 10h, Thermometer of H. F., 55° · 5; of V. F., 55° · 5.

				λ	AA GNETI	CAL OBS	ERVATIO	NS.		(	October 20th	and 21st.
		DECLINATI	on.						Angular Value o	of one Scale	Division =	0' 721.
21 ^h .	22 ^h .	23 ^h .	O ^h .	1 ^h .	2 ^h .	3h.	4 ^h .	5 ^h .	. 6 ^h .	7 ^h .	8 ^h .	9 ^h .
Sc. Div. 111'8 111'5 112'0 112'4	sc. Div. 114.6 114.6 114.3 114.8	Sc. Div. 115°0 114°6 114°2 114°2	Sc. Div. 114'6 114'6 115'0 115'0	Sc. Div. 116°4 116°8 116°8 116°9	Sc. Div. 118'0 118'4 119'3 120'4	Sc. Div. 119 4 118 8 118 8 118 2	Sc. Div. 117.6 117.2 116.4 116.4	sc. D 113 113 113 112	4   108°2 4   108°2 6   107°5	Sc. Div. 106 2 106 4 106 5 106 5	sc. Div. 107 '4 107 '6 107 '6 107 '6	\$c. Div. 107.9 107.8 108.2 108.4
12·4 11·6 11·4 11·4	115.4 115.6 115.5 114.8	114.4 114.6 114.6 114.6	115.0 115.2 115.0 115.0	116.7 117.2 117.6 117.6	121.5 120.3 120.2 120.2	117 · 4 117 · 4 118 · 6 118 · 6	115·2 115·2 114·2 114·2	110. 110. 110.	$ \begin{array}{c cccc} 6 & 107.1 \\ 3 & 107.0 \\ 2 & 106.5 \end{array} $	106.9 106.9 107.4 107.4	107 6 107 7 107 6 107 9	109.1 109.1 109.1
11.7 12.0 13.2 13.8	114'4 114'4 114'6 114'5	114.8 114.6 114.6 114.6	115.4 115.7 115.8 116.1	118.0 118.4 118.7 118.0	118'4 118'4 120'3 120'4	118'4 118'6 117'8 118'4	113.6 113.8 113.8 113.4	109 109 109	4 106.3 3 106.0 106.0	107 · 4 107 · 6 107 · 6 107 · 4	107.9 107.9 107.9	109°2 109°4 109°0 109°2
		Horizonta	L Force.		]	ncrease, in	Scale Divisi	ons, cori	responding to 1°	decrease of	Temperatur	e, 1°63.
16.0 15.8	615.5 615.5 616.0	620°5 620°5 620°7	621 ° 0 621 ° 0 620 ° 8	617:5 617:7 618:5	614.8 615.0 613.2	611.0 611.0 611.0	603.8 603.4 604.2	594 593 594	1   600°0 7   601°1 2   601°8	604.0 604.0	611.0 611.0 612.0	619°5 618°2 619°0
16.0 16.2 16.1 16.1 16.0	616.0 617.5 619.0 619.0 619.3	621.0 621.0 621.0 621.0 621.5 620.5	620.7 621.2 621.5 621.7 619.5 619.2	618.5 617.0 617.0 617.0 616.0	613.0 614.0 614.0 613.2 615.0 613.0	609'8 608'2 607'4 605'4 605'0 604'8 603'8	602'4 602'0 601'2 600'0 599'8 597'2 597'0	599 598 598 597 597 597 597	4   603°3 1   602°1 7   602°2 1   603°1 1   604°3	606.0 607.1 608.0 609.1 609.2 610.5 610.0	613.0 613.5 614.0 615.0 616.0 617.5	618'8 619'5 619'0 620'0 621'0 619'8 620'0
15.4 14.8 15.0	619.8 620.5 620.6	620°5 620°5	619.0 619.0	616.0 612.8	610.0 609.2 611.2	603.0	597.0 595.8	598· 599·	1 603.0	611.0 610.0	617°5 617°5 618°8	621.0 620.2
56.2	56.4	5Š·7	55.4	54°3	54.0	54.4	54.6	55.	1   55.1	55.5	55.5	55.9
		VERTICAL	Force.		I	ncrease, in	Scale Division	ons, corr	responding to 1°	decrease of	Temperatur	e, 1.64.
66:1 66:1 66:1 66:1 66:3 66:3 66:3 66:4 66:8 66:8	167.8 167.9 167.9 167.9 168.0 168.5 168.5 168.5 168.6 168.9 168.9	168 '9 168 '9 169 '0 169 '0 169 '0 170 '2 169 '8 169 '9 169 '9 169 '9	169 ° 9 169 ° 9 169 ° 9 169 ° 9 170 ° 3 170 ° 5 170 ° 7 170 ° 8 170 ° 8 170 ° 8 170 ° 8	170.8 170.8 171.5 171.8 171.8 172.3 172.7 172.7 172.7 173.7 173.7	174'1 174'1 174'1 174'1 174'1 174'9 174'9 174'9 174'9 174'4	174 · 4 174 · 4 174 · 4 174 · 4 174 · 4 174 · 4 173 · 8 173 · 8 173 · 8 173 · 8 173 · 8	173 · 2 173 · 2 173 · 0 173 · 0 172 · 8 172 · 8 172 · 8 172 · 1 171 · 6 171 · 1 171 · 2	171° 171° 171° 171° 171° 171° 171° 171°	2   170°8 0   170°8 9   170°8 9   170°8 9   170°8 7   170°8 7   171°5 2   171°5 2   171°5 9   172°2	172 '4 172 '2 172 '2 172 '2 172 '3 172 '4 172 '6 172 '6 172 '6 172 '5 172 '5	172.5 172.5 172.5 172.5 172.5 172.5 172.5 172.7 172.7 172.7 172.8 172.8 172.5	172.6 172.3 172.3 172.3 172.2 172.2 172.3 172.3 172.3 172.3 172.3 172.5
58°4	57°4	57°2	5 [°] 7 · 2	56°·5	$5\overset{\circ}{5}$ $\cdot$ $2$	55°2	55.4	55.	5 55.4	55.2	55.5	56.0 a
d increa	sing Horizo	ntal and Ver	tical Force									
					TEOROLO		DBSERVAT	TONS.	1			
	öttingen me.	Barometer at 32°.	Ther Dry.	Wet.	Direc	etion.	ind. Force.			Wea	ther.	
D. H. 20 22 21 21 3	. м. 2 0	at 32°. Dry. Wo  M. In. ° 0 29 943 31 0 27 0 29 959 33 9 30 0 29 956 34 5 30 0 29 962 35 9 31 0 29 984 38 1 34 0 29 961 41 5 37 0 29 939 44 0 38 0 29 930 44 7 39 0 29 938 44 7 39 0 29 882 44 0 38		27.6 30.5 30.9 31.7 34.2 37.0	N. b N. b N. b E. b E. S N.E. E. N E. N	y E. y E. y E. y E. y S. i.E. by E. i.E.	Calm. Calm. Very lig Very lig Calm. Very lig Very lig Very lig Very lig Very lig Very lig Light	ht. ht. ht. ht. ht. ht. ht.	Light clouds. Cloudy. Cloudy, with of Cloudy, with of Cloudy, with Cloudy, with Cloudy, with Cloudy, with Cloudy, with Cloudy, with Cloudy, with Cloudy, with Cloudy, with Cloudy, with Cloudy, with Cloudy, with	eir., eirstra eir., eirstra eir., eirstra eir., eirstra eir., eirstra eir., eirstra eir., eirstra	t., and haze. t., and haze. t., and haze. t., and haze. t., and haze. t., and haze. t., and haze. t., and haze. t., and haze.	

November 26th a	and 27th. MAGNETICAL OBSERVATIONS.										
Mean Göttingen	Ang	ular Value	of one Scale	Division =	= 0' . 72	l.			DECLINAT	ION.	
Time.	10 ^h .	11 ^h .	12 ^h .	13 ^h .	14h.	15 ^h .	16 ^h .	17 ^h .	18h.	19 ^h .	20 ^h .
M. S. O O O O O O O O O O O O O O O O O O	Sc. Div. 106 ° 9 106 ° 1 106 ° 6 106 ° 2 106 ° 6 105 ° 7 105 ° 0 104 ° 5 104 ° 9 104 ° 7 104 ° 4 104 ° 1	Sc. Div. 103 *8 104 *4 104 *9 105 *0 105 *4 106 *0 110 *4 111 *9 110 *0 112 *4 136 *2 130 *0	Sc. Div. 116.0 101.9 98.3 106.2 109.4 110.4 110.5 118.4 110.4 107.5 111.3 113.5	Sc. Div. 116 '6 117 '4 116 '4 114 '0 114 '6 115 '0 116 '0 114 '0 112 '4 110 '4 110 '8 110 '4	Sc. Di 111 ' C 111 ' C 112 ' C 113 ' C 117 ' C 119 ' C 119 ' C 119 ' C 111 ' C	6   106.0 109.4 113.0 111.2 110.0 4   112.4 6   116.4 116.6 4   116.0 7   115.9 8   116.0	Sc. Div. 115 '2 110 '9 109 '2 110 '5 112 '5 113 '1 113 '4 113 '5 113 '9 113 '4 112 '8	sc. Div. 111 '6 111 '9 111 '4 110 '4 109 '4 109 '4 109 '9 110 '4 110 '6 110 '9 111 '5	sc. Div. 111'4 111'2 110'4 110'6 111'0 111'3 110'8 110'4 110'2 110'2 110'4 110'3	Sc. Div. 110'4 110'2 110'2 109'6 109'4 108'9 109'2 108'9 109'3 109'5 109'6 108'8	sc. Div. 109 '2 109 '8 109 '8 109 '0 108 '5 108 '4 106 '6 105 '6 105 '6 104 '8 104 '3 104 '4
	1		sion = .00		1			1	1	AL FORCE.	
M. S.  2 0  7 0  12 0  17 0  22 0  27 0  32 0  37 0  42 0  47 0  52 0  57 0	623 '9 624 '6 619 '2 616 '2 613 '8 612 '2 612 '0 612 '9 612 '2 610 '0 610 '3 610 '0	610°0 608°7 609°1 607°9 607°7 610°0 605°0 619°8 621°2 611°0 617°0 623°6	624'3 618'7 604'9 602'8 608'0 615'0 613'0 619'0 612'1 604'1 604'0 603'3	607.0 611.8 614.0 613.0 609.0 611.2 612.4 614.8 614.0 614.2 615.0 615.0	614 1 1 614 0 615 0 615 0 615 0 615 0 615 0 625 0 625 0 635 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637 0 637	629°0 621°5 620°8 629°0 628°2 622°0 626°2 630°0 627°2 628°0 626°5	629.0 626.0 622.0 619.5 620.5 620.0 622.0 622.0 622.0 622.0 622.2 623.0	622.0 622.5 622.0 622.5 623.0 624.5 622.5 619.0 618.0 618.2 619.0	620°0 620°2 622°0 621°0 621°0 620°6 620°8 621°0 621°0 621°2 621°2 621°2	621.5 621.5 621.5 622.5 622.0 622.0 622.2 621.5 621.2 620.0 620.2 621.5	621 · 5 624 · 0 624 · 5 620 · 0 619 · 0 616 · 5 617 · 0 618 · 8 618 · 0 620 · 0 619 · 0
Thermometer	46.9	46.9	47.0	46.6	46.8	46.8	46.7	46.5	46.2	46.0	45.0
M. s. 3 0 8 0 13 0 18 0 23 0	193 '4 194 '4 193 '8 192 '5 192 '3	192.7 192.5 192.7 192.5 192.7	ion = '000 187'2 189'0 193'1 194'8 194'8	196.8 197.6 197.9 197.9 197.7	of the V.  197.6 197.6 197.6 196.8 195.9	184°3 184°3 184°5 184°5	186.7 186.7 187.3 187.9 188.3 188.3	188 1 188 5 189 0 189 0 189 0	VERTICAL   188.8   188.7   188.7   188.7   188.7	188.6 188.5 188.5 188.3 188.3 188.3	185.8 185.8 185.8 184.6 184.6
28 0 33 0 38 0 43 0 48 0 53 0 58 0	193°2 193°2 193°5 193°5 194°0 193°1	192.7 193.1 191.9 190.7 192.6 191.4 187.2	197°2 197°8 193°3 191°7 192°5 193°9 195°5	197 7 197 7 197 5 197 5 197 5 197 5	195 9 195 9 195 6 192 6 192 8 185 7	186°1 187°2 187°2	188.6 188.7 188.7 188.6 188.6 188.7	189.0 188.8 188.8 188.8 188.8	188.6 188.6 188.6 188.6	188°3 188°3 188°0 187°1 186°7 186°5	184.6 185.0 185.0 185.0 185.0
Thermometer	47.4	47°8	48°4	47°8	47.9	47.4	47°8	48.2	47.7	47.4	46.7
						]	Increasing N	Numbers der	ote decreasi	ng Westerly	Declination,
		1		reorolo		OBSERVATI	IONS.				
Mean Göttingen Time.	Barometer at 32°.	There Dry.	Wet.	Direc	Wir	Force.			Weathe	r.	
D. H. M.  26 10 0 11 0 12 0 13 0 14 0 15 0 16 0 17 0 18 0 19 0 20 0 21 0	In. 29.817 29.823 29.837 29.844 29.845 29.845 29.847 29.835 29.816 29.808 29.788	25·9 24·4 23·7 22·6 22·5 21·7 21·3 20·4 19·6 20·5 21·5 22·1	4								
Į.		1	At 27d 10h.	1	Į.						

^a At 27^d 10^h, Thermometer of H. F., 47° '0; of V. F., 47° '2.

					MAGNET	rical c	BSERVATIO	ONS.		No	vember 26tl	and 27th.
		DECLINATI	ON.					Ang	ular Value	of one Scale	Division =	= 0' · 721.
21 ^h .	22h.	23h.	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .
Sc. Div. 104°3 104°4	Sc. Div. 104'4 103'8	Sc. Div. 111'4 111'0	Sc. Div. 113 2 112 6	Sc. Div. 113 '4 113 '8	Sc. Div. 114'8 112'7	Sc. Div 108 5 109 7	113.0	Sc. Div. 113 1 112 4	Sc. Div. 109*6 108*6	Sc. Div. 105 2 105 0	Sc. Div. 107.4 105.8	Sc. Div. 107 4 107 2
103.9	103.6	111.0	112.4	114.0	111.4	109.7		111.6	109.3	105.2	105.8	106.4
104.0	104.5	110.4	112.2	113.0	111.3	109.4		112.2	108.9	104.6	107.6	106.6
104.3	106.4	109.4	111.5	113.2	111.4	109.4		111.3	107.8	104.6	108.4	106.2
105.4	106.8	108.2	111.0	114.3	112.1	109.6	116.4	110.6	106.6	105.4	110.4	105.8
106.5	108.6	108.6	113.4	114 5	111.4	111.2		111.4	106.6	105.3	110.5	106.4
107.3	108.6	109.4	112.4	114.5	110.4	111.0	115.4	109.2	106.5	104.7	111.0	106.2
108.2	110.5	110.4	112.8	114.3	109.8	111.4		110.4	104.4	104.4	110.4	105.4
108.4	111.4	110.4	113.2	115.4	110.5	109.5		108.6	105.4	104.4	110.5	105.0
108.4 106.4	111.8	112.5 113.4	113.8 114.0	114.6 115.2	$109.6 \\ 109.4$	110.8	114°3 112°6	109.4 108.8	105.4 $105.4$	105.4 105.4	108.4	105°8 106°2
	1	Horizonta	L Force.		]	nerease, i	n Scale Divisi	ons, correspo	nding to 1°	decrease of	Temperatu	e, 1.63.
619.9	621'9	627.5	631.4	630.2	627.0	615.8		619.0	615.3	615.0	624.0	628.8
619.8	621.0	629.8	630.0	628.8	627.0	616.0		619.0	617.0	616.0	622.2	627.6
619.0	619.0	631.4	630.2	629.8	621.9	618.0		619.2	618.8	617.0	620.0	628.0
616.9	620.2	633.5	630.8	628.8	619.1	619.1	623.0	618.2	620.0	618.0	619.8	625.2
617.0	622.5	631.0	629.8	628.0	618.4	621.0		618.2	619.5	620.0	621.2	625.4
616.0	619.8	634.3	$629^{\circ}2$	628.2	617.9	621.0	619.0	617.8	622.0	623.5	622.5	628.6
618.0	620.0	634.0	631.4	628.7	626.2	621.2		618.2	624.5	623.0	624.8	627.8
619.0	622.2	632.5	630.0	628.1	615.8	619.4		617.0	625.0	624.0	622.5	626.5
623.0	622.5	634.0	629.0	628.0	614.0	620.0		616.2	619.5	622.0	627.0	628.0
625.0	622.0	633.5	629'2	628.0	615.0	619.5	616.0	618.2	624.0	625.0	626.5	630.0
627°0 626°0	626°2 629°8	632.4 631.5	631.0 632.5	628°2 627°1	616.0 616.0	615.8		616.0	$613.0 \\ 614.2$	619.8	630.5	628*8 629*5
45.3	45.5	45°6	45°6	45°5	44.9	44.7	45°2	46°0	46.2	46°2	46°6	47°2 a
	<del></del> .	VERTICAL ]	Force.	<u></u>	]	nerease, i	n Scale Divisi	ons, correspo	nding to I	° decrease of	f Temperatu	re, 1.64.
185.4	185.3	185.8	186.2	187.1	188.0	187.7	190.4	193.0	191.3	190.7	193.9	193.8
185.4	185'3	185.8	186.5	188.0	188.0	187.7	190.4	193.0	191.3	190.7	193.9	193.8
184'1	185.3	185.6	186.4	187.9	188.0	187.7	191.2	193.0	191.1	191.5	193.7	193.1
184.1	185.4	187.4	187.8	187.9	187.7	187.7	191.2	193.0	191.5	191.5	193.7	193.1
184.1	185.4	187.6	187.8	187.9	187.7	187.7	191.2	192.2	191.5	191.2	193.7	193.5
184.1	185.4	187.6	187.2	188.0	187.7	187.8	192.2	192.5	192.5	191.2	193.7	193.2
184.1	186.2	187.6	187.2	188.0	187.7	187.8		192.4	192.5	191.5	194.3	192.8
185.1	186.5	187.3	187.1	188.0	187.7	189.8		192.5	192.5	192.1	193.8	192.8
185.9	186.2	187.1	186.8	188.0	187.7	189.8		191.3	192.1	192.1	193.8	192.6
185.9 186.4	185.3	187.1	186.8	188.0	187.7	189.8		192.0	$190.7 \\ 190.7$	193.1	193.6	193.6
186.4	186.1	186.5	186.6	188.0	187.7	190.4		191.6		193.1	193.6	192.4
		186.2	187.6	188.0	187.7	190.4		191.2	190.7	192.8	194.0	192.6
46.7	46.9	46.8	47.4	47.2	47.0	46.7	46.0	46.4	46.7	46.6	46.8	47.0 ª
and increas	sing Horizon	ntal and Vert	ical Force.									
				M E	TEOROL	OGICAL	OBSERVAT	TONS.				
Mean G	öttingen	Barometer	Ther	mometers.			Wind.		_	**	ooth	
	me.	at 32°.	Dry.	Wet.	Dire	etion.	For	rce.		W	eather.	
р. н	I. М.	In.										
26 2		29.758	22.5	21.2	337 6	s.w.	$_{ m Lig}$	ht	Claude	ain	nd cirstrat.	
20 2	-	29 738	25.0				Lig Lig				nd cirstrat. nd cirstrat.	
	0 0	29.677	24.6			by S.	Lig Lig				ircum., and	l haze.
	1 0	29.660	25.4			by S.	Very					l haze; snow.
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	29.645	26.5	24.2		$\mathbf{w}$ .	Very					d haze; snow.
	3 0	29.624	27.5	25.3		by W.	Very	light.			circum., an	
	4 0	29.622	26.7	25.2		s.w.	Mode		Cloudy	cirstrat.,	eircum., an	d haze.
	5 0	29.594	27.8		S.W.	by W.	Lig	ht.	Cloudy	; cirstrat.,	circum., an	d haze.
	6 0	29.556	27.8	25.9		s.w.	Lig	ht.	Cloudy;	cirstrat.,	eircum., an	d haze.
	7 0	29.544	30.8	28.5		S.W.	Mode	erate.				d haze; snow.
	8 0	29.533	31.6	29.3	W. 1	by S.	Moderate,					d haze; snow.
ı	9 0	29.539	31.2	29.3		s.w.	Mode	erate.	Cloudy	; cirstrat.,	circum., an	d haze; snow.
ĺ									1			

Decemb	er 22nd a	and 23rd.			MAGNET	CICAL (	DBSERVATIO	ONS.				
Mean Gö	ittingo	Ang	gular Value	of one Scale	Division =	= 0' .72	1.			DECLINAT	ion.	
Tim		10h.	11h.	12h.	13h.	14h	.   15h.	16h.	17 ^h .	18h.	19 ^h .	20h.
м. О 5	s. 0 0	Sc. Div. 106 '9 108 '3	Sc. Div. 106.6 106.6	Sc. Div. 134'2 132'4	Sc. Div. 107.6 104.5	Sc. Di 110 :	5   113.5	Sc. Div. 114'0 113'6	Sc. Div. 114.4 116.8	Sc. Div. 121.6 121.6	Sc. Div. 105 6 107 2	Sc. Div. 116°4 116°9
10	0	107.5	107.4	138.4	106.4	112	3   113.4	113.5	117.6	117.8	109.0	116.2
15	0	106.9	108.2	142.0	107.1	1111	4   113.4	112.4	117.0	116.2	110.6	114.8
20	0	105.5	108.4	132.6	107:3	112		112.4	117.4	108.4	110.7	114.3
$\frac{25}{30}$	0	104.4	109.4 109.6	123.6 123.4	106.8	112.3	8   113.6 4   113.6	112.8 113.4	120°2 121°4	107.0 104.4	111.5	111.3
35	o	104.4	112.3	119.4	110.7	112		113.4	120.6	104 4	113.0	111.2
40	Ö	105.2	119.9	114.0	110.4	112		113.6	120.0	105.8	112.4	110.9
45	0	106.6	120.9	109.4	110.9	112	9 113.2	112.8	121.4	105.2	112.3	112.6
50	0	106.9	121.9	107.4	110.6	113		112.6	121.6	105.2	114.6	113.6
55	0	107.0	125.4	108.9	110.9	113.4	4   113.4	112.4	120.4	105.4	116.3	112.4
M.	s.	I	1	sion = *000	1					1	FAL FORCE	T
2	0	635.8	641.0	655.0	642.0	638		636.2	624.2	624.4	633.2	636.1
$\begin{array}{c} 7 \\ 12 \end{array}$	0	640°0 640°2	642.5	651.0	636.0	638.		636.0	623.4	622.2	633.6	637.5
12 17	0	640 2	644.0	640°0 647°0	636.5	636 6 641 0		636.0	$624.8 \\ 626.5$	618.8	634.0	637.0 639.4
22	0	647.8	641.2	647.0	636.9	641		635.4	625.5	617.0	636.2	640.5
27	0	646.0	643.1	649.0	636.0	639	639.0	635.0	624.8	619.2	637.8	640.0
32	0	637.5	643.8	654.0	635.0	639.0		634'8	624.0	622.8	636.0	638.3
$\begin{array}{c} 37 \\ 42 \end{array}$	0	636.2	637.5 638.5	651.5	636.0	637:5		634.0	623.2	621.8	640.1	640.2
47	0	637.0	634.2	649.0 643.0	638°5 641°0	638.0		633.2	$620.0 \\ 620.8$	626.8	639°2 635°5	635.8 636.7
$\tilde{52}$	ŏ	640.1	642.0	638.8	640.2	638.0		631.8	621.5	630.8	635.5	634.0
57	0	641.0	643.0	638.2	639.2	639.0		631.2	622.2	633.8	635.3	638.2
Thermo	ometer	42°·5	43.0	43.0	42.5	4Î :	5 4ΰ1	41.4	4Î.8	4i°2	41°5	41.2
м.	s.	- One	Scale Divis	ion = '000	0063 parts	of the V	. <b>F.</b>			VERTICA	L Force.	
3	0	201.7	198.2	199.4	199.0	198.8	3   198.5	199.4	198.4	198.0	195.6	192.3
8	0	201.0	198.6	198.4	199.1	198.8		199'4	198.4	198.0	195.2	193.1
13 18	0	200.8	198.7	198.2	199.1	198.8		199'4	199.5	198.0	195.2	193.4
23	0	201.1	198.7 198.8	197°3 196°5	199 <b>·1</b>	198.8		199.4 199.4	$199.5 \\ 199.5$	197 <b>.</b> 9 197.4	195°2 194°9	194°3 194°3
28	Ö	201.6	199.4	197.0	199.1	198.5		198.2	198.6	196.4	194.9	193.8
33	0	200.5	199.4	197.4	199.1	198 :	5   198.9	198.5	198.1	196.3	194.9	193.8
38	0	199.0	198.3	197.2	199.1	198.5		198.5	198.3	197.1	195.9	193.8
$\begin{array}{c} 43 \\ 48 \end{array}$	0	199.0 198.8	199°0 198°7	197.2	199.1 199.1	198.5		198.5	198.0	197.9	195°7 193°7	193.8
53	0	198.6	199.3	197.6 197.8	199.1	198.5		198.6 198.1	197°3 198°0	197.8 197.8	193 7	193.8 193.8
58	Ö	198.6	200.4	198.2	199.1	198.2		199.4	198.0	196.4	192.8	194 4
		ļ				<b> </b> -						
Thermo	ometer	4η6	42.7	43.4	43.3	42°·4	42.5	42.2	42.2	42.2	42.2	42°5
·								Increasing N	umbers den	ote decreasi	ng Westerly	Declination
	1		The	ME mometers.	1 EOROLO	GICAL	Wind.	IONS.	1			
Mean Göt Time		Barometer at 32°.	Dry.	Wet.	Direc	tion.	For	ce.	-	W	eather.	
D. н.	м.	ln.	0	0								
22 10.	1	29.221	25.0	22.9	N.V	$_{N}$	Very l	ight.	Claud	alm	d ha	
11	ŏ	29.255	24.4	or and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state o		circum. an						
12	0	29:291	21.3	19.5	N.V	v.	Moderate, v	vith gusts.		circum. an		
13	0	29:317	19.6	17.5	N.N		Moderate, v		Cloudy;	circum. ar	d haze.	
14	0	29°345 29°349	19.6	16.8	N.V W		Mode Ligi			circum. an		
1.5	ŏ	29.356	18.6	17.0	w		Ligi			circum. an		
15 16	- 1	29.382	19.0	17.5	W. b							
16 17	0							Very light. Cloudy; circum. and haze.				
16 17 18	0	29.358	17.7	16.1	W. b.							
16 17 18 19	0	29.358 $29.358$	17.7	15.8	W.S	.W.	Very l	igh <b>t.</b>	Cloudy;	circum. an	d haze.	
16 17 18	0	29.358	17.7			w. w.		igh <b>t.</b> igh <b>t.</b>	Cloudy; Cloudy;		d haze. d haze.	

^a At 23^d 10^h, Thermometer of H. F., 40° '5; of V. F., 40° '3.

T						MAGNET	rical (	OBSERVATIO	ONS.		Dece	ember 22nd	and 23rd.
			DECLINATI	ON.					Λ	ngular Value	of one Scale	Division =	= 0''721.
	21h.	22h.	23h.	Oh.	1 h.	2h.	3h.	4 ^h .	5 ^h .	6h.	7 ^h .	8h.	9h.
	8c. Div. [11.0] [11.4] [11.1] [11.6]	sc. Div. 115'4 115'0 114'3 113'6 111'5	Sc. Div. 110'4 110'4 110'2 108'4 109'4	Sc. Div. 110°9 109°4 109°4 108°2 108°0	Sc. Div. 111 ° 0 112 ° 4 113 ° 4 112 ° 6 112 ° 9	Sc. Div. 111 ° 0 109 ° 6 112 ° 6 112 ° 4 113 ° 4	Sc. Di 115 '6 113 '6 113 '3 114 '2 113 '8	6   111°5 6   112°7 2   111°2 2   113°5	sc. Div. 111.6 112.0 111.4 111.8 110.4	Sc. Div. 109*4 109*2 108*4 108*2 107*4	Sc. Div. 107.5 106.9 108.2 108.4 107.2	sc. Div. 107 '2 105 '9 104 '9 106 '3 106 '4	Sc. Div. 104 6 103 4 104 4 103 0 100 8
1 1 1 1 1 1	11 · 2 12 · 4 13 · 4 13 · 7 12 · 7 13 · 1	112.0 111.9 113.3 114.0 114.4 113.4	112.4 112.8 113.0 113.0 113.2 115.4	109°5 109°8 109°0 110°0 109°7 110°0	112.0 111.4 111.6 111.6 112.8 113.4	114·4 115·4 114·0 115·0 115·4 112·4	116 ° 6 116 ° 6 116 ° 6 115 ° 6 112 ° 8 113 ° 6	6   114·4 6   112·7 2   113·5 0   112·8 112·2	110 4 110 2 108 8 110 0 111 2 109 0 110 2	106.6 106.6 107.4 106.4 106.9 107.3	106 4 106 5 106 5 106 0 105 8 107 0	109 4 109 4 107 4 107 2 105 4 105 4	102 2 103 4 105 9 109 0 110 0 112 0
	13.8	112.6	111.7	108.8	112.4	115.4	113	111.8	111.9	106.2	108.6	106.0	110.6
_			Horizonta		·			in Scale Divisi	1		1	<del></del>	
6 6 6 6 6 6 6 6	36.0 37.0 38.0 36.4 38.9 39.0 42.2 38.0 40.0 41.3 41.0 41.0	642.0 641.3 642.0 642.0 641.0 640.8 638.2 637.8 637.0 635.0 637.8 641.0	639 ° 0 638 ° 2 638 ° 0 634 ° 2 630 ° 0 632 ° 0 632 ° 4 633 ° 0 633 ° 0 633 ° 2 640 ° 0 640 ° 0	643.5 643.0 645.0 640.0 639.8 638.0 638.8 640.0 641.8 637.0 644.0 640.2	640.0 644.0 638.5 643.0 645.0 637.5 639.5 642.0 639.0 639.5 641.0 640.0	640.0 637.5 635.5 638.5 640.0 637.0 639.0 635.0 639.0 637.5 634.5	637 °C 639 °C 636 °C 636 °C 637 °C 637 °C 630 °C 630 °C 630 °C	628.0 626.0 626.0 626.0 626.0 626.0 626.5 627.0 628.8 628.5 629.2	631°3 631°2 631°2 632°8 633°0 628°2 625°2 622°5 633°0 630°8 629°6 622°4	623.8 621.6 624.2 624.0 624.5 623.2 618.8 623.0 620.6 624.0 628.9 624.7	626.0 629.0 627.8 627.8 633.0 631.0 630.2 639.0 633.7 637.0 629.8 633.0	637 3 638 0 638 6 638 0 639 0 638 2 636 0 637 0 640 5 640 0 639 0 640 0	637.0 634.4 633.0 632.0 631.8 632.0 633.0 630.0 629.8 636.0 641.0 643.0
	4ΰ5	42°0	41.8	4Ï·6	41°4	40°5	40.0	39.6	39.9	39.2	39.0	39.4	39.8*
		-	VERTICAL ]	Force.		1	Increase,	in Scale Divisi	ons, corres	ponding to 1°	decrease of	f Temperatu	re, 1.64.
19 19 19 19 19 19 19	93.4 93.6 93.4 93.4 93.4 93.4 93.4 93.4 93.3 93.0 93.0 93.0	192'1 192'3 192'1 192'1 192'3 192'4 192'4 192'4 192'5 192'5 192'5	192'9 192'9 192'9 192'9 192'9 192'9 192'7 192'7 192'9 192'9 192'9	192'9 191'1 191'2 191'2 191'2 191'2 191'2 191'2 193'5 193'5 193'8 193'8	193 '3 193 '7 195 '3 195 '3 195 '1 194 '0 195 '7 195 '7 195 '7 195 '7 195 '7	194'4 194'9 194'8 195'0 195'8 195'5 196'9 196'9 197'9 197'9	198.6 199.3 199.3 199.3 198.2 199.3 198.6 198.5 198.4 198.4	198.3 197.9 197.9 197.9 198.6 198.6 198.6 198.6 198.6 198.1	198'4 198'7 198'4 198'4 197'8 197'8 197'2 199'4 199'0 197'9	197.5 198.4 198.4 198.6 199.3 199.9 199.4 199.4 199.5 201.1 200.7	200°5 200°5 200°5 200°5 200°5 200°5 202°2 202°2 200°7 202°9 202°7 201°1 201°9	202.8 202.8 202.8 202.8 202.1 202.1 202.1 202.1 202.1 202.1 202.1 203.4	203 · 4 203 · 4 203 · 4 203 · 4 203 · 4 203 · 4 205 · 1 205 · 1 205 · 1 205 · 1 203 · 9
4	42°4	42.7	42.2	42.4	42°6	41°7	40.9	40.4	40.4	40.6	40.0	39.7	40°3 a
an	d increas	ing Horizo	ntal and Vert	ical Force.									
_						TEOROLO	GICAL	OBSERVAT	IONS.	1			· <del>,</del>
	Mean G		Barometer at 32°.	Thern Dry.	Wet.	Direc	etion.	Wind.	<b>.</b>		We	ather.	
	D. H. 22 22 23 0 1 2 3 4 5 6 6 7 8 9	0 0 0 0 0 0 0 0	In. 29°336 29°328 29°324 29°322 29°272 29°246 29°201 29°153 29°074 29°057 29°025 29°014	0 17.5 17.5 17.7 17.7 19.9 19.4 20.2 21.9 23.6 24.0 24.0 24.4	6.3 16.3 16.8 16.9 18.7 18.5 18.7 20.9 22.2 22.6 23.1 23.3	W.S. W.S. S.W. S.V. S.V. S.V. S.W. S.W.	.W. by S. W. W. W. W. by S. W. W. W. W. W. W. W. W. W. W. W. W. W.	Very lig Very lig Very lig Light Very lig Modera Light Fresh, with Brisk Modera	ght. ght. ght. ght. ste. squalls.	Cloudy; cir. Cloudy; cir. Cloudy; cir. Cloudy; cir. Cloudy; cir. Cloudy; cir. Cloudy; cir. Cloudy; cir. Cloudy; cir.	eum. and land, ceum., cir eum., cir eum., cir eum., cir eum., cirst -eum., cirst -eum., cirst	haze. strat., and he strat., and he strat., and he strat., and he strat., and he crat., and haze crat., and haze trat., and haze trat., and haze trat., and haze trat., and haze trat., and haze trat., and haze trat., and haze trat., and haze	ıze. ıze. ıze.

January 19th and	1 20th.			MAGNET	CICAL OF	BSERVATIO	ONS.				
Mean Göttingen	Angu	lar Value of	one Scale D	oivision = (	)'·721.				DECLINAT	ion.	
Time.	10h.	11 ^h .	12h.	13 ^h .	14 ^h .	15h.	16 ^h .	17 ^h .	18h.	19 ^h .	20h.
м. s.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div		Sc. Div.	Sc. Div.	Sc. Div.
0 0	106.8	107.5	107.6	109.7	114.0	116.1	113.3		111.3	112.6	104.4
5 0	107.4	107.6	107.4	110.0	117.6	115.3	113.0		111.4	112.3	102.0
10 0	107.1	107.8	107.5	110.1	119.0	114.4	112.4		111.7	109.6	102.5
15 0	106.7	107.4	107.6	111.3	118'4	113.2	112.0		112.2	110.4	101.4
20 0	106.0	107.0	109.0	111.8	119.0	113.0	112.4		112.7	111.4	102.2
25  0	105.4	107.8	108.6	113.4	118.0	112.6	112.8		113.5	110.4	104.4
30 O	104.4	108.0	108.2	115.4	117.4	112.5	112.3		113.0	110.4	103.5
35 O	104.4	108.4	109.2	115.4	116.9	112.4	112.5	5   111.4	111.6	110.5	105.8
40 0	105.7	108.9	109.4	114.0	117.4	112.3	112'4		112.4	110.5	106.6
45 O	107.0	109.0	109.6	113.3	117.4	112.9	112.5		112.3	111.4	105.4
50 O	107.8	109.8	109.2	112.3	118.0	113.4	112.8		112.6	113.5	107.2
<b>5</b> 5 0	107.5	109.0	110.0	112.3	117.4	113.4	112.4	111.2	113.5	107.4	107.4
	One S	Scale Division	n = .00008	37 parts of	the H.F.		*		Horizont	AL FORCE	•
M. S. 2 O 7 O	645.0	648.0	649.0	649.0	645.0	649.2	647 :	650.2	648.0	642.0	690.0
$\begin{array}{ccc} 2 & 0 \\ 7 & 0 \end{array}$	648.0	646.5	649.2	648.0	646.0	648.5	647 8		646.0	643.5	639.8
19 0	645.8	646.8	646.0	646.0	646.0	647.0	647.0			643.0	
$\begin{array}{ccc} 12 & 0 \\ 17 & 0 \end{array}$	650.0	649.0	645.8	645.2	644.6	648.8	647 6		645.0		635.0
	649.2	648.8	648.0	$645^{\circ}2$	645.0	648.0	647.5		644.8	641.4	630.0
$\begin{array}{ccc} 22 & 0 \\ 27 & 0 \end{array}$			648.0		645.5				643.9	643.2	
$egin{array}{ccc} 27 & 0 \ 32 & 0 \end{array}$	648.0 646.8	649.2	646.8	644'8 646'9	645.0	648.5	646 6		645.0	643.2	631°2
32  0 $37  0$	647.8	650.5	647.0	648.8	645.2	646.0	648.6		645.0	$645.0 \\ 642.0$	636.4
42 0	648.0	648.2	645.8	651.1	645.5	646.2	649		644.0	642.0	638.0
42 0 47 0	650.0	651.0	648.0	650.2	649.0	646.0	649.0		645.0	644.4	641.6
52 O	650.0	651.0	648.4	649.9	648.0	646.5	649		643.9	644.2	645.5
57 O	648.2	651.0	650.0	647.1	649.0	646.0	649 (		643.0	639.7	645.8
					ļ	-	ļ				
Thermometer	39.2	39.4	39°2	39°4	38.9	38.2	38.6	39.0	39°5	40.0	41°4
	One	Scale Divisio	n = .00000	63 parts of	the V.F.				VERTICAL	Force.	
M. S.	196.5	198.6	194.0	194.2	194.1	195.1	194.0	194.2	192.3	189.1	182.3
3 0	196.6	198.6	194.1	194.2	194.1	194.7	194 (				
8 0	196.8	198.6	194 1	194.5	194.8	194.7	194 (		192°3	188°2 186°3	181.7 180.3
13 0 18 0	198.7	196.9	194.4	194.5	194.8	194.7	193.8	194.2	192.0	185.2	180.3
$\begin{array}{ccc} 18 & 0 \\ 23 & 0 \end{array}$	198.7	196.9	194.4	196.0	194.6	194.0	193.8		192.0	184.7	179.5
28 0	198.7	196.9	194.4	196.0	194.6	194.0	193 9		192.0	183.2	179.3
33 0	196.9	196.9	194.5	195.3	194.8	193.8	193.8	194.2	192.0	183.2	179.3
	196.9	196.6	194.2	195.3	194.8	193.8	195.0		191.9	183.2	181.1
$ \begin{array}{ccc} 38 & 0 \\ 43 & 0 \end{array} $	198.3	194.3	194.2	194.7	194.8	194.0	195 (		191.1	183.5	181.3
48 0	198.2	194.3	194.2	194.1	195.1	194.0	195 (		191.1	183.3	181.2
53 0	198.2	194.3	194.5	194.1	195.1	194.0	195.0		190.1	183.3	181.5
58 O	198.6	194.3	194.5	194.1	195 1	194.0	194.2		190.1	182.6	181.2
							101				101 2
Thermometer	39.1	39.1	39°5	40.0	40.1	39.9	40°4	4 3§.6	40.2	40°6	4i°4
							Increasi	ng Numbers de	note decreas	sing Westerl	y Declinati
	11		ME	TEOROLO	OGICAL	OBSERVAT	CIONS.				
Mean Göttingen	Baromete	er Ther	mometers.		W	ind.			Wea	thor	
Time.	at 32°.	Dry.	Wet.	Direc	ction.	Force.					
р. н. м.	In.	0	0								
19 10 0	30.144	4 21.9	20.0	8.8	S.E.	Very lig	tht.	Mostly clear.			
19 10 0	30.100	1	1		by S.	Very lig		Circum. and	cumstrat.		
12 0	30.076	1			S.E.	Very lig	tht.	Cirstrat, and			
13 0	30.020				S	Modera		Circum. and			
14 0	30.056				š.	Modera		Circum. and			
	29.990				y E.	Modera		Clear and unc			
15 0 29	29.952				y E.	Modera		Clear and unc	-		
16 0	29.896				3. I	Light		Clear and unc			
$\begin{array}{ccc} 16 & 0 \\ 17 & 0 \end{array}$					.w.	Light		Clear.			
17 0		2   26.3	1 24 0								
$\begin{array}{cc} 17 & 0 \\ 18 & 0 \end{array}$	29.862 29.858					Light		Clear.			
$\begin{array}{cc} 17 & 0 \\ 18 & 0 \end{array}$	29.862	3 25.5	23.4	S.S	.W. W.		. [	Clear. Clear.			
17 0 18 0 19 0	29.862 29.858	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	23.4	S.S S.S	.W.	Light	the ght.				

² At 20d 10h, Thermometer of H. F., 48° ·4; of V. F., 47° ·2.

					MAGNE	TICA	L OB	SERVAT:	IONS.		J	anuary 19th	n and 20th.
		DECLINA	rion.						А	ngula <b>r V</b> alu	e of one Se	ale Division	= 0'·721.
21h.	22h.	23h.	Oh.	1 ^b .	2h.		3h.	4h.	5 ^h .	6h.	7 ^h .	8h.	9h.
sc. Div. 107 '6 108 '5 108 '8 109 '6 111 '8 113 '8 114 '5 115 '4 115 '8 116 '0 116 '6 116 '8	Sc. Div. 117'4 117'5 116'6 115'5 115'4 113'7 113'6 113'4 113'4 112'5 112'2	sc. Div. 112 '2 112 '4 111 '8 111 '9 111 '5 111 '5 111 '4 110 '7 111 '4 113 '5	Sc. Div. 112.5 113.4 113.6 112.5 112.4 112.8 111.4 111.2 110.6 111.6 110.7 112.5	Sc. Div. 112*4 112*6 113*4 113*3 112*8 114*8 116*0 115*5 115*8 115*8 115*4 117*0	Sc. Div. 118 '2 118 '2 118 '4 116 '8 116 '1 116 '0 117 '8 119 '4 119 '2 119 '0 117 '3	118 119 111 12 12 12 12: 12: 12: 12:	Div. S'3 9'4 7'6 1'4 1'6 9'4 4'0 2'0 3'4 1'0 9'4 8'6	Sc. Div. 117.6 116.0 115.6 114.0 113.4 113.3 114.0 112.9 112.5 112.1	Sc. Div. 110°6 109°4 111°1 111°4 110°8 112°2 111°5 111°5 111°9 111°5 111°5	Sc. Div. 111'0 110'4 109'5 109'6 110'2 109'4 109'4 109'6 108'6 108'6 108'6 107'8 107'4	Sc. Div. 107 *6 107 *8 107 *4 106 *4 106 *4 105 *8 105 *4 105 *0 104 *6 103 *8 103 *4	sc. Div. 103 '8 104 '1 104 '3 105 '2 105 '3 105 '3 105 '8 105 '4 104 '0 103 '4 103 '3	sc. Div. 103 '2 103 '0 102 '7 102 '9 103 '3 103 '4 104 '3 104 '2 104 '4 104 '6 104 '2 104 '6
	·	Horizont	AL FORCE	:.	<u></u>	Increas	se, in S	Scale Divis	ions, correspo	onding to 1°	decrease of	Temperatur	re, 1.63.
646°8 651°8 650°2 650°2 650°2 650°2 650°0 650°0 646°8 647°2 647°8	649 '8 650 '2 649 '8 650 '4 649 '0 650 '0 648 '7 650 '0 647 '3 646 '0 647 '4 646 '0	646.0 643.5 645.8 648.0 646.9 646.8 645.5 644.2 645.0 646.2 643.2 643.1	643°3 641°0 641°2 643°1 644°0 643°2 643°2 640°0 643°1 639°8 645°0 645°0	640.0 645.0 644.0 644.0 643.0 645.0 646.8 646.8 647.0 646.2 645.0 645.0	646 0 645 8 646 0 647 5 648 0 645 0 645 0 646 0 646 4 644 0 641 2	642 641 639 641 644 645 647 643 642 645 641 639	· 2 · 7 · 5 · 2 · 0 · 5 · 5 · 5 · 0	639 ° 0 638 ° 0 636 ° 5 637 ° 0 635 ° 5 634 ° 0 631 ° 2 629 ° 0 631 ° 0 630 ° 0 627 ° 5 628 ° 0	627.0 623.0 622.0 619.5 618.5 620.0 621.0 622.0 623.0 623.5 625.0 627.0	628.5 630.0 628.0 629.0 632.0 631.0 632.8 632.8 633.0 634.2 635.0 636.2	633 · 2 635 · 8 637 · 4 634 · 8 636 · 2 636 · 8 637 · 0 638 · 2 639 · 0 638 · 2 639 · 0 638 · 0	638·2 635·0 636·0 634·0 634·1 633·7 632·9 633·0 640·2 642·0 644·1	642.0 640.0 639.0 637.6 639.1 634.0 633.9 631.4 634.0 630.1 628.0
		VERTICAL ]				1			ions, correspo		l	1	<u> </u>
180 '8 181 '5 181 '5 181 '2 181 '2 180 '9 180 '9 180 '9 180 '8 180 '8 181 '2 181 '2	183°3 184°8 185°0 185°6 185°6 185°6 185°6 185°6 185°6 185°6 185°4	185.0 184.0 184.4 185.0 185.0 185.0 185.0 185.0 185.0 185.6 185.6	186.9 186.7 186.5 186.5 186.5 186.5 187.0 187.0 187.0 187.0 186.7	186'7 185'0 185'0 185'0 185'0 185'0 185'2 185'2 185'2 185'0 185'4	185.4 185.4 185.4 185.5 185.5 185.5 185.5 185.5 185.5 185.5	186   187   187   187   187   187   187   186   186	'3 '1 '1 '6 '6 '6 '6 '6 '1 '3 '3 '3	186°3 186°3 186°3 186°3 186°3 186°3 186°3 186°3 185°9 185°9 185°9	185°9 185°9 185°9 185°9 185°9 186°0 186°0 186°3 186°6 186°6	186.6 186.6 186.6 186.6 186.3 186.3 185.5 185.5 185.5 185.5	185.5 185.5 185.5 185.2 185.2 185.2 185.2 185.2 184.8 184.9 184.8	184'5 184'3 184'1 183'3 183'3 183'3 182'4 182'4 182'4 184'2 184'2 184'2	184.2 184.2 183.9 184.0 183.1 182.4 182.4 182.4 182.4 182.2 181.5
4ΰ5	4ΰ5	42°3	42.9	43.5	43.0	$4\mathring{3}$	.1	43°4	44.4	44.7	44°8	45°3	46°5°
and increa	sing Horizon	ntal and <b>V</b> ert	ical Force.										
	,				TEOROLO			SERVAT	TIONS.				
Mean G Tir	öttingen ne.	Barometer at 32°.	Ther.	wet.	Direct		ind.	orce.			Weather.		
19 2 2 20 4		In. 29.825 29.814 29.822 29.811 29.820 29.825 29.829 29.811 29.776 29.758 29.723 29.705	27.9 29.2 29.7 30.2 30.4 33.5 36.0 37.6 38.5 38.8 40.6 41.9	24'9 26'1 26'6 27'1 27'3 29'5 31'9 32'2 32'9 33'6 35'5 37'0	24 '9 S.W. by S. Very lig 26 '1 S.W. by S. Very lig 27 '1 S.S.W. Very lig 27 '3 S. by W. 29 '5 S. by W. Light. 31 '9 S. by W. Light. 32 '2 S. by W. 33 '6 S. by W. Very lig 35 '5 S. by W. Very lig 35 '5 S. by W. Very lig 35 '5 Very lig Yery lig Yery lig 35 '5 Very lig Yery lig Yery lig			y light. y light. y light. y light. y light. ight. ight. ight. ight. y light. r light.	Circum, and Circum, and Mostly clear and un Clear and un Cirstrat. and Cirstrat. and Clear and un Clear and un Clear. Clear. Clear.	nd cirstrat. c. nclouded. nclouded. nd haze. nd circum. nclouded.			

Vol. III.

February 25th and	1 26th.		]	MAGNETI	CAL OB	SERVATIO	NS.							
Mean Göttingen	Angu	lar Value of	one Scale I	Division =	0′ 721.			-	DECLINATI	on.				
Time.	10h.	11h.	12h.	13h.	14h.	15h.	16 ^h .	17 ^h .	18h.	19 ^h .	20h.			
м. s.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.			
0 0	112.4	117.3	121.0	112.4	115.4	120.8	119.8	116.2	115.6	116.4	115.8			
5 0	113.6	117.2	125.6	112.6	115.8	127.4	120'4	116.7	115.4	116.3	116.0			
10 0	114.2	117.2	137.6	112.6	116.2	129.5	121.0	117.3	115.3	116.3	116.0			
15 0	114.5	117.4	143.7	112.6	115.6	133.4	120.4	117.5	115.4	116.4	117.4			
20 0	114.6	118.6	139.2	113.0	115.5	132.4	117.4	117.4	116.3	116.3	116.0			
25 0	114.4	119.4	134.5	112.4	115.4	127.2	115.2	116.7	117.1	115.9	116.2			
30 0	114'4	119.4	127.0	113.4	115.8	119.8	114'8	116.8	117.3	115.9	116.4			
35 0	114.2	119.2	121.0	114'0	118.4	118.2	114'8	116'6	116.7	115.9	116.5			
40 0	114.7	119.4	118.6	114.4	119.2	119.2	115.4	116.2	117.5	115.8	116.8			
45 0	116.4	119.1	117.4	114.8	120.4	120.4	116.8	116.4	118.9	116.0	117.0			
50 0	116.2	119.4	115.6	115.4	118.6	121.5	117.2	116.6	117.3	115.9	117.2			
55 0	117.4	118.4	112.8	115.4	118.8	119.4	116.6	116.7	116.7	115.4	117.2			
	One S	cale Divisio	n = .0000	987 parts of	the H. F.			]	Horizont	L Force.				
M. S.	634.0	621.0	619.0	632.0	636.2	696.0	621.4	624.0	626.9	633.1	632.0			
$\begin{array}{ccc} 2 & 0 \\ 7 & 0 \end{array}$	634.0	631.0				626.2	631.4	634.2	636.3		635°0			
7 0	635.0	631.0	619 <b>°</b> 0 626 <b>°</b> 5	631.4	637.8	629.3	631.0	635.0						
12 0	631.5	630.0		631.8	637.5	630.8	633.0	636.0	634.2		634.0			
17 0	631.5	629.0	638.0	632.0	638.0	636.6	636.2	635.6	633.8	635.0	636.0			
22 0	634.0	629.5	641.0	631.8	634.2	641.2	637.3	635.0	635.0	634.0	635.8			
27 0	630.0	630.0	642.2	631.8	633.8	641.2	636.0	634.3	634.0	634.0	636.0			
32 0	633.0	628.0	639.0	632.0	628.8	641.2	634.0	634.0	633.8	635.0	636.4			
37 0	633.2	628.0	639.0	631.8	626.2	634.2	633.0	634.0	633.0	634.8	636.5			
42 0	632.8	629.0	633.0	632.8	626.0	632.2	632.8	633.9	632.0	635.0	637.0			
47 0	632.0	626.0	634.2	633.0	628.2	630.8	634.0	634.0	634.1	636.8	637.2			
52 0	632.0	625.0	636.9	633.8	628.8	635.0	635.2	635.9	634.2	635.0	637.2			
57 0	631.0	623.0	633.2	634.8	628.0	632.8	635.0	636.8	633.8	635.0	637.0			
Thermometer	45°0	45°2	45°0	45°5	46°6	46.6	46.3	45.2	45°7	45.7	45°6			
	One S	Scale Divisio	n = '0000	63 parts of	the V.F.				VERTICAL	Force.				
M. S. 3 O	190.7	189.7	189.1	182.8	181.6	180.6	178.4	180.6	182.1	181.4	181.4			
8 0	190.7	189.5	189.8	182.8	181.3	180.6	178.4	180.6	181.4	181.4	181.4			
13 0	189.3	189.2	189.2	183.1	181.1	180.3	178.9	180.6	181.4	181.4	181.4			
18 0	189.3	188.8	187.3	183.1	180.9	180.3	179.3	180.6	181.4	181.4	181.4			
23 0	189.3	188.8	185.3	182.7	180.8	179.9	179.3	181.6	181.4	181.4	181.4			
28 0	188.0	188.8	183.8	182.7	180.7	179.7	179.3	181.6	181.4	181.4	181.4			
33 0	188.0	188.8	184.4	182.0	180.2	179.7	178.8	181.6	181.4	181.2	181.4			
38 0	188.6	188.8	183.7	181.5	180.6	179.7	179.3	181.7	181.4	181.2	181.4			
43 0	189.7	188.8	183.7	181.2	180.3	177.8	179.3	181.7	181.4	181.2	181.4			
48 0	189.7	188.8	185.0	181.3	180.3	177.8	179.3	182.4	181.4	181.2	181.6			
53 0	189.7	189.1	184.0	181.4	180.2	179.1	179.3	182.4	181.4	181.2	181.6			
58 0	189.7	189.1	184.5	181.3	180.6	178.4	180.6	182.4	181.4	181.2	181.6			
						_	ļ		-					
Thermometer	43.8	44.3	44.4	46.4	47.6	48.2	48.0	46.7	46.6	46.6	45°4			
							Increasing	Numbers de	note decreas	ing Westerly	Declination			
		<del></del>	M	ETEOROL	OGICAL	OBSERVAT	rions.							
Mean Göttingen	Baromete	Ther	mometers.			Wind.			v	Veather.				
Time.	at 32°.	Dry.	Wet.	Direc	ction.	For	rce.		· · · · · · · · · · · · · · · · · · ·					
D. н. м.	In.	٥	0											
25 10 <b>0</b>	30.051	23.4	20.0	8.8	.E.	$\mathbf{v}_{\mathbf{ery}}$	light.	General	lv clear					
11 0	30.031	21.2	19.3		_			Clear.	J					
12 0	30.050	19.2	18.1		_	-	_	Clear.						
13 0	30.030	19.1	17.9		_			Clear.						
14 0	30.028	17.6		_	_	10.00	_	Clear.						
15 0	30.012	16.0		_	_		_	Clear.						
	30.012	15.2		_	_		<del></del>	Clear.						
	30.005	16.0		_	_			Clear.						
16 O				- 1	1		_	Clear.						
16 O 17 O		18.1	16.3		'									
16 0 17 0 18 0	29.991	18.1	16.2 14.8	-		_	_	4						
16 0 17 0 18 0 19 0	29 991 29 985	15.1	14.8		-	-	- -	Clear. Clear.						
16 0 17 0 18 0	29.991		14.8 14.6	S.E.	by S.	- Very	- - light.	Clear.						

^a At 26^d 10^h, Thermometer of H.F., 47° '6; of V.F., 47° '4.

					MAGNET	ICAL	OBS	ERVATIO	NS.		Feb	ruary 25th	and 26th.
		DECLINATIO	ON.						Л	ngular Value	of one Scale	Division =	= 0' 721.
21h.	22h.	23h.	Oh.	1h.	2h.	3	h.	4h.	5h.	6h.	7 ^h .	8h.	9 ^h .
sc. Div. 116'8 117'2 117'0 117'0 116'8 116'8 117'4 117'4	sc. Div. 116'8 117'4 116'6 116'4 117'4 116'6 116'6	sc. Div. 117 ' 4 117 ' 4 117 ' 5 117 ' 6 117 ' 4 117 ' 4 117 ' 4 117 ' 0	sc. Div. 118 * 5 118 * 4 118 * 3 118 * 2 118 * 0 118 * 2 118 * 4 117 * 8	sc. Div. 119°0 119°0 120°3 120°7 120°4 121°4 120°4 121°5	Sc. Div. 122 ' 3 124 ' 2 125 ' 2 125 ' 1 124 ' 4 125 ' 4 124 ' 9 126 ' 2	Sc. 1 125 126 126 126 126 127 127 127	·4 ·4 ·2 ·2 ·0 ·5	sc. Div. 126 ' 4 126 ' 4 127 ' 4 129 ' 4 129 ' 8 128 ' 6 125 ' 2 123 ' 4	se, Div. 121'8 122'4 122'4 122'9 123'6 124'6 123'4	sc. Div. 120°0 118°6 118°4 118°9 118°7 117°4 117°2 116°4	Sc. Div. 115 '4 115 '0 115 '4 115 '8 114 '5 114 '4 114 '4 115 '4	sc. Div. 114 '0 113 '4 113 '0 113 '0 112 '3 112 '2 112 '4 112 '4	sc. Div. 111*2 111*0 111*0 111*0 111*4 111*9 111*9 111*6
118 · 4 118 · 0 117 · 4 117 · 2	117.0 117.2 116.0 116.4	116.0 115.4 117.6 118.0	118.6 117.0 119.0 120.4	121.6 121.4 122.5 122.5	127 · 4 126 · 6 127 · 9 126 · 4	127 127 126 126	·5 ·4 ·2 ·4	122.6 122.4 122.4 122.5	121.1 121.4 120.3 120.4	116°5 116°4 116°0 115°8	115.0 114.6 114.3 113.9	112.0 111.6 111.4 111.3	111.9 111.4 111.6 112.2
	1	Horizonta	L FORCE.			1		Scale Divisio		onding to 1°	decrease of	1	
636 ° 0 636 ° 0 636 ° 4 637 ° 0 636 ° 9 635 ° 0 634 ° 8 636 ° 0 635 ° 8 639 ° 0 639 ° 2 639 ° 0	637 · 5 637 · 0 638 · 0 638 · 0 638 · 0 638 · 0 638 · 0 639 · 0 639 · 0 642 · 0 641 · 0	640.0 640.0 640.0 640.0 642.2 642.0 642.5 643.0 644.0 642.5 642.5	645.5 644.0 641.0 641.0 641.5 643.5 644.0 642.5 641.5 640.0 641.0 642.5	647.0 644.0 644.0 645.0 644.0 642.8 644.0 645.0 644.0 644.0 646.0	643.0 645.5 645.0 645.0 645.0 646.0 644.3 641.0 643.5 644.0 641.0	639 640 638 638 637 636 635 634 635 634 631	·4 ·8 ·8 ·8 ·0 ·5 ·4 ·2 ·0	630°0 630°0 626°4 623°0 620°3 617°8 619°5 617°8 620°2 621°6 621°8	624 ° 0 620 ° 8 620 ° 8 618 ° 5 617 ° 4 615 ° 8 615 ° 0 616 ° 2 616 ° 2 613 ° 7 614 ° 1 613 ° 3	611'3 608'0 611'8 610'0 612'2 612'0 612'0 612'0 610'0 607'0 611'0 612'2	614.0 611.0 611.0 610.0 611.0 613.8 614.0 613.0 614.5 618.0 616.5 615.0	618.0 618.0 618.0 620.0 620.5 622.0 620.0 620.5 622.0 623.0 625.0	623 ° 0 628 ° 0 628 ° 0 626 ° 5 627 ° 0 626 ° 5 626 ° 5 630 ° 0 626 ° 0 626 ° 0
44.2	43.8	43.5	43°3	42°7	43°5	45°	·2	46°1	4Ĝ·1	45.9	46.0	46.3	46.7ª
		VERTICAL 1	Force.	<u>'</u>	I	ncreaso	e, in S	scale Divisio	ons, corresp	onding to 1°	decrease of	Temperatui	re, 1.64.
181.6 181.6 181.6 181.6 181.6 181.6 181.6 181.6 181.6 181.6	181 4 181 4 181 4 182 5 182 5 182 5 182 5 182 5 182 5 182 5 182 3 182 3 181 0	180.6 180.6 180.6 179.5 179.5 179.5 179.5 179.5 179.5 178.7 178.5 178.5	184.5 184.5 184.5 184.5 185.5 185.5 185.5 184.8 179.5 182.0 182.0	183.5 183.5 184.9 184.9 184.9 185.5 185.5 186.1 186.2 186.2 186.2	186 1 186 1 186 1 186 1 184 9 184 8 184 4 184 5 184 5 185 0 184 4 183 3	181 181 180 180 180 180 179 179 179 177	·8 ·8 ·7 ·4 ·3 ·7 ·3 ·2 ·2	177'9 177'9 177'8 177'8 177'8 177'8 177'7 179'7 180'6 180'6 180'6	180.6 179.5 179.3 179.3 179.3 179.3 179.3 180.9 181.5 181.5 181.5	181·5 181·5 181·5 181·0 181·0 181·1 181·1 181·0 181·0 181·0	180.9 181.1 181.1 181.1 181.1 181.1 181.1 181.1 182.6 183.4 183.4	183.4 183.4 183.4 183.4 183.4 183.4 183.4 183.4 183.4 181.8 181.8	180.9 180.9 180.9 180.9 180.9 180.9 180.9 180.9 180.9 180.9
45.4	45.5	46.4	46°4	44.3	44°0	46	.3	46°2	46°5	46.3	46°4	46°4	47°1 a
and increa	sing Horizo	ntal and Vert	tical Force.										
				ME	TEOROLO	OGICA	T 01	BSERVAT	IONS.				
	öttingen me.	Barometer at 32°.	Thern Dry.	wet.	Direct		Wind	Force.			Weath	er.	
25 2 26		In. 29.949 29.926 29.918 29.920 29.902 29.883 29.852 29.827 29.789 29.744 29.656	31.1 31.8 33.5 34.3 34.3	0 13.5 12.7 12.4 12.3 18.1 24.1 27.0 26.7 27.0 27.7 29.3 29.6	S.E. by S.E. by S.E. by S.E. by S.W. by S.W. S.W. S.W. S.S.V S.S.V	y E. y E. y E. y S. V.	Vo Vo Vo	ery light. ery light. ery light. ery light. Light. Light. Light. Light. ery light.	Calm Gene Gene Gene Gene Clear Clear Clear	Calm. Calm. Generally clear. Generally clear. Generally clear. Generally clear. Generally clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear. Clear.			

March 22nd and 2	23rd.			MAGNE	FICAL C	BSERVATIO	ONS.		MAGNETICAL OBSERVATIONS.								
Mean Göttingen	Angula	ar Value of	one Scale D	ivision =	0′′721.				DECLINAT	TION.							
Time.	10h.	11h.	12h.	13h.	14h.	15h.	16 ^h .	17h.	18h.	19h.	20h.						
M. s. O O 5 O	Sc. Div. 107.8 108.0	Sc. Div. 109 0 107 8	Sc. Div. 110'4 110'6	Sc. Div. 109 3 108 5	Sc. Div 114 6 115 4	115.5	Sc. Div. 116.4 115.8	Sc. Div. 114.4 114.7	Sc. Div. 116 9 117 6	Sc. Div. 117.6 117.4	Sc. Div. 116'6 116'6						
10 0	108.4	107.4	109.8	110.4	115.8	116.3	117.0	116.4	117.5	117.2	116.4						
15 0	108.3	107.2	110.0	110.4	116.0	116.2	118.0	117.6	118.3	117.6	116.3						
$ \begin{array}{ccc} 20 & 0 \\ 25 & 0 \end{array} $	108'8 108'4	108.3 108.7	109.4 109.4	111'8 113'4	117.7 116.2		117.7 115.7	117.6	118.4	117°2 116°9	116.0						
30 0	108.3	109.4	110.1	113 4	115.4	119.7	114.0	116.0	119.4	116.9	116.0						
3 <b>5</b> 0	107.7	108.8	111.3	116.0	115.8	119.0	115.0	117.6	119.4	116.6	115.4						
40 0	107.6	109.4	111.3	117.4	116.4		115.8	117.4	118.4	116.9	117.2						
$ \begin{array}{ccc} 45 & 0 \\ 50 & 0 \end{array} $	109°2	108.7 108.6	110.6	117°5 117°5	115 <b>.</b> 9	114.4 114.4	115.4 115.6	117'0 116'4	117.4 117.6	116.6	116.4 116.3						
55 0	109.2	108.9	109.5	114.2	114.0		115.9	116.4	117.8	116.2	116.3						
м. s.	One S	Scale Divisi	on = '000	087 parts c	of the H. 1	Ŧ.			Horizon	TAL FORCE	Ξ.						
2 0	633.0	638.8	625.0	622*4	617.0		628.0	625.0	633.6	630.3	632.0						
7 0	633.8	640*8	626.0	620.8	617.2	622.0	626.2	624.5	633.0	630.0	632.1						
$\begin{array}{ccc} 12 & 0 \\ 17 & 0 \end{array}$	636.2	642.9	626'0	620.5	618.0		626.0	623.5									
$\begin{bmatrix} 17 & 0 \\ 22 & 0 \end{bmatrix}$	635.6	$642.0 \\ 638.2$	622°1 620°1	620°0 620°5	614.8	626.4	627.8	626°0 635°2	632.0	633.8	633.9						
27 0	638.9	637.0	618.8	620.4	612.8	$\frac{620.8}{627.0}$	630.0	637.0	628.5	633.0	634.0						
32 - 0	641.7	633.0	616.0	620.0	615.4	627.2	626.8	633.5	629.1	633.0	636.0						
37 0	641'3	631.4	617.0	620.0	617.0	630.0	625.0	635.4	631.0	633.0	633.0						
42 0	640.0	629.7	617.0	620.0	618.8	630.8	626.0	634.8	632.0	633.2	632.9						
$\begin{array}{ccc} 47 & 0 \\ 52 & 0 \end{array}$	636.1	$629.1 \\ 624.3$	618.3	620.2	621.0	628.0 626.4	627.0	635.0	631.6	633.2	633.1						
57 0	636.1	621.0	620.0	622°4 623°0	621.4 621.2	626.5	626.0	633.8 634.8	630.0 630.0	632.8 632.0	633°1 633°1						
Thermometer	5Î.6	5 <u>1</u> .9	51.6	5 <u>1</u> .1	50°6	50°5	50°·5	50°·6	50°.7	5 <b>1</b> °5	52.4						
M. S.	One S	cale Divisio	on = .0000	063 parts o	f the V. F	`.			VERTICAL	Force.	·						
3 0	175.2	175.5	174.7	173.8	173.3	173.1	173.2	171.7	166.9	166.2	164.7						
8 0	175.7	175.5	174.7	173.8	173.3	173.1	173.0	171.9	166.9	166.2	164.7						
13 0	175.8	175.5	175.5	173.8	173.2	173.1	170.5	171.9	166.9	166.3	164.0						
$\begin{array}{ccc} 18 & 0 \\ 23 & 0 \end{array}$	175.7	175.5	175.5	173.7	173.2	173.0	170.5	172.7	166.9	166.3	164.1						
$\begin{bmatrix} 23 & 0 \\ 28 & 0 \end{bmatrix}$	176°0 176°0	175°5 174°8	175 <b>·</b> 2 175 <b>·</b> 2	$173.7 \\ 173.7$	173°5 173°5	$\begin{array}{c c} 173.0 \\ 173.2 \end{array}$	170°5 170°4	172 <b>'</b> 9 169 <b>'</b> 4	166 <b>·</b> 9	166°3 165°5	164°1 164°1						
33 0	176.0	174.6	174.5	173.7	173.2	173.2	170.2	169 4	166.9	165.8	164.0						
38 0	176.0	174.6	174.5	173.5	173*3	172.5	170.2	166.9	166.9	165.8	164.0						
43 0	175.3	174.6	174.5	173.3	173.3	172.3	171.7	166.9	166.5	165.6	165.0						
48 0	174.5	174.6	174.5	173.3	173.8	172.3	171.7	166.9	166.5	165.4	165.0						
$\begin{array}{ccc} 53 & 0 \\ 58 & 0 \end{array}$	174°5   174°5	174.6 173.8	174°5 174°5	173°3 173°3	173°8 173°8	172°3 172°3	171.7 171.7	166 <b>·</b> 9	$\begin{array}{c} 166^{\boldsymbol{\cdot}}2\\ 166^{\boldsymbol{\cdot}}2\end{array}$	164.6 164.6	$\begin{array}{c} 165.0 \\ 165.0 \end{array}$						
		<del></del>		· · · · · · · · · · · · · · · · · · ·													
Thermometer	50°·8	51°3	5 <b>ì</b> °1	52.0	51°6	52.2	52.5	5 <b>ì</b> 9	52°0	53.0	54°2						
								Jumbers den	ote decreasi	ng Westerly	Declination,						
.1			<del></del>	TEOROLO		OBSERVATI	ions.										
Mean Göttingen Time.	Barometer at 32°.	Dry.	wet.	Direc	Win	Force.	_		Weather	·.							
		_	_				-										
D. н. м. 22 10 0	In. 29:653	97.1	99.6				Claudel	Clared all air annual a									
11 0	29 633	37.1	33.6	-	_		Clouded; circum. and cumstrat. Clouded.										
12 0	29.619	34.9	32.1	-	_		Clouded.										
13 0	29.617	33.8	31.3	-	- [		Clouded.										
14 0	29.616	32.8	31.1	-	-		Cireum. and cumstrat.										
15 0 16 0	29.654 29.664	32.9 32.4	30.3	-	-	_		. and cirstr									
	29.666	32.7	30.5		_	_	1										
17 0				1			Circum. and cirstrat. Circum. and cirstrat.										
18 0	29.666	32.7	30.3	_	-		Circum. and cirstrat.  Circum. and cirstrat.										
18 0 19 0	29.670	33.1	30.4	_	-		Circum	. and cirst	rat.								
18 0					-	_	Circum		rat.								

^{*} At 23d 10h, Thermometer of H. F., 53° '6; of V. F., 53° '0.

					MAGNE	FICAL OI	BSERVATIO	ons.				March 22nd	l and 23rd.
		DECLINAT	TION.						Ar	ngular Value	of one Scal	le Division =	= 0' 721.
21 ^h .	22h.	23h.	O ⁿ .	1 ^h .	2 ^h .	3 ^h .	4 ^h .		5 ^h .	6 ^h .	7 ^h .	8 ^h .	9h.
sc. Div. 115'8 115'9 116'4 116'4 116'4 116'4 116'4 116'6 117'0 117'2 117'2	Sc. Div. 117.2 117.3 117.3 117.4 117.6 117.4 117.7 118.0 117.6 116.4	sc. Div. 117'4 118'4 119'2 119'0 118'6 118'2 118'4 118'4 118'8 118'8	sc. Div. 119 '4 119 '6 120 '2 120 '4 120 '4 120 '6 121 '0 121 '8 121 '2 121 '6 121 '8 122 '2	sc. Div. 122*4 123*2 123*1 123*3 123*5 123*6 124*3 125*3 125*4 125*5 126*1	Sc. Div. 125 * 5 125 * 4 123 * 7 124 * 4 126 * 3 126 * 6 126 * 7 126 * 4 124 * 7 123 * 4	sc. Div. 123 '6 123 '4 123 '4 122 '5 122 '4 123 '4 123 '4 122 '8 123 '0 123 '4 122 '4	Sc. Div. 121 '5 121 '4 121 '5 121 '5 121 '5 121 '4 120 '8 120 '0 120 '2 118 '5 118 '4 117 '7	11'	3.5 1.0 1.0 3.0 3.0 2.9	Sc. Div. 112.4 111.6 110.6 110.4 110.0 109.0 108.6 108.2 107.8 107.6 106.6	Sc. Div. 106 ' 4 105 ' 7 105 ' 6 105 ' 4 105 ' 4 105 ' 5 105 ' 5 105 ' 5 105 ' 5 105 ' 5 104 ' 3 104 ' 3 103 ' 7	Sc. Div. 103 ° 6 103 ° 0 102 ° 4 102 ° 2 102 ° 2 102 ° 2 102 ° 6 102 ° 6 103 ° 0 104 ° 0 104 ° 0	Sc. Div. 104'6 105'2 105'6 106'0 106'4 106'4 106'4 106'8 107'2 107'6 108'2 108'4
111 2	110 1	Horizont.	1			1	Scale Division	1			<u> </u>	ł .	ļ <u>.</u>
633 ° 0 632 ° 2 631 ° 5 632 ° 0 631 ° 9 632 ° 0 632 ° 0 633 ° 0 633 ° 0 633 ° 0 632 ° 8	633 ° 0 633 ° 0 633 ° 0 633 ° 0 632 ° 2 632 ° 4 632 ° 4 632 ° 0 633 ° 2 634 ° 0 636 ° 0 634 ° 2	633.0 632.8 631.8 632.0 632.4 633.0 633.4 634.2 634.2 634.0 634.0 634.5	635.5 634.8 633.4 632.8 633.2 632.5 632.2 632.0 632.2 632.4 632.0 631.8	631'4 631'2 630'9 631'0 630'6 630'3 630'0 630'1 629'2 628'3 627'4 625'0	626*8 626*4 628*3 626*2 625*0 623*5 622*3 621*6 620*2 620*0 622*0 622*0	623 ° 0 623 ° 0 622 ° 0 622 ° 0 622 ° 0 618 ° 0 617 ° 8 618 ° 0 615 ° 6 615 ° 0 614 ° 0	613.0 612.0 611.8 611.0 611.5 610.0 610.8 611.5 611.0 610.0 610.5 613.0	610 610 609 609 608 608 607 607 607	·0 ·0 ·2 ·5 ·0 ·6 ·5 ·8 ·5 ·0	609.6 609.0 609.0 608.5 608.4 608.7 608.7 609.0 609.6 610.0 611.6 612.0	612.6 615.0 617.0 616.2 619.9 623.0 625.0 623.0 622.1 619.1 618.0 617.3	619.0 619.2 624.4 623.2 622.2 619.8 618.2 616.8 617.0 617.2 617.2 616.5	615.8 617.4 615.8 618.8 621.2 624.4 624.8 624.4 626.8 629.0 631.0 631.2
52.9	53.1	53.2	53°6	52°·8	52°0	5η5	52.1	52	•7	52.9	53.0	52°5	52°6°
		VERTICAL	Force.		In	crease, in S	Scale Division	ıs, cor	respoi	nding to 1°	decrease of	Temperature	e, 1°64.
165.0 165.0 165.0 165.4 165.4 165.4 165.4 165.4 165.4 165.4 164.9	164.9 164.9 164.9 164.8 164.8 164.8 164.8 164.6 164.6 164.6	164.4 164.3 164.4 165.0 165.0 165.0 165.0 165.0 165.0 165.0 165.0 165.0	165.0 165.4 165.3 165.3 165.6 167.0 167.0 167.5 168.4 168.4 168.7	170°3   170°3   169°3   169°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3   170°3	171 1 171 1 171 1 171 1 171 1 171 1 171 1 171 1 171 1 172 3 172 0 172 0 172 0 172 0	172.0 172.0 172.0 173.0 173.0 173.0 173.0 173.0 173.0 173.0 173.0 173.0	173.0 172.5 172.5 172.5 172.5 172.0 172.0 172.0 171.0 171.0 171.0	171 171 170 170 170 170 169 169 169 169	0 0 4 4 4 5 5 5 5 5 5	169°5 169°5 169°5 169°5 169°5 169°5 169°6 169°6 169°6 169°6 170°1	170°6 170°6 170°6 171°4 171°4 171°4 171°4 171°4 171°4 171°4 171°4 171°4	171'4 171'4 171'7 171'1 170'9 170'9 170'9 170'9 170'3 169'6 169'6	168:5 168:5 169:4 169:4 170:3 170:3 170:3 168:2 167:7 168:7 169:3 168:9
54°·2	54.2	54.4	5å·4	53.4	52°2	5η5	51.8	52°	2	52°·8	52°·8	52°4	52°2ª
and increas	sing Horizo	ntal and Vert	ical Force.	1						,			
				MET	reorolo	GICAL O	BSERVATI	ons.					
Mean Gö Tim		Barometer at 32°.		nometers.		Wi					Weath	ier.	
D. H. 22 22 23 23 0 1 2 2 3 4 5 6 7 8 9	M. 2: 0	In. 29.691 29.708 29.734 29.756 29.778 29.782 29.802 29.792 29.827 29.828 29.806 29.808	Dry.  33.4 33.7 33.7 33.7 33.9 34.7 35.1 37.8 39.4 40.2 41.2 39.5 40.2	wet.  30.7 30.6 30.7 30.7 30.7 30.7 31.3 33.1 33.4 36.1 36.9 35.5 36.1	GO'7 N. by E. Very light. GO'7 N. by E. Very light. GO'7 N. by E. Very light. GO'7 N. by E. Very light. GO'7 N. by E. Very light. GO'7 N. by E. Very light. GO'8 N. by E. Very light. GO'9 E. Very light. GO'9 E. Light. GO'9 E. Light. GO'9 C. Clouded. Clouded. Clouded. Clouded. Clouded. Clouded. Clouded. Clouded. Clouded. Clouded. Clear and unclouded.			ainder clear.					

April 19th and 20	)th.			MAGNET	ICAL OBS	SERVATIO	NS.	· · · · · · · · · · · · · · · · · · ·			
Mean Göttingen	Angul	ar Value of	one Scale 1	Division =	0′′721.				DECLINAT	ion.	
Time.	10h.	11 ^h .	12 ^h .	13h.	14h.	15h.	16h.	17h.	18h.	19h.	20h.
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
0 0	111.2	113.2	113.8	114.4	115.6	116.3	116.6	117.4	119.0	119.9	118.2
5 0	111.4	113.8	113.8	114.5	115.5	115.7	116.7	117.4	119.2	119.6	117.8
10 0	111.8	114.2	113.4	114.3	115.6	116.0	117.3	117.4	119.8	119.8	118.2
15 0	112.2	114.4 114.0	113 <b>.</b> 4 113 <b>.</b> 4	114.7 115.3	116°3 116°4	116.4 116.4	116.7	117.6 117.6	120.5	119.8	118.2
$egin{array}{ccc} 20 & 0 \ 25 & 0 \end{array}$	112.4	114.0	113.4	115.2	116.4	115.4	117.0	117.6	120.0	119.2	118.2
30 0	112.4	114.4	113.4	115.5	115.2	115.6	117.4	117.7	120.5	119.7	118.4
35 O	112.6 112.8	113.4	113.4	115.7	115.2	115.5	117.4	117.8	120.0 119.4	118.6 118.4	118.0
40 0	113.5	113.4	113.4	115.7	115.2	116.4	117.4	118.0	119.4		118.2
45 0	113.2	114.5	114.5	115.7	115.2	116.4	117.3	118.0	120.6	118.4 118.2	117*9 118*0
50 0	112.8	113.4	114.2	116.2	115.8	116.2	117.3	118.4	119.6	118.4	118.4
55 0	113.4	113.4	114.4	115.8	116.0	116.9	117.4	118.4	119.4	118.2	118.4
	One S	cale Divisio	ou = .0000	087 parts of	the H. F.		1	1	Horizon	TAL FORCE	1
M. S.						626.0	626:1	696.0	1	1	
$\begin{array}{ccc} 2 & 0 \\ 7 & 0 \end{array}$	642.4	645°0 643°2	640°2 639°8	631.9 632.2	636.0	636.0	636°1	636.9	637.0	639.0	638.5
7 0	643.8 646.4	$643.2 \\ 642.1$	640°0	632.2	636.0	635.0	636 3	637.0	637.1	638.5	638.5
12 0 17 0	647.1	642 1	639.8	633.0	636.0	636.0	637.0	637°0 637°0	638.0	638.0	638.0
$\begin{array}{ccc} 17 & 0 \\ 22 & 0 \end{array}$	649.8	643.0	638.8	633.1	636.0	637.0	636.0	636.0	639.6	637.8	638.0
27 0 27 0	649.5	642.8	639.2	634.0	636.8	636.2	636.0	635.9	639.6	637.8	638°0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	650.0	642.0	638.6	633.4	636.2	636.0	636.0	636.0	639.4	637.8	637.8
37 0	650.0	641.8	637.8	634.0	636.0	636.3	636.2	636.0	640.0	638.0	638.0
42 0	647.8	641.4	634.4	634.0	636.0	636.1	635.8	636.0	640.6	638.2	638.0
47 0	646.8	641.2	635.0	634.1	635.0	636.8	635.6	636.0	641.0	638.3	638.0
52 0	645.0	642.2	633.2	635.0	635.0	636.8	635.2	636.4	641.0	638.0	638.0
57 O	644.8	641.0	632.8	636.0	636.0	637.2	635.2	636.2	640.5	638.2	640.0
Thermometer	5i°7	5 <b>i</b> · 9		52.0	51.2	5ΰ0	50°5	49.9	49.0	48.9	48.3
	One Sc	cale Division	0000	63 parts of	the V. F	1	-	 	VERTICAL	<u> </u>	!
M. S.					1	1	1	· · · · · · · · · · · · · · · · · · ·	1	1	1
3 0	172.1	172.5	173.5	174.5	170.4	169.2	168.8	169.6	169.8	169.7	171.3
8 0	171.8	172.8	173.7	173.9	170.4	169.2	168.8	169.6	169.8	169.7	171.3
13 O	171.7	172.8	174.6	173.7	170.4	169.2	168.8	169.6	169'4	169.7	171.3
18 0	171.7	173.0	173.8	173.4	170.4	169.2	168.8	169.6	169.4	169.7	171.3
23 0	171.7	173.0	173.9	172.8	170.4	169'2	168.8	169.6	169.4	170.5	171.3
28 0	171.7	172.9	173.9	172.3	170.4	169.2	168.8	169.6	169.4	170.5	171.3
33 0	172.8	172.9	173.8	172.0	170.4	168.6	168.8	169.6	169.4	170.5	171.5
38 0	172.8	173.3	173.6	172.0	169.6	168.6	168.8	169'6	169.1	170.6	171.9
43 0	171.6	173.3	173.4	172.0	169.6	168.6	168.8	169.8	169.1	170.7	171'9
48 0	171.6	173.7	173.2	171.8	169.6	168.6	168.8	169.8	169.1	170'9	171.9
53 0	$172.3 \\ 172.7$	173.7 173.0	$173\cdot2$ $173\cdot8$	171.0 171.0	169.6	168.6 168.6	168.8 168.8	169.8	169°1	171.3	171.9
58 0	1/2/	173 0	173 8	171 0	109 6	108 0	108 8	169.8	109 1	171.3	171.9
Thermometer	50°2	5 <b>0°</b> 8	5ΰ0	5η2	52.2	52°·2	5η7	51.0	50°2	50°0	49°5
						]	Increasing 1	Numbers der	ote decreasi	ing Westerly	Declinatio
			ME	TEOROLO	GICAL O	BSERVATI	ions.				
Mean Göttingen	Barometer	Ther	mometers.		Wind		_		Weathe	_	
Time.	at 32°.	Dry.	Wet.	Direc	tion.	Force.			w eathe	er.	
р. н. м.	In.	۰	0		į						
19 10 0	30.028	38.2	33.0	S.S.	$\mathbf{v} + \mathbf{v}$	ery light.	Quite cl	ear all day.			
11 0	30.022	39.6	34.5		$\mathbf{w}$ . $\mathbf{v}$	ery light.		ear all day.			
12 0	30.013	38.6	33.7		$\mathbf{v}$ . $\mathbf{v}$	ery light.		ear all day.			
13 0	30.011	35.9	31.7	-			Calm.				
	30.011	33.0	29.4				Calm.				
14 0	30.015	34.2	30.4				Calm.				
14 0 15 0		31.2	27.5				Calm.				
14 0 15 0 16 0	30.011				t		Calm.				
14 0 15 0 16 0 17 0	30.002	27.8	26.0		·		1				
14 0 15 0 16 0 17 0 18 0	30.005 30.004	27.8 27.1	25.3			_	Calm.				
14 0 15 0 16 0 17 0 18 0 19 0	30.005 30.004 29.990	27.8 27.1 25.9	25.3 24.7	_		_	Calm. Calm.				
14 0 15 0 16 0 17 0 18 0	30.005 30.004	27.8 27.1	25.3				Calm.				

				<del></del>	MAGNE	TICAL (	OBSERVATI	ons.				April 19th	and 20th.
		DECLINAT	ION.						Λn	gular <b>V</b> alue	of one Scale	Division =	: 0' .721.
21h.	22h.	23h.	Oh.	1h.	2h.	3h	. 4h.		5h.	6h.	7h.	8h.	9 ^h .
Sc. Div. 118 '4 118 '4 118 '5 118 '5 118 '4 118 '4	Sc. Div. 119 ° 0 119 ° 2 119 ° 4 118 ° 7 117 ° 6 117 ° 0	sc. Div. 118 '3 118 '4 119 '0 119 '3 119 '5 120 '4	sc. Div. 121 '4 121 '4 121 '5 121 '6 121 '6 121 '6	sc. Div. 122 * 6 122 * 4 122 * 4 122 * 4 122 * 4 122 * 4 122 * 4	sc. Div. 122 ' 4 123 ' 2 123 ' 4 123 ' 6 123 ' 4 123 ' 4	Sc. Div 122 ' 7 122 ' 4 122 ' 4 121 ' 7 121 ' 7	7   120°4 120°4 120°0 119°4 119°1	11 11 11 11	6. Div. 7°2 6°5 6°4 6°2 5°8 4°8	sc. Div. 113 ' 9 113 ' 2 112 ' 9 113 ' 7 112 ' 4 112 ' 2	Sc. Div.   109.6   109.2   108.6   108.6   108.2   107.6	Sc. Div. 107 2 107 4 107 2 107 0 107 2 107 0	Sc. Div. 108'3 108'2 108'4 108'6 108'4 108'4
118.4 118.6 119.2 118.8 118.6 118.6	116.4 116.4 116.9 117.4 117.6 117.6	120.6 121.2 121.4 121.6 121.6	121.6 121.6 122.4 122.5 122.5 122.6	122 · 4 122 · 4 122 · 4 122 · 2 122 · 2 122 · 0	123 '4 123 '4 123 '5 123 '4 123 '4 123 '0	122°1 121°6 121°6 121°4 121°4 121°4	1 117.8 117.6 117.4 117.6 117.4	11 11 11 11	4·4 4·2 3·6 3·4 4·2 4·0	112.0 111.6 110.6 110.2 110.4 110.2	107.4 107.6 107.6 107.4 107.4	107.4 107.4 107.4 107.6 107.7 108.0	108.4 108.6 109.6 108.8 109.4 109.4
		Horizonta	L Force.		]	ncrease,	in Scale Divisi	ions, c	corresp	onding to 1°	decrease of	' Temperatu	е, 1 '63.
639 ° 0 639 ° 5 639 ° 0 639 ° 0 638 ° 9 638 ° 5 638 ° 0 638 ° 0 638 ° 1 638 ° 1	637 0 638 0 638 0 639 4 639 0 637 5 637 5 638 0 638 5 639 2 641 0 642 0	642.0 643.0 642.0 643.0 642.5 642.2 642.0 644.0 643.0 643.2 641.0	643.0 643.0 643.7 643.5 642.5 642.5 642.0 642.0 642.0 642.0	641.5 641.2 642.2 641.2 641.2 640.8 640.2 640.0 639.2 639.2 639.2	638 · 2 636 · 8 636 · 8 636 · 2 635 · 0 634 · 4 633 · 8 633 · 2 632 · 8 631 · 4 631 · 2 629 · 8	630°C 628°C 627°1 627°1 627°7 626°C 625°C 625°C 625°C 624°8 623°8	622.2 619.0 618.8 620.0 618.5 618.1 619.0 621.0 620.0 618.5	61 62 62 62 62 62 62 62 62 62 62	8.0 8.0 0.2 0.0 2.0 1.0 0.0 0.0 1.0 3.0 3.4 6.0	624 ° 0 623 ° 0 624 ° 0 625 ° 0 625 ° 0 625 ° 0 626 ° 0 626 ° 0 626 ° 5 625 ° 5	622.0 622.6 623.0 623.2 622.0 623.0 626.8 627.7 627.7 625.0 629.0	628.0 627.0 630.0 631.5 631.8 628.1 628.5 630.0 628.7 628.5 629.0 631.9	634.0 636.0 635.0 635.0 636.0 639.0 642.5 644.0 643.2 641.0 638.5 639.0
48°1	47.8	47°5	47°•4	48°0	49°•2	49.8	50°3	5	ů.0	51.4	5η8	52°4	53.0 a
	·	VERTICAL I	Force.		1	nerease, i	in Scale Divisi	ons, c	orrespo	onding to 1°	decrease of	Temperatu	re, 1.64.
171.9 171.9 171.9 171.9 171.9 171.4 171.4 171.4 171.3 171.3 171.3	171.3 171.9 171.9 171.9 171.9 171.9 172.5 172.5 172.5 172.5 172.5 172.5	172.5 172.9 172.9 172.9 172.9 172.9 173.3 173.3 173.3 173.5 175.0 175.4	175.4 175.4 175.4 175.4 175.4 175.4 174.8 174.8 174.8 174.8 174.5 174.5	173°9 173°8 173°8 173°4 173°4 173°4 173°4 173°4 171°9 171°9 171°9 171°9 172°1	171'3 171'5 171'5 170'6 170'4 170'6 170'6 170'4 170'6 169'9 169'9	169.9 169.9 169.9 170.8 170.1 170.1 170.1 170.1 170.1 170.1	169.5 169.8 169.8 169.8 169.8	16 16 16 16 16 16 16 16 16 16 16 16	9.0 9.0 9.0 9.0 9.2 9.2 9.2 9.2 9.3 9.5	169.5 169.4 169.4 169.4 169.4 169.7 169.7 169.7 169.7 170.2 170.2	169.9 169.9 169.9 169.9 169.7 169.7 169.9 169.5 169.5 169.5	169.5 169.5 169.5 169.5 169.5 168.9 168.9 168.9 168.9 168.9	169.6 169.6 169.6 169.5 169.5 170.1 170.1 169.6 169.6
49.5	49°5	49.3	48°·5	48°6	49°·8	50°2	50°·4	50	ő·7	5Ů·0	5 <u>1</u> °4	51.8	52°3 a
and increa	sing Horizo	ntal and Vert	ical Force.										
				мет	EOROLO	GICAL	OBSERVAT	IONS	3.				
Mean Go Tin		Barometer at 32°.	Therr Dry.	wet.	Direc	<del></del> -	Force.				Weath	er.	
	2 0 3 0 0 0 1 0 2 0 3 0 4 0 5 0 6 0	In. 29 '980 29 '966 29 '976 29 '974 29 '973 29 '935 29 '935 29 '904 29 '848 29 '812 29 '776 29 '730	26°3 25°0 27°6 31°8 39°1 41°0 42°5 43°8 46°9 47°9 49°1 50°4	24'1 23'6 25'4 28'2 31'9 35'1 36'7 38'1 41'5 40'9 43'8 44'7	S S. by S.S. S.S. S.S. S.S.	- - - - - 7 E. E.	Very light Very light Very light Very light Very light Very light Moderate		Clear : Clear :	all day, all day, all day, all day, all day,			

May 26th and 2	7th.			MAGNETI	CAL OBS	SERVAT	rions.				
Mean Göttingen	Angul	ar Value of	one Scale	Division = 0	7.721.				DECLINAT	HON.	
Time.	10h.	11h.	12h.	13h.	14h.	15h	. 16h.	17h.	18h.	19 ^h .	20 ^h .
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div. 114°0	Sc. Div. 112.4	Sc. Di 112		Sc. Div.	Sc. Div. 115°2	Sc. Div. 117.8	Sc. Div. 122 3
$egin{array}{ccc} 0 & 0 \ 5 & 0 \end{array}$	111.4	113.4	114.4	113.8	112.4	112.4		114.2	113 2	120.5	125.5
10 0	111.6	113.4	114.4	114.5	112.4	112.6		114.2	111.5	122.0	128.7
15 0	112.2	113.4	114.4	114.6	112.4	112.6		114.4	107.8	121.8	130.6
<b>2</b> 0 <b>0</b>	112.4	113.2	114.4	114.4	112.4	113.4		114.4	107:2	121.4	129*4
25 O	112.5	113.2	114.0	114.4	112.4	114.4		114.4	109.8	120.6	133.2
30 O	112.8	113.4	114.2	114.2	112.4	113.4		113.4	112.5	122.2	130.3
35 O 40 O	112.9 113.2	113.4 113.5	114.4	113.5 113.4	$\frac{112.6}{112.2}$	113.3		114.5	113°2 113°4	124.9 126.5	127°5 127°1
$\frac{40}{45} = 0$	113.2	113.6	114.4	113.4	112.4	114.4		112.0	113.4	$\frac{126 \cdot 3}{126 \cdot 2}$	125.4
50 0	113.3	113.6	114.4	112.4	113.4	115.6		111.4	113.2	125.2	126.1
55 0	113.4	114.3	114.0	112.4	112.4	116.4		112.6	115.3	122.6	127.6
M. S.	One S	cale Divisio	u = .000	087 parts of	the H. F.				Horizon	TAL FORCE	2•
2 0	621.0	619.0	619.0	616.0	617.2	619.0	607.0	613.2	634.5	597.8	585.0
$\begin{array}{ccc} z & 0 \\ 7 & 0 \end{array}$	621.0	620.0	618.8	615.0	619.0	619.0		614.0	629.3	598.2	587.0
12 0	619.0	620.5	618.8	615.0	619.5	620 2		615.0	626.8	598.4	585.0
17 O	620.0	620.5	618.3	615.0	619.0	620.9		614.8	625.4	600.0	580.0
$\frac{22}{2}$ 0	619.0	619.5	618.0	614.0	617.5	621 (		617.6	617.2	598.2	582.6
$\begin{array}{ccc} 27 & 0 \\ 32 & 0 \end{array}$	619.0	618.2 618.8	619.0	614.0	$616.0 \\ 616.0$	621.0		$619.0 \\ 619.2$	612.8	597°1 596°3	577.0 578.8
$\begin{array}{ccc} 32 & 0 \\ 37 & 0 \end{array}$	618.0 618.0	619.0	620.0	614.0	618.0	621.8		620.4	605.4	594.8	582.1
42  0	618.0	618.4	620.0	615.0	619.8	619.8		629.7	601.2	596.0	590.0
47 0	617.0	619.0	620.0	616.0	623.0	617.8		632.2	597.5	593.0	594.0
52 0	617.0	618.0	619.0	616.0	622.0	614		632.0	597.2	591.1	599.2
57 O	616.2	619.0	617.0	617.0	620.0	611.0	612.2	632.4	598.5	587.0	602.6
Thermometer	70.4	7 <b>0°</b> 3	70°3	69.0	68°1	67.8	67°2	66.6	65.7	65°2	64.5
M. S.	One Sc	ale Division	= .0000	063 parts of th	he V. F.				VERTICAL	Force.	
3 0	138.0	138.2	138.0	138.0	135.3	133.7	137.6	139.3	122.4	119.0	117.1
8 0	138.0	138.2	138.0	138.0	135.3	133.7	138.0	139.3	121.8	119.0	116.8
13 0	138.2	138.2	137.8	138.0	135.3	133.7		139.6	121.8	119.2	117.8
18 <b>o</b>	138.2	138.2	137.8	138.0	134.3	133.7		139.6	121.8	119.0	119.5
23 0	138.0	138.0	137.8 137.8	138.0	134 <b>°</b> 3 134 <b>°</b> 0	133.7   134.9	138.0	139.1	121.6	118.9	120.6
$\begin{array}{ccc} 28 & 0 \\ 33 & 0 \end{array}$	138.0 138.0	138.0 138.0	137.8	136.9	134.0	135.2	137.4 137.1	138.7 136.5	121°2 121°0	118.8 118.4	118.4
38 O	138.2	138.0	138.0	136.9	134.0	135.2		131.9	120.0	118.0	123.3
43 0	138.2	138.0	138.0	136.9	134.0	135.2	137.1	131.4	120.0	118.0	127.4
48 0	138.2	138.0	138.0	135.9	134.0	136.1	138.0	130.8	119.4	117.8	129.6
53 O	138.2	138.0	138.0	135.9	134.0	136.1		129.4	119.4	117.8	133.0
58 <b>0</b>	138.2	138.0	138.0	135.9	133.2	136.8	138.3	129.1	119.2	118.5	134.3
Thermometer	67°3	67°6	67°7	67.5	68°5	69°0	68°5	67.4	67.0	66°1	65.2
							Increasing 1	Numbers dei	note decreas	ing Westerly	/ Declination
1		1		ETEOROLO		BSERV	ATIONS.				
Mean Göttingen Time.	Barometer at 32°.		nometers.		Wind.			7	Weather.		
Time.	at 52 .	- Dry.	- Wet.	Direction,	For	ee.					
D. H. M. 26 10 0 11 0 12 0 13 0 14 0 15 0 16 0 17 0	In. 29.660 29.674 29.678 29.694 29.706 29.725 29.737	63.9 64.6 64.4 60.3 55.0 53.4 52.0 49.9	53.0 53.6 53.0 51.3 48.5 46.6 45.5 44.6	N. N. by E. N. by W. N. by W. N.N.W. N.N.W. N.N.W.	Very I Very I Very I	ht. ht. ht. ight. ight. ight. ight.	Mostly clear; Mostly clear. Mostly clear. Mostly clear. Mostly clear. Mostly clear. Clear.	auroral ligh	at in N. fron	1 18h to 21h	
18 0 19 0 20 0 21 0	29.767 29.768 29.782 29.782	49°1 48°7 47°1 47°8	44°3 44°1 43°3 43°2	N. by W. N.N.W. N.N.W. N. by E.	Very I Very I Very I Very I	ight.	Clear. Clear. Clear. Clear.				

*At 27a 10h, Thermometer of H. F., 68° · 5; of V. F., 67° · 0.

					MAGNET	ICAL O	BSERVATIO	NS.	- <del></del>		May 26th	and 27th.
		DECLINATI	ion.					Ang	ular Value o	of one Scale	Division =	0'.721.
21h.	22h.	23h.	Oh.	1 h.	2h.	3h.	4 ^h .	5h.	6h.	7 ^h .	8 ^h .	9h.
sc. Div. 128 '4 129 '2 129 '5 131 '0 131 '2 128 '4 126 '5 127 '3 126 '3	sc. Div. 121 '9 122 '8 122 '5 121 '5 120 '6 119 '4 120 '4 121 '2 123 '4	Sc. Div. 125 '8 125 '8 126 '0 124 '0 124 '2 124 '8 123 '4 125 '4 126 '4 127 '4	Sc. Div. 129°2 130°0 130°4 131°0 130°0 129°4 128°2 128°4 127°7 127°8	Sc. Div. 129 0 130 2 125 9 129 4 128 5 123 0 117 6 118 2 117 4 115 6	se, Div. 111.6 111.0 114.4 110.4 110.2 114.2 115.4 117.4 116.6 115.8	Sc. Div   145°2   145°4   145°4   146°4   144°2   111°5   111°4   113°4   114°5   115°4	100°9 106°4 100°2 111°5 113°5 113°5 111°3 107°0 106°4 107°4	Sc. Dic. 109*2   108*4   10.0*8   109*6   111*4   111*8   112*2   111*4   109*3   108*4   106*8	se. Div. 107 '3 107 '4 108 '8 107 '6 108 '2 107 '2 108 '2 107 '4 106 '0 105 '8 106 '3	se. Div. 105 '3 105 '4 106 '5 105 '4 106 '5 103 '3 102 '2 103 '0 103 '4 102 '4	se. Div. 103 '2 103 '3 103 '7 103 '4 105 '4 106 '1 106 '5 107 '0 107 '0 107 '0	Sc. Div. 106'8 106'7 107'2 107'0 107'2 108'0 107'5 108'4 108'7 109'0 109'8
125°2 122°6	123.6 124.2	128°2 129°2	127.6 126.2	115.6 114.4	112.1	114.5		106.4	105.3	105.4	106.8	109.4
	J	Horizonta	ь Force.		Iı	nerease, i	n Scale Divisio	ns, correspo	onding to 1°	decrease of	Temperatur	e, 1°63.
603.7 603.4 601.0 601.1 604.0 604.2 606.0 609.0 611.0 615.0 618.0	616.8 615.6 617.0 612.0 615.0 614.0 614.4 615.0 615.0 618.2 620.4 620.8	616°0 615°0 615°0 616°0 616°2 616°0 614°0 613°8 620°0 620°0 620°0 618°0	617.0 616.0 615.0 615.0 611.6 610.0 613.0 610.0 609.0 606.2 606.8 607.0	608.0 604.0 601.2 600.5 600.5 598.5 590.0 591.0 585.0 588.5 588.5	588°5 597°0 600°0 599°5 600°0 597°5 594°0 594°5 594°5 594°0 594°0	597°0 595°0 593°0 593°0 595°2 598°0 591°0 591°0 588°2 585°0 586°0	587°2 584°0 588°0 588°0 588°5 590°0 594°0 597°0 603°4 603°2	598°5 602°2 604°2 601°6 605°5 602°2 601°2 604°0 598°8 600°2 599°0 601°2	602.0 598.2 605.8 612.6 612.5 613.1 612.8 610.0 617.2 616.7 618.0 616.0	616*9 617*0 622*5 622*1 620*8 622*4 613*1 612*0 611*8 609*0 609*0	614.0 615.0 616.0 616.5 616.0 624.0 626.0 630.0 626.0 621.0 624.0 625.0	627·2 630·0 636·0 635·0 635·0 630·0 622·0 628·8 632·0 634·0 636·0 634·0
63.9	63.2	63.0	62°2	62°8	63°5	64.3	65.1	63.8	63.1	66.2	67.0	68.0 a
		VERTICAL	Force.		I	nerease,	in Scale Divisio	ons, correspo	onding to 1°	° decrease of	Temperatur	e, 1°64.
133 · 5 132 · 4 132 · 4 133 · 7 134 · 7 136 · 2 137 · 6 138 · 2 139 · 0 140 · 8 141 · 5 143 · 0	143.7 143.4 143.4 143.4 143.4 143.4 143.4 143.6 143.6 143.6 143.1 143.1	143°1 143°1 143°2 145°5 145°5 145°7 145°7 145°7 145°9 145°9 145°9 145°9 142°8	142 '8 142 '8 142 '8 142 '8 142 '8 142 '8 142 '8 143 '5 143 '5 143 '5 143 '5	140°2 140°2 140°2 140°2 140°2 139°2 136°4 136°4 136°5 136°5 137°1	13711 13711 13711 13711 13711 1368 1368 1368 1368 1368 1368 1368	138.0 138.3 138.3 139.3 140.0 139.3 139.3 139.3 138.8 138.3 139.9	142'1 140'1 139'1 140'2 140'4 140'9 140'9 140'9 141'4 141'4	140°0 141°7 141°7 141°7 142°3 142°3 141°5 141°4 140°9 141°6 142°2 142°2	142.7 142.2 143.1 143.7 144.6 145.2 145.2 145.2 146.0 146.0 146.0	147 · 2 147 · 2 148 · 5 148 · 5 149 · 3 149 · 3 148 · 7 148 · 7 148 · 8 148 · 8 148 · 8 148 · 4	149°5 149°2 149°2 149°2 149°7 149°9 149°9 149°9 149°9 148°2 148°2 148°2	148.2 148.2 148.2 148.4 147.3 147.1 146.9 146.9 146.9
64°6	64.0	63.2	63.2	63°5	63°.6	61.4	64°5	64.9	65.3	65.5	65°5	66.2 ¤
and increa	sing Horizo	ontal and Ver	tical Force.									
				ME	TEOROL	GICAL	OBSERVAT	IONS.				
Mean G Tin	öttingen ne.	Barometer at 32°.	Thern Dry.	wet.	Direc	Wi	nd. Force.			Weathe	r.	
26 22 27 27 3		In. 29 '795 29 '829 29 '850 29 '857 29 '857 29 '857 29 '822 29 '795 29 '773 29 '757	647.0 47.0 50.8 52.8 58.2 61.5 62.3 62.4 62.2 64.9 66.3 66.0	42·8 42·9 47·1 48·7 52·8 55·4 55·8 56·5 56·3 57·6 58·0 56·2	N		Very light. Very light.  Very light. Very light. Very light. Very light. Very light.	Clear. Calm. Calm. Calm. Calm. Calm. Calm. Clear. Clear. Clear. Clear. Clear.				
		J	1					_'				E

ll l	d.			MAGNET	CAL O	BSERVATIO	NS.				·
Mean Göttingen	Angu	lar Value of	f one Scale	Division =	0' . 721.				DECLINAT	ION.	
Time.	10h.	11h.	12 ^h .	13h.	14h.	15h.	16h.	17h.	18h.	19h.	20h.
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div	. Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
0 0	110.2	109.2	113.4	113.2	111.4	116.0	116.0	117.4	121.4	122.4	126.2
5 0	112.2	112.6	113.4	113.4	111.8	115.2	119.4	117.6	122.4	121.6	124.6
10 0		112.5	114.0	113.6	110.4		121.6	118.4	124.9	123.0	124.4
15 0		112.4	113.8	115.4	112.4		121.4	118.6	126.2	123.4	119.9
20 0	115.2	113.2	114.4	115.7	113.5		120.5	117.6	124.0	126.4	119.3
25 0							119.3	117.0	118.6	127.4	118.4
	114.4	113.2	114.0	116.0	113.5					127 4	
30 0	113.2	113.2	114.0	116.0	112.6		117.6	118.4	118.4	139.9	118.2
35 O	113.0	113.4	114.4	112.4	112.4	116.0	117.4	119.4	121.4	130.4	119.5
40 0	110.8	113.6	115.0	111.2	112.4		116.6	119.6	125.5	134.0	118.8
45 0	109.4	113.4	115.4	111.4	112.6	118.4	117.4	118.4	127.0	135.2	119.4
50 <b>0</b>	109.4	113.4	115.0	112.4	113.3		117.0	118.5	126.4	134.2	119.2
55 O	109.4	113.6	113.8	112.0	115.4		117.4	119.5	122.2	131.7	120.1
11		!			1		1	1		<u> </u>	1
M. s.	One S	Scale Divisi	on = .000	0087 parts	of the H.	F.			HORIZONT	AL FORCE	•
2 0	625.4	624.2	601.2	613.0	607.0	602.2	602.0	599.4	602.0	604.2	609.9
7 0	614.4	623.2	600.2	617.0	612.0		602.0	601.0	601.2	607.5	603.0
12 0	619.3	614.2	599.0	616.0	610.0		600.0	601.0	603.2	608.0	600.0
17 0	616.2	599.2	597.0	618.0	609.2		600.0	600.5	602.0	606.0	596.0
22 0	607.2	598.0	605.0	618.2	610.0		599.0	599.0	602.8	600.0	594.0
27 0	603.0	597.0	610.5	611.2	610.2		599.0	599.0	604.0	605.5	590.0
32 0	600.2	593.2	614.0	613.0	610.5	608.8	600.0	599.0	602.0	608.7	592.0
37 0	600.0	596.4	616.0	618.2	606.0	605.0	599.0	600.0	602.0	602.0	597.1
42 0	602.8	597.4	615.0	614.8	605.8	603.2	599.0	601.2	600.5	600.0	599.5
47 0	608.5	595.0	618.2	613.0	606.4		599.0	601.0	601.0	599.0	601.0
52 0	614.0	601.2	621.2	611.0	602		599.0	599.0	603.0	599.0	601.0
57 O	621.2	602.2	613.4	611.0	602.0		601.0	600.2	603.0	604.0	602.0
	-			<del></del>		_	·	<u> </u>	-		<u>-</u>
Thermometer	71.8	72°4	72°6	72.3	71.5	5 71°3	70.4	69.6	69.2	69.8	68.6
M. S.	One	Scale Divisi	ion = '000	0063 parts	of the V.	F.			VERTICAL	Force.	
	19011	105.0	100.5	100.1	100.0	101.5	105.4	1.07.0	11010	1.04.0	100.0
3 0	138.1	137.2	130.7	132'1	133.2		127.4	127.9	119.8	124.0	123.6
8 0	138.1	135.9	130.7	132.7	133.7		127.7	127.9	119.8	124.0	124.0
13 0	138.1	133.4	129.4	132.7	133.7		127.8	127.9	119.8	124.0	124.5
18 0	137.1	133.4	12914	132.7	133.7	131.5	127.8	127.7	119.8	122.7	124.2
23 0	135.1	133.4	129.0	132.7	133.7	131.1	128.6	127.7	119.8	122.7	122.6
28 0	133.9	133.2	132.1	132.7	133.7	131.1	128.6	127.9	123.0	121.5	120.2
33 0	133.9	133.1	132.1	132.7	133.7	131.1	128.9	127.9	123.3	119.6	121.2
38 0	133.6	133.1	132.1	133.0	133 2		128.9	127.9	125.0	119.6	121.3
	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	133.1	132.1	133.0	133.2						
							129.6	127.8	125.0	119.0	121.3
48 0	133.8	133.1	132.7	133.0	132.9		129.6	127.8	125.0	118.2	121.2
53 O	133.8	133.1	132.7	133.0	132.9		129.6	127.8	125.0	119.0	119.0
58 0	136.3	133.1	131.7	133.5	132.9	131.4	129.6	127.8	124.0	121.5	118.5
			_ 0		. 0		0			0	
Thermometer	7ů·6	71°3	71.3	71.3	70°5	70°·8	70°·8	70.5	70.2	70°5	70.0
							Increasing	Numbers de	note decreas	ing Westerl	y Declinatio
			ME	TEOROLO	OGICAL	OBSERVAT	TIONS.				
Mean Göttingen	Barometer	Ther	mometers.		Win	nd.					
Time.	at 32°.	Dry.	Wet.	Direc	etion.	Force.			Weathe	r.	
D " "	7		0				-	-			
D. H. M.	In.	1	1	1							
21 10 0	29.400	71.5	61.4		I.W.	Very light		louded; cir.	cum. and cu	mstrat.; a f	ew clear spa
11 0	29.401	70.6	61.1		I.W.	Very light	· Mostly	clouded; a :	few clear spa	ices.	
12 0	29.423	69.8	58.9		I.W.	Light.	Mostly	clouded: a	few clear spa	ices.	
13 0	29.457	67.3	58.2	W.N		Light.	Clouded	•	ope		
	29.460	63.1	55.6	W.N		Very light	· Clouded				
14 0	29.470	62.5	55.0		_		Clouded				
14 0		57.3	53.6	-			Clouded				
14 0 15 0	yu ana	1 01 0		1 -	-		1				
14 0 15 0 16 0	29.463	EE . 0					Clouded				
14 0 15 0 16 0 17 0	29.442	55.2	52.5	-	-						
14 0 15 0 16 0 17 0 18 0	29.442 29.449	52.8	50.8	_	_		Clouded	i <b>.</b>			
14 0 15 0 16 0 17 0 18 0 19 0	29.442 29.449 29.445	52.8 53.2	50.8 50.8	_	_			i <b>.</b>			
14 0 15 0 16 0 17 0 18 0	29.442 29.449	52.8	50.8 50.8 51.0		_	<u> </u>	Clouded	i.			

		~ <del></del>			MAGNET	ICAL OI	BSERVATI	ons.			June 21st a	and 22nd.
		DECLINATI	on.		·			An	gular Value	of one Scal	e Division =	=0'`721.
21 ^h .	22 ^h .	23 ^h .	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .
sc. Div. 121 '3 124 '0 125 '4 127 '4 126 '6 125 '4 117 '3 109 '8 104 '5 102 '3 103 '3	Sc. Div. 108 '8 114 '4 118 '4 122 '4 126 '6 125 '4 125 '5 122 '4 120 '0 120 '0 121 '8	Sc. Div. 127 · 4 135 · 0 133 · 4 131 · 4 122 · 4 118 · 8 118 · 2 116 · 4 116 · 0 116 · 4 118 · 8	Sc. Div. 117 ' 4 121 ' 8 118 ' 8 123 ' 0 122 ' 2 125 ' 0 128 ' 4 126 ' 4 125 ' 0 124 ' 8 124 ' 6 126 ' 4	Sc. Div. 126 1 124 4 124 9 124 8 123 4 123 4 127 0 125 6 124 0 122 0 124 6 123 0	sc. Div. 126 '4 127 '6 127 '4 128 '4 126 '4 123 '4 124 '7 121 '4 122 '4 121 '4 120 '0 123 '4	Sc. Div. 125 0 124 7 124 0 124 6 121 4 117 2 116 3 115 9 118 5 120 8 122 2 123 6	Sc. Div. 123 0 122 6 121 4 119 3 114 4 115 0 114 8 114 4 113 4 112 2 111 6	Se. Div. 112.6 115.6 116.6 117.4 117.8 117.5 118.2 120.0 119.4 119.0 117.4 116.6	Sc. Div. 114'9 115'2 115'6 114'4 112'4 107'4 104'8 104'5 105'4 105'2 104'6 105'4	Se. Div. 106 2 106 4 106 5 107 6 107 6 106 4 106 4 105 8 106 4	Sc. Div. 106 '4 107 '0 107 '4 107 '4 107 '7 108 '4 108 '9 109 '5 110 '3 110 '5 111 '3	Sc Div. 111'5 112'6 114'6 114'6 115'6 117'4 118'4 118'4 118'4 118'5 115'5 115'4 116'5
	· · · · · · · · · · · · · · · · · · ·	Horizonta				1		ions, correspo	1	1	1	i
600 '9 595 '0 590 '0 588 '9 585 '0 587 '5 590 '0 591 '0 599 '0 609 '0 612 '2	609.0 610.0 614.0 615.4 609.0 606.0 599.8 591.4 593.5 595.0 599.5 603.4	603·2 608·7 602·2 596·4 598·0 597·5 596·0 593·8 598·8 601·2 603·0 603·2	605.5 608.4 604.5 599.2 598.8 594.0 592.8 591.0 588.7 588.8 599.0	588 '8 585 '0 588 '0 589 '0 592 '8 592 '2 590 '0 596 '8 602 '0 605 '0 608 '5 610 '0	604.5 601.0 598.0 598.8 597.0 596.8 604.2 605.4 602.0 604.2 601.0 603.0	598.0 598.8 599.0 597.0 594.2 594.5 594.0 595.2 593.0 587.0 585.0 583.0	580.0 579.0 579.5 577.5 586.0 582.0 574.0 581.0 585.0 583.0 583.5	585.0 584.5 579.0 580.0 583.0 584.0 579.0 571.0 571.0 577.5	587.0 586.0 580.0 571.0 570.0 575.0 565.0 569.0 574.0 581.5 588.0 594.0	602·1 606·5 605·1 607·2 611·1 606·0 607·0 603·0 601·0 603·0 601·0	604'0 611'0 616'0 623'0 626'0 628'1 630'6 632'0 635'0 638'0 638'1 641'1	643.0 640.0 645.0 645.0 642.0 652.0 650.0 652.1 660.0 661.2 660.0 655.0
68°5	68°.0	67°8	67.4	6 [°] 0	67°5	68.5	69°4	70.0	70°5	7°1.4	71.7	72·2 a
	7	VERTICAL	Force.		I	ncrease, in	Scale Divisi	ons, correspo	onding to 1°	decrease of	Temperatur	e, 1°64.
114'8 112'8 111'8 111'8 111'8 113'6 113'6 112'6 112'0 111'0 108'9 108'9	105'4 105'4 105'4 107'0 106'1 106'1 109'0 108'5 108'5 109'0 110'0 111'0	111.7 116.0 116.4 118.3 118.9 118.9 120.0 121.0 122.9 123.7 124.0 124.0	128 ' 4 129 ' 2 129 ' 2 128 ' 9 130 ' 7 128 ' 4 128 ' 4 131 ' 9 132 ' 0 131 ' 9 131 ' 9 132 ' 7	131.8 133.3 133.3 135.1 135.1 135.1 134.8 134.8 136.6 136.6	136.7 136.7 136.5 136.5 136.5 136.7 136.7 136.7 136.1 136.1	134.5 134.5 134.5 134.5 132.2 134.8 133.6 133.0 132.9 132.0 131.5	131.5 131.5 133.0 133.5 133.5 132.5 132.5 132.5 132.5 132.5 132.5	132.6 132.6 132.9 132.9 132.9 133.2 133.2 133.2 133.2 134.1 136.0	136.0   136.0   136.0   136.0   136.8   137.3   137.3   137.3   137.3   137.3   138.5	139·2   139·2   139·2   139·2   140·5   140·5   140·5   140·5   140·8   140·8   141·2	141.2 141.2 140.8 142.4 142.4 142.4 142.4 142.4 143.8 143.8 145.0 145.0	146°1 146°9 148°8 148°8 150°2 151°5 151°0 150°6 150°9 150°9 150°9
69°5	69°4	68.3	6 <b>7°</b> 3	67°3	67.7	68°5	68.8	69°3	69.5	70°·1	70°·4	70°8ª
and increas	sing Horizon	ntal and Ver	tical Force.									
				ME	TEOROLO	GICAL (	OBSERVA'	TIONS.				
Mean Go Tin		Barometer at 32°.	Ther Dry.	wet.	Directi	Wind.	Force.			Weather.		
D. н 21 22 22 (	. м. 2 О	In. 29:496 29:498 29:498 29:498 29:510 29:496 29:505 29:495 29:493 29:486 29:474	52.6 53.7 57.2 59.7 67.3 68.9 66.5 67.7 69.1 71.5 69.9 70.1	%et. 51.0 52.1 54.8 56.4 62.2 64.0 62.7 62.9 63.7 64.9 63.6 63.4	S.S.1 S.E. by E. by E. E.	E. Vo E. Vo y E. Vo v S. Vo	ery light. ery light. ery light. ery light. ery light. ery light. ery light.	Mostly clou	ided; cum. ided; cum. ided. ided.	strat. and cir. strat. and ci strat. and ci	rstrat.	auroral light.
			<u> </u>	1		)					2 F	!

July 19t	h and 20	Oth.			MAGNETI	CAL OBS	ERVATIO	NS.						
Mean Gött		Ang	gula <b>r Va</b> lue	of one Scal	e division =	0'.721.				DECLINAT	ion.			
Time	•	10h.	11 ^h .	12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18h.	19 ^h .	20h.		
	s.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc Div.	Sc. Div.	Sc. Div		
	0	109.4	112.2	115.8	114.4	114.2	118.2	127.5	120.6	117.6	114.4	112.4		
	0	108.6	114'4	116.0	114.4	114.2	118.7	126.4	120.4	116.4	114.6	112.4		
	0	108.8	113.4	116.4	113.6	115.0	118.4	125.4	121.0	115.4	114.4	112.4		
	0	109.4	114.0	116.6	113.6	114.8	118.0	124.4	120.9	114.4	114.4	113.3		
	0	109.8	114.2	116.4	113.4	115.2	118.2	122.6	120.4	113.8	114.2	113.4		
	0	110.6	115.0	116.4	113.8	115.2	119.6	121.4	120.3	114.3	114.3	113 4		
	0	111.8	115.4	116.5	113.8	115.4	124.8	120.0	120.4	114.9	113.4	113.2		
	0	112.2	113.8	116.0	113.9	115.4	125.0	119.4	121.4	115.4	113.3	113.2		
	0	112.2	113.4	115.4	114.2	115.4	129.4	119.6	121.6	115.4	112.5	112		
	0	112.4	113.8	115.4	114.8	115.4	129.4	119.6	122.6	115.4	112.1	112.7		
	0	112.4	115.5	115.4	115.0	116.0	129.0	119.4	122.5	114.0	112.4	112		
55	0	112.4	115.4	115.5	114.6	117.2	128.2	119.8	119.6	113.8	112.4	112.5		
M.	s.	One	e Scale Divis	sion = '00	00087 parts	of the II. F	`.			Horizon	HORIZONTAL FORCE.			
0	0	COLLO	1 000:0	1 50110	1	1 500.0	1 00010	1 50010	1 50.440	70010	1 00010	700.1		
	0	601.8	609.8	594.2	596.8	598.0	600.0	599.0	594.0	590.2	602.0	598.1		
	0	605.4	607.2	593.8	596.0	598.5	598.0	597.5	594.5	589.0	603.1	597.8		
	0	609.2	602.2	593.8	596.2	599.0	597.8	596.0	595.0	591.0	601.8	597.0		
17	0	609.8	601.4	594.6	596.2	599.0	598.0	596.8	595.0	592.2	601.0	597.2		
	0	607.8	603.2	597.8	597.8	599.2	598.2	596.5	593.5	593.0	600.0	598.0		
	0	612.2	602.8	596.2	598.0	599.4	596.8	595.1	591.5	595.0	600.9	598.0		
	0	613.5	601.4	595.0	598.0	599.4	598.0	593.3	589.5	596.2	600.0	597.5		
	0	610.5	600.2	595.0	598.1	600.0	599.0	592.0	588.0	598.0	599.2	597.2		
	0	609.8	597.6	593.2	596.8	600.1	599.2	591.8	587.0	597.5	599.0	597.1		
	0	610.0	597.4	592.4	596.6	600.2	601.0	592.2	588.2	598.9	598.8	598.0		
	0	610.2	598.4	594.2	596.0	596.8	601.2	592.6	589.0	600.0	599.0	598.5		
57 ———	0	609.8	597.2	594.2	598.0	596.5	600.0	293.0	289.0	601.0	299.0	598.2		
Thermon	neter	76°2	76°2	76°2	75°·5	$7\mathring{5} \cdot 2$	74.4	73.9	74.0	73.8	73°7	73°·5		
M.	s.	One	e Scale Divi	sion = '00	00063 parts	of the V. F	•			VERTICAL	Force.			
3	0	126.9	128.0	123.8	124.0	122.5	121.4	118.7	119.6	120.0	120.8	121.7		
	0	126.9	128.0	123.6	123.4	122.5	1	1	1		1			
	0	127.4	126.7	123 6	123.4	122.5	$\begin{vmatrix} 121.7 \\ 121.7 \end{vmatrix}$	$\begin{vmatrix} 117.7 \\ 117.2 \end{vmatrix}$	119.6	120.0	120.8	121.7		
	0	127.7	126.6	123 4	123.2	122.5	$\begin{vmatrix} 121 & 7 \\ 121 & 7 \end{vmatrix}$	$\begin{vmatrix} 117.3 \\ 117.3 \end{vmatrix}$	119.7	120.0	120.4	121 · 7 121 · 7		
	0	127.7	126.6	123 4	123.2	122.5	121.8	$117.3 \\ 117.2$	119.6	120.0	120.4	$\frac{121}{121.7}$		
	0	129.7	126.6	123.4	123.2	122.5	121.8	117.7	119.6	120.0	120.4 121.5	121.7		
	0	129.7	126.7	124.8	$\frac{123 \cdot 2}{123 \cdot 2}$	122.5	121 8	117.9	119.3	119.9		122.8		
	0	128.9	126.5	124.8	123.2	121.4	121.8			120.0	121.5	$\begin{array}{c} 122.8 \\ 122.8 \end{array}$		
	0	128.0	126.5	124.8	123.2	121.4	121.8	110.3	118.6 118.4		121.5			
	0	128.0	125.7	124.8	123.3	121 4	119.0	110.3		120.5	121.5	122.8		
	0	128.0	125.6	124.0	123.3	121 4	118.7	119°3	118.4 118.4	120°5	121.7	122.8 122.8		
	0	128.0	125.6	124.0	123.8	121 4	118.7	119.6	118 4	120.3	121.7 121.7	122.8		
Thermon	neter	74.5	75°1	75°0	74.6	74°5	74.7	75°0	7 [°] 4.6	74°5	74.5	7 <u>å</u> ·5		

21 ^h .		Dagrassia										
		DECLINAT	CION.					Ang	gular Value	of one Scale	Division =	: 0′*721.
	22 ^h .	23h.	Oh.	1 ^h .	2h.	3h.	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9 ^h .
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. D
112.5	115.6	119.5	120.0	120.8	123.4	120.2	117.9	112.0	107.4	105.4	106.4	108.
112.4	116.2	119.5	150.0	121.8	124.0	120.0	117.0	111.2	107.2	105.4	106.7	108
113.3	116.5	119.4	120.5	122.8	123.2	118.6	117.3	110.8	107.0	105.4	107.3	108
113.4	116.4	119.4	120.5	122.4	122.4	118.8	117.2	110.4	105*4	105.6	107.4	108.
113.6	116.8	119.4	120.4	122.4	122.4	118.4	116.5	110.3	105.0	105.3	107.4	108
114.3	117.0	119.5	120.4	121.5	121.6	118.6	114.8	109.4	105.6	105.4	107:3	109
114.3	117.2	119.8	120.6	122'4	121.6	118.9	114.4	109.3	106.4	105.6	107.4	108
114.4	117.4	119.8	120.2	122.4	121.5	119.4	114.5	109.2	106.2	105.7	107.4	109
114.8	117.6	120.0	119.8	122.4	121.6	117.8	114.2	108.8	105.8	105.7	107.5	109
115.4	118.0	120.5	119.8	122.0	121.4	118.4	113.6	108.4	105.4	105.8	107.5	109
115.2	118.4	120.4	119.8	122.4	120.9	117.4	113.6	107.4	105.2	105.9	107.6	109
115.4	119.0	120.4	120.0	123.2	120.4	117.4	112.4	107.6	105.3	106.4	107.8	109
		<u>'</u>	<u>'</u>	<u>'</u>	<u> </u>				<u>'</u>	<u>'</u>	1	
		Horizont	AL FORCE.		]	Increase, in	Scale Divisi	ons, corresp	onding to 1°	decrease of	'Temperatui	re, 1.63.
299.0	601.0	602.2	592.8	591.2	592.0	588.8	588.2	580.0	583.8	593.0	596.0	601
599.5	602.0	601.4	593.6	590.2	588.4	589.0	586.0	578.5	581.8	594:0	595.0	601
299.8	601.2	601.2	593.8	590.0	288.0	588.7	585.0	578.6	283.0	594.0	597.0	600
99'0	601.4	600.8	591.2	591.0	588.2	588.5	585.0	578.5	582.2	592.5 592.8	598.0	598
598.5		597.6	591.6	590.0	591.0	589.0	584.0	578.4	588.0		598.0	597
599.2	602.0	598.8	593.0	589.0	591.0	590.2	583.2	579.0	586.0	592.5	598.1	597 1
8.665	601.9	600.0	591.2	589.8	591.0	590.0	583.4	581.0	589.0	592.0	599.0	597:
900.0	602.0	600.2	592.2	590.0	589.0	590.4	581.0	581.2	589.0	593.5	600.0	597
900.0	601.2	599.7	592.0	590.2	588.0	590.0	579'1	583.0	588.6	594.0	599.0	598
9.000	600.8	599.8	592 4	590.0	588.2	588.0	579.2	583.8	590.7	594.2	599.0	5991
301.0	601.0	597.8	592.3	592.0	587.0	587.0	580.2	581.5	591.8	595.0	600.0	599
200.0	601.2	592.6	591.5	593.0	589.0	588.0	579.5	582.0	593.7	596.0	600.0	599*0
73°0	72.5	72°2	71.8	72°2	72°5	73.2	74.5	75°7	77°0	77°0	77.8	78°:
		VERTICAL	Force.		I	ncrease, in S	Scale Divisio	ons, correspo	onding to $1^\circ$	decrease of	Temperatur	e, 1°64.
123.1	123.9	123.9	125.0	125.1	124.2	124.2	124.1	121.6	119.7	117.9	117.5	118.8
23.1	124.7	125.0	124.8	124.8	124.2	124.2	123.6	121.6	119.7	117.9	117.5	118.8
23.1	124.7	126.5	124.8	124.8	124.2	124.2	123.6	121.4	119.7	117.9	117.8	118.8
23.1	124 7	126.4	124 8	124.8	124 2	124.2	123.6	121 4				
23.1	123.8		126 1		$\frac{124}{124} \cdot 2$	124.5	123.6		119.7	116.4	117.8	118.8
23.6		126.4		124.8				121.0	119.7	116.4	117.6	118.8
23.6	123.8	126.7	126.1	124.8	$124.2 \\ 124.2$	124°2 124°2	123.6 123.6	120.8	110.0	117.6	117.6	118.8
23.6	124.2	126.7	125.7	124.8				120.6	110.0	117.6	118.1	118.3
23.6	124.2	126.8	125.7	125.0	123.8	124.2	123.4	120.6	110.0	116.8	118.1	118.3
23.9	123.6	126.8	125.7	125.0	123.8	124.6	122.6	120.6	119.0	116.6	118.1	118.3
23 <b>·</b> 9	123.8	126.8	125.7	124.8	123.8	124.6	122.6	120.6	118.7	116.8	118.1	118.3
23 <b>·</b> 9	123.8 123.8	126°1	125°5 125°1	$125.0 \\ 124.8$	123°8 123°8	124°0 124°1	122.6 122.6	120°4 119°7	$118.7 \\ 117.9$	116.6 116.2	118.1	118°2
7 [°] 3	73.7				- <del></del>		73.4	74.6	7 [°] 5.5			
17.0	15 1	72.3	72.0	72°1	12 3	(2-5)	13 4	74 6	10.2	75°7	76°5	76.5

August 25th and	26th.			MAGNETI	CAL OBS	ERVATIO	NS.				
Mean Göttingen	Angul	ar Value of	one Scale D	ivision = 0	·721.				Declinati	ON.	
Time.	10h.	11h.	12 ^h .	13h.	14h.	15 ^h .	16 ^h .	17h.	18h.	19h·	20h.
м. s.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.
0 0	111.4	116.4	116.4	114.6	113.6	113.7	113.4	115°2 114°6	113.2	113.4	108.2
5  0	111'4	116.4	116.4	114'3	113.6	113.6	113.4	116.4	$\frac{113.4}{113.2}$		110.2
10 0	111.8	116.8	116.4	114.2	114.0	113.6 113.6	113.4	116.2	113.4	110.4 110.9	113.8
15 0	111'4	117.0	116.5	113.8	113.9	113.7	113.3	115.4	113.4	106.6	114.4
20 0	113.0	116.8	116.2	113.9	114.0	113.7	113.3	115.4	113 4	107.8	114 4
25  0	113'4	116.4	115.4	114.8	113.8		1	114.4	113.4	106.6	115.4
30 0	114.2	116.4	115.4	114.4	113.6	113.7	114.1	114.3	113 4	106.4	115.0
35  0	114.6	116.8	115.0	114.6	113.6	113.8	113.5				
40 0	115 0	116.8	114.8	114.4	113.6	113.4	113.4	114.3	111.7	106.8	114.4
45  0	115.4	116.8	114.8	114.6	113.7	113.4	113.4	113.7	112.3	107.2	114.4
50 0	115.7	117.0	115.0	114.0	113.6	113.5	114.5	113.4	113.1	107.6	115.0
55 0	115.9	116.8	114.7	112.0	113.6	113.5	114.2	113.4	113.4	107.8	115.0
м. s.	One S	cale Divisior	= .0000	87 parts of	the II. F.				Horizont	AL FORCE	•
	001.5	702:0	604.0	600.0	603.2	606.0	608.0	607.0	606.2	606.0	606.0
2 0	601.5	593.0	602.0	600.0	603.9	909.0	608.0	608.1	607.0	606.9	605.8
$\begin{array}{ccc} 7 & 0 \\ 12 & 0 \end{array}$	598.5	593.0	602.2	900.0	604.0	607.0	608.0	609.9	606.9	607.9	605.2
12 0	597.8	597.0	600.0	900.0	605.2	608.0	607.0	609.0	607.0	607.9	605.0
17 0	598.0	599.8	600.0	601.2	605.8	608.0	607.0	609.0	607.0	607.8	606.2
22 0	596.0	602.0	1	602.0	605.8	608.0	607.0	608.2	606.1	608.2	000 2
27 0	595.0	603.2	600.0	603.0	605.5	607.0	607.1	607.1	606.3	607.8	606.0
32 0	595.2	603.4	601.0	603.0	605.5	607.0	606.9	606.2	606.9	608.0	605.0
37 0	596.0	603.2	600.0	605.0	605.8	608.0	604.1	606.0	606.0	607.2	604.8
42 0	596.2	604.0	600.0		606.2	607.0	607.0	606.2	605.2	607.8	605.0
47 0	595.0	604.2	599.0	604.0	606.2	608.0	607.0	607.0	605.0	607.6	604.8
52 0	593.8	604.4	600.0	603.0	606.2	608.5	606.3	606.2	605 1	607.4	605.0
57 0	594.0	604.0	600.0	003 0	000 2		000 3			007 4	
Thermometer	76°2	75°4	75.2	75.0	75.1	75°1	75.0	74.6	74.5	74.3	74.1
м. s.	One S	cale Divisio	n = '0000	63 parts of	the V. F.				VERTICAL	Force.	
3 0	116.5	118.3	118.6	117.2	115.9	114.0	114.5	115.3	114.7	115.2	116.0
8 0	116.2	118.3	118.6	117.0	115.9	114.0	114.2	115.3	114.7	115.2	116.0
13  0	116.2	118.3	118.8	117.0	114.9	114.0	114.2	115.3	115.1	115.2	116.0
18 0	116.2	118.2	118.8	116.0	114.6	114.0	114.2	115.0	115.1	115.2	116.0
$\begin{array}{ccc} 13 & 0 \\ 23 & 0 \end{array}$	116.2	118.2	118.8	116.0	114.6	114.0	114.2	114.7	115.1	115.2	116.2
$\begin{array}{ccc} 23 & 0 \\ 28 & 0 \end{array}$	116.2	118.2	118.8	116.0	114.0	114.0	115.3	114.7	115.1	115.2	
33 O	116.2	118.2	118.8	116.0	114.4	114.0	115.3	114.7	115.1	115.2	116.2
38 0	116.2	118.6	118.8	116.0	114.4	114.0	115.3	114.7	115.2	116.0	116.2
43 0	116.2	118.6	118.8	116.0	114.4	114.0	115.3	114.7	115.2	116.0	116.5
48 0	113.9	118.6	118.9	116.0	114.0	114.0	115.3	114.7	115.5	116.0	116.5
53 0	113.9	118.6	117.9	116.0	114.0	114.0	115.3	114.7	115.2	116.0	116.5
58 <b>0</b>	113.7	118.6	117.9	115.9	114.0	114.0	115.3	114.7	115.2	115.4	116.7
Thermometer	74°0	74.2	74.2	74.0	74.2	74.0	75.0	75.0	74°5	74.5	74.3

					MAGNET	ICAL OBS	ER <b>V</b> ATIO	NS.			August 25th	and 26th.
		DECLINAT	TION.					Ang	gula <b>r V</b> alue	of one Scale	Division =	: 0'`721.
21h.	22h.	23h.	Oh.	1h.	2h.	3h.	4h.	5h.	6 ^h .	7 ^h .	8h.	9 ^հ .
sc. Div. 115.0 115.8	Sc. Div. 115 2 115 4	Sc. Div. 118°0 119°6	sc. Div. 122.6 122.8	Sc. Div. 129.6 129.4	Sc. Div. 128°3 127°0	sc. Div. 122°0 121°0	Sc. Div. 114.5 114.0	Sc. Div. 108°4 108°2	Sc. Div. 104.7 105.2	Sc. Div. 104°2 104°0	Sc. Div. 106 0 106 4	Sc. Div. 110°0 110°2
115.0 114.4 115.0	114.8 115.4 117.6	119.8 120.4 121.4	123.8 124.0 125.0	128.6 128.0 127.4	126.6 126.0 125.6	120.6 120.4 119.4	113 '4 112 '4 112 '4	108°3 108°2 107°4	104.6 104.6	104.0 104.2 104.8	106.4 106.8 107.4	110.4 111.0 111.2
114.2 114.0 113.8 114.2	117.8 117.0 117.4 117.4	121.6 120.8 121.2 122.2	126.6 127.0 127.4 127.4	127.6 128.0 128.4 128.3	125°0 124°6 124°2 123°6	118.6 118.2 117.7 117.0	111.6 111.3 110.4 110.2	106.8 106.4 106.6 105.4	104.6 105.0 105.0	104.6 104.8 104.8 105.0	107 · 4 108 · 2 108 · 4 108 · 4	111.8 111.8 112.0 112.4
114.0 114.4 114.4	117.6 118.0 118.0	122 · 4 122 · 3 122 · 4	129·3 129·3	128 2 127 6 127 6	123.6 121.8 122.0	116.4 116.0 112.4	109.6 109.6 109.2	105.0 104.6	104.8 104.4 104.6	105.0 105.4 105.6	108.8 109.0 109.4	112.6 113.0 113.2
	'	Horizont	AL FORCE			Increase, in	Scale Divis	ions, corresp	oonding to 1	° decrease o	of Temperatu	re, 1.63.
606°5 606°2	604.8	606.0	602.0	598.0 597.0	589°0 589°0	582.1	579.0 579.0	576.0 577.0	581·2 581·4	590°2 591°0	600.0	604.4
605.8 605.0 604.8 604.2	604.2 605.0 605.0 605.0	607.0 604.0 604.8 604.8	602.0 602.0 601.2 600.0	598.0 596.0 594.5 594.5	588.0 588.0 587.1 586.5	582°2 582°0 582°0 582°0	578°5 578°0 577°5 577°5	578.0 578.2 579.0 580.0	582°2 583°4 584°0 585°0	591.3 591.8 592.8 593.2	600°8 601°2 602°0 602°2	605°0 605°2 605°2 608°8
604.0 604.0	605°2 605°0 606°0	605.0 602.2 602.2	600°0 600°4 600°2	595 · 2 593 · 5 591 · 8	586.0 585.0 584.0	581.0 581.0 580.0	577 · 0 577 · 0 578 · 0	581.0 581.0 581.0	586.0 587.0 587.8	594·2 594·5 597·0	602.8 601.8 601.2	609·2 608·0 608·4
603.0 603.2	606.4 606.0 606.0	602.2 602.0 601.8	598.6 598.0 597.0	591.0 591.2 591.2	584.4 583.1 583.0	580.0 580.0 579.0	577.0 576.0 576.5	581.5 581.5 581.5	588.2 588.0 588.8	597.8 599.0 598.0	601.5 602.2 603.2	608°2 609°4 608°2
7å·6	7ŝ·5	72.7	72.8	7å·0	73.1	73.8	74.8	75.3	75°4	75°4	75°5	75.3
	,	Vertical	Force.		2	Increase, in	Scale Divisi	ons, corresp	onding to 1	° decrease o	f Temperatu	re, 1°64.
116·7 117·0 117·1	118.0 118.0 117.5	117.7 117.7 117.7	117:9 117:9 117:9	118.0 118.0 118.0	117.7 117.7 117.7	117°3 117°3 117°3	116.8 116.7 116.2	114.0 114.0 114.0	114.0 114.0 114.0	115.0 115.1	116.6 116.6 116.6	116.5 116.5 116.4
117°1 117°1 117°5 117°5	117.5 117.5 117.5 117.7	117.7 117.7 117.7 117.7	117:9 117:9 117:9	118.0 117.7 117.6	117:5 117:5 117:5 117:4	117:3 117:3 117:3 117:3	116.0 116.0 116.0	114.0 114.2 114.2 114.2	114.0 114.0 114.0	116.0 116.0 116.0	116.6 116.6 116.5	116.4 116.4 116.6 117.0
117·5 117·5 117·8 118·0	117·7 117·7 117·7 117·7	117.7 117.7 117.7 117.7	117.9 117.9 117.9 118.0	117.6 117.6 117.6 117.6	117.4 117.4 117.4 117.3	117.3 117.3 116.8 116.8	115.0 115.0 115.0	114 · 2 114 · 2 114 · 2 114 · 2	114.0 114.3 112.0 115.0	116.3 116.6 116.7 116.7	115.8 115.8 115.8 115.8	117.0 116.6 116.6 117.0
118.0	117.7	117.9	118.0	73.0	117.3	116.8	112.0	114.5	115.0	116.7	116.0	117.0
73.8	$7\mathring{3}$ . 5	73°3	73.1	0	72.8	73.0	7å·7	74.5	74.0	74.5	74.0	74.0
nd increas	sing Horizon	ntal and Ver	rtical Force.									

Septem	ber 20th	and 21st.			MAGNET	ICAL OBS	ERVATIO	NS.		•			
Mean G		$\Lambda$ ngu	lar Value of	one Scale I	Division = (	)'·721 <b>.</b>				DECLINA	rion.		
Tin	ne.	10 ^h .	11 ^h .	12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18 ^h .	19 ^h .	20 ^h	
М.	s.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div	
0	0	109.4	113.3	113.6	112.8	111.8	114.4	114.2	115.7	114.6	114.4	114.6	
5	0	108.6	113.3	113.6	112.4	111.8	114.4	114.4	115.4	114.5	114.4	114	
10	0	110.4	112.6	114.2	112.4	112.8	113.4	113.8	115.3	114.4	113.6	114	
15	0	110.4	112.4	114.4	112.4	113.4	113.4	113.8	115.8	114.4	114.6	114.0	
20	0	110.4	112.9	114.5	112.4	113.4	114.8	115.0	116.0	114.4	115.0	114	
$\frac{25}{20}$	0	111.3	113.4	113.6	111.8	113.8	114.8	115.2	116.2	114.4	115.0	114	
30	0	111.2	113.2	114.4	112.4	114.0	117.4	115.4	115.4	114.5	114.6	114	
35	0	112.3	113.4	114.8	112.2	113.4	118.8	115.4	115.0	114.4	114.4	114	
40	0	112.2	113.4	114'4	113.0	114.0	119.4	114.4	115.4	114.8	114.4	114.	
45	0	112.4	113.4	113.4	112.2	114.9	115.4	114.0	115.4	114.6	114.4	115	
50	0	112.4	113.4	113.4	111'4	116.8	114.6	114.2	115.5	114.4	114.5	114	
55	0	113.5	113.4	113.5	111.4	115.4	114.4	114.4	115.4	114.5	114.6	114'	
м.	s.	One	Scale Divisio	on = .0000	087 parts of	f the H. F.				Horizoni	CAL FORCE		
2	0	618.0	626.0	624.7	624.0	623.8	637 2	624.0	622.5	623.0	623.2	624	
$\frac{7}{7}$	Ö	618.0	626.5	625.0	624.4	624.4	637.8	622.4	622.4	622.8	624.2	623	
$1\dot{2}$	Ö	617.2	625.0	622.9	625.0	623.2	631.2	620.2	621.4	623.0	625.2	625	
17	Ö	616.0	623 2	622.5	626.0	622.2	628.2	619.4	621.2	623 2	624.2	625	
$\frac{1}{22}$	0	617.0	622.0	623.1	625.2	$622 \cdot 2$	628.8	618.2	621.2	623.0	625.0	625	
$\frac{22}{27}$	0	616.2	622.0	622.1	625.0	622.0	628.5	618.0	621.0	623.0	624.0	625	
$\frac{21}{32}$	ő	618.6	622.9	622.0	624.2	622.4	623.2	620.6	621.0	622.0	624.0	625	
37	Ö	620.9	624.0	622.4	624.4	622.2	627 4	621.0	620.8	622.0	624.0	625	
42	ő	622.0	623.5	623.2	624.2	622.8	629.5	621.4	619.4	622.0	624.3	625	
$\frac{12}{47}$	Ö	623.2	624.0	624.2	623.8	622.0	627.0	621.2	619.2	622.2	624.0	625	
$\frac{1}{52}$	ŏ	624.0	625.0	624.0	623.6	635.4	626.8	621.4	619.0	622.3	624.0	625	
57	ŏ	623.2	624.8	624.5	623.8	639.8	625.8	621.6	622.0	622.0	624.0	625	
${f T}$ hermo	meter	63.8	63.8	63.8	63.9	63.8	63.6	63.4	63.0	62.6	62.4	61.8	
37	s.	One s	Scale Divisio	on = '0000	063 parts of	f the V.F.	·	<u> </u>		VERTICAL	Force.		
М.	<b>5.</b>		1	1	<u> </u>	1	1			1			
3	0	137.3	138.4	138.4	136.4	135.6	130.1	132.7	133.0	133.8	134.8	134.8	
8	0	137.4	138.4	138.4	136.0	135.6	130.1	132.8	133.0	134.0	134.8	134.8	
13	0	137.4	138 4	137.6	136.2	135.6	130.1	132.8	133.0	134.0	134.8	135 4	
18	0	137.4	138.4	137.6	136.2	135.5	129.6	132.8	133.2	134.0	134.8	135.4	
23	0	137.4	138.4	137.6	136.2	135.5	129.6	132.8	133.2	134.9	134.8	135'3	
28	0	137.4	138.4	137.6	136.0	135.5	129.6	133.0	133.2	134.9	134.8	135.0	
33	0	138.1	138.4	136.6	136.0	135.5	129.5	133.0	133'2	134.9	134.8	134.7	
38	0	138.0	138.4	136.5	135.7	135.5	129.5	133.0	133'2	134.9	134.8	134.7	
43	0	138.4	138.4	136.5	135.7	135.5	129.5	133.0	133.2	134.8	134.8	134.7	
48	0	138.4	138.4	136.5	135.7	135.8	132.7	133.0	133.2	134.8	134.8	134.7	
<b>5</b> 3	0	138.4 138.4	138.4 138.4	136 <b>·4</b> 136 <b>·4</b>	135.6 135.6	131.3 131.3	132.7 132.7	133.0 133.0	$133.2 \\ 133.8$	134.8	134.8	134°7 134°7	
58	0						104 /	199 0				$\frac{1347}{62.7}$	
Thermon	meter	62.8	63.0	63.0	63.6	63°7	$6\mathring{3}$ $\cdot$ $5$	63.4	63.5				

	-	·			PICAL OB					tember 20th	<del></del>
	DECLINAT	CION.			1		<b>A</b> ng	gular Value	of one Scale	Division =	: 0′ • 721.
22h.	23h.	Oh.	1h.	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8h.	9h.
Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
	116.2		122 0								110
				122 4							111.0
	117.4		122.0	122 2	110.4				107.0	109.2	111.6
			122.6								112.0
											112.6
			123.2						108.0	109.2	112.4
				123.0							112.4
116.4	120.1	121.2	124.8	122.8	119.4			107.8			112.4
											112.6
											112.6
116.6	120.4	123.1	123.4	120.5	117.6	114.0	109.2	107.7	108.8	111.0	112.8
	Horizont	AL FORCE		]	Increase, in	Scale Divisi	ons, corresp	onding to 1	decrease of	Temperatur	e, 1°63.
COC: "	000:0	025:0	C10:0	C11:0	1 001:0	1 505.7	1 507:0	000:0	1 000:0	C01:0	C00:0
											628.0
						II.					627.8 $625.0$
											623.0
			615.4								622.5
			614.0								623.0
627.0	629.0	623.5	612.5		595.0				614.0	623.0	623.0
											623 0
		622.0								623.2	624.5
											625.0
											625.0
629.7	626.9	619.8	611.2	601.2	595.0	596.6	602.0	608.0	620.5	625.3	625 (
6j.3	6j.0	61.1	60°.6	60°2	60°6	61.2	6 <u>1</u> .6	62°0	62°0	6 <b>i</b> °5	62.0
	VERTICAL	Force.		I	ncrease, in S	Scale Divisi	ons, corresp	onding to 1°	decrease of	Temperatur	e, 1°64.
194•1	126.7	197.5	138.8	140.8	130.2	130.1	130.1	130.5	140.7	141:5	141.8
				141.9		139.1	139.1	139.2		141.5	141.5
194 1											141.5
											141.5
	137.1										141.8
											141.8
		138.5								142.4	141 3
											141.8
											141.3
		138.8	140.0	139.9	138.6	139.1	139.7	139.2	141.5	142.3	140.8
136.7	137.5	138.8	140.8	139.9	138.6	139.1	139.7	139.4	141.5	141.9	140.8
136.7	137.2	138.8	140.8	139.9	138.6	139.1	139.7	139.4	141.2	141 9	140.8
62°4	62.5	62.0	61.2	60°7	6j.3	6 <u>1</u> .3	6η5	6i°5	61.2	6η5	61.5
	Se. Div. 113 '0 113 '0 113 '0 113 '8 115 '4 115 '8 116 '0 116 '5 116 '4 115 '9 116 '4 115 '9 116 '4 116 '6  626 '5 626 '0 625 '5 626 '8 626 '8 627 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0 628 '0	Sc. Div. 116.7 113.0 116.7 113.0 116.5 113.8 116.9 115.4 117.4 115.4 117.7 115.8 118.2 116.0 118.4 116.5 119.3 116.4 120.1 115.9 120.4 116.4 120.4 116.6 120.4  HORIZONT     Capacita	Sc. Div.   Sc. Div.   120'4   113'0   116'7   120'4   113'8   116'9   120'6   115'4   117'4   121'4   115'8   118'2   121'4   115'8   118'2   121'4   115'8   118'2   121'4   116'0   118'4   121'5   116'5   119'3   121'6   116'4   120'1   121'2   115'9   120'4   122'4   116'6   120'4   122'4   116'6   120'4   123'1	Sc. Div.   Sc. Div.   Sc. Div.   113 '0   116 '7   120 '4   122 '6   113 '0   116 '5   120 '4   122 '2   113 '8   116 '9   120 '6   122 '0   115 '4   117 '4   121 '4   122 '2   115 '4   117 '7   121 '4   122 '2   115 '4   117 '7   121 '4   122 '2   115 '8   118 '2   121 '4   122 '4   116 '0   118 '4   121 '5   123 '2   116 '5   119 '3   121 '6   124 '0   116 '4   120 '1   121 '2   124 '8   115 '9   120 '4   121 '7   123 '4   116 '4   120 '4   122 '4   123 '6   116 '6   120 '4   123 '1   123 '4   116 '6   120 '4   123 '1   123 '4   116 '6   120 '4   123 '1   123 '4   116 '6   120 '4   123 '1   123 '4   166 '6   120 '4   123 '1   123 '4   167 '6   167 '2   166 '5   628 '0   626 '0   618 '7   626 '5   628 '0   624 '0   616 '2   626 '8   629 '0   623 '5   615 '4   626 '8   629 '0   623 '5   615 '4   626 '8   629 '0   623 '5   615 '4   628 '0   627 '1   622 '0   611 '2   628 '0   627 '1   622 '0   611 '2   628 '0   627 '1   622 '0   611 '2   628 '2   627 '5   620 '0   611 '0   629 '7   626 '9   619 '8   611 '2   629 '7   626 '9   619 '8   611 '2   61 '3   61 '0   61 '1   60 '6   61 '3   61 '0   61 '1   60 '6   61 '1   60 '6   61 '1   60 '6   61 '1   60 '6   61 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60 '1   60	Sc. Div.   Sc. Div.   Sc. Div.   Sc. Div.   113 0   116 7   120 4   122 6   122 2   123 4   113 0   116 7   120 6   122 2   122 4   113 8   116 9   120 6   122 0   122 2   125 4   115 4   117 4   121 4   122 2   122 8   115 4   117 7   121 4   122 6   123 0   115 8   118 2   121 4   122 4   124 0   116 0   118 4   121 5   123 2   123 5   116 5   119 3   121 6   124 0   123 0   116 4   120 1   121 2   124 8   122 8   115 9   120 4   121 7   123 4   122 4   126 1   16 4   120 1   121 7   123 4   122 4   116 6   120 4   123 1   123 1   123 4   120 2   116 6   120 4   123 1   123 1   123 4   120 2   116 6   120 4   123 1   123 1   123 1   123 1   120 2   120 1   120 1   121 2   124 8   120 2   120 1   120 1   123 1   123 1   123 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   120 1   1	Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   113'0   116'7   120'4   122'6   122'8   120'0   113'0   116'5   120'4   122'0   122'2   122'4   119'4   113'8   116'9   120'6   122'0   122'2   122'8   119'4   115'4   117'4   121'4   122'2   122'8   119'4   115'4   117'7   121'4   122'6   123'0   119'3   115'8   118'2   121'4   122'6   123'0   119'3   115'8   118'2   121'4   122'6   123'0   119'4   116'0   118'4   121'5   123'2   123'5   119'4   116'5   119'3   121'6   124'0   123'0   119'4   116'5   119'3   121'6   124'0   123'0   119'4   116'4   120'1   121'2   124'8   122'8   119'4   116'4   120'1   121'2   124'8   122'4   118'9   116'4   120'4   122'4   123'6   120'4   118'9   116'4   120'4   122'4   123'6   120'4   118'4   116'6   120'4   123'1   123'4   120'2   117'6          Horizontal Force.	Sec. Div.   Sec. Div.   Sec. Div.   Sec. Div.   Sec. Div.   113 '0   116 '7   120 '4   122 '6   122 '8   120 '0   116 '6   113 '0   116 '5   120 '4   122 '2   122 '4   119 '4   116 '4   113 '8   116 '9   120 '6   122 '0   122 '2   119 '4   116 '4   115 '4   117 '4   121 '4   122 '2   122 '8   119 '4   116 '0   115 '4   117 '7   121 '4   122 '6   123 '0   119 '3   115 '6   115 '8   118 '2   121 '4   122 '4   124 '0   119 '4   115 '0   116 '0   118 '4   121 '5   123 '2   123 '5   119 '4   115 '0   116 '0   118 '4   121 '5   123 '2   123 '5   119 '4   115 '2   116 '5   119 '3   121 '6   124 '0   123 '0   119 '4   115 '0   116 '4   120 '1   121 '2   124 '8   122 '8   119 '4   115 '0   115 '9   120 '4   121 '7   123 '4   122 '4   118 '9   114 '5   116 '4   120 '4   122 '4   123 '6   120 '4   118 '4   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   116 '6   120 '4   123 '1   123 '4   120 '2   117 '6   114 '0   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120 '1   120	Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   113'0   116'7   120'4   122'6   122'8   120'0   116'6   113'8   113'0   116'5   120'4   122'2   122'4   119'4   116'4   113'4   113'8   116'9   120'6   122'0   122'2   119'4   116'4   112'5   115'4   117'4   121'4   122'2   122'8   119'4   116'0   111'9   115'4   117'7   121'4   122'6   123'0   119'3   115'6   111'5   115'8   118'2   121'4   122'4   124'0   119'4   115'0   110'5   116'0   118'4   121'5   123'2   123'5   119'4   115'2   110'4   116'5   119'3   121'6   124'0   123'0   119'4   115'2   110'4   116'5   119'3   121'6   124'0   123'0   119'4   115'2   110'4   116'4   120'1   121'2   124'8   122'8   119'4   115'4   110'4   116'4   120'1   121'2   124'8   122'8   119'4   115'0   110'8   115'9   120'4   121'7   123'4   122'4   118'9   114'5   110'4   116'4   120'4   122'4   123'6   120'4   118'4   114'0   109'7   116'6   120'4   123'1   123'4   120'2   117'6   114'0   109'5   116'6   120'4   123'1   123'4   120'2   117'6   114'0   109'5   116'6   120'4   123'1   123'4   120'2   117'6   114'0   109'5   116'6   120'4   123'1   123'4   120'2   117'6   114'0   109'5   116'6   120'4   123'1   123'4   120'2   117'6   114'0   109'5   116'6   120'4   123'1   123'4   120'2   117'6   114'0   109'5   116'6   120'4   123'1   123'4   120'2   117'6   114'0   109'5   116'6   120'4   123'1   123'4   120'2   117'6   114'0   109'5   116'6   114'0   109'5   116'6   114'0   109'5   116'6   114'0   116'4   116'4   116'4   116'4   116'4   116'4   116'4   116'4   116'4   116'4   116'4   116'4   116'4   116'4   116'4   116'4   116'4   110'4   116'4   110'4   116'5   110'4   116'5   110'4   116'5   110'4   116'5   110'4   116'5   110'4   110'4   116'5   110'4   116'5   110'4   110'4   116'5   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   110'4   11	Sc. Div.   Sc. Div.   Sc. Div.   Sc. Div.   Sc. Div.   Sc. Div.   Sc. Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.	Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. 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Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.	Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   T. Se. Div.   Se. Div.   Se. Div.   Se. Div.   T. Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. Div.   Se. 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Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   Div.   D

Vol. III.

October 18th	and 19th.			MAGNE	TICAL OB	SERVATI	ons.				
Mean Göttinge	n A	ngular Value o	of one Scale	Division =	0′ • 721.				DECLINAT	ion.	
Time.	10h	. 11 ^h .	12 ^h .	13 ^h .	14 ^h .	15h.	16 ^h .	17 ^h .	18h.	19 ^h .	20 ^h .
M. S. O O O O O O O O O O O O O O O O O O	se. D 93' 104' 93: 106' 101' 95' 98' 106' 120'	4   115.8 3   120.4 7   109.4 4   101.8 6   110.6 4   103.5 4   95.9 4   95.9 98.9	Sc. Div. 98 '2 113 '8 121 '5 118 '4 113 '4 110 '4 108 '4 103 '5 105 '2	Sc. Div. 92.5 104.8 109.4 125.8 136.4 161.8 108.4 78.6 101.8	Sc. Div. 118'8 124'2 125'4 118'6 102'8 99'2 101'4 106'8 104'5	Sc. Div. 122°0 119°8 114°8 122°2 124°8 120°4 111°2 111°0 111°8	Sc. Div. 127 ' 4 123 ' 6 121 ' 8 117 ' 7 116 ' 4 116 ' 4 116 ' 8 115 ' 7	Sc. Div. 100°5 90°4 119°8 123°4 124°4 100°4 87°4 100°4 95°4	Sc. Div. 105 0 107 8 98 4 109 4 110 8 115 0 114 4 113 4 107 9	Sc. Div. 82'0 83'4 89'4 87'4 91'0 91'2 102'4 121'6 139'0	Sc. Div. 65 0 78 0 92 0 107 0 137 0 130 8 123 2 130 0 139 0
$egin{array}{ccc} 45 & 0 \ 50 & 0 \ 55 & 0 \ \end{array}$	123° 115° 118°	4 94.2	105.6 104.3 106.4	108.4 126.4 125.2	105.8 109.4 119.2	115.4 126.0 129.5	107.6 121.8 118.8	94.4 98.4 102.4	97.4 85.4 78.4	120°4 83°4 65°0	139.6 141.8 147.0
M. S.	0	ne Scale Divisi	ion = '0000	087 parts of	the H.F.				Horizont	AL FORCE	
2 0 7 0 12 0 17 0 22 0 27 0 32 0 37 0 42 0 47 0 52 0 57 0	679° 700° 687° 692° 733° 742° 790° 770° 800° 767° 813° 770°	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	830°0 879°0 787°0 782°0 725°0 730°0 686°0 700°0 700°0 701°2 680°0 691°0	676°5 758°8 808°4 758°5 827°4 938°4 722°0 655°4 694°4 720°2 668°8 652°4	625 '4 623 '4 621 '8 618 '5 606 '2 620 '8 617 '6 614 '4 621 '5 621 '7 630 '2 635 '4	648*4 629*2 614*2 594*0 593*2 594*0 596*2 596*0 587*8 590*3 597*2 594*2	593 '4 598 '3 601 '0 599 '0 598 '0 592 '0 590 '0 590 '0 560 '4 535 '0 571 '0 573 '5	565 0 573 0 597 0 624 4 624 6 585 0 551 0 552 0 544 0 546 2 543 8 543 8	552.0 572.2 538.6 537.2 530.0 542.4 564.0 568.2 525.0 550.0 540.0 510.5	560°0 500°5 502°7 443°0 393°0 388°3 422°5 455°3 437°8 505°0 515°0 492°0	529'8 478'8 525'0 531'5 548'0 520'0 517'5 547'5 535'0 524'0 496'5 478'5
Thermomete	$\frac{1}{2}$	9   52.9	52.9	53.0	53.5	53.4	53.6	53.2	53.2	53.4	53.2
м. s.	C	ne Scale Divis	ion = .0000	063 parts of	the V.F.				VERTICAL	Force.	
3 0 8 0 13 0 18 0 23 0 28 0 33 0 38 0 43 0 48 0 53 0	276° 295° 288° 284° 303° 312° 315° 330° 312° 335° 334°	3 292.7 2 287.8 2 292.5 1 280.0 0 292.1 0 305.0 0 305.0 314.5 2 304.1 5 304.9	336·5 327·3 317·1 321·6 317·0 318·6 305·7 312·0 306·8 304·7 294·2 294·5	269°3 281°8 277°8 264°2 251°5 216°4 202°5 248°4 256°1 268°0 276°3 279°4	270°1 269°5 261°4 255°2 259°6 268°1 268°3 262°1 269°8 274°6 269°4	276 · 9 264 · 4 268 · 5 261 · 5 259 · 0 256 · 3 257 · 2 258 · 3 257 · 5 266 · 3 266 · 4 263 · 0	259.6 259.6 259.1 258.1 258.1 257.6 257.6 251.9 237.6 236.4 234.6 234.6	223.0 226.4 237.5 233.2 232.7 204.8 216.2 211.6 211.6 211.6	219 · 1 219 · 7 228 · 2 228 · 2 223 · 1 223 · 1 219 · 3 219 · 3 203 · 2 204 · 3 201 · 0 287 · 7	201.0 207.3 190.2 165.0 163.9 170.0 181.3 169.5 141.7 167.0 161.6 184.4	184.0 193.0 191.8 184.0 149.8 141.1 154.6 168.5 157.0 157.2 159.3 163.0
Thermometer	$\mathbf{r}  \boxed{ 52^{\circ}}.$	$7 \int 52.7$	53.9	54.0	54.5	5 ⁴ .0	54.2	5 <b>4</b> .6	54°4	54.6	55°·2

		DECLINAT	ION.					$oldsymbol{\Lambda}$ ng	ular Value	of one Scale	Division =	0' 721.
21 ^h .	22h.	23h.	O ^{li} .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 h.	8h.	9 ^h .
c. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Se. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Se. Div. 107.4	Sc. Div
46.5	136.0	117.4	93.5	106.4	111.6	120.0	110.6	115.0	109.4	110.6	107.4	110.0
50.4	133 · 4 129 · 8	120°4 118°6	83.2	108.8	113.4	120.4	119.0 112.5	109.4	109.9	113.4	108.0	109.0
63 <b>°</b> 8 59 <b>°</b> 4	123.4	117.4	78.0	105.4	115°5 117°4	118'4 117'6	112.3	111.5	110.0	108.4		108.9
47°0	120.0	111.4	78.4	116.0	116.4	111.4	112.8	111.0	110.4	109.8	110.3	107.7
47.4	127.2	114.4	89.4	121.2	117.6	114.4	113.8	108.8	111.5	108.0	110.9	106.6
50.4	125.9	113.3	90.5	117.4	118.4	116.6	110.8	108.2	109.4	108.0	111.0	106.6
47.4	124.4	113.0	91.6	118.8	118.8	118.4	110.8	109.4	107.0	109.5	110.4	107.6
41.0	107.0	114.4	98.0	120.4	119.6	121.4	111'4	114.4	108.0	109.4	109.6	107.4
37.0	105.2	104.4	98.4	114.8	119.8	118.4	112.8	110.6	108.4	109.0	110.0	107.6
37.5	114.9	101.5	97.0	115.4	117.4	118.9	113.4	111.5	110.8	110.4	109.8	108.3
37.0	112.4	92.2	103.2	115.4	118.4	120.1	112.6	110.4	110.5	110.3	109.6	109.7
		Horizont	AL FORCE.			ncrease, in	Scale Divisi	ons, corresp	onding to 1°	decrease of	f Temperatui	re, 1.63.
00.0	535.5	586.0	548.5	587.0	589.6	581.2	578.0	587.0	593.2	608.4	595.5	611.2
48.0	561.6	604.0	545.0	588.8	593.8	579.4	579.0	592.0	591.0	607.0	597.2	613.0
85.5	560.4	589.5	519.0	575.5	591.5	574.5	577.5	590.0	591.0	609.0	597.0	622.0
68.8	571.5	587.0	516.0	591.2	591 2	576.0	581.0	590.0	602.0	605'4	598.2	620.5
81.0	567.5	584.2	521.5	594.5	589'4	572.0	590.0	590.0	600.0	597.5	598.0	625.0
11.9	589.5	585.0	521.5	604.2	588.8	570.0	591.0	590.0	593.8	615.0	605.0	624.0
17:0 20:0	565.0	583°0 587°0	558°3 557°5	601.8	588°2 583°8	569°0 570°5	591°0 595°0	590°2 593°0	599.2	603 <b>·</b> 5 597 <b>·</b> 0	612.0	616.5
26·0	573.5	585.0	579.0	601.4	584.6	578.5	592.2	604.5	598.0	591.0	612.2	609.0
53.0	577.5	567.5	575.0	598.6	583.8	580.2	591.5	602.0	598.0	589.5	611.0	609.0
26.0	591.0	559.5	570.0	601.2	581.4	586.0	586.0	594.4	598.2	587.5	610.0	609.8
23.0	586.0	554.2	590.0	600.7	580.2	577.7	592.0	590.2	599.2	591.6	610.2	611.3
5å·0	52°8	52°6	52.9	52.9	52.8	5 <b>2°</b> 9°	52.9	53.5	53.2	53.2	5 <b>4°3</b>	54.2
		VERTICAL	Force.		I	ncrease, in S	Scale Divisio	ons, correspo	onding to 1°	decrease of	Temper <b>a</b> tur	e, 1°64.
50.9	196.9	223.8	214.3	218.4	232.7	238.4	248.0	238.0	237.8	245.3	242.4	240.8
78.7	210.9	232.2	219.5	219.0	232.9	237.9	248.0	238.0	237.8	245.3	242'4	240.8
77:3	213.0	224.3	209.3	225.2	235.2	239.7	248.0	238.0	237.8	243 1	242.4	242.6
79 <b>·3</b> 72·7	228.0	224.3	210.8	228.4	235.2	238.1	248.0	238.0	238.5	243.6	242.4	242.6
69 <b>·</b> 9	230.4	$\begin{vmatrix} 224.3 \\ 224.3 \end{vmatrix}$	$\begin{vmatrix} 210.4 \\ 202.2 \end{vmatrix}$	227 · 9 227 · 9	$\begin{vmatrix} 235.2 \\ 234.3 \end{vmatrix}$	238·1 240·0	248.0	$238.2 \\ 238.2$	239.4	244.6	240.8	$243.1 \\ 243.3$
70.0	232.2	225.6	208.7	228.4	234.1	339.2	240.7	238.2	239.7	245.8	240 3	243.2
72.0	231.1	230.7	214.3	229.9	226.0	239.2	240.7	238.2	239.7	243.7	241 1	242.0
73.0	227.0	228.5	212.4	230.1	236.3	239.9	241.7	240.1	239.7	243.7	241.1	242.0
75.4	222.5	221.2	218.2	230.1	236.4	241.6	241.5	240.1	243.1	243.2	241'1	242.0
	228.4	219.6	214.2	231 4	238.5	241.6	238 1	237.8	241.7	242.4	240'8	243.2
	227.4	219.0	216.2	231.4	238.4	242.8	238.1	237.8	241.7	242.4	240.8	243.2
78:5 86:1	·	54.2	54.2	54.2	53.6	53.3	53.2	53.7	53.7	54.5	54.5	54.7

Novemb	per 24th an	nd 25th.			MAGNET	ICAL OBS	SERVATIO	)NS.				
Mean Gö		Ang	gular Value	of one Scale	Division =	: 0' .721.				Declinati	ON.	
Tim	ie.	10 ^h .	11 ^h .	12 ^h .	13 ^h .	14 ^h .	15 ^h .	16 ^h .	17 ^h .	18h.	19 ^h .	20 ^h .
M. 0 5 10 15 20 25 30 35 40	s. 0 0 0 0 0 0 0 0 0 0 0	Sc. Div. 111.4 110.4 111.4 111.2 111.4 110.2 111.4 110.4 111.2 111.4 111.2	Sc. Div. 111 '2 110 '4 111 '6 111 '5 111 '2 111 '8 111 '8 111 '8 112 '4 112 '0	Sc. Div. 112 '2 112 '4 112 '5 113 '4 113 '5 112 '2 114 '2 113 '4 113 '4	Sc. Div. 113.5 114.2 114.2 114.4 114.2 114.0 113.8 113.5 113.4 112.6	Sc. Div. 113.6 113.4 113.5 113.3 113.4 113.4 113.4 113.4 113.3 113.3	Sc. Div. 113.4 113.0 113.4 113.0 113.0 112.4 112.4 112.2 112.0 112.2	Sc. Div. 112.0 111.7 111.5 111.6 111.6 111.6 111.6 111.6 111.6 111.5 111.5	Sc. Div. 111.4 111.4 111.3 111.3 111.4 111.8 111.6 111.6 111.5 111.8	Sc. Div. 111'8 112'3 112'4 111'9 112'4 112'0 112'4 112'3 112'4 113'0	Sc. Div. 113.3 113.4 113.4 113.6 113.5 113.2 112.6 112.0 112.0 112.3 112.7	Sc. Div. 113 0 113 0 112 9 111 8 113 0 113 5 112 0 111 3 110 4 109 3
50 55	0	111.5	111.8	113.4	113.8 113.4	113.4	111.8 111.8	111.6	111.8	113.3	113.0	108.4 109.4
м.	s.	One	e Scale Divi	sion = '00	00087 parts	s of the II. I	 F.			Horizont.	AL FORCE.	
2 7 12 17 22 27 32 37 42 47 52 57	0 0 0 0 0 0 0 0 0 0 0 0	631·2 631·5 631·0 629·2 631·8 631·2 628·2 626·8 632·2 632·5 630·8 630·2	630°2 630°2 631°2 631°2 630°2 630°2 630°2 630°0 631°8 631°8 631°0	631·2 631·2 632·2 632·4 631·2 633·2 635·4 636·0 632·8 632·2 633·8 635·0	632·2 632·2 633·4 634·0 634·2 633·0 631·4 631·2 630·8 631·0 632·4	633.0 633.2 633.2 632.2 631.8 632.2 632.4 631.2 631.4 631.7 631.8 632.0	631.2 631.2 631.8 632.0 632.0 631.8 632.0 631.8 630.0 630.2 630.3 631.0	631.5 631.1 631.0 631.2 631.0 630.0 630.8 630.2 629.8 630.0 629.7	631.0 631.0 631.0 631.0 630.5 629.5 630.0 630.0 629.0 631.5 633.0 631.3	631.0 631.0 629.0 629.0 630.0 629.2 630.0 630.1 630.2 629.0 629.7 630.2	630.5 631.0 631.0 631.1 632.5 633.5 635.0 631.0 631.5 632.0 632.5 632.2	636 ° 0 635 ° 0 635 ° 0 637 ° 1 637 ° 0 633 ° 0 635 ° 0 632 ° 0 632 ° 0 632 ° 0 635 ° 0
${ m The}^{{ m rm}\alpha}$	ometer	52°8	53.6	54.1	55.0	55.0	55.0	55.0	54.8	54.4	54.4	54.6
м.	s.	One	Scale Divis	ion = '00	0063 parts	of the V. F.				VERTICA	L FORCE.	
3 8 13 18 23 28 33 38 43 48 53 58	0 0 0 0 0 0 0 0 0 0 0 0	239 · 1 238 · 3 237 · 8 237 · 8 237 · 0 236 · 5 236 · 1 235 · 4 335 · 4 235 · 0 235 · 0	235 ° 0 235 ° 3 235 ° 3 235 ° 3 234 ° 0 233 ° 9 233 ° 9 233 ° 3 233 ° 3 233 ° 9 234 ° 1	234'1 234'9 234'9 234'9 235'0 235'0 235'0 235'0 234'2 233'1 233'1 233'1	233 · 1 233 · 1 232 · 7 232 · 7 232 · 7 232 · 2 232 · 2 232 · 2 232 · 1 232 · 3 232 · 3 232 · 3	232·5 232·5 232·7 232·7 232·7 232·1 232·1 232·1 232·1 232·1 232·1	231.6 231.6 231.6 231.6 231.6 231.6 231.6 231.6 230.6 230.6 230.6	230.6 231.4 231.4 231.5 231.5 231.5 231.7 232.9 232.9 232.9 232.9	232 '9 232 '9 232 '9 232 '9 232 '9 233 '1 233 '1 235 '0 235 '0 235 '0 235 '0	235 0 235 0 234 6 234 6 234 6 234 6 234 6 233 0 233 0 232 7 232 0 232 0	232.0 232.0 231.6 231.6 231.6 231.6 231.6 231.6 231.6 231.6 231.6 231.6 231.6	230 '7 230 '7 230 '7 230 '7 230 '7 229 '9 230 '0 229 '5 229 '5 229 '5 228 '2 228 '2
Therm	ometer	52.2	54.2	55.2	56°0	55.7	55.8	55.8	55.7	55.3	56.2	5 <b>6</b> °8

		DECLINAT	ION.					Ang	ular Value	of one Scale	Division =	: 0' • 721.
21h.	22 ^h .	23 ^h .	O ^h .	1 ^h .	2 ^h .	3 ^h .	4 ^h .	5 ^h .	6 ^h .	7 ^h .	8 ^h .	9 ^h .
		<u> </u>	<u> </u>	!	<del>!</del>	ļ	<u> </u>	1	1 0.		<del>!</del>	<u> </u>
Sc. Div.	Sc. Div. 118.5	Sc. Div. 123'4	Sc. Div. 120'2	Sc. Div. 117°2	Sc. Div.	Sc. Div. 119°0	Sc. Div.	Sc. Div. 108 7	Sc. Div. 105*6	Sc. Div. 106'4	Sc. Div. 109 4	Sc. Di 111
10.2	118.3	123.2	119.5	120.4	120.4	117.4	113.4	108.8	106.4	106.6	109.0	iii
12.4	112.6	122.4	120.3	118.4	120.4	112.4	113.3	109.4	106.5	107.2	109.8	112
14.3				118.8	120.0	113.4	114.4	108.5	106.3	107.0	109.7	112
14.4				116.4	121.6	115.0	113.2	107.6	106.3	107.4	110.1	112
18.2	116.5	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	119.0	121.8	116.0	112.2	106.6	106.0	107.5	110.4	112	
19.6			118.4	126.0	114.4	111.6	106.6	105.6	108.4	110.4	113.5	
21.6	115.5		120.3	123.8	117.4	111.4	107.4	105.6	108.2	110.4	113.4	
22.2	117.4     118.3     119.4     118       115.5     119.7     119.5     120       120.0     119.2     119.2     121       118.6     120.2     119.4     122       120.5     119.2     118.6     121	121.8	123.5	113.7	110.4	107.0	105.4	109.0	110.4	113.5		
22.0		122.0	122.8	113.6	110.0	106.2	106.2	109.6	110.8	113.3		
120'4		121.2	125.4	114.0	110.0	106.6	106.5	109.4	111.1	113		
120.4	120.8	119.0	117.8	121.4	125.6	114.4	109.4	105.7	105.4	109.6	111.4	113
		1	AL FORCE.	1		1	1			1	Temperatur	i
638.0	642.0	640.8	640.2	629.0	633.3	618.0	613.2	613.5	618.2	629.0	635.0	638
538 <b>.2</b>	$637^{\circ}2$	640.0	637.3	631.2	626.0	610.0	612.5	615.0	621.2	630.0	635.0	638.0
641.1	638.9	640.5	639.0	633.5	627.0	618.0	613.0	616.0	623.0	629.0	635.8	637 9
643.7	637.5	640.2	641'4	631.0	627.4	619.0	613.0	618.0	623.0	630.0	636.2	637.0
39.0	640.2	638.5	639.5	631.0	623.9	618.0	614.0	619.0	624.0	632.0	636.0	637 8
642.0	640.2	637.8	638.7	630.0	624.0	620.0	614.3	618.2	625.0	630.0	637.0	636.9
641.0	641.2	638.0	639.4	629.8	625.0	607.5	614.0	620.0	625.0	630.0	637.0	636.0
543.5	640.5	640.2	637.8	631.0	625.2	618.0	615.0	619.0	626.0	631.0	637:0	634
341.0	639.9	638.8	638.0	629.0	627.0	621.0	614.5	618.2	628.0	632.0	637.0	636
640.0	641.8	640.0	638'4 633'4	628.8	626.8	617.0	614.0	620.5	627.5	631.0	637.0	637 ° 636 ° 6
640°0 642°0	$642.5 \\ 643.0$	638.8	634.0	628.0	623.0 622.8	614.0 615.0	615.5	619.0	$\begin{vmatrix} 632.0 \\ 632.0 \end{vmatrix}$	634.0	637.0	638
5 <b>4</b> °6	5 <b>4</b> °5	54.1	53.9	53.8	53.2	52°5	52.2	52.2	52.0	52.0	51.8	52.
· · · · · · · · · · · · · · · · · · ·		VERTICAL	Force.		'	ncrease, in	Scale Division	ons, corresp	onding to 1°	decrease of	Temperatur	re, 1°64.
228.2	228.7	227.5	228.2	230.5	236.9	237.4	239.0	239.7	240.9	241.9	242.0	242
227.1	228.7	227.8	228.2	230.2	236.9	237.4	239.0	239.7	240.9	241.9	242.0	242
227.0	228.6	227.8	228.2	230.7	236.2	238.1	238.4	239.7	240.9	241.9	242.0	242
225.2	228.6	227.8	228.2	230.7	235.9	238.1	238.4	239.7	241.6	241.9	242.4	242
23.3	228.6	227.8	229.4	230.7	235.9	238.1	238.4	239.7	241.6	241.9	242.5	242
223.3	228.6	228.1	229.4	232.0	235.5	239.0	238.4	239.7	241.6	241.9	242.5	242
224.1	228.1	228.1	229.4	232.0	235.5	236.4	239.7	239.7	241.6	241.9	242.5	242
226.1	228.1	228.1	229.4	232.0	235.5	238.5	239.7	239.7	241.6	241.9	242.5	242
226'1	227.7	228.1	229.7	232.8	235.5	238.5	239.7	239.7	241.6	242.0	242.5	242
228.9	227.7	228.2	229.7	232.8	235.5	238.5	239.7	240.0	241.6	242.0	242.5	242
227.4	227.7	228.2	230.0	232.8	234.8	238.5	239.7	240.9	242.3	242.0	242.5	242
228.4	227.5	228.2	230.5	232.8	234.8	238.2	239.7	240.9	242.3	242.0	242.2	242:3
	56°4	55.6	56°3	55.4	53.9	53.0	52.2	52°7	52.2	52.2	52°·2	52.5

December 20th	and 21st.			MAGNET	TICAL OBS	SERVATIO	ons.				
Mean Göttingen	Ang	gular Value	of one Scale	Division =	= 0' .721.				Declinat	ion.	
Time.	10h.	11h.	12h.	13h.	14h.	15h.	16 ^h •	17h.	18h.	19 ^h .	20h
M. S.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Di
0 0	109.8	111.8	112.6	112.4	114.3	114.4	114'4	115.6	113.6	112.8	113
5 - 0	110.0	112.0	112.6	112.6	114.1	114.4	114.4	115.8	113.6	113.5	113
10 0	110.4	112.0	112.2	112.9	114.2	114.4	114.4	115.4	114.6	113.2	113.6
15 0	110.0	112.6	112.5	112.9	114.4	114.4	114.4	116.4	114.6	113.4	113
20 - 0	110.4	112.3	112.6	113.2	114.4	114.4	114.4	116.4	114.4	112.8	113
25 - 0	110.4	112.4	112.7	113.4	114.4	114.6	115.5	116.2	114.3	112.4	113
30 0	110.6	112.4	112.7	114.3	114.4	114.9	115.2	116.2	114.0	112.4	113
35 - 0	110.9	112.4	112.6	114'4	114.4	114.4	115.2	115.8	112.8	112.8	114
40 0	110.9	112.2	112.4	114.2	115.2	114.4	115.4	116.4	113.4	113.0	114
45 - 0	111.0	112.4	112.3	114.2	115.1	114.4	115.2	115.8	114.0	113.4	113
50 <b>0</b>	111.5	112.4	112.4	114.5	115.4	114.4	115.2	114.8	114.2	113.6	113
<b>55</b> 0	111.6	112.4	112.3	114.2	114.5	114.4	115.4	113.6	113.3	113.8	113.
M. S.	One	e Scale Divis	sion = '00	0087 parts	of the II. F.				Horizon	CAL FORCE	
2 0	664.0	663.5	663.0	660.0	661.4	663.1	662.0	663.0	661.6	666.6	668
$\begin{array}{ccc} 2 & 0 \\ 7 & 0 \end{array}$	665.0	663.5	663.0	661.0	662.2	662.9	662.0	661.8	662.2	667.4	668
	665.2	663.5	663.0	660.3	662.0	663.1	662.2				
	665.0	664.0	663.0	660.3	662.0	663.0	$\frac{662 \cdot 2}{662 \cdot 2}$	662.2	663.0	666.9	668
$\begin{array}{cc} 17 & 0 \\ 22 & 0 \end{array}$	663.1	664.0	662.2	660.2	662.0	663.0	662.0	663.2	663.8	667.0	
	662.5	664.0	662.3	660.2	663.0	663.0	662.0	663.2	664.0	667.5	668
	663.5	663.4	663.0	660.0	663.0	663.0	663.0	663.8	665.4	667.8	668
	664.0	663.4	663.0	660.8	663.0	662.5	662.8		1	668.0	
$egin{array}{ccc} 37 & 0 \ 42 & 0 \end{array}$	664.2	663.2	663.0	660.3	664.0	662.7	662.8	663.2	665.5	667.4	669
	664.5	663.0			664.0	662.2					669
$egin{array}{ccc} 47 & 0 \ 52 & 0 \end{array}$	664.1	663.0	662.9	661.7	664.0	663.0	662.4	664.2	665.8	667.4	668
								663.0	666.6	667.2	667
57 O	664.0	663.0	660.5	662.0	664.0	662.0	662.0	661.2	667.2	667 4	667
Thermometer	47°4	48°3	48.7	48.7	48°.7	48.2	47.9	47.1	46.4	46°1	45
M. S.	One	e Scale Divis	sion = '00	00063 parts	of the V.F.	•			VERTICAL	Force.	
3 0	248.6	246.7	244.7	245.0	244.9	245.6	246.1	246.6	247.3	247.3	247
8 0	248.6	245.8	244.7	245.0	244.9	245.6	246.1	246.6	247.3	247.3	247
13 0	248.6	245.8	244.7	245.0	244.9	245.6	246.1	246.6	247.3	247 3	247
18 0	247.9	245.8	244.7	244.9	244.9	245.6	246.1	246.6	247.3	247.3	247 2
23 0	247.9	245.6	245.4	244.9	$\frac{211}{244.9}$	245.6	246.1	247.0	247.3	247.3	247
28 0	246.8	245.6	245.4	244.9	244.9	245.6	246.1	247.0	247.1	247.3	247
33 0	246.8	244.8	245.4	244.9	244.9	245.6	246.1	247.0	247 1	247.3	247 2
38 0	246.8	244.8	246.0	244.9	244.9	245.6	246.1	247.0	247.1	247.3	247.2
43 0	246.8	244.8	246.0	244.9	244.9	245.6	246.1	247.0	247.1	247 3	$\frac{247}{247}$
48 0	246.8	244.8	245.9	244.9	244.9	245.6	246 1	247.0	247.3	247 1	247
53 0	246.7	244.8	245.9	244.9	245.6	245.6	246 1	247.0	247.3	247 1	247
58 0	246.7	244.8	245.9	244.9	245.6	246.1	246.1	247.0	247.3	247 1	247
Thermometer	4 [°] 7.0	48.0	48.7	48.4	48.7	48.4	48.0	47.0	46.4	46°4	46.2

		DECLINAT	rion.					An	gula <b>r V</b> alue	e of one Scal	e Division =	= 0' 721
21h.	22h.	23h.	Oh.	1h.	2h.	3 ^h .	4 ^h .	5 ^h .	6h.	7 ^h .	8h.	9h.
Sc. Div.		Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div.	Sc. Div
113.2	115.0	107.6	107.4	101.9	117.5	121.6	119.1	114.8	110.8	109.5	109.4	110.4
113.3 113.3	116.4	107.4	110.4	102.3	115.6	123°0 122°9	118.1	117.4	111.4	108.8	109.4	110.8
107.8	116.4	103.4	108.6	105 4	118.6	122.9 $122.4$	118.4	115.4	111.3	109.0	109.4	110.4
115.9	115.6	100.7	108.6	107.4	118.4	121.6	118.5	115.8	111.4	107.4	109.3	110.9
16.0	116.3	96.6	106.7	109.4	120.4	122.4	117.4	115.4	111.0	107.0	109.3	111.9
17.9	117.3	96.4	106.4	109.4	121.4	122.4	117.4	112.4	110.4	108.7	109.2	111.4
117.9	119.4	91.9	105.6	110.0	121.2	121.6	116.4	110.3	109.2	109.0	109.2	111.6
1181	116.0	90.0	105.2	110.7	123.4	121.4	117.6	114.8	108.4	108.6	109.4	112.0
116.4	113.4	91.4	105.4	111'4	124.5	122.4	115.4	115.2	107.8	109.4	109.0	1111.4
116.6	111.6	95.4	101.4	115.2	123.3	119.4	117.0	116.4	108.4	109.6	109.2	111.9
114.4	111.5	102.4	101.3	116.4	122.4	119.3	117.4	112.8	110.4	109.4	110.0	112'4
667.0	664:0	HORIZONT		1	1	, , , , , , , , , , , , , , , , , , ,	1				f Temperatur	
667°2	664.0	658.0	682.0	671.0	660.0	658.5	652.0	$\begin{vmatrix} 651.2 \\ 650.2 \end{vmatrix}$	655.4	$\begin{vmatrix} 651.0 \\ 651.8 \end{vmatrix}$	653.0	664.0
367.2 - 367.2	668.2	652.0	686.0	670.0	662.0	661.0	651.2	651.1	656.2	$\frac{650.0}{650}$	654.0	663.8
375°0	671.0	650.0	687.0	669.0	664.0	659.6	651.8	$\frac{650.5}{650.5}$	654.2	651.8	650.0	670.0
667.4	668.5	650.5	688.1	666.1	664.0	658.5	652.8	654.2	655.2	655.0	654.0	670.4
667.8	669.0	649.1	684.0	665.2	663.2	658.0	650.5	654.0	652.5	655.2	656.0	666.8
668.5	671.5	666.5	681.8	666.0	665.0	658.0	648.8	652.2	652.2	651.0	659.0	666.8
69.0	671.0	675.0	679.5	663.6	664.0	656.0	647.8	648.4	656.8	648.0	660.0	667.4
669.0	669.8	678.5	676.0	663.0	663.0	657.0	647.2	642.3	658.0	650.0	661.0	667.0
666.2	661.3	678.0	678.0	664.0	663.0	655.0	647.4	645.2	659.8	651.0	664.0	667.2
365.8	660.0	681.0	674.0	663.0	661.0	652.5	647.2	646.2	652.6	650.5	669.2	666.0
66.6	655.1	680.5	672.0	663.0	660.8	653.0	649.4	655.0	651.5	651.0	671.0	662.2
46.0	46.0	46.3	46.5	45°.7	46.0	46.0	45.2	45°5	45°6	45°6	45.3	44.7
		VERTICAL	Force.		]	ncrease, in S	Scale Divisi	ons, corresp	onding to 1	decrease of	f Temperatur	e, 1°64.
247.1	238.7	234.9	223.9	235.5	242.2	246.6	247.4	248.3	248.5	248.9	251.7	251.6
247.1	237.9	234.7	226.9	235.5	242.5	246.6	247.4	248.3	248.2	248.9	251.7	251.6
47.1	237.9	230.5	228.7	235.5	242.2	247.4	247.4	248.3	248.5	248.9	251.7	251.6
47.9	237.9	226.8	230.6	237.0	243.7	247.4	247.4	248.3	248.5	249.2	251.6	251.6
47.5	237.9	225'1	231.7	238.5	243.7	247.4	247.4	248.3	248.0	251.7	251.6	251.6
47.5	237.6	222.8	231.7	239.4	243.7	247.4	247.4	248.3	248.0	251.7	251.6	251.6
47.5	237.6	225.9	232.0	239.4	243.7	247.4	247.4	248.0	249.0	251.7	251.6	251.6
47.5	237.6	225.9	232.2	239.4	245.4	247.4	247.4	248.0	249.0	251.7	251.6	251.6
47°5 41°5	237:3	224.3	232.2	240.7	245.4	247.4	247.5	247.5	249.6	251.7	251.6	251.6
41.5	237.0	222.0	233.6	240.7	246.2	247.4	247.5	248.7	249.6	251.7	251.6	251.6
41.8	237.0 235.2	222.0	235*5 235*5	$241.3 \\ 242.2$	246°2 246°6	247.4 247.4	$247.5 \\ 247.6$	248.0 248.5	$248.9 \\ 248.9$	$\begin{vmatrix} 251.7 \\ 251.7 \end{vmatrix}$	252.7 252.7	$\begin{array}{c} 251.6 \\ 251.5 \end{array}$
46°6	46.6	47.2	4 [°] 7.3	 47°4	46.4	46.0	45.4	45.6	45°6	45.4	$\begin{vmatrix} -\frac{\circ}{4\mathring{5}\cdot 2} \end{vmatrix}$	44.8

		•	
*			

## TORONTO, 1846 to 1848.

METEOROLOGICAL OBSERVATIONS.

ours of	Mean )	0	1			****	sh inches +					3.0	7.7
Time	gen	0		$\frac{2}{2}$	3	4	5	6	7	8	9	10	11
Toron Tim	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	1 2 3	In. 2.714 1.929 2.314	In. 2.684 1.907 2.356	In. 2 · 674 1 · 866 2 · 388	In. 2.638 1.872 2.416	In. 2.641 1.864 2.443	In. 2.619 1.865 2.439	In. 2:569 1:855 2:427	In. · 2·521 1·833 2·424	In. 2.489 1.829 2.421	In. 2.469 1.835 2.407	In. 2.419 1.845 2.427	In. 2:367 1:858 2:441
	4 5 6 7 8 9	2·694 3·002 2·370 2·393 2·562 2·470	2.716 3.016 2.360 2.415 2.547 2.470	2.732 3.024 2.330 2.425 2.556 2.465	2·748 3·032 2·304 2·453 2·584 2·454	2·791 3·035 2·300 2·447 2·594 2·443	2.797 3.034 2.275 2.451 2.590 2.414	2·804 2·983 2·227 2·447 2·572 2·378	2·798 2·953 2·215 2·454 2·561 2·328	2.806 2.919 2.201 2.462 2.555 2.298	2.832 2.911 2.200 2.478 2.555 2.278	2.845 2.895 2.186 2.493 2.551 2.232	2.855 2.861 2.214 2.514 2.544 2.267
ANUARY.	11 12 13 14 15 16 17	2·329 2·765 2·566 2·636 2·486 2·536	2:339 2:786 2:562 2:646 2:482 2:547	2:351 2:824 2:558 2:644 2:488 2:572	2:375 2:840 2:561 2:646 2:514 2:580	2:393 2:856 2:587 2:626 2:516 2:583	2.401 2.844 2.582 2.591 2.492 2.577	2:401 2:825 2:567 2:558 2:472 2:547	2:400 2:812 2:576 2:535 2:468 2:555	2:416 2:819 2:590 2:527 2:468 2:558	2·438 2·818 2·615 2·509 2·470 2·580	2.464 2.818 2.625 2.504 2.466 2.612	2:494 2:818 2:633 2:506 2:480 2:647
Jr	18 19 20 21 22 23 24	3·121 3·073 2·498 3·078 3·293 2·897	3.116 3.073 2.506 3.120 3.319 2.891	3.137 3.064 2.531 3.144 3.335 2.867	3·171 3·078 2·537 3·154 3·335 2·871	3·173 3·057 2·532 3·161 3·317 2·835	3.167 3.008 2.512 3.167 3.303 2.816	3·157 2·982 2·490 3·157 3·268 2·766	3·143 2·922 2·481 3·135 3·224 2·700	3:152 2:899 2:494 3:147 3:200 2:648	3.156 2.893 2.525 3.184 3.181 2.618	3·133 2·878 2·545 3·193 3·151 2·592	3°157 2°838 2°554 3°212 3°153 2°560
Feb.	25 26 27 28 29 30 31	2:340 2:618 2:571 2:675 2:268 2:540	2·322 2·638 2·583 2·679 2·262 2·590	2:322 2:670 2:609 2:671 2:270 2:656	2·320 2·701 2·631 2·668 2·242 2·692	2·319 2·718 2·659 2·656 2·231 2·739	2·281 2·724 2·658 2·633 2·225 2·766	2·273 2·714 2·660 2·598 2·225 2·778	2:240 2:702 2:655 2:552 2:215 2:776	2·238 2·678 2·643 2·556 2·215 2·794	2:246 2:664 2:658 2:546 2:201 2:824	2·266 2·663 2·676 2·506 2·204 2·861	2·298 2·655 2·690 2·508 2·200 2·901
	Means	2.6199	2.6271	2.6360	2.6451	2.6487	2.6382	2.6185	2.5992	2.5934	2.5960	2.5944	2.600
RY.	2 3 4 5 6 7 8 9 10 11 12 13	2:910 2:586 2:772 2:375 2:787 2:269 — 2:600 2:851 2:430 2:818 2:854	2:907 2:578 2:788 2:411 2:806 2:251 2:632 2:835 2:409 2:857 2:865	2 · 913 2 · 602 2 · 808 2 · 431 2 · 806 2 · 243 ————————————————————————————————————	2·913 2·616 2·817 2·484 2·810 2·202 ————————————————————————————————	2:910 2:626 2:814 2:512 2:820 2:176 — 2:753 2:817 2:412 2:913 2:880	2:902 2:621 2:798 2:526 2:812 2:145 — 2:771 2:798 2:427 2:920 2:877	2·882 2·587 2·752 2·546 2·786 2·110 2·791 2·754 2·417 2·910 2·861	2.877 2.568 2.700 2.558 2.725 2.074 2.797 2.687 2.421 2.900 2.840	2:840 2:559 2:650 2:584 2:701 2:039 2:789 2:659 2:422 2:894 2:814	2·822 2·560 2·606 2·615 2·673 2·031 2·797 2·621 2·433 2·891 2·795	2·807 2·563 2·565 2·645 2·657 2·029 2·810 2·592 2·454 2·894 2·805	2·798 2·557 2·550 2·679 2·613 2·029 2·832 2·591 2·462 2·902 2·789
FEBRUARY.	14 15 16 17 18 19 20 21	2.710 2.555 2.648 2.911 2.909 2.108 1.961	2·729 2·560 2·680 2·923 2·890 2·086 1·983	2.727 2.566 2.684 2.946 2.895 2.069 1.993	2.714 2.548 2.713 2.964 2.859 2.039 2.023	2·710 	2.692 	2.650 2.496 2.729 2.988 2.758 1.966 2.070	2.609 	2·586 — 2·472 2·730 2·957 2·727 1·940 2·052	2·592 2·468 2·732 2·965 2·682 1·929 2·066	2·572 	2·503 2·499 2·754 2·955 2·611 1·917 2·122
Mar	23 24 25 26 27 28	2·436 2·613 2·878 3·122 3·219 2·727	2:448 2:637 2:900 3:143 3:218 2:727	2.450 2.677 2.909 3.182 3.220 2.740	2:448 2:695 2:915 3:202 3:211 2:720	2:440 2:692 2:935 3:217 3:192 2:724	2 · 438 2 · 696 2 · 907 3 · 231 3 · 168 2 · 714	2·424 2·684 2·900 3·226 3·143 2·708	2'406 2'691 2'888 3'214 3'097 2'695	2:395 2:705 2:875 3:198 3:078 2:692	2 · 405 2 · 722 2 · 876 3 · 198 3 · 046 2 · 694	2·376 2·748 2·875 3·200 3·009 2·702	2:370 2:772 2:883 3:208 3:008 2:719
Iourly	Means	2.6687	2.6776	2.6895	2.6933	2.6932	2.6888	2.6724	2.6536	2.6399	2.6341	2.6307	2.630

10	10	1.4	1	1	1	1	es + the nu	1	ī .	20	1 00	
12	13	14	15	16	17	18	19	20	21	22	23	Daily ar Monthl
6	7	8	9	10	11	12	13	14	15	16	17	Means
In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
342	2.318	2.580	2.256	2.229	2.175	2.145	2.108	2.085	2.038	2.006	1.957	2:364
·886	1.934	1.976	2.010	2.042	2.093	2.132	2.162	2.502	2.235	2.256	2.281	1.982
$^{\cdot}453$	2.465	2.479	2.475	2.477	2.481			2 200		2 200		!
		_	_			2.601	2.603	2.609	2.651	2.675	2.686	2.4816
.863	2.875	2.903	2.920	2.934	2.953	2.959	2.956	2.965	2.968	2.978	2.976	2.8612
.853	2.829	2.789	2.764	2.733	2.644	2.606	2.266	$\frac{2.535}{2.532}$	2.483	2.439	2.391	2.8038
226	2.236	2.249	2.265	2.274	2.586	2.300	2.314	2.342	2.369	$\frac{2}{2} \cdot \frac{103}{373}$	2.377	2.2830
537	2.561	2.569	2.269	2.573	2.573	2.565	2.221	2.51	2.551	2.556	2.550	2.505
554	2.567	2.567	2.575	2.563	2.263	2.221	2.535	2.529	2.21	2.201	2.473	2.5529
258	2.246	2.246	2.232	2.218	2.201	2 001		2 023	2 021	2 001	2 110	
					2 201	2.272	2.274	2.292	2.296	2.302	$2 \cdot \overline{308}$	2:3184
•526	2.548	2.566	2.597	2.627	2.645	2.657	2.684	2.706	$\frac{2.730}{2.714}$	2.743	2.746	2.233
.818	2.796	$\frac{5.778}{2}$	2.754	2.738	2.726	2.693	2.652	$\frac{2.652}{2.652}$	2.628	2.602	2.576	2.7599
639	2.654	2.648	2.631	2.636	2.634	2.635	2.644	2.652	2.646	$\frac{2.602}{2.642}$	2.635	2 613
.516	$\frac{2.514}{2.516}$	2.28	$\frac{2.531}{2.548}$	2.552	2.248	2.20	2.212	2.528	$\frac{2.040}{2.517}$	2.497	2.490	2.5500
481	$\frac{2.481}{2.481}$	$\frac{2.328}{2.482}$	2.484	2.486	2.495	2.491	2.492	2.228	2.528	2.520	2.490	2 3 3 0 0
684	$\frac{2.701}{2.708}$	$\frac{2.462}{2.733}$	$\frac{2.752}{2.752}$	$\frac{2.480}{2.772}$	$\frac{2.495}{2.784}$	431 —	4 734	2 010	2 020	2 020	2 019	1
					# 10 <del>1</del>	3.026	3.034	3.072	3.080	3.095	$[3.\overline{096}]$	2.738
151	3.141	3.141	3.143	3.148	3.132	3.115	3.094	3.047	3.102	$\frac{3.103}{9.093}$	3.073	3.1323
825	2.784	$\frac{3}{2}.759$	$\frac{3}{2}.733$	2.692	$\frac{3}{2}.685$	2.649	2.635	2.596	$\frac{3}{2}.570$	2.236	$\frac{3.073}{2.508}$	
$\frac{023}{598}$	2.616	$\frac{2.759}{2.653}$	2.690	$\frac{2.092}{2.712}$	$\frac{2.085}{2.755}$	2.812	$\frac{2.839}{2.839}$	$\frac{2.596}{2.928}$	$\frac{2.570}{2.967}$	2.993	3.039	2.8224 2.6586
$\cdot 239$	3.241	$\frac{2}{3} \cdot 243$	$\frac{2}{3} \cdot 257$	$\frac{2}{3} \cdot \frac{712}{269}$								
147					3.284	3.284	3.294	3.300	3.301	3.591	3.287	3.2142
	3.131	3.103	3.067	3.041	3.034	3.053	2.999	2.975	2.951	2.936	2.928	3.1428
•553	2.233	2.216	2.495	2.461	2.433		0:440				]	2.6083
	0.0.7	0.070	0.400	0.400		2.446	2.442	2.441	2.435	2.414	2:370 }	i
332	2.357	2:376	2.400	2.420	2.449	2.463	2.466	2.497	2.219	2.243	2.584	2:3696
640	2.628	2.600	2.576	2.526	2.20	2.508	2.520	2.522	2.527	2.523	2.541	2.615
698	2.712	2.712	2.726	2.722	2.716	2.715	2.713	2.716	2.720	2.711	2.684	2.676
504	2.482	2.470	2.430	2.409	2.396	2.368	2.347	2.349	2.351	2.313	2.279	2.496
183	2.183	2.183	2.556	2.530	2.536	2.257	2.310	2.371	2.421	2.456	2.201	2.263
.928	2.949	2.953	2.389	2.389	2.380						-	2.836
						2.883	2.883	2.901	2.904	2.902	2.900 }	2 000
6087	2.6108	2.6115	2.6135	2.6101	2.6082	2.6175	2.6160	2.6250	2.6284	2.6261	2.6206	2.6172
·788	2.777	2.751	2.708	2.692	2.675	2.655	2.651	2.647	2.631	2.619	2.603	2.7782
•579	2.601	2.611	2.617	2.627	2.661	2.667	2.704	2.723	2.735	2.739	2.762	2.6270
520	2.484	2.453	2.390	2.378	2.368	2.356	2.339	2.339	2.340	2.340	2.364	2.5538
.700	2.727	2.739	2.745	2.761	2.769	2.767	2.767	2.772	2.775	2.773	2.786	2.6436
•599	2.281	2.562	2.556	2.516	2.456	2.444	2.392	2.366	2.330	2.284	2.281	2.598
062	2.109	2.135	2.511	2.254	2.285				_		- 7	
	_					2.523	2.251	2.525	2.523	2.23	$\{2.562\}$	2.2428
832	2.870	2.885	2.862	2.860	2.872	2.875	2.878	2.880	2.876	2.880	2.873	2.809
$^{\circ}585$	2.583	2.571	2.544	2.514	2.208	2.489	2.475	2.458	2.448	2.423	2.430	2.619
502	2.221	2.605	2.645	2.673	2.703	2.721	$\frac{2.737}{2}$	$\frac{2.744}{2.744}$	$\frac{2.772}{2.772}$	2.792	2.804	2.556
<b>.</b> 918	2.918	2.920	2.923	2.919	2.912	2.892	2.868	2.878	2.868	2.856	2.852	2.891
789	$\frac{2.818}{2.818}$	2.816	2.809	2.813	2.800	2.790	2.782	$\frac{2}{2}.787$	$\frac{2}{2}.785$	2.755	2.716	2.8178
	2.432	2.362	2.390	2.376	2.340		02	2 101	2 100			
			- 550		- 5.10	2.551	2.259	2.223	2.553	2.260	$\{2.555\}$	2.562
	1	2.243	2.248	2.551	2.251	2.260	2.266	$\frac{2.582}{2.582}$	2.590	2.594	2.630	2.5388
·468	2.530	, - 0.0	2.813	2.827	2.828	2.836	2.846	2.852	2.868	$\frac{2.334}{2.878}$	2.901	$\frac{2.336}{2.775}$
·468  ·512	2.530	2.808		2.964	2.960	2.961	2.928	2.933	2.914	2.914	2.904	2.952
· 468  · 512 · 776	2.790	2.808	2.971			2.370	2.334	2.588	2.270	2.509	2.139	2.582
· 468 	2.790 2.981	2.981	2.486		2.410		1'936	1.942	1.940	1.942	1.946	1.964
·468 	2.790 2.981 2.564	2.981 2.557	2.486	2.446	2.410	1.034	・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・	1 274	טבט ג	1 374	1 31	
·468 	2.790 2.981 2.564 1.926	2.981 2.557 1.921	2.486 1.929	2.446 1.934	1.936	1.934						
·468 	2.790 2.981 2.564	2.981 2.557	2.486	2.446						2:451	$\{2.\frac{-}{436}\}$	2.1800
·468 ·512 ·776 ·955 ·579 ·917 ·155	2.790 2.981 2.564 1.926 2.185	2 · 981 2 · 557 1 · 921 2 · 193	2:486 1:929 2:214	2.446 1.934 2.210	1.936 2.206	2.411	2.429	2.438	2.460	2.451 2.593	2.436	
·468 	2.790 2.981 2.564 1.926 2.185 — 2.388	2.981 2.557 1.921 2.193 — 2.470	2.486 1.929 2.214 — 2.516	2.446 1.934 2.210 — 2.531	1.936 2.206 	2.411 2.548	2.429 2.550	$ \begin{array}{c c} - \\ 2.438 \\ 2.550 \end{array} $	2.460 2.571	2.23	2.436 } 2.597	2.468
· 468 	2.790 2.981 2.564 1.926 2.185 — 2.388 2.849	2 · 981 2 · 557 1 · 921 2 · 193 — 2 · 470 2 · 857	2.486 1.929 2.214 — 2.516 2.865	2:446 1:934 2:210 — 2:531 2:891	1.936 2.206  2.531 2.888	2.411 2.548 2.886	2.429 2.550 2.894	2.438 2.550 2.894	2.460 2.571 2.884	2.593 2.871	2.436 } 2.597 2.868	2.468 2.783
*468 	2.790 2.981 2.564 1.926 2.185 ————————————————————————————————————	2 · 981 2 · 557 1 · 921 2 · 193 ————————————————————————————————————	2:486 1:929 2:214 ————————————————————————————————————	2:446 1:934 2:210 	1 '936 2 '206 — 2 '531 2 '888 2 '999	2:411 2:548 2:886 3:011	2.429 2.550 2.894 3.043	2.438 2.550 2.894 3.057	2.460 2.571 2.884 3.077	2.593 2.871 3.083	2.436 } 2.597 2.868 3.112	2.468 2.783 2.951
·468 	2.790 2.981 2.564 1.926 2.185 — 2.388 2.849 2.922 3.234	2 · 981 2 · 557 1 · 921 2 · 193 ————————————————————————————————————	2:486 1:929 2:214 	2:446 1:934 2:210 	1 · 936 2 · 206 2 · 531 2 · 888 2 · 999 3 · 251	2'411 2'548 2'886 3'011 3'238	2.429 2.550 2.894 3.043 3.233	2.438 2.550 2.894 3.057 3.231	2.460 2.571 2.884 3.077 3.234	2.593 2.871 3.083 3.237	2.436 } 2.597 2.868 3.112 3.220	2.468 2.783 2.951 3.215
'468	2.790 2.981 2.564 1.926 2.185 — 2.388 2.849 2.922 3.234 2.971	2 · 981 2 · 557 1 · 921 2 · 193 — 2 · 470 2 · 857 2 · 943 3 · 245 2 · 909	2·486 1·929 2·214 ————————————————————————————————————	2:446 1:934 2:210 ————————————————————————————————————	1 · 936 2 · 206 ————————————————————————————————————	2:411 2:548 2:886 3:011	2.429 2.550 2.894 3.043	2.438 2.550 2.894 3.057	2.460 2.571 2.884 3.077	2.593 2.871 3.083	2.436 } 2.597 2.868 3.112	2.468 2.783 2.951 3.215
*468 	2.790 2.981 2.564 1.926 2.185 — 2.388 2.849 2.922 3.234	2 · 981 2 · 557 1 · 921 2 · 193 ————————————————————————————————————	2:486 1:929 2:214 	2:446 1:934 2:210 	1 · 936 2 · 206 2 · 531 2 · 888 2 · 999 3 · 251	2'411 2'548 2'886 3'011 3'238	2.429 2.550 2.894 3.043 3.233	2.438 2.550 2.894 3.057 3.231	2.460 2.571 2.884 3.077 3.234	2.593 2.871 3.083 3.237	2.436 } 2.597 2.868 3.112 3.220	2:468 2:783 2:951 3:215 2:992
*468 	2.790 2.981 2.564 1.926 2.185 — 2.388 2.849 2.922 3.234 2.971	2 · 981 2 · 557 1 · 921 2 · 193 ————————————————————————————————————	2·486 1·929 2·214 ————————————————————————————————————	2.446 1.934 2.210 	1 · 936 2 · 206 ————————————————————————————————————	2.411 2.548 2.886 3.011 3.238 2.827	2·429 2·550 2·894 3·043 3·233 2·801	2·438 2·550 2·894 3·057 3·231 2·789	2·460 2·571 2·884 3·077 3·234 2·785	2.593 2.871 3.083 3.237 2.757	2:436 } 2:597 2:868 3:112 3:220 2:731	2.468

				Barome	eter at 32° =		TRIC PRES		ers in the Ta	able.			
lours o Götti Ti	f Mean } ngen }	0	1	2	3	4	5	6	7	8	9	10	11
Hours o	of Mean	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{pmatrix}$	In. 2 · 952 3 · 073 2 · 749 2 · 567 2 · 502 2 · 664	In. 2 · 972 3 · 090 2 · 740 2 · 573 2 · 496 2 · 672	In. 2 '995 3 '098 2 '735 2 '581 2 '494 2 '668	In. 3 000 3 103 2 716 2 584 2 508 2 658	In. 3 015 3 099 2 692 2 586 2 514 2 638	In. 3 022 3 098 2 664 2 586 2 522 2 622	In. 3 023 3 073 2 617 2 593 2 528 2 624	In. 3 015 3 043 2 573 2 558 2 526 2 584	In. 3:006 3:020 2:521 2:542 2:511 2:526	In. 3 000 2 986 2 505 2 531 2 532 2 492	In. 3:002 2:975 2:435 2:532 2:553 2:488	In. 3 016 2 964 2 433 2 546 2 578 2 496
1	8 9 10 11 12 13 14 15	2*823 2*863 2*854 2*685 2*363 2*089	2.865 2.878 2.850 2.682 2.385 2.092	2:884 2:900 2:874 2:680 2:378 2:088	2.896 2.919 2.868 2.676 2.371 2.064	2 · 903 2 · 928 2 · 854 2 · 659 2 · 335 2 · 056	2.911 2.926 2.848 2.640 2.307 2.056	2.901 2.917 2.823 2.628 2.286 2.052	2.886 2.905 2.794 2.614 2.250 2.046	2.866 2.887 2.770 2.603 2.173 2.044	2.869 2.889 2.752 2.591 2.179 2.042	2.858 2.888 2.750 2.555 2.139 2.052	2.853 2.890 2.751 2.541 2.114 2.072
MARCH	16 17 18 19 20 21 22	2:349 2:748 2:850 2:691 2:700 2:808	2:381 2:778 2:861 2:691 2:702 2:832	2·399 2·791 2·873 2·654 2·681 2·859	2:392 2:805 2:861 2:657 2:693 2:898	2:448 2:803 2:858 2:654 2:697 2:911	2·482 2·815 2·844 2·639 2·688 2·921	2:513 2:813 2:841 2:610 2:663 2:925	2·519 2·808 2·810 2·611 2·575 2·921	2·531 2·798 2·777 2·602 2·546 2·915	2·539 2·795 2·751 2·606 2·540 2·911	2·557 2·792 2·752 2·590 2·584 2·912	2·577 2·805 2·754 2·589 2·565 2·920
	22 23 24 25 26 27 28 29	2·742 2·441 2·013 2·114 2·162 2·383	2.738 2.453 2.003 2.114 2.178 2.395	2.724 2.451 1.977 2.114 2.186 2.397	2.706 2.447 1.971 2.090 2.196 2.403	2.682 2.441 1.953 2.106 2.213 2.419	2.665 2.441 1.934 2.100 2.218 2.413	2:649 2:423 1:927 2:084 2:231 2:407	2.620 2.410 1.934 2.077 2.243 2.407	2.604 2.392 1.942 2.071 2.257 2.407	2:592 2:362 1:944 2:070 2:265 2:407	2:562 2:359 1:949 2:076 2:251 2:417	2:560 2:345 1:988 2:108 2:303 2:441
	$\begin{bmatrix} 23 \\ 30 \\ 31 \end{bmatrix}$	2.829 2.944	2:845 2:950	2.862 2.971	2.868 2.984	2.874 2.983	2.858 2.979	2.856 2.985	2.848 2.972	2.835 2.966	2.829 2.960	2.829 2.960	2.849 2.969
lourly	Means	2.6137	2.6237	2.6275	2.6285	2.6277	2.6230	2.6121	2.5980	2.2812	2.5746	2.5699	2.5789
	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{pmatrix}$	3·125 3·145 3·153 3·081	3:156 3:163 3:166 3:085	3:174 3:169 3:177 3:095	3°187 3°180 3°186 3°092	3:194 3:176 3:188 3:090	3:187 3:159 3:167 3:089	3:174 3:146 3:158 3:091	3·170 3·142 3·156 3·096	3.145 3.117 3.139 3.071	3.136 3.112 3.123 3.051	3·122 3·100 3·110 3·045	3·127 3·090 3·120 3·029
	6 7 8 9 10 a	3·146 2·746 2·805 3·039	3:170 2:732 2:840 3:076	3.184 2.732 2.861 3.076	3.184 2.695 2.876 3.064	3:185 2:672 2:882 3:052	3.168 2.659 2.874 3.036	3.152 2.620 2.863 3.002	3.127 2.605 2.853 2.968	3.112 2.581 2.849 2.951	3:090 2:549 2:855 2:913	3.074 2.548 2.863 2.898	3.055 2.541 2.878 2.883
APRIL.	11 12 13 14 15 16 17 18	2:179 2:329 2:653 2:773 2:977 2:715 2:597	2:169 2:353 2:660 2:855 2:987 2:720 2:645	2·128 2·373 2·659 2·883 2·976 2·714 2·653	2:106 2:395 2:646 2:900 2:973 2:703 2:666	2.085 	2·100 2·431 2·617 2·930 2·935 2·686 2·664	2.119 2.452 2.583 2.930 2.897 2.664 2.643	2·182 	2:255 	2:307 2:491 2:514 2:931 2:816 2:604 2:558	2:367 2:522 2:498 2:933 2:795 2:589 2:533	2·423 — 2·554 2·510 2·947 2·792 2·583 2·514
	19 20 21 22 23 24 25 26	3.010 2.682 2.790 2.639 2.402 2.559	3:005 2:676 2:800 2:650 2:400 2:582	3.003 2.666 2.808 2.646 2.400 2.608	2·997 2·653 2·797 2·654 2·396 2·623	2.984 2.634 2.797 2.648 2.398 2.616	2.950 2.600 2.797 2.635 2.395 2.610	2 · 921 2 · 575 2 · 775 2 · 617 2 · 393 2 · 616	2.865 2.555 2.753 2.605 2.383 2.604	2.842 2.541 2.736 2.597 2.380 2.604	2.804 2.551 2.551 2.565 2.565 2.352 2.608	2·774 2·574 2·574 2·533 2·356 2·608	2:761 2:643 2:700 2:549 2:364 2:592
	26 27 28 29 30	2:637 2:552 2:299 2:303	2:656 2:543 2:295 2:290	2.663 2.542 2.293 2.306	2.660 2.546 2.285 2.325	2.656 2.541 2.287 2.334	2:627 2:511 2:286 2:312	2:615 2:496 2:278 2:313	2·620 2·440 2·277 2·290	2·599 2·440 2·275 2·281	2:593 2:395 2:277 2:286	2:574 2:369 2:277 2:292	2:559 2:368 2:277 2:280
Hourly	y Means	2.7334	2.7470	2.7516	2.7516	2.7481	2.7370	2.7237	2.7128	2.7011	2.6876	2.6823	2.6856

			Bar	ometer at 3			RESSURE		e Table.			
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
In. 3 028 2 936 2 416 2 568 2 606	In. 3 ° 047 2 ° 932 2 ° 428 2 ° 566 2 ° 634 2 ° 480	In. 3.063 2.918 2.426 2.583 2.651 2.480	In. 3 '064 2 '899 2 '442 2 '577 2 '674 2 '470	In. 3 '053 2 '882 2 '450 2 '563 2 '704 2 '459	In. 3.062 2.858 2.468 2.581 2.695 2.454	In. 3.054 2.840 2.476 2.573 2.700	In. 3:055 2:858 2:474 2:578 2:700	In. 3 '045 2 '830 2 '482 2 '578 2 '692	In. 3.047 2.824 2.486 2.547 2.687	In. 3.050 2.793 2.486 2.523 2.710	In. 3 056 2 763 2 533 2 515 2 681	In. 3 0267 2 9565 2 5395 2 5638 2 5999
2.490 2.850 2.876 2.747 2.543 2.143 2.096	2.850 2.872 2.747 2.537 2.149 2.113	2.856 2.877 2.736 2.523 2.121 2.122	2 · 841 2 · 896 2 · 722 2 · 524 2 · 115 2 · 118	2 · 842 2 · 902 2 · 719 2 · 514 2 · 117 2 · 115	2·842 2·892 2·710 2·470 2·117 2·098	2.730 2.828 2.889 2.702 2.448 2.093	2.756 2.829 2.880 2.700 2.438 2.090	2.763 2.826 2.871 2.692 2.434 2.090	2.771 2.830 2.866 2.677 2.403 2.060	2.781 2.834 2.865 2.673 2.391 2.060	2·795 }  2·850 2·665 2·371 2·074	2:6067 2:8584 2:8886 2:7616 2:5479 2:1879
2.589 2.805 2.750 2.610 2.576 2.940	2.619 2.803 2.735 2.623 2.580 2.960	2.641 2.805 2.736 2.643 2.602 2.983	2.662 2.818 2.716 2.641 2.607 3.001	2.660 2.816 2.715 2.646 2.634 3.004	2.669 2.824 2.720 2.641 2.649 3.006	2 · 268 2 · 665 2 · 819 2 · 722 2 · 635 2 · 665	2·284 2·666 2·818 2·715 2·637 2·692	2 · 296 2 · 672 2 · 780 2 · 690 2 · 634 2 · 705	2:291 2:678 2:780 2:681 2:637 2:725	2:305 2:695 2:770 2:675 2:641 2:747	2·331 } 2·718 2·802 2·691 2·681 2·767	2:1329 2:5675 2:7996 2:7658 2:6360 2:6493 2:8961
2.520 2.315 2.012 2.118 2.317 2.449	2.527 2.289 2.036 2.139 2.319 2.455	2.518 2.270 2.055 2.153 2.351 2.483	2.518 2.242 2.082 2.148 2.363 2.495	2:492 2:210 2:101 2:142 2:373 2:495	2:466 2:193 2:109 2:142 2:377 2:501	2:875 2:440 2:145 2:116 2:142 2:381	2:849 2:448 2:134 2:110 2:162 2:398	2 · 823 2 · 422 2 · 131 2 · 111 2 · 158 2 · 412	2.795 2.406 2.075 2.101 2.152 2.400	2.785 2.403 2.051 2.101 2.156 2.382	2.752 } 2.409 2.021 2.106 2.161 2.375	2:5589 2:2934 2:0240 2:1207 2:2980
2·849 2·985	2.859 3.003	2.870 3.027	2.878 3.049	2.885 3.059	2·900 3·057	2.740 2.906 3.061	2.766 2.906 3.066	2.779 2.906 3.066	2.783 2.908 3.074	2.796 2.922 3.086	2.808 } 2.922 3.114	2.5186 2.8705 3.0114
2.2821	2.5885	2.5958	2.2582	2.5974	2.2965	2.6150	2.6157	2.6111	2.6032	2.6031	2.5986	2.6026
3.120 3.090 3.109 3.018 	3·112 3·080 3·095 3·013 ————————————————————————————————————	3·123 3·080 3·100 3·011 	3.114 3.102 3.086 3.002 — 2.972	3:117 3:106 3:067 2:987 — 2:943	3:114 3:102 3:068 2:991 ———————————————————————————————————	3:113 3:103 3:073 — 3:070 2:853	3:117 3:122 3:074 — 3:070 2:805	3:116 3:119 3:090 — 3:069 2:781	3:120 3:124 3:078 — 3:069 2:767	3:126 3:132 3:064 — 3:093 2:755	$ \begin{vmatrix} 3.139 \\ 3.138 \\ 3.058 \\$	3:1387 3:1249 3:1169 3:0595 3:0071
2'490 2'893 2'858	2.506 2.898 2.842	2.511 2.914 2.837	2 · 499 2 · 943 2 · 826 —	2:533 2:968 2:800 —	2:563 2:980 2:779 —	$ \begin{array}{c c} 2.595 \\ 3.008 \\ \\ 2.319 \end{array} $	2.630 3.016 - 2.283	2.656 3.019  2.221	$ \begin{array}{c c} 2.699 \\ 3.025 \\ \\ 2.211 \end{array} $	$ \begin{array}{c c} 2.717 \\ 3.027 \\ \\ 2.191 \end{array} $	$\left\{\begin{array}{c} 2.766 \\ 3.036 \\ \\ 2.187 \end{array}\right\}$	2.6185 2.9180 2.7630
2.569 2.518 2.518 2.944 2.765 2.577 2.566	2.516 2.588 2.516 2.944 2.775 2.555 2.566	2.553 2.608 2.524 2.972 2.781 2.549 2.568	2:547 2:636 2:510 2:978 2:768 2:539 2:539	2.527 2.636 2.488 2.977 2.786 2.541 2.565	2:529 2:636 2:488 2:975 2:780 2:530 2:569	2·395 2·646 2·512 2·977 2·758 2·520	2·379 2·651 2·548 — 2·744 2·519	2·377 2·661 2·574 2·973 — 2·505	2:367 2:662 2:627 2:970 2:695 2:499	2·331 2·656 2·681 2·978 2·695 2·501	2·327 } 2·650 2·718 2·959 2·699 2·561	2·3222 2·5355 2·5742 2·9356 2·8293 2·5984 2·6973
2.755 2.662 2.672 2.503 2.368 2.572	2.750 2.692 2.668 2.503 2.396 2.585	2.744 2.700 2.680 2.499 2.418 2.590	2.744 2.734 2.668 2.489 2.428 2.603	2.738 2.735 2.656 2.471 2.442 2.589	2·736 2·725 2·644 2·449 2·441 2·587	3:004 2:736 2:733 2:645 2:437 2:445	2 · 991 2 · 721 2 · 743 2 · 645 2 · 420 2 · 451	3:005 2:715 2:752 2:652 2:412 2:455	2 · 988 2 · 703 2 · 747 2 · 648 2 · 420 2 · 459	2 · 999 2 · 689 2 · 743 2 · 653 2 · 406 2 · 497	$\left\{ \begin{array}{c} - \\ 3.001 \\ 2.681 \\ 2.762 \\ 2.651 \\ 2.394 \\ 2.535 \\ - \end{array} \right\}$	2 · 8178 2 · 8178 2 · 6699 2 · 7104 2 · 5309 2 · 4148 2 · 5973
2:540 2:369 2:269 2:280	2:550 2:351 2:265 2:282	2·574 2·378 2·285 2·297	2·561 2·364 2·275 2·306	2·562 2·357 2·263 2·317	2·546 2·382 2·255 2·323	2.597 2.549 2.385 2.255 2.325	2:584 2:546 2:347 2:283 2:295	2:586 2:545 2:335 2:291 2:291	2.587 2.551 2.313 2.283 2.290	2:603 2:539 2:287 2:285 2:284	$ \begin{array}{c}  - \\  2 \cdot 612 \\  2 \cdot 533 \\  2 \cdot 297 \\  2 \cdot 297 \\  2 \cdot 294 \end{array} $	2 5973 2 5856 2 4128 2 2797 2 2929
2.6796	2.6818	2.6914	2.6901	2.6868	2.6835	2.6821	2.6660	2.6750	2.6761	2.6773	2.6867	2.7017

lours of	Mean )					= 27 Engli			<del> </del>		1		
Göttir Tim	e.	0	1	2	3	4	5	6	7	8	9	10	11
ours of Toroi Tim	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \\ 2 \end{pmatrix}$	In. 2:310 2:340	In. 2:314 2:348	In. 2:319 2:350	In. 2:327 2:350	In. 2:317 2:349	In. 2.301 2.359	In. 2.300 2.365	In. 2:294 2:381	In. 2.280 2.382	In. 2.286 2.384	In. 2:290 2:408	In. 2:29- 2:418
	3 4 5 6 7 8 9	2.696 2.645 2.578 2.615 2.612 2.429	2.720 2.653 2.594 2.624 2.620 2.429	2.718 2.635 2.600 2.628 2.634 2.413	2.731 2.627 2.630 2.622 2.629 2.385	2·725 2·629 2·637 2·636 2·626 2·375	2·720 2·638 2·659 2·625 2·623 2·357	2.713 2.624 2.650 2.620 2.612 2.343	2.683 2.634 2.646 2.601 2.618 2.294	2.666 2.614 2.644 2.601 2.592 2.270	2.659 2.589 2.624 2.583 2.582 2.252	2.641 2.585 2.622 2.582 2.579 2.234	2.636 2.576 2.61. 2.586 2.579 2.22
MAY.	10 11 12 13 14 15 16	2:404 2:397 2:379 2:410 2:359 2:819	2.433 2.400 2.353 2.406 2.383 2.825	2·455 2·404 2·347 2·428 2·461 2·823	2.464 2.402 2.339 2.419 2.492 2.819	2.465 2.400 2.329 2.413 2.554 2.808	2·450 2·401 2·310 2·388 2·600 2·826	2·442 2·403 2·290 2·356 2·627 2·810	2:436 2:405 2:269 2:396 2:645 2:802	2.423 2.414 2.267 2.380 2.668 2.787	2:409 2:407 2:264 2:323 2:680 2:794	2.408 2.410 2.292 2.321 2.681 2.789	2 · 409 2 · 417 2 · 317 2 · 289 2 · 704 2 · 790
M	17 18 19 20 21 22 23	2.605 2.840 2.508 2.740 2.836 2.557	2.602 2.853 2.491 2.762 2.844 2.553	2.643 2.862 2.483 2.775 2.841 2.542	2.664 2.848 2.452 2.791 2.836 2.545	2.677 2.834 2.432 2.796 2.834 2.544	2.693 2.803 2.420 2.818 2.815 2.543	2·712 2·781 2·396 2·820 2·797 2·541	2.725 2.749 2.419 2.782 2.790 2.538	2·735 2·721 2·401 2·780 2·786 2·550	2·742 2·687 2·401 2·789 2·757 2·561	2.765 2.652 2.402 2.763 2.749 2.578	2·78 2·64 2·418 2·760 2·739 2·578
	24 25 26 27 28 29 30 31	2°644 2°551 2°275 2°291 2°330 2°207	2.645 2.554 2.282 2.291 2.325 2.213	2.650 2.552 2.265 2.289 2.325 2.215	2.643 2.548 2.270 2.273 2.323 2.225	2:642 2:539 2:271 2:268 2:324 2:225	2.648 2.514 2.268 2.260 2.318 2.221	2.638 2.501 2.279 2.258 2.314 2.210	2.621 2.480 2.283 2.251 2.308 2.207	2.616 2.476 2.276 2.235 2.283 2.201	2.616 2.439 2.284 2.225 2.271 2.195	2.610 2.440 2.283 2.217 2.275 2.201	2 · 612 2 · 44: 2 · 278 2 · 200 2 · 263 2 · 200
Iourly	Means	2.5145	2.5200	2.5253	2.5252	2.5250	2.2522	2.2122	2.2100	2.2018	2.4924	2.4914	2.49
	1 2 3 4 5 6	2.483 2.370 2.517 2.432 2.319 2.480	2.492 2.370 2.531 2.428 2.325 2.486	2.465 2.409 2.531 2.446 2.340 2.504	2.461 2.427 2.518 2.420 2.344 2.512	2.425 2.415 2.528 2.409 2.351 2.532	2:449 2:408 2:474 2:399 2:335 2:541	2:441 2:401 2:477 2:376 2:325 2:549	2.420 2.355 2.461 2.357 2.355 2.559	2:382 2:367 2:457 2:323 2:338 2:579	2:390 2:357 2:433 2:313 2:342 2:592	2:366 2:355 2:418 2:307 2:366 2:594	2:339 2:357 2:395 2:285 2:367 2:590
re ²	7 8 9 10 11 12 13	2·932 3·045 2·782 2·547 2·859 2·867	2·952 3·037 2·782 2·563 2·867 2·873	2.958 3.041 2.772 2.583 2.880 2.872	2.971 3.041 2.756 2.585 2.904 2.866	2.990 3.041 2.726 2.590 2.914 2.877	2.982 3.041 2.715 2.605 2.908 2.874	2.981 3.023 2.685 2.620 2.899 2.869	2.971 3.006 2.662 2.621 2.903 2.849	2.962 2.978 2.621 2.609 2.899 2.835	2:955 2:951 2:605 2:585 2:899 2:818	2 · 948 2 · 926 2 · 591 2 · 593 2 · 881 2 · 804	2·949 2·897 2·562 2·593 2·877 2·778
JUNE	14 15 16 17 18 19 20 21	2.552 2.628 2.638 2.573 2.333 2.376	2.558 2.643 2.649 2.576 2.335 2.376	2.560 2.648 2.654 2.560 2.327 2.392	2.561 2.649 2.654 2.551 2.317 2.401	2.545 2.648 2.661 2.550 2.309 2.417	2.544 2.660 2.650 2.536 2.275 2.420	2.531 2.660 2.633 2.503 2.271 2.426	2·522 2·658 2·630 2·485 2·256 2·443	2.517 2.650 2.616 2.465 2.248 2.451	2:507 2:637 2:603 2:465 2:241 2:469	2·503 2·637 2·601 2·434 2·248 2·478	2:496 2:615 2:594 2:402 2:252 2:485
	21 22 23 24 25 26 27 28	2.683 2.825 2.804 2.723 2.598 2.501	2.681 2.836 2.818 2.730 2.598 2.515	2.685 2.826 2.821 2.722 2.582 2.517	2.681 2.821 2.823 2.710 2.566 2.517	2.683 2.807 2.821 2.704 2.560 2.519	2.688 2.792 2.812 2.693 2.555 2.516	2.681 2.775 2.801 2.674 2.550 2.515	2.680 2.775 2.796 2.658 2.547 2.525	2.695 2.769 2.770 2.647 2.532 2.512	2·708 2·756 2·755 2·643 2·511 2·502	2.723 2.755 2.739 2.635 2.506 2.508	2.754 2.753 2.719 2.623 2.497 2.506
,	28 29 30	$2.551 \\ 2.517$	2.553 2.522	2.553 $2.524$	2.559 2.529	2·557 2·539	2·561 2·542	2·556 2·542	2·546 2·528	2·522 2·522	2.509 2.511	2.519 2.506	2·507 2·489

			Bar	ometer at 3	$ \begin{array}{c} \text{BAROM} \\ 2^{\circ} = 27 \text{ E} \end{array} $		RESSURE. s + the nu	mbers in the	Table.			
12	13	14	15	16	17	18	19	20	21	22	23	Daily and
6	7	8	9	10	11	12	13	14	15	16	17	Means.
In.	In.	In. 2:304	In. 2.308	In. 2·326	In. 2·320	In. 2.308	In. 2.298	In. 2.302	In. 2.302	In. 2.304	In. 2.316	In. 2·3052
2:300 2:426	2·304 2·446	2.460	2.472	2.482	2.480			_		2.661	$\left\{\begin{array}{c} 2.510 \\ 2.689 \end{array}\right\}$	2.4631
	0:007	2.643	2.644	2.641	2.638	2.636 2.644	2.637 2.625	2.644 2.620	2.647 2.622	2.616	2.645	2.6632
2.635	$2.635 \\ 2.547$	2.545	2.561	$\frac{2.530}{2.530}$	$\frac{2.539}{2.539}$	2.527	2.514	$\frac{2.620}{2.510}$	$\frac{2.622}{2.514}$	2.534	2.264	$\frac{2.5788}{2.5788}$
2.549	2.612	$\frac{2.539}{2.612}$	2.628	2.630	$\frac{2.633}{2.633}$	2.623	2.612	$\frac{2.510}{2.599}$	$\frac{2.514}{2.592}$	$\frac{2.604}{2.604}$	$\frac{2.504}{2.598}$	2.6191
2.617 2.586	$\frac{2.512}{2.587}$	$\frac{2.512}{2.587}$	$\frac{2.028}{2.589}$	$\frac{2.589}{2.589}$	$\frac{2.033}{2.597}$	2.28	2.590	$\frac{2.586}{2.586}$	$\frac{2.582}{2.582}$	2.286	2.584	2.5993
$\frac{2.547}{2.547}$	2.241	2.243	2.552	2.534	2.523	2.497	2.476	2.464	2.461	2.441	2.424	2.5545
2.508	2.514	2.510	2.505	2.189	2.177	$\frac{-}{2\cdot 351}$	2.362	2.363	2.374	2.376	$\left  \frac{1}{2 \cdot 382} \right $	2:3089
··· 107	$2.\frac{-}{407}$	$\frac{-}{2.418}$	2.402	2.393	2.383	$\frac{2.361}{2.368}$	2.361	$\frac{2}{2} \cdot 357$	$\frac{2}{2} \cdot 355$	$\frac{2.370}{2.349}$	2.385	2.4076
2'407 2'436	2.407 $2.440$	2.413	2.466	$\frac{2.335}{2.451}$	$\frac{2.365}{2.446}$	2.444	2.422	2.414	2.403	$\frac{2}{2} \cdot \frac{313}{392}$	$\frac{2.386}{2.386}$	2.4168
2.325	$\frac{2}{2} \cdot 337$	2.339	$\frac{2}{2} \cdot 349$	2.371	2.373	2.370	2.380	2.380	2.382	2.386	2.396	2:3393
2.528	2.303	2.319	2.323	2.335	2.356	2.366	2.349	2.357	2.337	2.329	2.322	2.3544
$\frac{2}{2}.728$	$\frac{2.303}{2.742}$	$\frac{2.745}{2.745}$	2.759	2.744	2.767	2.784	2.776	$\frac{1}{2} \cdot 777$	2.771	2.772	2.812	2.6681
2.786	2.786	2.798	2.804	2.805	2.791		—	_		_ <del></del>		2.7538
			_			2.639	2.602	2.605	2.596	2.596	$2.\overline{591}$	
2.782	2.782	2.793	2.799	2.818	2.850	2.827	2.816	2.809	2.804	2.811	2.821	2.7511
2.634	2.629	2.627	2.618	2.556	2.552	2.567	2.551	2.238	2.217	2.507	2.514	2.6703
2.436	2.468	2.499	2.212	2.524	2.540	2.554	2.587	2.620	2.655	2.681	2.707	2.2005
2.754	2.758	2.768	2.776	2.768	2.763	2.776	2.778	2.778	2.779	2.783	2.821	2.7782
2.723	2.691	2.680	2.682	2.655	2.638	2.638	2.636	2.624	2.587	2.23	2.262	2.7223
2.596	2.614	2.628	2.645	2.644	2.644	0:500	0:000	0:010	0:010	0.010	$\left  \frac{1}{2 \cdot 644} \right $	2.5866
			-	0.570	0.574	2.596	2.602	2.610	2.616	2.613	$\begin{bmatrix} 2.644.5 \\ 2.561 \end{bmatrix}$	2.6013
2.600	2.596	2.282	2.578	2.578	2.574 2.330	$\begin{vmatrix} 2.567 \\ 2.314 \end{vmatrix}$	$2.570 \\ 2.298$	$2.558 \\ 2.291$	2:546 2:288	$\frac{2.536}{2.269}$	$\begin{bmatrix} 2.301 \\ 2.273 \end{bmatrix}$	$\frac{2.0013}{2.4197}$
2'442	2.443	2.383	2.361 2.305	2:344 2:306	2 330	2.314 2.297	$\frac{2.298}{2.288}$	$\frac{2.291}{2.288}$	$\frac{2}{2} \cdot \frac{288}{290}$	$\frac{2.269}{2.281}$	$\frac{2.273}{2.290}$	2.2850
2°278 2°232	2.589	2·304 2·261	2.267	2.300 2.275	2.288	2.260	$\frac{2}{2} \cdot \frac{200}{290}$	2.294	$\frac{2}{2} \cdot \frac{250}{300}$	$\frac{2}{2} \cdot \frac{201}{299}$	$\frac{2}{2} \cdot \frac{230}{320}$	$\frac{2}{2} \cdot 2657$
$\frac{2\cdot255}{2\cdot25}$	2.236 2.262	$\frac{2}{2} \cdot \frac{201}{252}$	2.258	2.240	2.247	2.200 $2.227$	2.241	2.203	$\frac{2}{2} \cdot \frac{300}{199}$	2.201	2.195	2.2682
2.511	$\frac{2}{2} \cdot \frac{202}{237}$	2.241	2.582	2.309	2.314						$\left\{ \frac{1}{2\cdot 492} \right\}$	2.2932
						2.200	2.488	2.482	2.476	2.477		
2.4910	2.4964	2.2000	2.5056	2.2013	2.2018	2.2106	2.2028	2.2027	2.4998	2.2000	2.2114	2.5067
2:338	2.342	2.339	2.347	2.339	2.339	2.346	2.338	2.340	2.340	2.353	2.358	2:3847
$\frac{2.375}{2.375}$	$\frac{2.342}{2.400}$	$\frac{2.339}{2.442}$	2.463	2.463	2.471	2.482	2.474	2.482	2.485	2.485	2.217	2.4221
2.409	2.395	2.391	2.447	2.409	2.419	2.433	2.446	2.439	2.434	2.434	2.438	2.4513
2.295	$\frac{2}{2} \cdot \frac{335}{295}$	2.304	2.328	2.323	2.312	2.313	2.300	2.298	2.292	2.309	2.321	2:3411
2.373	2.375	2.412	2.407	2.415	2.424	2.426	2.427	2.438	2.437	2.445	2.459	2.3810
2.616	2.625	2.653	2.675	2.687	2.694		<del>-</del>		—		- 1	2.6507
_	<u> </u>	<u> </u>				2.830	2.837	2.841	2.847	2.871	$2.\overline{918}$	
2.951	2.953	2.959	2.970	2.982	2.987	2.996	2.987	2.988	2.991	2.991	3.027	2.9722
2.884	2.874	2.864	2.857	2.836	2.825	2.812	2.825	2.817	2.806	2.793	2.786	2.9169
2.534	2.538	2.251	2.244	2.551	2.545	2.545	2:524	2.528	2.534	2.231	2.543	2.6124
2.605	2.617	2.627	2.675	2.694	$2.708 \\ 2.882$	$2.737 \\ 2.882$	$2.762 \\ 2.875$	2.777	2.792	2.820	2.838 2.867	2.6561 2.8815
2.868 2.766	2.874	$2.865 \\ 2.761$	2.879 2.760	2.885 2.751	$\begin{bmatrix} 2.882 \\ 2.735 \end{bmatrix}$	2 002	2 010	2.865	2.865	2.867	2 001	
- 100	2.763	2 701	2 700	2 701		2.546	2.238	2.26	2.20	2.526	$2.\overline{544}$	2.7466
2.498	2.508	2.211	2.239	2.550	2.259	2.569	2.592	2.590	2.590	$\frac{2.595}{2.595}$	2.612	2.5462
2.616	2.616	2.604	2.612	2.616	2.624	2.627	2.621	2.612	2.619	2.615	2.629	2.6311
2.294	2.286	2.590	2.255	2.592	2.585	2.579	2.571	2.572	2.568	2.562	2.572	2.6062
2.399	2.408	2.403	2.415	2.422	2.410	2.392	2.387	2.375	2.356	2.357	2.351	2.4490
2.274	2.298	2.303	2.350	2.305	2:309	2.325	2.333	2.333	2.334	2.355	2.366	2.3025
2.493	2.499	2.496	2.498	2.498	2.200						] }	2.5039
-		_				2.651	2.653	2.655	2.661	2.668	2.687	
2.765	2.765	2.777	2.788	2.795	2.810	2.829	2.797	2.789	2.785	2.788	2.813	2.7435
2.762	2.765	2.764	2.777	2.779	2.776	2.770	2.771	2.774	2.769	2.774	2.793	2.7818
2.713	2.721	2.719	2.735	2.731	2.722	2.726	2.720	2.703	2.704	2.699	2.725	2.7540 2.6384
2.613	2.613	2.609	2.614	2.608	2.605 2.491	2.606 2.491	2.583 2.486	2.570 2.484	2.567 2.486	2.569 2.490	2.603 2.500	2.5384 $2.5207$
2.487 2.502	2.489	2.497	2.500	$2.495 \\ 2.512$	2 491	431	2 400	404	400	2 73U	2 300	
- 002	2.497	2.483	2 001	2 012		$2.\overline{518}$	2.212	2.213	2.209	2.252	$\{2\cdot \frac{1}{535}\}$	2.5113
2.213	2.213	2.212	2.21	2.211	2.209	$\frac{2.510}{2.508}$	2.507	2.507	2.200	2.202	2.211	$2^{\circ}5254$
2.493	2.497	2.499	2.206	2.204	2.207	2.206	2.215	2.490	2.485	2.496	2.208	2.5114
2.5668	2.5702	2.5734	2.5874	2.5865	2.5870	2.5939	2.5916	2.5888	2.5874	2.5930	2.6082	2.5939

				Barome	ter at 32° =		RIC PRES		rs in the Ta	ble.			
ours of Göttir Tim	Mean }	0	1	2	3	4	5	6	7	8	9	10	11
	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	1 2 3 4	In. 2:497 2:608 2:723 2:547	In. 2:487 2:628 2:745 2:541	In. 2.500 2.639 2.745 2.540	In. 2 · 505 2 · 659 2 · 725 2 · 526	In. 2:509 2:659 2:720 2:527	In. 2:514 2:652 2:707 2:513	In. 2:501 2:647 2:695 2:498	In. 2:486 2:645 2:667 2:471	In. 2 · 473 2 · 648 2 · 649 2 · 442	In. 2:459 2:642 2:642 2:427	In. 2 · 473 2 · 632 2 · 636 2 · 402	In. 2 * 47 ! 2 * 626 2 * 609 2 * 416
	5 6 7 8 9 10	2:426 2:574 2:564 2:515 2:494 2:478	2·435 2·585 2·558 2·522 2·495 2·482	2·434 2·593 2·575 2·523 2·504 2·473	2.438 2.607 2.564 2.547 2.502 2.467	2·452 2·611 2·568 2·544 2·507 2·456	2:449 2:610 2:534 2:594 2:493 2:449	2.445 2.602 2.516 2.618 2.485 2.434	2·444 2·600 2·507 2·494 2·492 2·433	2:426 2:583 2:487 2:494 2:475 2:453	2:433 2:568 2:483 2:496 2:457 2:445	2.426 2.562 2.469 2.478 2.457 2.438	2:409 2:559 2:464 2:459 2:439 2:420
JULY.	12 13 14 15 16 17 18	2:595 2:607 2:824 2:930 3:006 2:909	2.603 2.614 2.831 2.945 3.027 2.921	2.595 2.643 2.838 2.956 3.024 2.915	2:572 2:641 2:834 2:962 3:017 2:917	2·573 2·641 2·841 2·973 3·020 2·914	2:544 2:647 2:841 2:975 3:011 2:905	2:538 2:647 2:829 2:965 2:986 2:891	2.518 2.645 2.834 2.949 2.978 2.880	2.513 2.649 2.834 2.944 2.959 2.867	2.510 2.666 2.838 2.945 2.947 2.858	2.481 2.676 2.833 2.953 2.946 2.853	2:46 2:69 2:84 2:94 2:98 2:84
	19 20 21 22 23 24 25	2:576 2:602 2:585 2:492 2:300 2:592	2.582 2.612 2.597 2.501 2.310 2.608	2.587 2.610 2.593 2.492 2.308 2.619	2·575 2·610 2·584 2·471 2·284 2·625	2.584 2.611 2.557 2.460 2.282 2.653	2.585 2.610 2.569 2.456 2.258 2.638	2·574 2·599 2·568 2·438 2·275 2·633	2:561 2:594 2:550 2:431 2:291 2:645	2:546 2:589 2:549 2:425 2:305 2:644	2.538 2.581 2.537 2.406 2.319 2.643	2:531 2:577 2:534 2:388 2:349 2:630	2·53 2·572 2·533 2·363 2·363 2·626
	26 27 28 29 30 31	2·773 2·646 2·463 2·322 2·548	2.793 2.644 2.446 2.322 2.546	2.793 2.639 2.450 2.309 2.550	2·792 2·649 2·478 2·316 2·559	2·782 2·641 2·447 2·311 2·570	2.785 2.631 2.436 2.313 2.598	2.779 2.610 2.434 2.304 2.594	2.781 2.584 2.429 2.296 2.592	2.765 2.562 2.401 2.293 2.590	2.750 2.544 2.403 2.296 2.588	2.739 2.543 2.416 2.319 2.590	2·71 2·54 2·36 2·31 2·58
lourly	Means	2.5999	2.6067	2.6093	2.6084	2.6079	2.6043	2.5965	2.2851	2.5765	2.211	2.5678	2.22
	1	2.663	2.685	2.693	2.700	2.700	2.697	2.691	2.685	2.682	2.670	2.677	2.67
!	2 3 4 5 6 7 8	2.797 2.729 2.646 2.642 2.780 2.691	2.803 2.733 2.646 2.657 2.793 2.683	2·808 2·728 2·636 2·664 2·789 2·711	2.818 2.722 2.643 2.671 2.795 2.735	2.835 2.697 2.641 2.681 2.793 2.699	2.812 2.685 2.631 2.688 2.785 2.681	2.805 2.673 2.609 2.685 2.775 2.655	2.791 2.653 2.582 2.675 2.771 2.650	2·758 2·647 2·563 2·675 2·762 2·641	2.739 2.628 2.547 2.667 2.750 2.616	2.727 2.609 2.534 2.664 2.739 2.608	2.733 2.617 2.543 2.677 2.727 2.588
ST.	9 10 11 12 13 14 15	2·527 2·699 2·615 2·491 2·520 2·462	2·533 2·714 2·619 2·503 2·534 2·464	2:543 2:719 2:612 2:502 2:536 2:464	2.557 2.739 2.598 2.506 2.542 2.480	2.567 2.740 2.591 2.512 2.553 2.468	2.586 2.709 2.573 2.509 2.540 2.459	2:580 2:700 2:554 2:544 2:528 2:444	2.565 2.691 2.532 2.488 2.528 2.421	2·559 2·670 2·512 2·487 2·503 2·392	2 546 2 664 2 503 2 477 2 486 2 367	2·544 2·649 2·486 2·473 2·476 2·354	2:546 2:63' 2:480 2:46' 2:478 2:320
AUGUST.	16 17 18 19 20 21 22	2·407 2·733 2·807 2·625 2·583 2·550	2·419 2·743 2·811 2·634 2·576 2·570	2:435 2:745 2:815 2:636 2:609 2:572	2·448 2·771 2·817 2·634 2·617 2·575	2·465 2·775 2·814 2·631 2·627 2·565	2·472 2·775 2·809 2·627 2·625 2·558	2·482 2·765 2·802 2·628 2·612 2·548	2:482 2:763 2:791 2:597 2:612 2:531	2·486 2·769 2·773 2·605 2·617 2·531	2·486 2·757 2·763 2·583 2·595 2·521	2·494 2·751 2·759 2·589 2·585 2·513	2.508 2.748 2.748 2.579 2.568 2.50-
	23- 24 25 26 27 28 29	2·792 2·787 2·711 2·717 2·767 2·691	2.800 2.787 2.723 2.727 2.776 2.695	2.819 2.800 2.739 2.732 2.776 2.687	2.827 2.804 2.726 2.750 2.786 2.687	2.844 2.807 2.723 2.757 2.789 2.668	2.841 2.801 2.721 2.759 2.789 2.663	2.820 2.788 2.712 2.758 2.786 2.648	2.819 2.771 2.693 2.754 2.739 2.657	2·811 2·753 2·680 2·753 2·718 2·658	2·799 2·745 2·670 2·731 2·713 2·622	2·791 2·741 2·668 2·716 2·709 2·616	2·783 2·678 2·678 2·729 2·708
	$\begin{bmatrix} 30 \\ 31 \end{bmatrix}$	2.611	2.641	2.642	2.642	2.635	2.625	2.611	2.608	2.296	2.27	2.23	2.56
lourl	y Means	2.6555	2.6641	2.6697	2.6765	2.6760	2.6700	2.6601	2.6480	2.6385	2.6239	2.6171	2.61

BAROMETRIC PRESSURE.  Barometer at 32° = 27 English inches + the numbers in the Table.  12													
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly	
6	7	8	9	10	11	12	13	14	15	16	17	Means.	
In. 2 · 473 2 · 625 2 · 603 2 · 408	In. 2:474 2:636 2:591 2:396	In. 2 · 473 2 · 642 2 · 582 2 · 392	In. 2 486 2 672 2 606 2 439	In. 2:494 2:659 2:599 2:445	In. 2 · 496 2 · 666 2 · 583 2 · 438	In. 2 · 497 2 · 675 2 · 563	In. 2 · 513 2 · 684 2 · 560	In. 2 · 527 2 · 690 2 · 555	In. 2.538 2.684 2.560	In. 2.565 2.684 2.560	In. 2 · 592 2 · 697 2 · 550	In. 2:5001 2:6541 2:6323	
2:415 2:565 2:459 2:450 2:494 2:428	2·445 2·567 2·471 2·430 2·474 2·428	2.452 2.570 2.463 2.442 2.498 2.429	2·474 2·587 2·492 2·446 2·547 2·450	2.490 2.589 2.494 2.448 2.534 2.446	2·498 2·582 2·497 2·452 2·527 2·432	2:339 2:505 2:565 2:487 2:447 2:524	2:347 2:506 2:568 2:490 2:455 2:517	2:355 2:508 2:565 2:492 2:469 2:485	2:368 2:519 2:561 2:497 2:471 2:487	2:378 2:518 2:559 2:506 2:488 2:491	2:397 } 2:555 2:563 2:504 2:494 2:483	2:4394 2:4626 2:5790 2:5059 2:4907 2:4942	
2:453 2:707 2:861 2:940 2:902 2:849	2.457 2.717 2.863 2.936 2.896 2.843	2.483 2.717 2.861 2.932 2.909 2.841	2.502 2.721 2.887 2.946 2.921 2.842	2:514 2:729 2:890 2:951 2:913 2:842	2:531 2:732 2:899 2:956 2:915 2:838	2.548 2.546 2.735 2.899 2.951 2.912	2.550 2.538 2.765 2.902 2.951 2.898	2:552 2:548 2:769 2:904 2:950 2:895	2:553 2:551 2:789 2:908 2:958 2:878	2:562 2:562 2:815 2:925 2:975 2:889	2·592 } 2·566 2·808 2·932 2·997 2·901	2:4752 2:5314 2:6988 2:8647 2:9536 2:9441	
2.525 2.564 2.505 2.350 2.392 2.634	2:536 2:566 2:566 2:364 2:418 2:642	2:544 2:575 2:515 2:356 2:448 2:648	2.561 2.589 2.508 2.362 2.460 2.678	2:569 2:589 2:518 2:359 2:483 2:695	2:578 2:586 2:511 2:358 2:497 2:699	2:561 2:579 2:590 2:509 2:347 2:513	2:563 2:579 2:572 2:486 2:338 2:526	2.551 2.578 2.577 2.467 2.318 2.535	2.551 2.574 2.588 2.465 2.308 2.543	2:548 2:576 2:576 2:445 2:293 2:546	2·570 } 2·572 2·583 2·465 2·298 2·578	2.7946 2.5642 2.5884 2.5274 2.3905 2.3992 2.6665	
2.697 2.525 2.364 2.332 2.601	2.693 2.525 2.366 2.348 2.617	2.691 2.511 2.385 2.381 2.626	2.707 2.515 2.373 2.398 2.635	2.702 2.520 2.343 2.405 2.635	2.704 2.526 2.345 2.414 2.642	2.741 2.695 2.501 2.333 2.415 2.638	2.742 2.688 2.497 2.313 2.419 2.647	2.740 2.685 2.464 2.303 2.439 2.648	2.738 2.678 2.426 2.304 2.448 2.646	2.739 2.662 2.464 2.317 2.455 2.646	2.744 } 2.648 2.472 2.321 2.502 2.658	2 6663 2 7291 2 5492 2 3850 2 3615 2 6063	
2.5600	2.5631	2.5691	2.5853	2.5872	2.5890	2.5783	2.5783	2.5766	2.5774	2.2831	2.5941	2.5847	
2.678 2.725 2.603 2.545 2.677 2.727 2.588	2.678 2.725 2.609 2.545 2.678 2.721 2.584	2.681 2.733 2.611 2.561 2.697 2.726 2.590	2.704 2.733 2.614 2.581 2.712 2.736 2.588	2·709 2·734 2·629 2·586 2·723 2·736 2·585	2·709 	2.758 2.734 2.623 2.593 2.733 2.727	2·754 2·729 2·631 2·590 2·735 2·697	2.746 2.713 2.636 2.596 2.737 2.699	2.740 2.713 2.631 2.597 2.736 2.688	2.770 2.719 2.625 2.606 2.730 2.683	2·774 } 2·774 } 2·733 2·634 2·614 2·755 2·673	2.7050 2.7563 2.6497 2.5924 2.6950 2.7420	
2·560 2·631 2·482 2·467 2·466 2·328	2:560 2:616 2:476 2:467 2:470 2:326	2.595 2.584 2.478 2.479 2.467 2.342	2.604 2.618 2.478 2.492 2.483 2.333	2.612 2.609 2.481 2.505 2.479 2.339	2.629 2.611 2.475 2.522 2.480 2.344	2.488 2.639 2.606 2.471 2.510 2.473	2.470 2.646 2.601 2.474 2.498 2.459	2.471 2.651 2.598 2.478 2.494 2.400	2:472 2:653 2:604 2:472 2:492 2:439	2 · 490 2 · 654 2 · 598 2 · 468 2 · 497 2 · 448	2:505 } 2:675 2:608 2:479 2:498 2:456	2:5986 2:5888 2:6506 2:5165 2:4933 2:4893 2:3867	
2.516 2.748 2.719 2.576 2.564 2.494	2·481 2·750 2·721 2·579 2·564 2·484	2.550 2.772 2.715 2.579 2.569 2.509	2·582 2·773 2·717 2·593 2·563 2·511	2:583 2:777 2:715 2:603 2:565 2:511	2:591 2:791 2:701 2:591 2:564 2:501	2:358 2:615 2:793 2:695 2:589 2:563	2:353 2:632 2:803 2:667 2:578 2:558	2:351 2:652 2:802 2:650 2:574 2:559	2:351 2:673 2:800 2:640 2:563 2:551	2:366 2:689 2:797 2:632 2:564 2:548	2:395 } 2:709 2:794 2:626 2:569 2:550 	2·5357 2·7706 2·7375 2·5969 2·5810 2·5785	
2.781 2.732 2.668 2.731 2.713 2.602	2.773 2.714 2.666 2.724 2.709 2.605	2.764 2.714 2.676 2.741 2.703 2.600	2.783 2.739 2.683 2.746 2.703 2.604	2.785 2.737 2.685 2.746 2.697 2.606	2·790 2·715 2·684 2·744 2·694 2·601	2.670 2.792 2.713 2.679 2.754 2.686	2.702 2.790 2.705 2.672 2.754 2.694	2.722 2.779 2.705 2.674 2.741 2.702	2.733 2.775 2.700 2.670 2.749 2.689	2.747 2.772 2.696 2.671 2.745 2.697	2.761 } 2.775 2.698 2.669 2.757 2.684	2:7960 2:7452 2:6892 2:7423 2:7260	
2.267	2.23	2.286	2.595	2.296	2.606	2.596 2.598	2:598 2:595	2.604	2.605 2.606	2.604 2.596	2.296	2.6018	
2.6111	2.6076	2.6162	2.6257	2.6282	2.6267	2.6329	2.6302	2.6282	2.6285	2.6315	2.6383	2.6382	

				Barom		BAROMET = 27 Engl			ers in the Ta	able.		·	
Hours of Göttin Tim	igen }	0	1	2	3	4	5	6	7	8	9	10	11
	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	1 2 3 4 5	In. 2.605 2.647 2.513 2.387 2.476	In. 2.620 2.656 2.514 2.403 2.486	In. 2 * 624 2 * 652 2 * 508 2 * 405 2 * 496	In. 2 627 2 646 2 516 2 395 2 518	In. 2 643 2 646 2 508 2 398 2 529	In. 2 * 630 2 * 638 2 * 510 2 * 374 2 * 525	In. 2 * 595 2 * 619 2 * 500 2 * 358 2 * 533	In. 2 * 591 2 * 601 2 * 479 2 * 354 2 * 536	In. 2:590 2:592 2:453 2:292 2:546	In. 2:578 2:568 2:419 2:321 2:557	In. 2.584 2.573 2.423 2.322 2.575	In. 2:587 2:564 2:408 2:317 2:589
3.	6 7 8 9 10 11 12	2.675 2.713 2.902 2.923 2.805 2.609	2.685 2.725 2.921 2.927 2.807 2.605	2.690 2.729 2.929 2.927 2.794 2.610	2.685 2.739 2.943 2.920 2.789 2.608	2.679 2.743 2.942 2.927 2.774 2.599	2.671 2.748 2.955 2.919 2.761 2.584	2.645 2.733 2.931 2.903 2.753 2.574	2.622 2.733 2.905 2.901 2.729 2.579	2·578 2·725 2·881 2·893 2·700 2·563	2·575 2·723 2·876 2·874 2·686 2·565	2.567 2.723 2.862 2.866 2.675 2.551	2.575 2.733 2.866 2.845 2.667 2.543
SEPTEMBER	13 14 15 16 17 18 19	2.510 2.633 2.810 2.577 2.460 2.674	2:506 2:665 2:851 2:571 2:484 2:687	2:490 2:695 2:827 2:565 2:490 2:696	2:478 2:717 2:811 2:560 2:499 2:724	2:457 2:729 2:805 2:542 2:531 2:735	2:440 2:732 2:797 2:530 2:535 2:737	2:440 2:714 2:772 2:516 2:550 2:736	2.459 2.688 2.754 2.511 2.548 2.743	2·387 2·672 2·720 2·494 2·541 2·731	2:366 2:674 2:701 2:506 2:546 2:718	2:360 2:672 2:678 2:498 2:555 2:728	2:358 2:660 2:671 2:490 2:563 2:733
	20 21 22 23 24 25 26	2.721 2.847 2.672 2.599 2.685 2.524	2.759 2.848 2.665 2.641 2.666 2.539	2.774 2.850 2.653 2.609 2.643 2.539	2.812 2.850 2.653 2.646 2.593 2.556	2.834 2.857 2.641 2.648 2.553 2.570	2.834 2.841 2.634 2.611 2.513 2.573	2.824 2.826 2.618 2.619 2.471 2.563	2.798 2.805 2.594 2.627 2.451 2.542	2·778 2·786 2·558 2·629 2·419 2·529	2·785 2·790 2·545 2·629 2·361 2·519	2·783 2·769 2·543 2 635 2·331 2·511	2.787 2.758 2.528 2.649 2.270 2.513
ļ	27 28 29 30	2.874 2.762 2.437	2·862 2·740 2·441	2·878 2·736 2·433	2·876 2·719 2·420	2·893 2·699 2·413	2·861 2·681 2·398	2.846 2.641 2.375	2 · 833 2 · 639 2 · 352	2·823 2·627 2·324	2·799 2·626 2·310	2.793 2.604 2.312	2.789 2.590 2.326
Hourly	Means	2.6554	2.6644	2.6632	2.6654	2.6652	2.6552	2.6406	2.6298	2.6089	2.6007	2.259	2.291
	$\begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$	2:475 2:434 2:732	2:491 2:470 2:766	2.518 2.471 2.766	2.543 2.505 2.765	2:543 2:525 2:776	2 · 555 2 · 541 2 · 747	2:549 2:546 2:732	2:547 2:545 2:726	2.535 2.557 2.686	2.533 2.587 2.675	2.529 2.587 2.671	2.505 2.607 2.658
	4 5 6 7 8 9	2.670 2.845 2.687 2.875 2.852 3.104	2.675 2.869 2.699 2.903 2.854 3.132	2.680 2.875 2.701 2.919 2.836 3.139	2.684 2.868 2.700 2.925 2.808 3.148	2.683 2.847 2.689 2.926 2.802 3.151	2.690 2.835 2.670 2.944 2.811 3.155	2.688 2.801 2.654 2.954 2.801 3.156	2:676 2:772 2:638 2:938 2:789 3:156	2.679 2.742 2.651 2.936 2.823 3.140	2.675 2.733 2.658 2.940 2.838 3.134	2.687 2.707 2.655 2.922 2.859 3.108	2·711 2·699 2·657 2·919 2·894 3·113
OCTOBER.	11 12 13 14 15 16 17	2.682 2.468 2.403 2.495 2.507 2.922	2.690 2.444 2.417 2.519 2.489 2.941	2.677 2.424 2.434 2.555 2.465 2.865	2.665 2.388 2.445 2.570 2.457 2.843	2.638 2.336 2.447 2.590 2.435 2.852	2.635 2.288 2.450 2.601 2.434 2.856	2.607 2.235 2.441 2.602 2.407 2.851	2.582 2.182 2.432 2.611 2.375 2.831	2·552 2·117 2·422 2·613 2·346 2·816	2·538 2·038 2·414 2·618 2·422 2·818	2:535 2:020 2:409 2:623 2:425 2:829	2.541 1.998 2.393 2.633 2.433 2.837
OCTO	18 19 20 21 22 23	2.772 2.604 2.764 2.587 2.712 2.464	2.783 2.604 2.768 2.581 2.712 2.476	2.785 2.604 2.798 2.557 2.693 2.516	2·787 2·598 2·796 2·538 2·639 2·528	2.776 2.600 2.794 2.538 2.559 2.531	2·762 2·589 2·787 2·587 2·507 2·541	2.746 2.585 2.769 2.609 2.445 2.556	2.751 2.574 2.765 2.638 2.351 2.564	2.750 2.585 2.756 2.674 2.358 2.598	2·739 2·607 2·760 2·726 2·336 2·625	2·736 2·618 2·756 2·780 2·346 2·647	2.712 2.619 2.754 2.810 2.364 2.694
No	25 26 27 28 29 30 31 v. 1	2:845 2:295 2:796 2:607 2:975 3:186	2 · 833 2 · 327 2 · 809 2 · 643 3 · 000 3 · 192	2.823 2.358 2.825 2.655 3.031 3.192	2.818 2.402 2.825 2.642 3.049 3.199	2.806 2.416 2.826 2.652 3.063 3.175	2·767 2·430 2·810 2·656 3·076 3·166	2·724 2·443 2·778 2·661 3·091 3·148	2.652 2.453 2.757 2.649 3.099 3.118	2.613 2.457 2.735 2.653 3.103 3.098	2·592 2·483 2·722 2·683 3·125 3·086	2:571 2:503 2:719 2:702 3:129 3:059	2·523 2·526 2·704 2·734 3·144 3·009
	Means	2.6947	2.7070	2.7097	2.7087	2.7028	2.6996	2.6881	2.6730	2.6665	2.6706	2.6716	2.673

BAROMETRIC PRESSURE.  Barometer at 32° = 27 English inches + the numbers in the Table.													
12	13	14	15	16	17	18	19	20	21	22	23	Daily and	
6	7	8	9	10	11	12	13	14	15	16	17	Monthly Means,	
In. 2 · 593 2 · 547 2 · 410 2 · 314 2 · 611	In. 2 · 613 2 · 537 2 · 405 2 · 344 2 · 638	In. 2.632 2.542 2.408 2.354 2.675	In. 2 · 624 2 · 546 2 · 408 2 · 357 2 · 719	In. 2.627 2.533 2.390 2.371 2.732	In. 2:634 2:537 2:382 2:385 2:736	In. 2.633 2.531 2.374 2.386	In. 2.630 2.530 2.325 2.394	In. 2.624 2.512 2.329 2.404	1a. 2.628 2.510 2.341 2.412	In. 2.628 2.498 2.347 2.418	In. 2 * 624 2 * 482 2 * 375 2 * 452	In. 2.6152 2.5711 2.4269 2.3715	
2 · 567 2 · 567 2 · 740 2 · 856 2 · 834 2 · 651 2 · 551	2.596 2.765 2.849 2.820 2.639 2.545	2.622 2.782 2.857 2.820 2.629 2.543	2.633 2.783 2.861 — 2.637 2.537	2.632 2.789 2.867 2.811 2.641 2.531	2.646 2.810 2.867 2.829 2.643 2.540	2·711 2·653 2·810 2·868 2·822 2·630	2.707 2.652 2.826 2.880 2.841 2.596	2.703 2.668 2.829 2.888 2.839 2.584	2:699 2:679 2:839 2:889 2:843 2:582	2:684 2:684 2:847 2:889 2:841 2:595	2·671 } 2·697 2·872 2·919 2·813 2·593	2.6105 2.6407 2.7691 2.8919 2.8669 2.6818	
2:356 2:675 2:667 2:477 2:583 2:717	2·376 2·696 2·659 2·477 2·573 2·708	2·412 2·708 2·663 2·477 2·599 2·718	2:391 2:714 2:642 2:487 2:604 2:717	2:391 2:714 2:636 2:463 2:614 2:720	2·399 2·722 2·624 2·454 2·621 2·721	2:533 2:409 2:723 2:607 2:462 2:632 ————————————————————————————————————	2:541 2:430 2:749 2:622 2:438 2:625 ————————————————————————————————————	2:538 2:443 2:745 2:610 2:434 2:630 	2:524 2:506 2:760 2:598 2:426 2:630 — 2:555	2:520 2:534 2:780 2:590 2:431 2:643 	2.521 } 2.593 2.809 2.586 2.432 2.660	2:5589 2:4371 2:7102 2:6959 2:4924 2:5715 2:6772	
2·789 2·755 2·527 2·668 2·266 2·501	2·793 2·753 2·555 2·698 2·246 2·499	2.794 2.753 2.562 2.727 2.312 2.493	2.819 2.729 2.543 2.743 2.323 2.495	2.812 2.730 2.552 2.752 2.346 2.488	2.806 2.720 2.554 2.748 2.368 2.489	2.809 2.715 2.562 2.743 2.382	2 · 808 2 · 733 2 · 554 2 · 726 2 · 430	2.793 2.729 2.553 2.718 2.454	2.797 2.683 2.565 2.710 2.456	2.810 2.687 2.557 2.693 2.480	2·837 2·664 2·577 2·690 2·500	2.7982 2.7699 2.5819 2.6732 2.4383 2.5838	
2·785 2·566 2·342	2·791 2·578 2·352	2·789 2·565 2·374	2·797 2·564 2·362	2·771 2·555 2·370	2·776 2·532 2·374	2.722 2.772 2.542 2.382	2.736 2.784 2.506 2.387	2.751 2.781 2.489 2.404	2.755 2.775 2.481 2.412	2.781 2.772 2.473 2.418	2·824 } 2·764 2·463 2·444	2:8118 2:5991 2:3817	
2.2903	2.5963	2.6081	2.6014	2.6092	2.6122	2.6112	2.6133	2.6139	2.6175	2.6231	2.6355	2.6237	
2.503 2.623 2.649	2:504 2:641 2:645	2:513 2:659 2:649	2:500 2:685 2:635	2:498 2:694 2:641	2:474 2:698 2:642	2:496 2:706	2.503 2.713	2·469 2·711	2:463 2:708	2:445 2:708	2:434 2:726	2.5052 2.6103 2.6838	
2.711 2.691 2.697 2.928 2.926 3.117	2.743 2.689 2.709 2.904 2.938 3.113	2·769 2·693 2·719 2·890 2·982 3·104	2·793 2·665 2·715 2·910 3·021 3·100	2.816 2.673 2.735 2.908 3.029 3.118	2.813 2.661 2.767 2.902 3.035 3.122	2.649 2.823 2.666 2.787 2.878 3.036	2:643 2:834 2:672 2:775 2:844 3:038	2:639 2:846 2:673 2:770 2:844 3:049	2:635 2:853 2:671 2:814 2:838 3:062	2:636 2:843 2:669 2:828 2:834 3:076	2:648 } 2:834 2:687 2:849 2:844 3:084	2 '7448 2 '7376 2 '7177 2 '9010 2 '9268 3 '0301	
2.547 2.000 2.405 2.644 2.458 2.843	2:559 2:033 2:400 2:660 2:460 2:844	2:559 2:085 2:409 2:672 2:536 2:834	2:552 2:108 2:425 2:659 2:579 2:822	2:574 2:146 2:423 2:680 2:619 2:820	2.571 2.184 2.412 2.662 2.656 2.816	2:777 2:549 2:225 2:408 2:663 2:626	2.763 2.540 2.283 2.415 2.667 2.620	2.747 2.532 2.304 2.427 2.678 2.702	2.721 2.500 2.320 2.447 2.653 2.745	2.716 2.494 2.343 2.459 2.635 2.792	2.688 } 2.480 2.377 2.485 2.563 2.787	2:5750 2:2227 2:4259 2:6194 2:5323	
2.716 2.648 2.770 2.841 2.370 2.710	2.716 2.665 2.793 2.860 2.386 2.732	2.714 2.667 2.772 2.866 2.380 2.752	2.700 2.706 2.779 2.878 2.399 2.748	2:699 2:716 2:765 2:880 2:403 2:771	2.680 2.721 2.783 2.864 2.411 2.771	2.770 2.678 2.735 2.760 2.859 2.413	2.764 2.670 2.750 2.752 2.831 2.405	2.764 2.660 2.750 2.712 2.804 2.407	2.764 2.654 2.750 2.676 2.798 2.422	2.758 2.648 2.740 2.644 2.771 2.410	2.772 } 2.620 2.764 2.617 2.730 2.454	2.8263 2.7189 2.6583 2.7537 2.7336 2.4534	
2·512 2·566 2·698 2·758 3·156 3·017	2 · 488 2 · 600 2 · 686 2 · 792 3 · 171 3 · 025	2.462 2.606 2.681 2.804 3.185 3.018	2.450 2.657 2.657 2.692 2.834 3.180 3.028	2:430 2:671 2:689 2:846 3:184 3:029	2:420 2:691 2:689 2:863 3:192 3:023	2 · 921 2 · 404 2 · 707 2 · 671 2 · 877 3 · 193	2 · 914 2 · 358 2 · 746 2 · 649 2 · 877 3 · 198	2.898 2.337 2.752 2.633 2.894 3.201	2.894 2.313 2.759 2.625 2.904 3.193	2.874 2.295 2.773 2.621 2.908 3.198	2·871 } 2·295 2·790 2·616 2·957 3·191	2.5555 2.5558 2.5588 2.7190 2.7605 3.1303	
						2.734	2.724	2.709	2.690	2.677	2.690}	2.9997	
2.6853	2.6947	2.7030	2.7119	2.7206	2.7231	2.7041	2.7018	2.7004	2.6990	2.6961	2.6983	2.6960	

lours of Mea Göttingen	n} 0	1	2	3	4	5	6	7	8	9	10	11
Göttingen Time. Hours of Mea	<u> </u>	1	<u> </u>			<u> </u>	1	<u> </u>	<u> </u>	1	<u> </u>	<u> </u>
Toronto Time.	18	19	20	21	22	23	0	1	2	3	4	5
$\left(\begin{array}{c}2\\3\\4\\5\\6\\7\end{array}\right)$	In. 2 · 680 2 · 786 2 · 920 3 · 148 3 · 070 2 · 962	In. 2.680 2.800 2.950 3.174 3.058 2.950	In. 2.687 2.820 2.970 3.192 3.082 2.950	In. 2.677 2.818 3.004 3.206 3.090 2.939	In. 2:694 2:828 3:013 3:200 3:070 2:929	In. 2.684 2.827 3.034 3.192 3.065 2.931	In. 2:674 2:805 3:024 3:178 3:053 2:912	In. 2.667 2.791 3.035 3.173 3.022 2.904	In. 2.660 2.799 3.023 3.153 3.009 2.886	In. 2.646 2.798 3.031 3.147 3.002 2.883	In. 2.656 2.778 3.047 3.136 2.999 2.868	In. 2.680 2.783 3.071 3.127 2.979 2.860
8 9 10 11 12 13 14 15 15	2·639 2·758 2·648 2·874 2·858 2·736	2.657 2.754 2.670 2.902 2.866 2.752	2:663 2:782 2:686 2:910 2:868 2:759	2.684 2.776 2.700 2.926 2.862 2.761	2.682 2.770 2.714 2.930 2.857 2.753	2.688 2.741 2.712 2.930 2.845 2.739	2:681 2:733 2:718 2:917 2:819 2:731	2.683 2.719 2.724 2.894 2.807 2.712	2.678 2.693 2.717 2.886 2.793 2.692	2.690 2.677 2.735 2.884 2.785 2.694	2.690 2.695 2.747 2.886 2.783 2.696	2·718 2·691 2·773 2·878 2·780 2·700
NOVEMBER. 19 10 12 12 12 12 12 12 12 12 12 12 12 12 12	2.812 2.827 2.569 2.466 2.295 2.501	2.834 2.817 2.569 2.451 2.319 2.510	2.847 2.817 2.581 2.403 2.337 2.512	2.854 2.811 2.589 2.351 2.367 2.509	2.867 2.793 2.596 2.339 2.397 2.503	2.865 2.770 2.586 2.269 2.410 2.494	2.867 2.746 2.581 2.191 2.411 2.466	2·879 2·736 2·573 2·188 2·411 2·459	2.867 2.722 2.595 2.075 2.441 2.415	2.878 2.696 2.590 2.073 2.464 2.403	2·878 2·670 2·609 2·058 2·466 2·391	2.892 2.650 2.616 2.050 2.476 2.383
22 23 24 25 26 27 28 29	2·499 2·378 2·261 2·214 2·560 2·350	2:531 2:386 2:259 2:223 2:554 2:366	2:539 2:396 2:256 2:233 2:568 2:394	2.591 2.400 2.258 2.242 2.578 2.437	2.604 2.397 2.211 2.238 2.572 2.475	2.617 2.395 2.184 2.212 2.548 2.483	2.613 2.385 2.172 2.199 2.521 2.498	2.631 2.375 2.153 2.192 2.497 2.506	2.621 2.379 2.156 2.188 2.467 2.514	2.604 2.385 2.168 2.213 2.439 2.521	2.600 2.378 2.184 2.232 2.429 2.525	2·583 2·373 2·197 2·250 2·395 2·535
$\binom{29}{30}$	3.030	3.036	3.052	3.073	3.081	3.062	3.067	3.041	3.027	3.039	3.021	3.061
Hourly Mea	ns 2.6736	2.6827	2.6922	2.7001	2.7005	2.6914	2.6785	2.6709	2.6582	2.6578	2.6581	2.660
$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ \end{pmatrix}$	3.097 2.582 2.299 2.686 3.125 ————————————————————————————————————	3:111 2:558 2:312 2:700 3:125 	3.097 2.534 2.331 2.721 3.129 	3.086 2.492 2.348 2.761 3.153 	3.085 2.481 2.354 2.776 3.159 	3.046 2.436 2.353 2.776 3.143 	3·020 2·402 2·345 2·788 3·124 2·507 2·367 2·708 2·320 2·658	2 · 992 2 · 375 2 · 369 2 · 868 3 · 108 — 2 · 486 2 · 363 2 · 726 2 · 306	2·974 2·358 2·375 2·830 3·008 — 2·440 2·364 2·742 2·306	2 · 955 2 · 347 2 · 401 2 · 853 3 · 092 — 2 · 434 2 · 381 2 · 746 2 · 305	2:940 2:317 2:405 2:877 3:091 — 2:416 2:394 2:746 2:301	2 · 922 2 · 262 2 · 435 2 · 919 3 · 096 2 · 390 2 · 421 2 · 749 2 · 303
DECEMBER. 12 13 14 15 16 17 18 19 19	2·877 2·924 2·893 2·795 2·544 2·388 2·028	2 · 889 	2 · 905 	2 · 922 	2 · 945 2 · 945 2 · 983 2 · 920 2 · 790 2 · 590 2 · 304 2 · 094	2 · 929 2 · 960 2 · 906 2 · 753 2 · 556 2 · 257 2 · 083	2 · 907 2 · 940 2 · 872 2 · 732 2 · 553 2 · 215 2 · 081	2.664 2.905 2.926 2.857 2.728 2.543 2.196 2.090	2.677 2.871 2.920 2.841 2.697 2.523 2.178 2.112	2.696   2.871   2.926   2.842   2.686   2.509   2.158   2.144	2.712 2.857 — 2.936 2.839 2.671 2.493 2.153 2.170	2.698 2.859 2.936 2.844 2.654 2.485 2.134 2.186
20 21 22 23 24 25		2.613 2.802 3.180 2.841	2.677 2.829 3.198 2.811	2·732 2·860 3·218 2·800	2.790 2.880 3.238 2.759	2.808 2.902 3.226 2.711	2·794 2·898 3·202 2·660	2.802 2.912 3.198 2.654	2.822 2.932 3.190 2.596	2.835 2.964 3.186 2.584	2.856 2.998 3.184 2.582	2.869 3.039 3.148 2.564
26 27 28 29 30 31	2·895 — 2·181 2·884 2·244 2·577	2 · 903 	2 · 900 	2 · 905 2 · 231 2 · 908 2 · 291 2 · 566	2.888 	2.859 2.236 2.890 2.340 2.503	2·780 2·246 2·868 2·361 2·459	2.743 	2.685 2.277 2.830 2.401 2.435	2.639 2.339 2.804 2.453 2.440	2.603 2.381 2.787 2.494 2.410	2:542 2:436 2:750 2:533 2:436

BAROMETRIC PRESSURE.  Barometer at 32° = 27 English inches + the numbers in the Table.													
12	13	14	15	16	17	18	19	20	21	22	23	Daily and	
6	7	8	9	10	11	12	13	14	15	16	17	Monthly Means.	
In. 2.655 2.787 3.071 3.134 2.977 2.850	In. 2.655 2.793 3.093 3.115 2.979 2.848	In. 2.669 2.805 3.091 3.099 2.977 2.845	In. 2 '690 2 '826 3 '106 3 '088 2 '982 2 '821	In. 2.688 2.830 3.115 3.077 2.987 2.815	In. 2.698 2.835 3.118 3.065 2.967 2.797	In. 2:719 2:847 3:134 3:058 2:968	In. 2.742 2.851 3.119 3.064 2.950	In. 2.754 2.855 3.123 3.068 2.936	In. 2.766 2.872 3.132 3.070 2.940	In. 2.782 2.891 3.132 3.061 2.940	In. 2 '780 2 '908 3 '144 3 '072 2 '957	In. 2 * 6951 2 * 8222 3 * 0625 3 * 1249 3 * 0024	
2.730 2.691 2.796 2.880 2.782 2.700	2.734 2.693 2.808 2.886 2.782 2.690	2.742 2.675 2.808 2.886 2.781 2.670	2.750 2.675 2.820 2.889 2.785 2.675	2·750 2·646 2·836 2·889 2·768 2·677	2.756 2.642 2.838 2.875 2.764 2.676	2.634 2.764 2.646 2.836 2.865 2.754	2.631 2.757 2.622 2.841 2.875 2.752	2.618 2.758 2.630 2.849 2.853 2.752	2.611 2.756 2.622 2.849 2.853 2.750	2.610 2.756 2.622 2.853 2.853 2.746	2.630 } 2.758 2.629 2.855 2.857 2.732	2.8202 2.7152 2.6909 2.7722 2.8866 2.7946	
2 · 906 2 · 642 2 · 608 2 · 021 2 · 502 2 · 390	2 · 906 2 · 638 2 · 626 2 · 019 2 · 496 2 · 365	2.898 2.608 2.631 2.007 2.498 2.307	2.890 2.608 2.629 2.005 2.506 2.289	2.882 2.590 2.609 2.041 2.506 2.271	2.870 2.580 2.580 2.598 2.066 2.513 2.277	2.780 2.866 2.564 2.598 2.092 2.505	2·772 2·857 2·566 2·580 2·126 2·493	2:784 2:855 2:567 2:554 2:132 2:479	2:792 2:845 2:566 2:514 2:178 2:482	2 · 803 2 · 831 2 · 562 2 · 476 2 · 243 2 · 490	2·800 } 2·833 2·561 2·470 2·271 2·499	2.7310 2.8658 2.6711 2.5811 2.1715 2.4485 2.4107	
2.563 2.385 2.201 2.258 2.367 2.553	2:549 2:382 2:201 2:286 2:373 2:565	2:537 2:386 2:201 2:300 2:364 2:571	2.521 2.364 2.201 2.308 2.359 2.560	2:514 2:346 2:195 2:334 2:356 2:552	2·496 2·328 2·185 2·358 2·334 2·564	2:338 2:472 2:321 2:190 2:376 2:337	2:372 2:444 2:301 2:192 2:450 2:326	2:388 2:426 2:301 2:196 2:484 2:338	2.411 2.411 2.291 2.202 2.512 2.331	2:433 2:409 2:263 2:204 2:538 2:327	2:469 } 2:380 2:263 2:204 2:542 2:329	2:5311 2:3566 2:2013 2:3076 2:4279	
3.082	3.098	3.103	3.104	3.102	3.102	3.102	2.969 3.102	2.973 3.098	3.002 3.092	3.010	3.004 } 3.095	2.6200 3.0752	
2.6614	2.6632	2.6584	2.6580	2.6550	2.6521	2.6687	2.6702	2.6708	2.6741	2.6768	2.6817	2.6714	
2.924 2.236 2.463 2.939 3.092	2.886 2.222 2.480 2.965 3.098	2.878 2.217 2.492 2.983 3.092	2.851 2.229 2.540 2.979 3.102	2.802 2.215 2.583 2.992 3.110	2.772 2.217 2.597 3.013 3.106	2.741 2.224 2.620 3.017	2:735 2:251 2:624 3:047	2.733 2.249 2.631 3.053	2.700 2.254 2.639 3.074	2:674 2:280 2:647 3:090	2.627 2.274 2.655 3.103	2 · 9020 2 · 3338 2 · 4707 2 · 9062 3 · 0435	
2·372 2·409 2·783 2·313 2·709 2·869	2:341 2:423 2:780 2:323 2:714 2:847	2:305 2:418 2:770 2:337 2:736 2:849	2·251 2·408 2·752 2·337 2·762 2·853	2·217 2·398 2·744 2·353 2·778 2·851	2:184 2:418 2:737 2:368 2:780 2:851	2:919 2:157 2:430 2:728 2:372 2:790	2:878 2:167 2:428 2:712 2:404 2:819	2.852 2.181 2.459 2.691 2.426 2.837	2 · 819 2 · 200 2 · 477 2 · 663 2 · 472 2 · 837	2.780 2.236 2.531 2.616 2.494 2.841	2.763 } 2.265 2.557 2.608 2.529 2.861	2:3983 2:4037 2:7042 2:3888 2:7198	
2 · 944 2 · 846 2 · 636 2 · 489 2 · 119 2 · 200	2 · 944 2 · 873 2 · 624 2 · 483 2 · 112 2 · 219	2·940 2·873 2·620 2·473 2·096 2·227	2 · 945 2 · 863 2 · 598 2 · 465 2 · 078 2 · 231	2.931 2.853 2.572 2.463 2.048 2.274	2 · 922 2 · 846 2 · 560 2 · 443 2 · 044 2 · 282	2:932 2:912 2:840 2:546 2:424 2:036	2 · 934 2 · 910 2 · 816 2 · 550 2 · 396 2 · 044	2 · 942 2 · 910 2 · 811 2 · 550 2 · 407 2 · 036	2 · 939 2 · 904 2 · 817 2 · 550 2 · 399 2 · 032	2:939 2:909 2:801 2:559 2:391 2:032	2·925 } 2·893 2·802 2·542 2·390 2·020	2 * 8945 2 * 9329 2 * 8582 2 * 6567 2 * 4860 2 * 1572	
2·877 3·048 3·155 2·562	2.885 3.060 3.157 2.545	2 · 887 3 · 067 3 · 146 2 · 522	2.887 3.059 3.126 2.506	2.890 3.069 3.097 2.496	2.866 3.069 3.069 2.494	2.400 2.853 3.067 3.035	2:390 2:809 3:085 3:021	2:382 2:799 3:091 3:011	2:407 2:781 3:119 2:992	2:457 2:779 3:135 2:978	$ \begin{array}{c}  - \\  2 \cdot 495 \\  2 \cdot 784 \\  3 \cdot 146 \\  2 \cdot 897 \\  - \\  2 \cdot 887 \end{array} $	2.2134 2.8017 2.9928 3.1255 2.6931	
2·499 	2·467 2·549 2·682 2·580 2·427	2·437 2·584 2·612 2·584 2·408	2·382 2·650 2·566 2·608 2·406	2·345 	2·312 2·684 2·440 2·610 2·399	2.800 2.190 2.751 2.414 2.597 2.400	2.826 2.190 2.785 2.376 2.616 2.366	2.854 	2:860 2:203 2:843 2:326 2:597 2:386	2.848 2.187 2.847 2.302 2.589 2.402	2.887 {	2.5391 2.4893 2.6617 2.4767 2.4526	
2.6420	2.6418	2.6367	2.6321	2.6257	2.6186	2.6229	2.6223	2.6267	2.6265	2.6286	2.6291	2.6424	

BAROMETRIC PRESSURE.  Barometer at 32° = 27 English inches + the numbers in the Table.													
lours of Cotting	Mean }	0	1	2	3	4	5	6	7	8	9	10	11
Time Iours of Toron Time	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
		In.	In.	In.	In.	In	In.	In.	In.	In.	In.	In.	Jn.
	$\begin{bmatrix} 1 \\ 2 \end{bmatrix}$	2.507 2.472	2.510 2.490	2.546 2.530	2.582 2.581	2.628 2.606	2.608 2.621	2.594 2.622	2.588 2.612	2.581 2.646	2:598 2:667	2.604 2.681	2.571 2.692
	3 4 5 6 7 8 9	2.813 2.036 2.580 2.005 2.440 2.852	2.748 2.095 2.586 1.933 2.483 2.866	2.713 2.148 2.600 1.946 2.521 2.870	2.656 2.181 2.645 1.917 2.559 2.858	2.624 2.232 2.634 1.895 2.607 2.861	2·552 2·224 2·608 1·871 2·612 2·836	2:474 2:213 2:578 1:893 2:615 2:798	2:401 2:237 2:555 1:921 2:628 2:775	2:337 2:242 2:546 1:966 2:667 2:782	2·283 2·260 2·538 2·008 2·708 2·794	2·208 2·270 2·523 2·034 2·738 2·801	2·161 2·284 2·535 2·078 2·746 2·794
ARY.	10 11 12 13 14 15 16	2.693 2.884 2.874 2.429 2.374 2.197	2.688 2.907 2.854 2.414 2.328 2.248	2.676 2.959 2.816 2.414 2.276 2.304	2.686 3.001 2.792 2.428 2.219 2.349	2.687 3.024 2.752 2.430 2.172 2.402	2.664 3.023 2.720 2.415 2.131 2.410	2.624 3.006 2.675 2.383 2.080 2.415	2.591 3.025 2.642 2.359 2.069 2.429	2.590 3.030 2.621 2.361 2.056 2.487	2.589 3.051 2.620 2.372 2.054 2.564	2.589 3.062 2.596 2.382 2.066 2.624	2.604 3.069 2.568 2.385 2.058 2.727
JAN	17 18 19 20 21 22 23	2:405 2:568 3:093 2:824 2:889 2:245	2:378 2:610 3:093 2:822 2:901 2:259	2:383 2:678 3:093 2:836 2:904 2:291	2:377 2:724 3:093 2:840 2:905 2:300	2:363 2:763 3:098 2:820 2:839 2:316	2:336 2:782 3:076 2:816 2:871 2:324	2:316 2:802 3:013 2:818 2:828 2:345	2·271 2·820 2·975 2·816 2·803 2·353	2·276 2·860 2·962 2·828 2·780 2·388	2·291 2·894 2·952 2·854 2·775 2·409	2·295 2·912 2·948 2·862 2·737 2·428	2:307 2:950 2:922 2:881 2:701 2:439
	24 25 26 27 28 29 30 31	2:902 2:411 2:867 3:218 2:638 2:207	2·922 2·378 2·898 3·219 2·616 2·227	2:948 2:304 2:937 3:216 2:599 2:288	2 · 958 2 · 295 2 · 956 3 · 232 2 · 593 2 · 312	2.960 2.268 2.984 3.219 2.545 2.337	2·959 2·254 2·990 3·208 2·472 2·356	2·941 2·236 3·001 3·163 2·370 2·372	2.931 2.232 3.008 3.137 2.296 2.385	2·930 2·286 3·021 3·104 2·231 2·401	2·917 2·357 3·051 3·090 2·189 2·429	2·922 2·432 3·087 3·051 2·149 2·451	2:901 2:472 3:107 3:007 2:123 2:473
lourly:	Means	2.5932	2.2021	2 6075	2.6169	2.6179	2.6054	2.5837	2.5715	2.5761	2.5890	2.2943	2.598
	1 2 3 4 5 6	2:371 2:531 2:098 2:322 2:736 2:747	2:406 2:521 2:057 2:362 2:742 2:762	2:428 2:520 2:017 2:406 2:747 2:779	2:445 2:517 1:959 2:491 2:755 2:789	2:473 2:501 1:907 2:529 2:744 2:802	2:483 2:488 1:857 2:545 2:742 2:788	2:499 2:458 1:803 2:550 2:722 2:758	2.498 2.449 1.747 2.552 2.713 2.734	2:521 2:431 1:734 2:561 2:711 2:725	2:539 2:435 1:721 2:591 2:705 2:729	2.548 2.425 1.732 2.625 2.684 2.732	2:543 2:411 1:744 2:647 2:680 2:726
ARY.	7 8 9 10 11 12 13	2:257 2:159 2:451 2:630 2:471 2:734	2·273 2·223 2·465 2·637 2·471 2·738	2·284 2·258 2·486 2·644 2·485 2·741	2·282 2·294 2·507 2·662 2·501 2·724	2·275 2·321 2·497 2·661 2·531 2·698	2·252 2·336 2·507 2·649 2·545 2·687	2:240 2:342 2:491 2:633 2:544 2:652	2·224 2·340 2·488 2·633 2·537 2·625	2·188 2·350 2·493 2·637 2·556 2·599	2·175 2·364 2·514 2·637 2·591 2·595	2·167 2·378 2·534 2·623 2·621 2·593	2:131 2:404 2:553 2:639 2:665 2:591
FEBRUARY.	14 15 16 17 18 19 20	2:505 2:919 2:677 2:893 2:768 2:986	2:563 2:903 2:694 2:893 2:780 3:005	2.631 2.903 2.742 2.919 2.821 3.015	2.673 2.865 2.745 2.931 2.845 3.024	2·724 2·838 2·745 2·925 2·842 3·022	2.776 2.801 2.768 2.905 2.870 3.026	2.800 2.733 2.760 2.888 2.876 3.012	2.808 2.664 2.755 2.854 2.873 3.001	2.836 2.614 2.757 2.821 2.876 2.989	2.874 2.570 2.756 2.820 2.885 2.879	2.906 2.540 2.769 2.800 2.913 2.987	2:901 2:517 2:763 2:792 2:907 2:995
	21 22 23 24 25 26 27 28	2:452 2:894 3:083 2:816 2:995 2:355	2·452 2·945 3·093 2·834 2·991 2·301	2.458 2.975 3.093 2.838 2.990 2.229	2·472 3·007 3·100 2·846 3·012 2·217	2·472 3·019 3·091 2·872 2·994 2·167	2:466 3:036 3:081 2:867 2:973 2:073	2:463 3:026 3:056 2:872 2:924 1:954	2·472 3·017 3·015 2·862 2·906 1·925	2:488 3:019 2:985 2:854 2:891 1:866	2:505 3:017 2:978 2:863 2:864 1:838	2·527 3·036 2·944 2·882 2·837 1·818	2:572 3:042 2:938 2:897 2:813 1:818
Hourly	Means	2.6187	2.6296	2.6420	2.6526	2.6521	2.6467	2.6273	2.6122	2.6043	2.6060	2.6092	2.612

12	13	1.1	1 =				1	1 20	0.1	00	23	
		14	15	16	17	18	19	20	21	22	20	Daily an Monthl
6	7	8	9	10	11	12	13	14	15	16	17	Means
In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
	2.479	2.401	2.310	2.306	2.313	2.289	2.316	2.342	2.365	2.392	2.426	2.473
2·509 2·712	2 479 2 726	$\frac{2.401}{2.724}$	$\frac{2.310}{2.738}$	$\begin{array}{c} 2.300 \\ 2.744 \end{array}$	$\frac{2.753}{2.753}$						)	2.706
						2.937	2.919	2.916	2.887	2.821	2.822 }	
.096	2.056	1.989	1.883	1.858	1.840	1.862	1'914	1.934	1.952	1.968	$\frac{2.002}{2.564}$	2.326
314	2.314	2.340	2.370	2.404	2.426	$2.475 \\ 2.275$	2:504 2:230	2:542 2:172	2.570 2.141	$\frac{2.582}{2.107}$	2.039	2.436
:527	2.497	2:457	2:393	2.381 $2.208$	2·324 2·229	$\frac{2}{2} \cdot \frac{2}{13}$	$\frac{2}{2} \cdot \frac{230}{274}$	$\frac{2}{2} \cdot \frac{112}{292}$	$\frac{2}{2} \cdot 331$	$\frac{2}{2} \cdot \frac{107}{367}$	$\frac{2.401}{2.401}$	2.100
103	2.130	2·174 2·796	2.189 2.818	2.830	2.829	2.833	2.831	2.843	2.848	2.832	2.842	2.7150
2.760 2.791	$\begin{array}{c} 2.774 \\ 2.822 \end{array}$	2.842	$\frac{2.839}{2.839}$	$\frac{2.850}{2.851}$	2.863	_					i i	2.806
	2 022					2.769	2.757	2.749	2.743	2.740	$\frac{-}{2.707}$	
2.613	2.640	2.656	2.680	2.730	2.746	-	2.771	2.803	2.822	2'851	2 863	2.689
070	3.081	3.072	3.028	3.045	3.044	3.016	2.986	2.968	2.934	2.888	2.888	3,003,
:546	2.230	2.506	2.468	2.454	2.460	2.448	2.455	2.453	2.466	2.461	2.429	$\frac{2:5920}{2:4270}$
2.421	2.427	2.447	2.490	2.476	2.472	2.467	2.485	2.485	2.457	2·429 2·120	2.419 2.160	2 427
2.074	2.070	2.022	2.038	2.058	2.052	2.044	2.028	2.099	2.108	2 120	Z 100	
2.777	2.864	2.899	2.930	2.944	2.979	2.649	2.602	2.592	2.246	2.498	2.436	2.578
	0.007	2.350	2.356	$2.\overline{371}$	2.393	2.375	2.388	2.431	2.458	2.476	2.494	2.364
2:327	2:337	2 330	$\frac{2.995}{2.995}$	3.004	3.022	3.029	$\frac{3.055}{2.005}$	3.069	3.079	3.079	3.075	2.904
? '972 ? '919	$2.974 \\ 2.917$	2.902	2.905	2.887	2.865	2.849	2.835	2.830	2.810	2.850	2.822	2.945
2.892	$\frac{2}{2} \cdot 897$	2.886	2.891	2.877	2.893	2.893	2.907	2.909	2'914	2.910	2.881	2.865
2.661	2.614	2.563	2.543	2.219	2.465	2.435	2.363	2.339	2.311	2.282	2.543	2.636
462	2.483	2.486	2.434	2.482	2.486						- )	2.507
		_	_			2.841	2.853	2.863	2.867	2.882	2.888	
8.896	2.894	2.864	2.839	2.811	2.766	2.736	2.692	2.658	2.626	$2.557 \\ 2.813$	2.481 2.838	2.833 2.514
2.26	2.578	2.605	2.654	2.663	2.693	2.717	$2.756 \\ 3.252$	$\begin{vmatrix} 2.777 \\ 3.272 \end{vmatrix}$	$\frac{2.795}{3.258}$	$\frac{2}{3}$ :227	$\frac{2}{3} \cdot 200$	3.103
3.142	3.154	3.181	3.205	3.208	3.220	3.248	$\frac{3}{2},\frac{232}{770}$	$\frac{3}{2}.758$	$\frac{3}{2}.743$	$\frac{3}{2}.704$	2.666	2.989
3.002	2.948	2.910	2.884	$2.858 \\ 2.025$	2.834	$\frac{2.035}{2.035}$	2.010	2.063	2.099	$\frac{2}{2} \cdot 141$	2.173	2.237
2:097	2.079	$2.055 \\ 2.516$	2.033 2.211	2.524	2.528	2 000					— 1	i
<del></del>	2.206	2 510 —			_	2.337	2.335	2.335	2.347	2:354	2.356	2:391
2.6044	2.6073	2.6015	2.5963	2.5967	2.5971	2.5843	2.2911	2.5960	2.5954	2.5899	2.5813	2.595
							1 0 000	2.004	01.500	0.700	0:740	0.524
2.240	2.566	2.582	2.618	2.642	2.603	2.598	2.600	2.604	2.589	2.562	2.549 2.140	2.534 2.397
394	2.390	2.374	2.369	2:369	2.356	2.328	2.308	2.302	2.510	$2.247 \\ 2.257$	2.140	1.949
791	1.835	1.862	1.905	$1.970 \\ 2.721$	2.019 2.719	2.039	2.707	$\frac{2.709}{2.709}$	$\frac{2}{2} \cdot 722$	2.716	2.732	2.613
2.675 2.685	2.695	2.707	$2.715 \\ 2.676$	2.688	2.696	2.695	2.692	2.692	2.722	$\frac{1}{2} \cdot 724$	2.730	2.710
716	2.684 2.694	2.684 2.688	2.699	2.709	2.713							2.608
, 110 —	2 094	2 000	2 000			2.204	2.198	2.209	2.213	<b>2</b> .233	$\left  \frac{-}{2 \cdot 247} \right\}$	ł
2.112	2.112	2.109	2.032	2.012	1.981	1.957	1.971	1.983	2.017	2.039	2.092	2.132
426	2.426	2.432	2.441	2.443	2.455	2.443	2.445	2.447	2'454	2.442	2.449	2:378
564	2.572	2.583	2.596	2.613	2.624	2.632	2.621	2.612	2.608	2.617	2.629	2.552 $2.599$
645	2.639	2.627	2.595	2.575	2.553	2.541	2.530	2.528	2.502	$2.493 \\ 2.722$	$2.470 \\ 2.732$	2 599 2 633
679	2.692	2.717	2.734	2.740	2.727	2.733	2.732	2.740	2.726	2 122		l
.603	2.609	2.638	2.645	2.632	2.620	2.439	2.434	2.436	2.441	2.455	$2.\frac{-}{457}$	2.599
	0:050	9:070	2:000	2.986	2.984	2 439	2 434	2.974	$\frac{2.441}{2.973}$	$\frac{2.455}{2.958}$	2.937	2.861
951 495	2.976 2.480	$2.976 \\ 2.464$	2.990 2.470	2 986	2 486	2.506	2.212	2.22	2.280	2.596	2.612	2.629
802	2 480	2 404	2.844	2.847	2.851	2.860	2.871	2.883	2.898	2.900	2.893	2.802
774	$\frac{2.320}{2.760}$	$\frac{2}{2}.771$	2.774	2.774	2.772	2.772	2.754	2.748	2.742	2.746	2,768	2.816
929	2.957	2.953	2.969	2.969	2.969	2.967	2.967	2.970	2.974	2.964	2.984	2.909
'994	2.985	2.979	2.987	2.990	2.935				0:460	0:400	0:45.	2.862
	_	_				2.469	2.467	2.467	2.462	2.462 2.831	2.454	2.609
594	2.631	2.647	2.689	2.732	2.744	2.758	2.757	2.776 3.070	2.799 3.067	$\frac{2.831}{3.073}$	2.864 3.085	3.034
050	3.058	3.074	3.065	3.058	3.062	$3.066 \\ 2.852$	3.073 2.826	2.797	2.793	2.793	2.803	2.939
896 902	2.882	2.859	2.864	2.864	2.860 2.964	$2.852 \\ 2.965$	2.973	2.981	2.982	2.982	3.002	2.909
41.17	2.928	2.932	2.947 2.700	$2.953 \\ 2.676$	2 964	2.584	2.228	2.494	2.466	2.448	2.392	2.765
		2.741	<i>△</i> 100	2 010		2 004		1 - ~~ 1	1 - 100	1		1
.774	2.742		1.895	1.858	1.831	1		I —				0.000
7774 826	1.828	1.822	1·825 —	1.828	1.831	2.191	2.207	2.227	2.539	2.251	2.282	2.038

	f Mean ngen ne.	0	1	2	eter at 32° =	4	5	6	7	8	9	10	11
	f vlean ill	18	19	20	21	22	23	0	<u> </u>		1	1	1
Tir	ne.	10	10	20	21		20		1	2	3	4	5
	, 1	In. 2°313	In. 2·329	In. 2:394	In. 2.428	2.442	In. 2.479	In. 2.486	In. 2·492	In.	In.	In.	In.
	$\left(\begin{array}{cc} \frac{1}{2} \end{array}\right)$	$\frac{2.779}{2.779}$	$\frac{2.787}{2.787}$	$\frac{2.797}{2.797}$	2.420	2.818	2.822	$\frac{2.486}{2.815}$	$\frac{2.492}{2.777}$	$2.491 \\ 2.758$	$2.501 \\ 2.758$	2.520 2.759	2.539 $2.768$
	3	2.730	2.731	$\frac{5.739}{2.739}$	2.702	2.690	2.667	2.646	2.636	2.615	2.609	2.593	$\frac{2}{2}.59$
	4	2.716	2.738	2.764	2.773	2.782	$\frac{1}{2}$ .797	2.802	2.799	2.794	2.804	2.804	2.81
	5	2.969	3.008	3.024	3.026	3.033	3.046	3.026	3.015	3.012	3.005	3.000	3.00
	6   7	3.049	3.065	3.064	3.02	3.021	3.048	3.058	2.999	2.983	2.976	2.948	2.30
	8	2.679	2.716	2.745	2.767	2.792	2.793	2.807	2.801	2.811	2.839	2.845	2.85
	$\begin{vmatrix} 9 \\ 10 \end{vmatrix}$	2.984	2.982	2.988	2.973	2.977	2.959	2.959	2.901	2.885	2.873	2.859	2.85
	11	$2.683 \\ 2.891$	2.693 2.923	2.695 2.905	2.713 2.896	2.705 2.890	2.683 2.864	2.672	2.663	2.659	2.658	2.670	2.69
	12	$\frac{2.733}{2.733}$	2.734	$\frac{2.305}{2.736}$	$\frac{2.390}{2.780}$	$\frac{2.350}{2.767}$	$\frac{2.504}{2.730}$	$2.855 \\ 2.724$	2.824 2.696	2.816 2.686	2.804	2.791 5.685	$\begin{vmatrix} 2.79 \\ 2.65 \end{vmatrix}$
	13	2.694	2.714	2.724	2.740	2.727	$\frac{2.728}{2.728}$	2.722	2.686	2.673	2.668	2.667	$\frac{2.65}{2.67}$
Н.	$\begin{vmatrix} 14 \\ 15 \end{vmatrix}$	2.742	2.755	2.763	$2.\overline{752}$	2.750	2.703	2.742	2.732	2.716	2.718	$\frac{-}{2.718}$	2.718
MARCH.	16	2.707	2.714	$\frac{2}{2} \cdot 732$	$\frac{2.732}{2.742}$	2.748	$\frac{2.763}{2.764}$	$\frac{2}{2}, \frac{742}{765}$	2.732 $2.771$	$\frac{2.710}{2.768}$	$\frac{2.718}{2.788}$	$\frac{2.718}{2.793}$	$\frac{2}{2}.79$
AI	17	2.965	3.002	3.008	3.006	3.004	2.988	2.979	2.948	2.925	2.892	2.883	2.87
M	18	2.763	2.757	2.757	2.746	2.734	2.716	2.705	2.706	2.682	2.682	2.683	2.45
	$\begin{vmatrix} 19\\20 \end{vmatrix}$	2.936 2.583	$2.950 \\ 2.563$	$2.970 \\ 2.517$	$2.971 \\ 2.457$	2.976 2.423	2.378 2.378	2.968	2.955	2.939	2.921	2.916	2.90
	21						2 378	2.338	2.289	2.559	2.185	2.500	2.17
	22	$2.535 \\ 2.343$	2.231	2.507	2.522	2.20	2.514	2.504	2.494	2.492	2.485	2.483	2.48
	$\begin{bmatrix} 23 \\ 24 \end{bmatrix}$	2.545 $2.531$	2:341 2:553	2.337 $2.581$	2·294 2·601	2.274 2.610	2.273	2.279	2.272	2.276	2:297	2.301	2:32
	25	$\frac{2.001}{2.299}$	2.331	2.318	$\frac{2}{2} \cdot 329$	$\frac{2.010}{2.352}$	2.613 2.373	2.612 2.402	2.622 $2.445$	2.606 2.461	2.604	2.583 2.509	$\begin{vmatrix} 2.57 \\ 2.52 \end{vmatrix}$
	26	2.572	2.593	2.288	2.578	2.566	2.558	$\frac{2.702}{2.574}$	2.240	2.528	$\frac{2.481}{2.518}$	2.505	2.50
	$\begin{vmatrix} 27 \\ 28 \end{vmatrix}$	2.467	2.472	2.463	2.480	2.471	2.470	2.470	2.468	2.458	2.469	2.483	2.20
	29	2.148	2.138	2.109	2.112	2.135	2.158	2.208	2.247	2.297	2.332	2.370	2.43
	30	2.613	2.631	2.635	2.647	2.645	2.646	2.598	2.288	2.556	2.212	2.484	2.49
<del></del>	31	2.601	2.639	2.664	2.708	2.720	2.743	2.749	2.748	2.754	2.760	2.776	2.49
lourly	y Means	2.6676	2.6810	2.6861	2.6892	2.6890	2.6849	2.6828	2.6708	2.6620	2.6609	2.6603	2.66
	$\begin{pmatrix} 1\\ 2a \end{pmatrix}$	2.903	2.914	2.906	2.889	2.868	2.850	2.813	2.782	2.736	2.715	2.708	2.680
	3	2.269	2.288	2.602	2.616	2.614	2.605	2.606	2.596	2.596	2.281	2.574	2.569
	$\begin{vmatrix} 4 \\ 5 \end{vmatrix}$	2.745	$\frac{-}{2.743}$	$2.\overline{742}$	$2.\overline{778}$	2.783	2.784	$2.\overline{71}$	2.766	2.768	2.767	$2.\overline{741}$	2.730
	6	2.287	2.279	2.273	2.226	$\frac{2.213}{2}$	2.193	$\frac{5}{2} \cdot 174$	2.154	2.111	$\frac{2}{2} \cdot 073$	2.088	2.120
	7	2.507	2.531	2.569	2.601	2.619	2.643	2.646	2.648	2.645	2.627	2.628	2.648
		2.541 2.623	$2.575 \\ 2.659$	$2.525 \\ 2.709$	$2.463 \\ 2.707$	$2.427 \\ 2.696$	2:382	2.350	2.311	2.275	2.264	2.264	2:290
	8		- 000	~ (U3	2 101	2 090	2.684	2.684	2.670	2.654	2.616 2.458	$2.598 \\ 2.477$	$\frac{2.575}{2.513}$
	9 10	2.334	2.341	2.352	2.367				2.407	2.416			
	9 10 11	2.334		2.352		2:377	2.403 —	2.415 —	2.407	2.416			2:50
	9 10 11 12	2:334	2.301	2.352 $ 2.314$	2·357	$\frac{2.377}{2.386}$	2·403 	2.415 $ 2.453$	2.475	2.503	2.210	2.528 2.615	
	9 10 11 12 13 14	2:334 2:277 2:757 2:665		2·352 2·314 2·744 2·698		2·377 ———————————————————————————————————	2.403 	2.415 	2·475 2·677	2·503 2·646	2·510 2·627	2.615	2.60
III.	9 10 11 12 13 14 15	2:334 2:277 2:757 2:665 2:626	$ \begin{array}{c c}  & - \\  2.301 \\  2.747 \\  2.683 \\  2.632 \end{array} $	2:352 	2·357 2·760 2·700 2·646	2·377 — 2·386 2·757 2·707 2·668	2·403 — 2·419 2·733 2·703 2·663	2.415 2.453 2.705 2.680 2.664	2·475 2·677 2·664 2·669	2·503 2·646 2·622 2·661	2·510 2·627 2·598 2·661	2.615 2.561 2.661	2.60 2.56 2.67
PRIL.	9 10 11 12 13 14 15 16	2:334 	2:301 2:747 2:683 2:632 2:740	2:352 	2·357 2·760 2·700 2·646 2·729	2:377 	2·403 2·419 2·733 2·703 2·663 2·665	2.415 2.453 2.705 2.680 2.664 2.639	2·475 2·677 2·664 2·669 2·563	2:503 2:646 2:622 2:661 2:489	2:510 2:627 2:598 2:661 2:465	2.615 2.561 2.661 2.455	2.60 2.56 2.67 2.40
APRIL.	9 10 11 12 13 14 15 16 17 18	2:334 	2:301 2:747 2:683 2:632 2:740 2:452	2:352 	2·357 2·760 2·700 2·646 2·729 2·490	2:377 	2·403 — 2·419 2·733 2·703 2·663	2.415 2.453 2.705 2.680 2.664	2·475 2·677 2·664 2·669	2·503 2·646 2·622 2·661	2·510 2·627 2·598 2·661	2.615 2.561 2.661	2.60 2.56 2.67 2.40
APRIL.	9 10 11 12 13 14 15 16 17 18 19	2·334 	2:301 2:747 2:683 2:632 2:740 2:452 ————————————————————————————————————	2:352 	2:357 2:760 2:700 2:646 2:729 2:490 ————————————————————————————————————	2:377 	2·403 — 2·419 2·733 2·703 2·663 2·665 2·504 — 2·916	2 · 415 — 2 · 453 2 · 705 2 · 680 2 · 664 2 · 639 2 · 516 — 2 · 889	2·475 2·677 2·664 2·669 2·563 2·530 — 2·868	2:503 2:646 2:622 2:661 2:489 2:538	2·510 2·627 2·598 2·661 2·465 2·546 — 2·836	2.615 2.561 2.661 2.455 2.554 	2.60 2.56 2.67 2.40 2.57 2.82
APRIL.	9 10 11 12 13 14 15 16 17 18 19 20	2·334 2·277 2·757 2·665 2·626 2·740 2·424 — 2·978 2·838	2·301 2·747 2·683 2·632 2·740 2·452 — 2·972 2·837	2:352 	2:357 2:760 2:700 2:646 2:729 2:490 — 2:943 2:819	2:377 	2·403 — 2·419 2·733 2·703 2·663 2·665 2·504 — 2·916 2·805	2·415 	2:475 2:677 2:664 2:669 2:563 2:530 — 2:868 2:766	2:503 2:646 2:622 2:661 2:489 2:538 — 2:847 2:749	2:510 2:627 2:598 2:661 2:465 2:546 — 2:836 2:740	2.615 2.561 2.661 2.455 2.554 — 2.823 2.704	2 · 60 2 · 56 2 · 67 2 · 40 2 · 57 2 · 82 2 · 71
APRIL.	9 10 11 12 13 14 15 16 17 18 19 20 21 22	2·334 	2:301 2:747 2:683 2:632 2:740 2:452 ————————————————————————————————————	2:352 2:314 2:744 2:698 2:632 2:740 2:462 	2:357 2:760 2:700 2:646 2:729 2:490 ————————————————————————————————————	2:377 2:386 2:757 2:707 2:668 2:719 2:496 2:930 2:815 2:515	2:403 	2.415 2.453 2.705 2.680 2.664 2.639 2.516 2.889 2.760 2.484	2:475 2:677 2:664 2:669 2:563 2:563 2:868 2:766 2:486	2·503 2·646 2·622 2·661 2·489 2·538 2·847 2·749 2·482	2:510 2:627 2:598 2:661 2:465 2:546 — 2:836 2:740 2:499	2:615 2:561 2:661 2:455 2:554 ———————————————————————————————————	2 · 560 2 · 600 2 · 567 2 · 407 2 · 571 2 · 824 2 · 714 2 · 483 2 · 680
APRIL.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	2·334 2·277 2·757 2·665 2·626 2·740 2·424 2·978 2·838 2·530 2·574 2·860	2·301 2·747 2·683 2·632 2·740 2·452 2·972 2·837 2·540 2·592 2·884	2:352 	2·357 2·760 2·700 2·646 2·729 2·490 ————————————————————————————————————	2:377 2:386 2:757 2:707 2:668 2:719 2:496 2:930 2:815 2:515 2:641 2:934	2·403 — 2·419 2·733 2·703 2·663 2·665 2·504 — 2·916 2·805	2.415 	2:475 2:677 2:664 2:669 2:563 2:530 	2:503 2:646 2:622 2:661 2:489 2:538 — 2:847 2:749	2:510 2:627 2:598 2:661 2:465 2:546 — 2:836 2:740	2.615 2.561 2.661 2.455 2.554 — 2.823 2.704	2.60 2.56 2.67 2.40 2.57 2.82 2.71 2.48 2.68 2.94
APRIL.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	2·334 2·277 2·757 2·665 2·626 2·740 2·424 2·978 2·838 2·530 2·574	2·301 2·747 2·683 2·632 2·740 2·452 — 2·972 2·837 2·540 2·592	2:352 2:314 2:744 2:698 2:632 2:740 2:462 	2·357 2·760 2·700 2·646 2·729 2·490 2·943 2·819 2·546 2·632	2:377 2:386 2:757 2:707 2:668 2:719 2:496 2:930 2:815 2:515 2:641 2:934 3:029	2:403 	2·415 2·453 2·705 2·680 2·664 2·639 2·516 — 2·889 2·760 2·484 2·667 2·949 3·035	2:475 2:677 2:664 2:669 2:563 2:530 2:868 2:766 2:486 2:684	2:503 2:646 2:622 2:661 2:489 2:538 	2·510 2·627 2·598 2·661 2·465 2·546 2·546 2·740 2·499 2·682	2:615 2:561 2:661 2:455 2:554 — 2:823 2:704 2:478 2:694 2:945 2:989	2 · 60 · 2 · 56 · 2 · 67 · 2 · 40 · 2 · 57 · 2 · 82 · 2 · 71 · 2 · 48 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 2 · 68 · 68
APRIL.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	2·334 2·277 2·757 2·665 2·626 2·740 2·424 — 2·978 2·838 2·530 2·574 2·860 2·993 — 2·500	2 · 301 2 · 747 2 · 683 2 · 632 2 · 740 2 · 452 — 2 · 972 2 · 837 2 · 540 2 · 592 2 · 884 3 · 005 — 2 · 490	2·352 2·314 2·744 2·698 2·632 2·740 2·462 — 2·949 2·837 2·556 2·603 2·896 3·011 — 2·496	2·357 2·760 2·700 2·646 2·729 2·490 ————————————————————————————————————	2:377 2:386 2:757 2:707 2:668 2:719 2:496 2:930 2:815 2:515 2:641 2:934	2:403 	2·415 	2:475 2:677 2:664 2:669 2:563 2:530 	2:503 2:646 2:622 2:661 2:489 2:538 	2:510 2:627 2:598 2:661 2:465 2:546 	2:615 2:561 2:661 2:455 2:554 — 2:823 2:704 2:478 2:694 2:945	2:60 2:56 2:67: 2:40' 2:57. 2:82- 2:71- 2:48 2:68' 2:94' 2:98:
APRIL.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	2·334 2·277 2·757 2·665 2·626 2·740 2·424 — 2·978 2·838 2·530 2·574 2·860 2·993 — 2·500 2·155	2 · 301 2 · 747 2 · 683 2 · 632 2 · 740 2 · 452 — 2 · 972 2 · 887 2 · 592 2 · 884 3 · 005 — 2 · 490 2 · 190	2·352 2·314 2·744 2·698 2·632 2·740 2·462 — 2·949 2·837 2·556 2·603 2·896 3·011 — 2·496 2·240	2·357 2·760 2·700 2·646 2·729 2·490 2·943 2·819 2·546 2·632 2·919 3·026 2·490 2·306	2:377 2:386 2:757 2:707 2:668 2:719 2:496 2:930 2:815 2:515 2:641 2:934 3:029 2:481 2:352	2·403 2·419 2·733 2·703 2·663 2·665 2·504 — 2·916 2·805 2·501 2·653 2·944 3·033 — 2·466 2·382	2·415	2·475 2·677 2·664 2·669 2·563 2·530 2·868 2·766 2·486 2·486 3·038 2·440 2·413	2:503 2:646 2:622 2:661 2:489 2:538 2:847 2:749 2:482 2:684 2:945 3:022 2:413 2:425	2:510 2:627 2:598 2:661 2:465 2:546 2:546 2:499 2:682 2:938 3:006 2:407 2:449	2:615 2:561 2:661 2:455 2:554 ———————————————————————————————————	2 · 60 2 · 56 2 · 67; 2 · 40' 2 · 57 2 · 82· 2 · 71- 2 · 48; 2 · 68' 2 · 94' 2 · 98; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2 · 40; 2
APRIL.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	2·334 2·277 2·757 2·665 2·626 2·740 2·424 — 2·978 2·978 2·530 2·574 2·860 2·993 — 2·500 2·155 2·608	2·301 2·747 2·683 2·632 2·740 2·452 ————————————————————————————————————	2·352 2·314 2·744 2·698 2·632 2·740 2·462 — 2·949 2·837 2·556 2·603 2·896 3·011 — 2·496 2·240 2·653	2·357 2·760 2·700 2·646 2·729 2·490 2·943 2·819 2·546 2·632 2·919 3·026 2·490 2·306 2·633	2:377 2:386 2:757 2:707 2:668 2:719 2:496 2:930 2:815 2:641 2:934 3:029 2:481 2:352 2:629	2·403 2·419 2·733 2·703 2·663 2·665 2·504 — 2·916 2·805 2·501 2·653 2·944 3·033 — 2·466 2·382 2·603	2·415	2·475 2·677 2·664 2·669 2·563 2·530 2·868 2·766 2·486 2·684 2·956 3·038 2·440 2·413 2·519	2:503 2:646 2:622 2:661 2:489 2:538 2:847 2:749 2:482 2:684 2:945 3:022 2:413 2:425 2:483	2:510 2:627 2:598 2:661 2:465 2:546 2:740 2:499 2:499 2:682 2:938 3:006 2:407 2:449 2:449	2:615 2:561 2:661 2:455 2:554 ———————————————————————————————————	2 · 60 2 · 56 2 · 67 2 · 40 2 · 57 2 · 82 2 · 71 2 · 48 2 · 68 2 · 98 2 · 98 2 · 40 2 · 47 2 · 36
APRIL.	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	2·334 2·277 2·757 2·665 2·626 2·740 2·424 — 2·978 2·838 2·530 2·574 2·860 2·993 — 2·500 2·155	2 · 301 2 · 747 2 · 683 2 · 632 2 · 740 2 · 452 — 2 · 972 2 · 887 2 · 592 2 · 884 3 · 005 — 2 · 490 2 · 190	2·352 2·314 2·744 2·698 2·632 2·740 2·462 — 2·949 2·837 2·556 2·603 2·896 3·011 — 2·496 2·240	2·357 2·760 2·700 2·646 2·729 2·490 2·943 2·819 2·546 2·632 2·919 3·026 2·490 2·306	2:377 2:386 2:757 2:707 2:668 2:719 2:496 2:930 2:815 2:515 2:641 2:934 3:029 2:481 2:352	2·403 2·419 2·733 2·703 2·663 2·665 2·504 — 2·916 2·805 2·501 2·653 2·944 3·033 — 2·466 2·382	2·415	2·475 2·677 2·664 2·669 2·563 2·530 2·868 2·766 2·486 2·486 3·038 2·440 2·413	2:503 2:646 2:622 2:661 2:489 2:538 2:847 2:749 2:482 2:684 2:945 3:022 2:413 2:425	2:510 2:627 2:598 2:661 2:465 2:546 2:546 2:499 2:682 2:938 3:006 2:407 2:449	2:615 2:561 2:661 2:455 2:554 ———————————————————————————————————	2:60 2:56 2:67: 2:40 2:57 2:82: 2:71: 2:48 2:68' 2:94' 2:98: 2:40: 2:47

				Bar	rometer at 3	BARO1 $2^{\circ} = 27 \text{ E}_{1}$	METRIC P	RESSURE s + the nur	mbers in the	Table.			
ľ	12	13	14	15	16	17	18	19 .	20	21	22	23	Daily and
	6	7	8	9	10	11	12	13	14	15	16	17	Monthly Means.
	In. 2·557 2·761 2·591 2·829 3·013 2·890	In. 2:575 2:758 2:607 2:829 3:010 2:867	In. 2.579 2.764 2.607 2.838 2.996 2.832	In. 2.579 2.780 2.591 2.867 3.016 2.798	In. 2.579 2.788 2.591 2.888 3.010 2.763	In. 2:599 2:778 2:621 2:893 3:011 2:747	In. 2.615 2.776 2.614 2.893 3.015	In. 2.629 2.768 2.625 2.920 3.013	In. 2.678 2.768 2.632 2.919 3.014	In. 2:700 2:750 2:630 2:934 3:010	In. 2·704 2·748 2·624 2·941 3·014	In. 2:745 2:742 2:693 2:946 3:041	In. 2:5397 2:7761 2:6407 2:8368 3:0138
	2.866 2.815 2.706 2.782 2.641 2.676	2.887 2.756 2.719 2.780 2.611 2.672	2·908 2·712 2·744 2·775 2·633 2·679	2.967 2.694 2.810 2.768 2.607 2.694	2.964 2.672 2.830 2.756 2.601 2.704	2 · 967 2 · 666 2 · 843 2 · 747 2 · 596 2 · 705	2:532 2:963 2:642 2:850 2:742 2:593	2.558 2.988 2.637 2.884 2.742 2.608	2:569 2:964 2:635 2:892 2:741 2:621	2.587 2.965 2.629 2.886 2.732 2.621	2.616 2.970 2.655 2.894 2.731 2.646	2.641 2.981 2.655 2.898 2.730 2.680	2 · 8570 2 · 8683 2 · 8054 2 · 7559 2 · 8033 2 · 6704 2 · 6973
	2.716 2.829 2.867 2.767 2.896 2.151	2.732 2.851 2.875 2.802 2.884 2.147	2.740 2.886 2.881 2.819 2.849 2.196	2.733 2.899 2.877 2.817 2.829 2.246	2.731 2.907 2.865 2.831 2.813 2.272	2.722 2.914 2.851 2.839 2.809 2.316	2.658 2.706 2.932 2.829 2.841 2.780	2.684 2.709 2.943 2.817 2.844 2.726	2:691 2:699 2:951 2:785 2:879 2:689	2.705 2.689 2.951 2.781 2.886 2.651	2.711 2.701 2.957 2.771 2.910 2.615	2.736 } 2.705 2.960 2.765 2.937 2.581	2 · 7247 2 · 8363 2 · 8934 2 · 7845 2 · 8545 2 · 3751
	2·497 2·331 2·561 2·551 2·500 2·517	2·480 2·353 2·561 2·562 2·504 2·531	2·482 2·355 2·565 2·562 2·511 2·551	2·482 2·371 2·551 2·583 2·493 2·577	2.480 2.394 2.520 2.578 2.498 2.593	2:476 2:424 2:500 2:571 2:484 2:586	2.604 2.456 2.437 2.454 2.569 2.468	2:580 2:436 2:438 2:412 2:553 2:459	2:563 2:410 2:434 2:357 2:563 2:424	2:543 2:392 2:446 2:284 2:543 2:432	2:531 2:383 2:465 2:272 2:576 2:436	2·523 }   2·523 }   2·355   2·481   2·278   2·590   2·441	2:4751 2:3557 2:5170 2:4845 2:5113
-	2·465 2·493 2·820	2·517 2·437 2·818	2·546 2·449 2·812	2·579 2·426 2·849	2·591 2·422 2·855	2.603 2.429 2.871	2:441 2:605 2:424 2:881	2:391 2:606 2:426 2:854	2:335 2:591 2:470 2:858	2:275 2:594 2:501 2:877	2:230 2:588 2:517 2:891	$\left\{ \begin{array}{c} -143 \\ 2.143 \\ 2.589 \\ 2.569 \\ 2.897 \end{array} \right\}$	2.4517 2.3985 2.5257 2.7891
-	2.6699	2.6713	2.6767	2.6846	2.6850	2.6877	2.6785	2.6759	2.6716	2.6664	2.6703	2.6779	2.6756
- 1	2.670 2.575	2.633	2.617	2.553	2.217	2.483	2.525	2.525	2.529	2.533	$\frac{-}{2.529}$	$\left\{ \frac{1}{2\cdot 549}\right\}$	2.6845
	2·708 2·170 2·661 2·314 2·546 2·539	2.571 2.666 2.222 2.660 2.346 2.504 2.547	2.595 2.667 2.273 2.656 2.375 2.507 2.590	2·572 2·635 2·305 2·664 2·396 2·493 2·611	2.565 2.617 2.326 2.665 2.401 2.466 2.626	2.561 2.560 2.338 2.660 2.439 2.446 2.627	2·707 2·520 2·352 2·633 2·458 2·421	2.707 2.497 2.368 2.634 2.471 2.385	2.711 2.409 2.381 2.601 2.493 2.350	2.690 2.391 2.411 2.579 2.509 2.321	2.672 2.335 2.441 2.595 2.529 2.309	$ \begin{array}{c}  - \\  2 \cdot 709 \\  2 \cdot 313 \\  2 \cdot 463 \\  2 \cdot 565 \\  2 \cdot 537 \\  2 \cdot 312 \\  - \\  2 \cdot 289 \end{array} $	2 · 6146 2 · 6432 2 · 2600 2 · 6202 2 · 4140 2 · 5388 2 · 4412
	2.606 2.600 2.561 2.691 2.389 2.591	2.619 2.590 2.547 2.703 2.371 2.621	2.646 2.596 2.565 2.719 2.369 2.660	2.675 2.596 2.568 2.721 2.351 2.674	2.675 2.580 2.574 2.722 2.375 2.711	2.675 2.592 2.569 2.723 2.367 2.712	2:477 2:707 2:572 2:575 2:724 2:361	2:433 2:718 2:561 2:579 2:726 2:361	2:368 2:716 2:587 2:603 2:724 2:377	2:321 2:716 2:633 2:601 2:725 2:365	2:301 2:716 2:637 2:589 2:723 2:371	2.731 2.639 2.580 2.726 2.409	2·5537 2·6480 2·6147 2·6867 2·4924
	2.841 2.714 2.492 2.688 2.949 2.988	2.836 2.680 2.509 2.703 2.964 2.976	2.856 2.673 2.510 2.705 2.972 2.976	2.870 2.649 2.522 2.704 2.984 2.989	2.852 2.628 2.522 2.709 2.970 2.978	2.862 2.578 2.524 2.712 2.979 2.984	3.003 2.860 2.566 2.544 2.738 2.983	3.003 2.856 2.510 2.542 2.749 2.987	3:005 2:838 2:500 2:540 2:761 2:985	3.001 2.836 2.516 2.518 2.784 2.980	2.991 2.818 2.516 2.534 2.795 2.981	2·979} 2·824 2·516 2·542 2·841 2·980	2.6681 2.8718 2.6846 2.5165 2.6951 2.9513
	2·382 2·507 2·349 2·186 2·500	2 · 348 2 · 520 2 · 352 2 · 218 2 · 529	2·330 2·539 2·313 2·258 2·563	2 · 268 2 · 268 2 · 524 2 · 275 2 · 272 2 · 593	2 978 2 225 2 523 2 260 2 272 2 607	2 · 158 2 · 158 2 · 531 2 · 273 2 · 265 2 · 603	2.573 2.096 2.535 2.264 2.259 2.619	2.543 2.066 2.539 2.216 2.265 2.647	2·515 2·057 2·542 2·197 2·275 2·629	2·499 2·086 2·547 2·178 2·283 2·617	2·490 2·083 2·563 2·152 2·277 2·621	2·475 } 2·129 2·582 2·146 2·309 2·630	2.8819 2.3196 2.4458 2.3968 2.1952 2.4893
	2.5687	2.5694	2.2815	2.5786	2.5746	2.5688	2.5629	2.5555	2.2477	2.5456	2.5427	2.5510	2.5731

Vol. III.

				Barome	eter at 32° =		TRIC PRES		rs in the Ta	ble.			_
Hours ( Götti Ti	of Mean {	0	1	2	3	4	5	6	7	8	9	10	11
Hours	of Mean )	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \end{pmatrix}$	In. 2.636	In. 2.658	In. 2.660	2·670	In. 2.677	2.698	In. 2.665	2.648	In. 2.641	In. 2.641	In. 2.615	In. 2.606
	3 4 5 6 7 8	2.616 2.906 2.953 2.852 2.515 2.140	2.617 2.917 2.959 2.863 2.509 2.148	2.620 2.916 2.966 2.860 2.499 2.138	2.643 2.920 2.965 2.835 2.465 2.140	2.654 2.933 2.970 2.818 2.452 2.138	2.662 2.907 2.959 2.802 2.431 2.137	2.691 2.903 2.942 2.774 2.396 2.139	2.697 2.870 2.925 2.745 2.364 2.149	2·705 2·861 2·894 2·722 2·331 2·156	2·723 2·847 2·875 2·701 2·313 2·154	2·745 2·847 2·859 2·699 2·288 2·168	2.750 2.847 2.848 2.679 2.286 2.153
Ţ.	10 11 12 13 14 15	2.622 2.526 2.405 2.648 2.714 2.760	2.636 2.538 2.413 2.667 2.732 2.767	2.641 2.530 2.407 2.684 2.752 2.779	2.641 2.506 2.412 2.699 2.760 2.778	2:649 2:505 2:419 2:714 2:763 2:776	2.641 2.497 2.419 2.712 2.772 2.770	2.631 2.487 2.415 2.706 2.778 2.761	2·592 2·481 2·416 2·702 2·761 2·748	2.567 2.468 2.418 2.687 2.757 2.735	2.549 2.458 2.432 2.673 2.743 2.716	2·542 2·445 2·432 2·673 2·737 2·711	2:545 2:435 2:436 2:691 2:727 2:707
MAY	16 17 18 19 20 21 22 23	2:537 2:479 2:519 2:683 2:586 2:285	2:545 2:483 2:523 2:696 2:590 2:287	2:541 2:487 2:533 2:702 2:554 2:294	2·538 2·474 2·544 2·716 2·538 2·314	2·534 2·484 2·559 2·718 2·536 2·331	2·532 2·484 2·565 2·709 2·520 2·337	2·525 2·475 2·570 2·706 2·509 2·341	2·511 2·460 2·566 2·725 2·451 2·365	2:489 2:445 2:555 2:689 2:418 2:376	2.480 2.432 2.566 2.681 2.388 2.373	2·472 2·424 2·563 2·673 2·355 2·387	2.462 2.426 2.561 2.648 2.353 2.384
	23 24 25 26 27 28 29 30	2:543 2:490 2:694 2:826 2:751 2:591	2.559 2.481 2.713 2.814 2.773 2.584	2·555 2·466 2·745 2·825 2·763 2·580	2·563 2·454 2·757 2·824 2·723 2·548	2·553 2·440 2·773 2·812 2·718 2·524	2.549 2.423 2.773 2.809 2.704 2.510	2·543 2·397 2·772 2·778 2·681 2·521	2·514 2·342 2·784 2·755 2·660 2·483	2:516 2:348 2:780 2:743 2:658 2:497	2:501 2:348 2:758 2:730 2:641 2:462	2·495 2·333 2·758 2·723 2·632 2·463	2·499 2·322 2·732 2·712 2·624 2·472
	31	2.247	2.24	2.263	2.248	2.252	2.242	2.241	2.235	2.222	2.218	2.212	2.222
Hourl	y Me <b>a</b> ns	2.6086	2.6160	2.6177	2.6144	2.6155	2.6103	2.6018	2.2862	2.5762	2.5655	2.5597	2.5550
	$\left(\begin{array}{c}1\\2\\3\\4\\5\end{array}\right)$	2.463 2.580 2.607 2.358 2.665	2.468 2.620 2.621 2.354 2.686	2:487 2:644 2:621 2:360 2:700	2:461 2:678 2:580 2:374 2:702	2:466 2:679 2:566 2:390 2:701	2.457 2.678 2.563 2.399 2.694	2:464 2:691 2:530 2:415 2:678	2:448 2:666 2:505 2:433 2:681	2:436 2:678 2:495 2:447 2:679	2:457 2:672 2:469 2:473 2:685	2:447 2:676 2:460 2:515 2:697	2.435 2.643 2.434 2.539 2.697
	6 7 8 9 10 11 12 13	2.798 2.690 2.517 2.320 2.135 2.455	2.802 2.698 2.501 2.318 2.133 2.467	2.799 2.690 2.505 2.298 2.133 2.472	2.819 2.672 2.492 2.294 2.137 2.474	2.814 2.692 2.527 2.284 2.126 2.480	2.808 2.663 2.466 2.284 2.111 2.492	2.783 2.668 2.449 2.280 2.129 2.480	2.764 2.659 2.432 2.257 2.115 2.451	2.731 2.651 2.422 2.250 2.157 2.434	2·741 2·643 2·371 2·231 2·149 2·413	2.718 2.630 2.375 2.211 2.168 2.399	2.691 2.636 2.356 2.207 2.191 2.392
JUNE.	14 15 16 17 18 19 20	2.021 2.358 2.651 2.858 2.800 2.441	2:020 2:373 2:658 2:872 2:788 2:433	2.060 2.379 2.658 2.875 2.778 2.403	2·072 2·401 2·657 2·876 2·774 2·385	2.097 2.423 2.658 2.881 2.751 2.372	2·125 2·450 2·671 2·883 2·741 2·364	2:163 2:463 2:689 2:871 2:710 2:371	2·195 2·474 2·699 2·882 2·663 2·395	2·238 2·474 2·698 2·876 2·632 2·427	2·254 2·480 2·711 2·880 2·604 2·434	2·276 2·485 2·713 2·868 2·584 2·438	2·292 2·502 2·713 2·839 2·565 2·431
	20 21 22 23 24 25 26 27	2.538 2.611 2.741 2.844 2.761 2.695	2.545 2.618 2.757 2.862 2.771 2.701	2·549 2·632 2·772 2·869 2·777 2·715	2:547 2:644 2:772 2:862 2:764 2:712	2:542 2:651 2:770 2:849 2:762 2:704	2:541 2:647 2:769 2:844 2:760 2:691	2:534 2:638 2:761 2:831 2:749 2:681	2·522 2·636 2·749 2·827 2·726 2·663	2:526 2:629 2:737 2:817 2:707 2:650	2·522 2·635 2·730 2·804 2·680 2·638	2·521 2·647 2·722 2·794 2·665 2·627	2:511 2:641 2:723 2:778 2:657 2:613
	28 29 30	2.628 2.593 2.659	2.636 2.596 2.673	2.644 2.598 2.681	2.639 2.583 2.696	2.633 2.584 2.691	2.646 2.577 2.690	2.634 2.573 2.683	2.616 2.577 2.676	2.603 2.564 2.658	2·585 2·564 2·652	2·567 2·556 2·641	2.563 2.559 2.639
Hourl	y Means	2.5694	2.5758	2.5807	2.5795	2.5805	2.5775	2.5738	2.5658	2.5622	2.5568	2.5538	2.5480

			Bar	rometer at 3			RESSURE s + the nu		Table.			
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
In. 2.604	In. 2.591	In. 2.581	In. 2.621	In. 2.633	In. 2.618	In.	In.	In.	In.	In.	In.	In.
2.762 2.849	2·774 2·835	2·800 2·843	2.810 2.853	2·822 2·856	$\begin{bmatrix} -1 \\ 2.831 \\ 2.866 \end{bmatrix}$	2.569 2.833 2.873	2.559 2.830 2.874	2:553 2:842 2:878	21561 21846 21894	2:570 2:861 2:900	2.602 } 2.867 2.937	2.6199 2.7500 2.8805
2.832 2.663 2.268 2.179	2.821 2.639 2.263 2.185	2·830 2·627 2·266 2·216	2.838 2.634 2.248 2.234	2.839 2.632 2.238 2.255	2 · 840 2 · 600 2 · 223 2 · 277	2·840 2·599 2·201	2.838 2.570 2.177	2.831 2.550 2.137	2.831 2.535 2.105	2 · 835 2 · 526 2 · 129	2.831 2.523 2.099	2:8800 2:6853 2:3001
2.525 2.431	2.525 2.425	2·534 2·426	2.548 2.428	$\frac{2.545}{2.418}$	$\begin{bmatrix} 2 & 217 \\ -2 & 547 \\ 2 & 413 \end{bmatrix}$	2:571 2:548 2:409	2.576 2.504 2.411	2:568 2:498 2:419	2:569 2:480 2:429	2·579 2·488 2·423	$\left\{ egin{array}{c}$	2.2739 2.5630 2.4543
2.460 2.689 2.725	2.467 2.699 2.727	2:479 2:691 2:737	2:494 2:679 2:727	2.530 2.684 2.727 2.722	2:534 2:692 2:721	2.554 $2.681$ $2.725$	$     \begin{array}{r}       2 \cdot 411 \\       2 \cdot 557 \\       2 \cdot 665 \\       2 \cdot 721     \end{array} $	2:565 2:663 2:714	2 · 429 2 · 580 2 · 670 2 · 722	2 · 600 2 · 675 2 · 731	2.624 $2.703$ $2.743$	2 · 4778 2 · 6853 2 · 7382
$ \begin{array}{c c} 2.702 \\ - \\ 2.454 \\ 2.425 \end{array} $	2.699 	$ \begin{array}{r} 2.687 \\ \\ 2.441 \\ 2.437 \end{array} $	2.410 2.440 2.464	$     \begin{array}{c}       2 & 422 \\       \hline       2 & 442 \\       2 & 468     \end{array} $	2.728  2.447 2.460	2·526 2·451 2·466	2.513 2.454 2.461	2:508 2:453 2:468	2.516 $2.456$ $2.477$	2·524 2·456 2·484	$\left\{ egin{array}{c}$	2.6824 2.4820 2.4618
2:571 2:644 2:331	2:573 2:636 2:363	2.581 2.641 2.372	2.589 2.633 2.371	2:593 2:625 2:364	$ \begin{array}{c c} 2.610 \\ 2.627 \\ 2.322 \end{array} $	2.616 2.596 2.298	2.615 2.597 2.246	2.621 2.590 2.233	2.624 2.582 2.233	2.632 2.587 2.235	2.640 2.583 2.269	• 2:5787 2:6536 2:3931
2·404 2·509 2·327	$ \begin{array}{c c} 2.442 \\ \\ 2.491 \\ 2.336 \end{array} $	2.461  2.501 2.366	2.498 	2·494 — 2·503 2·396	2.498  2.489 2.471	2.567 $2.497$ $2.514$	$\begin{bmatrix}$	2·543 2·494 2·576	2·539 2·491 2·609	2:543 2:482 2:626	$\left. \begin{array}{c} - \\ 2 \cdot 542 \\ 2 \cdot 492 \\ 2 \cdot 672 \end{array} \right\}$	2.4232 2.5149 2.4433
2.746 2.712 2.624	2.750 2.722 2.638	2.758 2.719 2.654	2.748 2.737 2.664	2.757 $2.744$ $2.682$	2.759 2.740 2.688	$ \begin{array}{c} 2.760 \\ 2.737 \\ 2.624 \end{array} $	$   \begin{array}{c}     \hline     2.763 \\     2.725 \\     2.638   \end{array} $	2.761 2.718 2.624	2.762 2.720 2.639	$   \begin{array}{c}     2.782 \\     2.721 \\     2.621   \end{array} $	2·828 2·738 2·613	2.7589 2.7539 2.6682
2.218 2.222	2.240 - 2.211	2·560 2·511	2.582	2.622 - 2.481	2.638  2.469	2.673 2.451	2.631 2.411	2·599 2·445	2·599 2·413	2·570 2·403	2·540 } 2·400	2·5545 2·4984
2.5569	2.5588	2.2661	2.5745	2.5797	2.2811	2.2838	2.5736	2.5712	2.5724	2.5763	2.5865	2.5837
2:427 2:644 2:424 2:559 2:743	2:425 2:628 2:424 2:559 2:749	2.431 2.636 2.393 2.573 2.753	2:439 2:637 2:381 2:617 2:740	2:447 2:631 2:367 2:620 2:746	2:459 2:635 2:362 2:630 2:751	2:475 2:637 2:338 2:621	2:489 2:594 2:344 2:607	2·493 2·582 2·341 2·616	2:512 2:584 2:334 2:615	2:526 2:580 2:338 2:630	2:580 2:609 2:328 2:642	2:4663 2:6376 2:4510 2:5144 2:7204
2.675 2.592 2.363 2.187 2.227	2.657 2.588 2.355 2.177 2.252	2.673 2.589 2.363 2.179 2.266	2.672 2.591 2.393 2.165 2.287	2.672 2.593 2.385 2.166 2.297	2.664 2.573 2.393 2.163 2.318	2.733 2.655 2.561 2.391 2.151 2.327	2.734 2.670 2.548 2.355 2.152 2.344	2.754 2.667 2.540 2.339 2.122 2.358	2.754 2.667 2.532 2.332 2.115 2.378	2.769 2.667 2.523 2.324 2.127 2.389	2·798 } 2·695 2·497 2·317 2·129 2·441	2 7204 2 7209 2 6133 2 4051 2 2111 2 2320
2:380 2:315 2:510 2:729 2:828	2·381 2·327 2·534 2·733 2·822	2·368 	2:376 	2:386 	2:386 2:356 2:591 2:787 2:796	2*042 2*342 2*606 2*801 2*804	2.036 2.340 2.604 2.792 2.803	2.018 2.338 2.624 2.796 2.813	2.020 2.332 2.625 2.811 2.817	2.010 2.341 2.633 2.830 2.798	$ \begin{vmatrix}  - \\  2.021 \end{vmatrix} $ $ \begin{vmatrix}  2.355 \\  2.645 \\  2.842 \\  2.798 \end{vmatrix} $	2·3264 2·2459 2·5141 2·7332 2·8419
2.527 2.425 2.501	2.520 2.476 — 2.501	2.500 2.486  2.501	2.492 2.512 — 2.545	2.487 2.512 — 2.556	2.486 2.525 — 2.562	2:484  2:528 2:532	2.455 	2:437 — 2:501 2:536	2.427 	2.427 	$\left\{ egin{array}{c} 2.432 \\ \\ 2.526 \\ 2.587 \end{array} \right\}$	2.5860 2.4545 2.5361
2.638 2.722 2.765 2.657 2.609	2.647 2.736 2.753 2.643 2.610	2.669 2.733 2.754 2.646 2.616	2.677 2.753 2.756 2.660 2.630	2.667 2.765 2.759 2.669 2.643	2.682 2.777 2.769 2.658 2.649	2.682 2.775 2.757 2.658	2.678 2.776 2.753 2.647	2.678 2.789 2.746 2.641	2.685 2.793 2.754 2.645	2.706 2.809 2.759 2.643	2.733 2.824 2.751 2.669	2.6571 2.7606 2.7940 2.6923
2.565 2.567 2.643	2.568 2.563 2.647	2.577 2.570 2.649	2 · 573 2 · 588 2 · 656	2 · 574 2 · 578 2 · 666	2 · 570 2 · 601 2 · 671	2·594 2·570 2·596 2·677	2:597 2:570 2:595 2:695	2:597 2:571 2:596 2:702	2:591 2:567 2:606 2:701	2:598 2:567 2:618 2:708	$\left\{ \begin{array}{c} - \\ 2.605 \\ 2.579 \\ 2.641 \\ 2.721 \end{array} \right\}$	2.6429 2.5935 2.5860 2.6740
2.5470	2.5490	2.5533	2.5640	2.5667	2.5698	2.5514	2.5469	2.5460	2.5483	2.5534	2.5679	2.5619

				Baron	neter at 32°		TRIC PRE	SSURE.	ers in the T	able.			
Hours of Göttir Tim	f Mean	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean )	18	19	20	21	22	23	0	1	2	3	4	5
	$\left( egin{array}{c c} 1 & 2 & \\ 3 & 4 & \end{array} \right)$	In. 2·732 2·782 2·775	In. 2·745 2·795 2·797	In. 2.751 2.795 2.804	In. 2.759 2.809 2.808	In. 2.760 2.816 2.797	In. 2.767 2.817 2.791	In. 2.762 2.803 2.780	In. 2.758 2.791 2.763	In. 2.746 2.778 2.753	In. 2.737 2.763 2.740	In. 2·726 2·763 2·729	In. 2.713 2.750 2.723
	5 6 7 8 9	2.735 2.725 2.756 2.665 2.661 2.558	2.743 2.737 2.762 2.681 2.661 2.565	2.743 2.765 2.761 2.688 2.660 2.574	2·742 2·787 2·761 2·691 2·663 2·583	2.740 2.763 2.764 2.690 2.656 2.581	2.737 2.756 2.751 2.671 2.647 2.584	2.727 2.752 2.743 2.665 2.633 2.576	2.711 2.751 2.739 2.651 2.622 2.551	2.692 2.746 2.722 2.643 2.614 2.541	2.679 2.730 2.701 2.621 2.592 2.527	2.693 2.716 2.693 2.611 2.590 2.524	2.689 2.700 2.681 2.606 2.580 2.506
JULY.	$egin{array}{c c} 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ \end{array}$	2:549 2:528 2:685 2:593 2:604 2:617	2:553 2:526 2:689 2:607 2:612 2:615	2.558 2.540 2.702 2.611 2.609 2.615	2.572 2.530 2.701 2.607 2.611 2.618	2:565 2:526 2:693 2:600 2:629 2:605	2:572 2:517 2:681 2:593 2:610 2:611	2.566 2.514 2.667 2.588 2.595 2.601	2.557 2.494 2.665 2.567 2.594 2.596	2.533 2.505 2.669 2.548 2.588 2.579	2:518 2:506 2:663 2:530 2:574 2:610	2.510 2.516 2.643 2.536 2.571 2.599	2:499 2:527 2:617 2:528 2:579 2:611
	18 19 20 21 22 23 24	2.678 2.605 2.538 2.507 2.847 2.837	2.682 2.607 2.534 2.526 2.871 2.834	2.681 2.622 2.536 2.550 2.879 2.839	2.677 2.619 2.528 2.572 2.881 2.829	2.641 2.615 2.524 2.576 2.882 2.839	2.644 2.603 2.495 2.594 2.886 2.822	2.638 2.603 2.477 2.599 2.885 2.802	2.623 2.577 2.465 2.610 2.881 2.786	2.607 2.567 2.445 2.608 2.863 2.772	2.588 2.545 2.415 2.605 2.853 2.733	2.585 2.545 2.406 2.607 2.835 2.717	2:576 2:537 2:426 2:619 2:812 2:705
Aug	25 26 27 28 29 30 31 g. 1	2:439 2:777 2:765 2:578 2:482 2:486	2:469 2:797 2:761 2:574 2:486 2:496	2.518 2.809 2.762 2.564 2.492 2.490	2.513 2.834 2.757 2.555 2.491 2.497	2:554 2:832 2:757 2:534 2:506 2:484	2.601 2.828 2.734 2.511 2.496 2.484	2.617 2.832 2.728 2.507 2.485 2.476	2.613 2.817 2.709 2.483 2.482 2.463	2.621 2.807 2.691 2.454 2.478 2.463	2.623 2.799 2.670 2.442 2.462 2.477	2.621 2.783 2.661 2.443 2.458 2.483	2.629 2.785 2.649 2.423 2.453 2.459
Hourly	y Means	2.6483	2.6565	2.6636	2.6665	2.6640	2.6594	2.6526	2.6414	2.6309	2.6186	2.6135	2.6082
	$\left( \begin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{array} \right)$	2.732 2.799 2.726 2.485 2.293 2.497	2.740 2.801 2.715 2.484 2.302 2.523	2.760 2.799 2.715 2.477 2.314 2.542	2.777 2.805 2.713 2.479 2.316 2.547	2.785 2.810 2.711 2.495 2.317 2.551	2:778 2:794 2:698 2:449 2:319 2:540	2:775 2:777 2:672 2:433 2:320 2:540	2.750 2.773 2.666 2.409 2.328 2.544	2.746 2.760 2.643 2.393 2.328 2.543	2.731 2.757 2.625 2.368 2.315 2.534	2.747 2.752 2.603 2.355 2.338 2.540	2.742 2.751 2.593 2.329 2.333 2.550
	8 9 10 11 12 13 14	2.762 2.810 2.747 2.768 2.714 2.575	2.796 2.816 2.751 2.780 2.724 2.583	2.796 2.826 2.752 2.792 2.717 2.583	2·798 2·838 2·765 2·792 2·703 2·600	2:809 2:835 2:761 2:793 2:700 2:591	2.809 2.821 2.762 2.788 2.697 2.592	2.799 2.812 2.753 2.763 2.674 2.583	2.796 2.801 2.759 2.763 2.658 2.576	2.789 2.777 2.753 2.734 2.640 2.572	2.783 2.761 2.739 2.741 2.624 2.560	2·780 2·767 2·721 2·713 2·610 2·549	2·783 2·753 2·736 2·701 2·606 2·570
AUGUST	15 16 17 18 19 20 21 22	2.581 2.458 2.431 2.558 2.534 2.555	2·579 2·454 2·445 2·560 2·534 2·559	2.582 2.454 2.447 2.577 2.526 2.564	2:591 2:437 2:455 2:559 2:523 2:569	2:602 2:445 2:457 2:556 2:521 2:574	2·596 2·428 2·460 2·540 2·494 2·574	2.595 2.364 2.464 2.532 2.468 2.562	2:583 2:395 2:471 2:526 2:460 2:562	2·572 2·363 2·465 2·518 2·447 2·556	2·572 2·344 2·469 2·517 2·439 2·549	2:536 2:362 2:496 2:521 2:458 2:554	2.520 2.343 2.520 2.524 2.483 2.559
	22 23. 24 25 26 27 28 29	2·788 2·867 2·929 2·757 2·575 2·658	2·795 2·872 2·929 2·747 2·591 2·666	2.800 2.883 2.953 2.733 2.593 2.665	2·812 2·899 2·946 2·717 2·617 2·672	2.818 2.907 2.941 2.716 2.631 2.667	2.813 2.902 2.941 2.679 2.639 2.663	2·801 2·895 2·924 2·662 2·627 2·653	2·797 2·891 2·910 2·646 2·633 2·647	2·771 2·880 2·915 2·616 2·622 2·630	2·773 2·878 2·891 2·593 2·620 2·618	2.770 2.874 2.869 2.581 2.613 2.608	2.758 2.871 2.863 2.558 2.610 2.610
	30 31	2.682 2.765	2·674 2·789	2.664 2.801	2.655 2.814	2.640 2.824	2.629 2.816	2.612 2.800	2.603 2.788	$2.\overline{585} \\ 2.784$	2·583 2·765	2.567 2.755	2:591 2:753
Hourl	y Means	2.6556	2.6619	2.6660	2.6692	2.6714	2.6623	2.6485	2.6437	2.6308	2.6212	2.6169	2.6158

1						BARO	METRIC P	RESSURE					
				Bar	ometer at 3			s + the nu		Table.			
	12	13	14	15	16	17	18	19	20	21	22	23	Daily and
İ	6	7	8	9	10	11	12	13	14	15	16	17	Monthly Means.
	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
-	2.717 2.746	$2.711 \\ 2.740$	$\begin{vmatrix} 2.711 \\ 2.749 \end{vmatrix}$	$\begin{vmatrix} 2.743 \\ 2.745 \end{vmatrix}$	$2.753 \\ 2.746$	$2.760 \\ 2.752$	$2.760 \\ 2.747$	$2.749 \\ 2.741$	$2.745 \\ 2.751$	$\frac{2.745}{2.760}$	$\frac{2.753}{2.770}$	$\begin{vmatrix} 2.771 \\ 2.775 \end{vmatrix}$	$2.7447 \\ 2.7702$
	2.717	2.697	2.700	2.707	2.709	2.720						$2.\overline{731}$	2.7366
	2.687	2.686	2.696	2.708	2.710	2.700	$2.686 \\ 2.702$	$2.685 \\ 2.715$	$\frac{2.685}{2.717}$	2.691 2.712	$\frac{2.692}{2.708}$	$\frac{2.731}{2.706}$	2.7116
	2.714	2.728	2.717	2.733	2.735	2.729	2.729	2.727	2.725	2.727	2.723	2.728	2.7350
- }	2.681 2.596	2.665 2.600	2.667 2.603	2.680 2.605	2.674 2.598	$2.671 \\ 2.599$	2.661 2.602	$\frac{2.649}{2.608}$	2.653 2.610	2.646 2.611	$2.647 \\ 2.611$	2.645 2.649	2.6989 2.6323
	2.288	2.578	2.281	2.587	2.589	2.589	2.251	2.228	2.264	2.560	2.558	2.224	2.6035
Í	2.497	2.487	2.26	2:527	2.231	2.528	$\frac{-}{2.520}$	2.508	$\frac{-}{2.502}$	2.508	$\frac{-}{2.525}$	$\left  \begin{array}{c} - \\ 2 \cdot \overline{553} \end{array} \right\} \left  \begin{array}{c} - \\ \end{array} \right.$	2.5367
-	2.493	2.492	2.500	2.214	2.505	2.515	2.506	2.508	2.499	2.496	2.500	2.510	2.5246
	2.548 2.603	2.567 2.586	2.596 2.602	$2.621 \\ 2.597$	2.624 2.594	2.636 2.596	$\frac{2.641}{2.584}$	2.643 2.580	2.646 2.580	$\frac{2.649}{2.577}$	$\frac{2.663}{2.581}$	$2.662 \\ 2.591$	2.5719 2.6311
1	2.528	2.516	2.214	2.212	2.513	2.543	2.559	2.554	2.555	2.551	2.563	2.604	2.5592
-	2.587 2.639	2.588 2.639	2.576 2.646	$2.588 \\ 2.654$	$2.596 \ 2.671$	$2.591 \\ 2.675$	2.291	2.587	2:595	2.296	2.604	2.608	2.25951
-					_		2.649	2.653	2.654	2.653	2.655	2.650 }	2.6298
	2.574 2.540	2.568 2.544	2.574 2.555	2.541 2.555	$2.578 \\ 2.551$	$2.581 \\ 2.539$	2.583 $2.530$	$2.583 \\ 2.530$	$2.585 \\ 2.525$	$2.589 \\ 2.521$	$\frac{2.593}{2.520}$	2.590 2.520	2.6066 2.5615
	2.419	2.427	2.422	2.424	2.440	2.432	2.432	2.438	2.448	2.453	2.469	2.495	2.4620
	2.627 2.792	$2.655 \\ 2.796$	2.683 2.806	$2.732 \\ 2.829$	2.746 2.841	$\begin{array}{c} 2.755 \\ 2.848 \end{array}$	$2.767 \\ 2.841$	$\frac{2.803}{2.837}$	$\frac{2.794}{2.828}$	2.803 2.846	2.814 2.841	2 843 2 831	$oxed{2.6665}\ 2.8463$
	2.699	2.685	2.673	2.653	2.630	2.610	_					l ) l	2.6442
	2.647	2.665	2.686	2.702	2.719	2.719	$2.315 \\ 2.733$	$\frac{2.308}{2.741}$	$2.308 \\ 2.746$	2:336 2:740	$2.357 \\ 2.740$	2:372 }	2.6416
	2.779	2.776	2.767	2.773	2.778	2.779	2.785	2.773	2.773	2.795	2.765	2.767	2.7921
	2.646 2.419	2.646 2.397	2.636 2.375	2.616 2.392	2.618 2.417	2.623 2.423	2.607 $2.437$	2.601 $2.437$	$2.582 \\ 2.435$	$2.576 \\ 2.446$	$2.571 \\ 2.463$	$\begin{vmatrix} 2.578 \\ 2.464 \end{vmatrix}$	2.6643 2.4655
	2.449	2.449	2.449	2.463	2.467	2.466	2.471	$\frac{2}{2} \cdot \frac{167}{462}$	2.462	$\frac{2}{2}.452$	2.459	2.463	2.4701
	2.505	2.211	2·537 —	2.534	2.234	2.249	2.668 a	2.675	2.678	2.683	2.688	$2.\overline{709}$	2.5445
	2.6088	2.6074	2.6129	2.6198	2.6247	2.6270	2.6184	2.6168	2.6164	2.6193	2.6234	2.6338	2.6313
	2.738	2.738	2.744	2.757	2.760	2.760	2.718	2.720	2.720	2.764	2.785	2.799	2.7527
	2.730 2.591	2.730 2.599	2.736 2.569	2.726 2.556	2.726 2.553	$2.726 \\ 2.538$	2.729 2.528	$2.731 \\ 2.518$	2.731 2.503	2.697 2.483	2.697 2.477	$\begin{vmatrix} 2.716 \\ 2.474 \end{vmatrix}$	$2.7522 \\ 2.6029$
-	2.316	2.309	2.317	2.350	2.311	2.302	2.300	2.284	2.277	2.278	2.269	2.263	2:3627
	2.352 2.561	2.365 2.559	2.393 2.564	2·393 2·573	2.398 2.569	$2.410 \\ 2.567$	2'411	2.415	2.418	2.418	2.456	2.446	2.3624
						_	2.736	2.726	2.728	2.734	2.724	$2.\overline{7}_{62}$	2.5939
	2.784 2.755	$2.781 \\ 2.755$	$2.780 \\ 2.751$	2.790 2.755	2.791 2.755	$2.793 \\ 2.744$	$2.789 \\ 2.734$	$2.782 \\ 2.728$	$2.783 \\ 2.729$	2.783 2.726	2.790 2.724	$\begin{vmatrix} 2.798 \\ 2.725 \end{vmatrix}$	2.7893 2.7708
	2.734	2.728	2.739	2.756	2.761	2.760	2.754	2.746	2.746	2.749	2.749	2.752	2.7489
	2.703 2.601	2.701 2.595	2.710 2.596	2.708 2.602	2.708 2.595	$2.711 \\ 2.589$	$2.711 \\ 2.586$	2.708 2.594	$2.704 \\ 2.571$	2.713 2.565	2.709 2.549	2.716 2.555	2.7346 2.6277
	2.21	2.574	2.592	2.598	2.600	$\frac{2}{2}.593$	<del></del>					$\left \frac{2.580}{2.580}\right\}$	2.5752
1	2.524	2.542	2.242	2.217	2.201	2.506	2.552 2.490	$2.552 \\ 2.482$	2.552 2.481	2.547 2.481	$2.559 \\ 2.457$	2.580 \( 2.456	2.5328
	2.307	2.312	2.334	2.346	2.358	2:361	2.356	2.349	2.345	2.356	2:369	2.388	2.3763
	2.516 2.520	$2.516 \\ 2.525$	$2.527 \\ 2.537$	2.513 $2.547$	2.514 2.535	2.518 $2.531$	2.518 2.530	$2.518 \\ 2.520$	$2.518 \\ 2.518$	$2.532 \\ 2.520$	$2.536 \\ 2.520$	2:538 2:523	$2.4935 \\ 2.5331$
	2.491	2.500	2.203	2.218	2.20	2.215	2.20	2.210	2.201	2.219	2.232	2.243	2.2023
	2.264	2.269	2.22	2.567	2.268	2.570	2.721	2.728	$\frac{-}{2.734}$	$2.\overline{747}$	$\frac{-}{2.756}$	$2.\overline{745}$	2.6074
	2.766	2.772	2.786	2.807	2.807	2.818	2.827	2.807	2.814	2.817	2.830	2.839	2.7994
	2.867 2.851	2.871 2.833	2.890 2.825	2.882	2.897 2.806	2.807	2.905 2.808	2.898 2.791	$2.901 \\ 2.772$	$\frac{2.903}{2.779}$	2.908 2.775	2 · 925 2 · 767	2.8905 2.8603
	2.554	2.537	2.526	2.217	2.216	2.496	2.479	2.488	2.498	2.502	2.210	2.529	2.5899
	2.618 2.610	2.612 2.596	2.626 2.620	2.628 2.647	2.629 2.639	2.643 2.632	2.652	2.645	2.641	2.650	2.653	2.658	2.6261
		-		_			2.693	2.693	2.685	2.677	2.670	$\{2.668\}$	2.6495
	2.623 2.747	2.626 2.721	2.650 2.728	$2.636 \\ 2.713$	$2.649 \\ 2.711$	$2.676 \\ 2.711$	$2.697 \\ 2.713$	$2.701 \\ 2.685$	$2.717 \\ 2.683$	2.726 2.665	$2.735 \\ 2.657$	2.739 2.663	2.6525 2.7438
	2.6152	2.6142	2.6214	2.6228	2.6222	2.6224	2.6330	2.6277	2.6258	2.6281	2.6306	2.6372	2.6360

^{*} Proportion of 1st August.

				Barome		BAROMET = 27 Engli			ers in the Ta	ible.			
lours o Götti Tin	f Mean }	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \end{pmatrix}$	In. 2.669 2.665 2.542 2.675	In. 2.669 2.675 2.540 2.687	In. 2.674 2.683 2.540 2.688	In. 2.670 2.686 2.542 2.688	In. 2.661 2.688 2.529 2.686	In. 2:647 2:681 2:525 2:676	In. 2.638 2.675 2.517 2.666	In. 2.639 2.669 2.510 2.644	In. 2.622 2.659 2.499 2.634	In. 2.615 2.641 2.478 2.604	In. 2.602 2.640 2.512 2.594	In. 2 · 598 2 · 639 2 · 542 2 · 594
લ્સ	5 6 7 8 9 10 11	2.711 2.787 2.498 2.623 2.903 2.995	2.713 2.787 2.482 2.639 2.912 2.995	2.735 2.787 2.474 2.668 2.932 2.995	2.762 2.770 2.457 2.700 2.950 3.007	2.763 2.760 2.451 2.710 2.959 2.988	2.752 2.735 2.438 2.718 2.969 2.957	2·752 2·728 2·422 2·724 2·971 2·944	2·753 2·718 2·412 2·726 2·966 2·925	2·741 2·700 2·381 2·722 2·965 2·908	2.741 2.659 2.359 2.722 2.960 2.888	2.746 2.653 2.344 2.722 2.968 2.867	2:749 2:635 2:335 2:727 2:967 2:859
SEPTEMBER	12 13 14 15 16 17 18	2:581 2:764 2:893 2:782 2:620 2:445	2.583 2.772 2.901 2.782 2.620 2.447	2:589 2:779 2:906 2:782 2:610 2:439	2·595 2·794 2·901 2·783 2·611 2·439	2:601 2:796 2:894 2:768 2:608 2:433	2.603 2.814 2.882 2.749 2.600 2.439	2.602 2.814 2.853 2.727 2.597 2.425	2.600 2.803 2.840 2.697 2.581 2.428	2.602 2.789 2.818 2.683 2.568 2.428	2.617 2.785 2.805 2.676 2.558 2.420	2.630 2.786 2.796 2.674 2.533 2.432	2.636 2.789 2.783 2.653 2.534 2.430
	19 20 21 22 23 24 25	2:436 2:575 2:795 2:720 2:659 2:607	2.442 2.594 2.801 2.720 2.663 2.609	2:446 2:598 2:806 2:723 2:665 2:620	2.454 2.618 2.808 2.729 2.667 2.624	2:462 2:632 2:815 2:720 2:663 2:635	2:461 2:631 2:823 2:709 2:647 2:639	2:465 2:637 2:800 2:695 2:637 2:624	2·462 2·645 2·794 2·667 2·623 2·624	2.459 2.637 2.784 2.654 2.619 2.612	2:467 2:643 2:759 2:636 2:615 2:622	2·471 2·650 2·765 2·637 2·609 2·632	2:483 2:655 2:745 2:634 2:603 2:626
	26 27 28 29 30	2:298 2:292 2:345 2:380	2·303 2·290 2·363 2·406	2:300 2:301 2:351 2:419	2·302 2·305 2·351 2·426	2·293 2·303 2·351 2·433	2·279 2·306 2·337 2·426	2·268 2·302 2·325 2·410	2·255 2·322 2·298 2·405	2·234 2·318 2·317 2·404	2·226 2·327 2·297 2·397	2·210 2·328 2·287 2·392	2·182 2·349 2·298 2·390
Hourly	y Means	2.6254	2.6306	2.6350	2.6400	2.6385	2.6324	2.6238	2.6156	2.6060	2.5968	2.5954	2.5937
	$\begin{pmatrix} 1 \\ 2 \end{pmatrix}$	2:309 2:691	2:328 2:718	2·359 2·725	2·378 2·748	2·399 2·751	2.432 2.750	2.459 2.741	2:467 2:730	2·477 2·723	2.486 2.732	2:498 2:745	2.516 2.745
	3 4 5 6 7 8 9	2·763 2·299 2·396 2·581 2·321 2·378	2.753 2.301 2.428 2.597 2.327 2.327 2.382	2.756 2.293 2.446 2.595 2.323 2.383	2.752 2.267 2.466 2.597 2.326 2.375	2.746 2.266 2.478 2.589 2.322 2.359	2.745 2.252 2.492 2.580 2.299 2.357	2·710 2·251 2·497 2·571 2·295 2·339	2.667 2.248 2.509 2.541 2.284 2.300	2.624 2.249 2.519 2.529 2.281 2.266	2.630 2.246 2.523 2.513 2.257 2.259	2.608 2.257 2.541 2.503 2.259 2.214	2·594 2·270 2·540 2·484 2·249 2·208
OCTOBER.	10 11 12 13 14 15 16	2.608 2.563 2.093 2.411 2.784 2.763	2.632 2.547 2.110 2.446 2.804 2.762	2.650 2.497 2.126 2.469 2.818 2.768	2.689 2.481 2.150 2.483 2.828 2.755	2·708 2·441 2·174 2·492 2·838 2·750	2.706 2.400 2.191 2.517 2.829 2.733	2.694 2.340 2.201 2.516 2.818 2.683	2.694 2.290 2.183 2.515 2.810 2.630	2.674 2.208 2.190 2.525 2.806 2.596	2.661 2.163 2.205 2.531 2.812 2.577	2.659 2.117 2.232 2.553 2.810 2.543	2.655 2.071 2.252 2.571 2.808 2.541
. OC1	17 18 19 20 21 22 23	2.693 2.690 2.838 2.956 2.629 2.725	2.697 2.710 2.844 2.962 2.617 2.753	2.679 2.736 2.854 2.984 2.637 2.783	2.669 2.736 2.858 2.961 2.663 2.791	2.616 2.744 2.852 2.939 2.653 2.804	2.587 2.746 2.831 2.950 2.664 2.799	2·536 2·734 2·798 2·938 2·670 2·791	2·510 2·721 2·777 2·898 2·660 2·779	2·477 2·705 2·764 2·882 2·658 2·766	2·468 2·704 2·781 2·863 2·672 2·769	2.464 2.719 2.785 2.840 2.675 2.794	2·437 2·735 2·797 2·834 2·675 2·819
	24 25 26 27 28 29 30 31	2·344 2·963 3·271 3·343 3·136 2·967	2°372 2°999 3°282 3°358 3°150 2°970	2·412 3·031 3·292 3·377 3·156 2·980	2·420 3·059 3·292 3·389 3·152 2·970	2.465 3.085 3.290 3.396 3.135 2.962	2·487 3·106 3·277 3·381 3·120 2·951	2·504 3·108 3·263 3·367 3·100 2·928	2·529 3·121 3·241 3·339 3·073 2·908	2·576 3·137 3·228 3·316 3·063 2·889	2.635 3.157 3.225 3.293 3.048 2.891	2.698 3.173 3.225 3.272 3.038 2.889	2.753 3.185 3.247 3.255 3.014 2.889
—— Hourly	y Means	2.6737	2.6865	2.6973	2.7021	2.7021	2.6993	2.6866	2.6702	2.6588	2.6577	2.6581	2.6594

			Baı	rometer at 3			RESSURE. s + the nu	mbers in the	Table.			
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In. 2.6322
2.603	2.603	2.616	2.615	2.619	2.621	2.625	2.630	2.630	2.631	2.632	2.652	2.6322 $2.6277$
2.636	2.619	2.610	2.615	2.618	2.607	2.293	2.249	2.268	2.556	2.239	2.528	2.5800
2.552	2.590	2.605	2.632	2.652	2.663	2.664	2.656	2.621	2.659	5.660	5.628	
2.574	2.563	2.570	2.246	2.206	2.218		0:020	$2.\overline{657}$	2.666	2.677	$\left[\begin{array}{c} -2.689 \\ 2.689 \end{array}\right]$	2.6280
	0.707	0.7.7	0.50	0.700	0.500	$\begin{vmatrix} 2.630 \\ 2.765 \end{vmatrix}$	$\begin{vmatrix} 2.639 \\ 2.774 \end{vmatrix}$	$\frac{2.037}{2.770}$	$\frac{2.000}{2.772}$	$\frac{5}{2} \cdot 764$	2.793	2.7532
2.749	2.735	2.747	2.759	2.768	2.763 2.562	2.260	$\frac{2}{2} \cdot 534$	$\frac{5}{2} \cdot 514$	2 498	2.200	2.505	2.6402
2.627	2.604 2.355	$2.594 \\ 2.398$	2.578	$2.576 \\ 2.466$	$\frac{2.362}{2.480}$	2.481	2.21	2.546	2.249	2.568	2.588	2.4475
2.335 2.733	$\frac{2}{2},\frac{333}{743}$	$\frac{2}{2}.770$	$\frac{2.400}{2.792}$	2.807	2.814	2.822	2.817	2.823	2.834	2.852	2.859	2.7528
2.963	2.969	$\frac{2}{2}.978$	2.974	$\frac{2.975}{2.975}$	2.976	2.979	2.983	2.984	2.085	2.983	2.987	2.9648
2.851	2.831	2.822	2.818	2.817	2.813			<u> </u>			J }	2.8222
_			_			2.299	2.575	2.575	2.567	2.569	2.569	2.6505
2.652	2.666	2.677	2.704	2.689	2.691	2.695	2.701	2.708	2.708	2.734	2.748	2.8123
2.790	2.803	2.830	2.843	2.839	2.844	2.844	2.855	2.852	2.860	$\frac{2.861}{2.773}$	2.863 2.782	2.8159
2.785	2.783	2.787	2.784	2.791	2.789	2.785	2.774	2.766	$2.759 \\ 2.637$	$\frac{2}{2}.617$	2.619	2.6869
2.659	2.659	2.659	2.654	2.655	2.644	2.644	$2.642 \\ 2.482$	2.640 2.476	$\begin{bmatrix} 2.657 \\ 2.464 \end{bmatrix}$	$\frac{2.442}{2.442}$	$\frac{2.013}{2.442}$	2.2422
2.527	2.548	2.557	$2.537 \\ 2.442$	2.529 2.438	2.489 2.434	2.481	2 402					2.4347
2.436	2.444	2.446	2 442 	2 100	2 704	2.448	2.440	2.436	2.415	2.420	2.430 }	1
2.492	$2.\overline{510}$	$2.\overline{514}$	2.21	$2.\overline{523}$	2.524	2.524	$\frac{2}{2}.524$	2.526	2.528	2.534	2.551	2.4908
2.668	$\frac{2.680}{2.680}$	$\frac{2.697}{2.697}$	$\frac{2.021}{2.717}$	$\frac{2.020}{2.721}$	$\frac{2.321}{2.720}$	2.732	2.743	2.744	2.745	2.752	2.753	2.6745
2.746	2.754	2.748	2.745	2.745	2.734	2.732	2.743	2.732	2.725	2.721	2.719	2.7641
2.634	2.640	2.651	2.659	2.647	2.644	2.652	2.654	2.638	2.638	2.632	2.640	2.6655
2.602	2.607	2.611	2.653	2.615	2.600	2.611	2.604	2.596	2.596	2.296	2.605	2.6222
2.614	2.614	2.620	2.654	2.624	2.614		0.050	0:050	2.330	2.324	$\left\{ \frac{1}{2}, \frac{1}{300} \right\}$	2.5525
						2:394	$2.376 \\ 2.307$	$\frac{2.352}{2.292}$	2 330	$\frac{2.324}{2.297}$	$\frac{2.300}{2.307}$	2.2636
2.202	2.183	2.184	2:234	2.271	2.299	2.304	$\frac{2.307}{2.355}$	$\frac{2}{2} \cdot \frac{292}{362}$	$\frac{2}{2} \cdot \frac{23}{349}$	2.346	2.347	2.3359
2:364 2:299	2.376	2:376 2:316	$\begin{bmatrix} 2.376 \\ 2.327 \end{bmatrix}$	$2.371 \\ 2.330$	2:350 2:306	$\frac{2.348}{2.298}$	$\frac{2}{2} \cdot 305$	$\frac{2}{2} \cdot \frac{302}{309}$	$\frac{2}{2} \cdot 316$	2.335	2.358	2:3217
2.390	2:303 2:390	$\frac{2}{3}$	2.384	2.386	2.343	$\frac{2}{2} \cdot \frac{230}{329}$	2·28 <b>5</b>	2.257	2.261	2.581	2.292	2.3699
2.5956	2.5988	2.6067	2.6114	2.6145	2.6093	2.5975	2.5961	2.5925	2.201	2.5927	2.5994	2.6099
										2.0	2.000	0:7190
2.218	2.538	2.556	2.586	2.596	2.599	2.611	2.622	2.629	2.639	2.659	2.670	2.2138
2.751	2.763	2.784	2.793	2.802	2.850	0.700	$2.\overline{780}$	$2.\overline{761}$	2.762	2.762	$\{2.762\}$	2.7553
0:700		0.500	0:470	2.506	2.480	$2.786 \\ 2.456$	2.446	$\frac{2}{2} \cdot 437$	$\frac{2}{2} \cdot 355$	2.317	2.327	2.5768
2.596 2.283	2:572 2:300	2.528 2.316	2.476 2.312	$\frac{2.309}{2.309}$	2 480	$\frac{2}{2},\frac{430}{295}$	2.324	$\frac{2}{2} \cdot 323$	$\frac{2}{2} \cdot 325$	2.333	2.373	2.2913
2.243	2.564	2.568	$\frac{2.512}{2.582}$	$\frac{2.503}{2.574}$	$\frac{2.533}{2.572}$	$\frac{2.577}{2.577}$	2.575	2.575	2.579	2.573	2.269	2.5286
2.478	2.474	$\frac{2}{2}$ .472	2.458	2.452	2.400	2.385	2.387	2.365	2.349	2:327	2:327	2.4814
2.235	2.235	$\frac{2}{2} \cdot \frac{259}{259}$	2.290	2.599	2.312	2.336	2.338	2.356	2.357	2.363	2.368	2.3038
2.148	2.124	2.130	2.158	2.185	2.206	_				0.510	$2.\overline{576}$	2:3297
	_		_			2.486	2.495	2:507	2:507	2.513 $2.619$	$\begin{bmatrix} 2 & 576 \\ 2 & 607 \end{bmatrix}$	2.6642
2.667	2.682	2.687	2.690	2.688	2.680	2.676	2.645	$2.642 \\ 2.035$	$2.629 \\ 2.043$	2.063	$\begin{bmatrix} 2.607 \\ 2.074 \end{bmatrix}$	2.1922
2.063	2.047	2.043	2.014	2.018	$2.030 \\ 2.338$	2.031 2.344	$2.035 \\ 2.358$	2 035	$\frac{2.043}{2.367}$	$\frac{2}{2} \cdot 379$	$[\frac{2}{2}, \frac{3}{3}]$	2.2555
2.280 2.585	2.293	2.295	2.295 2.670	2:325 2:679	2 338	2.696	$\frac{2}{2}.711$	$\frac{2.301}{2.719}$	$\frac{2.307}{2.726}$	$\frac{2.747}{2.747}$	2.761	2.5952
2.806	2.622 2.796	$2.647 \\ 2.782$	$\frac{2.670}{2.792}$	2.679	$\frac{2.094}{2.777}$	$\frac{2}{2}.792$	$\frac{2}{2}.796$	2.802	$\frac{2.780}{2.782}$	2.782	2.777	2.8019
2.21	$\frac{2.796}{2.529}$	$\frac{2.782}{2.502}$	2.505	2.497	2.491		_				$\left\{ 2.\overline{728} \right\}$	2.6472
_	- 020	2 002				2.734	2.726	2.732	2.736	2.732		1
2.417	2.416	2.413	2.458	2.482	2.210	2.534	2.576	2.600	2.616	2.640	2.677	2.5488
2.755	2.760	2.760	2.796	2.803	2.801	2.800	2.804	2.802	2.808	2.819	2.836	2.7595 $2.8551$
2.851	2.837	2.860	2.879	2.887	2.898	2.902	2.909	2.916	2.933	2.638	2.959 2.622	2.8138
2.810	2.791	2.762	2.756	2.740	2.708	2.695	2.687	2.678	2.638 2.695	$2.638 \\ 2.699$	2.710	2.6756
2.683	2.684	2.682	2.709	2.727	2.703	2.686	2.683	2.681	∠ U90 		(	
2.851	2.814	2.830	2.833	2.834	2.836	$2.\overline{311}$	2.598	2.293	$2.\overline{293}$	2.304	$2.\overline{308}$	2.6728
2.791	2.806	2.824	2.851	2.861	2.872	2.890	2.899	2.907	2.919	2.935	2.949	2.6957
3.204	3.519	$\frac{2}{3} \cdot 234$	3.257	$\frac{2}{3} \cdot 251$	3.253	3.256	3.253	3.255	3.245	3.246	3.264	3.1692
3.256	3.264	3.271	3.275	3.273	3.278	3.278	3.276	3.274	3.302	3.307	3.335	3.2719
3.237	3.519	3.511	3.214	3.216	3.185	3.169	3.168	3.168	3.128	3.128	3.150 2.976	3.2640 3.0430
2.994	3.000	3.004	3.004	2.996	2.993	2.977	2.980	2.988	2.968	2.968	1	
2.889	2.887	2.889	2.874	2.872	2.864	2.655	2.653	$2.\overline{653}$	2.659	2.667	$2.\overline{669}$	2.8510
2.6608	2.6641	010077	2.6741	2.6796	2.6768	2.6676	2.6702	2.6716	2.6690	2.6727	2.6833	2.6753

				Barome	eter at 32° :	BAROMET = 27 Engli			ers in the Ta	able.			
Hours o Göttir Tin	f Mean ngen ne.	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	1 2 3 4 5 6	In. 2.669 2.692 2.472 2.549 2.587 2.834	In. 2.694 2.695 2.472 2.561 2.584 2.854	In. 2.699 2.677 2.462 2.575 2.601 2.871	In. 2 * 696 2 * 655 2 * 448 2 * 582 2 * 617 2 * 898	In. 2.703 2.649 2.450 2.574 2.621 2.912	In. 2.701 2.637 2.439 2.563 2.621 2.914	In. 2 · 692 2 · 602 2 · 420 2 · 542 2 · 609 2 · 908	In. 2.686 2.582 2.397 2.534 2.602 2.906	In. 2.684 2.573 2.389 2.504 2.614 2.896	In. 2.680 2.550 2.393 2.499 2.631 2.889	In. 2.680 2.544 2.403 2.495 2.650 2.876	In. 2.680 2.542 2.414 2.499 2.672 2.888
ER.	7 8 9 10 11 12 13 14	2.606 2.346 2.761 2.866 2.851 2.803	2.626 2.330 2.789 2.880 2.860 2.802	2.611 2.360 2.797 2.896 2.870 2.844	2.641 2.349 2.826 2.911 2.849 2.858	2.612 2.385 2.844 2.919 2.845 2.857	2.603 2.402 2.846 2.915 2.821 2.850	2:577 2:451 2:841 2:903 2:790 2:832	2:544 2:473 2:845 2:896 2:762 2:849	2.516 2.486 2.845 2.892 2.750 2.829	2:540 2:504 2:849 2:895 2:748 2:790	2:538 2:520 2:849 2:898 2:746 2:792	2·533 2·532 2·844 2·909 2·748 2·748
NOVEMBER	15 16 17 18 19 20 21	2:357 2:859 2:619 2:562 2:541 3:104	2·379 2·859 2·639 2·551 2·573 3·095	2·427 2·865 2·649 2·573 2·642 3·115	2.471 2.860 2.659 2.555 2.687 3.114	2:506 2:840 2:654 2:541 2:717 3:123	2:531 2:798 2:665 2:505 2:737 3:104	2.562 2.737 2.661 2.474 2.749 3.068	2:578 2:712 2:662 2:447 2:773 3:045	2.608 2.658 2.649 2.407 2.800 3.016	2.632 2.629 2.652 2.367 2.838 3.003	2:670 2:605 2:656 2:342 2:870 2:983	2.686 2.574 2.664 2.352 2.910 2.967
	22 23 24 25 26 27 28	2·828 2·598 2·372 2·257 2·603 2·677	2.841 2.582 2.380 2.265 2.632 2.660	2.853 2.558 2.384 2.283 2.663 2.645	2.863 2.537 2.400 2.271 2.708 2.624	2.878 2.531 2.414 2.276 2.753 2.622	2.871 2.510 2.412 2.267 2.765 2.594	2·863 2·471 2·386 2·263 2·774 2·556	2.858 2.464 2.376 2.263 2.778 2.544	2.823 2.449 2.351 2.293 2.787 2.533	2·824 2·453 2·351 2·307 2·803 2·539	2.830 2.444 2.335 2.321 2.817 2.552	2·825 2·423 2·307 2·344 2·823 2·553
(	29 30	3.195 3.148	3.213 3.148	3:221 3:152	3·247 3·144	3·256 3·143	3·249 3·117	$3.245 \\ 3.092$	3·218 3·074	3·216 3·052	3·221 3·050	3·211 3·041	3.506 3.019
Hourly	Means	2.6829	2.6909	2.7036	2.7104	2.7163	2.7091	2.6949	2.6872	2.6777	2.6783	2.6795	2.679
	1 2 3 4 5	2:843 2:410 2:566 2:728	2.841 2.430 2.582 2.726	2:851 2:455 2:586 2:735	2:839 2:465 2:607 2:737	2.822 2.475 2.587 2.727	2.806 2.488 2.583 2.721	2·769 2·497 2·552 2·696	2:741 2:497 2:531 2:674	2·703 2·491 2·540 2·642	2.691 2.520 2.553 2.625	2:687 2:530 2:574 2:623	2:699 2:556 2:586 2:624
	6 7 8 9 10 11 12	2.697 2.878 2.821 2.827 2.345 2.595	2.715 2.886 2.821 2.817 2.343 2.634	2.738 2.881 2.813 2.802 2.355 2.676	2.750 2.897 2.801 2.784 2.369 2.719	2.784 2.917 2.781 2.756 2.369 2.766	2·796 2·912 2·750 2·697 2·373 2·772	2·796 2·898 2·700 2·641 2·386 2·792	2·794 2·888 2·676 2·589 2·402 2·804	2·794 2·895 2·677 2·542 2·420 2·821	2.806 2.906 2.685 2.491 2.448 2.855	2.806 2.926 2.694 2.477 2.480 2.880	2:816 2:930 2:695 2:443 2:498 2:901
DECEMBER.	13 14 15 16 17 18 19	2.650 2.700 2.633 3.096 2.788 2.810	2.662 2.702 2.653 3.092 2.787 2.808	2:690 2:688 2:665 3:105 2:801 2:804	2.704 2.670 2.708 3.122 2.789 2.826	2·724 2·654 2·736 3·125 2·788 2·810	2·720 2·627 2·734 3·092 2·776 2·786	2.708 2.601 2.736 3.108 2.754 2.753	2.698 2.583 2.736 3.079 2.726 2.706	2·727 2·567 2·756 3·076 2·723 2·671	2·735 2·577 2·772 3·061 2·736 2·647	2.735 2.589 2.801 3.076 2.764 2.617	2·745 2·573 2·829 3·041 2·755 2·587
. '	20 21 22 23 24 25 a	2·792 2·940 2·178 2·324 2·051	2.822 2.930 2.180 2.322 2.063	2·842 2·912 2·172 2·272 2·125	2·860 2·907 2·170 2·246 2·177	2.886 2.889 2.166 2.201 2.215	2.877 2.853 2.161 2.153 2.254	2.877 2.792 2.143 2.074 2.273	2.865 2.750 2.151 2.057 2.300	2.868 2.719 2.162 2.025 2.314	2·898 2·646 2·193 2·014 2·331	2 · 926 2 · 638 2 · 221 2 · 027 2 · 350	2 · 961 2 · 586 2 · 255 2 · 007 2 · 357
	26 27 28 29 30 31	2.981 2.658 2.627 2.597 2.750	3:007 2:666 2:641 2:612 2:740	3:006 2:668 2:649 2:626 2:740	3 · 023 2 · 671 2 · 650 2 · 646 2 · 745	3.023 2.689 2.663 2.655 2.737	3 · 007 2 · 657 2 · 655 2 · 645 2 · 707	2·974 2·644 2·625 2·633 2·689	2.956 2.620 2.615 2.622 2.662	2:940 2:624 2:615 2:622 2:630	2·918 2·637 2·624 2·641 2·630	2.900 2.633 2.628 2.657 2.625	2 · 861 2 · 653 2 · 652 2 · 683 2 · 627
Iourly	Means	2.6648	2.6724	2.6787	2.6878	2.6902	2.6770	2.6581	2.6432	2.6371	2.6400	2.6486	2.6508

^a Christmas Day.

			Bar	ometer at 3:		METRIC P			e Table.			
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
In. 2 : 696 2 : 536 2 : 430 2 : 493 2 : 696	In. 2.710 2.544 2.434 2.491 2.720	In. 2:714 2:549 2:442 2:506 2:741	In. 2:722 2:553 2:466 2:504 2:756	In. 2.720 2.545 2.472 2.505 2.756	In. 2 · 722 2 · 530 2 · 480 2 · 525 2 · 766	In. 2.714 2.526 2.482 2.538 2.786	In. 2.690 2.521 2.504 2.553 2.795	In. 2.690 2.521 2.521 2.557 2.787	In. 2.690 2.499 2.535 2.564 2.785	In. 2.680 2.487 2.542 2.572 2.803	In. 2:676 2:480 2:546 2:582 2:820	In. 2 * 6953 2 * 5704 2 * 4589 2 * 5361 2 * 6925
2:901 2:536 2:547 2:840 2:918 2:748 2:724	2.889 2.539 2.553 2.866 2.920 2.760 2.646	2 · 876 2 · 529 2 · 573 2 · 870 2 · 910 2 · 760 2 · 606	2.5880 2.523 2.591 2.876 2.914 2.758 2.571	2.871 2.510 2.597 2.878 2.916 2.762 2.503	2.866 2.494 2.603 2.860 2.910 2.762 2.414	2.648 2.468 2.606 2.858 2.898 2.758	2.636 2.443 2.659 2.864 2.884 2.754	2.627 2.435 2.677 2.856 2.882 2.769	2.613 2.405 2.692 2.851 2.868 2.769	2.619 2.393 2.709 2.856 2.869 2.777	2·605 } 2·360 2·745 2·860 2·855 2·783	2*8199 2*5243 2*5287 2*8446 2*8968 2*7833 2*6281
2.711 2.561 2.666 2.314 2.938 2.926	2.751 2.559 2.666 2.296 2.968 2.919	2·772 2·541 2·650 2·290 2·982 2·889	2.782 2.542 2.660 2.297 2.999 2.861	2.786 2.552 2.630 2.317 3.015 2.858	2·791 2·559 2·646 2·355 3·024 2·860	2:287 2:797 2:565 2:616 2:369 3:031	2 · 281 2 · 828 2 · 556 2 · 614 2 · 376 3 · 048	2:281 2:838 2:574 2:634 2:397 3:068	2:285 2:836 2:578 2:608 2:415 3:069	2:287 2:842 2:592 2:594 2:452 3:065	2:335} 2:858 2:577 2:561 2:496 3:084	2.6666 2.6563 2.6406 2.4187 2.8803 2.9599
2·827 2·407 2·307 2·352 2·837 2·554	2·827 2·399 2·297 2·357 2·844 2·586	2.813 2.393 2.297 2.367 2.845 2.582	2.796 2.358 2.271 2.374 2.845 2.569	2·800 2·350 2·248 2·394 2·847 2·551	2·790 2·340 2·330 2·406 2·835 2·541	2.832 2.756 2.340 2.246 2.423 2.816	2:832 2:730 2:340 2:222 2:445 2:808	2:840 2:702 2:342 2:223 2:455 2:788	2.836 2.661 2.346 2.246 2.462 2.774	2.828 2.645 2.358 2.253 2.533 2.758	2·819 }   2·611   2·352   2·264   2·558   2·724   — }	2.7965 2.4310 2.3155 2.3557 2.7761 2.7151
3·202 3·006	3·201 2·990	3·195 2·976	3·190 2·962	3·180 2·951	3·180 2·937	3.059 3.180 2.929	3.079 3.185 2.923	3.106 3.187 2.923	3:130 3:189 2:891	3:138 3:166 2:875	3·169 } 3·156 2·860	3°2045 3°0168
2.6797	2.6820	2.6795	2.6777	2.6736	2.6702	2.6742	2.6758	2.6800	2.6768	2.6805	2.6822	2.6851
2.686 2.557 2.604	2.660 2.575 2.606	2.640 2.565 2.610	2.628 2.575 2.618	2.588 2.581 2.634	2.552 2.577 2.640	2.510 2.583 2.649	2.486 2.575 2.665	2:442 2:565 2:681	2:414 2:553 2:691	2:404 2:547 2:699	2:402 2:538 2:716	2.6543 2.5252 2.6108
2.612 	2·595 	2.575 	2:541 2:844 2:932 2:779 2:371 2:577	2·518 — 2·841 2·918 2·793 2·369 2·577	2·514 	2.587 2.836 2.905 2.814 2.360 2.567	2.595 2.834 2.903 2.802 2.337 2.541	2.622 2.845 2.877 2.828 2.347 2.546	2.633 2.849 2.857 2.822 2.351 2.550	2.651 2.853 2.851 2.826 2.325 2.568	2.669 2.856 2.825 2.833 2.339 2.603	2.6404 2.8078 2.9001 2.7684 2.5105 2.4808
2.907 2.771 2.573 2.847 3.035 2.766	2.941 2.791 2.564 2.904 3.018 2.780	2.920 2.806 2.569 2.926 2.978 2.792	2 · 954 	2.972 2.788 2.541 2.933 2.930 2.830	2.968 2.794 2.571 2.966 2.919 2.829	2.629 2.758 2.581 2.974 2.903 2.823	2.617 2.763 2.579 3.001 2.893 2.823	2.629 2.763 2.595 3.038 2.871 2.824	2.625 2.732 2.603 3.039 2.854 2.823	2.625 2.724 2.607 3.054 2.808 2.814	$ \begin{bmatrix}  - \\  2.621 \\  2.702 \\  2.613 \\  3.072 \\  2.782 \\  2.806 \end{bmatrix} $	2.7760 2.7374 2.6030 2.8523 3.0016 2.7881
2.579 2.980 2.550 2.291 2.011 2.387	2.546 2.990 2.501 2.317 2.011 2.403	2·524 — 3·008 3·491 3·345 1·997 2·399	2·496 — 3·017 3·447 3·349 1·981 2·393	2.486 3.008 3.413 3.356 1.954 2.394	2.456 3.018 3.384 3.382 1.956 2.400	2.709 3.018 3.341 3.358 1.957	2·719 2·997 2·275 2·358 1·967	2·733 2·994 2·255 2·357 1·977	2·742 2·988 2·230 2·349 2·007	2.758 2.971 2.199 2.336 2.015	2·773 2·953 2·186 2·328 2·019	2.6811 2.9340 2.5764 2.2616 2.0656
2.847 2.675 2.658 2.699 2.625	2 403 — 2 831 2 703 2 668 2 709 2 627	2 · 399 	2.767 2.667 2.665 2.722 2.588	2 · 731 2 · 696 2 · 656 2 · 726 2 · 576	2 · 729 2 · 692 2 · 640 2 · 720 2 · 562	2.915 2.690 2.677 2.638 2.720 2.558	2 · 933 2 · 660 2 · 671 2 · 626 2 · 718 2 · 528	2 · 948 2 · 688 2 · 653 2 · 626 2 · 718 2 · 504	2'954 2'691 2'663 2'614 2'739 2'487	2.953 2.659 2.636 2.604 2.747 2.459	$ \begin{array}{c}                                     $	2.4523 2.8474 2.6639 2.6377 2.6793 2.6175
2.6581	2.6615	2.6583	2.6549	2.6465	2.6456	2.6562	2.6487	2.6510	2.6485	2.6420	2.6398	2.6567

The content   18	Hours of Mo Göttinge Time.	ean ) in }	0	1	2	3	4	5	6	7	8	9	10	11
1	Hours of Me Toronto	ean}	18	19	20	21	22	23	0	1	2	3	4	5
1		II	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
1			2.382	2.368	2.348	2.334			2.251			2.182		2.229
A			2.714	2.720	2.716		2.716	2.702	2.660	2.632	2.612		2.604	2.587
Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Second Process   Seco					2.793									2.982
Fig.   2				_										2.147
8 2 329 2 2333 2 338 2 344 2 325 2 2350 2 334 2 325 2 2354 2 365 2 90 10 2 90 2 90 2 90 2 90 2 90 2 90 2														2.637
9													2 393	2.579 2.363
11		- 11				2.421		_				2.584		
Table   1	1	- 11											3.172	3.180
Heart   13														2.703 $2.972$
Temporal Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of Process of														$\frac{2}{2} \cdot 738$
19	$\frac{\lambda}{\epsilon}$ 14						2.780	2.766	2.736	2.718	2.708	2.702	2.692	2.680
19	$\left[\frac{15}{16}\right]^{15}$		2.366	2 360	2.368		2.390	2:390	2.377	2'382	2.402		2.477	2.241
19	<b>岩石</b>	7		2.815	2.875		2.978	2.987	$2.\overline{971}$	2.961	2.961		2.942	2.91
19   3   239   3   267   3   298   3   298   3   298   3   298   3   298   3   297   3   2776   2   2767   2   2765   2   2665   2   2   2   2   2   3   2   399   2   2   375   2   344   2   2   347   2   2   3   3   2   399   2   375   2   344   2   2   347   2   2   3   3   3   3   3   3   3   3	<b>A</b> 18			2.587	2.653									3.06
21	19											3.161		3.106
22 2 2 2 8 24 2 7 7 6 2 7 7 6 2 7 8 0 2 7 8 0 2 7 7 7 2 7 4 7 2 6 9 0 2 6 5 1 2 6 1 2 5 9 5 2 5 9 3 2 3 0 7 0 3 0 7 1 3 0 7 1 3 0 9 5 3 0 9 2 3 0 9 0 3 0 5 1 3 0 3 0 3 0 1 9 3 0 1 2 3 0 0 5 2 5 2 5 2 9 2 0 2 9 1 9 2 9 1 9 9 2 9 2 9 2 9 9 2 9 9 8 2 8 8 9 2 8 9 2 8 4 2 8 8 9 2 8 7 5 2 6 2 6 9 2 6 8 2 6 6 7 2 6 4 9 2 6 2 5 2 6 2 6 6 7 2 6 4 9 2 6 2 5 2 7 8 8 2 7 8 8 9 2 8 7 8 8 2 8 8 9 2 8 7 8 8 2 8 8 9 2 8 7 8 8 2 8 8 9 2 8 7 8 8 2 8 8 9 2 8 7 8 8 9 2 8 7 8 8 9 2 8 7 8 8 9 2 8 7 8 8 9 2 8 7 8 8 9 2 8 7 8 8 9 2 8 7 8 9 2 8 7 8 9 2 8 7 8 9 2 8 7 8 9 2 8 7 8 9 2 8 9 9 2 8 7 8 9 2 8 9 9 2 8 9 9 2 8 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 2 9 9 2 9 9 2 9 9 2 9 9 2 9 2 9 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 9 2 2 9 2 9 2 2				I		2 825						2.705		2.673
23								1						$\begin{vmatrix} 2.578 \\ 2.626 \end{vmatrix}$
25				1		2.999						3.019		
26														2.99
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{20}{26}$	3												2.878 2.410
288	27	7												2.271
Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Separation   Sep						2.261	2.234	2.214	2.167	2.133	2.098	2.080		2.059
Courty Means   2.6769   2.6815   2.6878   2.6960   2.6936   2.6810   2.6508   2.6325   2.6259   2.6302   2.6370			2*356	2,390	2.434		2.24	2.606	2.602	2.607	2.630		2.673	2.699
1			2.348	2.330	2.315		2.248	2.221	2.174	2.143	2.129		$2.\overline{157}$	2.176
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Iourly Me	eans	2.6769	2.6812	2.6878	2.6960	2.6936	2.6810	2.6508	2.6325	2.6259	2.6302	2.6370	2.643
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	( ]	1	2.254	2.258	2.252	2.253	2.257	2:265	2:277	2:286	2:306	2:328	2:340	2.362
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	- 11		2.428	2.454	2.452	2.459	2.452	2.443	2.422	2.419	2.418		2.431
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					2.420									2:397
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		5												1.928
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	(	6					2 003	2 008	1 996	2 001	2 015		2 046	2.060
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$											2.591	2.589	2.582	2.281
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						2.528							2.649	2.683
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														2.430 2.837
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	1	3.093	3.112	3.141	3.155								3.023
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\Rightarrow$ $\frac{12}{12}$		3.012	3.053	3.037	3.047						3.021		3.029
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	AR 17		2.625	2.625	2.637		2:600	2:507	9:500	2:570	9.500		0:574	0.50
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\vec{\mathbf{p}} \langle \hat{\mathbf{i}}  $				2.860									$\frac{2.591}{2.791}$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Hg   16		2.744	2.747	2.772	2.784	2.778	2.768	2.745	2.723		2.710		2.703
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	H 1								2.735	2.733		2.736	2.744	2.755
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		- 11											2.779	$\frac{2.765}{2.397}$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	20	0			ļ <u> </u>	1.957			<u>~ 509</u>	- 401			∠ 428 —	4 001
$ \begin{bmatrix} 23 & 2 \cdot 552 & 2 \cdot 588 & 2 \cdot 608 & 2 \cdot 627 & 2 \cdot 631 & 2 \cdot 635 & 2 \cdot 625 & 2 \cdot 648 & 2 \cdot 648 & 2 \cdot 677 \\ 24 & 2 \cdot 890 & 2 \cdot 890 & 2 \cdot 910 & 2 \cdot 921 & 2 \cdot 923 & 2 \cdot 921 & 2 \cdot 909 & 2 \cdot 889 & 2 \cdot 875 & 2 \cdot 874 \\ 25 & 3 \cdot 091 & 3 \cdot 109 & 3 \cdot 118 & 3 \cdot 120 & 3 \cdot 119 & 3 \cdot 120 & 3 \cdot 106 & 3 \cdot 086 & 3 \cdot 066 & 3 \cdot 053 & 3 \cdot 051 \\ 26 & 2 \cdot 918 & 2 \cdot 920 & 2 \cdot 902 & 2 \cdot 883 & 2 \cdot 852 & 2 \cdot 827 & 2 \cdot 789 & 2 \cdot 744 & 2 \cdot 694 & 2 \cdot 656 & 2 \cdot 636 \\ 27 & - & - & 2 \cdot 645 & - & - & - & 2 \cdot 645 & - & - & - & 2 \cdot 666 & 2 \cdot 666 \\ 28 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 399 & 2 \cdot 359 & 2 \cdot 299 & 2 \cdot 267 & 2 \cdot 244 & 2 \cdot 184 & 2 \cdot 170 & 2 \cdot 165 & 2 \cdot 175 \\ 28 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 399 & 2 \cdot 359 & 2 \cdot 299 & 2 \cdot 267 & 2 \cdot 244 & 2 \cdot 184 & 2 \cdot 170 & 2 \cdot 165 & 2 \cdot 175 \\ 29 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 399 & 2 \cdot 359 & 2 \cdot 299 & 2 \cdot 267 & 2 \cdot 244 & 2 \cdot 184 & 2 \cdot 170 & 2 \cdot 165 & 2 \cdot 175 \\ 29 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 399 & 2 \cdot 359 & 2 \cdot 299 & 2 \cdot 267 & 2 \cdot 244 & 2 \cdot 184 & 2 \cdot 170 & 2 \cdot 165 & 2 \cdot 175 \\ 29 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 & 2 \cdot 487 &$						$2^{•}445$						2.558		2.571
$ \begin{bmatrix} 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 2 \\ 487 \\ 2 \\ 487 \\ 2 \\ 487 \\ 2 \\ 2 \\ 487 \\ 2 \\ 2 \\ 3 \\ 2 \\ 3 \\ 2 \\ 3 \\ 3 \\ 2 \\ 3 \\ 3$														2:474
$ \begin{bmatrix} 25 & 3 \cdot 091 & 3 \cdot 109 & 3 \cdot 118 & 3 \cdot 120 & 3 \cdot 119 & 3 \cdot 120 & 3 \cdot 106 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 086 & 3 \cdot 08$	24	4												2.697 2.892
	2.	5	3.091	3.109	3.118	3.120								3.040
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	$\frac{6}{7}$	2.918	2.920	2.902	2.883						2.656		2.635
177 8 7 780 1 7 7804 1 7 799 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	28	8				2.359						2.165	$\frac{-}{2.175}$	2.195
2 364 2 364 2 360 2 360 2 367 2 379 2 385 2 399 2 423 2 445	(29	9	2.580	2.304	2.328	2:340	2.360	2.367	2.379	2.382	2.399	2.423	2.445	2.450

^a The Observations made at 9 a.m. and 3 p.m. on Sunday are for the first time given in this Abstract: they are not included in the Means.

			Bar	ometer at 32			RESSURE.		Table.			
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
In. 2·241	In. 2.300	In. 2·301	In. 2.370	In. 2.368	In. 2.388	In. 2.678	In. 2.706	In. 2.728	In. 2.728	In. 2.714	$\left\{\begin{array}{c} \text{I n.} \\ 2.724 \end{array}\right\}$	In. 2:3975
2·581 2·990 2·226 2·646 2·579	2·573 3·000 2·257 2·650 2·554	2.573 3.002 2.323 2.652 2.549	2:559 2:979 2:397 2:652 2:518	2.575 2.981 2.471 2.650 2.510	2·575 2·956 2·507 2·644 2·490	2.581 2.954 2.524 2.622 2.480	2.591 2.920 2.550 2.644 2.430	2.617 2.904 2.576 2.653 2.414	2.619 2.868 2.614 2.653 2.384	2:642 2:816 2:610 2:651 2:365	2.661 2.804 2.701 2.645 2.345	2.6303 2.8983 2.3987 2.6586 2.5498
2°342 3°186 2°743 2°956 2°748 2°672 2°601	2:321 3:186 2:776 2:957 2:747 2:659 2:659	2:351 3:180 2:790 2:952 2:747 2:647 2:703	2:330 	2·298 	2·248 	2.859 3.118 2.830 2.896 2.740 2.496	2.881 3.100 2.848 2.876 2.740 2.486	2.907 3.072 2.880 2.866 2.742 2.456	2·925 3·044 2·908 2·853 2·741 2·448	2·933 3·021 2·893 2·840 2·729 2·406	2·958 } 3·014 2·908 2·823 2·734 2·368	2:4777 3:1047 2:8015 2:9418 2:7585 2:6332
2 · 904 3 · 090 3 · 076 2 · 671 2 · 606 2 · 631	2 · 874 3 · 122 3 · 050 2 · 653 2 · 622 2 · 649	2 *844 3 *133 3 *026 2 *661 2 *670 2 *668	2 · 805 3 · 143 2 · 996 2 · 613 2 · 712 2 · 688	2.775 3.148 2.952 2.587 2.724 2.691	2.721 3.156 2.896 2.565 2.751 2.697	2.639 2.649 3.159 2.862 2.544 2.778	2.632 2.638 3.173 2.858 2.531 2.785	2.632 2.567 3.201 2.868 2.515 2.811	2.622 2.517 3.212 2.853 2.481 2.824	2.634 2.501 3.226 2.825 2.457 2.823	2:642 } 2:495 3:251 2:814 2:426 2:825	2:5393 2:8053 2:9949 3:0732 2:6647 2:5786 2:7901
2.989 2.872 2.401 2.263 2.057 2.723	2.985 2.887 2.397 2.259 2.057 2.747	2.972 2.889 2.390 2.241 2.059 2.766	2.968 2.878 2.380 2.240 2.071 2.776	2.964 2.860 2.383 2.231 2.091 2.790	2.964 2.840 2.373 2.217 2.132 2.800	3.062 2.943 2.820 2.373 2.212 2.148	3.064 2.944 2.802 2.385 2.206 2.167	3.069 2.944 2.800 2.383 2.220 2.193	3.070 2.926 2.776 2.383 2.231 2.211	3 · 074 2 · 926 2 · 750 2 · 365 2 · 250 2 · 216	3.080 } 2.926 2.724 2.355 2.272 2.296	3:0022 2:8636 2:4701 2:2848 2:1597 2:5840
2.202	2.244	2.265	2.274	2.598	2.301	2.200 2.290	2.477 2.288	2:467 2:296	2.427 2.294	2:417 2:271	2.380 }	2 3040
2.6537	2.6610	2.6675	2.6673	2.6648	2.6606	2.6830	2.6816	2.6839	2.6774	2.6675	2.6701	2.6657
2:382 2:429 2:400 1:926 2:070	2:396 2:420 2:398 1:925 2:084	2·403 2·420 2·393 1·944 2·088	2:427 2:420 2:376 1:950 2:076	2.427 2.408 2.365 1.964 2.079	2.428 2.397 2.364 1.978 2.067	2:432 2:388 2:346 1:991	2:440 2:376 2:336 1:986	2:442 2:376 2:318 1:976	2:430 2:384 2:293 1:973	2:429 2:376 2:275 1:937	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2:3541 2:4166 2:3774 2:0138 2:1433
2·577 2·702 2·428 2·856 3·045 3·035	2.571 2.728 2.446 2.887 3.045 3.035	2·571 2·742 2·472 2·909 3·020 3·043	2·551 2·754 2·475 2·940 3·011 3·042	2·533 2·766 2·486 2·952 3·010 3·039	2·536 2·762 2·500 2·986 3·006 3·039	2:428 2:536 2:772 2:514 3:000 2:992	2:450 2:531 2:775 2:522 3:025 2:982	2:472 2:523 2:778 2:537 3:046 2:988	2:494 2:500 2:774 2:547 3:047 2:984	2 · 508 2 · 484 2 · 776 2 · 570 3 · 051 2 · 985	2:476 2:779 2:599 3:089 3:005	2:5598 2:6671 2:5533 2:8747 3:0558 2:9385
2.622 2.781 2.699 2.757 2.757 2.396	2.644 2.773 2.702 2.758 2.755 2.386	2.666 2.768 2.700 2.772 2.753 2.361	2.686 2.766 2.702 2.780 2.734 2.352	2.691 2.767 2.700 2.800 2.724 2.306	2.706 2.770 2.678 2.810 2.706 2.290	2.692 2.725 2.767 2.677 2.816 2.683	2.662 2.731 2.763 2.662 2.805 2.673	2.654 2.746 2.751 2.662 2.806 2.652	2:642 2:767 2:737 2:658 2:806 2:638	2.630 2.785 2.740 2.666 2.810 2.637	2.613 2.793 2.752 2.662 2.823 2.616	2 '6567 2 '8041 2 '7112 2 '7606 2 '7568 2 '3852
2:603 2:470 2:702 2:934 3:029 2:621	2.611 2.468 2.728 2.957 3.030 2.629	2.617 2.474 2.754 2.966 3.028 2.617	2.613 2.466 2.752 2.989 3.017 2.612	2.619 2.470 2.761 2.987 3.015 2.614	2.627 2.464 2.771 2.995 3.002 2.607	2.076 2.628 2.464 2.787 3.017 2.991	2·113 2·630 2·501 2·807 3·037 2·985	2:136 2:627 2:519 2:860 3:041 2:977	2:174 2:623 2:518 2:868 3:053 2:962	2:220 2:605 2:527 2:876 3:074 2:949	2·259 } 2·596 2·550 2·895 3·080 2·926 — 2·527 }	2:5475 2:5180 2:7150 2:9542 3:0412 2:6985
$ \begin{array}{c}     -2.195 \\     2.450 \end{array} $	2·199 2·504	2·199 2·528	2·199 2·555	2·173 2·561	2·173 2·567	2.644 2.171 2.565	2.642 2.181 2.575	2.622 2.198 2.581	2.606 2.217 2.591	2:566 2:230 2:600	2:527 } 2:262 2:635	2·2420 2·4655
2.5946	2.6032	2.6083	2.6098	2.6087	2.6092	2.6041	2.6076	2.6112	2.6114	2.6122	2.6188	2.6084

ours of Mean Göttingen	0	1	2	3	4	5	6	7	8	9	10	11
Ours of Mean Toronto	18	19	20	21	22	23	0	1	2	3	4	5
Time. $\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \end{pmatrix}$	In. 2 '663 3 '022 2 '445 2 '848	In. 2.700 3.020 2.445 2.846	In. 2.723 3.026 2.415 2.839	In. 2 '742 3 '017 2 '423 2 '833	In. 2.762 3.015 2.412 2.840	In. 2.765 3.002 2.407 2.818	In. 2.766 2.982 2.395 2.785	In. 2.749 2.946 2.379 2.737	In. 2.747 2.921 2.376 2.689	In. 2.755 2.894 2.396 2.676	In. 2.764 2.886 2.438 2.646	In. 2.811 2.856 2.486 2.623
5 6 7 8 9 10	2·597 2·704 2·245 2·642 2·517 2·700	2.611 2.712 2.227 2.684 2.508 2.714	2.612 2.696 2.225 2.692 2.526 2.731	2.615 2.683 2.203 2.708 2.517 2.744	2.614 2.650 2.173 2.712 2.495 2.746	2.608 2.612 2.164 2.723 2.492 2.749	2.609 2.579 2.139 2.720 2.488 2.747	2.600 2.534 2.114 2.688 2.459 2.741	2.595 2.482 2.127 2.696 2.453 2.722	2.603 2.450 2.125 2.665 2.458 2.714	2.619 2.421 2.207 2.666 2.482 2.713	2.626 2.390 2.216 2.666 2.507 2.716
MARCH. 112 133 144 155 166 177 188	2·570 2·768 2·922 2·954 2·660 2·429	2.591 2.782 2.938 2.960 2.659 2.431	2.608 2.784 2.970 2.956 2.670 2.417	2.622 2.775 2.976 2.949 2.689 2.429	2.634 2.768 2.970 2.946 2.671 2.426	2.640 2.752 2.960 2.931 2.652 2.423	2.656 2.736 2.947 2.905 2.635 2.418	2.653 2.731 2.927 2.857 2.631 2.400	2.668 2.732 2.906 2.817 2.614 2.405	2.692 2.740 2.905 2.792 2.591 2.414	2·713 2·759 2·912 2·774 2·576 2·394	2.731 2.783 2.929 2.766 2.554 2.415
19 20 21 22 23 24 25	2.692 2.348 2.712 2.734 2.928 2.734	2.686 2.416 2.716 2.756 2.942 2.728	2.700 2.436 2.723 2.778 2.952 2.716	2.629 2.458 2.734 2.782 2.962 2.691	2.604 2.473 2.725 2.802 2.954 2.669	2.615 2.501 2.723 2.792 2.935 2.645	2.570 2.504 2.708 2.827 2.948 2.641	2·486 2·520 2·700 2·828 2·920 2·607	2:442 2:517 2:685 2:806 2:903 2:586	2·356 2·533 2·661 2·808 2·896 2·551	2:335 2:544 2:653 2:810 2:906 2:541	2·272 2·566 2·641 2·815 2·893 2·503
$\begin{bmatrix} 26 \\ 27 \\ 28 \\ 29 \\ 30 \\ 31 \end{bmatrix}$	2.565 2.724 2.790 2.928 2.412	2·575 2·739 2·804 2·940 2·403	2·569 2·752 2·805 2·941 2·377	2·581 2·778 2·804 2·919 2·341	2·589 2·764 2·799 2·894 2·298	2·577 2·761 2·800 2·874 2·238	2.572 2.760 2.802 2.840 2.195	2.566 2.750 2.802 2.806 2.183	2.563 2.726 2.795 2.763 2.163	2:542 2:697 2:792 2:726 2:161	2.553 2.707 2.790 2.698 2.156	2.5698 2.698 2.807 2.673 2.158
lourly Means	2.6760	2.6864	2.6903	2.6890	2.6817	2.6726	2.6620	2.6413	2.6259	2.6146	2.6171	2.617
$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \end{pmatrix}$	2·571 3·048 2·745 2·954 2·870 2·843 2·774	2.629 3.056 2.750 2.967 2.873 2.849 2.792	2.659 3.059 2.750 2.984 2.872 2.868 2.780	2.704 3.074 2.758 2.992 2.862 2.886 2.771	2.725 	2.733 	2.752 3.024 2.736 2.955 2.838 2.885 2.706	2·761 3·001 2·734 2·944 2·819 2·867 2·685	2·812 2·956 2·730 2·934 2·796 2·855 2·660	2·831 2·938 2·740 2·912 2·774 2·833 2·649	2·860 2·920 2·744 2·904 2·765 2·826 2·638	2·876 2·889 2·754 2·882 2·765 2·799 2·631
10 11 12 13 14 15 16 17	2.633 2.590 2.801 2.337 2.446 2.648	2.658 2.618 2.792 2.351 2.458 2.667	2.640 2.672 2.777 2.330 2.487 2.676	2.626 2.638 2.751 2.325 2.503 2.688	2.621 2.636 2.740 2.307 2.511 2.673	2.600 2.644 2.709 2.307 2.531 2.666	2.582 2.632 2.662 2.307 2.541 2.650	2.566 2.656 2.625 2.311 2.552 2.656	2.547 2.661 2.595 2.341 2.556 2.647	2.524 2.628 2.563 2.351 2.556 2.642	2.508 2.640 2.520 2.363 2.565 2.635	2:500 2:638 2:504 2:377 2:584 2:636
18 19 20	2.952 2.784 3.030 2.976	2.960 2.771 3.038 2.974	2.962 2.761 3.069 2.973	2.962 2.751 3.089 2.955	2*962 2*759 3*088 2*935	2.950 2.770 3.082 2.904	2.934 2.788 3.061 2.848	2.905 2.804 3.069 2.812	2.887 2.802 3.060 2.776	2.883 2.801 3.041 2.730	2.877 2.819 3.028 2.699	2.861 2.845 3.022 2.694
21 a 22 23 24 25 26 27 28 29 30	2.599 2.429 2.684 2.725 2.949 2.911 2.471	2.619 2.439 2.686 2.748 2.963 2.916 2.523	2.635 2.459 2.689 2.756 2.978 2.916 2.582	2·643 2·459 2·701 2·768 2·989 2·902 2·638	2.659 2.451 2.697 2.779 2.994 2.862 2.670	2.651 2.494 2.682 2.777 2.979 2.850 2.704	2·652 2·488 2·633 2·775 2·963 2·830 2·726	2.645 2.498 2.617 2.781 2.946 2.790 2.752	2.633 2.515 2.580 2.777 2.934 2.740 2.769	2·620 2·529 2·561 2·777 2·916 2·715 2·779	2.614 2.535 2.540 2.787 2.923 2.674 2.788	2.621 2.551 2.536 2.798 2.909 2.659 2.806

			Ва	rometer at 8			PRESSURE es + the nu		e Table.			
12	13	14	15	16	17	18	19	20	21	22	23	Daily and
6	7	8	9	10	11	12	13	14	15	16	17	Monthly Means.
In. 2.837 2.833 2.534	In. 2.873 2.797 2.599	In. 2.873 2.769 2.638	In. 2 918 2 749 2 669	In. 2.935 2.706 2.703	In. 2.936 2.660 2.735	In. 2.940 2.629 2.757	In. 2.960 2.583 2.770	In. 2.966 2.537 2.782	In. 2 • 998 2 • 503 2 • 796	In. 2.479 2.821	In. 3.003 2.475 2.844	In. 2:8342 2:8045 2:5694
2.612 	2.602 	2.575 	2·565 — 2·701 2·370	2.557 — 2.710 2.366	2.538 	2.696 2.718 2.368	$\begin{bmatrix} -2.670 \\ 2.731 \\ 2.366 \end{bmatrix}$	2.638 2.723 2.346	2.621 2.695 2.340	2.610 2.694 2.320	$\left. \begin{array}{c} - \\ 2 \cdot 580 \\ 2 \cdot 704 \\ 2 \cdot 271 \end{array} \right\}$	2.6852 2.6534 2.4657
2·241 2·661 2·521 2·709	2·313 2·673 2·538 2·712	2:349 2:665 2:574 2:712	2·385 2·662 2·595 2·718	2·403 2·622 2·597 2·715	2.418 2.608 2.598 2.711	2:433 2:581 2:597	2.487 2.561 2.624	2.514 2.561 2.636	2:535 2:561 2:655	2:573 2:528 2:663	2.596 2.530 2.680	2:3088 2:6448 2:5492
2.751 2.751 2.798 2.945	2.770 2.824 2.949	2.774 2.827 2.957	$ \begin{array}{c cccc}  & - & \\  & 2.776 \\  & 2.849 \\  & 2.953 \end{array} $	2.776 2.850 2.945	2.768 2.852 2.950	2·394 2·769 2·860 2·946	2:466 2:771 2:862 2:940	2.498 2.773 2.862 2.946	2:508 2:755 2:867 2:946	2.518 2.759 2.880 2.942	2.544 $2.760$ $2.893$ $2.951$	2.6643 2.7075 2.8056 2.9430
2·742 2·551 2·431	2.745 2.516 2.454	2.738 2.506 2.490	2.728 2.491 2.504	2.726 2.486 2.532	2.738 2.472 2.530	$ \begin{array}{r} 2.742 \\ 2.466 \\ \\ 2.708 \end{array} $	2.726 2.467 — 2.699	2.695 2.444 	$ \begin{array}{c c} 2.674 \\ 2.426 \\ - \\ 2.709 \end{array} $	2.652 2.412  2.699	2.656 $2.429$ $2.703$	2.7987 2.5528 2.5076
2:242 2:600 2:619 2:821 2:889	2:219 2:635 2:617 2:830 2:887	2:217 2:652 2:616 2:849 2:859	2:170 2:675 2:654 2:846 2:846	2.188 2.674 2.664 2.845 2.824	2.200 2.692 2.666 2.856 2.818	2.204 2.690 2.666 2.854 2.790	2:210 2:692 2:670 2:857 2:796	2.210 2.678 2.689 2.859 2.773	2:216 2:671 2:678 2:876 2:753	2:248 2:675 2:691 2:890 2:744	2.258 2.688 2.708 2.913 2.754	2:3737 2:5766 2:6800 2:8264 2:8694
2.488 	2.464 2.594 2.683 2.847 2.633	2.456 2.623 2.675 2.857 2.584	2.452 2.635 2.658 2.886 2.545	2.425 2.628 2.650 2.904 2.513	2.425 2.632 2.668 2.911 2.499	2:549 2:640 2:667 2:912 2:499	2.528 2.648 2.681 2.899 2.493	2.520 2.654 2.705 2.900 2.470	2·521 2·673 2·701 2·926 2·458	2.521 2.684 2.709 2.929 2.438	$\begin{bmatrix}$	2.5618 2.6047 2.7122 2.8455 2.6753
2·137 2·6193	$\frac{2.111}{2.6270}$	2.108	2.130 $2.6342$	2.196	$\frac{2.251}{2.6379}$	$\frac{2.339}{2.6450}$	2.380	$\frac{2.415}{2.6487}$	$\frac{2.417}{2.6474}$	2.463	2.495	$\frac{2.2720}{2.6476}$
2.892	2.907	2.927	2.929	2.951	2.972						)	
2·865 2·758 2·882 2·768 2·793 2·628	2·861 2·788 2·900 2·778 2·796 2·624	2 · 867 2 · 797 2 · 903 2 · 801 2 · 806 2 · 625	2.860 2.837 2.896 2.807 2.793 2.627	2.850 2.829 2.896 2.809 2.783 2.626	2.848 2.834 2.888 2.802 2.777 2.626	3.040 2.838 2.856 2.874 2.814 2.784	3.035 2.822 2.856 2.859 2.804 2.788	3.031 2.804 2.856 2.869 2.814 2.807	3:026 2:775 2:870 2:863 2:813 2:790	3:036 2:759 2:892 2:866 2:813 2:777	3·035 } 2·743 2·925 2·866 2·826 2·770	2.8624 2.9152 2.7936 2.9143 2.8166 2.8234
2·492 2·652 2·470 2·393 2·592	2.527 2.658 2.457 2.401 2.601	2:543 2:683 2:442 2:419 2:613	2.551 2.698 2.430 2.418 2.607	2.554 2.704 2.402 2.419 2.610	2.548 2.714 2.370 2.416 2.612	2.611 2.557 2.730 2.347 2.417 2.610	2.609 2.551 2.746 2.313 2.415 2.592	2.600 2.547 2.757 2.291 2.415 2.585	2.604 2.543 2.764 2.297 2.424 2.602	2.608 2.550 2.770 2.306 2.425 2.608	2.609 } 2.578 2.767 2.322 2.426 2.628	2.6654 2.5644 2.6790 2.5202 2.3748 2.5646
2.642 2.853 2.871 3.013 2.694	2.648 2.845 2.899 3.011 2.677	2.657 2.853 2.924 3.011 2.692	2.666 2.829 2.928 3.012 2.694	2.677 2.816 2.936 3.011 2.693	2.693 2.806 2.940 3.005 2.691	2.829 2.792 2.950 3.004	2.841 2.794 2.940 2.990	2.852 2.776 2.955 2.990	2.884 2.789 2.972 2.986	2.900 2.775 2.978 2.980	2·926 } 2·776 2·981 2·966	2.7125 2.8666 2.8637 3.0273
2.620	2.626	2.647	2.641	2.638	2.646	2·461 —	2.492	2.206	2.217	2·529 —	2·555 }	2.7282 2.5661
2:561 2:522 2:802 2:909 2:639	2.563 2.491 2.811 2.913 2.588	2.575 2.481 2.826 2.911 2.534	2.588 2.479 2.840 2.918 2.549	2.610 2.475 2.842 2.932 2.536	2.619 2.503 2.852 2.934 2.482	2:327 2:620 2:533 2:853 2:918 2:462	2:330 2:628 2:577 2:864 2:918 2:444	2:361 2:623 2:605 2:874 2:914 2:425	2:376 2:623 2:636 2:895 2:916 2:433	2.388 2.637 2.654 2.905 2.915 2.433	2·395 } 2·654 2·701 2·925 2·919 2·437	2 5478 2 5478 2 5943 2 8140 2 9358 2 6553
2.806	2.832	2·857 —	2.861	2.863	2.876	2.763	2.757	2.739	2.732	2.700	$2.\overline{701}$	2.7373
2.7133	2.7168	2.7248	2.7274	2.7276	2.7273	2.7079	2.7069	2.7082	2.7137	2.7168	2.7263	2.7310

Götti	f Mean ngen ne.	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean	18	19	20	21	22	23	0	1	2	3	4	5
		In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
	, 1	2.681	2.683	2.663	2.659	2.643	2.630	2.613	2.605	2.251	2.567	2.557	2.24
	2	2.499	2.512	2.496	2.481	2.467	2.483	2.468	2.463	2.454	2.451	2.444	2.444
	3	2.452	2.443	2.444	2.453	2.446	2.438	2.428	2.416	2.393	2.374	2.370	2:36
	4	2.455	2.461	2.481	2.453	2.462	2.454	2.437	2.409	2.399	2.380	2.330	2,31
	5	2.310	2.306	2.309	2.306	2.312	2.309	2.300	2.285	2.235	2.245	2.254	2.25
	6	2.429	2.429	2.437	2.430	2.431	2.421	2.410	2.406	2.409	2.385	2.369	2.38
	7				2.363						2.359		
	8	2.620	2.620	2.620	2.621	2.610	2.597	2.587	2.555	2.552	2.530	2.521	2:50
	9	2.532	2.536	2.242	2.546	2.540	2.531	2.219	2.502	2.484	2.484	2.468	2:46
	10	$2.481 \\ 2.265$	2.487	2.494	2.485	2.476	2.480	2.458	2.452	2.436	2.420	$\begin{vmatrix} 2.410 \\ 2.315 \end{vmatrix}$	2.39
	$\begin{array}{c c} 11 \\ 12 \end{array}$	2.429	2.263 2.444	2.251	2.256	2.258	2.261	2.265	2:275	2.285	2.295	$\frac{2.315}{2.430}$	2.32 2.44
	$\frac{12}{13}$	2.395	2.385	2.463 2.349	2.480	2.479	2.468	2.457	2.451 2.146	2.432 2.172	2.440	2.430	2 44
	14	2 000	2 000	2 343	$2.277 \\ 2.701$	2.558	2.170	2'140	2 140	2 172	$\frac{2.200}{2.762}$	2 200	2 20
	15	2.861	$2.\overline{856}$	2.844	2.843	2.819	2.795	$2.\overline{754}$	2.724	2.688	2.632	2.2592	2.60
$\Xi$	16	$\frac{2.501}{2.578}$	2.592	2.596	2.601	2.605	$\frac{2}{2} \cdot \frac{793}{620}$	$\frac{2.734}{2.623}$	2.617	2.616	2.616	2.596	2.59
$\widetilde{\mathrm{MAY}}$	17	2.684	2.688	$\frac{2.694}{2.694}$	2.689	2.689	$\frac{2.620}{2.676}$	$\frac{2.623}{2.662}$	2.649	2.628	2.614	$\frac{2.598}{2.598}$	$\frac{2.58}{2.58}$
$\geq$	18	$\frac{2.671}{2}$	2.686	2.693	$\frac{2.003}{2.701}$	$\frac{2.003}{2.701}$	2.686	$\frac{2.662}{2.670}$	2.651	2.636	2.617	2.605	$\frac{1}{2} \cdot \frac{1}{60}$
	19	2.612	2.616	2.606	2.599	$\frac{2.761}{2.587}$	$\frac{2}{2} \cdot 577$	$\frac{2.570}{2.532}$	2.530	2.507	2.546	2.502	2.46
	20	2.452	2.469	2.469	2.470	2.469	2.476	2.462	2.437	2.427	2.431	2.426	2.43
	21				2.418						2.334		
	22	2.418	2.438	2.452	2.466	2.452	2.462	2.483	2.478	2.476	2.464	2.464	2.46
	23	2.504	2.517	2.528	2.512	2.513	2.508	2.492	2.494	2.462	2.440	2.429	2.40
	24	2.252	2.258	2.272	2.274	2.284	2.291	2.322	2.340	2.361	2.366	2.367	2:38
	25	2.495	2.209	2.25	2.514	2.519	2.214	2.499	2.490	2.476	2.465	2.469	2.46
	26	2.638	2.640	2.639	2.638	2.650	2.647	2.645	2.627	2.632	2.642	2.660	2.67
	27	2.829	2.850	2.850	2.857	2.831	2.825	2.822	2.795	2.773	2.757	2.752	2.74
	28				2.810						2.741		
	29	2.566	2.572	2.238	2.525	2.491	2.216	2.468	2.449	2.407	2.375	2:394	2,39
	30	2.356	2.360	2.363	2.358	2.374	2.372	2.364	2.363	2.398	2.425	2.440	2.45
	\31	2.628	2.642	2.658	2.659	2.663	2.657	2.639	2.633	2.633	2.624	2.612	2.59
ourl	y Means	2.219	2.5282	2.2589	2.5242	2.5185	2.2134	2.2007	2.4903	2.4801	2.4733	2*4668	2.46
	(1	2.691	2.705	2.728	2.726	2.718	2.705	2.691	2.662	2.650	2.645	2.644	2.63
	2	2.627	2.628	2.605	2.288	2.563	2.531	2.209	2.481	2.458	2.424	2.404	2.38
	3	2:377	2.404	2.414	2.412	2.421	2.426	2.428	2.412	2.411	2.388	2.388	2.38
	4	0.454	2.101		2.358		_				2.519		
	5	2.454	2.464	2.467	2.486	2.486	2.468	2.443	2.431	2.407	2.413	2.388	2:40
	6	$\begin{vmatrix} 2.576 \\ 2.778 \end{vmatrix}$	2.580	2.592	2.594	2.630	2.644	2.650	2.659	2.662	2.659	2.675	2.69
	7 8	2.800	2.788	2.796 2.807	2.791	2.777	2.761	2.750	2.743	2.736	2.736	2.733	$\frac{2.74}{2.69}$
	9	$\frac{2.600}{2.661}$	2.663	2.807 $2.653$	2.793	2.784	2.773	2.761	2.739	2.736	2.710	$2.710 \\ 2.508$	2·49
	10	2.503	2.21	$\frac{2.503}{2.509}$	2.641 2.506	2.626 2.486	2.608	2.583	2.550	2.532	$2.521 \\ 2.435$	$\begin{bmatrix} 2 & 508 \\ 2 & 428 \end{bmatrix}$	2·43
	11		- 511	2 003	2.663	400	2.481	2.469	2.461	2.458	2 433	440	Z 10
	12	2.913	2.917	2.912	$\frac{2.003}{2.907}$	2.900	2.892	2.880	2.863	2.840	2.820	2.813	2.80
	13	2.781	2.804	2.792	$\frac{2.307}{2.789}$	$\frac{2.300}{2.773}$	$\frac{2.592}{2.757}$	$\frac{2.580}{2.741}$	$\frac{2.803}{2.722}$	$\frac{2.701}{2.701}$	2.620 $2.697$	$\frac{2.613}{2.684}$	$\frac{2}{2} \cdot 67$
	14	2.640	2.640	2.670	$\frac{2.664}{2.664}$	2.665	$\frac{2.649}{2.649}$	2.611	$\frac{2.722}{2.592}$	2.548	2.535	2.201	$\frac{1}{2} \cdot \frac{3}{47}$
		2.529	2.230	2.231	2.534	2.523	$\frac{2.543}{2.507}$	2.2011	$\frac{2.392}{2.495}$	2.478	2.462	2.455	2.44
E.	15	2.558	2.557	2.555	2.544	2.545	$\frac{2.507}{2.525}$	2.508	2.497	$\frac{2}{2} \cdot 479$	2.461	2.449	2.43
INE.	( 16	11 - 000	2 001				2.470	2.451	2.445	2.427	2.423	2.406	2.40
JUNE.	$\begin{pmatrix} 16 \\ 17 \end{pmatrix}$	2.498	2.494	2.494	2.492	2.484	2 110			1	2.326		
JUNE.	$ \begin{vmatrix} 16 \\ 17 \\ 18 \end{vmatrix} $	2.498	2.494	2.494	2.371			-		_			2.43
JUNE.	\ \begin{pmatrix} 16 \\ 17 \\ 18 \\ 19 \end{pmatrix}	2·498 2·509	$\begin{vmatrix} 2.494 \\ - \\ 2.513 \end{vmatrix}$	2.494	2°371 2°514	2.218	2.520	2.200	2.481	2.454	2.448	2.439	
JUNE.	16 17 18 19 20	2·498 2·509 2·409	2·494  2·513 2·403	2.494  2.513 2.401	2:371 2:514 2:395	$\begin{bmatrix} -1 \\ 2.518 \\ 2.376 \end{bmatrix}$	2.520 2.349	2.343	2.325	2.292	2.448 2.253	2.238	2:30
JUNE.	16 17 18 19 20 21	2·498 2·509 2·409 2·296	2·494 2·513 2·403 2·313	2.494 2.513 2.401 2.322	2:371 2:514 2:395 2:315	$\begin{vmatrix} - \\ 2.518 \\ 2.376 \\ 2.319 \end{vmatrix}$	2.520 2.349 2.343	2°343 2°355	2·322 2·369	2.292 2.378	2:448 2:253 2:396	2.238 2.400	2:30 2:40
JUNE.	\begin{pmatrix} 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \end{pmatrix}	2.498 2.509 2.409 2.296 2.498	2·494 2·513 2·403 2·313 2·498	2 · 494 2 · 513 2 · 401 2 · 322 2 · 510	2:371 2:514 2:395 2:315 2:496	2.518 2.376 2.319 2.505	2:520 2:349 2:343 2:495	2:343 2:355 2:492	2:322 2:369 2:493	2:292 2:378 2:486	2:448 2:253 2:396 2:474	2·238 2·400 2·474	2:30 2:40 2:46
JUNE.	\begin{pmatrix} 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \end{pmatrix}	2·498 2·509 2·409 2·296 2·498 2·298	2·494 	2.494 2.513 2.401 2.322 2.510 2.222	2:371 2:514 2:395 2:315 2:496 2:213	2.518 2.376 2.319 2.505 2.202	2·520 2·349 2·343 2·495 2·189	2:343 2:355 2:492 2:180	2:322 2:369 2:493 2:168	2 · 292 2 · 378 2 · 486 2 · 197	2:448 2:253 2:396 2:474 2:236	2:238 2:400 2:474 2:258	2:30 2:40 2:46 2:31
JUNE.	\begin{pmatrix} 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \end{pmatrix}	2.498 2.509 2.409 2.296 2.498	2·494 2·513 2·403 2·313 2·498	2·494 2·513 2·401 2·322 2·510 2·222 2·595	2:371 2:514 2:395 2:315 2:496 2:213 2:604	2.518 2.376 2.319 2.505	2:520 2:349 2:343 2:495	2:343 2:355 2:492 2:180 2:617	2:322 2:369 2:493	2:292 2:378 2:486	2:448 2:253 2:396 2:474 2:236 2:614	2·238 2·400 2·474	2:30 2:40 2:46 2:31 2:63
JUNE.	\begin{pmatrix} 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \end{pmatrix}	2·498 	2·494 — 2·513 2·403 2·313 2·498 2·257 2·576	2·494 	2:371 2:514 2:395 2:315 2:496 2:213 2:604 2:669	2·518 2·376 2·319 2·505 2·202 2·615	2·520 2·349 2·343 2·495 2·189 2·623	2:343 2:355 2:492 2:180 2:617	2:322 2:369 2:493 2:168 2:616	2·292 2·378 2·486 2·197 2·617	2:448 2:253 2:396 2:474 2:236 2:614 2:608	2·238 2·400 2·474 2·258 2·626	2:30 2:40 2:46 2:31 2:63
JUNE.	\begin{aligned} \ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \\ 26 \end{aligned} \end{aligned}	2·498 2·509 2·409 2·296 2·498 2·298 2·568 — 2·673	2·494 	2.494 2.513 2.401 2.322 2.510 2.222 2.595 — 2.684	2:371 2:514 2:395 2:315 2:496 2:213 2:604 2:669 2:702	2.518 2.376 2.319 2.505 2.202 2.615 2.693	2·520 2·349 2·343 2·495 2·189 2·623 — 2·689	2:343 2:355 2:492 2:180 2:617 ————————————————————————————————————	2:322 2:369 2:493 2:168 2:616 — 2:665	2 · 292 2 · 378 2 · 486 2 · 197 2 · 617 — 2 · 651	2:448 2:253 2:396 2:474 2:236 2:614 2:608 2:634	2·238 2·400 2·474 2·258 2·626 2·610	2:30 2:40 2:46 2:31 2:63 
JUNE.	\begin{pmatrix} 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \end{pmatrix}	2·498 	2·494 — 2·513 2·403 2·313 2·498 2·257 2·576	2·494 	2:371 2:514 2:395 2:315 2:496 2:213 2:604 2:669 2:702 2:543	2.518 2.376 2.319 2.505 2.202 2.615 — 2.693 2.535	2·520 2·349 2·343 2·495 2·189 2·623 — 2·689 2·525	2:343 2:355 2:492 2:180 2:617 — 2:687 2:498	2:322 2:369 2:493 2:168 2:616 — 2:665 2:488	2:292 2:378 2:486 2:197 2:617 — 2:651 2:469	2:448 2:253 2:396 2:474 2:236 2:614 2:608 2:634 2:444	2·238 2·400 2·474 2·258 2·626 2·610 2·422	2:30 2:40 2:46 2:31 2:63
JUNE.	\( \begin{array}{c} 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 29 \end{array} \)	2·498 2·509 2·409 2·296 2·498 2·568 2·673 2·571 2·535 2·648	2·494 — 2·513 2·403 2·313 2·498 2·257 2·576 — 2·672 2·563	2.494 	2:371 2:514 2:395 2:315 2:496 2:213 2:604 2:669 2:702 2:543 2:580	2.518 2.376 2.319 2.505 2.202 2.615 — 2.693 2.535 2.594	2 · 520 2 · 349 2 · 343 2 · 495 2 · 189 2 · 623 2 · 689 2 · 525 2 · 602	2:343 2:355 2:492 2:180 2:617 ————————————————————————————————————	2:322 2:369 2:493 2:168 2:616 ———————————————————————————————————	2:292 2:378 2:486 2:197 2:617 ————————————————————————————————————	2:448 2:253 2:396 2:474 2:236 2:614 2:608 2:634 2:444 2:584	2·238 2·400 2·474 2·258 2·626 2·610	2:30 2:40 2:46 2:31 2:63 
JUNE.	\ \begin{array}{c} 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \end{array}	2·498 2·509 2·409 2·296 2·498 2·298 2·568 2·673 2·571 2·535	2·494 	2 · 494 	2:371 2:514 2:395 2:315 2:496 2:213 2:604 2:669 2:702 2:543	2.518 2.376 2.319 2.505 2.202 2.615 — 2.693 2.535	2·520 2·349 2·343 2·495 2·189 2·623 — 2·689 2·525	2:343 2:355 2:492 2:180 2:617 — 2:687 2:498	2:322 2:369 2:493 2:168 2:616 — 2:665 2:488	2:292 2:378 2:486 2:197 2:617 — 2:651 2:469	2:448 2:253 2:396 2:474 2:236 2:614 2:608 2:634 2:444	2:238 2:400 2:474 2:258 2:626 —————————————————————————————————	2:30 2:40 2:46 2:31 2:63 

			Ba	rometer at {	BAROI 32° = 27 E	METRIC P	RESSURE. s + the nu	nbers in the	Table.			
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
2.545 $2.414$	2.545 2.446	2.545 2.446	2.562 2.453	2.568	2.535	2.531	2.510	2.508	2.498	2.470	2.479	2:5723 2:4531
2:370	2.376	2.394	2.414	$2.445 \\ 2.425$	$\begin{vmatrix} 2.438 \\ 2.425 \end{vmatrix}$	2.427 2.428	2.405 2.440	$\begin{vmatrix} 2.419 \\ 2.455 \end{vmatrix}$	2.420 2.462	$2.430 \\ 2.458$	2.440 2.441	2.4331 $2.4212$
$\frac{2.278}{2.278}$	2.270	2.242	2.48	$\frac{2.420}{2.230}$	$\frac{2.425}{2.216}$	$\frac{2}{2} \cdot \frac{420}{210}$	$\frac{2.310}{2.206}$	2.207	$\frac{2.402}{2.230}$	$\frac{2.450}{2.250}$	2.591	2.3297
2.278	2.308	2.395	2.330	2.390	2.377	2.386	2.386	2.368	2.361	2.385	2.409	2.3246
2.380	2.368	2:377	2.392	2.409	2.426						— i	2.4424
						2.233	2.542	2.544	2.550	2.557	2.604	l
2.496 2.489	$2.481 \\ 2.454$	2.506	2.214	2.506	2.497	2.495	2.500	2.500	2.501	2:504	2.526	2.2402
5.395	$\frac{2.454}{2.392}$	2.486 2.376	2.494 2.379	$2.487 \\ 2.357$	$2.475 \\ 2.344$	2.467 2.338	$2.471 \\ 2.326$	2.469 2.305	2.466 2.296	$2.464 \\ 2.268$	2.480 2.262	2.4939 2.3962
2.354	$\frac{2.332}{2.334}$	$\frac{2}{2} \cdot 344$	2.343	2.343	2.338	$\frac{2.339}{2.339}$	2.353	2.354	2.360	$\frac{2}{2} \cdot \frac{208}{382}$	2.409	2.3139
2.445	2.452	2.452	2.458	$\frac{2.343}{2.464}$	$\frac{2.333}{2.447}$	2.446	$\frac{2}{2} \cdot 455$	2.430	2.418	$\frac{2.302}{2.409}$	2.393	2.4453
2.297	2.367	2.405	2.427	2.456	2.470				_			
						2.834	2.838	2.840	2.846	2.857	$2.\overline{847}$	2.4350
2.583	2.585	2.565	2.547	2.545	2.537	2.217	2.515	2.213	2.524	2.538	2.548	2.6469
2.617	2.621	2.631	2.649	2.653	2.650	2.642	2.647	2.647	2.648	2.659	2.667	2.6245
2:589 2:602	2.599 2.596	2.605 2.588	2.610	2.611	2.610	2.628	2.625	2.621	2.639	2.648	2.661 2.596	2.6376
2.469	2 396	$2.588 \\ 2.473$	2.586 2.482	2.585 2.482	2.608 2.464	2.609 2.462	2.624 2.441	2.621 2.429	$2.615 \\ 2.417$	2.430	2 396	2.6317 2.5061
$\frac{2}{2} \cdot 417$	2.413	2.451	$\frac{2.462}{2.462}$	2.452	2.446			— U	<u> </u>		j	i
						2.352	2.340	2.346	2.340	2.352	$ 2 \cdot 364 $	2.4231
2.473	2.467	2.474	2.483	2.489	2.476	2.480	2.483	2.467	2.479	2.489	2.496	2.4697
2.389	2.379	2.353	2.350	2.322	2.298	2.285	2.276	2.245	2.555	2.268	2.248	2:3930
2.427	2.427	2.427	2.458	2.448	2.456	2.460	2.460	2.469	2.465	2.465	2.488	2.3841
2.500	2.213	2.527	2.543	2.562	2:578	2.580	2.597	2.604	2.612	2.622	2.634	2.5340
$2.678 \\ 2.751$	$2.694 \\ 2.754$	$2.706 \\ 2.756$	2.725	$\begin{vmatrix} 2.737 \\ 2.776 \end{vmatrix}$	2.757	2.767	2.768	2.782	2.782	2.795	2.495	2.6962
- 101 	2 (04	2 750	2.769	2 110	2.779	2.612	2.611	2.613	2.592	2.592	$\left[\frac{-}{2\cdot 591}\right]$	2.7448
2*395	2.399	2.405	2.410	2.410	2.415	2.417	2.417	2.424	2.427	2.362	2.351	2.4387
2.467	2.480	2.487	2.496	2.518	2.539	2.521	2.545	2.562	2.572	2.593	2.616	2.4592
2.603	2.604	2.603	2.620	2.614	2.624	2.633	2.648	2.652	2.661	2.672	2.689	2.6361
2.4703	2.4738	2.4821	2.4891	2.4921	2.4898	2.4961	2 4974	2.4960	2.4964	2.2010	2 5099	2.4961
2.633	2.627	2.631	2.644	2.633	2'634	2.638	2.644	2.633	2.635	2.628	2.634	2.6588
2.376	2.376	$\frac{2.376}{2.376}$	$\frac{2.370}{2.370}$	$\frac{2}{2} \cdot 371$	2.381	2.381	2.370	2.370	2.370	2.378	2.377	2.4456
2.390	2.388	2.412	2.417	2.419	2.419	_			_	_	— ì	Ħ
					_	2.358	2.370	2.392	2.405	2.413	2.436	11
2.439	2.439	2.454	2.462	2.468	2.468	2.490	2.525	2.525	2.532	2.545	2.574	2.4678
2.707	2.713	2.723	2.738	2.732	2.731	2.729	2.739	2.749	2.756	2.756	2.770	2.6856
2.747 2.697	2.757	2.761	2.735	2.737	$2.760 \\ 2.705$	2.753	2.756	2.763	$\begin{vmatrix} 2.771 \\ 2.667 \end{vmatrix}$	2.776	$\begin{vmatrix} 2.788 \\ 2.650 \end{vmatrix}$	$2.7598 \ 2.7224$
2.499	2.699 2.501	2.701 2.494	$2.710 \\ 2.495$	$\begin{vmatrix} 2.714 \\ 2.495 \end{vmatrix}$	2.497	2.689 2.498	2.666 2.500	$\begin{vmatrix} 2.667 \\ 2.501 \end{vmatrix}$	2.478	$2.655 \\ 2.478$	2.495	2.5404
2.442	$\frac{2.301}{2.454}$	2.460	2.468	2.453	$2.497 \\ 2.512$	4 190		2 301		2 410		}
		l —		l —	_	2.795	2.829	2.827	2.843	2.860	$\left  \frac{-}{2 \cdot 891} \right\}$	2.2641
2.809	2.781	2.773	2.784	2.793	2.798	2.791	2.771	2.768	2.758	2.759	2.775	2.8261
2.678	2.680	2.660	2.662	2.667	2.667	2.652	2.651	2.629	2.622	2.630	2.633	2.6979
2.452	2.454	2.467	2.459	2.496	2.496	2.485	2.483	2.480	2.478	2.483	2:507	2.5387
2.456 2.428	2.468	2.479	2.487	2.490	2.494	2:497	2.218	2.506	2.210	2.523	2.550	2.4988
$\frac{2.428}{2.397}$	2.452 $2.390$	2.473 2.396	2.495 2.390	2.506 2.396	$2.517 \\ 2.382$	2.206	2.498	2.488	2.482	2.483	2.494	2.4974
	2 030	2 030	2 390	2 000	2 002	2.439	2.458	2.459	2.464	2.464	$\left  \frac{-}{2 \cdot 486} \right $	2.4420
2.437	2.436	2.428	2.434	2.430	2.414	2.408	2.410	2.412	2.407	2.404	2.405	2.4530
2.216	2.232	2.263	2.302	2.255	2.269	2.266	2.270	2.259	2.252	2.235	2.267	2.2990
2.423	2.457	2.460	2.470	2.463	2.442	2.449	2.445	2.475	2.482	2.496	2.489	2.4066
2.463	2.478	2.470	2.474	2.461	2.451	2.442	2.433	2.409	2.381	2:369	2.336	2.4605
$2.345 \\ 2.643$	2.377	2.398	2.438	2.448	2.465	2.475	2.493	2.202	2.210	2.222	2.236	2:3437
	2.661	2.662	2.669	2.669	2.661	2.649	2.653	2.661	$2.\overline{654}$	2.666	$\left[ 2.\overline{673} \right]$	2.6345
$\frac{-}{2.586}$	2.572	2.575	2.607	2.612	2.610	2.600	$\frac{2.583}{2.583}$	$\frac{2.589}{2.589}$	2.584	$\frac{2.569}{2.569}$	2.564	2.6252
2.428	2.463	$\frac{2.471}{2.471}$	2.478	$\frac{2.012}{2.492}$	$\frac{2.010}{2.487}$	2.490	2.482	2.491	2.491	2.499	2.233	2.4933
2.597	2.598	2.602	2.611	2.616	2.621	2.628	2.618	2.618	2.621	2.627	2.633	2.5973
2.580	2.580	2.572	2.570	2.571	2.574	2.565	2.261	2.260	2.550	2.542	2.535	2.5956
2.406	2.424	2.411	2.419	2.414	2.428	2.428	2.428	2.432	2.460	2.475	2.219	2.4720
2.2102	2.5176	2.5220	2.5303	2.5316	2.5340	2.5423	2.5444	2.5449	2.5447	2.5476	2.5596	2.5435

					SI	TANDARD	THERMO	METER.	· · · · · · · · · · · · · · · · · · ·				
Hours o Göttii Tin	f Mean ngen ne.	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean )	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	28.5 36.4 29.9	29°2 36°5 30°3	29.6 37.2 30.3	30°8 37°6 31°1	31.8 31.8	32°9 37°9 33°9	32·4 36·7 35·0	32·7 36·7 35·5	32·2 36·3 35·9	32°4 35°9 35°9	33·2 35·5 35·6	34·2 35·4 35·3
	$egin{array}{c c} 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ \end{array}$	28.4 26.5 34.7 33.5 28.4 29.2	28°3 30°1 34°7 33°9 28°0 30°1	27.6 30.6 35.0 34.1 27.4 30.3	29°9 32°0 35°9 34°1 27°5 30°6	32.7 32.9 36.0 33.9 27.9 30.6	32.7 33.6 36.5 34.1 27.5 30.7	34.3 34.4 36.7 33.9 27.2 30.8	35.7 34.4 36.6 33.8 28.6 32.0	35.7 34.4 36.2 34.1 29.1 31.8	35°1 34°5 36°5 33°9 29°1 31°2	34.8 32.8 35.6 33.5 30.2 29.9	33·1 32·7 35·0 33·1 30·7 29·5
JANUARY.	11 12 13 14 15 16 17	25°0 9°5 28°4 18°4 30°6 11°6	25.0 9.7 28.1 24.5 31.0 10.7	24.9 12.0 27.8 28.7 31.1 9.7	24.6 13.0 28.7 32.0 31.4 8.8	24.6 17.8 29.9 34.1 31.8 10.1	26°1 20°6 32°0 35°4 31°8 10°5	26.7 23.5 33.3 37.3 29.9 10.5	27 ¹ 24 ¹ 33 ⁹ 29 ⁰ 28 ⁴ 10 ⁰	26.7 24.3 34.8 40.1 28.0 10.9	25°3 24°0 35°0 40°5 26°7 12°5	24.4 23.4 34.6 38.4 26.1 10.3	23.7 21.3 32.5 38.8 25.4 9.2
J	18 19 20 21 22 23 24	7.1 $9.5$ $21.9$ $-0.7$ $6.6$ $20.2$	$ \begin{array}{r}  - \\  6.9 \\  9.5 \\  22.1 \\  - 0.2 \\  6.0 \\  19.2 \end{array} $	6.9 9.7 22.3 - 0.8 4.9 20.8	8'4 10'9 22'0 2'7 9'5 22'9	11.6 14.5 21.7 6.4 13.9 26.3	13.4 15.2 22.7 9.5 17.4 29.0	14.8 17.3 22.7 12.4 19.2 31.0	14.8 20.0 23.2 16.6 20.2 31.4	15.2 21.6 24.6 18.8 20.8 32.9	15.8 22.0 25.1 18.9 21.9 34.9	16.2 22.0 25.6 18.8 22.3 34.7	14'3 22'1 25'5 17'1 20'8 33'5
Feb.	25 26 27 28 29 30 31	33°9 18°2 31°2 33°5 37°2 18°4	34°3 15°8 31°9 34°0 37°4 15°8	34.7 15.0 32.3 34.4 36.3 14.1	35.4 17.0 32.7 34.4 37.8 12.2	38.8 18.5 33.7 35.4 39.4 12.0	38.6 20.1 35.8 36.2 38.8 14.1	37.0 21.9 36.8 37.3 39.5 16.7	37.5 22.7 36.8 36.8 41.0 16.7	37.5 23.2 37.9 35.8 41.2 19.5	37.5 23.7 37.3 35.2 40.8 19.9	36.6 22.7 35.9 35.6 40.6 19.7	35.4 22.3 35.2 35.6 40.4 19.0
Hourly	Means	23.22	23.81	23.96	24.96	26.55	27.67	28.20	29.12	29.61	29.68	29.22	<b>2</b> 8.56
FEBRUARY.	2 3 4 5 6 7 8 9 10 11 12 13 14	19°2 29°7 28°8 34°9 24°0 25°5 — 17°3 3°6 21°3 — 2°8 24°7 15°6	21.5 30.7 29.0 36.1 24.4 24.8 — 13.2 4.5 22.9 — 5.2 25.5 18.6	$\begin{array}{c} 21.9 \\ 32.7 \\ 29.2 \\ 35.5 \\ 27.1 \\ 25.0 \\ -12.1 \\ 4.9 \\ 19.8 \\ -5.4 \\ 27.0 \\ 21.1 \\ \end{array}$	23.7 36.2 30.6 38.6 29.0 34.3 — 11.9 9.3 18.6 5.9 29.1 23.8	26.0 36.8 31.8 39.4 34.1 37.5 ————————————————————————————————————	28·1 38·1 33·3 38·6 36·2 39·7 ————————————————————————————————————	29°3 39°4 34°1 38°4 38°6 39°5 — 13°3 21°6 18°4 16°2 33°1 34°0	29'9 39'8 35'2 39'5 38'3 39'4 13'9 21'9 18'6 18'9 33'7 34'4	30°2 41°3 36°0 38°6 38°9 38°4 ————————————————————————————————————	30°2 40°8 36°0 37°2 39°0 37°4 — 15°0 24°8 18°8 22°2 35°2 33°7	29 · 9 40 · 2 35 · 2 35 · 8 38 · 6 37 · 8 	29.7 40.0 34.5 35.1 36.5 37.0 — 13.7 24.7 17.5 20.5 35.2 32.0
FEBRI	15 16 17 18 19 20 21 22	21.4 18.4 10.7 6.4 24.5 25.5	21.3 19.2 11.3 11.8 24.7 26.1	21.5 20.2 15.6 11.6 25.1 27.1	21.7 23.6 16.6 19.6 25.9 28.8	25.5 25.9 23.6 27.2 26.3 30.6	26.5 28.6 24.2 27.7 26.5 31.0	26.1 30.1 25.3 28.3 26.3 31.6	26.9 29.7 26.1 29.2 26.8 30.8	26.3 30.1 26.9 28.9 28.1 29.0	26.1 31.0 27.6 26.9 30.3 29.9	25.7 29.7 26.7 28.2 29.7 28.6	24·4 27·4 25·5 27·4 28·0 26·1
Mar	23 24 25 26 27 28	12.4 11.6 0.3 -11.2 -12.1 11.3	15.4 10.2 1.8 - 9.8 - 3.4 11.8	16.6 12.6 3.6 - 5.6 - 9.5 12.4 -	21.1 15.6 7.8 0.8 1.4 14.9	23.8 17.3 10.9 1.9 7.0 16.7	24.7 18.0 14.1 3.9 11.3 18.3	25·4 22·7 16·6 5·8 14·0 18·5	24.7 23.8 16.4 7.2 15.2 17.7	25.4 20.4 17.2 8.4 15.8 18.1	25°1 20°1 16°5 7°4 15°0 19°4	23.6 18.8 15.5 6.0 14.5 19.2	20.0 16.4 14.0 4.9 13.0 18.5
Hourl	y Means	15.04	16.10	16.72	20:37	23.12	24.68	26.11	26.28	26.02	26.90	26.26	25.08

					STANDA	ARD THEI	RMOMETE	R.				
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
34.6 35.4 34.9	35°0 34°4 34°5	35·4 33·1 34·2	35·2 32·8 33·3	35.6 32.5 32.4	35.8 32.4 31.6	35.6 29.6	35·4 29·2 —	35.4 29.0	35.8 29.0	36·2 28·8	$37.3 \\ 29.5 \\ -26.7$	33.63 34.03 32.99
30.8 33.5 34.7 32.3 31.0 29.5	28.4 34.7 34.7 32.0 30.0 29.9	28·2 34·1 35·2 30·8 29·6 30·3	28.8 33.7 35.2 30.1 29.2 30.4	29°0 33°1 34°9 29°8 28°7 31°2	28°2 33°1 35°1 29°8 28°6 31°0	32.7 28.0 33.5 35.2 29.5 28.6	33.8 25.9 33.9 36.1 29.2 28.6	33.7 25.1 33.9 35.4 29.0 28.4	31 · 9 24 · 4 34 · 7 35 · 1 29 · 1 29 · 2	31.6 23.6 34.7 34.1 29.0 29.9	26'3 33'7 33'8 28'5 29'9	29.79 33.15 35.37 31.88 28.89 29.48
22.6 20.2 31.3 40.0 24.8 8.0	22.0 16.3 26.3 40.0 24.3 8.8	21·1 22·2 25·0 39·5 23·3 8·0	19.9 22.8 29.5 37.2 22.3 7.4	18:3 22:5 28:6 38:2 21:5 6:0	16:4 22:7 28:4 37:1 20:0 4:3	27·4 14·8 24·2 25·9 36·6 19·0	27·1 14·3 24·4 20·4 35·8 17·5	26.6 13.7 25.9 22.1 34.3 15.8	26.1 13.3 26.9 20.0 33.7 15.4	26.1 12.0 27.4 19.4 32.4 13.4	25:3 } 10:5 28:5 18:8 30:6 11:6	20°96 21°13 28°11 35°11 24°21 9°18
12°1 21°9 24°2 15°4 20°0 32°7	11.6 22.9 23.0 14.5 18.8 31.0	10°1 23°3 20°6 13°7 18°2 31°4	8'9 25'0 17'1 13'2 16'5 32'2	8.0 24.7 13.5 13.0 16.0 32.0	7:0 24:7 11:6 12:6 14:9 33:5	10.5 5.7 21.8 8.8 9.7 13.3	9.9 5.9 21.9 6.0 12.1 11.8	9.0 7.2 21.9 3.3 7.7 11.4	8:4 7:3 22:1 1:2 6:5 15:9	7·9 7·5 22·3 1·0 4·4 16·4	$     \begin{array}{r}       7 \cdot 4 \\       8 \cdot 2 \\       21 \cdot 9 \\       - 0 \cdot 4 \\       2 \cdot 9 \\       17 \cdot 3 \\       - \end{array} $	10·20 19·53 17·05 10·22 15·58
33.9 22.7 34.9 36.4 39.9 17.5	33°1 25°3 34°5 36°4 39°8 15°3	31.8 27.8 34.7 36.4 40.9 14.2	31.1 26.9 34.0 37.1 40.2 13.7	30.6 28.0 33.7 36.3 38.2 11.6	29.7 29.2 33.3 36.2 36.9 10.5	32.4 28.4 29.5 33.1 36.4 36.0	31.8 28.2 28.8 31.7 37.1 33.0	31.6 26.9 29.0 31.9 36.1 28.8	31.6 23.4 29.2 32.2 36.7 25.2	33°1 21°3 29°0 32°4 36°1 22°3	$\begin{bmatrix} - \\ 33.5 \end{bmatrix}$ $\begin{bmatrix} 19.2 \\ 30.4 \\ 33.1 \\ 36.7 \\ \end{bmatrix}$	32·28 24·04 34·04 35·92 36·30 15·85
27:97		27.15				16.9	17.6	15'4	16.0	23.27	$\frac{-17\cdot7}{22\cdot91}$	26.56
21 91	27.31	27 15	26.80	26.22	25.72	24.93	24.72	24.02	23.71	20 21	22 31	20 20
29.5 38.6 35.2 34.6 34.9 37.1	29.9 38.0 35.6 34.1 34.5 32.7	29.9 36.8 36.4 32.4 34.2 29.0	31'4 35'4 37'2 32'1 33'9 23'2	32.0 35.2 39.2 31.4 34.2 20.2	31.8 33.6 39.5 31.2 31.2 18.2	30.6 32.4 38.7 30.7 30.3	30°3 31°9 37°4 28°6 28°2	30.8 31.4 37.2 28.2 27.6	31.0 30.1 36.5 27.8 26.5	31·2 29·7 36·2 26·9 26·5	29.9 29.5 35.2 25.3 25.3 	28.66 35.35 34.92 33.79 32.17 29.20
11:3 25:0 17:3 18:8 30:3 31:8	9.9 25.7 16.4 18.5 31.0 31.0	8'4 26'5 14'8 17'8 32'0 29'7	7'4 25'0 14'1 17'7 30'6 29'5	7:4 25:8 13:4 18:0 29:8 29:7	6.9 26.9 12.6 19.6 25.0 28.0	21·3 4·9 26·4 11·3 19·7 19·8	21·1 4·7 25·5 11·2 21·5 16·0	20.8 4.7 22.7 11.1 22.5 14.3	20.6 3.9 22.3 3.5 23.4 13.0	20.5 3.6 21.6 -1.4 23.8 13.5	3.5 21.5 - 1.6 24.4 15.3 - 21.3	10.08 20.26 14.73 15.89 26.97
22.8 25.4 17.9 28.1 27.1 25.0	22.9 24.3 13.2 28.7 25.9 25.0	22.9 23.7 10.7 25.0 23.6 23.4	21.9 22.9 10.7 25.5 25.5 23.2	21.5 22.5 10.1 25.5 26.3 20.9	20.4 21.3 9.9 25.5 26.3 20.0	18.0 18.8 21.1 8.4 25.7 24.6	19.6 18.4 19.4 6.4 25.1 25.7	20·4 20·0 18·2 7·3 24·2 25·7	21·1 20·2 10·1 6·0 24·0 26·2	21 · 4 20 · 6 6 · 1 5 · 7 24 · 0 26 · 7	20.2 4.1 5.5 24.3 26.6 -13.1}	22.67 22.21 15.50 24.12 26.35 24.01
19.8 14.2 13.0 2.7 11.8 17.8	18.8 10.7 10.9 - 0.1 11.1 17.3	17.2 8.9 8.2 - 0.2 11.1 16.6	16.2 7.2 5.5 - 8.9 11.0 16.4	17.0 5.3 5.9 -11.0 10.7 16.0	15 · 4 3 · 1 5 · 1 -12 · 8 10 · 5 15 · 1	17.1 15.4 4.3 0.2 -14.5 10.7	17·3 14·5 6·4 0·0 -15·3 11·0	16.4 14.5 3.9 - 1.0 -15.8 11.1	15.7 12.4 2.3 0.0 -16.2 11.0	14.1 11.6 0.8 - 1.6 -12.2 11.8	11.6 0.4 - 9.8 -10.4 11.6	18:44 11:46 7:11 - 3:96 8:98 16:04
						16'4	15.6	14.8	14.2	13.9	13.7}	
23.75	22.75	21*63	20.61	19.46	19.33	18.02	19.23	16.13	16.08	15.62	14.18	20.86

Vol. III.

					S.	randari	THERM	OMETER.					
Iours o Göttii Tim	f Mean	0	1	2	3	4	5	6	7	8	9	10	11
lours o Toro Tin		18	19	20	21	22	23	0	1	2	3	4	5
	2 3 4 5 6 7 8	13.2 9.5 14.0 32.0 28.0 10.3	14.3 10.3 20.1 31.0 28.2 13.7	17.5 14.8 26.3 33.5 29.6 17.5	20.8 23.4 32.3 35.3 31.4 24.0	23.4 28.0 34.1 38.2 29.7 27.4	24.4 29.3 35.7 39.1 29.7 28.6	24.2 30.0 37.2 37.8 31.0 29.5	25.6 29.9 38.2 38.0 29.7 28.8	26·1 30·2 38·1 39·8 30·3 29·0	26.6 30.3 37.4 43.6 29.7 30.6	26.7 30.3 37.3 39.8 29.7 30.7	25·7 29·0 38·2 43·6 28·3 30·3
	9 10 11 12 13 14	33.7 28.7 25.9 33.6 39.0 35.4	33.7 30.3 24.9 36.3 39.2 36.2	34.7 35.3 32.3 37.8 38.4 38.0	35.9 38.3 37.8 40.2 39.8 38.9	37.7 39.3 39.7 42.4 40.4 39.5	37.2 39.0 39.2 43.1 41.3 39.3	37.3 39.5 39.2 42.6 42.0 39.3	37.1 39.4 39.7 43.8 42.4 39.5	36.2 39.8 39.5 41.1 43.3 38.2	36.0 40.2 39.9 39.8 43.5 37.9	36.2 40.1 40.4 39.7 45.0 37.4	35.6 39.2 40.0 39.8 43.1 34.0
MARCH	15 16 17 18 19 20 21	29 · 9 25 · 9 22 · 5 35 · 0 27 · 4 33 · 1	29.6 26.1 24.9 36.8 30.1 33.1	29.7 26.9 26.7 38.2 36.8 33.2	28.8 27.8 31.4 42.8 43.3 33.1	29°2 28°8 36°0 44°7 40°9 33°5	29.6 29.0 38.2 46.2 42.8 34.2	29°1 30°8 38°2 47°5 44°5 34°9	29.9 33.1 39.2 49.2 45.4 36.3	31.2 34.7 39.5 46.4 47.6 37.2	31.6 36.0 39.7 45.0 46.4 38.0	32.8 35.4 39.4 40.8 44.9 38.6	33·3 33·9 37·5 40·7 42·1 38·6
	22 23 24 25 26 27 28	34.1 38.6 38.8 35.2 35.7 34.5	35.6 39.2 39.2 35.8 37.0 34.7	37.7 39.5 39.4 37.0 38.1 36.4	39.6 40.4 39.4 41.6 38.6 37.4	40°8 40°4 40°3 42°4 42°5 39°4	42°1 39°5 40°8 44°5 42°4 41°3	42.6 39.5 41.0 44.1 43.0 40.0	43°3 39°5 42°2 45°1 42°5 39°5	42 · 2 40 · 0 40 · 7 46 · 7 44 · 4 39 · 8	40.8 41.2 40.8 43.8 41.5 38.2	41.0 39.5 39.9 40.0 40.4 37.6	40.6 40.0 39.4 38.4 38.6 36.6
	$\begin{bmatrix} 29\\30\\31 \end{bmatrix}$	31.6 28.4	33.7 32.9	34.4 35.6	35.6 37.4	37·4 39·1	38.0 42.4	39.4 40.6	40°2 40°4	39·5 41·3	39·4 41·9	37·8 40·4	38.2 40.3
Hourly	Means	29.00	30.27	32.21	35.50	36.74	37.57	37.88	38.38	38.22	38*45	37.76	37.0
	1 2 3 4 5 6	29°2 29°6 31°2 34°9 — 42°1	31.8 33.5 35.6 38.6 — 41.5	35°2 38°2 40°3 40°2 — 42°1	38'9 39'0 40'7 42'6 — 43'6	40°3 39°2 41°9 43°8 — 48°2	41.5 40.7 43.0 44.9 — 50.7	41.7 41.7 44.2 45.8 — 51.0	41.5 41.2 44.7 45.8 — 52.5	42.2 41.7 45.4 47.8 — 51.1	41.9 42.3 45.4 48.8 — 50.5	43°0 40°6 45°9 49°6 — 51°0	41.0 40.4 44.0 49.3 — 49.2
	7 8 9 10°	44.0 33.9 24.5	45°9 34°9 33°5 —	49.0 36.4 37.6	51.7 36.9 41.8	55°1 37°9 42°7	55 · 1 39 · 8 44 · 3	54.4 39.4 46.2	54.2 41.3 48.0	53·2 41·9 48·6	54.7 42.4 47.8	55.7 42.4 43.2	52.7 42.2 39.8
APRIL.	11 12 13 14 15 16 17 18	38.8 26.8 28.2 30.8 27.4 33.5 54.2	38.7  27.5 34.3 30.1 33.5 41.9 52.8	41.3  28.0 38.6 30.3 38.2 45.4 51.4	49.6 	52·2 32·7 43·5 34·1 43·4 51·8 49·3	55.0  33.9 44.4 35.8 43.4 54.1 51.4	55.8 35.6 43.2 38.0 43.7 54.5 50.0	53.4 36.7 43.2 39.0 45.8 55.6 55.3	49.0 38.8 42.6 40.6 46.6 54.9 53.8	45.6  38.8 44.7 40.4 45.7 55.9 56.7	43.9  39.0 44.2 41.9 41.3 56.2 56.6	41.2 37.4 41.0 41.9 39.9 56.6 57.8
	19 20 21 22 23 24 25 26	31.2 44.5 43.0 49.2 50.8 43.8	39.4 53.2 44.4 50.9 51.3 44.2	44.9 58.5 44.7 50.8 51.3 43.4	46.8 62.3 45.2 47.4 51.9 41.3	50°4 64°6 45°8 50°3 53°2 41°3	54.0 67.9 46.4 51.8 53.8 42.6	56.6 70.8 48.0 53.8 54.6 42.3	59°0 70°8 50°5 54°5 56°1 44°4	62·2 79·1 50·6 55·3 54·5 46·2	61.5 74.6 50.2 55.0 55.2 45.0	60.9 71.4 51.6 54.8 55.8 44.6	58.8 62.9 48.4 55.3 56.0 44.7
	26 27 28 29 30	42°9 46°6 46°2 48°5	49.6 53.6 46.0 49.4	52.8 53.4 45.8 51.2	56.6 54.0 48.1 48.8	57°2 53°6 49°6 49°0	57.0 55.6 49.2 52.1	56.4 55.3 50.5 54.2	55°9 55°7 49°0 56°1	54.7 57.2 48.0 57.7	56°2 59°2 48°2 54°8	57.8 59.9 47.6 55.3	58.0 61.0 48.7 54.2
Hourl	y Means	38.23	41.44	43.26	45.39	46.84	48.34	49.11	50.01	50.24	50.46	50.17	48.9

a Good Friday.

						STANDA	RD THER	MOMETE	R.				
	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
	6	7	8	9	10	11	12	13	14	15	16	17	Means.
	$\stackrel{\circ}{2}\cdot_2$	16·1	15°6	12.9	12.5	$ {\circ}_2$	<b>8.</b> 6	°7.6	8·4	10.1	$ {8\cdot2}$	10°3	0 17·08
	8.0	23.0	18.6	16.9	17.1	16.6	21.2	21.1	22.1	19.8	16.9	15.2	22.17
	9.0	38.4	37.5	36.9	36.8	35.4	31.8	34.2	33.1	33.7	34.9	34.1	33.94
	1.0	39.2	36.6	32.2	32.2	29.6	26.8	27.6	27.9	29.2	28.7	28.4	34.64
	4.6	20.8	17.1	15.0	13.2	13.1	10.2	10.5	9.2	8.4	9.5	8.6	21.47
3	0.1	30.1	30.3	30.6	30.1	29.5		0515		-		33·7}	28.74
	4.5	31.4	29.2	31.6	$\frac{-}{32\cdot7}$	32.9	35.7 33.7	35°7 34°1	35.1 33.7	$34.5 \\ 32.2$	33.9 $29.7$	33 ()	34.22
	6.1	30.6	$\frac{29}{28} \cdot \frac{2}{2}$	28.0	27.1	26.9	25.2	26.1	26.9	26.9	$\frac{25}{25} \cdot 7$	25.3	32.60
	8.0	35.6	34.7	33.4	33.2	33.3	32.2	31.6	31.0	31.0	31.6	31.8	34.84
	9.8	39.6	38.2	39.2	40.0	40.1	39.9	39.8	40.2	40.3	38.6	38.4	39.76
	1.0	39.7	37.5	37.2	36.9	36.9	37.0	36.4	35.6	35.6	35.2	36.5	39.25
3	3.2	31.6	31.5	31.5	30.8	30.8						<del></del>	34.60
		90:0	27.8	05.7	04:0	$\frac{-}{24\cdot 4}$	31.9	$\frac{32\cdot4}{25\cdot6}$	$\frac{31.6}{24.9}$	$\frac{30.8}{24.2}$	$\frac{30.4}{23.8}$	30.6 } 24.9	28.21
9	$\begin{bmatrix} 1 \cdot 4 \\ 2 \cdot 2 \end{bmatrix}$	29'0 28'4	$\frac{27.8}{27.4}$	25.7 25.6	24.8 24.6	23.3	25.9 21.7	$\frac{25.6}{21.5}$	21.6	21.9	21.8	20.4	$\begin{array}{c} 23 & 21 \\ 27 \cdot 45 \end{array}$
	$5.\overline{0}$	33.6	32.4	33.5	33.9	33.3	32.9	34.6	34.6	34.1	34.6	$35 \cdot 2$	34.50
	9.0	37.6	35.4	34.3	31.0	30.1	29.2	30.1	30.1	28.4	28.4	29.0	37:33
-1	0.4	40.0	42.3	37.8	38.2	38.2	36.6	35.8	35.8	35.4	34.1	33.5	39.17
3	7.2	34.2	31.4	27.6	26.8	27.8			-			$\frac{-}{33\cdot 7}\}$	33.97
				-			34°3	34.3	35.2 $39.5$	34.7 39.0	33 <b>·</b> 9 38 <b>·</b> 5	38.6	39.52
	0.4	39°1 40°7	38.4 41.6	38·3 41·3	38.4 41.7	39.0 40.4	39.8	39°5 38°7	38.4	38.3	38.4	38.4	$\frac{39.32}{39.79}$
	9.3	39.3	$\frac{41.6}{39.6}$	39.3	38.6	38.4	37.8	36.8	36.4	35.8	$35\cdot 4$	35.0	38.90
	8.2	37.0	37.0	36.4	36.2	36.6	36.4	36.5	35.8	36.0	35.4	36.0	38.82
	8.4	37.6	38.2	37.8	37.0	37.2	36.8	35.9	35.2	34.5	34.2	34.8	38.43
3	5.4	34.7	34.7	35.0	34.5	34'1						<del></del> }	35.19
	7:0	05:0		-	-		29.2	30.5	30.6	30.2 31.8	30.8	30·3 } 29·7	34.55
	$\begin{array}{c c} 7.2 \\ 1.2 \end{array}$	35.6 36.0	33.3 32.3	31.2 33.5	29.6 31.9	29.0 30.8	31.2 29.8	$\frac{32.3}{27.1}$	$\frac{31.8}{26.9}$	29.0	29.0	29.2	35.02
	5.89	33.83	32.70	31.63	31.12	30.65	30.62	30.29	30.46	30.51	29.69	29.65	33.61
-	3 89	33 83	32 10	31 03	31 15	30 65	30 62	30 39	30 40	50 21	29 09	25 00	30 01
	9.0	33.3	31.0	30.1	28.8	29.5	29.5	28.8	26.9	26:3	25.5	27.6	34.35
	7.8	33.3	30.3	29.5	29.5	29.7	30.1	30.6	29.9	30·3	$\frac{29.7}{32.0}$	28.8 $32.2$	$\frac{34.89}{38.03}$
	1°5 5°8	35.6 45.0	$\begin{array}{c} 34.1 \\ 45.2 \end{array}$	$\frac{32.2}{43.0}$	34°1 41°9	35°2 40°3	35.7	34.2	32.9	30 3 —	32 U	32 Z — )	
1		40 0	40 2	40 0	41 3	40 3	46.9	46.5	46.7	46.7	45.5	$43 \cdot 2$	44.53
4	9.1	48.2	48.0	46.3	46.8	45.9	45.4	45.0	44.7	43.6	43.2	42.6	46.76
	1.2	50.6	50.2	47.6	48.0	45.4	44.2	42.2	39.2	36.8	36.6	35.1	48.06
	0.2	37.4	36.0	32.9	32.0	32.0	28.6	27.5	26.6	25.7	26.1	24.4	34.95
	8.4	36.8	36.8	36.6	35.4	35.0	42.4	41.7	41.3	41.0	40.0	$\frac{-}{39\cdot 3}$	40.11
3	9.1	38.0	37.5	36.4	35.8	34.9		-			00:5	$\frac{-}{26.8}$	39.44
9	5.6	33.2	29.7	97:0	07:4	28.4	26.9	26.9	26.8 27.4	26.5 28.1	26.5 $28.4$	26.83	31.48
	9.8	33.5	36.4	27.6 36.4	27.4 35.6	$egin{array}{c c} 28^{\circ}4 &   \\ 35^{\circ}8 &   \end{array}$	28.6 34.6	28:3 34:1	32.1	31.4	30.9	31.6	$\frac{37.48}{37.77}$
	9.5	34.8	31.0	28.9	27.6	$\frac{33}{27}$ .6	27.1	OT 1	26.6	26.0	26.0	24.8	32.81
3	9.7	39.8	39.7	40.3	39.2	39.2	39.2	39.5		38.8	36.0	33.5	39.80
	6'1	51.9	49.3	44.9	43.0	42.2	40.8	39.4	42.1	41.0	46.1	53.5	48.40
5	6.4	53.4	50.0	49.7	45.0	42.2				21:0	30.1	${29\cdot 2}\}$	46.94
	6.5	55.0	54.9	5.1.5		16:6	32.5	$\frac{32.8}{50.2}$	31.6 45.5	31.0 44.9	45.6	46.0	51.03
	7.0	55°8 55°5	54 9 52.7	54.5 51.6	51.5 50.9	46.6 51.0	47.2 50.3	50.0	50.0	44.8	42.9	42.6	57.50
	6.2	44.6	43.6	44.0	43°4	44.4	46.0	46.2	46.3	46.0	47.2	47.8	46.45
5	4.8	54.1	53.1	53.2	54.2	55.3	55.8	55.3	54.0	50.6	50.4	50.8	52.96
	54.2	48*4	46'0	46.2	47.6	49.2	49.4	50.1	50.1	49.4	49.4	44.7	51.23
4	4.7	44.0	43.0	42.8	44.7	44.6	20.8	41.3	40.7	40.4	39.5	$\frac{-}{39\cdot 3}$	42.86
5	6.1	50.1	45.4	43.8	43.8	43.1	39.8 43.2	42.8	39.7	39.2	37.2	37.2	49.03
5	9.4	57.8	50.7	49.1	47.8	44.7	44.8	45.8	47.8	48.6	48.4	47.4	52.39
	8.8	48.7	48.2	47.6	47.2	46.8	46.8	46*8	46.6	47.2	47.2	47.8	47.78
-	54.4	52.6	51.5	50.5	50.8	50.6	50.4	50.3	51.0	50.9	52.3	52.4	52.02
4	17.28	44.83	<b>42 9</b> 6	41.82	41.30	40.80	40°26	40.69	39.45	38.61	38.21	38*26	44.09

					S'.	FANDARI	THERMO	METER.					
lours of Götting Time	Mean }	0	1	2	3	4	5	6	7	8	9	10	11
	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	1 2	53°.5 52°.7	$\begin{bmatrix} 5\overset{\circ}{4} \cdot 2 \\ 54 \cdot 1 \end{bmatrix}$	55°0 57°1	55°0 59°3	56°0 60°9	56.6 62.1	55.7 59.2	55°.7 58°6	56°8 59°0	58.0	53.8 58.0	53°2 58°0
	3 4 5 6 7 8 9	42.4 45.8 54.8 49.0 51.3 54.5	53.0 51.4 55.9 53.2 55.2 55.1	57.6 58.0 56.3 54.5 56.9 56.0	59.8 59.1 56.6 55.1 59.5 55.1	62.7 55.5 53.9 54.7 60.7 55.1	63.8 54.5 52.9 56.4 61.7 54.5	65.7 58.8 52.3 57.1 61.3 55.1	64.7 62.1 52.3 57.8 62.1 55.8	65.0 62.9 53.6 55.3 61.7 55.7	64.9 64.7 55.7 56.4 59.7 55.8	66'9 63'3 55'8 56'2 58'8 56'3	66:5 59:5 56:0 56:2 57:8 57:0
MAY.	10 11 12 13 14 15 16	35.8 44.2 43.2 54.2 50.6 47.6	37.0 47.1 46.2 58.0 50.8 49.2	37.0 50.0 47.0 60.0 50.0 54.2	36.9 53.0 54.3 64.2 51.7 58.8	38.0 55.3 57.7 65.5 54.0 59.8	40°0 57°4 60°5 64°7 54°4 61°4	42.2 58.8 63.0 65.1 57.9 60.4	42.6 58.8 64.2 65.3 59.9 61.5	44.6 60.5 67.5 67.1 57.4 61.3	46.2 61.3 67.7 64.2 59.4 60.5	47.2 60.6 68.3 69.3 62.4 61.9	47.4 63.1 69.4 66.9 59.7 60.1
N	17 18 19 20 21 22 23	54.1 39.0 44.1 42.8 42.4 50.1	53.9 42.5 48.7 44.7 47.4 54.3	53.1 44.9 53.2 45.4 49.0 56.4	54.7 47.2 57.2 45.8 53.8 57.4	55°3 48°7 61°3 46°6 54°9 61°3	55.8 50.8 64.0 46.8 57.6 61.5	55°5 50°4 64°6 47°4 56°6 65°1	54.2 51.6 65.1 48.2 56.6 69.6	53°1 54°0 66°5 49°3 57°8 69°8	53°3 55°1 66°1 51°5 56°0 68°1	53.0 55.2 65.7 50.3 55.9 66.4	51.6 53.8 64.9 49.6 53.5 66.1
	24 25 26 27 28 29 30 31	60.7 64.1 65.7 59.3 57.4 59.6	64.9 65.7 71.8 63.4 62.3 58.2	67:2 70:1 73:4 65:1 66:7 60:9	69°2 71°6 74°6 65°7 69°3 63°1	69.4 71.2 74.2 69.2 70.8 69.6	69.0 71.3 75.1 68.0 69.2 71.2	71.1 73.3 75.6 69.3 70.0 71.8	71.4 76.2 75.8 71.9 70.1 72.8	73.0 74.2 76.7 70.6 70.8 71.4	70.0 73.6 76.0 68.5 69.5 72.3	68.4 72.2 77.6 67.1 68.6 72.1	69°3 72°0 78°1 68°6 64°2 72°1
Hourly	Means	50.84	53.78	55.96	58.00	59.32	60.02	60.90	61.73	62.14	61.92	61.97	61.33
	1 2 3 4 5 6	59.8 63.5 56.2 60.4 56.1 45.0	64.7 63.3 59.9 64.2 55.7 49.1	66.2 64.7 62.9 63.5 54.4 51.2	64.6 68.1 66.2 64.0 54.2 54.5	61.9 65.9 63.1 65.2 54.3 55.3	65°3 65°9 65°7 64°0 54°2 56°4	69°1 62°5 64°6 67°7 55°1 57°9	69'9 65'0 64'1 69'6 57'2 56'6	69.4 65.7 67.7 66.1 57.8 57.8	69°3 66°1 69°1 60°7 61°1 56°6	72.0 66.2 68.0 61.9 58.0 58.0	73.0 65.7 71.0 61.5 58.6 58.9
	7 8 9 10 11 12 13	48.0 51.1 53.4 58.2 52.6 58.4	55°3 55°8 58°2 63°1 54°5 62°5	59°5 62°1 64°7 65°0 56°5 62°3	61 ' 9 66 ' 0 66 ' 2 68 ' 7 59 ' 2 65 ' 5	63°3 68°2 66°5 69°9 61°5 65°3	65.7 68.3 69.4 67.5 59.5 64.7	65°4 66°9 71°6 64°6 59°2 64°6	65.6 67.4 72.2 62.5 59.7 64.6	65°3 68°7 74°1 63°3 60°3 65°5	66°2 69°1 74°7 66°3 61°1 63°9	67.5 69.6 74.9 65.7 62.3 62.7	66'9 69'0 71'8 67'9 62'7 62'0
JUNE.	14 15 16 17 18 19 20	60°4 60°7 56°0 61°7 67°5 59°2	63.4 62.9 62.0 62.9 68.7 59.5	67°3 65°7 66°7 64°2 68°4 59°7	71.8 68.1 70.2 69.8 69.1 60.1	74·2 69·0 71·2 73·6 71·2 60·7	73.7 67.5 72.6 74.8 75.0 60.3	74.4 68.7 73.8 75.6 76.9 60.0	74.5 69.1 74.8 77.8 78.9 60.5	74.4 69.1 75.0 72.3 79.5 60.7	74.6 69.4 76.4 70.4 80.3 59.4	74.6 69.3 75.2 76.2 80.5 59.7	77.5 69.8 73.2 75.9 80.5 59.0
	21 22 23 24 25 26 27	54.3 58.4 60.7 66.1 64.2 63.0	55.8 61.9 64.6 68.4 64.9 68.0	58°0 63°6 66°4 71°8 67°7 66°9	60°3 67°3 69°3 75°7 68°9 67°7	64.1 71.0 72.6 78.5 73.6 69.1	66.5 72.8 75.0 80.9 76.0 71.6	65.7 73.7 77.8 81.9 75.5 73.2	68°1 74°2 78°2 83°3 75°4 71°4	68°1 74°4 78°9 81°2 78°7 69°3	67.9 75.0 77.3 79.9 80.3 68.6	66.7 75.2 79.3 79.7 75.6 69.3	
	28 29 30	65.1 69.0	$\frac{-}{64.9}$ $72.1$	65.9 74.2	68.4 75.6	72.0 76.2	73.6 77.8	74·2 77·8	76·2 77·8	75.0 78.3	75·2 78·5	77·1 79·1	76·4 79·9
Hourly	Means	58.81	61.48	63.83	66.51	67:59	68.64	69:17	69.79	69.87	69.90	70.17	70.17

					STANDA	RD THEF	RMOMETE	R.				
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
53.4	53°0	52°6	53.9	5 <b>4</b> °5	52°5	51°8	51°6	5ΰ4	5η9	52·4	52.4	53.84
58·4 —	55.2	50°6	48.3	47.3	49.0	 44.2	43.0	41.5	40.8	41.1	$\frac{-}{40.6}$	52.39
64.0 59.0	58.8 57.0	54.4 54.6	51.0 51.4	49.8 51.7	$\frac{47.0}{52.0}$	46°2 52°0	44.4 51.2	42.6 51.0	41.7 51.0	41.3 50.6	40°4 53°6	54°78 55°45
54.4	50.8	48.6	47.8	46.0	44.4	44.4	44.9 49.3	44.3 48.2	42.4 49.2	41.4 48.0	41.0 49.6	50°27 52°71
55.8 58.2	54°4 57°1	53.0 55.8	50°2 55°8	49°0 56°0	47.8 55.7	48.7 55.8	56°0	55.1	54·9	53.8	54.2	57.30
57.6	57.8	58·4 —	58.8	58·4 —	58 <b>·</b> 4	42.8	40.8	38.4	36.2	35°4	35.6	51.86
47.6	45°9 53°6	41.4 46.4	41·3 44·6	40.4 43.6	$\begin{array}{c} 41.2 \\ 41.7 \end{array}$	41°0 41°3	41°3 37°9	$\begin{array}{c} 41.3 \\ 37.8 \end{array}$	41.7 38.7	41.9 41.2	42°9 42°2	41°78 49°84
57.0 69.3	61.7	58.8	56.7	62.2	62.9	59.9	60.7	58.2	56.8	54.9	54°3 52°0	59°56 62°03
61.9 57.0	62.1 54.3	$\begin{array}{c} 61.1 \\ 52.4 \end{array}$	$\begin{array}{c} 61.1 \\ 50.2 \end{array}$	61 <b>·</b> 3 49 <b>·</b> 3	59 <b>·</b> 9 48 <b>·</b> 9	64.6 46.3	63.6 46.0	63.0 46.0	57°0 45°4	56.7 44.9	45.2	$\frac{62.03}{52.25}$
59.4	57.6	53.3	50.4	49.0	49.0	56.5	<u>-</u>	<u></u> 55`1	55.1		$\frac{-}{54.5}$	56.13
50°2 52°2	46.8 51.0	$\begin{array}{c} 44.2 \\ 47.5 \end{array}$	42.9 40.2	41°3 38°7	40°8 38°5	40.4 39.7	37.5 39.8	36.2 42.1	36°1 42°1	35.2 42.1	35'6 40'4	47°28 46°19
63.2	58.1	54.4	50.0	51.2	47.2	46.6	45.8	42.6	41.8	36.3	37.8 34.9	54.02 43.05
49.6 53.2	44'9 52'6	42.1 $52.3$	$\frac{39\cdot2}{51\cdot8}$	38*6 51*4	$\frac{37.6}{52.4}$	37.0 49.6	36.4 48.0	$\begin{array}{c} 35.6 \\ 47.2 \end{array}$	34.5 47.4	34°3 47°6	47.7	51.78
63.8	61.9	59°5	58.2	28.0	58.0	50°5	50.0	48.9	52.1	$\frac{-}{55\cdot 2}$	$\frac{-}{57 \cdot 2}\}$	59.14
71.4	69.6	66.3	63.9	63.1	62.0	60.7	60.4 60.5	60°5 60°4	$\begin{array}{c} 61.1 \\ 61.2 \end{array}$	59°1 60°5	$\frac{61.2}{60.9}$	65°97 66°80
69.3	67.0	$\frac{62.7}{67.7}$	62°1	$\frac{61.1}{62.0}$	61 · 1 57 · 5	59 <b>·</b> 9 56·7	56.2	54.9	55.2	55.1	55.8	67.80
71.0 64.4	70°8 63°4	66.7 61.1	61.3	58 <b>.</b> 8	58.8 61.5	$\frac{58.4}{62.0}$	56°1 61°2	53°2 59°4	50.4 59.9	$52 \cdot 3$ $59 \cdot 8$	59.8 59.8	63°18 64°32
72.2	67.7	64.6	63.2	64.7	63.2	57·6	56.2	55.3	57°0	56.4	$\frac{-}{58 \cdot 2} \}$	64.67
60.31	57:98	55.02	52.99	52.63	51.90	50.56	49.80	48.93	48.55	48.17	48*45	55.55
68.4	65.6	64.1	64.6	63.3	62.5	62.2	61.2	60.2	60.2	59.7	60.9	64.95
$\frac{62.9}{69.5}$	59°0 64°5	63.1 62.0	$\frac{60.3}{62.1}$	55.8 60.5	53°2 60°1	52°0 59°4	$51^{\circ}2$ $59^{\circ}4$	51'8 59'4	$\frac{50.2}{58.2}$	$\frac{49\cdot2}{58\cdot2}$	49.6 58.8	60°04 62°94
61.5	61.9	58.8	58.8	59.4	59°1	58.8	$59^{\circ}2$	57.4	56.6	56°5 43°4	56.4 42.8	$\frac{61.38}{52.79}$
58.4 58.1	56.6 55.1	54°4 48°2	48°5 45°6	50°1 43°0	49°4 41°5	49.0	48.0	45.4	44.2		ì	51.50
64.4	60.3	<u>-</u>	50.1	49.3	48 <b>`5</b>	51.5 48.0	50.8 46.2	49°3 44°7	48°3 44°0	$\begin{array}{c} 44.5 \\ 43.8 \end{array}$	42.8 } 45.0	56.17
68.0	62.0	55.8	52·2 59·7	59 <b>.</b> 9	50.4 58.0	49.0 56.8	47.4 54.5	47.4 55.4	46°0 55°8	46°2 54°5	46.4 55.4	58°46 63°60
69:4 66:3	66.9 62.7	62.5 57.4	55.3	52.6	54.7	55'3	54.0	53.0	51.4	50.2	49°3 54°1	60°20 57°27
61.2 61.4	58.0 60.3	54 <b>·</b> 9 59 <b>·</b> 4	52°2 56°3	52.4 54.6	51 <b>'</b> 8 53 <b>'</b> 8	54.2	57 <b>·</b> 9	28.0	56.1	54.6	- }	60.45
76.3	73.0	69 <b>.</b> 9	 67:5	65.7	 65°1	56*4 64*2	$57.0 \\ 63.5$	57.0 63.3	57°0 62°5	57 <b>·</b> 2 60 <b>·</b> 5	58°4 }   57°6	68.75
68.1	64.0	61.3	59.5	56.6 60.3	57.4 59.6	57.4 60.5	56.0 60.1	53 <b>·</b> 9 58 <b>·</b> 7	51.0 59.7	50.0 60.1	59.9 59.6	62°30 66°49
72.4 76.7	68 <b>·</b> 9	66.2 68.9	62.0 68.2	67.4	65.7	64.7	63.5	62.3	62.7	63.5	63.3	69.04 69.48
76.7 58.3	69°4 57°1	68.5 57.2	65°5 54°7	66.0 54.4	65°2	62.3	60.1	59.3	59.2	59.9	$\frac{59.0}{52.4}$	56.42
62.7	61.3	59.0	<u></u> 59·2	57·4	55.3	49.6 52.7	49.7 53.6	49.6 54.5	49.7 54.4	49.6 54.7	55.3	60.04
74·2 77·1	$\begin{array}{c} 71.2 \\ 73.3 \end{array}$	67.3 68.1	65·3 66·7	$63.8 \\ 64.7$	61.8 65.6	61.3 64.9	60°5 64°7	60°2 63°8	57.8 63.8	57.6 63.3	58.6 63.8	66°74 69°94
74.6	74.2	71.0	69.3	67.1	66.6	66.1	64.7 65.7	64.2 65.1	64.6 63.8	64.6 61.9	63.1 59.3	$72.33 \\ 69.96$
72.6 69.3	71.6 66.5	70°4 65°3	69°4 64°7	63.8	63.3 63.1						$\frac{-64.5}{64.5}$	66.88
75.6	$\frac{-}{72\cdot 2}$	<u>-</u>	67.0	$\frac{-}{65.5}$	$\frac{-}{65.7}$	65.9 64.6	64.5 67.9	63.8 66.1	$\begin{array}{c} 62.9 \\ 64.0 \end{array}$	64·1 63·1	63.9	69.60
79.3	76.5	$\begin{array}{c} 72 \cdot 2 \\ - \end{array}$	71.3	70.3	69.6	66.9	65.1	64.4	63.0	63.4	$\frac{65.7}{}$	72.65
68.29	65.65	62.65	60.62	59:30	58.65	58.45	57.94	57.25	56.44	55.92	56.03	63.48

					s	TANDARI	THERM	JMETER.	1	<del>                                     </del>			,
lours o Götti Tir	of Mean ngen ne.	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean	18	19	20	21	22	23	0	1	2	3	4	5
	$\left(\begin{array}{c}1\\2\\3\\4\end{array}\right)$	69°4 65°3 61°5 58°0	72.8 67.3 66.9 66.6	75°2 68°1 69°8 71°3	75°8 68°2 71°6 72°0	76°4 70°2 72°4 74°5	77°3 72°8 73°0 77°3	78°3 75°5 74°2 77°8	75°6 76°2 73°8 75°4	76°9 74°9 74°6 78°9	75°4 75°3 74°6 75°4	74°8 75°4 73°3 78°2	71° 8 75° 6 74° 2 75° 8
	5 6 7 8 9 10	63.8 60.5 62.2 62.9 76.9 69.6	67.4 64.0 64.3 69.9 80.4 75.6	69.9 66.1 63.0 76.3 85.2 77.3	73.2 66.9 64.4 78.5 86.1 79.3	75.8 70.2 67.9 77.5 89.9 85.3	77.5 72.8 69.9 73.4 91.9 84.3	78.2 73.8 72.2 69.6 94.0 86.3	79.9 74.0 75.0 67.1 77.3 86.1	81·1 73·4 78·0 73·0 87·0 80·7	80°3 76°5 79°1 74°4 90°5 75°6	80.9 77.8 80.1 78.3 90.9 76.7	81: 77: 77: 79: 85: 79:
JULY.	12 13 14 15 16 17 18	57.6 52.2 50.0 54.0 49.6 56.2	59.7 55.8 54.2 59.7 58.8 63.5	63°1 58°6 56°1 61°7 66°1 66°7	67.9 60.5 58.4 63.6 67.3 69.1	69.6 61.5 58.2 64.9 69.5 70.6	71.6 62.9 59.7 62.7 70.6 71.6	74'1 64'9 61'9 65'3 71'0 72'8	75.8 64.0 61.9 66.5 71.0 73.8	75.0 64.9 62.6 69.1 73.0 74.4	76.9 63.9 61.1 68.3 70.0 74.1	77 · 2 62 · 9 64 · 6 69 · 3 69 · 3 75 · 0	74:8 61:3 64:4 70:4 68:1 74:0
	19 20 21 22 23 24 25	66.7 65.5 64.4 60.9 66.9 64.1	69.6 69.2 66.1 66.9 68.1	69°1 72°0 66°7 70°1 65°1 71°2	72.6 75.0 70.0 73.9 65.6 74.4	75.4 75.9 69.3 78.3 65.7 76.3	75.7 76.2 70.6 76.0 66.3 78.2	76.8 77.9 74.7 78.1 65.8 78.5	77°1 76°7 75°8 79°1 65°6 79°1	77.5 75.9 73.9 80.1 68.1 80.6	78.6 74.5 75.8 78.7 71.4 79.1	78.5 74.6 73.4 81.9 68.9 79.4	76:8 72:8 72:4 80:0 70:9 78:7
	26 27 28 29 30 31	63.5 62.6 69.3 72.4 65.0	68.5 66.1 74.0 75.2 65.5	71.2 70.0 74.8 78.0 66.9	72·3 72·9 77·5 78·9 69·8	73°1 75°3 78°9 80°5 72°6	72.6 75.5 79.7 79.9 72.8	73°2 74°1 82°7 79°5 75°1	73°1 74°0 80°9 82°9 76°2	74.0 75.4 78.2 84.5 76.9	75.5 76.0 81.3 84.9 77.4	75.0 75.4 82.7 81.5 78.0	74:575:581:482:577:5
lourly	Means	62.63	66.75	69:24	71.32	73.17	73.81	75.05	74.59	75.65	75.73	76.07	75.2
		62.4	66.9	70.2	73.2	74.5	75.2	76.2	76.0	76.7	77.1	76.4	76.0
	2 3 4 5 6 7 8	59.7 65.9 69.4 63.5 65.4 66.5	65.5 70.4 73.6 67.9 68.9 67.9	70'4 73'9 76'7 72'8 72'1 70'0	73.4 77.3 79.7 78.2 75.4 66.4	75.2 78.9 81.9 81.7 76.9 66.1	76.9 81.9 83.7 82.7 79.9 68.3	78:7 83:7 84:1 82:7 81:0 72:7	80'3 84'3 85'9 82'7 82'3 73'9	81'3 84'7 86'1 81'5 82'2 73'8	81.5 84.7 85.9 81.5 81.3 73.8	81'1 85'1 85'3 80'2 80'3 73'2	79:5 85:3 85:3 82:0 79:5 71:2
JST.	9 10 11 12 13 14 15	67.2 55.7 55.7 69.1 64.7 60.0	67.4 60.5 62.5 71.4 66.3 66.4	68.6 64.6 68.7 73.8 71.8 70.2	70.6 68.1 72.8 75.4 75.2 74.4	73.8 70.2 76.4 79.5 77.1 78.0	74.6 70.2 77.0 79.9 77.3 78.0	74.6 71.8 78.4 83.9 77.3 79.9	76.2 72.3 80.1 84.5 76.4 79.7	77:3 72:8 80:9 73:3 77:3 80:5	78.3 73.3 81.3 76.7 78.0 82.3	77.5 73.0 79.7 78.5 79.3 82.1	76.0 73.0 78.7 79.2 77.1 80.7
AUGUST.	16 17 18 19 20 21 22	61'3 50'4 54'6 61'5 57'1 64'4	63.8 53.3 61.7 61.9 62.6 65.1	66.5 55.7 62.5 62.1 67.7 65.3	68°1 59°1 64°0 62°8 70°8 65°3	71.2 62.3 64.4 63.8 71.4 66.3	71.0 63.3 66.7 64.5 72.0 69.1	71'4 63'3 66'3 65'5 72'4 71'0	70.6 64.1 66.6 67.3 71.6 70.7	72.1 64.4 68.7 67.5 72.4 73.5	72.4 65.3 66.1 67.7 74.0 71.3	72.4 65.3 65.6 68.3 73.1 70.3	71:0 65:6 64:7 68:7 72:8 68:3
	23 24 25 26 27 28 29 30	57.0 55.9 56.4 59.9 62.1 61.1	60°3 61°1 64°9 65°4 64°4 65°8	62.9 66.1 69.6 69.3 67.9 70.8	66.4 68.7 71.6 72.4 68.5 73.4	67.9 69.5 71.9 74.8 72.0 75.1	70.8 71.8 75.8 73.3 76.7	67.3 70.8 74.3 75.2 75.2 76.4	67.7 70.3 74.8 73.9 76.2 73.0	68.1 72.6 74.4 74.4 76.9 66.3	69°3 73°3 73°8 73°8 75°4 66°6	69.2 72.5 73.8 73.4 73.9 67.8	69:3 71:4 71:8 72:8 71:4 68:3
	31	65.4	66.2	72.4	74.1	75.9	77.1	79:3	80.1	80.2	80.8	79.9	78:3
Hourl;	y Means	61.24	65.10	68.26	70.97	72.95	74.05	75.13	75.83	75:39	75.60	75.28	74

		<u></u>				STANDA	RD THEF	RMOMETE	R.				
	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
	6	7	8	9	10	11	12	13	14	15	16	17	Means.
	°°2	69°3	66.9	65°7	64.4	65°6	62°9	66°5	66°1	65.3	64.4	64.0	70°·45
	74.7	71.0	65'1	60.6	59.4	57.4	58.4	59.4	59.5	58.8	58.0	57 <b>.</b> 6 55.3	66.84 65.26
	72.2	69.3	60.9	58.0	56.6	56.2	54.9	55.0	56.0	56.1	55.8	_ 1	! #
	73.8	70.8	69.4	66.7	66.7	64.9	64.6	64.7	64.9	63.8	63.8	$\frac{-}{62\cdot 4}$	69.90
	78.0	73.2	70.6	67.4	64.7	62.9	60.8	60.0	59.6	56.4	56.7	55.7	69:79 66:84
	75.3	72.2	65.3	64.7	63.6	58.7	55.8	60.3	59.7	59.7 59.7	57.8 58.5	58°0 58°1	68.73
	77.4	76°2 76°7	73.3	65.5 69.6	67.7 70.0	66°3	64.6 $71.8$	64.0 70.4	64.7 70.2	69.1	68.3	74.2	72.76
	79°5 78°9	76.2	73.8 72.6	69.8	70.0	69.1	69.5	70.4	68.1	67.7	67.3	66.3	78.42
	75.1	72.1	74.2	73.4	74.4	73.0						$\frac{-}{55.8}$	72.80
							62.1	61 <b>.</b> 4 52.6	58°2 49°3	55.7 46.4	55°2 46°0	46.4	63.48
	70.6 59.7	66'9 57'6	62'1 54'9	61'3 52'6	61.5 50.4	59°6 51°4	57.6 50.8	48.2	48.3	46.4	46.0	47.1	56.14
	64.2	61.9	28.0	57.0	54.7	54.4	54.4	54.0	53.2	51.4	49.7	49.7	57.32
	66.9	62.7	56.8	51.8	50.8	49.6	48.4	48.4	47.6	47°1 51°3	46.8 50.2	44 <b>.</b> 9 50.8	58.22 61.53
	66.2	64 1 67 3	59.5	55.5	56.6	55°1 56°6	55.3	54'1	53.3	51 5		— }	
	70.9	01 3	61.1	58.8	57.8		$\frac{-}{65.9}$	64.2	62.7	62.1	62.7	$\frac{-}{62.7}$	00 47
	74.0	70.6	67.5	62.5	60.3	60.1	59.9	61.1	60.7	59.2	57.2	58.6 60.9	68.57 69.44
	72.0	70.0	69.1	67.1	65.5	64.9	65.1	62.8	60.9 56.4	60.7 55.3	$\begin{array}{c} 61.3 \\ 56.2 \end{array}$	57.4	65.76
	72·4 77·5	68.5 73.3	62.7 69.4	61.3 67.8	59.4 66.4	59°0 65°7	58.6 65.7	58°0 66°4	66.2	66.2	66.3	66.2	71.72
	70.6	69.8	68.7	67.3	65.7	63.2	62.3	62.4	62.3	62.3	62.2	62'1	66.10
,	78.7	76.2	72.2	70.0	67.9	67.7			61.5	59.4	59.9	${59.5}$	71.12
	73.0	67.5	61.1		57.4	57.0	$\frac{63\cdot5}{57\cdot2}$	62.7 58.0	57.8	58.0	59.4	60.2	66.30
	74.6	70.8	68.9	65.1	63.2	61.9	63.2	63.8	65.2	65.7	65.5	66.1	69.46
'	76.5	75.3	75.2	74.0	74.3	71.7	71.8	71.4	70.6	70.2	70.1	68.7 65.0	75°47 74°95
	79.2	77.4	73.8	72.1	69.6	68.6	67.9	67·1 60·4	66.5 60.1	65.7 59.7	65°1 59°5	59.0	67.98
	74.6	70.6	66.6	63.2	61.3	61.3	61.2	61.04	60.37	59.25	58.89	59.02	67.85
	73.22	70.28	66.66	63.97	63.02	62:00	61.29	61 04	00 31	03 20		1	
	74.0	69.3	65.7	65.9	65.7	65.7	58.7	58.0	57.0	56.2	57.6	<del>56.</del> 6}	67.97
	77.3	73.2	72.3	69.3	62.9	61.9	61.4	64.0	60.9	59.7	58.6	59.1	70°17 75°28
	81.6	77.1	75.3	73.4	72.1	68.7	68.5	68.9	67°5 71°4	65.9 67.1	66.6 64.2	65°3 64°0	78.29
	85°1 80°6	83 <b>·9</b> 79·0	$\frac{82\cdot 2}{72\cdot 0}$	80°1 67°1	80°1 64°4	79.7 63.3	73.6 64.0	70°0 65°7	66.3	65.1	64.5	64.5	73.05
	77.1	73.0	70.0	67.1	66.3	66.9	66.9	67.2	66.9	66.3	65.9	66.2	72.72
	68.7	68.2	67.9	67.5	67.7	67.3			<u> </u>	65.0	65.6	$\frac{-}{65\cdot 7}$	68.24
	73.3	60:0		64.7	61.9	60.5	66:3 59:7	66°1 58°2	64.9 56.2	65°2 55°5	54.2	53.4	67.22
	71.3	68°3 67°1	64 <b>.</b> 9 62 <b>.</b> 0	64.7 60.0	59.0	57.6	57.3	55°8	54.7	54.5	55.1	53.8	63.90
	76.2	73.9	72.2	71.2	$70^{\circ}2$	69.3	69.6	70.2	68.3	68.1	67.7	66.5 62.9	72:33 73:05
	77:3	76.2	73.4	72.2	69.3	69.1	68.5 61.7	65.6 61.5	65.5 60.7	64.7 60.0	63°3 59°9	59.5	69.23
	76:9 76:9	72.0 $75.2$	68.5 74.0	$64^{\circ}2$ $73^{\circ}2$	63.4 71.4	62.6 70.8	OT 1	01.0		_		60.5}	
			_				60.6	60.0	61.9	61.5	61.9	60.2 }	63.38
	69.4	64.9	62.2	60.2	59.2	58.3	57.8	52.4	50.8 51.2	51.6 50.8	51.6 50.6	51.2	57.27
	63°1 64°2	57.5 62.9	54.9 62.3	53.6 62.1	53°2 61°5	52.6 62.3	51.6 62.1	52.0 62.5	$\frac{51}{62}$ .5	61.5	61.2	61.2	63.58
	67.9	65.5	63.2	63.1	62.2	62.1	61.4	60.7	59.9	58.4	58.0	57.2	63.40
- 1	69.8	68.5	66.2	66.2	66.8	64.9	65.0	63.3	62.7	62.7	63.8	64.4	67.62
	67.1	65.1	64.9	63.2	62.6	61.7	62.3	58.4	58.2	58.6	58.2	57.8}	64.96
	67.4	60.1	56.8	54·5	54.4	53.8	53.2	52.0	52.2	52.2	52.0	52.8	60.60
-   -	69.3	66.3	64.6	62.9	63.2	62.3	62.3	60.9	59.7	59.0	57.6	56.6 58.0	65:33 65:90
	69.8	63.2	61.9	61.7	60.9	60.9	60.3	59.5	59°1 63°3	58.6 61.9	$\begin{array}{c c} 58.2 \\ 61.5 \end{array}$	58.0 61.3	67.69
	69.6 71.0	65°8 68°7	64.6 67.3	62 <b>.4</b> 65.3	62.9 65.0	62.5 64.9	64.0 63.3	63.8 $62.3$	61.1	60.3	60.1	60.0	67.77
	69.6	65.5	64.6	62.9	62.3	62.9	_					$\frac{-}{64\cdot 4}$	66.84
- 1	74 4	72.2	71.2	69.6	69.3	65.9	64.6 63.8	61 <b>.9</b> 63.5	61.3 62.9	61.3 62.1	61.5 65.1	64.47	71.46
-	72.66	69.34	67.14	65.22	64.55	63.79	62.63	61.71	61.04	60.34	59.80	59.96	68.04

					SI	ANDARD	THERMO	METER.					
Hours of Göttin Tim	Mean }	0	1	2	3	4	5	6	7	8	9	10	11
	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	1 2 3 4 5	65.2 65.5 69.4 67.0 70.4	68.5 69.2 70.6 69.4 72.4	72.1 71.8 72.0 71.8 74.3	77.1 75.8 71.0 72.6 77.0	78·7 78·0 73·2 73·3 79·3	81.7 79.5 74.4 76.2 76.9	84·0 80·5 73·6 76·4 76·2	83.5 81.9 72.2 76.3 77.5	82.7 81.3 71.7 78.0 76.9	81.9 79.7 72.6 77.3 77.1	81°3 79°5 71°8 76°8 76°9	77.5 77.5 71.9 76.0 75.0
;;	6 7 8 9 10 11 12	65.5 60.7 52.0 61.5 64.7 68.2	69'9 62'7 54'0 61'5 67'4 72'4	74.8 64.4 56.4 61.7 69.8 76.1	78.0 66.7 58.0 64.0 72.4 78.5	79.7 69.1 59.0 64.7 72.7 78.3	80'9 70'1 59'7 65'9 73'6 79'3	82.9 70.0 61.0 66.5 74.9 75.0	82.7 69.6 62.7 66.2 77.8 66.5	83°1 69°4 64°3 66°8 78°6 68°7	82.7 68.7 64.5 67.5 76.0 71.6	81.5 68.5 65.2 68.1 74.4 72.0	80°5 66°9 64°9 68°0 75°2 72°8
SEPTEMBER.	13 14 15 16 17 18	66°1 55°1 45°0 54°0 56°9 46°8	68.8 56.0 50.8 55.3 57.8 52.6	72.6 56.4 58.2 57.0 58.7 58.7	75°0 57°0 62°3 58°9 62°9 64°0	78°5 59°0 64°0 60°3 66°1 68°3	81'3 60'1 64'7 62'5 67'1 70'2	80°1 61°7 65°0 63°3 66°5 71°8	81°3 62°7 65°1 63°3 66°7 72°0	81.9 64.6 65.7 61.9 67.1 72.2	79.7 65.3 64.7 59.7 66.5 71.3	77.1 66.1 63.5 58.1 67.1 72.0	79.1 64.8 63.8 57.2 65.9 70.6
	20 21 22 23 24 25 26	51.6 40.0 45.5 59.4 49.7 43.4	51'8 43'8 53'5 63'3 50'3 46'2	51.6 52.0 59.9 64.2 50.8 49.2	52'4 57'6 64'2 64'0 50'6 52'8	54.2 58.8 66.5 64.2 53.2 55.5	56°1 60°5 69°3 64°2 54°6 56°5	57.8 62.1 71.1 65.5 55.1 58.0	59 1 62 5 72 3 65 0 55 8 60 3	60°1 63°8 72°4 61°1 56°5 59°4	60.0 64.5 72.2 61.5 56.8 60.0	60.7 64.6 71.5 61.7 55.3 61.0	59°5 63°2 69°3 60°9 53°0 59°0
	27 28 29 30	39.0 56.2 57.6	41.7 58.6 59.7	44.7 59.7 61.5	48·2 62·8 65·1	51.6 64.8 67.2	54°5 66°5 68°7	55.8 67.6 69.2	56.0 67.1 68.2	57.8 67.5 67.3	59°0 66°3 66°9	58.9 63.8 65.3	57.8 62.7 62.5
Hourly	Means	56.78	59.55	62.35	64.96	66.82	68.27	68.91	69.01	69.26	69.00	68.57	67:52
	$\left( egin{array}{c} 1 \ 2 \ 3 \end{array}  ight)$	52.7 47.0 39.7	51.8 46.4 41.3	51.4 46.0 47.6	51.0 46.8 51.7	$51.2 \\ 48.2 \\ 52.4$	52.4 49.6 53.6	53.0 50.2 54.2	53.0 51.3 54.6	$53.6 \\ 52.1 \\ 55.5$	54·2 53·0 54·7	52.8 54.5 54.2	$52.1 \ 54.2 \ 51.4$
	4 5 6 7 8 9	44.7 45.9 50.5 60.1 57.0 37.6	45.8 42.8 52.6 60.5 57.4 39.6	49.7 48.7 59.9 62.3 58.0 40.9	53.4 56.0 63.8 62.9 65.7 42.3	57.8 58.8 65.7 63.5 69.7 43.4	60°1 60°1 66°9 64°2 69°1 45°5	62:3 61:2 68:3 61:3 67:4 45:4	62°3 63°1 68°9 59°5 67°5 46°2	62:1 62:9 66:9 58:7 58:6 47:2	63.8 63.8 67.7 58.2 56.3 48.4	65.6 62.9 67.3 58.2 54.8 47.3	62.9 62.1 65.2 57.7 53.4 45.4
OCTOBER.	11 12 13 14 15 16 17	50.7 49.1 35.6 37.0 47.2 35.1	54.7 48.7 34.9 37.6 48.2 33.5	56.7 48.9 39.7 40.4 50.0 33.6	58.7 48.8 43.8 44.3 50.9 34.6	60°1 48°2 48°2 46°0 53°0 35°2	61.1 47.8 49.2 46.8 54.3 35.5	61.5 47.6 50.6 47.4 55.8 36.1	61 5 47 7 51 4 48 3 58 4 36 6	62:3 47:2 51:5 49:0 57:6 36:8	62.5 46.4 52.0 50.2 56.8 36.4	61:3 45:4 51:4 48:8 56:5 36:6	60°3 43°2 46°4 45°8 56°4 36°0
0	18 19 20 21 22 23 24 25	32·2 42·1 33·1 37·8 24·5 33·7	31.7 43.0 33.5 37.6 26.3 35.0	38.4 44.6 35.2 37.8 27.2 38.3	43.4 45.0 38.8 37.8 29.1 41.2	47.0 45.4 40.6 38.0 34.3 43.6	47.8 46.6 41.5 38.0 36.5 45.8	48.2 48.4 43.0 37.2 37.6 46.2	46.4 48.1 43.7 38.0 39.8 46.2	46.0 45.8 42.4 37.2 40.8 41.9	46.8 44.0 40.5 35.4 40.6 45.0	46.6 44.0 40.0 33.2 43.2 44.2	44.1 43.5 39.6 32.0 42.8 44.0
Nov	26 27 28 29 30 31	33.5 51.0 29.5 35.9 34.4 31.6	36.0 49.6 29.7 36.5 34.4 32.2	39.4 48.8 31.9 37.6 35.2 32.4	41.7 47.8 32.3 41.9 36.6 32.4	44.2 47.8 34.4 44.2 38.0 33.1	47.8 49.7 35.0 46.0 39.4 33.7	51.4 49.1 36.5 43.2 39.7 34.1	53°2 48°3 38°0 46°4 39°7 35°6	53.0 48.8 40.1 47.4 39.7 36.6	51'8 46'6 40'2 46'8 39'0 37'2	51.2 45.6 39.4 46.2 38.6 39.2	50.0 44.2 35.2 43.8 36.6 39.2
											49.57		47.69

					STANDA	RD THER	MOMETE	R.				
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
75.4	73.2	73.8	72.4	69°8	73.4	69°8	68.0	66°7	67°1	65°9	65°7	73.98
76.2	76.8	73.4	72.7	73.0	$72^{•}4$	71.6	71.0	70.6	70.1	70.4	69.3	74.49
71.8	71.0	69.4	68.6	69.3	69.3	69.2	70.2	70.4	69.8	69.4	67.1	70.83
74.0	72.8	72.3	72.0	71.4	71.2	71.4	71.4	71.4	71.6	71.2	70.0	72.99
74.4	72.6	69.6	66.2	65.3	65'1						$\left\{\begin{array}{c} -65.3 \end{array}\right\}$	71.59
				<u> </u>		66.9	66.4	65.7	64.9	65.2	62.1	73.83
77.9	76.1	76.9	71.5	70.9	70.8	68 <b>·</b> 5 56 <b>·</b> 2	65°8 55°7	64.4	62°9 53°4	62°0 53°2	52.4	62.30
63.8	61.3	63°3	59°3 62°4	58.7 61.9	57°1 61°9	61.6	57.8	55°1 61°4	60.7	59.5	59.7	60.41
67.2	65.7	64.0	04 4	59.5	59.1	59.9	59.2	59.7	61.9	63.3	63.8	63.74
73.4	69.1	69.1	67.9	66.2	66.2	65.7	67.2	66.9	67.3	66.2	67.2	70.45
69.8	66.9	64.7	62.8	61.7	62.3						$\frac{-}{64\cdot 7}$	69.13
						65.2	65.2	65.4	65.3	65.3	64.75	t :
79.0	77.2	77'1	75.8	74.7	72.1	70.4	68.4	66.7	59.7	57.7	55.7	73.17
61.7	55.9	56.2	54.5	53.6	54.2	52'4	52.0	51.4	49.0	47.4	46.8	56.83 59.10
64.0	64.2	61.2	59.7	58.2	56.8	53.8	53.6	53.6	53.4	53 <b>.4</b>	53°8 57°4	58.29
57.2	57.4	57.6	57.4	57.1	56°8 54°9	57°2 52°8	57°2 52°6	57.6 50.8	57.6 48.4	57°0 47°9	47.3	58.76
62.9	58.0 64.6	55°1 64°6	$55^{\circ}1$ $62^{\circ}3$	55°2 60°8	57·9	04 0	02 0	30 8	40 1			
01		04.0	02 0			64.0	63.1	60.5	56.2	54.7	$\begin{bmatrix} - \\ 52 \cdot 4 \end{bmatrix}$	63.30
55.4	51.4	49.2	48.7	48.2	47.2	46.3	44.6	43.8	43.0	43.0	41'3	51.54
60.7	55*3	52.8	50.4	50.0	48.4	47°4	47.6	47.0	46.0	45.4	45.0	53.73
66.7	66.1	65.3	65.1	64.2	62.0	62.2	63 <b>.2</b>	62.7	60.2	59.4	59.3	64.38
60.3	59.2	58.0	56.4	55'4	53.7	<b>53.3</b>	52.9	52'0	51.4	50.7	50.0	58.69
51.6	51.2	51.8	51.5	51.2	51.6	50'8	51.1	51.0	47.9	46.9	44.9	51.80
57.6	56.6	<b>55°</b> 8	53.2	51.8	48.0	44.4	43.6	42.4	41.0	39.7	$\frac{39.0}{-}$	51.43
56.8	55.8	5 <b>4</b> • 9	52.6	52.6	53.4	23.0	53.4	53.6	53.6	53.6	54.8	53.05
61.7	59.2	60.1	58'8	54.7	58.6	57.6	56.9	57.4	57.6	57.1	57.7	60.88
64.6	61.7	62.1	64'3	62.4	60.9	59.2	57.6	54.8	52.6	51.0	53.5	61.82
66.04	-	63.03	61.68	60.40	60.22	59.67	59.09	58.28	57.42	56.83	56.03	63.09
					1						10.0	10.07
51.2	51.2	49.2	47.8	47.4	47.3	46.9	46.0	45.2	45.0	46.1	46°2 39°5	49 <b>·</b> 95 46 <b>·</b> 10
52.0	46.2	46.0	41.9	41.2	41.7	41'3	40.4	39.7	38.6	38.6		13
46.2	46.4	45.2	45.6	44.7	43.4	45.4	43.4	42.5	41.9	41.7	$\frac{-}{42\cdot 1}$	47.48
54.9	52.0	55°1	$\frac{-}{53.5}$	49.2	47.6	46.6	43.0	41.7	40.4	40.6	42.3	52.38
61.7	59.0	57.4	$53.\overline{2}$	51.6	54.2	55.0	55.8	52.9	51.3	52.1	49.8	55.94
62.8	65.9	65.7	65.2	64.7	67.1	62.7	60.1	59.3	60.2	60.3	60.1	63.25
57.5	57.1	57'1	57.8	57.5	57.8	57.8	56.8	57.2	57.2	57.0	57.3	58.97
51.7	50.8	50.3	48.2	42.6	41.2	41.2	40.9	40.4	39.7	38.8	39.3	52.20
40.4	37.7	38.0	37.9	38.4	36.6				51.2	50.0	48.4	44°18
61.1	59.5		 50:0	52.0	51.8	50°3 51°6	51.0 51.5	51.2 52.1	51.2	51.4	51.3	56.35
43.6	43.2	$54.5 \\ 43.2$	$\frac{52.8}{44.0}$	43.4	42.4	41.6	41.3	39.6	39.3	38.6	38.2	44.48
42.0	41.7	44.2	44.2	43.7	53.4	43.7	44.0	43.2	42.6	39.7	38.0	44.81
41'8	41.1	40.8	41.3	41.9	42.6	43.0	43.2	43.0	44.7	46.6	47.2	44.12
55.8	55°1	53.4	50.0	46.0	44.9	44.6	41.8	40.4	39.5	38.3	36.5	49.62
35.6	33.9	32.7	31.7	31.0	31.2	26.0	25.4	95.0	35.1	34.9	$\frac{-}{34\cdot 9}$	34.74
43.1	42.1	42.1	41.0	41.5	$\frac{-}{42.7}$	36°3 43°0	$\begin{array}{c} 35.4 \\ 42.7 \end{array}$	35.0 42.0	41.6	42.2	41.7	42.71
42.2	39.5	38.6	41'8 36'8	35.2	33.0	32.3	33.2	32.7	32.2	31.0	32.7	40.02
38.8	38.0	35.4	36.0	37.0	36.8	36.4	36.4	36.8	37.2	38.0	38.0	38.20
31.5	30.6	29.5	27.8	25.2	22.7	22.3	21.9	20.8	20'6	22.2	23.8	30.79
42.1	41.2	39.4	38.4	38.2	36.4	36.8	36.0	36.0	35.7	34.9	32.9	36.58
40.1	38.4	37.2	34.1	33.0	31.6		00.5				$\frac{-}{32\cdot 9}$ }	38.47
52:0		50:0		<u> </u>		33.6	$\frac{32.7}{51.4}$	34.2	34'1 51'0	33.2 $51.6$	51 6	49.18
53.2	53.1	53°0 41°2	53.4 $39.7$	52.2	51.8 38.2	53°3 36°6	51.4 35.5	51.4 34.7	34.2	34.3	31.4	42.85
31.6	42.2	28.8	$\frac{39}{29}$ .7	39.2 31.6	31.4	29.0	35.5	33.2	33.2	32.9	33.9	33.30
41.3	39.8	39.5	38.4	38.0	37.4	36.8	36.1	35.6	35.3	35.0	34.8	40.16
36.5	35.6	35.4	35.1	34.4	33.2	32.9	31.6	31.5	31.2	31.2	31.6	35*48
39.4	40.0	41.0	40.1	40.3	40.3	47.2	<u>-</u> 47°4	 47.6	48.6	49.0	$\frac{-}{48.6}$	39.45
45:00	14100	44422								41.13	40'91	44.88
45.95	44.83	44.22	43.20	42.30	42.20	42.90	41.93	41.48	40.88	41 10	40 31	77 00

		•			ST	TANDARD	THERMO	METER.					
Gött T	of Mean ingen ime.	U	1	2	3	4	5	6	7	8	9	10	11
Hours o	of Mean conto ime.	18	19	20	21	22	23	0	1	2	3	4	5
	$\left(\begin{array}{c}2\\3\\4\\5\\6\\7\end{array}\right)$	48.6 46.6 42.0 36.9 30.6 39.0	48·4 46·8 42·2 37·4 32·2 40·7	47.8 47.6 45.0 40.5 36.2 41.9	50°3 49°1 49°4 43°8 39°8 43°6	51·2 50·2 50·9 47·2 44·7 45·8	51.8 52.7 51.4 49.2 47.8 48.3	52.2 53.1 52.0 50.0 49.0 49.7	52°1 52°2 52°2 49°6 50°0 48°9	52.7 52.4 52.8 48.8 50.2 49.7	53.0 52.2 53.0 49.4 50.4 49.7	53°3 52°1 51°2 47°6 49°3 49°3	53.0 49.0 48.0 43.6 46.4 49.0
ER.	8 9 10 11 12 13 14	49.7 49.8 50.9 45.4 46.0 44.2	49.6 49.6 51.1 45.2 46.2 43.5	50.4 50.4 51.2 45.2 46.2 42.7	51.0 51.2 51.2 46.0 46.2 43.6	53°4 53°0 51°6 46°6 46°5 44°4	53.4 54.4 52.0 47.6 46.4 43.8	54.4 55.5 51.6 47.8 46.0 44.6	54.2 55.5 51.8 48.5 46.4 46.0	53.9 55.3 51.6 48.6 46.8 45.6	53.5 53.8 52.6 48.0 46.8 45.9	53.9 53.0 52.6 47.8 46.8 45.2	52.8 52.0 52.0 47.2 46.4 44.4
NOVEMBER.	15 16 17 18 19 20 21	42.8 39.6 43.6 41.9 37.0 37.4	43.9 41.3 42.8 41.6 37.2 36.8	43.7 43.6 45.0 41.2 37.2 37.4	44.7 45.0 48.8 40.4 37.3 38.1	46.1 47.0 52.0 40.7 39.7 38.5	47.8 46.2 54.0 41.5 40.4 39.9	48.0 47.0 52.8 41.5 41.7 40.6	47.8 49.2 52.8 41.2 42.4 41.0	47.3 48.0 51.3 41.0 43.2 42.4	46.4 47.6 50.1 41.4 42.4 43.0	45.6 47.4 48.4 40.5 41.4 42.1	45.6 47.0 47.0 38.9 39.4 42.1
	22 23 24 25 26 27 28	30°3 34°1 25°3 19°4 24°2 37°2	30.0 32.7 22.1 19.5 22.5 36.8	30°2 33°5 20°2 20°9 22°9 38°2	31.6 34.9 20.2 22.7 24.4 37.9	33°3 38°2 19°8 24°6 25°8 38°4	33.9 40.6 20.4 27.4 26.9 40.1	34.7 41.7 20.8 27.6 28.4 41.7	36°0 43°2 21°3 28°2 30°0 42°8	37.4 40.5 21.6 29.0 31.4 43.5	36.8 40.0 21.4 27.8 32.9 42.4	36.2 38.6 21.7 26.3 33.7 40.2	35°2 34°6 21°1 24°8 34°7 39°0
	$\begin{bmatrix} 29\\30 \end{bmatrix}$	27.4	25.5	25.7	26.7	28.2	29.0	29.2	29.0	29.2	28.4	28.5	27.1
Hourly	y Means	38.80	38.62	39:39	40.72	42:31	43.48	44.06	44.49	44.57	44*36	43.71	42.41
	$\left(egin{array}{c c}1&&\\2&\\3&\\4&\\5&\end{array} ight)$	13.9 34.5 34.4 25.8 29.9	13.0 35.0 34.1 25.9 29.5	15.6 35.7 33.5 27.0 29.5	19°1 36°6 33°4 29°9 30°8	20°8 37°5 34°0 31°8 32°4	23°2 38°5 34°3 32°5 33°5	24.9 39.5 34.2 33.7 34.3	26.7 41.3 33.1 34.3 34.7	27.4 43.6 33.5 33.7 34.3	27.6 42.3 32.7 34.6 34.3	28 1 42 1 31 6 34 6 33 5	28.9 43.6 31.4 34.7 33.3
	6 7 8 9 10 11 12	34.3 37.8 32.5 32.4 25.5 20.0	34.9 38.0 32.4 32.4 24.4 17.3	35.5 36.1 31.9 32.4 23.6 17.1	37.0 36.5 31.4 30.3 24.0 16.7	37.4 37.2 31.4 29.9 25.8 16.0	38°1 37°5 31°7 30°7 27°6 17°2	38.6 36.6 32.3 31.2 28.1 18.0	39°1 37°4 32°8 32°0 28°5 18°4	39.0 37.4 33.0 32.3 28.9 19.8	38.9 37.4 32.9 32.4 29.3 20.6	39.4 36.2 32.9 31.8 29.5 21.0	40°1 34°7 33°1 31°0 29°2 21°4
DECEMBER.	13 14 15 16 17 18 19	16°2 7°7 12°8 22°3 12°8 29°5	16°3 7°1 13°0 22°5 12°6 29°5	17.0 9.0 14.3 23.2 12.1 29.0	16.6 12.4 18.8 24.8 16.0 28.8	16.9 17.8 22.1 26.1 19.2 29.8	18°2 20°0 26°7 26°3 22°7 31°2	20°2 23°4 27°6 27°4 25°6 32°3	22°1 25°3 28°2 26°5 28°5 33°5	23.2 26.5 27.6 27.1 30.6 31.8	21.9 27.2 27.1 27.8 29.8 32.9	21.4 25.9 26.1 26.9 28.8 32.3	20.6 21.9 23.2 24.1 29.0 31.5
;	20 21 22 23 24 25	22°1 22°1 7°1 27°5	20°8 20°6 3°7 28°1	18.9 20.4 4.5 28.8	19.6 21.5 9.2 29.9	21·2 22·3 14·8 31·2	23°2 22°5 18°2 33°9	24.9 24.2 20.5 34.1	26.5 24.2 22.1 33.9	27.9 26.1 23.6 34.4	27.6 26.1 23.8 34.6	26°3 25°5 23°9 34°7	21.4 21.9 15.8 35.3
	25 26 27	16.6	16.6	16.7	18.8	22.9	26.7	29.7	30.3	31.5	32.9	31.5	33.0
	28 29 30 31	35·2 19·4 36·6 34·1	34.9 19.0 37.0 34.3	35°2 20°2 36°8 35°3	34.9 22.3 37.5 37.4	36°0 26°1 37°8 38°6	34.3 27.4 39.1 39.1	31.7 27.6 38.9 39.1	32.9 27.8 40.3 40.0	31·2 28·1 39·6 40·5	31.3 28.6 38.7 40.3	31.0 28.5 37.6 39.4	30°2 29°1 36°8 38°6
Hourly	y Means	24.73	24.34	24.29	25.93	27.58	29.01	29.95	30.78	31.24	31.59	30.77	29.76

					STANDA	RD THER	MOMETE	R.				
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
52.7	52.0	52.2	51.8	50°6	50.4	<b>49</b> •2	49°4	46°0	42.6	43.6	44°9	9°99
49.0	48.8	48.8	49.2	49.2	47.4	43.4	42'1	40.6	41.7	41.2	42.0	47.81
45.4	43.6	42.6	41.3	40.8	40.4	40.2	39.4	38.7	38.8	38.0	37.6	44.87
38.6 44.8	35.6 42.0	35.8 39.2	36.1 37.7	34.1 37.0	32.7 37.5	30.9 $37.5$	$\frac{31.8}{36.0}$	31.6 38.4	31·3 37·6	30.6 37.6	$\frac{32\cdot4}{38\cdot2}$	39.40 41.25
50.5	50.1	50.5	50.6	50.0	50.0		<del></del>	——			)	
_			_			49.0	49.2	49*4	49.7	49.7	50.2}	48.11
52.8	52.4	52°2 52°0	52.3	52.2	51.8	51.6	51.0	51°0	50.8 51.0	50°3 50°4	50.8	52.02 52.28
51.8	52.0 50.8	52 0 50 4	52.6 49.0	52 <b>.</b> 8 48 <b>.</b> 0	52.6 47.2	52°3 47°1	51.6 46.9	51'4 47'2	47°0	47.0	46°4	52 28 49 93
47.0	47.1	46.9	46.6	46.6	46.0	45.8	46.2	46.2	46.5	46.3	46.1	46.70
46.4	46.6	46.6	46.4	46.0	45.2	44.9	$45^{\circ}2$	44.9	44.7	44.6	44.7	45.95
44.7	46.0	46.6	47.2	47.0	46.6	44.0	44.0	43.6	42.1	42.2	$\overline{42\cdot7}$	44*61
45.2	45.0	44.7	44.6	44.6	44.4	44 0	44.0	43 6 42 4	$\frac{42}{41}$	$\frac{42}{41}.5$	42 7 7	44.64
46.2	46'6	46.4	47.2	47.7	48'1	47.5	46.8	46.4	46.4	45.8	43.3	46.14
45.5	44.6	44.3	43.9	43.6	42.9	42.9	42.4	42.4	42.4	42.1	41.9	46.14
38.8 38.8	38.6 38.2	39.7 37.6	38.0	$\frac{38\cdot2}{35\cdot6}$	36.8 34.7	36.6 33.7	36.8 34.7	36°6 35°4	36.8 36.8	36.4 38.0	36.2 37.4	39°20 38°21
42.0	42.2	44.6	45.0	45.4	44.0		0± /	55 4 —-			)	
_			_	_		31.7	31.8	31.1	31.3	31.2	29.8}	38.74
35.2	34.7	34.9	34.9	34.7	36.1	36.2	37.6	37.6	36.0	35.6	35.2	34.77
34·1 20·7	32.4 20.2	$\frac{32.1}{18.7}$	31.6 18.8	31.0	30.6 18.2	30.6 18.2	29 <b>.</b> 5 18.4	28.8 19.0	27.4 20.6	26°1 20°7	25.9 19.4	33.86 20.31
24.6	25.3	25.7	25.5	25.3	26.9	26.5	26.5	$\frac{15}{26}.7$	26.1	$\frac{26}{26} \cdot 1$	$\frac{13}{24}$ .8	25.38
36.0	36.0	35.1	35.1	34.1	34.9	35.6	35.2	$35^{\circ}2$	35.3	36.6	37.2	31.85
38.6	37.8	38.0	35.8	34.4	33.0	30.9	29.7	29.1	29.6	29.5	30.3	36.45
24.8	23.4	22.7	20.5	19•4	19.0	18.5	16.6	15.5	14.2	15.0	14.3	23.23
41.79	41.28	41.15	40.74	40.28	39.90	38.74	38.52	38*20	37.91	37.86	37.72	40.87
28.9	30.3	31.2	32*2	32*2	32.7	32.7	33.1	33.2	32.9	33.1	33.2	27:31
45.0	45.2	45.0	43.6	43.8	49.2	48.9	$\frac{66}{43}$ .2	41.2	$\frac{37.8}{37.8}$	37.0	35.2	41.07
31.0	30.3	30.1	28.5	26.9	25.9	25.3	25.6	25.7	25.7	25.8	25.8	30.50
34.2 32.0	34.5	33.3	32 <b>·</b> 3	32·3 30·4	32·2 30·2	32.0	31.8	31.9	32.0	30.9	29.9	31.92
32 U	31.1	31 0	31 0	30 4 	30 2	$\frac{-}{32\cdot 2}$	$\frac{-}{32.7}$	32.7	$\frac{-}{32.7}$	33.5	$\{33.5\}$	32.50
40.3	40.1	39.6	39.4	39.4	39.7	39.8	39.8	38.6	38.2	37.8	38.1	38.46
33.9	34.1	33.9	33.2	33.3	33.1	33.3	33.1	31.9	31.2	31.6	32.8	34'94
32.7	31.6 29.9	$\frac{31\cdot2}{28\cdot1}$	$\begin{array}{c} 31.2 \\ 27.5 \end{array}$	$\frac{31.0}{27.0}$	$\frac{31.0}{27.6}$	30.7 27.5	30°3 27°4	30 <b>.0</b> 27.1	30.0 $27.1$	$\begin{array}{c} 29 \cdot 3 \\ 27 \cdot 2 \end{array}$	28.4 $26.3$	31.49 29.69
29.7	29.5	29.5	29.2	29.2	28.1	26.2	21.2	20.4	19.6	18.4	19.0	26.04
21.3	21.7	20.2	19.4	17.5	17.1	_					- 1	18.11
19.4	18.4	16.6	 15`5	13.2	10.2	15.6 10.2	$\begin{array}{c} 15.8 \\ 12.0 \end{array}$	$15^{\cdot}4$ $12^{\cdot}2$	15.6 12.7	15°4 9°0	$\frac{16\cdot 2}{9\cdot 3}$	16.52
17.7	15.6	13.4	12.0	11.4	10.3	11.0	9.6	10.2	$\frac{12}{12}$ .	11.6	11.6	15.49
22.9	24.6	27.8	23.7	23.9	22.1	22.1	22.1	22.7	22.8	23.2	22.5	22.84
19.3	17.1	18.8	19.8	19.6	18.2	16.5	16.4	15.6	15.4	15.2	14.8	21.31
31.5	28.1 30.8	27.4 30.1	30°1 29°5	29.5 29.7	30.8 29.5	30.6	30.4	30.4	30.1	29.5	29.6	25.97
	_		_			25.3	24.5	23.6	22.8	23.6	$\frac{-}{22\cdot 4}\}$	28.96
16.4	15.0	14.8	15.2	17.3	18.9	19.6	21.7	22.9	24.4	26.5	26.0	21.63
20.4	19.4 17.6	22.1 16.7	$\begin{array}{c} 22.9 \\ 19.5 \end{array}$	23.0 16.2	22.6 12.6	20.4 13.7	16.4 15.6	8.6 15.5	13.7 15.6	11.2 16.6	$\begin{array}{c} 8.4 \\ 21.7 \end{array}$	$\begin{array}{c} 20.27 \\ 15.93 \end{array}$
35.3	36.0	35.9	35°4	35.6	36.5		70.0	70.0			ì	
33.2	33.7	34.1	34.3	35.3	36.0	21.7	21.5	21.2	21.2	20.5	$\frac{36.1}{36.9}$	30.16
1 —	_					41.1	39.5	39.4	38.7	38.8	36.1	31.13
29.5 28.4	29.3 30.7	27.4 30.8	26.1 31.8	25.7 32.4	25°3 32°9	26.8 33.1	$\frac{23.4}{33.1}$	21 <b>.</b> 9	22.5 34.9	$\begin{bmatrix} 21.7 \\ 35.4 \end{bmatrix}$	20.8 36.0	29.10 29.03
36.4	36.2	35.8	35.0	34·7	32 9 34·9	34.7	35.4	35.8	34.4	34.1	34.2	36.61
38.5	38.5	37.4	37.6	37.0	36.9	37.2	37.0	37.3	36.6	36.7	36.8	37.65
28.91	28.81	28.22	28:32	27.98	27.88	27.25	26.65	26.14	26.19	25.91	25.62	27.84

					, S	TANDARI	THERM	OMETER.					
Götti	of Mean ngen me.	0	1	2	3	4	5	6	7	8	9	10	11
Hours o Tore Tin	of Mean onto he.	18	19	20	21	22	23	0	1	2	3	4	5
	$\left(egin{array}{c}1\2\3\4\end{array} ight)$	36.7 36.1 — 34.0	36.7 35.5 — 34.5	36.2 35.7 — 34.6	35.9 35.4 — 34.9	35.7 36.7 — 35.3	35°8 36°7 — 36°5	35.9 37.4 — 34.8	35.7 37.3 — 34.3	34.9 36.8 — 34.8	34.8 36.0  34.8	33.8 35.5 — 34.9	33.4 35.3 — 35.4
	5 6 7 8 9	37.1 30.4 29.3 10.2 11.4	36.5 30.7 28.1 8.3 11.4	36.8 30.9 27.6 7.5 11.4	35.7 32.2 26.8 7.5 12.7	36°3 33°4 26°2 8°1 14°1	37.5 34.4 25.8 9.1 15.2	37.9 34.2 25.6 9.6 17.4	38°3 33°8 23°7 10°8 19°8	37.6 33.2 23.5 10.8 20.2	35.9 33.2 25.1 11.0 19.3	35°3 33°0 23°9 10°4 18°5	35.3 32.1 22.0 10.0 18.2
ANUARY.	11 12 13 14 15 16 17	- 2.1 12.9 24.9 35.5 36.9 36.1	1 '4 13 '0 25 '4 35 '7 36 '9 35 '5	1:0 13:8 26:2 36:1 37:1 33:8	6°1 14°6 27°5 36°1 38°3 33°0	10°9 16°0 30°7 36°6 38°6 32°7	11.7 17.2 31.1 37.1 39.0 32.7	12.0 17.6 32.1 38.5 40.4 33.7	12.6 18.1 34.2 40.2 42.0 30.3	13.8 18.7 35.0 39.6 41.8 28.3	14.8 18.3 34.7 39.4 40.7 24.7	14.5 17.4 33.9 38.7 39.6 22.3	13.8 15.5 33.0 37.8 40.2 18.5
JAN	18 19 20 21 22 23 24	31°1 10°8 6°2 14°0 7°5 22°5	32.5 9.2 6.0 13.5 7.1 23.3	32.7 9.3 7.1 12.9 6.5 24.8	33·1 8·9 9·8 13·3 8·5 27·7	34.0 10.4 14.4 13.8 8.5 30.1	35°3 11°0 18°3 13°3 11°3 32°5	35·2 11·4 20·1 9·8 11·3 32·5	35°2 10°8 20°8 9°8 13°8 32°8	35.2 11.4 21.4 8.7 14.2 33.0	34.2 10.6 21.5 6.5 14.1 33.0	33.4 9.6 21.3 5.9 14.6 33.4	32·3 8·2 20·0 4·6 15·3 30·2
	24 25 26 27 28 29 30 31	18.1 25.9 12.5 3.8 21.4 22.2	18.1 29.3 12.7 4.8 23.3 21.9	18°3 32°8 13°3 4°9 24°3 19°2 —	21:3 33:2 15:1 8:6 25:6 19:3	24.5 33.8 15.7 12.3 27.5 19.3	25 · 4 34 · 4 15 · 7 16 · 7 29 · 1 17 · 8	25.8 34.6 15.5 19.3 30.9 18.1	25.6 32.5 15.9 20.4 32.5 17.8	25°8 28°6 15°8 21°4 33°2 17°8	25.8 26.8 15.6 22.5 30.9 16.7	25°8 26°6 14°4 21°8 29°3 15°7	25·1 26·5 12·2 20·3 28·5 14·0
Hourl	y Means	21.75	21.97	22.11	23.12	24.45	25.41	25.83	26.15	25.98	25.42	24.75	23.70
	1 2 3 4 5 6 7 8 9	23.8 28.6 37.9 12.2 10.6 13.7 — 29.0 29.0	24.6 28.8 37.9 12.4 9.6 12.4 	25·1 31·3 37·9 12·2 9·9 13·9 — 29·0 27·1	25.9 34.8 37.6 13.2 12.1 16.0 	28·1 38·9 37·5 15·1 13·7 17·8 	30.5 39.2 37.4 17.2 15.6 20.1 — 34.3 32.2	32·1 39·7 37·6 19·3 17·9 23·0 — 34·7 32·3	32.8 40.2 37.9 22.4 19.3 25.7 — 35.7 32.6	32.4 40.6 35.7 23.6 21.5 27.3 — 35.2 32.3	32.8 39.9 32.4 24.2 21.7 28.3 — 35.7 31.8	32.6 39.2 29.3 23.0 22.0 28.5 — 35.3 32.0	31.7 39.1 26.3 21.8 21.7 27.7 32.3 31.1
FEBRUARY.	10 11 12 13 14	26.9 16.7 13.3 16.0	27.0 17.0 14.9 15.8	26.7 16.3 14.3 16.0	28.5 17.8 17.0 17.9	29.8 20.7 20.9 21.4	31.8 21.3 23.2 23.6	32.4 21.6 23.8 24.5	35°3 22°2 25°1 24°9	34.8 21.7 27.1 25.7	33.8 21.6 24.3 25.7	32°1 21°3 22°5 25°6	29.4 19.7 20.4 25.3
FEBR	15 16 17 18 19 20 21	29.8 17.8 21.0 22.0 28.1 26.7	29.0 12.2 21.0 22.2 27.6 26.2	27.8 17.0 21.3 24.2 27.5 25.5	26.8 17.8 24.9 26.2 27.1 24.0	27.4 13.1 29.2 30.2 27.9 23.0	26.5 13.4 31.3 32.3 29.8 22.8	24.7 14.0 30.2 33.2 30.9 23.6	24.0 21.8 30.9 34.6 30.9 23.2	23.0 23.4 31.1 33.5 32.3 22.8	23°1 24°7 32°3 33°1 32°7 23°0	22.8 23.8 32.3 32.5 32.3 22.4	21.3 20.7 30.5 31.7 31.3 22.2
	22 23 24 25 26 27 28	15.8 4.4 3.6 18.3 9.1 26.9	15.8 3.2 2.8 17.8 10.3 27.1	15.9 4.6 7.4 18.1 17.3 28.5	16.6 7.2 10.0 21.1 21.8 27.6	17.8 9.7 15.4 23.4 26.9 28.3	20°2 11°7 19°7 24°9 27°8 29°4	19.7 14.3 21.8 25.9 27.5 29.8	20.7 15.7 22.8 26.2 27.7 30.4	20°5 17°4 23°0 26°6 27°1 31°1	20.9 17.9 23.2 26.5 26.3 31.2	20°9 18°7 22°2 26°0 25°9 32°2	20.7 16.8 21.8 24.6 25.7 32.5
Hourl	y Means	20.02	19.65	20.62	22*16	24.14	25.68	26.44	27.63	27.90	27.80	27:31	26.10

					STANDA	RD THER	MOMETEI	R.				
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
0	•	0	•	0	o	0	0	0	o	0	o	٥
32.8 35.4	32.5 35.4	$\frac{32.8}{34.9}$	32.5 35.1	32 <b>·</b> 9 35 <b>·</b> 1	34°1 35°1	35.0	34.8	36.3	36.3	36.5	36·1	34°91 34°33
35.4	 37·1	36.7	38.2	39.8	42.2	25°1 41°6	24.7 40.6	30°2	38.6 31.9	$\begin{array}{c} 33.4 \\ 37.4 \end{array}$	33·2 } 37·3	36.79
$\frac{35.7}{31.7}$	35 <b>.</b> 9	36.1 36.1	35.5 30.7	35.5 30.4	35.5 30.2	34.2 29.8	33.0	33.0 29.8	$\begin{array}{c} 30.2 \\ 29.9 \end{array}$	30°2 30°1	30.0 30.3	35.22 31.21
19.1	17.4	16.4	15.9	16.8	14.4	14.8	13.8	12.9	15.1	14.9	12.9	20.20
10°3	10.3	10°2 18°1	9°5 17°4	$8\overset{\cdot}{3}$	8'4 17'0	$\frac{-}{6.3}$	<del></del> 9.9	10.5	10.4	10.8	— ) 10.8	9.65 12.88
						7.5	5.0	$\begin{array}{c} 2.4 \\ 12.2 \end{array}$	$0.0 \\ 12.3$	$0.0 \\ 12.2$	$-\frac{-}{1.2}$	10.61
13°1	12.5 13.5	$\begin{array}{c} 11.7 \\ 14.2 \end{array}$	11.7 15.1	11.9 15.2	$\begin{array}{c} 11.8 \\ 15.1 \end{array}$	13.2	12°1 20°7	22.0	20.8	23.3	24.5	16.84
32 <b>·</b> 3 37 <b>·</b> 1	32.4	31.9	32.7	32.5 36.3	$36.3 \\ 33.3$	35°1 34°7	35°8 35°3	35.7 35.3	36°1 35°7	35°9 36°7	35°9 37°0	32.43 36.83
41.1	36 <b>.</b> 4 41.1	$\begin{array}{c} 35.7 \\ 42.7 \end{array}$	36°1 42°2	42.2	42.7	41.6	41.2	40.1	38.6	37.8	36.1	39.95
16.1	14.5	13.3	12.9	12.3	12.0	22.2	23.3	24.7	26.4	27°0	$\frac{-}{28\cdot 7}$	24.78
30.7	30.0	29.1	28.1	26.8	24.9	24.5	22.3	20.1	17.4	14.4	13.8	28.62
7.8 19.4	7°1 18°9	6°9 18°1	7°4 16°9	$7.4 \\ 16.9$	7.3 $15.3$	7°3 14°4	$7^{ullet}2$ $13^{ullet}5$	6.8 14.2	6.8 14.0	6°8 14°4	$\begin{array}{c} 6.5 \\ 14.2 \end{array}$	8.62 15.73
3.8	2.2	3.9	5.8	5.6	5.4	5.4	5.6	6.0	6.2	6.9	6.9	7.92
14.6 28.9	13.5 26.2	15°1 25°1	16.1 23.3	18 <b>.</b> 9	19.6 22.4	20.2	20.2	20.1	19.9	20.7	22.2	14.77 25.28
					_	16.5	17.0	17:3	17.6	17.6	$\begin{bmatrix} -17.4 \\ 25.5 \end{bmatrix}$	25 28
25.1 $26.4$	$25^{\circ}1$ $24^{\circ}2$	26.0 23.5	$\begin{array}{c} 26.8 \\ 22.2 \end{array}$	26.8 22.0	$\begin{array}{c} 26.1 \\ 22.2 \end{array}$	24.8 22.2	24.4 18.9	$\begin{array}{c} 27^{\circ}2 \\ 17^{\circ}2 \end{array}$	28°1 17°0	26 <b>·</b> 9 15 <b>·</b> 3	14.0	25.42
10.4	8.3	6.8	6.0	5.2	5.0	4.8	4.0	3°0 19°5	$\frac{2\cdot1}{20\cdot0}$	$\begin{array}{c} 2.6 \\ 19.7 \end{array}$	3.8 20.5	9.85 16.79
19.9 $28.4$	18.1 $28.3$	18.3 $27.0$	17.4 26.3	16°1 25°6	19 <b>·</b> 9 24 <b>·</b> 4	17.6 $23.0$	$\begin{array}{c} 19.1 \\ 22.2 \end{array}$	$\begin{array}{c} 19.5 \\ 22.7 \end{array}$	23.8	23.8	23.3	26.47
12.1	11.0	10.6	10.6	10.3	10.1	24.3	23.0	23.0	22.3	22.1	$\frac{-}{22\cdot 4}\}$	17.57
23.03	22:36	22.16	22.03	21.93	21.95	21.98	21.44	21.28	21.44	21.44	21.29	23.06
				22.0	22.5	2112	2011	0010	0014	9017	00.0	20:00
31.7 40.0	31°3 40°4	32.1 39.9	31 <b>.</b> 9	31.2 37.9	30 <b>·</b> 9	31.3 38.1	29 <b>.</b> 4 37.9	28°3 38°3	30°4 38°6	$\begin{array}{c} 30.5 \\ 37.5 \end{array}$	29 <b>.</b> 0 36 <b>.</b> 9	30.02 37.59
23.6	21.7	19.9	18.7	17.4	16.6	16.6	16.7	15.2	14.4	13.8	12.6	26.36 16.88
$\begin{array}{c} 20.3 \\ 21.7 \end{array}$	$\begin{array}{c} 19.1 \\ 22.2 \end{array}$	17.8 21.1	16.8 20.7	16.2 19.8	16.0 18.4	15°4 18°1	14.2 18.0	14'1 16'2	13.6 15.8	13'0 14'1	11.6 13.4	17:30
24.7	22.4	22.5	21.7	20.9	20.9	20.5	25.7	26.7	27.9	27.9	$\frac{-}{26.5}$	22.60
31.7	31.7	31.1	$\frac{-}{32\cdot 1}$	32.4	32.8	32.4	3 <b>2</b> .2	31.9	31.1	31.2	30.5	32.23
30°2 28°8	29.6 26.9	29°4 26°3	$29.6 \\ 24.2$	29 <b>.</b> 6 20.3	$28\cdot2$ $17\cdot4$	29.4 15.6	25 <b>.</b> 1 12.8	23.0 11.7	$\begin{array}{c} 21.2 \\ 15.0 \end{array}$	24.4 15.5	26.0 12.8	28.91 24.95
18.7	17.9	17.4	16.4	17.5	17.5	17.1	17.0	17.0	16.1	14.4	12.4	18.22
19°3	18.6 24.0	23.9 18.1	16.7 23.2	15.9 23.0	10.6 23.0	11.6	13.7	14.9	16.8	17.9	16.6	18.23
			_			29.6	29.5	30.0	30.2	29.8	$\frac{-}{29.6}$	24.30 22.23
20.5 21.5	20.7 22.4	$20\overset{\circ}{.}3$	19.5 $23.5$	18'1 20'3	17.0 19.1	16 <b>°</b> 8 19°3	17 <b>'</b> 9 20'1	19.8 19.1	19 <b>'</b> 7 19'8	18.9 50.0	19.9	19·48
29.4	27.1	25.7	22.7	20.5	19.6	16.9	16.0	16.6	16.6 28.6	19.6 28.1	21.0 27.9	24.49
30.8 30.8	30.8 30.0	29°1 30°5	28.5 30.5	28 <b>·</b> 1	28.1 29.8	28.1	28.5 29.2	28.6 29.0	28.2	28.1	27.3	29.13 29.68
22.2	22.2	22.0	21.8	21.2	21.7	 18 <b>°</b> 4	17.8	 17`0	16.4	16°4	16.0}	21.62
20.6	19.5	17.6	15.6	11.7	10.6	9.9	8.7	8.5	7.0	6.2	7.9	15:39
10°8 21°1	$\begin{bmatrix} 6.0 \\ 21.2 \end{bmatrix}$	$4.2 \\ 22.3$	6°4 21°1	7°8 21°4	$\frac{5.2}{21.3}$	$\begin{array}{c} 1.6 \\ 21.7 \end{array}$	$\frac{4.6}{20.9}$	5°2 20°1	5'4 20'1	4.6 20.1	4°0 19°6	8.64 18.53
21.4	15.0	12.6	13.7	13.0	12.8	13.0	12.1	9.9	9.1	9.1	10.8	18.00
26.1 33.1	26.5 33.1	26.9 33.1	$\frac{28\cdot2}{33\cdot1}$	28.5 32.1	28.3 31.1	28.5	28.5	28.2	28.1	28.1	28.1	25·31 28·08
						20.3	20.2	21.3	21.1	20.6	19.6}	20 00
25.13	24.18	23.57	23.15	22:30	21.43	20.81	20.72	20.43	20.49	20.42	20.06	23.26

					S	TANDARI	THERM	OMETER.					
Iours of Göttin Tim	f Mean }	0	1	2	3	4	5	6	7	8	9	10	11
lours of Toro Tin		18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{pmatrix}$	20°1 19°2 23°0 13°9 12°2 28°8	20·3 18·4 27·0 14·2 9·8 29·4	22·2 21·2 27·8 21·3 12·8 31·9	24·2 23·0 29·3 25·7 18·8 34·0	24.9 24.6 31.4 27.5 25.2 34.5	26.4 26.0 33.8 29.0 28.4 36.5	27.8 28.7 34.8 30.8 28.9 35.7	28.9 30.7 34.0 32.0 29.9 35.6	29°6 30°9 35°8 33°0 31°0 35°5	29.6 30.2 36.0 33.3 30.5 35.1	28.9 29.2 36.0 32.2 30.5 34.0	27.9 27.0 35.5 31.6 30.4 34.5
	7 8 9 10 11 12 13	25.0 19.1 22.7 15.0 6.1 10.3	26.3 19.1 23.4 15.2 6.8 9.9	28.8 18.8 27.3 17.1 10.6 12.6	30.0 20.3 31.0 19.6 15.3 15.4	31.6 21.8 33.8 20.1 17.8 19.4	34.6 21.8 35.2 20.6 19.1 21.8	35.8 21.5 36.1 20.8 20.2 23.6	36.2 21.3 36.8 21.7 21.3 24.3	31.7 21.4 37.1 22.5 22.5 26.9	32.0 21.4 37.1 22.5 23.4 26.5	31.7 21.3 36.4 21.9 22.5 25.1	31 · 2 20 · 9 35 · 5 21 · 6 21 · 5 24 · 6
MARCH.	14 15 16 17 18 19 20	13.9 10.0 15.0 29.2 24.6 32.9	15.2 10.2 16.5 30.2 26.3 33.1	16.4 13.0 20.0 32.5 29.8 33.1	17.9 15.0 23.8 34.6 31.3 34.5	19.7 18.3 27.0 35.1 34.7 35.7	22.7 19.5 32.0 38.1 36.0 37.2	21.5 22.7 33.5 38.6 37.3 39.0	24.3 20.2 33.1 38.9 36.6 39.9	24.4 24.0 35.1 40.3 36.4 38.4	22·3 22·7 34·6 40·2 37·0 38·6	22.1 21.7 34.3 42.8 37.3	21.5 22.0 33.8 42.1 34.9 37.1
	21 22 23 24 25 26 27	25.7 33.8 28.2 34.5 32.4 18.5	27.3 34.7 29.2 33.5 31.5 17.9	29.6 34.7 30.3 38.6 32.4 18.9	30.7 34.9 32.1 44.2 32.0 20.5	31:3 36:1 33:2 44:1 33:1 22:1	31.6 37.5 34.9 42.5 33.8 23.3	32.0 40.2 35.4 42.1 35.3 23.8	32·2 39·2 37·3 41·2 36·1 24·4	32.0 41.6 37.3 42.5 37.4 24.7	31.8 41.6 38.7 42.4 36.7 25.5	31.7 40.4 37.9 41.6 34.8 25.5	32.0 39.8 36.7 40.1 34.3 26.5
	28 29 30 31	32°0 23°6 14°3	34.0 23.8 16.2	37·4 26·9 17·9	40.7 26.5 18.7	42.5 27.1 20.8	43 · 4 28 · 4 22 · 3	44.4 27.8 24.3	43°1 26°7 25°5	40.8 26.5 26.1	38.5 25.7 27.0	36.9 24.8 27.0	35.0 24.7 26.1
Hourly	Means	21.66	22.20	24.29	26.81	28.64	30.24	31.51	31.53	32.05	31.89	31.33	30.70
į	1	9.5	13.9	19.2	27.5	29.8	31.3	31.8	32.4	32.2	33.3	32.8	31.7
	$\begin{bmatrix} 2 \\ 3 \\ 4 \end{bmatrix}$	28.6	31.9	34.5	38.2	40.0	42.2	42.6	41.9	41.1	41.2	39.9	39.6
	5 6 7 8 9	31.4 38.3 40.0 41.9 34.3 38.5	36.7 38.8 42.4 41.7 35.3 44.2	39.7 41.5 42.9 43.1 36.6 45.2	40.8 43.1 43.6 45.4 39.5 46.2	41'9 44'4 46'3 48'1 41'3 48'4	41.7 46.5 48.4 49.9 42.9 47.4	41.5 44.0 50.6 58.3 45.0 47.6	41.8 45.6 52.2 58.3 43.8 49.2	42.2 46.1 53.9 55.0 45.5 48.5	39.8 48.4 55.6 55.8 46.3 44.3	40°1 49°1 55°5 59°9 45°7 44°5	38.4 50.1 55.2 56.9 43.6 40.7
APRIL.	11 12 13 14 15 16 17	33·5 29·3 31·7 31·7 25·9 33·8	36.5 36.8 35.4 33.0 29.2 33.4	44.2 40.5 39.4 34.3 32.3 34.3	46.1 42.6 43.5 35.7 37.6 35.1	48.7 44.0 45.6 34.9 38.5 36.0	48.7 44.5 46.3 37.7 38.6 36.2	48.3 46.5 45.8 37.4 40.0 36.2	48.7 46.9 46.3 36.9 40.5 35.5	47.1 47.1 45.9 37.6 38.4 33.7	47:4 45:7 45:5 38:9 36:4 33:0	46.9 45.7 43.4 37.1 37.0 33.4	45.5 44.6 41.5 37.7 36.9 32.0
	18 19 20 21 22 23 24	29.6 34.4 42.6 49.3 36.3 31.0	31.3 36.0 41.6 49.9 36.4 34.5	33°1 37°4 43°4 52°4 36°9 38°5	35°1 39°7 45°4 51°2 38°9 41°6	36.7 41.7 45.9 51.0 40.0 43.0	39.8 44.5 54.4 49.3 40.7 44.0	42.7 46.2 57.0 47.9 41.2 44.8	42.5 45.1 63.3 46.9 41.0 45.4	44.0 44.6 65.5 45.9 42.9 45.2	44.4 43.6 65.4 45.5 45.9 41.7	45°9 43°0 65°0 45°3 42°8 45°5	45.4 43.2 62.7 45.3 43.2 45.4
	25 26 27 28 29 30	47.9 43.8 30.5 34.9 36.7	49°1 44°5 33°7 35°5 37°1	50°7 43°8 36°8 36°1 37°9	53.2 42.4 40.0 36.5 40.7	55.8 42.0 40.2 36.1 41.9	58.4 42.9 42.5 37.3 43.6	59 · 9 43 · 4 43 · 2 39 · 2 44 · 5	58°0 43°6 40°7 39°7 45°0	58.5 44.6 40.1 41.6 47.5	56.5 43.8 39.6 45.1 48.1	58.5 42.6 37.1 41.5 44.5	58.5 41.1 37.3 39.7 41.9
Hourl	y Means	34.60	36.75	38.99	41.50	42.49	43.99	45.02	45.25	45.39	45.37	44.91	43.9

•						STANDA	RD THER	MOMETE	3.				
•	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
	6	7	8	9	10	11	12	13	14	15	16	17	Means.
	26.4 24.6 33.6 30.5 28.2	26°1 24°4 31°7 29°2 24°5	25.4 24.3 31.3 27.8 25.6	25.7 23.7 25.6 26.4 26.8	25·2 23·5 24·2 22·0 26·2	24.4 23.4 20.0 20.1 25.2	24°0 21°2 20°9 18°5 25°1	23°5 21°5 19°1 16°2 26°6	23°5 20°5 22°9 15°9 27°6	22°0 20°1 24°4 13°6 28°0	21.6 21.2 24.3 13.6 27.6	19°5 22°5 18°4 14°1 27°3	24.92 24.17 28.37 23.85 25.30
	32.6 	32.6 	32.8 	33.1 20.8 24.0 24.3 14.0	32.5 20.0 25.2 21.6 11.5	32.6 	39.1 18.9 24.8 20.1 8.9	38.8 18.8 23.0 19.8 8.6	34°1 18°5 22°9 19°3 6°1	33°2 18°6 22°2 17°1 4°8	30°1 18°9 22°4 16°5 5°0	$\begin{bmatrix} -28.2 \\ 19.1 \\ 22.5 \\ 14.5 \\ 4.9 \end{bmatrix}$	33.55 25.89 21.97 27.57 15.28
	19.5 22.4	19°1 20°4	16.8 10.0	15.8 18.6	14°1 18°3	13.2 18.3	$\frac{13.3}{-26.5}$	12.9 - 24.0	$\frac{13 \cdot 2}{22 \cdot 3}$	13.2	$\frac{12.3}{16.7}$	$\frac{11.1}{15.4}$	15.91 20.10
	19.4 21.7 31.7 39.1 31.9 37.1	17.5 20.4 30.8 36.3 29.6 37.1	16.3 19.0 30.7 33.6 28.4 36.8	13.9 17.3 30.3 31.9 26.9 39.1	13.6 15.7 29.9 29.9 28.6 36.1	-13.6 $14.7$ $30.0$ $28.7$ $29.9$ $35.1$	13 · 9 13 · 9 30 · 2 27 · 6 29 · 2	12.7 13.2 30.2 26.9 30.3	12·4 13·0 29·8 26·2 31·3	12·2 12·5 29·1 26·3 32·2	10 7 12 1 13 6 29 6 26 2 32 4	10.5 15.5 29.6 24.9 32.5	17.08 17.08 29.19 33.34 31.89
	32·4 39·7 35·0 39·0 32·2	32.4 37.1 33.1 37.6 32.0	32.4 36.3 32.8 36.9 32.2	32·2 36·3 32·2 36·4 31·4	32°3 34°6 32°6 36°0 30°1	32.6 34.3 30.7 35.0 29.2	27 ' 3 33 ' 2 33 ' 2 30 ' 7 33 ' 8 28 ' 0	25'4 33'1 32'5 31'2 34'7 27'1	24.6 33.0 32.1 32.9 33.7 25.9	24.6 33.2 31.4 34.1 33.5 24.6	24.7 33.5 31.1 34.1 32.4 23.9	24.5 } 33.7 30.7 32.0 19.7	33.72 31.75 35.99 33.51 37.85 31.09
	25.5  31.8 22.2 23.8	24.9 — 30.8 22.1 21.7	23.6 	22.3 	22.0 ———————————————————————————————————	22·3 — 26·7 21·0 13·2	32·2 26·2 21·0 15·2	32·3 25·7 20·8 13·0	32·2 25·5 20·4 13·0	31.9 25.5 18.4 10.3	32.6 25.1 17.8 8.4	$\begin{bmatrix} -1 \\ 32 \cdot 9 \\ 24 \cdot 7 \\ 16 \cdot 2 \\ 8 \cdot 8 \end{bmatrix}$	25°26 33°12 23°27 18°56
-	28.97	27.67	26.87	25.80	24.74	24.06	24.33	23.77	23.44	22.85	22.21	21.75	26.65
	31.0 38.7 —	29.9 35.9	29.6 33.1 —	30.1	30.8 30.7	31.2	33.0 - 37.4	29.6 — 36.8	29.0 — 36.9	36.9 31.3	29.6 - 32.8	$\begin{bmatrix} -1 \\ 28 \cdot 0 \end{bmatrix}$	28.68 36.51
	36.9 48.4 48.3 46.6 41.5 41.6	35.8 46.3 44.2 44.5 39.2 39.0	35.9 44.7 40.8 43.2 38.7 38.6	36.1 44.0 40.1 41.6 38.3 37.8	36 1 42 1 38 0 41 2 37 0 36 6	37:3 41:6 36:6 40:7 36:9 35:8	37·3 41·2 38·3 39·0 37·1	37.9 41.0 37.8 38.1 37.7	37.7 40.4 38.1 36.3 37.5	36.6 40.4 39.2 35.4 37.5	37.4 40.4 40.3 34.9 39.6	38.1 39.8 41.4 34.7 38.7	38°25 43°59 44°57 45°44 39°98
	43.0 42.1 40.3 34.9 36.9 31.0	40°3 39°1 39°7 35°1 36°2 28°0	38'3 37'9 39'3 31'4 35'0	37.2 36.9 39.2 29.7 34.8	36'4 36'1 35'8 29'1 34'0	35°3 34°9 33°3 28°0 33°6	34.5 35.1 34.5 33.7 28.2 33.1	35.4 35.0 38.7 33.3 27.5 32.2	35.4 33.8 36.3 32.9 27.5 32.6	35.5 31.1 34.9 32.8 25.9 32.2	35'9 29'6 34'0 31'8 25'1 33'3	34.9 27.8 32.0 31.7 24.2 33.5	41.07 40.19 39.65 38.92 32.48 34.95
	41.9 43.1 59.8 44.7 41.5	37.7 43.2 58.5 44.4 35.7	26'4 	25.4 38.9 43.9 59.7 41.1 33.7	23.7  37.1 44.4 59.5 40.8 32.6	23°1 36°3 43°8 58°1 40°5 32°0	26.1 34.9 44.8 55.6 39.7 30.5	24.8 32.3 44.0 52.0 37.1 29.7	26.3 30.5 43.6 53.8 36.9 30.0	27.2 29.7 43.7 55.6 36.7 29.7	28.5 29.7 44.6 54.4 36.3 29.8	29.6 32.0 44.6 52.2 35.9 30.1	30°53 37°13 42°76 55°50 44°05 36°51
	44.6 	40°2 46°5 35°7 35°5 37°7 39°8	37.7 45.2 33.5 34.8 36.9 38.4	34.8 -43.8 32.3 34.3 35.5 36.6	34.2 44.6 30.9 34.5 35.5 35.7	33.8 45.8 28.7 34.8 36.1 33.5	44.4 46.6 28.6 34.8 37.1 33.5	43:3 46:5 28:7 34:3 40:5 32:0		42:3 46:3 26:2 34:5 39:3 29:1	41.6 45.0 25.1 34.5 38.3 27.8	$-44\cdot3$ $42\cdot5$ $24\cdot2$ $34\cdot5$ $37\cdot1$ $29\cdot2$	41.15 50.75 36.59 36.65 38.20 38.19
	41.87	39.52	38.43	37.50	36.40	36.08	36.76	36.25	35.87	35.60	35.51	34.97	39.69

					S'.	TANDARD	THERMO	METER.					
Hours o Göttir Tir	of Mean }	0	1	2	3	4	5	6	7	8	9	10	11
Hours of Tore Tir	of Mean onto me.	18	19	20	21	22	23	0	1	2	3	4	5
	/ 1	0	<u>•</u>	•	<u>°</u>	<u> </u>	0	<u>•</u>	<u> </u>	<u> </u>	<u> </u>	° —	0
	3		_		_	_	_	_		<u> </u>		_	_
	4 5	$\begin{array}{c} 38.8 \\ 36.9 \end{array}$	44.1 46.6	48 · 1 51 · 5	49.8 53.3	52·7 57·0	53.7 59.0	55.6 $59.2$	54.7 61.7	52.5 61.5	61.1 23.0	52.6 60.6	51.8
	6 7	40.5 41.6	46°8 50°5	53.6	54.9 56.5	57°3 57°8	60°2 59°0	63.5 59.6	62.8 61.4	61.3 62.4	59.6 58.0	57.7 59.2	57:3 60:4
	8 9	48'1	49.6	52.2	57.0	56.4	55.7	56.3	57.2	62.4	64.7 61.5	64.6 61.6	60.7
	10 11	48.8 52.5	52.5 52.5	55.9 53.7	58.0 59.8	59.8 63.1	59.8 64.1	59°4 64°7	59.7 64.0 66.4	61.7 63.4 64.9	63.6 61.6	59.8 62.2	58.9 61.2
	12 13	54.2 54.7	55.4 58.0	60.0	60.0	63.4	65.3	66.2 60.8	63.2	63.2	63.8	64.2 60.6	64.1
$\left[\begin{array}{c} x \end{array}\right]$	14 15	53°1 47°6	58°5 56°1	69.9 29.2	63.8	59.4 64.4	59.0 66.2	57.6 67.2	56.8 66.8	56.8 68.3	58 <b>.</b> 1	67.4	65.3
MAY.	16 17 18	46.0 47.1	52.5 53.7	58.8 58.5	61 ° 0 62 ° 3	63.7 64.6	61·4 67·1	63.3	64.7 69.8	64.9 66.7	65·3 67·6	65°8 67°4	65°1 67°2
	19	50·4 49·6	54·1 52·9	58·5 56·3	61·2 60·5	64·9 62·1	63 · 0 62 · 3	$\begin{array}{c} 63 \cdot 2 \\ 63 \cdot 0 \end{array}$	$\begin{array}{c} 65.7 \\ 62.8 \end{array}$	63.0 69.0	65 · 7 62 · 3	65°3 61°8	65.7 58.4
	20 21	48.3	50.6 60.4	50.8 58.8	53.5	52·7 64·9	55.4 68.8	59.0 68.4	62·2 64·5	62.8 67.0	63·3 67·0	60.7 64.6	58.8 61.4
	22 23	57.2  55.8	57.2	58.0	57.3	58.0	58.8	59.7	61.9	63.1	63.1	64.8	63.7
	25	50.2	53.7	57.7	61.1	61.8 49.1	$62.9 \\ 52.1$	63·2 52·2	65.5 52.9	66.3 23.5	63.0 56.4	58.9 58.1	60·1 56·9
	26 27	39.6 45.3	41.7 50.9	44.7 54.2	46°9 54°7	56.9	58.7	5 <b>7</b> .6	56.0	58.3	58.2	58.9 67.8	59·5 66·9
	28 29	54°1 57°5	54.0 55.7	56.8 56.8	56.9 62.9	64 <b>°</b> 0	61.2 68.0	71 <b>.</b> 9 59.3	72.4 58.3	72 <b>.</b> 4 62 <b>.</b> 1	68°8 64°6	60.7	65.7
	30 31	48.2	47.7	47.6	47.0	45.9	45 2	44.2	44.5	44.5	44.5	44.4	44.4
Hourl	y Means	48.61	52.34	55.19	57.56	59.23	60.32	61.03	61.48	62.02	61.85	61.25	60.64
	$\begin{pmatrix} 1 \\ 0 \end{pmatrix}$	45'9	45'9	48.2	52°8 56°2	55.6 58.9	60.7 60.5	62·3 62·9	60.9	60°5	59.9 56.0	58.6 60.3	57·7 61·5
	$\begin{bmatrix} 2 \\ 3 \end{bmatrix}$	52.6 48.7	53.0 52.6	54.6	56.5	57.6	59.2	62'4	61.6	58.6	59°4 58°1	58·3 55·0	56·2 53·8
	$\begin{bmatrix} 4 \\ 5 \end{bmatrix}$	54.7 41.9	56.0 44.8	58.7 49.1	57.7 50.4	53.8 58.9	61°3 57°1	62.7 59.9	59°7 59°5	59 <b>·</b> 9	62.0	64.0	63.3
	6 7	50.8	55.0	62·1 55·7	$\begin{array}{c} \overline{64.7} \\ 57.1 \end{array}$	65.3 	66.9 58.9	67·7 58·2	70·1 58·7	70°8 61°5	70·3 62·1	67.5 60.6	$64.5 \\ 58.1$
	8 9	55°2 56°3	55.6 58.4	62.2	66.0	66.7	68.2	69.1	72.7	74·1 63·9	74·1 64·8	75.5 62.7	72·5 62·9
	10 11	63°2 58°0	63.7	64.8 65.0	63.7 66.7	63.1 65.3	63°1 67°0	63.6 62.7	63.7 65.1	61.2	59·4 65·7	58·5 66·9	57·3 66·3
	12 13	49'1	52.8	57.7	59°9  50°4	60°5 	60.7	62.3	64.6  44.6	65°2  44°6	48.2	48.6	49.1
JUNE.	14 15	39.8 39.8	55.0 41.3	42.9	44.6	46.3	50°0 47°6	48.2 48.7	52.0	55.7	57·9 56·3	58.9 57.1	58.5 56.7
JU	$\begin{bmatrix} 16 \\ 17 \end{bmatrix}$	46°9 48°5	49°1 53°0	51.8 57.5	53°5 59°7	55.3 60.3	56.0 60.9	56.1 62.3	54.8 61.5	55.0 63.2	65.0	68.2	67.7 59.3
	18 19	52.6 56.0	$\begin{array}{c} 58.3 \\ 56.2 \end{array}$	58°3 57°9	60°9 59°7	61.7 62.1	64.8 62.1	65.8 61.3	65.6 62.6	64.9 60.2	64·2 61·5	62.4 65.6	67.4
	20 21	55.6	59.5	63°1 53°4	63 '9 59 '7	$\frac{-}{65.2}$	65°2 65°7	67.0 67.0	67°3 68°7	59°4 68°5	63.0 62.9	60.3 60.3	67·1 63·3
	.22 23	53°3 57°1	54.8 61.7	64.8	67.7	67.8	69.9	69.6 72.3	70·1 72·3	70°1 73°4	71·4 73·7	70°7 74°1	67.6 74.9
	24 25	57.4 60.3	64.1 65.3	66.7 63.5	69.1 66.9	$71.7 \\ 69.2 \\ 75.9$	72.7 71.1	71·5 75·8	73·5 76·5	73·9 74·5	75·3 76·5	72.9 74.3	68.7 74.7
	26 27	63.7	68.2	72.9	74.9	75.2	78.2	69.9	73·1	74.1	75°2	74.3	70.7
	28 29	62.1 59.3 58.0	62.7 60.8 63.0	63°1 62°5 68°8	66.8 64.7 70.9	68.1 66.6 71.5	67.7 68.8 69.7	70·4 72·0	70·8 72·1	72·7 72·4	68·1 70·9	68.3 70.8	69.6
Hourl	30 y Means	58.9	56.73	58.98	60.97	62.24	63.64	64.30	64.77	64.24	64.70	64.64	63.76

						DIMINDI	KD THEK	MOMETEI	.bo				
- 1	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
	6	7	8	9	10	11	12	13	14	15	16	17	Means.
-	0	0	<u> </u>	<u>•</u>	<u> </u>	0	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u>°</u>	0	<u> </u>
-	_	_						_	_	_	_		_
	9.8	48.0 50.1	46.8 48.3	44 <b>.</b> 9 45.6	42 <b>.</b> 4 42 <b>.</b> 4	38.3 40.6	$\frac{38.5}{39.8}$	$\frac{43\cdot 4}{37\cdot 2}$	$\frac{42.6}{36.7}$	39 <b>·1</b> 36·7	35°1 36°0	33.4 35.9	46°24 48°29
5-	4.8	49.7	47.4	45.9	46'1	43.9	43.2	42.2	40.4	39.6	39.5	38.0	50.17
	9·4 8·6	56°2 57°2	55.9 57.6	50.6 $57.3$	49°2 57°4	53.3	54°7 —	55 <b>·</b> 2	26.0	57°5 —	57:3	— ₹ — ₹	56°05 55°35
-	6.3	55.7	54.4	53.2	52.8	 54·7	48°5 54°6	48°3 54°3	51.3 53.3	51.8 51.9	50°2 53°1	$\frac{-}{48.6}$	56.11
57	7.7	54.1	53.7	53.7	53.5	55.1	56.0	54.2	53.4	53.1	54.3	<b>5</b> 5.6	57.27
	0.0	61.0 59.6	61.0 57.7	60°5 53°8	59°8 52°0	60°0 52°1	57°3 51°1	58.1 50.0	57.7 50.4	55.7 49.7	53.5 49.5	$\begin{array}{c} 54.3 \\ 48.3 \end{array}$	60°05 57°15
5	7.0	56.6	53.8	52.5	49.6	49.8	45.6	44.1	43.4	42.7	42.9	42.3	53.40
66	2.0	59.5	54.7	52 <b>.</b> 4	51.8	51°4 —	51.6	52.2	51.0	47.3	45.3	${43}\cdot_{2}\}$	57.88
	3.4	61:7	61.2	59.3	56.2	52.3	55.2	54.5	50.8	46.3	45.3	45°1 48°3	57°66 58°46
	$\begin{bmatrix} 5.2 \\ 5.3 \end{bmatrix}$	59.7 63.7	56.7 60.3	$\begin{array}{c} 54\cdot 2 \\ 59\cdot 2 \end{array}$	53°4 58°7	52.0 56.4	51.8 55.8	50°9 54°1	50.0 52.9	49.8 51.6	49.8 50.1	48 3 50.8	59.28
57	7.4	54.7	53.6	50.6	49'4	47.7	46.5	45.9	43.7	43.3	42.9	44.6	33.97
	9.3	55.2 60.0	54.8 59.3	49°2 59°3	48 <b>·1</b> 57·5	$51.\overline{5}$	51.3	53°4 —	51.8	52.4 —	53.2	54·3	54.69 59.62
-   -	-						53.4	51.5	51.5 49.2	$\begin{bmatrix} 51.7 \\ 48.7 \end{bmatrix}$	51.6 47.3	$\frac{-}{54 \cdot 0}$	56.80
	$\begin{bmatrix} 1.2 \\ 9.9 \end{bmatrix}$	59.7 59.6	59°1 57°9	56.2 55.9	55°8 56°9	53.5 46.8	52.6 45.2	49.7 43.1	41.3	40.0	39.6	38.3	54.23
54	4.9	48.1	47.1	45'1	43.9	41.7	40.0	$\frac{39.6}{45.2}$	40°2 43°2	40.0 42.8	36.8 44.6	37.5 45.8	46.64 52.04
	$\begin{array}{c c} 9.2 \\ 6.9 \end{array}$	55°3 63°1	51.9 60.3	49.8 64.1	$\begin{array}{c} 48.6 \\ 63.7 \end{array}$	46°9 62°7	46'3 61'1	60.9	57.2	58.2	57.5	56.6	62.75
61	1.2	58.2	56.7	56.3	56.0	56.0	50.9	50.2	 48*8	49.4	49.8	$\frac{-}{49.5}$	57.07
44	4.8	44.8	45.0	45.9	46.1	46.8	47.2	47.0	47.0	47.3	47.6	47.3	46.04
58	8.98	56.33	54.80	53.16	52.14	51.09	49*93	49.38	48.49	47.79	47.19	47.23	54.91
57	7.3	56.3	54.2	54.0	54.3	53.4	52.4	51.0	50.4	49.7	51.3	52.0	54.24
	$\begin{array}{c c} 0.4 \\ 6.5 \end{array}$	57.0 56.2	54.7 55.0	53.0 54.4	52.4 $52.4$	48.9 $52.4$	$\frac{48\cdot2}{53\cdot2}$	46.7 53.4	45°3 53°8	45 2 54 0	44.1 53.8	44.9 53.7	54°29 55°82
53	3.6	52.8	50.6	47.3	46.1	45.0	43.0	42.1	39.8	37.9	37.2	36.7	51.12
1	1.1	60.3	55.6	23.0	48.4	45.6	51.0	50.4	45.9	44.6	42.6	$\frac{-}{43.6}$	52.83
60	0.4	58.0	56.3	56.0	55.4	55.4	54.4	54.4	53.2	53.2	53.1	53.6 53.5	59:96 57:19
	$\begin{bmatrix} 7.2 \\ 2.7 \end{bmatrix}$	$\begin{array}{c c} 57.1 \\ 72.9 \end{array}$	56.7 69.5	57.7 65.0	$\begin{bmatrix} 57.7 \\ 65.3 \end{bmatrix}$	56.5 67.3	55°4 65°5	55.6 63.3	56°2 62°4	54.0 62.4	53.4 61.0	99.8	66.84
61	1.9	61.7	60.3	60.2	59.3	58.6	59.6 50.8	61.1	60.3 50.6	60°3 49°0	57.7 47.9	57°1 46°9	61.73 56.41
	5.0 2.4	51.4 61.7	51°2 56°5	51.0 55.8	$\begin{bmatrix} 50.7 \\ 55.2 \end{bmatrix}$	50°9 54°4		51.0	-			$\frac{10^{-9}}{51\cdot 4}$	57.96
-	-		]	43.5	$\frac{-}{42.3}$	41.7	52·3 41·3	52.0 41.0	51'4 41'3	51.6 41.3	51.6 40.1	51.4 §	46.13
	$\begin{array}{c c} 8.0 \\ 7.3 \end{array}$	47° I 55° 2	44.6 52.1	43 2 49 5	42.5	46.8	47.7	47:3	46.0	45.5	44.8	45.2	49.11
5	5.6	55.8	55.8	47.1	45.7 47.6	45°7 47°4	44.9 45.6	45°1 44°4	44.2 43.6	43.9 43.0	41.7	42.6 48.1	50.69 55.28
	6.2 7.8	61°1 57°0	54.8 57.5	50.6 $58.3$	58.1	58.5	58.3	56.7	56.7	56.9	56.7	56.7	59.20
	6.2	57.9	55.8	53.1	51.6	51.0	53.4	52.0	52 <b>.</b> 8	52.4	52.4	$\frac{-}{51.7}$	57.65
	6.0	60.1	57:5	56.9	56.3	56.3	54.9	53.2	51.6	49.7	49.5	52.0	59.44
	$\begin{bmatrix} 3.2 \\ 7.5 \end{bmatrix}$	60°4 64°4	57.7 61.1	56.6 59.1	56.7 $58.3$	55'4 58'1	55.7 55.8	55°7 55°8	55°4 53°2	55.0 52.8	50'4 51'4	$\begin{array}{c} 52.0 \\ 51.4 \end{array}$	58.91 62.39
73	3.9	69.7	68.3	60.2	58.2	57.5	55.8	54.4	53.4	53.8	53.0	55.2	64.86
	8.3 1.6	63.7 68.7	62°1 67°7	$\begin{array}{c} 61.5 \\ 69.3 \end{array}$	60°7 65°9	60°1 64°4	61.3	61.9	61.2	61.2	60.9	59°3	65.62
-	-						68.4	67.6	65.8	64.1	63.7	61.9	70.19
	9°2 0°5	66.9 67.4	66°1 63°7	61.8	64.5 60.3	63.6 59.5	62.0 57.9	$\frac{61.3}{56.5}$	60°3 56°7	59°5 55°4	55.7 54.8	57°5 55°6	65`80 63`40
	8.1	64.4	61.1	57.7	56.2	56.7	55.4	52.8	50.8	50.1	50.1	52.0	62.76
6	2.74	60.50	57:95	56.07	54.91	54.27	54.01	53.33	52.41	51.80	50.96	51.36	58.47

					ST	TANDARD	THERMO	METER.					
Hours o Götti Tir	of Mean }	0	1	2	3	4	5	6	7	8	9	10	11
Hours o Tord Tir		18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \end{pmatrix}$	56°7 57°1 61°5	61.1 63.8 67.9	$\begin{array}{c c} 6\mathring{5}^{\circ} 1 & \\ 70^{\circ} 1 & \\ 73^{\circ} 5 & \end{array}$	69°9 76°2 76°5	73°1 75°3 78°5	72.7 74.5 80.4	74.5 76.5 81.7	74.8 78.7 81.8	76°1 78°2 81°6	75°4 78°9 81°2	75.7 79.3 81.5	74°9 79°0 79°7
	4 5 6 7 8 9	62.0 67.1 65.2 67.7 68.0 69.3	67.6 67.7 67.8 71.1 72.5 69.9	72·2 67·2 69·1 76·3 75·9 71·8	77.9 69.7 76.1 79.0 78.0 74.1	80°1 71°2 76°9 79°7 78°7 74°9	79.6 73.5 78.2 80.7 81.5 76.3	80.1 75.9 80.3 80.3 81.2 76.7	81:3 78:7 80:3 80:3 81:2 79:5	81.8 77.1 81.3 77.6 79.6 81.7	80.9 76.6 81.1 78.0 79.6 80.6	78.2 78.7 81.3 77.6 77.2 80.5	70·5 75·2 79·9 77·9 77·0 77·5
JULY.	11 12 13 14 15 16 17	68.9 72.5 57.5 54.6 65.2 70.0	74.7 75.5 61.5 58.7 70.6 71.4	76°3 76°8 65°3 63°7 74°0 74°3	76.8 79.7 69.3 68.8 77.1 78.2	78.0 81.5 70.7 71.4 79.4 82.7	79.7 83.3 73.3 73.3 81.1 83.5	79.5 83.6 73.9 75.4 82.5 84.7	79.8 83.1 74.0 76.5 83.3 83.7	81.7 79.7 72.7 76.7 81.7 84.3	82.1 77.8 71.5 76.7 82.1 75.3	83.2 77.1 70.7 75.4 80.0 76.8	79.4 74.3 70.2 73.0 77.8 78.2
	18 19 20 21 22 23 24	71.6 71.2 69.1 69.7 53.6 58.7	77.4 75.7 72.0 72.0 59.3 62.8	80.0 79.1 71.7 71.7 64.9 67.1	80°1 77°8 73°2 72°9 69°1 69°3	82.9 79.7 76.5 74.7 69.9 67.9	85°1 77°4 79°7 75°7 70°7 67°5	87.0 79.5 79.7 77.8 71.3 67.1	85.1 77.6 79.4 78.2 71.4 66.1	82.1 77.8 81.5 79.3 70.3 68.7	85.1 80.7 79.1 78.9 72.7 69.9	86.1 76.3 80.3 78.2 74.5 69.5	85.5 76.7 78.2 78.2 73.3 68.2
f Augu	25 26 27 28 29 30 31 ust 1	57.8 51.2 50.8 57.7 55.9 51.4	56°3 55°0 56°9 62°1 59°5 60°1	55°8 58°1 62°3 64°8 60°3 64°6	56.0 61.5 64.6 66.8 60.1 66.1	55°2 61°7 65°3 68°6 66°3 68°5	56.2 63.1 65.3 70.4 63.9 68.1	56.3 64.1 64.1 70.7 65.2 71.5	59°1 63°5 65°7 70°0 62°1 67°0	62:1 63:5 65:2 68:9 63:5 68:1	61.7 63.3 65.2 69.0 65.3 68.7	62.7 65.0 65.5 69.1 66.1 70.5	63·2 64·8 65·0 68·1 66·5 67·1
Hourly	y Means	62:30	66.33	69.33	72.03	74.12	74.62	75.60	75.64	74.92	75.46	75.44	74.05
	$\left( \begin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{array} \right)$	52°2 55°4 59°4 59°9 63°1 59°5	59°1 61°9 65°6 65°4 65°7 60°1	65.2 65.9 70.1 69.2 71.5 64.6	66.0 69.8 70.5 70.9 74.3 67.1	69°5 70°3 70°9 71°5 77°8 68°9	71.0 70.5 73.0 72.7 77.6 72.7	71.5 70.7 73.9 72.9 77.7 73.1	72.5 71.1 74.2 73.1 76.5 73.1	70.8 70.6 75.7 74.7 78.5 71.2	72.5 72.1 75.9 74.5 76.7 71.3	72·3 73·2 76·9 73·1 75·1 70·2	69.5 74.1 76.3 71.5 70.3 68.9
ľ.	8 9 10 11 12 13 14	63°1 64°7 66°1 57°7 63°5 66°3	63°5 66°3 67°4 59°3 66°9 69°1	64.1 67.9 69.7 63.9 78.1 71.6	66.2 71.6 68.2 69.1 78.1 74.3	66.9 74.9 68.9 73.5 74.9 77.4	68.9 76.2 70.1 74.8 74.5 77.2	71.1 76.4 72.1 75.3 75.5 77.8	73·2 76·5 73·3 74·8 75·3 79·6	73.4 77.8 71.1 75.5 77.2 75.7	74.6 76.0 67.3 75.1 74.3 78.9	73.7 75.1 69.1 72.3 74.2 76.4	73:3 74:3 69:9 73:9 73:5 77:0
AUGUST.	15 16 17 18 19 20 21 22	68.0 64.8 56.3 46.0 54.2 54.9	71.2 72.6 57.3 50.1 59.1 57.2	73.8 73.7 59.1 55.4 61.3 59.8	76.7 74.9 61.5 57.7 66.0 64.4	78.2 75.9 63.1 61.3 68.7 66.8	80°2 72°5 63°7 61°5 67°1 68°5	79.8 72.7 65.7 63.0 70.5 70.5	80°5 71°1 66°3 64°1 70°7 71°5	82·1 73·9 67·3 64·4 70·5 73·0	82.5 71.3 67.7 66.3 72.9 73.5	81'9 70'3 64'9 65'2 69'1 73'5	83°1 71°1 60°7 65°4 60°7 73°9
	22 23 24 25 26 27 28 29	53.5 52.8 53.8 53.4 56.2 47.5	59.0 57.3 57.1 58.3 56.8 54.0	63.5 60.5 65.5 63.1 58.9 62.0	65 · 2 64 · 4 68 · 7 67 · 2 60 · 3 63 · 8	63.5 67.0 70.3 68.7 61.7 66.1	64.4 69.3 69.7 71.7 63.6 67.8	66.1 70.5 70.5 71.2 64.9 68.1	66.5 70.0 69.9 73.9 66.0 68.3	67.5 70.4 70.7 74.0 65.3 69.0	68:3 70:4 71:1 74:7 63:9 68:1	68:1 70:6 69:5 74:8 64:6 68:3	67.8 70.6 68.4 70.9 65.5 68.7
	$\begin{bmatrix} 30 \\ 31 \end{bmatrix}$	58.7 50.6	64°5 54°1	65.8 56.2	69.6 57.5	$\begin{bmatrix} -71.5 \\ 58.7 \end{bmatrix}$	72.7 59.6	73.0 60.7	73·3 61·7	72.5 61.7	70.7 62.7	68.7 61.6	66.4 60.4
Hourly	y Means	57.75	61.20	65.41	67.85	69.20	70.44	71.35	71.81	72.10	72.05	71.26	70.23

						STANDA	RD THER	MOMETE	R.				
-	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
!-	6	7	8	9	10	11	12	13	14	15	16	17	Means.
-	74.7 76.5	69°5 70°9	63.7 66.7	60°.7 64°6	59.1 63.9	59°8 62°0	60°·1	$5\overset{\circ}{8}\overset{\circ}{.}6$ $58\overset{\circ}{.}3$	59.6 56.9	$\begin{bmatrix} 5\mathring{8} \cdot 1 \\ 56 \cdot 3 \end{bmatrix}$	55°9 55°1	54°0 55°2	65.99 68.04
	78.3	72.5	66.9	62.8	60.1	60.0	60.3	59.7	59.1	57.5	57.1	$\frac{-}{56\cdot 7}$	69.87
:	71.0 72.2	70°5 71°1	68:3 67:2	67.8 65.1	67°3 63°7	$\begin{array}{c} 68.9 \\ 63.5 \end{array}$	68.9 64.4	66.9 62.8	67.9 61.5	63.1	67:3 62:9	63.0 63.2 63.9	72.13 69.15 71.56
	77:8 77:7	73.7 75.5	68.9 71.7	66.5 69.6	65.4 70.5	65.7 69.9	66.5 69.9 70.1	$\begin{array}{c c} 69.3 \\ 69.3 \\ \hline 62.3 \end{array}$	$62.3 \\ 68.7 \\ 69.5$	61:8 66:4 68:7	63.0 65.8 68.7	66·1 68·7	73.64 74.17
i	76°3 76°1	74·1 73·3	71.2 73.3	71.9 72.2	70.5 72.2	70°3 71°3	67.3	66.7	65.5	65.5	65:3	$\frac{0}{65.0}$	72.77
	80.7 72.1	79.5 69.1	73·5 66·3	70°3 63°9	69°1 62°3	68.7 60.7	69.5 60.0	68.8 59.3	65.9 58.7	63.5 57.8	65°5 56°7	70°3 56°2	74°39 70°33
	69.1	64.1	60.3	57·5 68·3	56.6 68.3	55°3 66°5	53°1 66°1	52.5 60.7	51.8 61.3	51.2 60.3	52°3 59°5	51.8 59.1	62.76 67.63
	75°3 78°0	75°1 77°4	71.3 74.3	69°3 73°1	68.7 73.5	$68^{\circ}1$ $73^{\circ}1$	68.2	68.1	67.9	66.2	65.7	$\frac{67.1}{66.7}$	73.60 75.07
	84.3	79·4	75.2	72.9 70.3	71·5 70·6	70.9 70.0	70°2 70°3 70°0	68.7 68.1 69.3	69.1 68.3 68.5	67:5 68:7 69:5	66.9 68.3 68.4	68.0 68.5	77 [·] 25 73 [·] 73
	72°3 75°1 76°2	71.7 73.3 71.1	70.8 70.9 67.2	68.9 62.9	67.7 60.7	65.7 58.3	67:3 54:8	66.3 52.8	65.8 52.0	66.7 51.0	68.7 48.7	68.5 48.3	72.72 67.14
	73·3 67·5	68.3 68.3	63.3	59.5 65.5	57·7 66·1	57·3 66·3	55.9	55.8	55.4	54.4	53.6	$\frac{53.8}{59.2}$	63.72 - 66.29
	60.3	58.3	54.9	52.6	48.7	47.5	65.6 47.3	68.4 47.1	69.0 46.7	67.7 46.3	61.5 43.8	47.1	54.29
	64.4 62.5	60°4 60°9	54.7 57.7	51.8 54.0	51°2 53°2	48.9 52.2	48 · 1 52 · 2	48.5 52.6	46.9 52.6	46.5 51.3	45°3 49°5 55°3	45.5 48.7 54.9	56.13 58.47 64.25
	68°1 65°5	67.0 62.5	67.0	63.7 59.4	62.9 57.9	61.9 57.1	60.7 55.8	59°5 53°1	58.9 52.8	55.8 50.1	48.7	48.3	59.42
	63.7	<u></u> 60.0	61.3	58.1	56.2	54°5 —	56.0	55.4	54.4	52.0	51.5	50.1}	61.03
_	72.59	69.81	66.69	64.26	63.24	62.80	62.14	61.18	60.63	59*69	58.91	58.93	67.98
	72·3 73·7	67°3	61'9 62'4	60.7 58.1	60°3 55°1	58°1 54°4	57°1 55°1	53 <b>·</b> 2 54·2	52.6 52.8	52.8 52.4	49 <b>·</b> 7 51·4	48.5 52.0	62.78 63.20
-	75·1 69·1	71·7 67·1	64.0 64.8	59.9 63.1	58.6 64.1	57:9 63:3	58·1 63·3	56.5 63.6	56.2 62.7	56.5 62.4	55 <b>·</b> 9	<b>60.</b> 9	66°24 67°32
	63.9 67.5	64.7 64.6	67.0 63.3	$\begin{array}{c} 66.7 \\ 62.3 \end{array}$	67.0 62.3	66.9 61.7	66.8	65.8	64.4	61.1	$\frac{58.7}{61.7}$	$\frac{57.5}{62.5}$	68°97 65°65
	72.3	70.0	68.3	68.5	68.3	66.7	62:3 65:1	62:3 64:4	62.3 63.3 65.3	62.1 62.5 65.0	$62.7 \\ 65.5$	$63.7 \\ 66.1$	67.83 70.24
Ì	70.5 70.9	69.7 66.7	69°1 64°6	68.5 62.1	67.9 61.1 66.8	67.7 60.6 66.5	67:3 59:7 66:3	65.4 59.3 66.1	59.0 65.3	59.5 62.5	57.8 62.7	57·3 62·3	65.49 68.31
	72·3 72·7 75·0	68.7 70.5 73.7	67.9 69.3 70.3	66.9 69.1 68.7	67·3 67·5	66.9 67.0	66.1	68.1	67.3	67.0	66.3	$\frac{66.5}{64.0}$	70°96 71°33
	80.8	75.7	70.5	69.3	67.1	66.3	66.1 65.2	65.5 64.8	65°2 64°7	64.0 64.4	63.7 64.6	63.0	73.16
	59.3 59.3	67.9 56.3	66°3 54°6	65.7 $52.2$	62.6 51.6	61.7 49.6	59.6 48.6	56.8 48.3	55°1 48°3	56.4 48.3	58.5 48.1	56.5 45.0	66.70 56.83
	64.8	60°3 58°7	56.5 58.7	55.9	55.7 57.1	55.6 55.2	56.0 55.4	54.2 54.0	52.4 54.0	50.4	51.4 53.0	51.8	57.73 60.90
	71.5	66.5	56.9 26.9	58°3 56°2	57.5 	55.4 — 53.1	54.1 52.0	53.0 52.1	51.8 52.8	51.4 52.3	50.6 49.6	$\frac{-}{50.8}$	62°00 59°53
	69·1 66·4	61.7 62.2	58.5 58.5	57.6 57.5	55·1 56·9	55·1 56·3	55·4 55·9	54.6 55.0	54.4 54.1	54°2 53°5	52.8 53.6	52.6 51.9	61.47 61.96
	69°3	66°1 59°0	65°2 58°5	65°1 56°5	66.5 54.6	66.3 53.1	64.0 53.2	62.9 52.4	63°3 49°5	61.7 47.3	60°3 48°0	56.9 48.8	66 <b>°2</b> 3 58 <b>°</b> 09
	65.2	<u></u>	58.7	56.2	56.4	55.0	59.0	57.5 56.9	56.0 55.4	55.5 49.9	55.6 49.5	$\begin{bmatrix} -55.4 \\ 48.5 \end{bmatrix}$	60°95 62°78
	63.8 58.9	62.0 54.7	59.4 51.3	60.4	59.4 48.5	58.1 48.3	56.6 47.7	56.2 47.5	45.5	48.1	49.1	50.4	54.36
	68.68	65.23	62.59	61.28	60.37	59.49	59.08	58.22	57.45	56.72	56.25	55°85	64.27

Iours o	f Mean ]						THERMO	THE TEN.	,				
Göttii Tin	ngen ne.	0	1	2	3	4	5	6	7	8	9	10	11
Iours o Toro Tin	f Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	1 2 3 4 5	51.4 49.3 57.4 56.0	52.8 55.2 62.4 56.1	56.4 60.9 64.1 56.1	59.2 64.8 64.2 56.3	62:3 67:5 70:4 57:1	64°1 68°7 73°1 57°7	63.9 69.4 73.7 57.3	65.9 70.1 70.9 57.8	66.4 72.1 74.8 57.7	66°3 71°9 73°5 58°3	66.0 72.1 70.6 58.5	65°4 69°5 65°5 58°9
	6 7 8 9 10 11	49'2 52'6 65'0 50'1 45'3 46'8	51.8 59.6 66.1 50.1 49.7 52.0	56.2 63.7 68.4 51.1 55.8 56.1	62'3 64'9 69'6 52'7 60'3 61'5	63:3 65:2 73:0 55:8 61:7 61:5	63°5 65°3 74°6 56°8 62°2 63°1	63·3 64·6 74·8 58·2 63·5 62·2	65°3 65°1 73°5 60°5 63°5 62°1	65.9 63.0 73.8 60.3 64.0 61.9	67.7 63.3 72.9 60.1 63.7 61.6	65.8 63.1 72.5 60.2 63.3 60.9	65°1 62°7 70°8 59°0 63°0 60°3
SEPTEMBER.	12 13 14 15 16 17 18 19	54.6 45.0 38.1 38.1 50.4 57.3	53.9 45.7 42.9 43.3 51.4 58.1	53.2 46.7 46.3 50.8 56.5 59.4	54.8 47.4 50.1 53.4 60.0 59.8	54.8 48.7 52.0 57.7 61.5 61.1	54.8 48.4 54.2 58.3 62.5 60.7	55.0 49.4 55.6 58.7 62.1 61.3	55.5 50.0 57.1 58.3 62.0 61.5	53.8 53.0 57.0 59.0 61.1 60.5	52.2 53.3 57.3 59.5 61.3 61.0	50.9 52.9 57.9 59.7 61.0 61.0	49°2 51°8 57°3 58°3 60°0 60°1
	20 21 22 23 24 25 26	54.8 51.4 44.8 49.9 54.6 49.0	55.4 53.7 48.3 52.8 54.0 48.9	56.3 56.3 52.5 58.7 54.0 50.0	56.5 58.3 56.2 61.5 54.4 53.1	57:1 59:9 59:2 62:9 54:4 55:1	56.8 60.1 59.5 65.0 54.6 56.7	57.0 62.5 59.4 65.5 56.0 59.1	57.0 61.7 58.7 66.1 55.8 58.1	56.7 62.7 59.5 67.3 55.8 57.2	56.5 61.7 59.3 67.1 55.6 56.2	56.6 59.7 60.1 66.7 55.7 55.5	57: 58: 58: 66: 55:
	27 28 29 30	58.0 46.7 43.6 39.6	59·2 49·3 44·4 41·9	60°1 53°0 48°3 45°0	60.6 54.9 51.4 48.9	62:3 57:5 54:2 52:8	64°1 59°5 50°4 53°2	66°3 60°3 54°2 54°7	67.5 52.2 55.4 54.8	68°3 55°0 48°7 52°2	68.7 54.4 46.6 52.0	69 ¹ 52 ² 48 ² 53 ⁰	67 : 51 : 48 : 48 : 51 : 6
lourly	Means	49.96	52.27	55*23	57.58	59.58	60.30	61.08	61.02	61.07	60.85	60.21	59:8
	$\begin{pmatrix} 1 \\ 2 \end{pmatrix}$	44.4 39.3	46°3 41°9	48°9 46°9	50°0 51°3	50°9 53°5	52.7 54.8	52.8 54.6	53·7 55·0	52.8 56.2	54°0 56°3	54.0 55.0	52.2 52.8
	3 4 5 6 7 8 9	40.7 57.3 57.3 55.5 55.6 40.8	44.0 58.3 57.2 54.8 55.5 44.2	51°5 58°8 57°0 55°0 55°7 47°1	56.7 60.7 56.9 55.0 56.2 51.9	58°1 59°5 56°7 56°2 57°5 54°2	59.5 60.1 56.9 55.6 58.5 53.8	60°5 63°7 57°5 55°0 59°0 53°6	59°4 63°2 57°3 55°5 56°8 54°0	59.3 63.9 58.0 55.6 56.7 56.5	58.1 65.0 58.7 55.8 56.3 56.5	58.0 62.3 58.5 56.0 56.8 56.5	56 · 9 60 · 5 58 · 7 56 · 0 57 · 9 55 · 6
OCTOBER.	11 12 13 14 15 16 17	39'4 41'4 38'6 35'0 29'7 42'8	39.6 42.4 39.1 35.4 30.6 44.3	41.7 43.8 41.3 35.6 33.7 46.1	44.4 45.0 41.7 39.1 35.3 47.9	46.5 46.7 43.0 41.0 37.6 49.9	47.8 47.8 43.9 40.3 41.5 51.2	49.5 45.3 46.5 41.0 41.9 52.7	49.5 45.3 47.3 40.0 41.6 54.5	50.6 44.0 47.1 40.8 43.2 55.4	51.0 44.2 46.0 41.0 42.6 55.7	50.7 43.9 44.1 40.2 41.7 54.5	48°1 44°0 43°4 38°9 39°8 53°2
00	18 19 20 21 22 -23 24	39°1 41°9 29°9 34°5 38°1 35°3	42°1 41°1 31°9 35°9 38°2 35°1	45°3 44°3 37°8 38°1 38°1 37°2	49°8 48°5 44°4 41°5 37°9 41°6	54.0 49.5 47.3 44.0 38.7 46.0	56.3 51.6 49.5 44.9 39.2 48.0	60°3 53°6 49°9 44°7 38°9 49°3	61.7 52.4 51.4 44.1 39.4 48.9	61.5 54.5 54.0 44.0 40.0 49.1	61.0 53.5 54.4 43.9 40.4 49.1	60.5 52.8 52.8 44.0 41.0 48.9	58.5 50.1 48.6 43.4 40.6 46.1
	25 26 27 28 29 30 31	46'3 29'1 21'9 25'3 28'6 34'1	46°3 30°2 21°7 27°0 32°7 33°9	46.6 31.8 23.8 32.4 34.5 36.4	48'3 31'6 29'0 35'3 41'0 43'7	47.9 31.9 30.8 39.4 45.2 47.3	48.7 31.3 32.0 41.0 47.3 50.5	48.4 32.4 33.7 41.0 48.0 50.4	48 '2 31 '0 35 '8 41 '0 49 '0 51 '3	45.2 30.9 36.2 41.4 49.2 50.2	42.6 30.7 35.7 40.8 48.9 50.1	39.6 29.7 34.7 40.4 48.1 49.3	37:8 27:8 33:6 44:6 46:3
lourly	Means	39:30	40.37	42.67	45.57	47:43	48.64	49:39	49.51				47.4

					STANDA	RD THER	MOMETER	De.				
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
63.9	58.4	56°3	<b>54.</b> 9	54°4	53.9	53°1	52°0	5η1	5η4	5η1	49.7	57.93
68.1 62.3	65°2 60°0	65°2 59°1	64°1 58°9	$61.7 \\ 58.2$	59°5 56°3	58°3 55°9	56°7 55°8	56°2 56°7	54°4 56°7	55 <b>°</b> 6 56 <b>°</b> 3	55°4 56°2	63.00 63.04
59.3	59.7	60.3	60.6	60.6	59.2						48.1	55.77
-	-					49.8	48.7	48.3	48.1	47.7		
63.6	60°0 62°2	57.7 61.3	57 <b>·</b> 2 63 <b>·</b> 1	56.8 64.1	55.0 55.0	55°0 63°3	53 <b>·</b> 6	52.6 63.5	51 <b>.</b> 9	51.6 63.9	51.8 64.1	$\begin{array}{c} 58.59 \\ 62.93 \end{array}$
68.0	66.2	66.1	65.7	58.3	55.2	55.2	54.0	54.0	53.6	51.8	49.5	64.70
58.9 60.6	57°2 53°7	56.5 51.4	53.2	50.1	48.0	45.7	44.4 48.4	44°5 47°7	43°9 46°7	43.6 46.3	43°3 46°5	52.68 54.79
59.0	52.6	51.0	50°6 50°8	49.5 50.4	48.9 50.1	48.6	40 4	4/ /	40 7			
						56.3	55.6	54.6	54.4	54.2	$\frac{-}{55.4}$ }	56.43
48.1 51.2	47°1 46°1	46°1 44°6	$\begin{array}{c} 45.5 \\ 43.2 \end{array}$	$\begin{array}{c} 45.2 \\ 43.6 \end{array}$	44.6 42.4	44.6 41.9	44.6 40.1	44.4 39.5	44'4 38'1	44°1 39°1	44.6 38.6	49°42 45°86
55.0	49.5	48.3	49.2	48.3	47.1	45.8	43.2	40.9	39.7	38.9	38.2	48.78
55.3	50.8	49.0	47.8	48.5	49.5	49.5	49.3	49.3	48.7	49.3	50.1	52.18
59.3 59.3	58.7 60.1	58°5 59°8	58°3 59°1	$\begin{array}{c} 55.8 \\ 58.9 \end{array}$	55°4 59°3	54.6	58.3	58.3	58 <b>.</b> 1	57·5	57.5	58.32
	_		_			55.4	55.4	55.2	54.8	54.8	54.8}	58.70
55°6 55°6	53.0	53.6	53.2	52.8	52.0	52.0	53.4	53.0 43.6	52°3 44°7	54°1 44°9	$\begin{array}{c} 52.7 \\ 44.4 \end{array}$	54°81 53°24
53.8	51.6 51.9	49°9 50°1	49°3 49°2	48.4 50.6	48°3 48°9	46.7 47.3	44.6 46.1	45 6	44 7	44 9	45.7	53.24 $52.36$
62.5	61.1	59.5	58.1	56.9	56.3	58.3	57.1	56.2	56.0	55.2	54.6	60.07
54.8 54.8	54.4 54.6	54.6 54.1	55.0 $53.6$	54'1 53'4	53°4 53°4	531	52.8	52.1	50.6	49.5	48.8	53.89
	J4 0	9 <del>4</del> 1			99 4	56.2	57.3	58.1	58.3	58.3	$\frac{-}{57\cdot 9}$	55.50
64.6	62.3	62.3	60.9	58.7	56.3	52.8	49.7	48.6	46.7	46.9	46.3	59.48
49°8 47°7	48.7 47.1	46.7 46.2	44 <b>·</b> 9 44 <b>·</b> 8	44.8 44.4	43°0 45°3	42°1 45°3	41.7 43.4	41.5 40.4	43°0 41°5	43°4 38°5	43.9 39.6	49.16 46.59
51.0	45.9	45.2	45.2	46.1	47.7	49'1	20.0	49.9	48.7	48.1	45.9	48.85
57.77	55.32	54.36	53.71	52.87	52.01	51.47	50.77	50.25	49.84	49.62	49.38	55.26
40:1	40:1	40.4	90.0	10:1	4010	20:0	0.20	2015	40.0	20:0	39.6	45.96
48.1 48.3	43.4 45.7	42.4 45.3	39.8 46.6	40 <b>.4</b> 46.7	40°8 44°3	39.8	37 <b>·</b> 9	38 <b>`</b> 5	40 0	39.6		
	_					45.5	45.7	44.2	43.8	42.9	$\frac{-}{42.6}$	48.30
56.2 59.5	56.2 59.0	55°8 58°5	55.8	54°0 57°5	53°9 57°1	54.5 57.3	54°4 57°2	53°3 57°3	$54^{\circ}2$ $57^{\circ}2$	$\frac{54\cdot2}{57\cdot2}$	56°0 57°1	55 <b>.05</b> 59.44
58.2	58.3	57.3	56.9	57.1	56.6	56.6	56.1	55.8	55.6	55.4	55.5	57.10
56.2	56.5	56.7	55.8	55.8	55.8	56.1	56.2	55.8	55°8	55°8	55.8	55.76
57°5 53°1	57°3 52°9	55.6 54.4	52.8 $54.4$	51.2 53.6	50°1 53°0	48.1	47.3	46°3	44.5	42.5	42.1	53.25
		_				42.3	41.5	40.6	41.0	41.0	$\frac{-}{40\cdot 2}$	49.70
46.7 44.0	43.4 43.6	43.0	$\frac{41.2}{42.8}$	40°4 42°4	37 <b>·</b> 9 43 <b>·</b> 0	37.7 42.8	37.7 $41.2$	38.4 40.3	38.7 $39.6$	40°0 39°5	$\frac{41.5}{38.6}$	45.64 43.53
40.3	39.5	$\frac{43\cdot2}{37\cdot2}$	35.3	34.1	32.9	32.5	$\frac{41}{33}.7$	34'1	$\frac{39.0}{34.7}$	35.4	35.2	39.45
36.1	33.1	31.6	30.3	29.0	28.8	27.5	27.4	27.7	28.6	29.0	29.0	34.43
39·3 53·8	41.5 $53.2$	40°9 52°6	$\frac{40.3}{52.2}$	41.8 52.0	42.8 51.8	42 <b>.</b> 8	42.4	44°4 —	44.3	44.3	43.4	40.31
		J2 O	- J2 Z	- JZ 0		40.6	39.1	39.1	38.2	37.6	$\frac{-}{37\cdot 4}$	48.16
59.1	57.2	56.3	57.9	54.0	52.2	51.2	50.1	48.9	47.1	43'4	42.2	52.91
46°1 45°3	44.8 43.4	43.8 43.0	40.8 40.6	$\frac{39.9}{38.9}$	34.3 36.6	33.5 32.9	32'1 31'4	31.1	$\frac{30.9}{31.2}$	31.0	$\frac{33.8}{30.8}$	43.00 41.32
43.2	43.2	42.6	42.5	42.5	39.8	39.0	38.7	38.3	38.3	38.1	38.3	41.15
40°3 45°3	39.9	39.8	39.5	38.9	39.1	39.3	37.5	35.2	34.3	34.8	36.2	38.57
	40.2	40.2	38.6	38.3	38.9	46.7	46.7	46.7	46.5	46.5	$\frac{-}{46\cdot 3}$	43.98
35.3	34.2	34.2	32.2	32.2	31.8	31.2	31.0	30.8	30.3	28.8	28.2	38.59
26.5 31.7	25.7 $32.0$	24.6 31.6	$\frac{23.8}{31.5}$	$\frac{22.7}{31.8}$	21.7 28.8	$\frac{21\cdot1}{28\cdot2}$	$20.2 \\ 27.8$	20.6 27.6	20.6 28.2	20 <b>.</b> 9 28 <b>.</b> 0	20.8 27.1	$26.57 \\ 30.96$
37.9	32 0 37 0	35.7	31.1	29 <b>.</b> 9	28 8 29 5	28.2	30.0	28.8	28.8	28.3	29.0	34.13
43.4	41.5	41.1	37.4	38.5	35.0	34.6	33.9	33.1	32.9	33.1	33.3	39.79
43.8	45.2	41.4	38.7 —	36.6	35 <b>.</b> 9	48.9	48.8	47.7	48'1	47.7	47.8}	44.75
45.98	44.93	44.50	45.27	42.33	41.25	40.77	40.23	39.82	39.75	39.46	39.56	44.27

	<u></u>				SI	ANDARD	THERMO	METER.					
Hours of Göttii Tim	ngen	О	1	2	3	4	5	6	7	8	9	10	11
Hours of Toro	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	1 2 3 4 5 6	47°7 49°7 46°0 41°9 35°7 31°8	48°2 49°7 46°2 41°5 35°6 29°7	49°4 50°8 53°4 45°1 38°6 32°4	50°6 52°3 54°0 48°9 40°5 35°5	52.6 54.0 53.2 49.3 42.9 36.7	53.6 55.8 53.0 51.5 43.6 37.7	55·2 56·3 54·4 51·4 44·6 37·5	55.2 58.2 54.3 51.1 46.2 37.2	54.4 56.1 54.8 51.0 44.6 37.3	53°2 55°8 54°0 48°8 45°0 38°3	51°9 54°8 53°8 49°6 43°1 38°7	49.7 52.0 53.0 46.1 41.2 36.1
SR.	7 8 9 10 11 12 13	45.2 50.8 37.3 35.7 31.8 34.4	45.5 51.0 37.5 35.9 30.8 34.0	46.0 53.2 38.1 36.3 32.3 34.7	46.6 53.6 38.5 36.7 36.5 37.4	46.0 55.6 38.3 37.0 38.3 38.6	46.3 54.1 39.6 37.2 39.3 39.6	46.9 52.6 39.9 37.7 39.2 40.4	48.3 51.2 40.1 37.9 39.8 41.0	48.0 51.8 39.8 37.9 39.5 40.8	48.3 52.1 39.6 37.7 40.0 40.0	48.5 51.8 39.0 37.5 38.9 39.2	48.3 47.4 38.3 36.7 37.9 39.1
NOVEMBER	14 15 16 17 18 19 20	38.2 28.4 46.0 42.4 33.8 18.8	38.7 27.4 46.1 41.9 33.6 18.6	38'9 30'6 45'9 41'9 31'4 20'0	40°0 36°3 46°6 42°2 30°8 23°6	41 · 3 39 · 5 48 · 7 42 · 6 29 · 9 26 · 3	41.5 41.0 50.6 42.8 28.8 27.8	40.0 43.3 52.4 42.6 28.4 28.8	40.6 44.4 50.6 42.6 28.4 29.5	41.2 46.5 49.5 43.0 29.6 30.2	41'3 46'9 52'0 43'7 28'6 30'0	40.7 46.3 51.7 45.2 28.2 29.2	40°0 45°7 49°3 45°5 27°6 27°9
	21 22 23 24 25 26 27	35°4 42°0 47°5 40°4 26°2 24°6	35.9 42.3 45.4 40.4 25.5 25.4	36.1 42.6 45.7 39.3 25.7 26.5	38.4 43.9 45.9 41.9 25.7 27.5	40.8 45.5 47.9 42.4 25.7 26.7	43.7 47.6 49.5 42.4 25.9 27.8	45°3 50°0 50°0 41°4 25°9 27°8	46.5 51.2 50.0 40.3 26.3 30.8	45.8 50.8 49.8 39.3 26.3 31.6	45.2 51.3 48.1 39.1 26.5 31.2	43.3 51.6 47.5 38.9 25.9 29.9	41.5 52.4 47.1 37.7 24.4 30.1
	28 29 30	9.6 	9.3 18.2	9.8 21.1	10.1 22.6	$\frac{-}{11.2}$ $23.7$	13.4 24.6	13.4 25.1	$\begin{array}{c} -13.7 \\ 25.7 \end{array}$	14.3 26.5	15.4 26.8	15.4 25.7	$\begin{bmatrix} 13.4 \\ 24.4 \end{bmatrix}$
Hourly	Means	36.12	35.93	37:15	38.72	39.80	40.72	41.17	41.28	41.55	41.20	41.01	39.72
	$\begin{pmatrix} 1\\2\\3\\4 \end{pmatrix}$	31.8 35.0 33.7 25.9	33°3 34°5 33°6 25°7	36°1 34°4 33°5 25°7	37·2 35·9 33·6 27·5	37.9 36.9 33.7 27.8	38.9 37.7 34.2 29.7	40.6 38.7 34.1 30.0	40°2 38°7 33°8 30°0	40.6 38.6 32.3 30.3	42.2 38.3 32.0 31.1	38.8 37.2 31.3 31.0	38°1 35°0 30°6 30°9
	5 6 7 8 9 10	26.9 32.7 36.3 37.6 47.1 33.4	26.5 32.7 36.1 37.1 45.7 33.9	27.6 31.6 37.4 36.5 45.8 34.7	29.5 36.1 39.6 36.1 45.7 35.1	31 · 2 37 · 7 42 · 1 36 · 5 47 · 2 36 · 1	30°2 38°4 44°1 37°5 47°1 36°5	31.4 39.1 45.3 38.2 49.5 36.1	32.0 39.5 45.8 38.5 49.9 37.1	33.7 40.0 44.5 39.7 49.5 37.4	32.7 39.8 44.7 41.6 45.9 37.6	32.7 38.1 44.6 42.3 44.7 36.2	29'9 35'2 43'9 42'9 44'0 33'7
DECEMBER.	12 13 14 15 16 17 18	37.0 32.0 34.1 13.2 16.4 13.2	36.9 32.0 32.4 13.2 17.5 13.7	36°1 32°2 29°9 13°8 18°2 14°6	36.1 32.7 30.1 13.8 19.2 18.4	36°1 33°1 31°0 15°0 21°2 22°5	36°1 33°2 31°6 15°8 21°5 24°8	36.7 33.5 32.3 17.2 24.0 27.0	36.3 33.3 32.8 18.1 25.9 29.9	34.6 33.1 32.7 19.4 27.1 31.3	33.5 33.0 32.7 19.8 27.5 31.4	33.7 32.9 31.8 20.0 27.6 32.4	33.3 32.7 29.7 21.2 26.1 33.1
I	19 20 21 22 23 24 25 a	13.7 10.4 21.1 17.7 21.3	13.7 9.9 20.8 17.7 20.6	13.2 9.5 20.6 19.9 20.4	12.1 10.3 21.3 19.4 22.3	12.8 13.0 22.3 20.2 22.0	13.4 16.1 23.4 21.9 21.3	14·1 17·2 24·0 23·6 21·7	15.0 18.2 23.9 24.0 21.6	15°1 18°7 24°6 24°0 22°1	15.7 20.2 24.9 24.4 22.1	14.1 21.3 25.0 24.6 21.5	11.0 21.5 24.4 24.4 20.9
	25 ° 26 27 28 29 30 31	13.0 30.3 37.2 41.7 42.4	12.0 30.9 38.0 40.6 41.7	10.7 31.4 38.3 41.0 41.9	12.1 33.0 39.5 43.0 42.4	15.7 34.1 41.7 43.3 43.9	17.3 34.4 42.4 44.3 45.5	18.8 34.4 43.4 45.2 45.1	18·2 34·5 42·4 46·2 44·9	19°1 34°1 42°2 45°5 44°9	19.8 34.7 42.1 44.2 44.2	19'4 34'7 42'4 44'2 44'0	19.8 34.7 41.9 43.2 43.6
Hourly	y Means	28.27	28.10	28:27	29:31	30.28	31.43	32.32	32.72	32.89	32.93	32.26	31.76

Christmas Day.

						STANDA	RD THER	MOMETE	₹.				
	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
i	6	7	8	9	10	11	12	13	14	15	16	17	Means.
	46.8 50.6 53.8 43.0 38.5	48°3 49°4 52°5 41°5 37°1	49°·3 50°·4 52°·5 42°·4 36°·1 29°·3	50°1 52°6 52°8 38°5 35°3 29°7	49°3 51°6 52°6 41°1 36°1 29°7	49°5 50°2 50°0 40°9 36°3 29°5	49°7 49°9 49°1 40°0 35°3	50°9 49°7 49°3 37°5 34°5	49°5 49°7 46°1 35°7 33°8	49°4 49°3 44°8 34°9 33°1	49°5 47°4 42°8 35°1 32°7	49° 5 47° 1 41° 3 36° 3 32° 2	50° 56 51° 81 50° 74 43° 46 38° 44
	32.9 48.3 46.5 37.7 36.4 37.5 39.6	30'3 48'3 41'7 37'3 36'0 36'9 40'0	48.5 41.3 36.9 35.7 36.5 40.0	48.1 43.8 37.2 35.5 35.7 40.0	48.0 42.8 36.7 35.5 35.7 40.2	48.2 42.1 35.7 35.5 35.7 38.9	43.7 49.3 42.1 35.9 35.5 35.7	43.6 49.1 38.7 35.9 34.9 36.1	44.2 49.1 37.3 35.7 34.7 36.9	44.6 50.8 37.5 35.5 34.1 37.3	44.8 50.6 37.6 35.5 33.5 37.0	$-\frac{1}{45.0}$ $51.8$ $38.1$ $35.5$ $33.0$ $36.6$ $-\frac{1}{37.9}$	36.51 48.08 46.45 37.56 36.02 36.75 38.46
	38'9 45'2 47'7 45'3 27'6 29'1	37.4 45.7 47.3 45.3 26.7 30.7	36.9 45.5 47.6 45.3 26.1 31.8	35.6 45.2 46.3 49.9 25.6 31.4	33.7 45.2 46.1 48.1 24.9 31.1	33°5 48°0 46°3 46°3 23°8 30°6	37.8 33.7 45.9 46.3 45.3 22.8	37·7 33·7 45·9 45·9 43·3 21·7	37.7 32.4 45.7 45.3 41.8 21.5	37·3 30·1 46·7 44·2 40·4 20·2  35·1	36.7 30.6 45.3 44.0 37.3 20.0	$     \begin{array}{c}       37.9 \\       29.2 \\       45.9 \\       43.1 \\       36.1 \\       19.0 \\       \hline       35.6     \end{array} $	37.00 42.77 47.48 43.25 26.63 29.25
	40°4 51°4 45°8 37°7 23°7 30°1	40°3 51°8 44°3 37°3 22°6 30°1	40'4 51'2 43'3 36'0 22'5 29'9	41.0 51.2 42.4 36.0 21.7 31.1	41.5 51.8 42.3 35.1 21.3 30.6	41.5 50.8 42.1 33.9 20.4 30.0	33°1 42°1 49°7 41°9 32°9 19°6	33°1 41°9 49°1 41°5 31°6 20°5	34 1 42 2 48 3 41 1 31 2 21 5 9 2	33 1 42 6 49 7 40 9 30 6 22 1 — 8 8	42°2 49°1 40°7 28°4 22°5 — 8°4	41.7 49.4 40.8 27.1 25.0 7.8	41:49 48:95 45:06 36:72 23:86 24:02
	12·1 23·8	11.6 25.1	11.6 26.3	$\begin{array}{c} -12.1 \\ 27.5 \end{array}$	12.6 29.5	14.3 30.1	10.4 15.2 30.4	10.2 17.4 30.0	17.2 26.1	$\begin{array}{c c} 16.2 \\ 23.6 \end{array}$	18·1 24·2	18:3 24:2	13°57 25°16
	38.86	38.29	38.20	38.22	38.50	37.85	37.43	37.07	36.46	36.12	35.75	35.67	38*46
	37.5 35.4 29.9 31.1	35°9 35°4 29°2 31°7	36.1 35.6 29.0 32.5	35°7 35°3 28°8 33°7	34.8 34.9 28.8 33.9	36·1 33·7 28·4 33·7	36.7 32.9 27.6	36.7 33.6 26.9	36.0 33.5 27.4 —	35.7 33.9 26.7	35.7 33.8 26.3	$   \begin{bmatrix}     35.1 \\     33.5 \\     26.1 \\     \hline     _{26.4}   \end{bmatrix} $	36.99 35.52 30.48 29.17
	28:4 32:7 42:9 43:0 42:1 29:9	31.8 32.2 41.9 43.7 41.2 28.4	30°4 31°4 41°6 43°7 41°2 27°4	28.9 31.8 41.7 44.8 40.2 27.9	33°1 33°1 41°5 44°3 39°3 27°2	32.7 31.8 42.6 47.1 38.7 28.3	26:3 32:7 32:4 42:6 46:5 38:4	26.5 32.3 32.2 42.4 46.9 37.9	26.8 32.8 33.3 41.0 45.3 36.5	26.4 32.9 33.1 40.4 44.8 35.3	25.5 33.0 34.9 39.8 46.0 33.2	32.9 35.9 38.1 46.2 33.3	31.09 34.82 41.70 41.95 42.48 34.63
	33°1 32°9 28°8 21°5 25°5	33°1 32°9 26°9 21°5 24°6	31'4 32'9 25'7 20'7 24'6	31.8 32.7 23.0 20.4 23.0	30.8 32.4 20.6 20.6 21.1	31.0 32.4 19.4 20.0 18.9	39.6 30.7 32.4 17.7 18.8 18.4	39.2 30.6 33.4 16.6 17.7 16.5	39.0 30.6 33.3 15.2 16.1 14.5	38.7 31.2 33.5 14.1 15.2 14.0	39.0 31.4 33.7 13.0 15.0 14.8	38·7 } 31·8 33·9 12·6 16·4 14·5	33.50 32.92 25.61 17.68 20.94
	33.9 	33.7 9.7 23.2 19.6 24.2 20.4	34'3 9'0 23'4 19'6 24'2 20'0	33.7 10.5 23.7 18.4 24.2 19.2	31.9 	33.5 	18.4 10.9 24.4 17.7 22.9	18:3 10:1 24:8 17:3 23:2	18.0 9.9 24.0 17.3 23.9	17.7 10.0 23.2 17.2 24.4	16.4 9.7 22.1 17.5 23.8	16.2 8.9 21.5 17.5 22.9	24.93 11.87 19.42 20.72 22.85
	19.6 34.7 41.2 42.8 43.2	19.4 35.3 40.4 43.2 42.4	19.0 35.3 39.8 43.2 42.1	21.5 36.1 38.8 42.1 41.9	22.7 35.4 38.7 42.0 43.4	24.5 35.5 38.6 41.6 43.2	9'9 25'0 36'1 40'0 41'5 44'0	10.1 26.1 36.3 40.3 41.6 44.6		12.0 27.0 36.5 41.7 41.2 45.7	14.3 28.4 36.7 42.3 40.6 45.8		18.55 20.18 34.72 40.69 42.74 43.83
	31.10	30.84	30.54	30.38	30.25	30.35	29.40	29.31	29.07	28.94	28.95	28.94	30.38

					SI	ANDARD	THERMO	METER.					
Hours o Götti Tin	f Mean	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \end{pmatrix}$	45°8	46.9	6.3 -	46.7	6.3 	47.8	48.2	48.0 	48.9 —	48.5	51.5 —	51°4
	3 4 5 6 7 8	33.0 34.7 23.8 11.8 12.8 30.3	33.0 33.8 25.5 10.9 13.7 31.2	33.9 31.9 26.7 10.0 13.9 31.0	35`4 30`3 27`4 10`0 14`8 30`8	36.0 30.1 27.8 10.7 15.0 31.4	36.9 28.9 29.1 12.0 16.0 32.0	37.1 27.6 31.6 12.7 18.4 32.3	37.9 27.1 34.9 14.0 19.4 33.7	38 · 2 26 · 6 34 · 7 13 · 2 19 · 8 34 · 1	38°3 25°6 36°9 13°9 19°8 32°7	37.7 23.9 35.1 13.8 19.6 32.1	36.7 21.5 31.2 13.0 19.6 30.6
RY.	9 10 11 12 13 14 15	-11.3 8.8 10.9 33.3 36.7 39.8	$ \begin{array}{c} -12.0 \\ 9.2 \\ 8.1 \\ 33.7 \\ 36.8 \\ 39.6 \end{array} $	$ \begin{array}{c c} -11.8 \\ 15.0 \\ 7.2 \\ 33.1 \\ 37.1 \\ 41.1 \end{array} $	-9.3 16.9 13.7 35.2 37.3 41.2	$ \begin{array}{c c} -6.9 \\ 17.8 \\ 19.1 \\ 35.9 \\ 37.3 \\ 42.4 \end{array} $	$ \begin{array}{c c} -4.6 \\ 19.8 \\ 21.7 \\ 35.9 \\ 37.9 \\ 43.2 \end{array} $	$ \begin{array}{r} -2.5 \\ 20.0 \\ 25.0 \\ 35.6 \\ 37.8 \\ 44.4 \end{array} $	0.6 21.7 26.7 36.9 38.1 44.1	0.2 22.5 25.9 37.1 38.3 44.6	0°2 22°5 26°9 37°2 38°3 47°3	0°1 21°7 25°0 36°9 38°3 47°1	0.6 21.1 21.3 36.9 38.2 43.8
JANUARY	16 17 18 19 20 21 22	31.5 30.3 5.0 29.7 38.3 15.2	31.3 25.3 5.0 30.2 38.0 15.4	25.9 22.7 5.7 30.4 38.0 16.9	24.8 22.8 9.2 33.5 40.6 18.4	23.4 21.9 13.2 36.0 43.2 20.0	24 · 0 21 · 1 14 · 6 37 · 6 45 · 2 22 · 7	24.3 21.5 17.4 38.5 45.3 25.3	25°0 21°1 18°1 38°8 44°4 26°3	25.7 20.4 19.8 40.6 41.9 27.8	26.5 20.6 21.3 41.9 38.2 29.7	25°3 18°8 21°9 39°2 34°2 29°2	24.8 17.6 21.1 37.1 32.0 27.2
	23 24 25 26 27 28 29	21 '9 27 '4 38 '0 38 '1 31 '0 26 '5	20.6 28.0 37.7 37.4 31.7 29.5	21.1 28.9 37.9 37.9 31.8 30.7	26.7 33.5 38.2 38.7 31.4 31.6	29.5 36.1 38.2 39.9 33.8 31.6	30.6 37.7 38.0 40.7 34.5 31.3	31·2 37·7 38·3 42·3 35·1 31·6	31.0 38.2 38.5 41.4 35.5 31.8	32.7 39.8 39.3 40.2 35.5 32.1	32.7 39.9 39.6 40.2 35.1 32.4	32·3 38·3 39·8 39·3 33·3 32·1	30.8 35.9 40.0 38.3 33.1 31.6
	30 31	33.3	33.9	34.3	35.9	36.5	36.7	37.3	37.8	37.9	39.5	38.8	36.2
Hourl	y Means	26.02	25.90	26.06	27.53	28.69	29.67	30.24	31.19	31.45	31.73	31.00	29.69
2	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ \end{pmatrix}$	27.1 20.8 28.6 32.0 28.8 — 22.7 18.9 22.3 21.1 0.4 13.0	27.4 21.3 27.4 33.7 28.0 — 21.7 19.5 22.5 18.7 0.6 13.4	28.0 21.7 27.4 34.3 27.4 ————————————————————————————————————	29°1 28°7 31°8 36°7 27°1 ————————————————————————————————————	30°2 33°7 35°7 39°3 27°9 22°9 23°2 29°0 13°9 5°5 19°6	30°2 35°5 38°1 39°6 28°4 ————————————————————————————————————	28 '9 35 '5 39 '3 39 '6 28 '3 	27.6 36.1 41.0 38.7 27.8 25.3 26.9 33.5 16.0 11.8 24.4	28.6 36.5 41.4 37.5 28.4 — 26.7 28.2 34.9 16.9 12.7 25.5	29·2 36·5 40·8 37·4 28·0 ————————————————————————————————————	29.0 35.9 39.1 37.5 27.6 ————————————————————————————————————	26.9 34.1 36.3 37.2 26.1 ————————————————————————————————————
FEBRUARY.	13 14 15 16 17 18 19 20	19°2 20°3 21°7 21°7 20°6 30°8	18.2 18.8 24.8 20.7 20.8 31.7	20°2 19°0 26°1 25°5 25°7 32°9	27.6 21.5 32.0 30.2 31.9 34.9	32 · 1 24 · 7 34 · 1 33 · 8 34 · 8 35 · 9	34 · 3 27 · 4 35 · 7 35 · 7 36 · 3 37 · 1	36.9 30.1 36.7 36.7 37.1 39.0	37.9 33.3 36.7 36.9 37.7 39.5	38 · 9 32 · 4 35 · 9 36 · 8 38 · 1 39 · 3	38.8 31.6 35.8 36.1 37.4 38.1	38°3 32°0 35°3 35°3 37°7 36°9	36.9 31.3 33.3 32.7 36.9 36.7
	21 22 23 24 25 26 27	36.9 30.3 31.5 22.4 11.0 12.1	37.1 31.6 29.8 23.0 10.6 12.2	37 1 33 1 32 7 24 1 12 1 19 2	39°1 34°4 35°0 24°9 15°8 26°3	40.0 35.9 35.7 25.8 17.7 30.3	41.5 37.7 35.7 27.5 19.0 31.1	43.8 38.7 35.1 26.9 20.1 31.8	45'3 40'6 37'2 28'0 20'8 33'5	46°3 39°7 33°4 29°0 23°6 34°3	46 '9 37 '1 33 '9 30 '1 22 '3 34 '3	46.5 36.6 32.4 30.3 23.4 34.2 	43.0 35.8 30.8 27.6 21.5 32.7 — 36.8
Па	28 Maana	28.2	$\frac{28.4}{22.58}$	$\frac{29.7}{23.98}$	$\frac{28.8}{26.70}$	29.9	30.8	31.30	33.8	34.9	$\frac{36.1}{32.32}$	31.99	30.28
Hourly	y Means	22 60	22 58	25 98	20 /0	20 82	ου Δ1	01 20	02 10	. 02 00	02 02	01 00	

						STANDA	RD THER	MOMETE	R.				
	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
	6	7	8	9	10	11	12	13	14	15	16	17	Means.
	0	0	0	o	0	0	0		0	0	0	0	0
	43.2	40.6	38.9	37.1	36.1	34.2	32.2	32.9	31.8	32.7	32.7	$\frac{-}{33\cdot 1}$	41.75
	36.7	37.3	37.2	37·3	37.3	37.7	38.3	37.6	$\frac{31.8}{36.7}$	35.5	36.0	36.3	36.28
	20.2	19.7	19.4	19.0	18.6	18.4	18.2	19.0	19.3	20.3	20.5	20.5	$23.96 \\ 24.95$
	28.6 12.1	26.7 11.7	26.4 11.0	$\frac{23.3}{11.0}$	20.0 10.2	$\frac{18\cdot2}{10\cdot6}$	17°2 10°5	$\frac{16.9}{10.7}$	17.7 10.8	14.8 11.3	12.4 11.2	$\begin{array}{c} 12.0 \\ 12.3 \end{array}$	24 95 11.65
l	22.8	23.6	23.5	24.8	25.6	26.5	27.2	27.2	28.4	28.8	29.5	30.1	21.40
	29.9	29.9	28.6	26.9	25.5	23.6	_ <del>_</del> 4.5	$-\frac{-}{6.4}$	_ <del>7</del> .7	- 8·9	-10.5	-11.0	20.73
	5.3	<b>-</b> 7·3	<b>-</b> 7·3	<b>-</b> 6.5	- <del>7·</del> 7	- 8.9	- 9.1	-8.6	_ 5.3	_ 2.7	0.4	0.5	- 5.20
	20.8	21.1 26.1	21.4 26.7	21.5 26.7	$\begin{array}{c} 21.5 \\ 28.0 \end{array}$	21.3 $28.4$	21°1 27°8	$\frac{211}{291}$	20°4 29°3	20.0 32.0	14.6 32.4	$\frac{9\cdot2}{9\cdot2}$	18.79 23.84
	36.7	36.9	36.7	36.9	36.7	36.6	36.9	36.9	36.7	36.9	37.1	36.2	36.25
	38.7	39.1	39.5	39.6	40.0	39.8	39.6	40.6	39.8	39.6	40.0	39.8	38.68
	40.0	37.5	36.4	36.1	34.4	34.2	30.6	30.6	31.4	31.8	31.6	$\frac{1}{31\cdot 4}$	38.23
	25.7	26.2	26.5	27.6	26.4	27.4	28.0	28.0	30.3	31.0	30.8	30.8 5.7	27:13 16:86
	16.0 20.6	14.4 23.6	$\begin{array}{c} 13.9 \\ 23.8 \end{array}$	14.1 24.6	14.8 25.3	15°0 25°0	13.7 26.3	10.3 $25.5$	$\begin{array}{c c} 9.1 \\ 25.5 \end{array}$	$\begin{bmatrix} 7.1 \\ 27.4 \end{bmatrix}$	$\begin{bmatrix} 6.4 \\ 27.9 \end{bmatrix}$	$\begin{array}{c c} 3 & i \\ 29 & 2 \end{array}$	19.88
-	36.4	34.1	35.7	36'1	35.9	37.7	38.1	38.7	39.1	39.5	39.3	38.6	36.78
	30.6 26.5	28.4 23.4	26.5 23.0	$\begin{array}{c} 24.2 \\ 22.3 \end{array}$	$\begin{array}{c} 23.7 \\ 22.5 \end{array}$	$\begin{array}{c} 22.3 \\ 21.8 \end{array}$	20.4	19.2	19.0	18.1	17.0	16.9	31.07
- 1	1						24.2	24.0	24.0	23.8	23.6	$\frac{-}{24\cdot 4}\}$	23.24
	28.8 36.7	27.5	26.7	26.5	26.3	$\begin{array}{c} 26.3 \\ 35.7 \end{array}$	25 <b>.</b> 9 36.1	24.6 $36.7$	25°9 37°3	$\begin{array}{c} 25.7 \\ 37.7 \end{array}$	26.5 39.3	$\frac{26.9}{38.2}$	27.45 36.00
	40.8	36.7 40.3	36.2 38.9	35.2 38.9	36·1 38·1	38.3	$\frac{30.1}{37.3}$	36.2	37.1	37.6	$\frac{39.5}{37.6}$	$\frac{36.2}{37.9}$	38.45
- 1	37.5	36.3	34.5	35.3	35.3	35.0	34.3	34.8	34.5	34.6	33.8	32.5	37:19
	33.5 30.8	33.8 30.6	$\frac{30.0}{33.3}$	33.5 $29.7$	30.7 $29.2$	$28^{\circ}6$ $29^{\circ}2$	27.1	26.3	25.7	25°5	26.3	24.7	31.27
- 1	35.7	32.0	31.6	29.5	26.3	26.1	31.3 25.5	$\frac{31.6}{25.1}$	31.8 25.3	$\begin{array}{c} 32.0 \\ 25.3 \end{array}$	$\frac{32\cdot2}{25\cdot5}$	$\begin{bmatrix} \overline{32\cdot7} \\ 25\cdot7 \end{bmatrix}$	31.00
-	28.65	28.08	27.67	27:35	26.81	26.21	25.16	24.96	25.12	25.58	25.16	24.90	27.70
			1						<u> </u>		l	<u> </u>	
	26.3	23.8	21.1	19.4	17.7	18.0	18.6	19.4	20.8	21.7	22.5	22.1	24.73
	33.1	33°1 31°4	32°7 31°0	32.4 30.0	32.0 29.0	32.4 $28.7$	32.9 27.5	$\begin{array}{c} 32.9 \\ 27.2 \end{array}$	$\frac{32.7}{27.6}$	$\begin{array}{c} 31.6 \\ 28.4 \end{array}$	$\frac{31.3}{29.5}$	31.0 31.4	31.85 32.55
- 1	37.1	36.1	34'1	33.7	32.7	31.8	31.0	30.1	29.7	29.5	29.2	29.0	34.48
Ì	25.3	25.0	24.4	24.6	24.4	24·8 —	24.0	23.4	23.5	$\frac{-}{22.5}$	22.3	$\left\{ \begin{array}{c} -22.9 \end{array} \right\}$	25.86
	24.0	22.3	20.6	20.6	18.8	18.6	16.6	16.4	16.0	16.6	17:3	18.1	21.54
	25·3 33·1	25.3	25.3	25.6 $32.0$	26.0 31.8	30.8	23°2 29°1	$\begin{array}{c} 21.8 \\ 27.4 \end{array}$	19°2 27°0	$\begin{array}{c} 18.1 \\ 27.8 \end{array}$	21.2 $26.3$	$\frac{22.1}{25.0}$	23.58 30.03
	13.3	$\begin{array}{c} 32.7 \\ 12.4 \end{array}$	$\frac{32\cdot4}{12\cdot2}$	12.5	12.0	9.9	7.8	5.7	4.3	$\frac{27.6}{2.5}$	1.9	1.5	12.01
- 1	12.6	12.6	13.0	12.8	12.4	12.2	12.6	13.4	13.1	13'4	13.4	13.5	10.49
- 1	20.2	17.7	16.6	15.2	14.4	13 <b>·</b> 9	26.7	2 <b>4</b> .8	27.8	28.5	23.6	$\frac{1}{20\cdot 4}$	20.53
	34.9	33.1	31.6	30.0	<b>2</b> 9.6	27.1	26.3	25.5	24.4	<b>25</b> • 9	23.3	$\begin{array}{c} 22.8 \\ 22.7 \end{array}$	29.74
	28.6 28.8	26.7 27.0	26.6 26.0	23.6 25.5	23.5 25.3	23.8 24.2	21.7 24.0	$20.8 \\ 23.6$	20°3 24°4	20°3 23°6	$\begin{array}{c} 20.0 \\ 25.3 \end{array}$	21.9	25.04 28.53
ı	31.2	28.0	27.4	25.9	25.3	24.4	24.1	22.7	21.8	21.5	20.4	22.1	28.22
	32.0 37.8	30°1 37°7	29°2 38°6	28.8 38.4	29.7 38.1	$\begin{array}{c} 29.7 \\ 37.0 \end{array}$	30.1	29.5	30.0	29.6	29.3	29.2	31.32
1	-						38.0	38.0	37.8	37.4	37.6	$\frac{-}{37.5}$	36.95
	38·2 34·7	38.7 34.1	38°3	38.6 33.7	36.7 32.7	35°1 33°5	34.9 32.7	$\frac{34.9}{32.4}$	32.0 32.4	31.6 32.3	31.1	31.3 32.0	38°56 34°45
	29.5	28.4	27.6	27.9	26.9	26.8	26.2	26.1	24.1	22.7	22.3	22.1	29.75
	24.0	22.1	22.1	22.5	22.1	21.9	20.4	19.0	17.5	16.3	13.1 13.4	$\begin{array}{c} 12.5 \\ 12.4 \end{array}$	23.05 17.05
	30.6	19.1 29.8	17.6 29.1	16.0 30.4	15°5 29°7	16.0 28.9	18.1	15.1	14.5	14.3		$\frac{12}{26.6}$	25.43
-	35.4	33.9	32.1	32.7	31.6	29.7	15°2 28°6	14.8 26.8	13.0 25.0	12.2 22.9	18.0 23.5	26.6 §	30.34
	28.68	27.55	26.81	26.32	25.75	25.12	24.61	23.85	23.28	22.97	22.67	22.93	26.96

					SI	ANDARD	THERMO	METER.					
	of Mean ingen me.	0	1	2	3	4	5	6	7	8	9	10	11
Hours o	of Mean onto me.	18	19	20	21	22	23	0	1	2	3	4	5
	$\left( egin{array}{c} 1 \\ 2 \\ 3 \\ 4 \end{array} \right)$	10°1 8°0 18°4 18°3	7·2 8·7 18·6 17·7	9.6 11.9 17.5 18.8	10°7 14°1 18°6 20°2	12°4 16°2 19°5 23°4	15°2 16°9 21°6 23°2	18·2 18·4 22·9 24·4	20°0 20°8 23°9 24°0	21°1 20°8 26°0 23°6	18.9 20.3 26.4 21.9	20°0 20°0 25°3 20°9	18°0 17°7 24°4 19°5
	5 6 7 8 9 10 11	20.0 17.3 36.5 23.6 16.4 16.5	19.8 20.0 37.9 22.9 16.3 17.7	21.7 24.1 38.9 23.8 16.2 21.1	23.4 31.0 39.8 24.8 18.4 26.3	25°3 34°4 42°8 25°7 20°9 29°2	26°1 36°1 44°4 25°9 23°8 30°6	27.1 38.5 44.8 26.9 26.3 33.1	28.7 39.8 45.0 27.1 28.4 32.9	31.0 40.6 43.6 28.4 32.0 33.9	32.0 41.6 47.4 29.2 31.1 34.7	32.8 41.1 40.8 28.4 29.6 34.0	32.7 40.0 36.5 27.4 29.7 33.1
MARCH.	12 13 14 15 16 17 18	24'1 11'6 2'7 11'6 24'2 20'0	24.6 11.1 3.9 13.1 25.1 22.9	24.5 12.6 5.9 16.6 25.7 27.4	24.3 13.2 8.0 20.4 24.7 30.7	23.0 15.6 10.9 22.3 24.7 32.1	24.5 15.2 12.0 24.3 25.1 33.1	24.6 15.6 14.8 25.7 25.7 33.8	25°3 15°6 15°5 27°0 25°8 34°9	25°3 14°8 17°1 28°2 26°3 33°9	23.0 13.9 17.5 28.8 26.4 33.2	22.9 12.2 17.3 28.1 27.0 32.7	22.7 10.4 16.4 28.4 26.8 32.0
	19 20 21 22 23 24 25	24.8 40.4 30.4 33.7 28.2 36.2	26.8 39.5 32.2 33.9 32.4 37.1	31.0 39.1 34.2 34.7 35.7 40.6	32.7 41.9 36.3 35.1 37.0 41.8	34.9 43.7 36.9 37.8 39.1 39.1	34.7 46.6 37.3 39.4 38.9 39.3	35°3 48°1 37°5 40°2 39°2 39°3	34.5 48.9 37.5 41.2 39.6 39.6	35.0 49.3 37.3 39.5 38.3 41.5	35.7 49.3 37.7 40.2 38.8 44.2	36.5 48.3 37.1 39.7 39.2 44.2	36.6 46.3 36.1 39.6 37.5 44.1
	26 27 28 29 30 31	33·3 27·4 32·0 33·2 36·3	33°3 29°5 36°1 37°5 38°5	33°3 33°3 41°5 38°9 42°5	33 '9 37 '1 45 '3 40 '8 48 '0	34.7 40.0 47.3 40.8 51.4	36.7 43.2 48.3 41.0 55.0	40°2 44°6 50°6 41°5 57°1	41.5 43.8 52.6 40.6 56.9	41.7 45.6 57.8 43.0 58.3	40.6 44.5 57.7 44.4 61.9	39.1 44.6 58.9 45.3 59.9	38.0 44.6 58.9 44.8 57.5
Hourly	Means	23.23	24.60	26.71	28.83	30.52	31.79	33.13	33.76	34.59	34.86	34.29	33.32
	1	33.7	34.3	33.7	33.7	34.2	36.8	36.7	36.4	36.4	36.9	35.7	35.2
	2 3 4 5 6 7 8	33 · 1 43 · 1 31 · 9 29 · 7 35 · 3 29 · 5	38·1 43·2 33·2 33·1 38·5 34·4	40.8 42.8 34.6 37.8 41.9 43.2	42.3 44.4 36.5 42.9 45.7 46.9	43.8 44.9 38.9 44.5 46.8 48.2	44'4 44'9 41'3 46'0 46'3 48'7	44.4 45.3 43.9 46.3 45.3 49.9	45°3 45°4 42°4 46°9 44°4 50°1	45.3 47.5 41.9 46.9 44.6 53.3	45 · 2 46 · 7 41 · 6 47 · 9 46 · 0 53 · 9	47.9 45.2 41.3 48.3 45.2 53.2	48.0 44.4 41.9 49.9 44.7 53.5
IL.	9 10 11 12 13 14 15	38°1 46°9 32°2 37°1 37°5 40°6	45.1 48.5 38.9 38.7 39.1 44.0	54.0 51.4 43.6 39.4 39.5 47.7	59.7 50.7 48.3 39.5 41.8 50.0	58.7 50.6 50.1 41.2 42.9 53.4	62.5 51.5 51.0 40.4 43.4 55.1	63°1 51°0 50°4 40°2 45°5 56°3	65.4 50.4 53.8 42.6 48.1 56.7	64.5 50.4 54.4 40.4 45.5 56.5	62.5 48.9 53.4 40.4 45.7 56.7	63.4 47.3 52.4 40.0 45.2 56.1	60°3 47°3 49°5 38°5 42°8 55°4
APRIL,	16 17 18 19 20	33.6 33.8 26.3 27.6	36.0 33.3 30.6 31.8	36°8 34°7 32°2 39°1	38.2 35.3 33.3 41.0	40°4 36°0 35°9 42°5	42°2 37°3 36°7 43°8	43.8 33.7 39.5 46.9	45°1 32°2 39°1 47°9	45°2 29°2 39°4 49°1	42.5 29.0 37.9 50.4	43.4 29.9 38.2 48.1	43.8 29.9 39.6 48.1
	21 a 22	41.5	41.9	43.6	45.2	44.4	45.3	48.9	49.9	49.0	46.7	48.1	51.0
	23 24 25 26 27 28 29 30	36°3 28°8 33°3 29°6 38°8 42°6 —	36.7 33.9 36.7 38.4 46.4 44.4	37.5 36.5 38.7 42.7 41.5 43.9	40'4 41'0 40'6 45'3 42'4 42'8	42·3 42·3 44·0 46·7 44·0 44·2	43.2 43.4 44.5 49.5 45.7 45.5	44.0 45.0 45.1 49.8 44.8 47.8	43.4 46.0 45.1 52.8 46.1 49.1	42.8 45.6 48.1 52.8 48.3 49.3	43.2 43.6 46.7 54.2 49.6 50.4	42.3 44.4 47.2 52.4 47.9 50.4	41.8 41.7 46.6 50.1 47.1 48.7
Hourl	y Means	35.04	38.30	40.73	42.41	44.22	45.39	46.12	46.86	46.92	46.67	46'40	45.84

a Good Friday.

					STAND	ARD THE	RMOMETI	ER.				
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
16°2	15.2	13.0	8.0	12.2	11.3	6.4	o.8	4.5	8.0	8.4	8.8	12.26
15°5 22°9	15.0 21.1	15.0	15.6 18.4	15°3 17°6	16.0 17.3	17.5 18.6	18°2 18°4	18.8	19.0	19.3	19.0 18.4	16.58 20.29
18.1	17.5	17.6	17.4	18.0	16.6	19.2	20.2	21.3	20.3	21.9	$\left\{ \begin{array}{c} - \\ 22 \cdot 8 \end{array} \right\}$	20.28
32.2	26.9 38.5	23·2 37·9	20.5	20.2	20.7	17.5 38.4	17.7 38.7	17.7 39.3	18.0	17.5 38.1	16.0 37.0	23.70 36.15
35.2	34.9	34.5	34.3	34.4	34.1	33.2	31.9	29.9	28.7	27.8	27.1	36.88
27.5 27.8	26.4 25.5	26.3	26.5	25.2 20.6	24.7 20.2	24.3	24.0 18.6	21.2 17.6	20.7 16.9	18.5 16.0	17.5 17.3	24.87 22.22
31.6	29.9	29.8	29.9	29.1	30.3	30.6	30.8	28.8	27.4	26.1	$\frac{1}{24\cdot 4}$	28.83
20.0	18.8	18.0	17:3	16.0	15.2	14.5	14.0	13.4	13.1	12.8	12.6	19.77
7.8 14.5	6.8 12.4	6.6 12.0	5.7	5.6 10.2	5°3	4.8 9.0	4.6 8.6	$\frac{3.7}{7.4}$	$\begin{vmatrix} 3.5 \\ 7.2 \end{vmatrix}$	3.6 3.6	3·3 10·5	9:30 10:59
27.4 26.3	27·4 22·9	26.5 21.1	26.3 20.8	26.3 19.6	26°1 18°4	25.7 19.4	25°3 17°8	24.7 16.0	24.4 17.8	24.8 18.6	24.6 19.4	24·33 22·73
31.6	31.5	31.0	31.0	30.3	30.1						$\frac{13}{23.9}$	29.58
37.1	37.1	36.6	36.1	35.4	35.0	28°1 35°1	24.9 35.5	25°3 37°1	24°3 43°1	24.2 43.7	43.2	35.28
41.2 34.9	38·2 33·8	$\frac{37.1}{32.8}$	36.0 32.9	$\frac{33.8}{32.4}$	$\frac{33.3}{32.7}$	31.8 32.7	31.4 33.1	$\frac{30.8}{32.4}$	$\frac{30.6}{32.9}$	29.7 33.4	29.7 33.7	39°38 34°51
37.0	35.2	32.8	30.6	29.5	29.0	29.0	28.6	27.8	28.6	27.4	28.0	34.15
35°3 43°0	34·1 42·6	34.8 42.2	35°1 41°4	35.5 41.1	36.0 40.6	36.7	36.8	35.7 —	36.0	36.7	36.3	36°37 39°50
36.6	35.1	34.1	33.3	31.1	30.8	36.9 29.3	$\frac{35.9}{29.9}$	$\begin{array}{c} 35.2 \\ 28.2 \end{array}$	$\begin{array}{c} 34.6 \\ 28.4 \end{array}$	33.9 $28.2$	$\begin{bmatrix} -33.7 \\ 27.4 \end{bmatrix}$	34.11
42.4	41.1	40.8	40.8	40.6	39.2	38.7	36.3	38.9	36.4	36.1	32.4	39.26
55.6 42.6	47.8 40.6	44 <b>.2</b> 39.8	40.7 39.6	38 <b>.</b> 8	36.9	$\begin{array}{c} 34.1 \\ 38.3 \end{array}$	$\frac{32.0}{37.9}$	31.4 37.3	31.8 $36.7$	36.0 30.1	30.6 35.5	43°38 39°78
54.0	51.5	49.1	48.3	47.5	40.7	37.3	36.8	35.9	35.1	34.7	34.2	47.02
31.64	29.91	28.84	28.03	27.59	26.61	26.50	25.21	25.50	25*29	25.13	24.74	28.94
34.7	<b>3</b> 3.3	32.8	32.8	32.3	32.0	 34·9	34.3	33.9	33.7	33.4	31.8}	34.34
46.6 43.0	$\frac{46.0}{42.3}$	46.5 41.0	45°3	$\frac{44.8}{37.7}$	$\frac{46\cdot3}{37\cdot2}$	46 <b>·</b> 9	$\begin{array}{c} 45.7 \\ 34.9 \end{array}$	45°3 33°9	$\frac{44.3}{33.3}$	$45^{\circ}2$ $32^{\circ}4$	44.0 30.9	44.40 40.85
41.4	38.3	36.1	34.2	33.2	32.0	30.3	29.2	28.0	27.8	27.6	27.5	35.65
48.2 44.6	44.8 40.4	41.9 36.7	40.6 35.0	$38.7 \\ 35.5$	$\frac{38\cdot1}{37\cdot2}$	$\frac{33.9}{36.9}$	$\frac{35\cdot2}{33\cdot7}$	$\begin{array}{c c} 35.7 \\ 33.7 \end{array}$	$\frac{35.7}{30.7}$	35.4 $30.1$	34.4 28.2	$\frac{41.08}{39.35}$
53.0	47.5	42.6	41.4	40.6	40.8	39.3	39.3	38.2	36.6	36.9	36.6}	44.08
59.3	58.7	57.3	51.0	49.1	47.5	48.3	51.2	51.2	50.9	47.1	43.9	54.70
47.7	47°1 47°7	47.5 46.7	$\frac{49.7}{48.1}$	49 <b>·</b> 9 48 <b>·</b> 7	48.7 $45.0$	46°3 43°8	41°4 44°1	37:3 43:8	$\begin{array}{c} 34.5 \\ 42.5 \end{array}$	35°1 40°6	31.3 39.8	46°31 46°54
38.7 41.3	37.7	36.9	37.1	36.8 40.0	$\frac{36.2}{39.5}$	36.9 35.4	36.7	35·7 40·0	36·7 40·3	36.7 39.8	37·1 39·2	38.40
53.4	40.0 48.9	38·3 46·3	37.7 45.0	44.6	43.6	- 1	35.1				$\frac{35 \cdot 2}{31 \cdot 4}$	40°98 47°01
42.8	39.5	38.7	38.7	38.7	38.7	40.8 39.3	39°3	36.9 37.8	35.7 36.1	33.9 35.4	31.4 }	39.55
30.1	29.5	29.7	30.3	29.8	27.8	26.8	27.4	25.7	24.7	24.2	24.0	30.19
38.6 47.5	$\begin{array}{c} 35.9 \\ 43.8 \end{array}$	33.0 40.9	34.5 40.4	31.2 $39.6$	27.8 39.6	27.1	25.9	25.0	26.9	26.3	$\frac{25.0}{42.1}$	32.75 43.63
52.0	44.8	44.6	42.3	40.6	$\frac{-}{35.9}$	48.7	49.8	47.4	45.7	45.3		į
41.9	39.1	36.9	35.4	35.1	32.4	35.1	35.7 30.6	36.3	$\frac{36.5}{26.9}$	35.9 26.3	$\frac{-}{35\cdot 3}$	42.94 36.96
41.0	41.3	41.5	40.8	40.4	43.8	42.4	38.7	36.2	34'1	32.0	29.9	39.78
44.3	41.5 44.8	39°3 44°8	37.5 41.5	36.5 38.7	33°1 37°4	31.0 37.9	28.4 37.3	$\begin{bmatrix} 28.4 \\ 36.3 \end{bmatrix}$	27.6 36.2	$\frac{26.7}{37.0}$	27.4 37.8	38 26 43 39
45°3 48°3	43.8 44.6	42.4 42.1	42.9 39.6	43°5 38°8	42.9 34.8	42.9	42.8	42.6	42.4	42.2	42.0	44.10
	T1 U	42 1				36.7	36.3	35.2	34.7	38.2	39.2}	42.85
44.96	42.55	41.02	40.06	39:38	38.26	37.88	37.13	36.20	35.60	35.18	34.18	41.17

					S'.	randari	THERMO	METER.					
lours o Göttir Tir	f Mean }	0	1	2	3	4	5	6	7	8	9	10	11
Iours o Toro Tim	f Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	1 2 3 4 5 6 6	40°8 41°4 45°6 46°4 54°2 52°4	42.6 42.3 51.4 49.4 60.3 59.7	44°0 44°8 55°0 53°2 60°9 62°7	46°9 50°7 56°2 58°3 65°9 65°0	48°1 53°6 59°5 57°9 67°7 66°7	48°9 51°7 60°4 58°7 69°7 70°3	49°7 52°5 61°4 56°5 69°3 70°1	46°3 53°3 60°1 55°2 70°9 71°0	44.5 54.0 61.3 54.7 68.5 72.1	46°3 53°1 64°1 54°0 69°7 70°7	47°4 53°1 63°7 52°0 70°0 68°4	47 4 64 6 62 4 68 4
	7 8 9 10 11 12 13	41.3 45.1 45.8 46.1 42.1 36.3	46.1 52.3 47.9 46.1 44.5 38.7	49.9 55.7 50.0 47.7 46.2 40.0	53°5 57°5 52°4 49°4 48°3 40°1	53.7 57.7 52.5 50.2 50.8 40.2	55.6 57.9 52.5 51.8 52.3 42.3	56.6 59.5 53.1 51.2 52.9 43.8	57.0 62.3 54.4 49.3 53.3 48.1	56.6 60.3 55.4 48.7 54.3 45.9	56.9 56.9 54.8 48.3 54.2 46.1	57.4 57.9 54.4 49.8 54.2 43.2	56°5 56°5 50°5 54°4
MAY.	14 15 16 17 18 19 20	39'9 49'1 42'4 50'8 56'3 58'5	46.6 52.5 52.2 58.3 57.9 58.6	52.5 54.9 54.0 59.9 63.5 62.8	54°1 56°5 57°0 64°4 66°1 68°4	55°7 57°9 58°1 66°0 68°7 69°9	57°5 58°5 60°7 67°0 71°7 69°6	56.0 58.7 61.7 68.9 71.4 73.9	56.5 59.7 62.9 70.6 70.7 68.9	54.0 59.3 63.7 72.8 72.0 69.5	50.6 57.9 64.6 73.2 69.5 67.6	50°4 59°3 65°0 72°7 64°9 65°6	47:3 57:6 62:3 71:6 66:4
	21 22 23 24 25 26 27	57.4 57.1 53.8 56.0 51.9 50.8	55°1 55°0 54°4 57°3 54°3 52°8	55°9 55°6 57°8 59°7 56°5 58°2	59°5 55°2 60°1 62°5 57°5 61°5	61 · 1 55 · 0 65 · 0 66 · 7 59 · 4 62 · 3	61'4 55'0 66'7 69'4 61'5 62'4	60.7 55.2 69.2 70.3 65.6 62.2	61:3 55:8 71:7 70:4 66:1 64:9	61.5 56.9 72.1 72.3 67.1 66.3	61.5 59.5 73.3 76.3 65.3 66.0	60°3 58°9 74°1 78°5 63°9 66°9	62: 59:9 67:3 64:0 64:0
	28 29 30 31	59°3 54°0 43°8	63°3 59°1 45°5	62°5 63°3 46°1	64°0 63°7 48°8	69°4 64°4 50°7	64°1 66°3 52°5	69.6 67.2 54.0	72·1 67·6 54·9	71.5 61.9 55.1	73°3 59°2 55°6	70°9 57°6 56°7	75° 55° 57°
Hourly	Means	48.84	52.01	54.57	57:17	58.82	59.87	60.79	61:31	61.20	61.06	60.64	59.8
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	46.6 48.7 66.1	51°2 55°1 65°5	53.4 59.0 65.5	54°9 61°3 67°1	55°9 64°0 67°9	58°1 66°5 68°1	59°8 67°9 69°3	61.3 69.6 69.5	60°7 70°3 70°9	61°3 69°3 71°3	62°2 66°4 70°1	64°3 68°9
	4 5 6 7 8 9	55.2 48.1 47.2 52.7 54.8 60.3	59.1 50.8 49.6 56.4 61.1 60.7	62.9 51.2 51.4 60.4 61.1 66.7	63°3 53°0 53°6 62°4 65°6 69°3	64·1 52·4 56·2 64·1 67·5 71·5	66.6 53.8 58.0 65.2 69.0 70.3	67.3 56.3 60.2 64.2 70.9 70.1	60°2 56°4 61°6 64°5 72°1 70°6	59 '9 56 '4 63 '5 64 '1 73 '1 71 '7	64.0 56.7 63.8 65.7 73.3 79.1	68.9 56.7 62.1 68.6 74.3 67.7	62:6 55:4 62:3 63:3 71:7
JUNE.	11 12 13 14 15 16 17	48.5 46.6 45.0 61.0 73.1 67.1	49.7 48.9 45.2 67.4 75.5 72.5	51.0 52.0 49.3 72.1 79.4 76.0	52.0 53.4 54.2 74.0 82.0 76.9	54.6 56.7 55.7 78.2 84.6 79.9	55°1 58°3 61°8 85°1 83°4 82°3	56.0 60.7 59.3 88.0 87.8 82.7	56°3 61°7 56°9 89°5 83°5 78°7	56.7 62.5 61.7 91.1 85.1 76.3	56.9 63.0 65.5 92.0 85.7 81.9	56.8 62.2 65.9 91.0 81.9 77.0	56:3 61:3 64:4 90:8 82:3 79:9
	18 19 20 21 22 23 24	63.9 62.6 58.9 57.2 61.1 58.9	65.5 65.5 62.7 59.7 62.0 61.9	70.0 69.5 61.3 67.3 63.6 64.8	72·7 72·3 63·9 68·9 64·4 65·2	72.7 73.9 66.1 66.5 67.5 68.5	74.9 70.7 65.1 67.7 70.3 70.3	75:3 71:8 67:3 69:1 71:9 71:7	78.0 71.5 68.3 71.5 74.8 72.7	73°1 71°9 68°3 69°9 77°8 73°1	72.5 71.1 69.7 70.1 73.5 73.9	74.5 72.5 71.5 69.9 72.9 73.1	72:3 60:7 70:6 65:3 68:0 72:7
	25 26 27 28 29 30	61.8 60.1 69.1 60.4 58.7	69.5 65.4 68.0 64.9 62.3	75°1 70°5 70°9 69°3 67°9	74.7 74.3 71.1 71.9 68.8	77:1 74:7 71:9 72:3 70:4	78.6 74.1 70.7 72.1 73.7	80°3 75°7 70°7 73°1 72°9	81.5 76.1 70.7 73.5 78.5	82.1 77.8 71.2 74.5 77.6	82.5 76.6 72.1 74.8 77.2	81.9 77.6 71.7 75.9 77.1	80:8 72:6 71:1 73:8 77:8
Iourly	Means	57.45	60.62	63.91	65.82	67:50	68.84	70.01	70:37	70.82	71.67	71.17	69.4

	<del></del>				STANDA	RD THER	MOMETE	R.				
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
45°.4 52°.9 57°.7 53°.0 60°.7 61°.3	43°0 49°3 53°6 54°0 57°4 62°6	41°8 45°7 49°7 54°8 62°9 62°4	40° 4 43° 4 47° 1 54° 2 62° 1 62° 5	39°6 41°4 45°2 54°6 56°2 61°3	38°9 39°5 43°3 54°7 56°6 60°1	38°5 47°3 44°4 53°4 55°7	37°5 47°7 43°5 52°6 55°4	36°9 45°0 43°4 52°4 50°4	37°0 41°0 43°5 51°2 49°3	36°8 39°1 41°0 50°4 48°3	37°1 41°0 39°7 47°6 47°5	42.74 47.41 52.31 53.36 60.50
53.6 53.4 51.8 51.2 52.1 39.6	51.4 52.9 52.2 50.8 48.5 40.6	49.7 50.6 51.0 49.8 44.5 41.2	49.5 49.3 49.6 48.9 41.2 41.5	51.2 48.9 48.6 48.1 40.6 42.1	52.6 47.5 48.7 47.1 38.7 41.9	46:1 51:7 44:9 48:2 46:0 37:7	40°4 46°3 42°8 47°4 45°8 33°5	39.6 44.2 45.4 47.1 44.0 33.9	37°1 41°4 45°6 46°5 43°2 35°3	38.7 40.6 45.7 46.4 42.1 31.8	39·3 } 41·5 44·3 46·4 41·7 33·7	58.71 50.63 52.11 50.45 47.84 44.96 40.51
47.7 55.6 59.2 69.7 66.5 66.6	47°1 53°0 56°2 65°0 60°9 65°9	45.5 50.1 54.4 60.2 56.5 62.9	45.7 51.9 51.6 57.5 57.9 56.5	45.1 48.5 49.5 56.3 58.8 57.5	46'1 47'3 48'3 52'6 58'4 59'3	42·3 46·5 45·0 49·3 51·5 57·5	38.7 46.9 42.2 47.3 50.1 57.0	36°3 46°9 39°1 46°9 49°7 57°0	33.6 46.9 39.0 45.0 49.7 56.5 ——————————————————————————————————	34·1 46·7 37·4 44·4 49·7 55·4 ——————————————————————————————————	34.5 $47.2$ $38.9$ $44.2$ $51.0$ $56.2$ $ 58.3$	49°17 51°22 54°23 60°80 62°42 63°43
59.1 58.8 65.3 69.9 64.4 66.3	56°5 57°0 63°5 65°9 60°3 62°1	53.6 56.9 60.5 62.3 55.0 55.8	53°3 57°7 57°5 56°9 53°4 52°7	53.8 58.2 57.1 55.8 52.0 52.5	54.7 57.5 56.3 55.2 49.9 53.0	59.7 52.3 55.5 56.2 53.1 49.1	59°2 54°1 54°8 52°8 52°4 48°7	59°1 54°0 55°9 52°2 50°6 47°1 — 54°4	58 9 53 6 55 6 51 0 48 1 47 8	58 6 54 8 56 3 50 6 47 5 47 0	55.8 53.6 46.4 47.0 	57°19 56°63 60°94 61°54 56°48 58°66
75.9 54.0 55.6	71:3 52:0 55:0	67.9 49.4 49.5	62.7 49.0 47.5	59.5 49.3 44.1	56.6 48.9 45.3	56.3 54.5 46.7 46.3	54.0 54.2 43.7 43.0	53.4 45.3 41.2	51.4 44.8 40.3	49.5 42.6 39.5	48·1 42·0 40·4 45·62	63°35 54°57 48°70 54°10
58.02	55*85	53.50	51.91	50.96	50.33	49.47	47.85	47.09	46.51	45.21	45 62	54 10
59.8 66.9 67.3 56.8 54.6 61.9 59.3 68.0 70.5 55.2 59.1 65.0 87.6 87.6 74.9 70.8 64.1 69.8 63.3 67.5 70.3 73.2 71.4 70.3 70.9	59·1 64·6 64·1	51'2 62'1 62'7	47.1 59.7 60.9	47:3 60:8 59:5	47.0 63.1 57.3 	44.6 61.7 61.5 50.1 43.8 52.0 54.3 63.3 49.7 41.0 45.5 52.5 69.3 66.8 	45.0 60.8 	43.8 58.4	44.5 59.4 — 60.3 45.0 41.0 48.9 49.3 58.1 — 45.3 42.2 41.0 48.3 70.5 61.3 — 63.9 60.1 52.6 59.5 56.4 — 56.3 56.5 65.7 55.2 50.4	42.8 61.1 -4.4 44.9 41.4 48.1 48.0 57.3 -44.1 42.4 40.9 51.4 70.7 59.5 -61.3 59.9 54.6 61.1 55.5 56.5 66.3 54.0 52.4	42.6 63.7	52.68 62.85 64.18 56.63 50.04 55.08 58.25 65.43 61.98 49.64 52.47 55.89 77.66 75.47 71.68 68.22 63.82 61.97 63.93 64.03 64.04 69.76 70.27 65.74 64.53
67.77	71·7 65·54	$\frac{70.1}{62.45}$	$\frac{70.3}{60.23}$	68·7 58·72	57.69	64.9 56.73	63.1	$\frac{62.3}{54.95}$	$\frac{61.5}{54.07}$	53.68	53.3	68.72
	01											

						WET T	HERMOMI	ETER.					,
Iours o Göttir Tim	f Mean	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	° 26°1 36°4 28°8	27.3 37.3 28.9	27.7 37.5 29.3	29.4 36.6 29.3	30.8 38.6 30.4	31.7 36.9 32.1	30·1 35·8 31·9	29.9 36.2 32.2	30.7 35.8 32.2	32·2 35·4 33·0	32.6 34.8 33.7	33.8 34.8 32.0
	4 5 6 7 8 9	27.7 25.9 34.2 33.0 27.6 27.7	27.5 29.6 34.6 32.6 27.4 28.7	27.1 30.3 34.8 32.3 26.5 28.7	29.5 31.4 35.5 32.4 26.7 29.2	31.6 32.0 35.9 32.2 25.7 29.2	31.0 32.2 36.1 32.0 25.9 28.8	32:3 33:5 36:2 31:3 25:2 29:2	33.4 33.0 36.1 31.4 26.5 30.4	33.0 33.0 36.1 32.3 27.5 31.0	33.4 32.4 36.5 31.5 28.1 29.3	33.5 31.7 35.6 31.8 28.8 28.0	32.0 32.0 34.7 31.5 29.4 27.9
JANUARY.	11 12 13 14 15 16 17	23.9 9.1 26.3 17.8 29.2 10.1	23.6 9.1 26.3 24.1 29.4 9.5	23.7 11.1 26.7 27.9 29.3 8.0	23.0 12.4 27.9 30.8 29.7 7.2	22.4 16.9 28.5 32.0 29.7 8.6	23°0 18°7 30°6 32°1 29°2 8°7	24·3 20·7 30·9 34·5 27·9 8·8	24.1 21.0 31.5 36.2 26.3 8.7	24·1 21·6 31·6 36·5 25·9 8·9	23·2 21·5 32·4 37·2 24·5 10·2	22.0 20.9 32.0 36.2 23.9 8.5	21.6 19.5 29.9 36.2 23.6 7.0
JA	18 19 20 21 22 23 24	5:5 8:7 21:1 - 1:3 5:8 18:8	$ \begin{array}{r}     \hline       4.7 \\       8.8 \\       21.4 \\       - 2.1 \\       5.3 \\       17.8 \end{array} $	4.5 8.8 21.5 - 1.3 4.5 19.4	7.4 10.4 21.4 2.8 9.0 21.1	9'3 14'0 21'1 5'4 12'8 24'0	12.1 14.3 21.8 8.8 16.3 26.5	12.6 16.6 21.8 12.2 18.0 29.2	12.6 19.0 22.8 15.6 17.8 29.8	13.4 20.5 24.1 16.1 19.4 31.4	14.1 21.5 24.6 16.6 19.9 32.2	14.6 21.4 24.8 16.2 20.8 32.3	13'1 21'1 24'1 14'8 19'7 32'2
Feb	25 26 27 28 29 30 31	33·7 17·1 29·8 32·5 37·2 16·4	34·1 14·9 30·8 32·5 37·2 13·9	34·4 14·4 31·2 33·0 36·2 12·4	35°3 15°9 31°5 33°3 37°7 10°7	38·1 16·9 32·1 33·3 38·7 10·7	38 · 1 18 · 5 33 · 9 34 · 0 38 · 5 13 · 2	36.9 20.5 34.1 34.9 39.2 14.3	37.1 21.1 34.3 34.3 40.6 14.3	37·2 21·4 34·8 34·2 40·5 16·8	37.2 21.9 34.4 34.3 40.2 17.7	36°3 21°6 34°6 34°5 40°3 16°3	34.6 21.1 33.4 34.5 39.9 16.2
Hourly	Means	22.26	22.78	22.96	23.98	25.19	26.11	26.77	27:27	27.78	27.98	27.69	27.06
ARY.	$\begin{pmatrix} 2\\ 3\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 10\\ 11\\ 12\\ 13\\ 14\\ \end{pmatrix}$	18'3 29'3 28'2 31'6 22'8 24'9 — 15'0 2'5 20'8 — 3'4 23'2 15'1	20°6 30°5 25°3 32°5 23°5 24°5 — 11°3 3°5 22°6 — 23°6 18°3	20°5 31°6 26°1 33°0 25°9 24°4 — 10°6 4°1 19°2 — 25°2 20°9	22·2 34·3 26·4 34·9 27·5 31·8 — 10·0 8·5 17·8 — 27·3 23·2	24.5 35.1 28.1 34.5 32.0 34.4 — 10.1 12.4 18.3 — 28.4 26.5	26'1 36'2 29'6 32'5 32'2 37'1 10'0 14'9 17'4 12'0 28'8 30'4	27.5 37.2 30.7 32.4 35.3 37.1 — 10.7 20.3 17.7 16.0 29.6 31.7	27'9 37'9 31'4 33'3 35'0 36'9 — 11'2 20'3 17'8 17'7 30'0 31'6	27'8 38'7 32'0 32'9 35'2 36'4 12'6 20'6 18'7 20'7 31'0 31'6	27.6 38.1 32.0 32.2 35.4 35.2 — 11.8 22.0 18.0 20.5 31.5 31.9	27'9 37'2 31'8 32'0 34'9 36'2	27.9 36.2 31.6 30.6 34.0 35.8 
FEBRUARY.	15 16 17 18 19 20 21 22	20°1 18°0 10°7 6°6 24°1 24°3	20.4 18.7 10.5 10.7 24.3 24.9	20.8 19.9 14.7 10.7 24.9 26.1	21 · 1 23 · 0 16 · 0 17 · 7 25 · 7 26 · 7	24'1 25'3 21'5 24'3 25'9 27'9	25°1 27°4 21°3 24°3 26°0 28°3	24.8 28.8 22.4 25.9 25.6 29.5	25°2 28°5 23°5 25°3 26°4 28°8	25°1 28°4 23°7 25°3 27°4 27°1	24.8 29.7 24.6 24.3 29.8 27.9	24.5 28.4 24.3 24.6 28.8 25.9	23.6 26.4 23.5 25.9 27.3 24.9
Marc	23 24 25 26 27 28	12.0 11.2 - 0.9 - 10.3 -	14.6 10.2 1.4 — 10.6 —	15.6 12.1 3.2 — 11.1	20°2 14°8 7°6 — 1°4 13°9	21.8 16.8 10.2 	22.2 17.2 14.0 2.8 10.2 17.2	23 · 2 21 · 3 15 · 1 4 · 4 12 · 9 17 · 4	22.7 22.0 14.6 5.5 14.0 17.0	23°1 18°7 15°4 6°9 14°4 16°9	23°1 18°3 15°6 6°0 13°8 17°4	21.9 16.8 14.2 4.5 13.5 17.5	18.5 14.8 13.2 3.4 11.5 17.2
Hourl	y Means	16.28	18.51	19.08	20.55	22.82	22.63	24.06	24.35	24.61	24.65	24.53	23.36

					WET	THERMO	METER.					
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
34.0 34.8	34.4 33.0	34.6 32.0	34.8 31.5	° 34.8 30.4	° 34.5	° 34.7 27.9	35.0 26.6	35.4 26.5	35.6 27.1	36.2 26.6	36°2 27°3	32.60 32.92
31.5	30.6	30.3	29.9	29·7  28·3	28.8 — 27.5	32·4 27·1	32.5 25.3	$\begin{bmatrix} -32.6 \\ 23.9 \end{bmatrix}$	31.0 23.9	30.9 23.0	$\begin{bmatrix} -26.2 \\ 25.7 \end{bmatrix}$	30.84 28.72
32.5 34.4 32.0 30.1 28.1	33.0 34.3 30.7 29.7 27.9	33.4 35.1 29.8 28.8 28.8	32.8 34.8 29.5 28.2 29.6	32.5 34.5 29.6 26.8 30.0	32.5 34.8 29.6 27.3 29.2	32.8 34.6 28.6 27.3	33.0 35.1 28.7 27.9	33·3 34·9 28·1 27·8	34·3 34·3 28·0 28·2	34 · 2 33 · 1 27 · 7 29 · 3	33.4 33.0 27.6 29.2	32.28 34.97 30.59 27.75 28.01
20.5 18.3 29.5 36.6	19°9 15°4 24°9 35°9	19.6 20.4 24.3 36.6	18.7 20.9 28.3 35.4	16°3 21°1 27°5 36°2	15.6 21.3 27.3 35.2 17.9	26.3 14.2 22.8 24.6 34.9 17.2	25.5 13.8 23.0 19.9 34.6 15.9	25 1 13 1 23 8 21 5 32 6 14 4	24.6 12.7 24.9 19.4 31.6 14.4	24.5 11.5 25.4 19.0 31.0 12.4	$\begin{bmatrix} -24.5 \\ 10.0 \\ 27.2 \\ 18.8 \\ 29.5 \\ 11.5 \end{bmatrix}$	19°37 19°46 26°65 32°98 22°48
22.8 6.3 — 11.1	22.6 6.8 - 9.8	21.7 6.3 — 9.2	20.6 6.4	19.5 5.4 7.1	$\frac{3.5}{6.0}$	9·3 5·3	7.7 5.3 21.1	7·1 6·3 21·1	6.4 6.4 21.1	6·1 7·1 21·4	$\frac{-5.6}{5.6}$	7.53 8.91 18.50
21'1 22'5 13'7 19'1 31'2	21.7 21.0 13.0 17.9 29.6	21.7 18.8 12.6 17.0 29.8	22.2 16.8 12.3 15.9 30.5	22.9 13.2 12.1 15.0 30.5	22.9 11.5 12.0 14.1 31.5	20.9 8.8 8.9 13.0	6.2 11.4 11.1	3.7 7.6 11.1	1 · 2 6 · 0 15 · 4	0.8 3.9 15.7	$   \begin{bmatrix}     -0.9 \\     2.2 \\     16.0 \\     \hline     -33.4   \end{bmatrix} $	16:42 9:15 14:61 28:67
33.3 20.9 33.3 35.1 39.7	32.5 23.8 32.5 35.6 39.4	31.8 26.0 32.6 35.6 40.7	30°3 25°5 33°2 36°1 39°6	29.8 26.7 32.9 36.2 37.2	28.5 27.6 32.4 36.2 35.6	32.1 27.6 27.7 31.6 35.9 34.4	31·2 27·4 27·5 31·0 37·1 30·5	30.9 25.3 27.6 31.0 36.0 27.8	30.8 21.8 27.7 31.2 36.7 24.3	31.9 19.8 28.2 31.4 36.1 20.6	33.4 } 17.8 29.6 32.0 36.7 18.6	31.62 22.67 32.50 34.94 35.61
14.8	13.2	12.8	11.2 —	10.6	— 8.8	16.4	16.9	14.8	15.5	14.8	16.0}	14.13
26.24	25.81	25.83	25.63	25.07	24.53	24.35	23.75	23.09	22.75	22.32	22.07	25.00
27.9 34.4 32.2 30.5 32.7 34.4	28.6 33.8 33.0 29.4 32.0 29.4	28.7 33.1 33.4 29.2 31.8 25.3	30.4 32.7 33.7 30.0 32.0 20.6	30.6 32.2 34.2 28.6 32.5 18.0	30.5 32.0 34.7 28.4 30.5 15.9	29°5 30°3 33°7 28°3 29°5	30°0 31°4 33°0 26°6 27°9	30°3 28°8 32°8 26°5 26°8	30.8 29.2 32.2 26.3 25.7	31.0 27.7 32.0 25.9 25.9	29.8 27.4 31.5 24.2 24.7	27:37 33:14 31:23 30:26 30:24 27:45
9·2 23·3 16·5 18·0 28·3	8·2 23·9 15·2 17·9 28·9	7:1 25:3 13:9 17:3 29:8	6.8 24.5 12.9 17.3 28.8	6:5 25:3 12:6 17:1 28:6	6'2 26'3 11'6 18'5 24'4	20°3 4°3 25°8 10°2 18°8 19°2	20.2 4.1 24.6 10.3 20.8 16.3	20.1 4.1 22.0 10.3 21.3 13.5	20.1 3.4 21.5 2.8 21.8 13.3	20°1 2°9 20°8 	$ \begin{array}{c} 19.6 \\ 2.5 \\ 21.1 \\ -2.9 \\ 23.2 \\ 14.8 \\ \end{array} $	8:40 19:12 13:89 17:87 25:22
30°3 22°4 24°5 16°7 25°9 26°3	29'4 	27.5 — 22.2 22.6 10.3 24.7 23.0	27.5 	27.2  20.9 21.7 10.3 25.5 25.7	26.8 — 19.8 20.0 9.9 25.3 25.7	17.7 17.9 20.0 8.2 25.4 24.5	18.9 17.7 18.8 6.2 24.9 24.9	19.8 19.2 16.8 6.8 23.7 24.7	20.5 19.5 9.9 5.2 23.8 25.4	20.5 19.9 5.9 5.0 23.7 25.7		25.39 21.77 21.31 14.32 22.68 25.75
24'1 18'7 12'8 11'4 1'4	23.9 — 17.5 9.5 8.8 — 1.4	22.2 15.9 8.0 6.9 - 1.7	21.7 15.0 6.4 4.1	19.2  15.7 4.6 4.8	18.1 — 13.8 2.3 4.1 —	16.4 12.2 3.7 - 1.5	16.7 12.8 5.4 —	15.6 12.9 3.5 —	15.2 11.4 1.6	14.6 10.7 - 0.9 -	$\begin{bmatrix} - \\ 12.7 \\ 11.6 \\ -0.9 \\ - \end{bmatrix}$	16.96 10.43 8.54 3.18
11.4	11.8 12.4	10.5 14.6	10.5 14.3 —	10.0 14.2	10°3 13°5 —	10.3 - 12.9	13.8  10.3	10.6 - 13.2	10.6	10.7  12.7	$\frac{11.2}{10.3}$	10.67 14.60
22.04	21.11	20.07	20.55	20.26	19.21	18.29	18.90	18.35	17.43	16.74	16:30	20.70

						WET TH	HERMOME	TER.	T				
Hours o Götti Tir	f Mean ngen ne.	0	1	2	3	4	5	6	7	8	9	10	11
Tore	of Mean onto me.	18	19	20	21	22	23	0	1	2	3	4	5
	2 3 4 5 6 7 8	0 11.4 8.5 12.9 29.7 27.1 8.8	3:5 9:1 17:8 28:8 27:7 12:8	° 16.9 12.4 24.3 30.5 28.4 17.1	20.7 21.3 30.3 32.0 29.4 23.7	23.0 24.5 31.6 33.9 27.5 26.4	21.8 26.3 32.2 34.1 27.3 27.8	22.7 26.6 34.7 34.3 27.9 28.6	22:3 27:1 34:8 34:9 27:6 28:3	24.9 27.7 35.4 36.0 27.9 28.8	24.5 27.9 34.9 37.0 27.3 30.3	23.7 27.4 34.5 36.4 27.5 30.0	23.0 26.8 34.7 39.0 26.6 29.7
<b>H</b>	9 10 11 12 13 14	31.0 27.3 25.1 31.8 38.1 35.2	30.7 28.3 24.4 34.5 38.6 35.8	31.2 32.4 30.8 35.8 37.9 37.6	32.4 34.9 — 37.4 39.5 37.5	33.9 35.4 36.2 39.0 40.3 37.4	33.8 35.8 35.8 35.8 39.1 41.1 38.1	34·3 35·6 36·2 39·4 41·9 37·0	34·2 34·9 36·2 41·2 42·1 37·1	33°1 35°8 35°8 40°4 42°9 36°4	33.7 35.8 36.2 39.1 43.5 35.8	34·1 35·0 35·3 39·1 44·7 34·2	33.7 34.1 36.0 39.0 43.4 32.9
MARCH	15 16 17 18 19 20 21	27.5 23.7 21.1 33.2 26.8 29.8	27.3 24.0 23.4 33.9 29.6 29.3	26°3 24°5 24°9 33°5 35°6 29°5	27.5 24.9 28.2 37.2 37.5 28.6	26°1 25°4 32°0 36°9 38°5 30°5	26.8 25.9 32.4 39.4 40.8 29.6	25.9 27.9 33.9 39.4 40.8 29.7	26.8 29.4 34.9 41.9 40.5 30.8	28.8 30.5 35.4 40.2 42.8 32.0	30.0 31.5 34.9 39.6 42.3 33.0	31.0 31.3 35.6 36.0 40.3 32.2	32.0 30.8 34.3 36.1 39.0 32.7
	22 23 24 25 26 27 28 29	32.0 38.1 38.1 34.7 34.9 33.5	33·3 38·4 38·3 34·6 36·0 33·4	34.6 38.7 38.5 36.0 36.9 34.7	35.8 39.1 39.0 39.6 37.3 35.4	36.7 39.1 39.4 40.4 40.4 35.8	37.4 38.4 40.2 41.1 39.7 37.7	38.1 38.4 40.5 41.6 40.4 36.7	38°1 38°5 41°8 40°7 39°9 36°3	38·3 39·0 40·5 41·9 40·8 36·7	36.8 39.6 40.5 40.3 38.7 35.8	37.0 38.4 39.6 37.7 38.5 35.2	36.7 39.0 39.0 36.5 36.5 33.9
	$\begin{bmatrix} 30 \\ 31 \end{bmatrix}$	30°5 27°9	31.7 31.0	32.0 32.0	30.0	32.6 35.3	$\frac{32.7}{38.0}$	33.9 37.3	36.0 37.3	35.8 37.5	35.3 37.9	34.9 38.1	34.7 39.4
Hourly	Means	28.75	29.85	31.40	33.89	35.13	35.73	36.12	36.24	37.02	36.89	36.31	35.98
	1 2 3 4 5 6 7 8	27·3 27·7 28·5 31·6 — 39·6 42·1 29·6 23·5	30.0 30.5 32.2 34.3 — 39.2 43.4 29.6 30.8	31.7 33.9 33.9 36.7 — 39.4 44.7 31.7 32.2	33.7 34.1 34.4 38.4 	35:4 34:2 36:1 38:9 	35.4 36.5 37.2 40.3 — 46.4 49.4 34.1 37.5	36'3 36'1 38'7 40'8	36.7 35.4 37.2 41.0  47.5 48.7 33.5 39.9	37.2 35.3 37.4 42.1 	35.8 35.6 36.5 41.8 	36.2 34.5 36.3 42.6 — 47.3 51.5 34.5 37.0	35.8 34.3 35.8 41.4 
APRIL.	10 a 11 12 13 14 15 16 17	38°3 25°9 27°6 28°4 26°5 31°7 46°4	38°3	40.7 26.6 34.5 27.9 32.7 41.7 48.5		50.0 	51·1 30·3 39·0 33·5 38·3 47·2 48·2	49.1 	45·3  32·0 38·7 34·5 39·2 48·5 50·9	40.9 32.4 38.7 39.4 39.7 47.5 50.1	32·2 38·2 35·2 40·0 48·4 51·4	38·7  32·9 38·3 35·8 37·1 48·7 51·2	36.0 31.4 38.5 36.2 35.6 48.1 51.7
	19 20 21 22 - 23 24 25 26	30.0 40.3 41.4 47.2 48.2 39.4	37°0 47°7 42°3 49°3 49°2 39°6	41 '4 50 '7 42 '5 50 '7 49 '2 39 '4	42.7 53.2 43.1 46.5 49.2 37.2	45 '4 55 '4 43 '3 48 '2 50 '0 37 '2	47.6 57.3 43.4 48.7 51.2 38.3	49.7 58.3 44.7 49.7 51.4 37.4	51·1 58·5 46·9 50·4 54·4 38·1	52·2 59·4 47·3 50·3 52·4 40·1	51 · 9 58 · 3 46 · 7 50 · 4 54 · 1 38 · 7	51'4 56'6 47'7 49'1 55'1 38'2	50°1 54°9 45°5 51°2 55°5 38°5
	27 28 29 30	37°1 40°3 44°6 47°7	41°9 43°8 44°6 48°5	42.5 44.4 44.6 49.4	46.5 44.2 46.4 48.1	47.2 44.1 47.4 48.0	47.0 45.0 47.1 50.7	46.9 45.3 48.2 52.3	46°5 46°2 47°2 53°7	46.5 48.3 46.8 55.3	47·1 49·4 47·2 52·5	48°3 50°5 46°7 53°4	48.3 49.7 48.1 52.7
Hourl	y Means	35.64	38.24	39.66	41.17	42.28	43*23	43.61	44.08	44.37	44.01	43.98	43.37

					WET	THERMO	METER.					
12	13	14	15	16	17	18 -	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
0 19.5 24.4 35.1 35.8 23.2	° 14.6 21.5 35.1 33.2 19.6	° 14.0 18.0 34.6 32.3 16.1	° 11.5 16.7 33.7 26.3 14.7	° 11.4 16.9 33.7 27.3 12.1	8'4 16'4 33'1 25'4 12'3	7.8 20.9 30.3 23.6 9.8	7.4 20.1 32.8 25.6 10.1	7.7 19.9 31.6 26.1 9.0	9·2 17·7 31·3 27·7 8·6	7:1 15:6 32:4 28:4 9:0	9 · 2 14 · 5 31 · 0 28 · 2 8 · 3	15.68 20.34 31.37 31.10 20.21
29.4	29.4	29.4	30.1	29.8	29.0	31.7	32.2	31.7	30.8	<b>3</b> 0.2	30.8	27.38
32.9 32.0 34.5 39.0 40.9 32.0	29.6 27.9 32.8 39.0 39.4 30.0	27.7 26.3 31.8 37.7 37.4 29.3	29.5 26.3 31.6 38.5 37.2 28.8	30.6 25.7 31.8 39.9 36.9 28.6	31.0 25.2 31.6 40.1 36.9 28.6	31.7 24.5 30.8 39.7 37.2	31.9 25.3 30.3 39.7 36.1	31.8 25.6 29.7 40.2 35.3	31.0 25.9 29.6 40.3 35.3	30.6 25.1 30.4 38.4 34.8	24.6 30.6 38.1 36.0	31 '90 29 '98 32 '30 38 '60 39 '05
28·4 31·0 32·4 35·3 37·3 31·7	26.4 26.8 30.7 33.7 36.5	25 °9 25 °6 29 °5 32 °1 37 °5 28 °8	24.6 24.5 30.5 31.4 36.7 26.3	23.5 23.3 30.4 29.5 36.4 24.9	23·2 22·4 29·6 28·4 34·5 25·4	30°8 23°9 21°1 29°4 28°4 33°3	31.0 23.9 20.5 31.5 29.6 32.7	28.4 23.5 19.8 31.0 29.6 32.4	29 · 4 23 · 0 18 · 7 32 · 0 28 · 3 31 · 2	29.8 22.6 19.4 32.0 28.1 30.8	28.6 23.7 19.4 32.8 28.6 30.6	26.19 25.09 30.95 33.76 36.02
35.8 39.0 39.0 36.9 37.1 33.6	30.7 36.5 38.9 38.9 36.1 36.9 33.3	34.5 40.0 39.2 35.8 36.8 32.6	36.6 40.4 37.3 35.3 36.3 32.8	37.1 40.0 36.7 35.3 35.6 32.6	37.7 39.0 36.3 35.5 36.2 32.6	31.8 38.1 38.3 35.8 35.4 35.8	31.6 38.1 38.0 35.5 35.4 34.6	31.6 38.2 37.4 35.2 35.5 34.2	32.0 38.1 37.5 34.7 35.3 33.4	31.6 38.0 37.9 34.4 35.1 33.4		30°23 36°73 38°70 38°03 37°14 36°82 33°20
33.9 36.2	33 · 1 32 · 7	31.8 32.3	29.8 30.2	28·2 29·4	28·1 27·9	28.3 32.0 27.3	29°3 30°9 26°1	29·2 31·0 25·9	28.6 31.0 26.4	29.5 30.0 26.6	$     \begin{bmatrix}       -29 \cdot 4 \\       29 \cdot 3 \\       26 \cdot 6     \end{bmatrix} $	32.05 32.24
34.66	32.93	31.88	31.15	30.40	30.19	30.31	30.41	30.06	29.88	29.66	29.60	32.72
35·1 32·9 35·7 39·7 	29.8 29.5 30.7 38.8 — 45.8 48.9 31.0 32.5 — 33.4 — 30.8 37.1 32.6 36.9	28·3 27·8 29·4 38·1 —— 45·6 48·2 30·0 33·8 —— 26·6 36·2 29·6 36·5	26.6 28.2 29.2 37.9 	26.3 27.6 30.6 37.6 - 45.2 44.6 27.2 31.4 - 32.0 - 25.5 35.2 26.8 36.5	26.5 26.6 31.6 37.4 	26.4 27.0 32.4 	25.9 27.3 30.7 	25·1 27·1 29·3 - 45·4 43·3 36·0 24·7 - 38·9 - 25·4 25·9 28·5 25·9	24.9 27.5 27.9 45.5 42.3 33.3 24.5 — 25.6 27.1 28.8 25.4 36.2	24.6 27.4 30.5 	25°3 26°4 30°5 40°8 40°9 31°4 23°5	44.17 44.28 29.81 35.79 36.11 28.56 34.86 30.43 36.14
47.9 47.4 	46.9 46.2 	45.2 45.5 	42.5 45.8 47.7 50.1 42.5 48.1 45.8 38.5 - 39.2 43.5	41'0 42'9 46'2 50'1 42'6 48'7 47'4 38'8 - 38'5 43'1	40.9 39.4 42.9 50.1 43.5 49.0 48.5 38.6 — 38.5 42.9	39.6 31.0 42.4 49.3 44.7 47.7 48.3 35.4 38.5 43.5	38.5 31.4 43.4 49.1 45.1 47.4 49.4 	30.7 41.8 49.3 44.4 46.9 49.4 - 35.3 36.7 47.0	29.6 40.9 43.6 44.4 46.5 48.9 - 35.1 36.0 47.4	28 · 8 41 · 4 41 · 8 46 · 5 46 · 2 47 · 2 — 34 · 9 34 · 9 47 · 1	47.1 28.4 41.6 41.2 45.8 48.5 41.6 34.5 34.4 46.4	43.87 43.25 45.15 51.30 44.29 48.65 49.73 37.70 42.15 46.69
48·1 52·4 42·46	48.1 51.0 40.73	$   \begin{array}{r}     47.2 \\     50.1 \\     \hline     39.53   \end{array} $	46.7 49.7 38.93	46.3 50.1 38.49	46°1 49°7 38°16	45.8 49.7 37.82	46°3 49°6 38°11	46.0 50.3 37.23	46.5 49.9 36.68	46.5 50.9 36.54	47.0 50.4 36.09	46.69 50.67 40.19

						WET T	HERMOMI	ETER.					
Hours o Göttir Tim	of Mean	0	1	2	3	4	5	6	7	8	9	10	11
Hours o Toro Tim		18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$	51°3 49°6	51.7 50.7	$\begin{bmatrix} 5\overset{\circ}{2} \cdot 2 \\ 52 \cdot 4 \end{bmatrix}$	51.7 53.4	52·2 56·3	52·3 56·8	$\begin{bmatrix} 5\overset{\circ}{2} \cdot 4 \\ 54 \cdot 6 \end{bmatrix}$	52.7 55.5	52°5 55°5	51.4 55.1	51.4 55.1	52·3 54·4
	4 5 6 7 8 9	40°3 44°0 51°5 41°8 49°7 54°0	48.5 47.7 49.4 44.2 52.7 54.3	53.8 52.0 48.4 44.7 53.8 55.0	53.8 55.0 48.6 45.6 55.0 54.3	55.5 51.7 47.1 47.1 54.8 54.1	54.4 50.3 46.4 49.3 55.6 53.9	56'1 53'6 45'3 51'1 55'3 54'3	54.8 55.5 45.6 52.0 56.1 55.2	55°5 58°0 45°2 50°9 56°0 55°2	55.6 58.8 47.2 51.2 53.7 55.2	57.1 58.0 46.9 52.3 53.6 55.8	53.8 56.0 47.4 52.3 53.5 56.0
MAY.	10 11 12 13 14 15 16	31.2 39.2 41.8 53.6 50.2 44.8	30.9 41.2 44.6 56.9 49.9 47.5	30.9 42.7 45.8 58.3 48.9 51.9	32.4 45.5 51.7 60.9 50.3 55.4	33°3 46°2 54°8 61°5 52°0 55°8	35°1 47°7 56°9 59°4 51°9 57°7	36.5 52.7 57.7 59.7 54.0 57.1	35.4 52.2 57.6 60.2 57.9 <b>5</b> 7.6	37.5 53.3 58.8 60.4 55.6 57.0	39.7 53.1 59.0 58.0 57.9 56.4	39.1 53.7 59.0 61.6 59.4 57.3	39.0 54.2 59.7 59.1 57.2 55.5
M	17 18 19 20 21 22 23	51'9 36'0 40'3 37'7 39'2 49'0	51'3 38'0 43'3 38'5 42'9 52'5	48.5 39.2 45.6 40.6 44.5 54.6	48.9 39.4 48.2 41.2 47.9 56.8	48.4 41.7 49.9 41.9 49.0 59.5	47.2 45.0 50.7 42.1 50.5 59.0	46.9 44.6 50.9 43.3 48.3 63.1	43.0 45.8 50.4 43.4 48.7 64.1	43.5 46.9 53.4 44.6 48.5 64.2	43.9 48.1 50.9 45.0 46.7 61.9	43°1 49°1 50°5 44°6 46°7 61°3	41.6 48.1 49.9 43.8 48.1 60.5
	24 25 26 27 28 29 30 31	59.9 63.3 64.1 57.9 54.9 58.3	 62.9 64.1 67.6 60.2 58.7 57.3	65°3 67°2 67°7 61°3 60°2 59°7	66.8 68.4 66.9 63.1 62.6 61.6	67.2 67.7 66.2 66.1 65.1 67.4	66.2 67.6 66.7 64.0 62.9 68.4	68.5 69.4 66.3 65.9 64.4 69.1	69.0 71.9 65.5 67.6 64.1 69.3	70°0 70°3 65°5 66°1 64°1 68°1	68°1 69°2 65°3 63°8 63°5 67°7	66.8 67.9 65.9 63.1 62.5 67.0	67.7 67.9 67.7 63.1 59.7 67.1
Hourly	y Means	48.29	50.59	51.74	53.58	54.33	54.24	55.43	55.81	56.02	55.63	55.72	55.52
	1 2 3 4 5 6	58.8 62.5 55.2 59.7 52.9 42.5	62·1 61·9 57·5 62·7 52·4 45·8	62.8 63.4 58.7 62.2 52.7 47.7	61.9 65.9 61.4 62.5 53.0 48.9	61.4 64.5 61.2 63.0 52.9 49.7	63.7 64.5 62.3 62.3 52.5 49.8	66.1 60.2 59.2 64.3 53.1 50.3	66.6 62.7 59.0 65.4 54.2 49.4	66.6 62.7 59.9 62.9 54.6 50.7	65.9 62.5 62.8 58.3 58.5 50.0	67.4 61.2 62.7 58.5 55.9 50.5	68.5 61.3 64.7 60.0 56.4 47.9
Б.	7 8 9 10 11 12 13	46.1 46.4 50.3 53.9 46.3 54.8	48.7 50.5 53.7 58.0 47.2 57.4	54.2 55.0 58.7 59.6 48.2 57.5	55°2 49°8 57°1 62°5 50°5 59°4	55.5 60.2 59.5 63.5 54.3 59.9	57.8 58.5 63.8 62.6 53.0 59.7	57.8 58.3 65.7 60.9 52.7 58.8	58°3 59°1 65°9 59°1 52°9 57°9	57.5 60.0 65.7 59.8 53.2 59.7	57'9 61'1 67'2 61'5 53'3 58'7	59.4 61.5 66.8 61.9 54.3 56.6	59.5 59.0 64.9 63.5 64.2 55.5
JUNE.	14 15 16 17 18 19 20	58.7 56.3 53.2 60.2 66.4 55.5	60°2 57°7 57°7 61°8 67°4 55°7	61 · 1 58 · 9 60 · 9 62 · 1 66 · 7 55 · 7	64.7 60.4 64.1 66.8 67.9 56.2	68.4 61.6 64.5 70.2 68.8 56.9	67.7 60.2 64.9 70.1 72.1 56.0	69.4 62.6 67.2 71.3 72.1 55.4	68.4 62.8 68.1 73.2 70.2 55.2	68.2 62.7 68.1 70.8 69.1 55.0	65°9 62°8 69°1 67°7 66°5 54°2	67.9 63.9 69.1 74.0 65.1 53.6	64.9 63.9 67.5 72.4 66.9 53.4
	21 22 23 24 25 26 27 28	50°2 51°4 53°4 55°3 57°5 60°4	50.7 54.3 58.4 56.4 58.0 64.6	52.9 55.3 56.9 60.0 60.6 63.1	53°5 57°0 57°8 62°4 61°5 62°9	55°3 59°1 59°3 61°8 64°3 62°9	54.6 59.3 59.7 63.5 65.4 64.9	55°0 57°5 59°7 63°7 65°1 65°4	54.8 59.9 60.8 65.4 64.8 64.9	53°5 60°4 59°9 69°1 66°9 62°2	54.6 59.9 63.6 68.1 66.9 62.1	54.9 60.1 58.9 67.9 67.9	54.4 58.1 61.3 67.8 67.0 63.4
	$\begin{vmatrix} 26 \\ 29 \\ 30 \end{vmatrix}$	64°1 65°6	63°8 67°2	64°7 68°1	65.7 69.1	68°3 70°1	68.7 69.8	68.9 69.5	69.1 69.2	69°2 70°3	69.9 68.3	68.8 68.8	69·2 69·5
Hourly	Means	55.59	57:38	58.76	59.93	61.43	61.81	61.93	62.50	62:26	62.20	62:39	62.20

6 7 8 9 10 11 12 13 14 15 16 17 Modella Means 1	1						WET	THERMO	METER.					
Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sect	t	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
\$5.6   \$5.7   \$4.9   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7   \$4.7		6	7	8	9	10	11	12	13	14	15	16	17	Means.
\$\frac{1}{45\cong 5}\$ \frac{1}{65\cong 7}\$ \frac{1}{47\cong 4}\$ \frac{1}{47\cong 8}\$ \frac{1}{47\cong 7}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}{47\cong 6}\$ \frac{1}		52°·1 55°·6	5 ¹ .7 52.7										1	51°72 49°41
39'4   39'4   36'2   37'3   36'5   36'3   36'2   37'2   37'2   37'1   39'0   36'2   39'0   36'2   39'0   36'3   36'5   37'5   39'0   36'6   44'9   39'9   55'2   66'0   66'0   66'9   65'9   65'5   66'1   65'6   60'6   60'4   60'7   56'2   56'1   51'3   58'0   58'0   56'4   56'9   48'7   47'1   46'7   46'6   44'8   44'3   44'1   43'7   43'4   43'1   49'9   48'7   47'1   46'7   46'6   44'8   44'3   44'1   43'7   43'4   43'1   49'9   49'1   47'5   47'5   47'7   — — — — — — — — — — — — — — — — — —		55.7 46.2 52.5	53.7 44.9 51.5 54.0	52.4 42.5 50.5 53.1	50.0 41.8 48.3 53.0	50.0 41.8 47.0 54.1	44.1 50.2 40.0 45.6 54.1	43.8 50.7 40.0 46.3	41.7 48.6 40.9 46.8	40°5 48°6 40°2 46°7	39.6 48.6 38.2 47.9	39.3 48.1 38.1 47.0	38.8 51.2 36.7 48.3 53.6	48.98 52.02 44.18 48.37 53.97
47:6 38:3 37:4 36:9 35:8 35:6 35:3 34:3 33:1 33:3 32:6 33:1 41:0 41:3 42:9 42:1 33:1 37:3 37:2 37:5 37:0 33:2 38:3 38:5 37:7 41:4 42:4 42:6 40:9 40:4 39:1 38:0 34:5 35:6 45:3 41:1 44:2 42:6 40:9 40:4 39:1 38:0 34:5 35:6 45:3 41:1 44:2 42:6 40:9 40:4 39:1 38:0 34:5 35:6 45:3 41:1 36:7 36:0 35:4 34:9 39:1 38:0 34:5 35:6 45:3 41:1 36:7 36:0 35:4 34:9 39:1 38:0 34:5 35:6 45:3 41:1 36:7 36:0 35:4 34:9 39:1 38:0 34:5 35:6 45:3 41:1 36:7 36:0 35:4 34:9 39:1 38:0 34:5 35:6 45:3 41:1 36:7 36:0 35:4 34:9 39:1 38:0 34:5 35:6 45:3 41:1 36:7 36:0 35:4 34:9 39:1 38:0 34:5 35:6 45:9 36:0 36:0 36:0 36:0 36:0 36:0 36:0 36:0		39'4 52'1 59'9 56'6	39'4 48'5 55'2 56'4 49'9	36.2 44.0 54.0 56.9 48.7	37:3 42:7 52:5 56:9 47:1	36.5 41.0 56.2 56.1	36°3 39°2 58°2 55°6 46°6	36°3 39°0 57°2 60°6	37·2 36·3 58·7 60·4	37·2 36·5 57·3 60·7	37·2 37·5 56·4 56·2	37.1 39.8 54.1 56.1	39.0 40.6 53.6 51.3 43.1	50°09 36°25 44°95 55°03 58°06 49°95
68'8 67'7 64'9 63'4 62'7 61'7 60'4 59'5 50'6 60'6 58'3 60'4 66'4 66'2 64'4 62'2 60'4 59'9 60'0 59'0 59'7 59'3 59'7 69'2 64'3 66'8 64'9 61'6 59'2 59'2 55'9 55'8 55'4 54'6 53'6 54'0 53'5 54'4 62'0 66'8 64'9 61'6 59'2 59'2 55'9 55'8 55'4 54'6 53'6 54'0 53'5 54'4 62'0 66'8 61'9 59'5 55'8 55'4 54'2 52'1 49'2 50'5 50'5 59'7 59'7 59'5 57'7 56'8 56'9 57'0 56'3 56'9 57'0 56'3 56'9 57'0 56'3 56'9 57'0 56'3 56'9 57'0 56'3 56'9 56'1 54'9 54'3 55'5 55'1 56'9} 67'1 63'2 60'9 61'6 61'9 61'5 61' 54'9 54'3 55'5 55'1 56'9} 62'0 54'76 52'97 51'18 49'91 49'69 49'17 47'85 47'34 46'86 46'64 46'38 46'61 51'4 65'3 63'5 62'5 62'1 61'6 61'3 60'6 59'7 59'2 59'7 58'2 48'5 57'5 56'31 58'9 58'5 59'7 59'4 58'9 58'3 58'3 58'3 57'3 57'3 58'3 59'6 60'0 60'6 68'1 58'1 59'1 68'6 57'9 56'5 55'2 51'2 53'5 52'9 59'4 56'3 54'6 50'9 46'5 46'4 45'6 44'6 44'0 42'7 41'8 41'2 40'5 50'1 48'4 47'7 44'8 42'8 41'2 40'1 61'4 49'1 48'5 45'2 44'7 41'8 41'2 40'5 50'1 48'4 47'7 44'8 42'8 41'2 40'1 62'4 45'0 44'4 43'3 41'4 41'1 42'1 51'1 60'4 57'4 50'9 49'0 55'9 49'0 49'0 48'2 44'6' 55'1 58'8 55'5 55'5 53'5 50'7 55'2 53'2 53'2 53'5 52'9 59'4 44'6 44'0 42'7 41'8 41'2 40'5 50'1 63'1 68'6 61'3 68'0 50'9 46'5 46'4 45'6 44'6 44'0 42'7 41'8 41'2 40'5 50'1 65'3 56'6 55'5 55'5 53'5 55'7 55'2 53'5 50'7 55'2 53'1 55'9 55'4 55'5 55'5 53'5 50'7 55'2 48'5 46'1 45'0 44'4 43'8 45'0 42'3 41'4 41'1 42'1 51'1 60'4 57'4 50'9 49'6 47'5 47'1 46'4 45'0 45'0 44'4 43'8 45'0 52'9 62'6 61'3 68'0 57'0 56'3 54'2 53'1 52'5 52'9 51'4 51'9 58'5 53'8 52'5 49'7 47'9 47'7 47'7 49'7 51'9 52'5 52'9 51'4 51'9 58'5 53'8 52'5 49'7 47'9 47'7 47'7 49'7 51'9 52'5 52'9 51'4 51'9 58'5 53'8 52'5 51'4 51'9 58'5 51'5 53'4 50'9 58'3 58'3 58'3 58'3 58'3 57'6 54'8 62'2 66'4 64'1 63'1 63'1 62'6 61'5 59'6 58'3 58'3 58'3 57'6 54'8 62'2 50'3 49'4 48'5 48'5 48'4 52'7 55'5 55'5 55'3 54'4 53'3 52'3 49'9 55'5 55'3 55'3 55'6 56'6 56'6 66'9 56'4 64'1 63'9 63'3 63'3 62'5 61'3 60'9 61'6 61'1 61'3 62'9 62'9 62'6 61'9 62'9 52'5 55'4 55'5 55'5 55'3 55'3 55'7 55'3 55'3 55'5 55'4 55'5 55'5 55'5 55'3 55'5 55'5		40.6 47.3 50.1 44.0 47.7	38'3 42'9 47'9 40'5 47'5	37.4 42.1 46.5 38.7 45.6	36.9 38.1 44.1 37.1 45.0	35.8 37.3 44.2 36.7 44.8	35.6 37.2 42.6 36.0 45.3	35°3 37°5 40°9 35°4 46°3	52.4 34.3 37.0 40.4 34.9 44.8	53.7 33.1 38.2 39.1 34.1 45.8	33°3 38°3 38°0 32°9 45°8	32.6 38.5 34.5 32.7 46.7	33°1 37°7 35°6 33°1 46°9	53°14 41°02 41°42 45°33 39°28 46°38 56°44
65:3 63:5 62:5 62:1 61:6 61:3 60:6 59:7 59:2 59:7 58:2 59:8 62:7 58:8 55:8 55:7 55:2 53:2 51:4 50:7 49:9 50:9 49:0 48:2 48:5 57:5 63:1 59:9 58:5 59:7 59:4 58:9 58:3 58:3 58:3 57:3 57:3 58:3 58:3 59:6 60:0 60:6 58:1 58:1 59:1 58:6 57:9 56:5 55:2 54:2 53:5 52:9 59:4 56:3 54:6 50:9 46:5 46:4 45:6 44:6 44:0 42:7 41:8 41:2 40:5 50:1 48:4 47:7 44:8 42:8 41:2 40:1 — — — — — — — — — — — — — — — — — — —		65°2 66°8 65°7 59°7	64.4 64.9 63.1 59.5	62.2 61.6 59.6 57.7	60.4 59.2 57.3 56.8 61.6	59°9 59°2 57°1 56°9	60°0 55°9 55°0 57°0	60°4 59°0 55°8 55°4 57°7	59.5 59.7 54.6 54.2 58.7	59.6 59.4 53.6 52.1 57.5	60°6 60°2 54°0 49°2 58°3	58°3 59°7 53°5 50°5 58°7	60.4 60.2 54.4 50.5 58.8	64'43 64'38 62'04 59'70 60'00 62'08
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ŀ	54.76	52.97	51.18	49.91	49.69	49.17	47.85	47:34	46.86	46.64	46.38	46.61	51.49
58*8         56*0         50*9         47*7         46*4         45*2         44*2         43*0         42*3         41*4         41*1         42*1         51*1           60*4         57*4         50*9         49*6         47*5         47*1         46*4         45*0         45*0         44*4         43*8         45*0         52*9         58*5         55*5         50*7         55*9         54*2         53*1         52*5         52*9         51*4         51*9         58*5         55*5         53*5         50*7         52*9         48*5         46*1         45*9         45*3         44*8         44*2         55*5         53*8         52*5         52*5         51*7         51*7         51*6         55*5         53*8         52*5         49*7         47*9         47*7         47*7         49*7         51*9         52*5         52*5         51*7         51*7         51*6         55*5         53*8         52*4         50*7         —         —         —         —         —         —         —         —         —         —         —         —         —         —         —         —         —         —         —         —         —         —         —<		58.8 63.1 60.0 56.3	55.8 59.9 60.6 54.6	55.7 58.5 58.1 50.9	55.2 59.7 58.1 46.5	53°2 59°4 59°1 46°4	51.4 58.9 58.6 45.6	50.7 58.3 57.9 44.6	49.9 58.3 56.5 44.0	50°9 58°3 55°2 42°7	49.0 57.3 54.2 41.8	48.2 57.3 53.5 41.2	48.5 58.3 52.9 40.5	62.72 57.52 59.66 59.44 50.17 46.67
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		60°4 62°6 60°9 53°8	57.4 61.3 58.5 52.5	50.9 58.0 55.5 49.7	49.6 57.0 53.5 47.9	46.4 47.5 56.3 50.7 47.7	45 · 2 47 · 1 54 · 9 52 · 9 47 · 7	44.2 46.4 54.2 48.5 49.7	43.0 45.0 53.1 46.1	42·3 45·0 52·5 45·9	41.4 44.4 52.9 45.3	41'1 43'8 51'4 44'8 51'7	42°1 45°0 51°9 44°2 51°7	51°12 52°91 58°56 55°57 51°64
$\begin{bmatrix} 55.8 & 55.3 & 54.4 & 54.0 & 53.8 & 52.7 & 50.2 & 50.3 & 49.4 & 48.5 & 48.5 & 48.4 \\ 59.5 & 58.3 & 54.4 & 53.3 & 52.3 & 49.9 & 52.5 & 52.4 & 52.2 & 51.7 & 51.5 & 51.5 \\ 61.5 & 62.9 & 57.9 & 55.7 & 55.3 & 54.9 & 54.1 & 54.2 & 53.2 & 53.0 & 52.5 & 53.0 \\ 68.1 & 62.3 & 60.4 & 59.8 & 57.5 & 57.0 & 56.4 & 55.7 & 55.4 & 55.6 & 55.6 & 58.0 \\ 64.9 & 64.4 & 64.1 & 63.9 & 63.3 & 63.0 & 62.5 & 61.3 & 60.2 & 60.2 & 59.2 & 57.4 \\ 62.5 & 61.3 & 60.9 & 61.6 & 61.1 & 61.3 & - & - & - & - & - & - \\ 68.2 & 67.6 & 65.7 & 64.1 & 62.9 & 63.0 & 63.1 & 63.7 & 63.3 & 61.8 & 61.6 & 62.1 & 66.57 \\ \hline \end{bmatrix}$		63.8 63.9 67.5 73.5 66.4	61.6 59.5 64.6 72.7 64.1	60:0 58:1 62:3 66:7 64:1	59'9 57'1 59'8 66'1 63'1	58°3 54°3 58°7 65°5 62°6	58°3 54°6 58°0 64°9 61°5	55.1 57.8 54.6 58.9 64.1	58.6 53.0 58.3 62.9	58°3 52°1 57°1 61°7	58°3 49°2 58°0 62°1 56°9	55.9 57.6 48.5 58.3 62.7 56.2	54.8 48.9 58.9 62.6 55.6	56.74 62.20 57.82 62.28 66.92 64.37
68·2 67·6 65·7 64·1 62·9 63·0 63·1 63·7 63·3 61·8 61·6 62·1 65·7		55.8 59.5 61.5 68.1 64.9	55'3 58'3 62'9 62'3 64'4	54.4 54.4 57.9 60.4 64.1	54.0 53.3 55.7 59.8 63.9	53.8 52.3 55.3 57.5 63.3	52.7 49.9 54.9 57.0 63.0	50°2 52°5 54°1 56°4 62°5	50°3 52°4 54°2 55°7	49.4 52.2 53.2 55.4	46.4 48.5 51.7 53.0 55.6	46.4 48.5 51.5 52.5 55.6 59.2	48.4 51.5 53.0 58.0 57.4	52:30 52:74 55:49 57:41 60:30 62:93
		68.5	67.6	65.7	64·1	62.9	63.0	62.9 63.1	63.7	63.3	61.8	62.9 61.6	62.1	62.78 65.77 66.58
61.62 59.91 57.62 56.48 55.20 54.92 54.87 54.34 53.74 53.20 52.81 53.07 58.18									54.34	53.74	53.50	52.81	53.07	58.18

سور حجوب						WET T	HERMOME	TER.				,	
Hours o Götti: Tin	f Mean	0	1	2	3	4	5.	6	7	8	9	10	11
	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix}$	65°3 61°7 60°4 55°0	$\begin{array}{c c} 67^{\circ}.2 \\ 62^{\circ}.4 \\ 63^{\circ}.7 \\ 62^{\circ}.7 \end{array}$	69°6 62°1 64°3 66°9	68°5 62°5 64°5 67°0	69°8 63°8 64°5 69°0	69°3 63°5 62°4 70°3	71°6 68°3 64°3 71°2	69°8 67°9 63°1 69°4	70°2 67°9 65°6 70°5	68.7 68.2 63.6 68.7	69°0 67°4 62°5 69°8	68°4 67°4 64°3 68°1
	5 6 7 8 9 10 11	60'9 57'6 56'0 60'4 72'6 67'2	64.1 59.1 58.7 64.5 74.2 72.8	62.6 58.3 61.7 67.9 78.1 74.0	67.6 59.1 62.7 71.0 78.3 74.8	63.5 57.9 65.4 70.0 77.6 76.3	67.2 58.9 65.1 69.8 77.3 76.1	67.6 58.5 66.7 65.4 81.1 74.6	63.6 63.5 68.1 65.2 72.3 74.6	64.3 64.4 69.1 68.5 78.2 73.8	63:9 58:3 70:0 69:8 80:0 71:3	63.7 59.3 70.9 71.0 78.7 72.3	64.6 58.1 69.3 71.5 71.3 74.2
JULY.	12 13 14 15 16 17 18	56°1 50°1 48°4 51°9 47°7 54°3	58.7 54.8 50.3 57.5 54.0 59.7	59.5 57.2 51.5 58.3 59.1 61.9	63°0 53°9 53°0 61°8 58°7 63°1	61:7 55:5 51:4 57:2 60:4 63:7	61.7 55.3 52.7 56.0 61.8 64.5	63.3 56.0 54.2 56.6 60.9 64.3	69.8 55.9 55.0 56.2 61.3 63.9	65:3 57:1 57:9 57:1 61:3 64:5	67.7 57.1 55.4 57.3 59.2 63.6	70°3 54°1 60°6 57°2 58°3 64°3	65.6 53.4 57.1 58.1 58.9 64.3
	19 20 21 22 23 24 25	62.5 63.7 62.8 59.2 65.6 60.0	65.6 66.1 63.9 63.1 64.9 62.5	65 · 2 67 · 7 64 · 5 63 · 9 63 · 9 64 · 5	67.7 67.2 66.1 64.5 64.5 64.9	68.6 68.1 65.6 68.7 64.3 64.9	68 2 67 7 65 9 68 8 64 6 65 3	68.4 68.5 67.9 69.8 64.8 64.5	67.5 67.4 67.7 70.1 63.8 65.8	69.2 66.6 66.4 67.9 65.3 70.2	69°0 66°4 68°2 67°1 66°9 69°1	68.7 65.4 66.7 68.4 66.5 68.8	67.6 64.6 66.6 67.0 66.4 69.0
	26 27 28 29 30 31	61.5 59.4 68.3 71.2 61.8	64.9 62.6 71.2 73.5 61.6	66°3 65°1 70°5 75°1 62°4	66°3 66°3 72°8 75°6 63°3	66.5 67.9 73.3 75.4 63.6	65°3 67°4 74°3 74°3 62°9	62.9 66.9 75.8 75.0 64.7	61.8 67.2 74.0 73.0 63.3	61.8 68.4 72.8 74.8 63.9	62.9 68.3 74.3 73.9 63.7	62.7 67.7 74.6 72.4 64.5	61:3 69:0 72:8 72:3 66:5
Hourly	Means	60.06	63.15	64.2	65.21	65.73	65.80	66.44	65.97	66.78	66.39	66.21	65.84
	$\left(\begin{array}{c}1\\2\end{array}\right)$	58.7	60.2	60.2 -	61.1	62.3	64.6	66.1	66.8	65.9	65.9	64.8	64.3
	3 4 5 6 7 8	57.9 60.6 67.7 60.4 60.4 62.9	63°1 64°1 68°9 62°3 62°9 63°3	66.5 68.3 71.3 64.5 65.3 63.7	67.9 69.2 74.6 68.1 68.4 64.1	68.6 71.5 74.8 73.4 73.2 63.8	69.8 72.3 75.8 73.0 71.0 65.9	70°5 73°4 75°8 72°6 71°2 69°2	72.6 74.1 76.5 72.0 72.0 68.9	70.8 74.1 76.4 71.2 72.8 68.5	68.7 74.2 75.6 70.8 70.8 68.1	66.8 74.8 74.6 70.1 69.3 69.0	66.8 75.2 74.6 69.8 70.2 67.9
JST.	9 10 11 12 13 14 15	64.4 50.7 55.0 66.9 59.7 57.9	64.4 53.1 60.6 69.3 61.1 62.8	64.9 55.9 65.1 70.6 63.6 65.9	65 · 2 60 · 0 67 · 7 71 · 0 64 · 1 69 · 2	66.2 61.5 71.2 73.8 69.2 71.1	67.7 61.9 70.5 74.1 69.5 71.2	66.2 64.5 69.6 73.5 69.8 70.4	66°2 64°1 70°2 74°5 68°4 69°8	67.0 64.5 70.2 70.8 67.6 72.0	67.5 64.5 70.6 71.9 69.1 71.2	66.7 63.9 69.6 72.8 69.8 71.0	64.5 63.9 67.4 73.5 68.8 71.3
AUGUST.	16 17 18 19 20 21 22	59°1 47°4 53°1 60°1 56°0 61°9	60°8 48°9 56°6 60°9 61°7 62°4	61 · 9 49 · 9 56 · 8 61 · 3 65 · 6 62 · 4	63°1 53°3 56°1 61°9 68°1 62°9	63°9 56°7 56°2 62°8 67°6 64°3	62.9 57.8 57.8 63.5 67.7 64.5	62.6 57.3 58.0 64.2 68.7 68.1	61·7 57·7 58·5 63·8 67·9 67·5	62.7 58.1 60.2 65.2 68.7 68.7	60°9 59°3 59°3 64°1 69°0 67°2	60.6 58.8 59.8 66.6 66.7 66.6	59.4 58.4 59.7 66.8 66.3 64.5
	23 24 25 26 27 28 29 30	49°9 53°1 55°1 58°3 60°4 60°4	52.0 57.5 63.4 63.1 62.4 64.3	54.6 61.7 66.2 65.6 63.5 68.5	58°1 63°4 66°6 68°5 . 64°3 70°3	59.4 63.8 65.9 70.0 68.7 70.4	60°4 64°7 65°9 70°3 69°3 71°8	60.9 64.4 67.9 69.8 71.0 71.8	61.5 64.4 66.7 68.8 71.8 70.8	60.4 64.9 65.6 68.8 71.0 63.9	61.5 65.9 63.4 67.4 70.8 64.5	60°6 65°3 62°9 66°8 69°5 64°9	61.8 64.6 62.6 66.0 69.1 65.9
	30	63.2	64.1	69.8	70.8	71.0	72.4	72.9	73.0	71.8	72.1	72.0	72.1
Hourl	y Means	58.52	61.32	63.60	65:31	66.97	67.55	68.09	68.08	67.76	67:46	67.09	66.75

					WET	THERMO	METER.					
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
66.8	66.4	65.3	64.4	63.3	62.7	62.1	64.6	63.8	62°.8	62°1	6Î.3	66.38
68.1 64.9	65°9 63°9	62°1 57°9	59°1 55°9	57.6 54.3	$56\cdot 3 \\ 53\cdot 4$	$57^{\cdot}2$ $52^{\cdot}7$	$\frac{58.3}{52.5}$	58°3 52°9	57.4 $52.5$	$\frac{57\cdot2}{52\cdot3}$	56°8 52°3	62·39 59·53
68.1	66.6	65.2	63.0	63.2	62.0	·				<u> </u>	$\frac{-}{59\cdot 8}$	65.43
61.1	59.4	59.2	58.8	57.5	57.2	$63^{\circ}8$ $56^{\circ}4$	$\begin{array}{c} 63.1 \\ 56.2 \end{array}$	63°1 56°1	62.1 53.6	$61.5 \\ 54.6$	54.3	60.75
57.0	56.6	55.4	55.4	54.6	51.4	51.1	52.5	52.5	52.6	52.7	54.4	56.63
69°3 72°1	70°3 71°6	66°2 69°2	61.7 67.7	61.5 68.1	$69.6 \\ 60.9$	60.7 69.8	68.3 68.1	68.8 60.8	58 <b>·1</b> 67·0	57.4 66.7	56.9 69.2	$63.70 \\ 68.47$
69.8	67.9	68.3	66.7	68.1	67.0	68.0	66.8	64.9	65.1	65.1	64.3	71.74
71.2	69.3	71.3	70.1	71.0	70.3	60.5	59.2	57.1	55.4	53.1	$\begin{bmatrix} -55\cdot 3 \end{bmatrix}$	68.56
65'1	63.3	59.9	59.3	59.2	58.3	56.1	48.4	47.1	44.8	44.3	45.0	58.89
52.4 57.4	51 4 55 4	49.7 54.8	48.8 54.8	46°4 52°0	$\begin{array}{c} 47.5 \\ 51.5 \end{array}$	47.4 51.5	46.4 50.5	46'4 50'5	44.6 49.2	44.6 47.7	45°1 47°9	51°30 52°95
57.7	54.6	51.2	49.1	47.5	46.5	46.3	46'1	45.5	45.0	44.7	43.6	52.64
58°1 63°1	57.5 62.6	54.4 58.7	51.2 $56.6$	51.9 56.0	51'2 54'6	51.2	50.2	49.7	48.9	48.3	49.2	55.44
						59.6	59.0	58.1	58.3	60.2	59.2}	60.75
67.7 64.1	66.4 63.9	64.1 63.8	60°2 63°3	$\begin{array}{c} 58.8 \\ 62.5 \end{array}$	58.8 $62.1$	58.7 63.1	60.8 60.0	59°2 59°6	57°8 59°8	$\frac{56\cdot2}{60\cdot2}$	57°9 59°8	$63.92 \\ 64.27$
66.5	64.1	60.2	59°6	58.1	56.6	56.6	56.6	55.1	54.0	55.5	56.4	62.14
67.0	66.8	64.9	64.1	63.7	63°1 60°5	62.4 60.2	$63.3 \\ 60.4$	$\frac{63.9}{60.2}$	$62.9 \\ 60.5$	63.8 60.2	64.0 59.4	65°35 63°64
66.2	66°1 67°7	65.4 63.9	64.5 $61.1$	61.9 59.2	59°2							63.63
-			_	53.4	<u></u> 52.9	61.1 53.6	61.3 54.4	60°2 55°2	58°3 55°0	58°3 56°4	58·1 }	59.79
62.4	58.8 67.6	$\begin{array}{c} 56.5 \\ 66.2 \end{array}$	54.6 63.9	62.4	60.8	62.7	62.9	$\frac{55}{64.5}$	64.2	64.9	65.0	65.43
71.8	72.2	72.0	72.3	72.3	71.3	70.9	70.5	69.8	69.3	69.3	68.1	71.85
70.4 65.9	69°5 63°1	66.9 60.2	65.6 58.6	63°6 55°5	62'1 55'2	64°1 55°0	63°8 56°2	62°9 56°0	$\begin{array}{c} 61.6 \\ 55.8 \end{array}$	61.7 56.4	61.8 56.4	60.69
65.26	64.03	61.98	60.38	59:39	58.63	· 58°61	58.58	57.87	56.92	56.88	57.00	62.41
64.1	61.2	58.8	58.3	58.3	58.3						55.2}	60.67
64.3	64.7	63.5	62.5	58°1	57.9	57°3 57°1	56°2 56°9	55°8 56°4	55°2 56°1	56°0 55°5	55 9	63.29
74.4	71.2	71.5	69.3	68.9	66.8	66.4	66.4	64.9	64.0	65.1	64.1	69.37
73.0	$\begin{array}{c c} 71.8 \\ 63.6 \end{array}$	$\frac{71.6}{63.1}$	$71.5 \\ 60.9$	70°8 59°3	70°8 59°1	68.1 59.3	$\begin{array}{c} 64.7 \\ 59.2 \end{array}$	$\begin{array}{c} 63.3 \\ 59.2 \end{array}$	61.2 58.8	$\begin{array}{c} 60.2 \\ 59.7 \end{array}$	60°2 58°9	70°59 64°96
69.2	66.2	64.6	63.1	63.1	61.2	62.1	62.7	62.7	62.2	62.4	62.3	66.23
66.8	65.9	66.4	66°3	66°5	65.9	64.1	64.5	63.3	62.6	62.9	$\frac{-}{62 \cdot 8}$	65.55
61.3	57.7	55.6	56.2	54.4	54.6	52.8	51.7	50.7	50.1	49'1	48.7	59.74
64.4	62°3 66°4	59.7 64.6	$58\cdot3$ $64\cdot3$	57.5 64.1	56.6 63.8	55 <b>·</b> 9 64 <b>·</b> 4	54.6 64.7	53.6 64.2	53°8 64°9	54.0 64.9	52·3 64·4	58.81 66.08
72.7	65.9	65.5	65.4	62.3	$62^{\circ}3$	62.3	60.7	59.6	58.1	57.5	57.0	67.17
68°3 70°4	66.5 69.2	64.5 68.7	61°3 67°9	60.4 68.5	59.6 67.9	28.9	59.1	58.3	57.6	57 <b>·7</b>	57.1	63.75
-	_		—			59.8	59.2	59.7	59.5	59.7	$\frac{-}{58\cdot 1}$	66.35
58.5 57.4	57.7 54.3	55.9 53.4	55.0 $51.2$	54.4 51.2	54.0 50.9	53.7 50.1	50°0 50°4	48.5 49.6	48.6 48.9	$\begin{array}{c} 48.5 \\ 48.9 \end{array}$	$\frac{48.1}{49.2}$	57 <b>·</b> 19 53 <b>·</b> 29
60.2	59.8	59.5	60.2	59.8	60.4	60.2	60.2	60.7	60.4	60.0	59.8	58.90
66.3	64.1	$62.7 \\ 64.7$	62.5 $64.4$	61.5 64.9	$\begin{array}{c} 61.5 \\ 63.7 \end{array}$	63.6 63.6	59.9 62.5	59°2 61°8	57°5 61°8	$\begin{array}{c} 57.2 \\ 61.7 \end{array}$	56.6 62.4	$62.12 \\ 64.89$
64.1	65.5 62.8	62.3	61.8	61.1	60.2						<u> </u>	61.61
60.8	56.7	- 54.4	52.5	52.4	52.0	57.4 51.4	55°5 50°3	55°1 49°4	54°3 49°4	52 <b>.</b> 1 49.6	50°6 } 50°5	55.44
63.9	63.3	62.1	61.1	61.3	60.7	60.2	59.5	58.7	57.7	56.9	55.6	61.45
61.1	60°2 61°9	59.4 61.1	58°1 59°3	58.0 59.1	58.1 58.9	57.9 59.6	56.8 58.8	56°2 58°7	56.6 59.7	56.0 59.4	56.2 59.6	61.12 $63.53$
67.7	66.6	65.6	64.1	63.2	63.6	62.3	61.4	60.4	59.6	59.4	58.8	65.50
66.4	63.8	63.1	62.3	61.4	62.3	63.1	60.2	59.6	59.6	60.5	$\frac{-}{62 \cdot 9}$	64.68
69.4	68.5	67.0	66.2	65.7	63.1	62.1	62.1	61.9	60.4	63.3	63.1	67.43
65.89	63.76	62.67	61.70	61.02	60.56	59.65	58.79	58.13	57.66	57.61	57.32	63.07

						WET T	HERMOME	TER.					
I ours o Götti Tim	f Mean }	o	-1	2	3	4	5	6	7	8	9	10	11
	f Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\left( egin{array}{c c} 1 & & \\ 2 & \\ 3 & \\ 4 & \\ 5 & \\ \end{array} \right)$	63.7 64.4 68.2 65.9 69.8	$6\overset{\circ}{7}\overset{\circ}{.}0$ $6\overset{\circ}{7}\overset{\circ}{.}9$ $6\overset{\circ}{9}\overset{\circ}{.}4$ $6\overset{\circ}{7}\overset{\circ}{.}9$ $7\overset{\circ}{1}\overset{\circ}{.}3$	68°3 70°2 69°4 69°0 73°0	72°3 72°5 69°4 70°0 74°6	73.7 73.6 70.8 70.8 75.5	70°5 74°6 71°8 73°6 74°2	71°0 76°0 71°3 73°4 73°5	$72^{\circ}4$ $75^{\circ}5$ $71^{\circ}0$ $73^{\circ}4$ $73^{\circ}8$	72°8 74°8 71°0 73°8 73°5	71°8 74°0 71°8 73°5 74°3	71°8 73°8 70°6 73°2 73°8	71°1 73°2 71°1 72°8 72°5
•	6 7 8 9 10 11 12	64.7 57.8 45.5 53.7 62.9 67.2	69.2 59.1 47.0 54.4 65.3 70.8	73°0 60°2 49°1 55°2 65°7 73°3	74.8 61.3 50.2 54.1 68.0 74.2	76.2 62.8 51.7 54.6 68.4 74.2	77.0 63.5 51.9 54.8 69.3 73.9	78.4 63.1 51.3 54.4 69.8 71.8	76.7 63.1 53.8 55.0 71.8 63.4	76.1 64.9 54.2 56.9 72.2 65.9	75.5 60.5 54.1 57.6 70.8 67.0	74.6 59.2 54.2 58.5 70.5 67.4	73 · 9 58 · 3 54 · 6 59 · 4 71 · 3 68 · 7
SEPTEMBER	13 14 15 16 17 18 19	65°3 50°4 43°1 52°1 54°6 45°8	68°3 50°0 47°9 52°5 55°1 50°7	71 · 2 49 · 2 52 · 7 54 · 2 55 · 8 56 · 8	72·2 49·2 55·5 55·2 58·3 59·3	73.8 50.0 57.2 57.0 59.6 63.6	75°5 49°1 57°8 57°8 60°7 65°1	75.0 51.2 57.9 59.6 60.5 66.1	75.8 50.2 57.5 59.2 60.8 64.7	76.7 50.9 57.9 57.8 61.5 65.7	75°4 51°4 57°2 57°3 61°6 65°1	74.4 52.7 56.9 56.2 61.8 65.1	75·4 52·7 57·2 55·6 61·7 64·3
	20 21 22 23 24 25 26	45.8 38.5 44.5 58.3 48.4 42.3	48.4 42.3 52.7 61.8 48.9 44.8	48°2 49°0 58°9 61°8 49°2 47°1	48.7 54.0 61.2 62.9 49.9 50.7	48.7 55.4 62.9 63.3 52.3 52.7	49.7 56.8 64.7 63.4 53.7 52.9	51.0 57.5 66.6 64.4 54.2 53.8	52°1 58°0 66°4 63°9 54°6 55°4	52°2 58°6 66°7 59°4 55°5 55°0	52.4 58.9 66.5 58.9 55.9	52°2 59°3 66°1 59°1 54°2 55°5	50.9 58.7 65.1 58.3 51.9 55.1
	27 28 29 30	37·7 54·1 55·6	40°3 55°5 57°4	42.9 56.8 57.8	45.2 59.2 60.5	47.1 60.5 60.8	51.7 61.2 62.6	51.2 60.2 63.3	51.2 61.1 63.1	53.4 60.6 62.3	53 · 9 59 · 7 62 · 3	53°7 59°5 61°3	52.9 60.0 59.2
Hourl	y Means	54.63	57.15	59.15	60.90	62.50	62.99	63.35	63.24	63.47	63.50	62.91	62.23
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	49.1 45.5 38.3	47°3 45°1 39°6	47.7 44.9 45.0	47.0 45.3 48.5	47.0 46.2 48.9	47.8 47.1 50.3	48.5 47.1 50.9	48.7 48.0 51.1	49.9 47.3 51.4	50.0 47.5 50.3	48°3 49°2 49°2	48.3 49.0 47.2
	5 6 7 8 9	44.2 40.5 49.3 59.3 56.4 36.2	45°3 41°2 51°7 59°0 57°0 36°5	49°1 47°1 58°3 60°9 57°3 37°0	51.6 54.3 60.8 60.9 64.5 38.5	55°2 56°5 61°5 62°1 65°5 40°1	57·1 57·5 62·1 62·5 65·3 42·4	57 · 9 58 · 8 63 · 4 59 · 6 65 · 1 43 · 5	57 · 9 59 · 5 63 · 9 58 · 5 64 · 3 44 · 1	57.5 59.5 62.4 57.5 54.5 44.5	58°1 59°4 63°6 57°2 53°0 45°4	57°3 58°0 63°3 57°0 51°3 45°1	56.9 57.5 61.7 56.4 50.7 44.2
OCTOBER.	11 12 13 14 15 16 17	48.4 47.5 34.9 36.2 45.4 33.9	51'3 47'1 34'3 36'0 46'5 32'6	52.8 47.1 39.1 39.0 47.5 31.8	54.6 47.4 41.5 40.5 48.2 33.4	55°0 46°9 46°4 41°2 51°3 34°1	55.9 46.2 46.5 41.6 52.2 34.3	56.4 45.6 46.4 41.7 53.8 34.9	56.4 45.8 46.2 41.8 56.1 35.1	57.0 45.8 45.8 42.6 55.6 34.2	56.9 45.8 46.4 43.2 55.8 34.2	57.2 44.8 46.2 43.3 55.0 33.6	56.9 42.7 44.1 41.2 55.5 32.9
Ō	18 19 20 21 22 23 24 25	31.8 41.0 31.7 36.3 23.8 32.8	31.0 42.6 32.0 36.2 25.1 34.3	35.8 42.6 33.5 36.5 25.5 37.1	38.8 43.5 36.2 37.0 27.6 39.4	40.4 43.1 37.3 36.4 32.4 41.4	42:3 43:8 37:9 35:8 36:2 40:9	42.1 45.0 38.8 34.9 37.1 40.9	40.8 45.4 39.5 34.1 39.0 40.9	40.3 43.3 38.5 34.1 38.8 38.9	40.8 41.2 37.6 32.9 38.9 39.1	41'2 41'4 37'4 31'2 40'0 38'2	40.0 40.2 37.2 31.0 38.9 36.7
Nov	26 27 28 29 30 31	32.3 49.9 28.0 34.3 32.0 28.4	35.5 47.9 28.5 34.7 32.2 30.5	38°3 46°7 30°0 35°8 32°9 29°4	40.5 45.4 30.0 39.4 33.9 29.7	43 1 44 8 31 4 40 9 34 1 30 5	46.4 46.4 31.7 42.5 34.6 31.6	48.2 44.2 32.3 39.4 34.4 32.0	49.4 44.2 34.3 40.9 34.5 33.9	49°1 44°2 35°6 41°2 34°9 35°5	48.4 42.6 36.0 40.9 34.5 36.3	48.1 41.9 35.6 39.9 33.9 36.9	47.0 40.8 33.2 39.4 32.6 38.1
	y Means	39.53	40.04	41.80	43.64	44.95	45.89	46.03	46.46	45.92	45.78	45.35	44.46

					WET	THERM	METER.					
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
71°0	69°6	69°.8	69°3	67°7	69°3	67°5	66°7	65.2	65.4	6 <del>4</del> °5	64·5	69.05
72.8	72.4	71.8	71.0	69.8	69.4	69.5	69.2	68.4	68.0	68.6	67.6	71.21
71.0	70'4	68.3	67.7	67.9	68.2	68.3	69.2	69.5	691	68'6	65.9	69.58
71.6 70.2	70°8 67°9	70°5 66°7	70°3 65°1	70.0	70.0	70.5	70.8	70.8	70.8	70.4	69.4	70.97
10 2	019	00 /	05 1	64.1	64.1	$\frac{65.9}{}$	65.5	64.9	64.0	64.9	$\frac{-}{64.5}$ }	69.48
72.8	72.3	69.6	69.4	67.9	67.0	63.9	69.3	59.7	58.9	58.9	59.0	69.58
57.2	55.4	55.5	54.0	50.6	48.9	47.5	46.7	46.0	45.8	45.3	45°1	55.49
53.2	53.1	54.0	54.6	54.2	56.1	56.2	52.5	55.8	54.8	54.0	$\begin{array}{c} 52.7 \\ 62.1 \end{array}$	52*87 57*49
59.0 70.2	59.9 66.9	59.7 67.4	66.7	57·7 65·3	57.8 65.3	58.5	58°1 66°3	59.3 $65.4$	60°3 66°7	$\begin{array}{c} 61.3 \\ 65.9 \end{array}$	$\frac{62}{66} \cdot 7$	67.64
66.9	65.1	62.9	60.7	60.6	61.2							
						64.4	64.3	64.6	64.2	64.4	$\frac{-}{64 \cdot 1}$	66.74
74.0	74.0	73.8	72.2	70.1	67.1	66.1	63.4	60.9	54.0	53.1	51.2	69.12
51.3	50.1	49.2	48.1	47.5	48'1	47.9	47.1	46.9	45.4 51.0	44°3 51°1	44'4 51'9	49°05 54°20
57.4 55.4	57°3 55°1	56.8 55.5	56.4 55.4	54.8 55.3	52.9 55.1	51°1 54°9	50'3 54'8	50°9 55°2	$\frac{51}{55}$	54.6	55.4	55.68
59.4	55.6	53.6	54.0	53.2	53.1	51.8	51.2	49.7	47.1	46.7	45.8	55.56
63.9	60.7	60.4	58.2	57.4	55.7	_					$\frac{-}{49\cdot 7}\}$	59.45
_						61.7	61.4	58.7	54.2	52.1	49.7 \$   40.4	47.43
52.2	49.2	47.3	46.7	45.6	44.6	44.2	42.9	42°1 45°8	41.4 44.8	41.5 44.4	44.4	51.12
57.6 63.6	53°5 64°1	51.4 63.7	49°2 63°1	48.5 62.9	47:3 61:1	46°5 61°7	46.4 62.5	$\frac{45.8}{62.0}$	59.7	58.8	58.2	61.83
58.1	57.1	56.0	54.9	53.7	52.7	52.0	51.3	50.2	50.1	49.2	48.7	57.07
50.3	49.7	50.3	49.4	49.2	49.9	49.1	48.9	48.7	46.2	44.8	43'4	50°3 <b>6</b>
54.6	53.2	53.3	50.7	49.7	46.5		40.5		39.8	38.9	$\frac{-38.2}{38.2}$	48.91
53.5	52.4	51.5	49.7	49.3	49.4	43°3 49°4	$\frac{42.5}{49.7}$	$\frac{41.8}{49.7}$	49.7	50.9	$52 \cdot 7$	49.57
58.9	56.2	54.4	54.6	52.7	55.6	55.2	55.2	55.2	55.4	55.0	55.4	57:20
61.7	60.7	60.4	60.4	58.3	56.0	53.8	53.2	52.3	50.4	48.7	50.5	58.03
61.84	60.20	59.76	58.88	57.86	57.41	57.14	56.55	56.17	55:10	54.65	54.32	59.41
48.1	47.9	46.4	45.1	44.6	44.7	44.7	44.0	44.3	44.0	44.6	44.8	46.78
47.3	43.7	43.1	40.3	39.4	40.2	40.2	39.0	38.6	37.5	37.5	38.3	43.64
44.0	43.6	43.6	42.6	42.1	41.2						$\frac{-}{41.2}$	44.97
				40.5		44.7	42.5	41.6	40.7	40.7 39.8	40.9	49.52
52·2 57·5	49.2	50°2 55°2	49°3 52°3	46.7 50.5	44.6 53.3	44.6 53.5	42.1 53.6	40°9 51°3	39 <b>·</b> 9 49 <b>·</b> 7	50.7	48.2	53.36
60.2	54.8 63.3	63.1	63.3	62.8	61.9	61.6	59.1	58.0	59.2	59.2	59.2	60.55
56.0	55.9	56.0	56.9	56.7	57.0	57.0	56.4	56.6	56.9	56.6	56.6	57.89
48.8	47.9	47.5	44.6	40.5	39.6	39.5	39.6	39.2	38.3	37.7	36.1	50.16
39.4	37.5	37.1	37.1	37.4	36.1	49.4	48.7	48.8	49.1	48.7	$\frac{-}{46.5}$	42.22
57.1	57.4	53.1	51.5	51.1	51.1	50.9	50.8	50.8	49.6	49.7	49.8	53.40
43.3	42'1	41.9	41.3	41.3	40.2	39.8	39.4	38.1	37.9	37.2	36.8	43.01
40.7	40.7	42.7	42.5	42.5	42.5	42.6	42.1	41.0	40.9	38.3	37.4	42.15
39.0 54.2	38.3	38.1	37.9	38.5	39.5	39.8	40.0	40.9	$43.5 \\ 37.3$	$\frac{44.5}{36.2}$	45.6 34.7	40.62 47.67
33.2	52.9 32.0	51'4 30'6	47°9 29°4	43°1 28°6	$\begin{array}{c} 42.8 \\ 29.2 \end{array}$	42.8	40.0	37.9	- 010			33.04
_	_		_			34.8	34.5	33.9	34.3	33.8	33.5	
39.8	39.0	39.0	38.8	38.7	39°4	40.6	40.9	40.8	40.6	40.8	40.6	39.35
39·3 36·7	37.7	36.9	35.3	34.1	33.2	31.5	32.0	31.3	$\frac{31.0}{35.3}$	36.0 30.3	31.7 36.2	$38^{\circ}22$ $35^{\circ}74$
28.8	35.6 28.4	$\begin{array}{c c} 33.7 \\ 27.9 \end{array}$	34.2 26.8	34.9 24.9	34.3 22.4	34.3 21.8	$\frac{34.3}{21.5}$	34.7 20.5	20.2	22.0	23.0	29.36
38.2	38.1	36.5	36.3	36.7	35.3	35.6	34.1	35.1	34.9	34.2	32.5	34.62
36.3	35.3	34.3	31.8	31.3	30.2	_					$\frac{-}{31\cdot 6}$	35.69
49.8	40:5	10.7	40:5	40.5	40:5	33.1	32.3	33.5	33.4 49.1	32.5 50.0	50.2	46.81
49.8	49°7 39°1	49.7 38.7	49.7 37.1	49.7 36.7	49.7 35.9	50°2 35°3	49:7 34:6	$\frac{49.7}{32.9}$	32.2	32.0	29.4	40.12
30.3	28.1	27.5	29.2	31.0	31.0	28.4	30.8	$\frac{32.5}{32.5}$	32.6	31.7	32.3	31.33
37.9	36.7	36.5	36.1	35.1	34.3	33.2	33.0	32.9	32.6	32.5	32.0	36.75
32.3	31.8	32.2	31.8	31.1	30.2	30.1	29.2	28.6	28.8	28.3	28.4	31.98
38.2	39.1	40.4	39.4	39.8	39.9	45.5	46.1	46.2	47.0	47.2	$\frac{-}{47.5}$	37.89
43.33	42.44	41.95	41.06	40.36	40.02	40.94	40.41	40.02	39.87	39.73	39.46	42.48
- 30	14 11	TI 30	11 00	10 00	40 02	10 31	10 11	10 02	50 01			1

						WET TH	HERMOME	TER.					
lours o Götti Tin	f Mean }	0	1	2	3	4	5	6	7	8	9	10	11
Hours of Toro Tin	of Mean onto	18	19	20	21	22	23	0	1	2	3	4	5
	$\left( \begin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ \end{array} \right)$	47.7 46.0 40.9 36.0 30.0 37.3	6 47.3 46.0 41.0 36.2 31.2 38.3	° 47.1 46.7 44.0 38.3 32.2 39.7	9 49 2 47 9 46 8 41 2 38 3 41 6	50°1 48°7 45°6 44°0 43°1 43°1	51.4 49.6 46.2 44.8 44.8	51·1 49·7 46·0 45·3 45·3 46·4	51.0 48.7 45.8 45.5 45.0 45.5	51.6 49.2 45.8 44.5 45.4 45.4	52·2 48·5 45·5 44·8 45·6 46·1	52.4 49.4 44.5 44.0 42.9 44.9	52.4 47.5 42.9 41.6 42.4 43.5
BER.	8 9 10 11 12 13 14	49 2 48 8 49 4 42 9 44 1 42 9	49.1 48.9 49.9 42.4 44.1 42.1	49.9 49.4 50.1 42.8 44.1 41.6	50°3 50°3 50°2 43°6 44°2 42°1	52.7 51.2 50.4 44.2 44.4 42.3	52.4 52.0 50.5 44.6 44.7 41.8	53°3 52°3 50°3 44°6 44°6 41°9	53.0 52.5 50.7 45.4 44.6 43.5	52.7 52.4 50.5 45.4 44.6 42.5	52.6 51.3 51.2 45.2 44.6 41.7	52.5 50.5 51.2 44.8 44.7 41.4	51.7 49.7 49.9 45.0 44.7 41.0
NOVEMBER	15 16 17 18 19 20 21	42.0 38.9 42.8 40.9 34.9 35.1	42.8 40.2 42.1 40.2 34.5 34.5	43°1 42°1 44°5 39°4 34°5 34°7	43.8 43.5 47.7 39.2 34.5 35.4	45°3 44°7 49°7 39°6 35°8 35°1	46.5 44.5 49.7 40.2 37.1 36.3	46.4 45.0 48.7 40.2 37.4 37.4	45.8 46.1 46.8 40.0 38.2 37.7	45.4 45.5 46.2 40.0 39.4 39.1	44.8 45.6 44.9 40.2 39.1 40.4	44.3 45.5 44.6 39.2 38.1 39.0	44 · 2 45 · 8 43 · 8 37 · 7 36 · 7 39 · 4
	22 23 24 25 26 27 28	28·3 33·1 23·9 17·5 22·2 36·4	28°3 31°5 20°9 17°4 21°1 36°0	28.4 32.4 19.2 18.8 21.7 36.2	29'3 33'6 19'4 20'8 23'4 36'1	30.4 36.2 18.2 22.8 23.4 36.7	31.2 37.5 18.7 25.1 24.2 37.9	30.6 38.1 18.9 26.2 25.9 38.1	31.0 39.0 19.1 26.8 28.0 38.7	32.0 37.9 19.6 27.6 29.4 39.1	32.7 36.9 19.4 24.9 30.7 38.2	32.6 34.9 20.0 23.6 31.0 37.3	32·7 32·0 20·1 22·6 32·0 36·2
	$\begin{bmatrix} 29 \\ 30 \end{bmatrix}$	25.5	$\frac{-}{24\cdot 2}$	24.5	25.1	25.9	26.6	26.7	26.8	27.4	26.4	26.1	25.1
Hourly	Means	37.47	37.21	37.80	39.10	40.14	40.92	41.22	41.41	41°56	41.34	40.74	40.0
	$\left( egin{array}{c c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 2 \end{array} \right)$	13.1 33.5 31.0 24.5 27.7 — 32.0	12.6 34.3 30.8 24.6 28.3 ————————————————————————————————————	13.7 35.2 29.5 25.7 28.3	17.9 36.0 30.3 28.3 28.8 — 34.8	19.4 37.2 30.5 31.0 30.8 	21.9 38.1 30.9 29.5 31.5	23 · 2 39 · 0 31 · 5 30 · 6 31 · 8 — 36 · 5	24.7 40.7 31.0 31.2 32.0 — 36.9	25.5 42.6 28.8 31.6 31.6 	26.0 41.3 28.8 32.0 32.0 — 37.1	26.4 40.9 28.4 32.0 32.1 — 37.5	27·2 42·5 28·5 31·0 32·0 — 38·9 32·7
	8 9 10 11 12 13	36.3 30.4 31.0 23.9 18.9	36.2 30.0 31.0 22.5 16.9	34.2 29.6 30.3 22.0 16.1	35.1 28.8 29.3 22.2 15.9	35°0 29°4 29°4 23°6 15°0	34.8 29.5 30.1 24.9 16.1	33.5 30.3 30.6 25.5 16.6	34.4 30.5 31.2 26.2 16.6	34.3 30.3 31.8 26.4 18.0	34.4 30.3 32.0 27.3 18.8	33°3 30°3 31°2 27°1 19°4	30.3 29.8 27.4 20.1
DECEMBER.	14 15 16 17 18 19	15.7 8.0 11.6 21.1 11.5 27.7	15.9 7.3 11.9 21.5 11.3 27.6	15.6 10.0 12.4 22.0 10.7 27.9	15·2 12·1 17·1 23·9 14·4 27·2	15.1 16.7 19.9 24.9 17.1 27.5	16.4 18.5 24.2 25.4 20.1 28.4	17'9 20'0 24'9 25'9 23'0 28'8	19°2 21°7 25°6 25°1 25°4 30°6	20°3 23°3 25°6 25°4 26°8 30°6	20°1 22°8 24°6 26°1 27°3 30°6	19°1 22°2 24°6 25°2 26°8 28°8	18.6 19.2 21.7 22.3 26.6 28.8
	20 21 22 23 24 25 a	20.6 20.6 7.4 25.5	19°2 19°6 4°2 27°1	17.0 18.8 4.6 27.1	17.8 18.9 9.6 28.3	19 ² 19 ⁷ 14 ⁴ 28 ⁸	20°4 20°0 17°0 31°4	21.6 20.9 18.8 31.7	22.8 21.3 20.2 31.6	23.5 23.0 21.4 31.8	23·3 23·4 21·3 32·2	22.8 23.0 21.3 32.2	19.7 20.6 15.6 33.3
	26 26 27	16.3	16.1	15.7	17.9	21.4	24.5	27.1	27.9	29.2	30.0	29.2	30.8
	28 29 30 31	32.9 17.6 36.2 33.7	31.8 18.0 36.7 33.8	32°3 18°8 36°5 35°1	32.0 20.5 37.0 36.5	32.8 23.7 37.2 37.7	31·2 25·1 38·6 37·9	28:4 25:9 38:1 37:9	29.5 25.9 39.0 38.5	28·2 25·6 37·5 39·0	28°1 26°2 36°7 38°3	27.9 26.2 36.3 38.0	27.5 26.8 35.8 37.7
Hourl	ly Means	23.41	23.15	23.12	24.45	25.86	27.02	27.69	28.45	28.81	28.88	28.55	27.9

^a Christmas Day.

6 7 8 9 10 11 12 13 14 15 16 17 Mac.  c							WET	THERMO	METER.					
6         7         8         9         10         11         12         13         14         15         16         17         Machine           5         2         51-77         51-9         51-2         60-11         49-77         48-5         48-9         44-8         41-4         42-77         44-3         49-74         44-8         41-8         41-4         42-77         44-3         49-74         44-8         41-8         41-4         42-77         44-3         49-74         44-8         41-8         41-8         41-8         41-8         41-8         41-8         41-8         41-9         41-0         40-7         48-9         36-6         36-6         44-4         41-7         46-7         38-8         36-6         36-7         36-7         38-3         38-3         36-3         36-6         36-6         44-6         44-1         44-7         46-7         49-7         49-7         36-7         38-3         36-6         36-7         36-3         36-6         36-7         36-3         36-8         36-7         36-3         36-6         36-7         36-7         38-7         38-3         36-7         36-7         38-7         38-3         36-7         36	15	2   18	3 14	<b>4</b>   1	15	16	17	18	19	20	21	22	23	Daily and Monthly
17	6	7	8		9	10	11	12	13	14	15	16	17	Means.
41'-5 47'-2 47'-3 37'-4 47'-4 44'-8 41'-8 41'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8 31'-8					,	0	0	0	0	0	0			[]
1414   40.77   39.98   38.77   38.73   38.73   38.73   38.73   37.77   37.42   37.73   36.65   36.67   36.74   41.77   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73   38.73														49.20
377   3573   3475   3571   3228   3115   299   3076   3076   2999   3075   3170   377   3479   4470   4572   4570   4399   4379   477   475   4876   4973   4073   4973   4977   4977   4978   4879   5070   4977   4977   4978   4879   5070   4977   4977   4978   4977   4977   4978   4879   4977   4977   4978   4977   4977   4978   4978   4977   4978   4978   4977   4978   4978   4977   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978   4978							44.8				40.4			45.98
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$														41.48
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$														
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$								36.3	34.9	36.3	35.6	36.0		1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	43	9   44	0   45	$2 \mid 45$	0	43.9	1	47:0	47.7	10:6	40:2	40.5	40.3	44.78
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	51:	4 51.	2 51.	0 51	-,	50:7							48.0	50.97
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$													49.1	50.26
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$														48.07
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$													43.5	44.01
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												42.9	43.2	44.11
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	41	5 42	5 43	9   43	.9								<b>—</b> }	42.33
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-	.   —		-   _	- 1								41.8	
43'3   42'2   42'1   42'0   41'4   41'7   41'6   41'8   41'5   40'9   40'9   43'3   37'5   38'2   37'5   38'2   36'5   36'3   35'3   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1   35'1													40.2	43.43
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				4   46	$\frac{1}{2}$		46.6							43.87
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$														37.88
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														35.83
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								32 9	00 0	01 2		_		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	05	.   10		. 12	_*			28.6	28.4	28:4	28.3	29.2	28.1	1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	32.	8 32.	2   32	0   32	.9	32.4	35.2		36.0	36.2	34.9		34.6	32.37
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										26.3			24.1	31.63
32   1			6 17.	7   16		16.7	16.4							18.77
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$													22.7	23.28
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$								35.0	34.9	34.7	34.8	,	4	30.17
23.0   22.0   21.6   20.1   18.5   18.2   16.9   15.4   14.7   13.6   14.2   13.5   21.	35	6 35.	3   34.	9   34	2	32.6	31.8		-	00:0	07.7		97:6	33.97
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	23.	0 22.	$0  \boxed{21}$	6 20	-1	18.2	18.2						13.2	21.74
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	39.	55 39	21 39	06 38	79	38.29	38.03	37.21	36.92	36.66	36.40	36.47	36.59	38.83
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			<u> </u>											1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	97.	4 97.	9 29.	4 30		20.8	30.6	30.8	31.7	31.7	32.0	32.0	32.4	25.72
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$													32.4	39.62
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												24.1		27.55
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						31.2	31.0		30.6	<b>3</b> 0.9	30.8	29.4		29.95
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	30.	3   28.	4 28	4 28	.6	28.2	28.2						<del></del>	30.19
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-		.	-   -		-							31 4 )	36.96
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$														$\frac{30.50}{32.61}$
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$														29.38
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$														28.70
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			5 27.			27.2								24.27
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$								_					<b>—</b> }	17.02
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		-	.   _	.   _	-			15.0	15.0	15.0			15.6	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														15.12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														14.33
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														19.94
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														23.43
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$								20 8	Z/ 3	21 3	210			1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	.   21	.'   "_	.   21				23.0	22.8	21.5	21.1	21.8	$_{20} \cdot _{9} \}$	26.68
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			3   14.	1   14	$\cdot_4$						22.1	23.2	24.9	19.23
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	19	2 18.	6 20.				21.7	19.7			13.2	11.1		18.80
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		3   16.	8   16.	3   18	7		12.4	13.4			15.0	16.1		15.18
30.6     31.0     31.6     31.7     32.0     33.7     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —     —	33.	3 33.	6 33.	$\begin{array}{c c} 6 & 33 \\ \hline \end{array}$	2	33.7	34.1	21.2	21.1	20.3	20.3	19.7	$\frac{16.8}{16.8}$	28.41
27·3     27·3     23·5     23·4     22·9     22·8     23·7     21·9     19·4     20·8     20·5     19·9     26·       26·5     28·4     28·3     28·8     29·6     30·8     31·5     31·8     31·8     33·7     34·3     35·6     27·       35·3     35·4     34·7     34·3     33·9     33·9     33·9     34·5     35·1     33·9     33·7     33·8     35·6       37·9     37·6     36·3     37·1     36·5     36·4     36·5     36·2     36·3     35·6     35·4     35·6     36·6	30.	6   31.	0   31.	6   31	.7	32.0	33.7						<del>-</del> 3	29.22
26.5     28.4     28.3     28.8     29.6     30.8     31.5     31.8     31.8     33.7     34.3     35.6     27.       35.3     35.4     34.7     34.3     33.9     33.9     33.9     34.5     35.1     33.9     33.7     33.8     35.6       37.9     37.6     36.3     37.1     36.5     36.4     36.5     36.2     36.3     35.6     35.4     35.6     36.3	07:	.	.	·	-,									26.20
35.3     35.4     34.7     34.3     33.9     33.9     33.9     34.5     35.1     33.9     33.7     33.8     35.6       37.9     37.6     36.3     37.1     36.5     36.4     36.5     36.2     36.3     35.6     35.4     35.6														27.10
37.9     37.6     36.3     37.1     36.5     36.4     36.5     36.2     36.3     35.6     35.4     35.6     36.3														35.75
27.20 27.12 26.85 26.73 26.40 26.25 25.80 25.30 24.79 24.94 24.57 24.41 26.														36.73
	27	20 27	12 26	85 26	.73	26.40	26.52	25.80	25:30	24.79	24.94	24.24	24'41	26.16

Vol. III.

						WET TH	HERMOME	TER.					
Göt: Ti	of Mean tingen me.	U	1	2	3	4	5	6	7	8	9	10	11
Tor	of Mean conto me.	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	35.4 33.2	35·2 32·9	35°0 32°5	34.5 32.7	34°4 33°4	34°3 33°4	34.5 34.9	34°1 35°0	。 33·2 34·7	33.0 33.0	° 32*4 33*5	32.0 33.0
	4 5 6 7 8 9	31.6 33.3 27.6 27.4 8.8 10.7	31.7 32.2 28.0 26.8 7.4 10.4	31.6 30.6 28.3 26.4 6.3 10.7	32·2 30·8 29·4 25·9 6·8 11·4	32.2 30.2 32.3 25.3 7.1 12.6	31.7 31.8 31.5 24.9 7.7 13.5	31.8 31.3 28.9 23.6 8.2 15.1	32.0 31.3 28.6 22.0 9.2 17.3	33°1 33°9 28°1 21°5 9°3 17°2	33.4 31.4 28.5 22.5 10.0 17.0	33.9 32.6 28.8 21.5 9.3 16.3	34.4 30.7 28.3 20.0 8.9 16.1
ANUARY.	11 12 13 14 15 16	-2.7 10.9 21.9 33.5 36.0 34.1	1'0 12'0 22'4 34'3 36'1 32'0	0°9 12°2 23°4 35°1 36°3 29°6	5.5 12.8 24.7 35.1 37.7 28.5	9°3 13°9 27°2 35°4 38°1 28°6	9'9 15'0 26'8 36'2 38'5 28'4	10.2 15.1 28.5 37.5 39.9 31.6	10'4 15'2 30'0 38'1 41'2 30'0	11.1 15.9 31.0 37.4 41.0 25.3	12.2 15.5 31.0 37.4 39.7 21.0	12·1 15·4 30·0 37·3 39·0 18·7	11'9 14'5 30'0 36'5 39'6 15'2
JAN	17 18 19 20 21 22 23 24	27.8 9.5 5.3 12.6 6.3 19.5	29·3 8·9 5·3 12·2 5·8 20·3	29.6 8.0 6.2 11.0 5.6 21.6	30.0 7.7 8.7 11.3 7.1 23.9	30.5 7.8 12.3 11.3 7.3 25.3	30.6 8.4 15.1 10.7 9.3 27.4	30.5 8.7 17.0 8.7 9.4 28.1	31.0 8.4 17.5 8.7 11.4 26.3	30.0 9.0 17.9 7.6 11.8 26.8	28.6 8.6 18.5 5.3 10.7 26.6	27.9 7.5 17.7 4.7 12.8 27.3	27.9 6.6 17.3 3.8 13.7 25.6
to soft .	24 25 26 27 28 29 30 31	16.4 24.9 11.4 3.6 20.6 19.6	16.7 28.5 11.5 4.5 22.2 19.6	17°1 32°0 12°1 4°5 23°1 17°5	19.0 32.0 13.7 8.1 23.6 17.6	22.0 32.7 13.9 11.1 25.5 17.3	22.8 33.9 13.7 15.5 27.9 15.1	23°2 33°9 13°3 18°3 28°8 15°1	23.4 31.4 13.7 19.2 29.2 15.4	23.6 26.8 13.6 20.5 29.4 15.4	24.0 25.1 13.0 21.3 28.8 14.6	23.4 24.1 11.8 20.7 27.9 14.0	22.8 23.8 10.5 19.5 27.4 12.8
Hourly	Means	19*97	20.58	20.28	21.18	22*19	22.82	23.31	23.46	23.27	22.75	22.33	21.65
ARY.	1 2 3 4 5 6 7 8 9 10 11 12 13	22:3 28:1 37:8 9:2 8:4 10:9 27:3 27:1 25:5 14:8 11:5 14:0	23·3 28·1 37·9 9·3 7·5 10·2 ————————————————————————————————————	23.5 30.4 37.7 9.0 7.6 11.1 ————————————————————————————————	24.4 32.2 37.3 10.2 9.2 13.2 — 28.5 26.6 26.6 15.4 15.1 16.1	26.4 36.1 37.2 11.5 11.0 14.7 — 29.8 28.1 28.2 18.5 18.8 18.5	29.4 36.2 37.1 13.6 12.4 17.0 — 31.6 29.6 29.6 28.7 18.9 20.6 20.5	31.0 36.3 37.3 15.3 15.7 19.4 — 32.0 28.6 30.0 18.9 21.1 20.7	31.6 37.2 37.6 18.3 16.3 21.6 — 32.1 29.2 31.8 20.0 22.8 21.3	31.6 38.0 34.4 18.9 18.9 23.0 — 32.1 28.4 32.0 18.8 25.1 22.3	31.5 38.0 31.2 19.8 19.2 24.1 — 33.1 28.3 32.0 18.8 21.3 22.3	31.7 36.8 27.4 19.4 19.9 24.5 — 32.0 28.4 30.8 18.8 21.9	30·7 36·4 24·1 18·1 19·8 24·0 — 31·0 27·6 28·6 17·3 16·8 21·7
FEBRUARY.	14 15 16 17 18 19 20 21	27.9 15.6 19.6 19.2 25.5 25.3	27·1 10·2 19·4 19·6 25·2 24·5	25°3 15°2 20°0 20°8 25°3 24°1	24·2 16·5 23·0 23·7 25·7 22·2	24.8 11.3 27.3 29.2 26.2 21.0	22.6 11.6 29.2 31.1 28.1 20.7	21 · 4 12 · 4 27 · 5 32 · 0 28 · 5 21 · 4	19.8 20.5 28.4 32.2 28.8 21.1	19°2 21°7 28°6 32°2 31°0 20°6	19°2 23°4 29°6 32°0 31°4 20°9	19.0 22.5 28.1 31.6 30.9 20.2	17.8 19.4 28.1 29.6 30.0 20.0
	22 23 24 25 26 27 28	13·3 1·0 0·1 15·2 6·2 25·9	13.6 - 0.4 - 0.9 14.3 7.6 26.1	13.8 1.2 3.6 14.6 14.6 27.6	14.4 3.6 6.8 17.9 18.9 26.8	15.9 6.0 12.0 19.6 23.5 27.7	17.7 8.0 16.1 20.7 24.5 28.7	17.5 11.0 18.9 21.8 24.8 29.4	18.0 12.3 20.6 22.0 24.9 29.5	18.1 13.4 20.5 23.3 24.6 30.7	18°5 13°9 20°6 23°1 23°6 30°7	18.8 15.1 19.9 23.0 23.2 31.7	18.5 14.6 19.6 22.0 22.4 32.0
Iourly	Means	17:99	17.60	18.49	19'94	21.80	23.11	23.87	24.91	25.31	25.27	24.75	23.75

					WET	THERMON	ÆTER.					,
12	13	14	15	16	17	18	19	20	21	22	23	Daily and
6	7	8	9	10	11	12	13	14	15	16	17	Monthly Means.
31.6 32.7 —	31·2 32·6	31·4 32·2	31·1 31·8 —	31.8 31.9 —	31.8 33.0	$\frac{\overset{\circ}{34.3}}{\overset{-}{24.7}}$	34°1 24°1	34.9  28.6	35·1 30·1	34.6  31.8	33·2 31·1}	33.51 31.94
34.4 31.4 26.6 16.6 9.2 15.9	36.2 32.0 27.9 15.1 9.1 15.6	35.8 31.8 27.3 14.3 8.8 16.0	38 1 31 8 27 4 14 0 8 3 15 7	38.9 31.8 26.8 13.7 7.5 15.2	40.6 31.0 26.4 12.3 7.6 15.1	39.0 31.0 26.3 13.0 7.9	37.4 30.3 26.3 12.6 8.7	36 · 2 31 · 0 26 · 4 12 · 0 8 · 8	35.5 28.7 26.8 13.4 9.1	35°3 27°9 27°3 13°2 9°5	$ \begin{array}{c} 34 \cdot 3 \\ 27 \cdot 5 \\ 27 \cdot 5 \\ 11 \cdot 8 \\ 9 \cdot 5 \\ -2 \cdot 3 \end{array} $	34.64 31.09 27.97 18.74 8.46 11.22
11.5 12.6 29.6 36.2 40.5 13.7	10.7 12.2 29.4 35.9 40.5 12.5	10.7 13.0 29.3 35.0 42.1 11.4	10.6 13.7 29.9 35.2 41.6 11.2	10.7 14.1 30.0 35.4 41.4 10.7	11.0 13.9 31.0 35.2 41.4 10.5	6°1 	4.7 11.0 19.2 33.4 34.5 39.7	2.5 11.5 19.6 33.5 34.2 38.5	- 1.7 11.4 19.5 33.9 34.6 37.4	- 1.9 11.4 21.1 33.3 35.4 36.0	10°9 21°9 33°3 36°3 34°5	9°27 15°10 29°40 35°62 39°04 22°07
27.9 6.5 17.1 3.6 13.1 25.1	28.4 5.8 16.6 2.3 12.1 23.9	27.1 5.7 16.3 3.2 13.3 23.0	26.8 5.9 15.4 4.6 14.2 21.6	25.4 6.0 15.5 4.7 16.2 20.5	23.7 6.1 14.2 4.5 17.2 20.5	20°3 21°6 6°1 13°1 4°6 17°5	20.9 18.7 6.1 12.4 4.8 17.7	22:0 17:1 5:9 13:1 5:2 17:6	23.5 15.2 5.9 13.0 5.2 17.4	24.3 12.5 5.6 12.8 5.8 17.7	$\begin{bmatrix} - \\ 25 \cdot 9 \\ 12 \cdot 2 \\ 5 \cdot 4 \\ 13 \cdot 0 \\ 5 \cdot 8 \\ 19 \cdot 1 \\ - \\ 15 \cdot 6 \end{bmatrix}$	25 '43 7 '09 13 '80 6 '76 12 '68 22 '05
23·2 23·9 8·5 19·0 27·3 10·8	23 · 2 21 · 8 7 · 0 17 · 3 26 · 8 9 · 8	24·2 21·6 5·8 17·5 26·3 9·2	24.7 19.6 5.2 17.0 25.5 9.2	25.4 19.2 4.4 15.9 24.7 9.2	24.4 19.8 4.3 19.0 23.1 9.2	15.9 23.5 19.9 4.1 17.1 21.3 —	15.9 23.3 17.1 3.6 17.9 21.1 — 19.6	16.2 26.4 15.4 3.2 18.6 21.6 — 19.8	16.2 26.7 15.2 2.1 19.1 21.7 — 20.5	16.0 25.9 13.8 2.8 19.2 21.8 —	$ \begin{array}{c} 13 & 6 \\ 24 & 6 \\ 12 & 8 \\ 2 & 7 \\ 19 & 8 \\ 21 & 0 \\ \hline 21 & 4 \end{array} $	22.91 23.72 8.58 16.01 24.86 15.66
21.10	20.60	20°47	20:38	20.27	20.27	20.32	19.81	19 <b>.89</b>	19.83	19.78	19.57	21.08
30.7 37.5 21.5 17.0 19.6 22.5	30.6 37.9 18.9 15.9 19.0 20.7	30.8 37.4 16.9 15.6 17.9 20.1	30°0 37°0 16°2 14°5 17°4 19°0	29'4 36'9 15'0 13'7 16'7 18'3	29'4 36'7 13'7 13'2 15'7 18'5	30°1 37°4 14°1 12°6 15°5	28.6 37.1 14.2 12.0 15.5	27.4 37.2 12.6 11.5 13.5	29°2 37°4 11°8 11°2 13°2	29.4 36.9 11.0 10.7 11.8	28.5 36.7 9.5 9.5 11.0	28*81 35*83 24*68 13*75 14*69
30.6 27.2 27.9 17.0 16.0 21.6	30.6 26.3 25.5 16.2 15.3 20.4	30.5 26.4 24.9 15.4 14.8 20.6	31.3 27.2 22.0 14.7 14.3 20.1	31.4 27.6 18.5 15.5 13.5 20.1	31.8 26.4 16.0 16.0 8.2 20.3	19:0 31:8 27:5 14:3 15:9 8:7	24.4 31.0 23.2 11.5 15.6 11.0	25·2 30·7 21·1 10·3 15·6 12·4	25.9 30.5 19.4 13.6 14.7 14.2	25.7 30.8 22.0 14.0 12.8 15.4	24.9 28.8 24.6 14.2 10.7 15.4	19'91 30'56 26'31 23'25 16'21 15'70
17.7 19.6 26.6 28.3 29.7 20.0	17.3 21.3 24.5 28.4 29.5 20.0	16.7 21.1 22.6 27.5 29.3 19.6	16:1 22:2 20:2 26:3 29:3 19:4	14.7 18.7 17.9 25.9 29.2 18.9	13.8 17.7 17.5 26.3 28.6 19.0	29'4 13'8 17'6 15'1 26'3 28'3	29°3 14°3 18°4 14°4 26°1 28°3	29.4 16.7 18.0 14.7 26.1 28.1	29.6 17.4 18.0 14.7 26.3 27.2	28.8 16.8 18.4 17.3 25.5 26.8	$\left\{ \begin{array}{c} -1\\ 28.5\\ 16.8\\ 18.1\\ 18.5\\ 26.7\\ 25.9\\ -13.7 \end{array} \right\}$	21'87 19'18 17'89 22'20 27'20 28'20 19'46
18.1 8.0 19.0 18.9 23.6 33.1	17·1 2·5 18·9 12·8 23·4 32·9	14.7 1.2 20.1 9.5 24.1 32.0	13°1 3°2 19°6 10°7 25°6 31°2	8.6 4.0 18.7 10.3 26.1 30.8	7.7 2.0 18.7 9.5 26.6 30.3	16.0 6.9 - 1.3 19.2 9.5 27.1 - 19.1	15.6 5.4 0.8 18.7 9.3 27.3	14.8 4.7 1.2 18.1 6.8 27.1 — 17.9	14.0 3.8 1.6 18.1 5.8 27.2 — 18.5	14.1 2.9 0.6 17.8 5.8 27.2 — 18.3	13.73 1.9 0.1 17.4 8.4 27.2 	12.63 5.15 15.92 14.78 22.97 26.91
22.99	21.91	21.24	20.86	20.02	19:32	18.81	18.72	18:38	18.47	18:37	18.11	21.00

		-				WET TH	ERMOME	TER.					
Hours o Göttir Tim	f Mean	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean	18	19	20	21	22	23	0	1	2	3	4	5
	7 1 2 3 4 5 6 7	18°5 17°4 21°6 13°0 12°1 27°1	18.6 17.1 25.1 13.3 9.8 27.8	19.8 19.2 26.4 20.2 12.6 30.3	20°8 20°7 27°9 23°8 17°7 30°5	20°8 21°1 29°4 24°5 23°6 32°0	22.6 22.0 30.8 25.1 26.0 32.7	24.6 24.6 32.4 26.8 26.2 32.5	26.5 27.1 31.1 28.1 27.3 32.3	27.4 26.8 31.8 29.4 28.2 31.8	25.8 26.4 31.7 29.4 27.9 31.4	25.1 26.3 32.0 28.8 27.9 31.4	24.5 24.2 32.0 28.4 27.4 32.5
	8 9 10 11 12 13 14	23.5 16.4 21.9 14.0 5.7 8.9	23·2 16·5 22·5 14·3 6·3 8·7	25°3 16°5 26°2 15°9 9°9 11°1	26.5 18.6 28.6 17.1 13.8 13.3	28.4 19.9 31.0 17.7 14.7 15.6	31.7 19.9 31.0 18.3 15.9 17.6	32·2 19·7 31·2 20·2 16·7 19·4	33.5 19.4 31.0 19.7 17.1 20.4	28.9 19.3 31.9 20.0 18.3 21.7	28.5 19.6 32.7 19.8 20.2 23.0	27.3 19.7 33.8 18.6 19.8 21.5	27 · 2 19 · 9 33 · 5 18 · 1 19 · 2 21 · 3
MARCH.	15 16 17 18 19 20 21	11.9 9.0 13.7 27.3 22.2 30.4	13.3 9.2 15.2 27.9 23.5 31.0	14.7 11.6 18.1 30.0 25.3 31.2	16.0 13.2 22.6 31.5 27.1 32.4	17.3 15.9 23.9 30.6 29.4 34.1	20°1 16°6 27°8 32°2 30°6 34°2	18°3 19°4 29°2 33°3 32°0 35°6	20.6 18.1 29.4 34.1 32.2 36.5	21 · 1 21 · 2 29 · 2 35 · 5 32 · 1 35 · 4	19.8 20.9 29.4 35.6 32.1 35.6	19.2 20.4 29.2 36.5 32.0 35.4	19.0 20.2 28.4 37.3 30.4 35.4
	22 23 24 25 26 27 28	24.5 22.2 26.0 30.7 27.3 16.7	25.9 33.0 26.8 30.4 27.8 15.5	27.9 33.1 27.8 35.3 28.0 15.7	29.2 33.3 29.7 38.5 28.4 17.1	29.8 34.3 29.8 38.1 28.9 19.0	30.0 35.3 31.8 38.1 30.3 20.3	30.5 37.8 31.4 37.9 31.6 21.1	29.6 36.6 31.4 35.4 31.9 21.5	29.9 37.1 31.9 35.8 34.5 21.9	30.0 36.2 32.7 35.8 32.7 22.2	30·1 35·2 33·2 35·4 33·3 22·2	30.6 34.7 31.7 36.5 32.5 22.2
	29 30 31	29·4 21·2 11·6	30.9 21.2 14.4	32·3 23·9 15·2	35°3 23°3 15°0	37.9 23.7 16.9	38°2 24°3 17°9	36.7 23.7 19.8	37·1 22·6 21·2	34.4 22.9 22.3	32.7 23.0 22.1	31.4 21.6 21.9	29.8 22.3 22.3
Hourly	Means	19.78	20.34	22:35	24.14	25*49	26.71	27.59	27.84	28.17	28.04	27.75	27:46
APRIL.	1 a 2 3 4 5 6 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30												
L													

^a No reliable observations for this month.

						WET THE	RMOMET	ER.					
ours o Göttii Tin	f Mean	0	1	2	3	4	5	6	7	8	9	10	11
ours o Toro Tir		18	19	20	21	22	23	0	1	2	3	4	5
	$\left( egin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \end{array} \right)$		° - 41.6 42.6 44.3 45.4 45.6	°		° - 47.8 49.4 49.1 50.2 48.4		948.2 50.7 52.6 51.9 47.8	- 46.9 51.2 52.5 52.1 48.6		- 45.8 50.1 50.6 50.0 52.5	- 45'9 50'3 49'7 49'8 52'5	- 46.2 - 47.5 51.6 51.9
$\max_{\widetilde{\Lambda}} Y.$	9 10 11 12 13 14 15	45.4 52.0 53.6 52.8 48.8 46.2	47.8 52.0 54.4 54.2 52.0 50.8	50°2 53°1 57°1 54°7 54°6 54°9	51°1 57°0 58°2 53°7 53°1 56°8	52.7 58.6 59.8 53.3 51.4 56.7	53.7 59.4 60.7 52.3 52.2 58.6	53°5 57°9 61°7 52°7 51°3 58°6	54·1 57·8 60·8 54·7 50·4 58·8	56.0 57.5 59.1 54.9 50.8 59.0	55°9 58°5 59°0 55°7 52°5 59°1	57.0 56.2 58.8 56.2 52.4 57.9	55.7 56.3 58.6 55.9 54.8 57.1
M	16 17 18 19 20 21 22	43.9 44.7 47.3 45.3 46.5 56.3	48.3 49.4 49.4 47.1 47.7 59.4	53.8 52.9 51.8 49.0 48.4 57.8	55°3 57°4 53°9 51°8 50°1 59°6	55.4 57.8 59.4 51.9 49.9 61.9	55°5 57°8 57°1 52°4 51°8 64°1	54.9 59.1 56.6 53.1 53.9 63.5	55.8 60.2 58.0 53.7 56.4 60.8	54.7 58.0 58.3 53.9 56.8 62.7	54·1 58·3 57·1 53·4 57·4 62·9	54.2 58.2 57.3 53.3 54.4 60.9	53°3 58°5 58°5 51°8 52°7 58°6
	23 24 25 26 27 28 29	55°1 50°2 36°6 44°6 50°6 54°7	56.7 52.8 38.3 48.8 51.2 52.9	57·1 55·9 40·3 50·6 53·4 53·7	56.9 59.2 41.9 50.4 53.4 59.1	57.5 59.1 43.0 52.3 58.6 57.0	58.4 59.9 46.1 53.6 61.4 57.5	58.7 58.4 47.7 53.0 64.8 55.9	60°6 60°9 47°6 51°5 64°0 56°4	62.0 60.8 48.0 53.1 64.2 59.0	61.6 59.3 50.0 52.4 62.0 61.7	61.8 56.7 51.4 52.7 60.9 58.0	61.4 58.0 50.6 53.6 61.7 62.8
	$\begin{bmatrix} 30 \\ 31 \end{bmatrix}$	47.8	47.0	47.0	46.2	45.3	44.8	44.2	44.0	43.9	43.8	44.0	44.0
Iourl	y Means	46.68	49.15	51.17	52.70	53.60	54.37	54.61	54.91	55.29	55.12	54.60	<b>54</b> .8
	$\left(egin{array}{c c}1\\2\\3\\4\\5\end{array} ight]$	45.6 50.6 48.2 53.0 40.1	45.6 50.6 54.1 54.2 42.0	48.2 51.6 54.7 55.8 45.4	52·2 52·0 54·6 54·1 46·3	54.9 53.9 55.2 54.2 48.4	59°2 55°3 56°6 55°1 50°5	59.8 56.9 59.2 53.1 52.4	58.2 58.7 58.7 53.5 54.9	57.8 56.5 55.8 52.0 5 <b>5</b> .5	54.6 56.5 56.4 51.0 56.9	56.1 56.4 55.3 49.0 54.2	56°5 57°2 53°5 48°0 54°1
	6 7 8 9 10 11 12	47.8 52.1 55.9 61.8 57.4 46.7	51.4 51.4 57.8 62.0 60.0 48.8	56°3 51°4 60°6 63°0 62°6 54°7	58.5 52.6 63.5 63.0 64.6 56.3	58°2 55°4 63°8 62°4 62°0 55°6	59°2 55°2 65°0 62°0 63°6 56°3	59.8 54.8 65.6 62.6 61.0 56.6	61.2 54.9 68.5 62.5 62.1 58.0	61:3 57:1 69:6 63:2 59:0 58:5	61.4 58.0 69.3 64.0 58.5 58.9	58.5 56.8 69.6 62.0 57.8 60.0	56.5 55.1 67.0 62.2 53.1 <b>5</b> 9.6
JUNE.	13 14 15 16 17 18 19	54.5 38.0 43.2 46.8 49.0 55.3	53·2 39·1 44·9 48·4 53·3 55·3	48.6 40.1 46.3 52.4 53.3 57.2	49°0 41°2 47°5 55°9 55°4 59°3	47.4 42.8 48.6 55.7 56.0 61.6	46.7 43.9 49.6 56.2 57.8 61.2	45.0 44.9 49.7 57.5 59.0 60.6	43°2 47°6 49°0 57°2 61°0 60°8	42.2 50.4 48.8 56.9 58.0 57.4	44.7 52.0 50.3 58.0 57.2 58.7	44.0 52.3 50.6 58.3 56.4 61.2	44.4 51.8 50.6 57.3 56.3 62.8
	20 21 22 23 24 25 26	53.8 52.5 55.1 55.5 56.7 61.6	56.4 53.9 58.2 60.6 61.5 63.7	59.7 52.5 59.6 62.8 60.5 67.9	61.0 57.4 63.0 64.5 62.6 69.7	61.5 59.6 63.4 66.4 62.8 70.1	61 · 2 63 · 0 65 · 4 68 · 4 62 · 6 72 · 3	62:3 63:8 65:4 65:9 64:0 70:9	62·2 64·6 65·5 63·8 64·8 70·7	57.5 64.0 65.0 65.0 65.0 69.5	60.7 60.4 65.4 67.1 66.6 70.3	62.9 58.5 64.8 66.2 65.1 69.1	62.8 60.1 62.8 66.5 60.4 69.1
	27 28 29 30	58.7 54.3 53.9	58.7 55.5 57.4	56.7 56.1 61.7	58·1 58·0 62·8	59.2 59.0 63.4	59°3 60°3 62°0	62.0 60.6 64.2	66°3 61°4 65°1	61 0 63 0 65 0	60.8 63.2 64.0	63.9 63.0 63.0	61.5 63.6 63.0
ourly	y Means	51.85	53.77	55.38	57:04	57.75	58.77	59.14	59.78	59.04	59.42	58.97	58.3

					WET	THERMO	METER.					
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
<u> </u>	-	<u>-</u>	0	<u> </u>	<u>-</u>	<u>.</u>	°	<u> </u>	°	<u> </u>	0	<u> </u>
	=		_	_		_	'-	<u> </u>	_	_	_	
44.7 46.7	43°5 44°5	42.9 44.3	41.3 41.8	39 <b>·</b> 5	38.0 38.8	36°5- 38°1	38.7 36.5	38°1 35°8	36°2 35°5	33.7 34.6	31.9 34.7	41.98 43.20
46.6 49.8	44.9	43.7 45.9	42.8 44.2	42.8 43.8	41.7 45.6	40.7 46.1	39 <b>·</b> 9 46 <b>·</b> 7	39°1 47°1	38°3 49°9	37.7 $52.2$	$\begin{array}{c} 36.6 \\ 52.7 \end{array}$	45.00 48.50
50.2	49.9	49.5	49.3	49 <b>°</b> 6	48.9	<del></del> 47.7			49.6	47.3	$\frac{-}{44\cdot 7}$ }	48.70
53°8 56°1	54.7 53.0	53.6 52.5	52 <b>·</b> 9 53 <b>·</b> 1	52°1 53°1	54°3 53°5	54·4 53·7	53.3	52.9 $53.1$	$\begin{bmatrix} 51.2 \\ 52.7 \end{bmatrix}$	$\begin{bmatrix} 52.7 \\ 53.7 \end{bmatrix}$	53.3 55.0	53°04 54°96
57.8 55.7	58.4 54.2	58.4 53.0	58.6 50.0	57.8 49.0	57.8	55.7	56 <b>·</b> 5 47·3	55°4 47°0	$\begin{array}{c} 53.9 \\ 46.7 \end{array}$	51 4 46 4	52.9 45.7	57:35 51:77
51.4	52.1	49.6 52.6	48.4	46.9	48.5 46.7	47.8 44.6	43.0	42.4	41.3	41.6	40.9	48.88
_	55.9		49.8	49.4	49.2	45.7	45.9	45.4	43.5	42.4	41.1	52.15
52.0 57.4	50.6	51.0 50.8	50°6 49°6	49 <b>°</b> 6 49 <b>°</b> 3	$\begin{array}{c} 47.7 \\ 48.2 \end{array}$	47.5 48.0	$\begin{array}{c} 47.2 \\ 47.7 \end{array}$	44'9 47'8	43 · 3 47 · 8	42.6 47.2	42.4 46.7	50°36 52°68
59 <b>·</b> 9	55.0 50.7	52°2 50°0	50°3 47°8	50°0 46°9	49.5 45.9	48.5 44.9	47 <b>·</b> 9 44 <b>·</b> 6	47°1 43°2	46.1 42.9	45.4 42.6	45.9 43.6	52.60 48.79
53.8 57.8	51.7	53.1	48.2	47.4	50.8	50.7	52.9	51.5	51.6	52.4	53.6	51.81
_	58.1	57·7 —	57 <b>·</b> 9	56·7 —	55°5 —	52.4	51.0	51.0	51.5	51.1	53.5	57.60
60°2 57°9	58.6 58.2	57.8 57.3	55.5 54.8	55°3	$\begin{array}{c} 52.9 \\ 44.2 \end{array}$	51.6 41.9	49°2 40°1	48.6 38.2	48.4 37.3	47°1 36°4	$\begin{array}{c} 48.1 \\ 35.2 \end{array}$	55.87 52.00
49.8	45.5	44.6	43.5	42.4	40.8	39.4	39.1	39.7	39.2	36.4	37.0	43.30
52.9 61.7	50.7 57.9	49°0 57°1	47.6 58.0	46 <b>·</b> 9 58 <b>·</b> 3	45°5 56°9	45°0 56°7	43.5 56.7	42.6 55.0	42°2 55°5	44°0 55°5	45°1 55°2	48.82 57.95
58.4	55.3	54°1	54 <b>°</b> 0	52 <b>·</b> 9	53.1	45.7	45°3	46.6	47.4	48.5	$\frac{-}{48.7}$	54'11
44.6	44.6	44.6	45.6	46.0	46.6	47.1	46.8	46.9	47.0	47.4	47.2	45.70
53.61	51.91	51.05	49.82	49.19	48.28	47.10	46.71	46.12	45.79	45.43	45.49	50.43
55.5	55.3	53.7 52.5	52.8	52.3	51.2	50.6	49.2	48.8	48 <b>·2</b> 44 <b>·</b> 8	49°8 43°8	50°2 44°4	52.76 51.72
56.4 53.9	53.7 53.0	52.7	$51\cdot 3$ $52\cdot 7$	50°9 51°2	48°3 51°6	47.5 52.5	46.5 $52.3$	44.9 53.1	53.1	52.7	52.5	53.90
47.8 52.7	46.9 52.7	45°1 50°0	44 <b>·</b> 2 48 <b>·</b> 4	42.8 46.0	$\begin{array}{c} 42 \cdot 0 \\ 44 \cdot 2 \end{array}$	40.7	40.0	37.4	36.1	35.1	34.7	46.91
-	_	_		_	52.3	46.5	46.3	44.7	44.0	42.4	$\frac{-}{42.6}$	48°38 54°70
53.8 54.3	52°5 54°1	52°3 53°9	52°0 53°9	51.5 54.7	54.3	51.6 54.3	51.6 54.3	50°6 55°4	51 <b>·</b> 2 53·3	51'4 52'9	51.9 52.9	54.29
67°1 61°2	67.5 61.0	65.6 59.8	62°4 60°1	63°1 58°8	64.4 58.2	63.5	61.7 60.4	61·1 59·8	60.8 59.8	59°8 57°4	59.6 56.5	63.87 60.96
50.6	48.5	49.0	48.0	47.9	48.2	48.0	47.7	47.5	46.3	45.1	44.9	53.89
59.3	56.6	53°1 —	52·7 —	52·2 —	51°5 —	51.3	51.1	50.7	50.7	50.9	50.7	54.50
44·1 51·2	43.5 49.6	41.5 47.7	39°5 46°1	38.6 44.8	38.0 44.6	37.8 44.6	37.5 44.2	37.6 44.7	37.6 43.3	37·2 42·3	37·4 42·1	43.05 45.39
50.4	50.6	50.6	45'1	44.6	44.3	43.3	43:3	42.6	42.3	40.5	41.7	46.60
56.2 55.7	56°1 55°9	50.7 56.8	47 <b>·</b> 9 57·7	45°7 57°4	45°2 57°9	$\begin{array}{c} 43.9 \\ 57.8 \end{array}$	43°0 56°0	41.7 56.1	41°3 56°2	42 <b>·</b> 8 55 <b>·</b> 9	44 <b>.</b> 9 55.9	50.83 56.33
62.2	55.6	53°7 —	52.0	50 <b>.</b> 6	50.2	<u></u> 52.5	51.1	51.4	50.6	<u> </u>	50.6}	55.94
61.8	58.0	56.2	55.2	55.3	54.9	53.9	52.1	50.6	49'1	48.8	51.1	57.04
59·9 62·9	57.9 60.7	56°1	55°0 57°8	54 <b>·</b> 9 57 <b>·</b> 0	54°0 56°9	53.7 54.3	53°7 52°3	53°4 50°6	53°3 49°8	49°0 50°0	50.6 50.2	56.74 58.96
65.6 62.2	64.0 60.0	63 <b>·2</b> 59·6	56.5 57.3	54°7 57°0	54°3 58°5	53.2 59.6	52.5 $60.3$	51.8 59.9	51.8 60.1	51.4 59.6	53·1 57·8	60°20 61°02
66.8	65.2	65.0	65.8	64·3	62.2						57·5}	65.59
60.9	59.4	56°6	56.2	<u> </u>	<del></del> 55·4	66°6 54°6	64°0 54°0	57 <b>·</b> 9 53 <b>·</b> 2	57°3 53°1	56.7 53.4	57.5 S	57.85
59·9 61·8	58.8 59.8	55.7 56.2	53.7 54.3	53.9 52.9	53·3 51·8	51.4 50.8	50.6 49.0	50.6 48.1	50.6 47.5	50°2 47°2	50.9 48.0	56.57 57.24
57:47	56.01	54.47	53.02	52.24	51.83	51.68	50.95	50.16	49.70	49.12	49.45	54.81

	<del>- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1</del>			·····		WET TH	IERMOME	TER.					
Gött	of Mean ingen me.	0	1	2	3	4	5	6	7	8	9	10	11
Hours o	of Mean onto	18	19	20	21	22	23	0	1	2	3	4	5
	$\left[\begin{array}{c}1\\2\\3\end{array}\right]$	51°1 54°4 58°2	54°5 58°8 62°8	57°4 62°0 68°3	61°.4 67°.5 68°.9	66°0 67°0 70°0	65°0 66°6 70°4	66°5 67°7 69°6	66°5 69°0 70°3	65.5 68.7 70.8	64.2 69.0 70.2	64.2 69.3 70.9	64.6 69.7 71.6
	4 5 6 7 8 9	60°2 62°4 62°9 65°5 65°4 64°8	62.6 64.8 64.3 68.3 68.3 66.6	65.0 64.6 65.3 71.0 70.9 67.3	70.6 65.8 69.4 73.7 72.2 68.7	71.0 66.6 70.0 71.9 72.0 69.4	70.4 68.3 72.0 73.7 74.3 70.7	71.4 69.3 72.5 73.5 73.0 69.8	71.4 71.5 72.5 73.7 73.2 71.1	71.4 73.6 73.0 72.1 72.6 71.5	71.7 72.7 73.2 71.9 72.1 70.5	67.1 75.6 72.4 71.1 70.0 70.1	65.9 70.0 73.5 71.9 69.1 68.7
JULY.	11 12 13 14 15 16 17	66.6 66.2 52.9 53.3 63.0 67.9	70.7 69.7 54.7 56.5 66.3 68.4	71.9 70.4 56.7 59.8 68.4 69.9	72.7 73.3 58.2 62.7 69.8 72.5	73.5 72.1 58.6 65.0 71.5 74.7	74.7 72.7 61.0 66.2 72.1 75.1	73.6 72.9 61.0 68.1 71.9 76.1	76.2 72.3 62.8 68.9 73.1 74.7	77.0 70.3 62.0 68.4 72.5 76.1	75.7 68.7 60.4 68.9 71.9 72.7	74.1 67.7 61.0 68.3 71.7 74.3	72.7 65.6 60.8 67.3 70.5 74.9
	18 19 20 21 22 23 24	70.0 69.1 68.5 68.1 51.7 57.3	73.7 72.0 71.2 66.4 56.6 60.8	76°2 74°2 70°3 66°4 61°1 64°4	75.9 73.5 71.4 64.7 64.2 65.6	77.2 75.1 73.5 64.8 64.4 64.4	78.2 73.3 74.7 64.8 64.8 64.8	78.8 74.9 73.9 66.5 64.8 64.8	77.0 75.1 74.4 67.9 63.9 64.2	74.9 74.7 75.5 65.8 63.0 65.3	77.2 76.1 73.5 66.0 65.0 66.6	77.0 73.3 73.3 65.6 66.6 65.6	76.4 72.7 72.5 65.6 66.2 64.0
Aug	25 26 27 28 29 30 31	56.1 47.7 48.5 55.7 55.0 50.6	54.9 50.2 52.9 59.1 57.9 58.4	53°5 52°1 55°5 60°6 58°3 60°6	51.8 54.7 57.3 61.9 58.3 62.0	52.0 55.3 59.8 62.7 62.2 63.4	52°1 56°1 58°2 63°9 60°3 63°3	52.0 57.3 56.7 64.0 60.8 65.0	55°3 57°3 59°0 63°4 60°3 62°2	53°5 56°2 57°5 63°6 62°0 62°2	53°3 56°1 57°2 65°7 62°8 62°3	53.7 57.3 57.7 63.6 62.6 62.8	52.7 58.2 56.5 63.1 62.8 59.6
	Means	59.74	62.64	64.2	66.25	67:11	67.69	68.01	68.41	68.14	67.99	67:29	66.93
	( 2 3 4 5 6 7	51.2 53.3 56.7 57.9 60.5 55.7	57:3 58:2 61:0 61:1 61:7 55:9	60°0 59°4 65°3 64°4 64°0 58°2	61.8 63.1 64.8 66.6 66.3 60.0	63.4 62.6 64.0 66.5 69.9 62.6	64·4 62·4 65·7 65·7 69·7 66·0	64.4 63.0 66.0 66.4 69.9 65.9	65.8 62.8 65.8 66.6 69.1 66.0	64.0 62.0 67.2 66.6 68.7 64.7	64.9 62.7 67.5 65.4 69.4 64.1	66.4 64.8 67.1 65.2 66.8 65.2	62.8 65.8 66.8 64.4 64.0 63.9
_•	8 9 10 11 12 13 14		62.8 65.8 66.6 58.4 65.4 68.3	63.6 67.2 68.1 63.4 70.1 69.9	65°0 69°6 67°4 66°5 69°7 71°4	65.4 71.8 67.7 70.1 71.1 73.7	66.6 72.1 69.7 70.3 70.7 73.7	68°1 71°7 70°2 70°4 69°7 74°0	69.7 72.0 70.7 70.7 69.2 75.1	69.7 72.5 68.5 70.7 71.1 72.7	70.6 70.9 65.6 70.3 69.2 74.7	69.6 70.9 66.6 66.8 69.5 72.7	69°1 70°3 66°6 68°1 69°4 72°7
AUGUST.	15 16 17 18 19 20 21	67:1 64:3 53:7 44:9 52:1 50:6	69 · 4 71 · 3 55 · 5 47 · 7 55 · 7 52 · 0	70°5 72°1 55°5 51°4 58°1 54°6	71.0 72.6 56.1 50.6 59.0 57.1	70°2 73°3 56°3 53°1 60°7 56°6	74.3 70.7 55.9 52.3 61.5 57.3	74.0 71.7 56.7 53.2 62.6 58.2	74.2 69.2 58.0 53.4 61.0 58.9	73.7 70.1 57.3 53.9 61.2 59.9	73.7 69.5 58.0 55.4 59.8 60.2	74.7 68.5 55.7 54.4 62.6 59.2	75·1 69·3 53·3 53·9 57·8 61·2
	22 ·23 ·24 ·25 ·26 ·27 ·28 ·28	50.7 51.0 50.4 52.5 54.5 46.5	55.2 54.9 54.1 56.9 54.8 52.0	58.0 57.2 61.2 61.0 55.1 58.5	58.8 61.0 63.5 63.9 56.1 60.8	57°3 61°6 64°6 65°0 55°9 61°8	59°2 62°4 64°4 68°7 56°8 60°8	61.0 63.8 63.2 66.9 57.3 61.4	62.0 62.6 62.4 69.1 57.8 60.0	63.0 62.1 62.7 68.3 59.0 60.9	64.8 61.4 62.2 69.0 59.1 60.0	63:3 61:5 61:0 68:1 59:3 61:2	63·1 62·0 60·8 65·8 60·2 62·3
	29 30 31	58.0 50.0	63.0 52.7	63.6 54.0	66.0 52.5	66.3 53.7	66.8 53.2	66.0 54.2	66.2 54.8	65°8 54°7	64.6 56.7	62.8 56.8	63.0 55.7
Hourly	Means	56.14	59.14	61.71	63.12	64.05	64.68	65.01	65.13	65.04	64.99	64.64	64.13

					WET	THERMO	METER.					
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
63°6 69°4	61°6 64°8	58°6 62°0	55°.7 60°0	53°9 59°1 57°1	53°6 58°3 56°6	53°3 56°5	52°6 55°9	53°5 55°3	53°2 54°8	52°6 53°3	51°2 53°5	58.75 62.19
70°5 66°6 68°8 70°7	66°3 67°8 68°5	64.2 66.4 64.6 66.4	59.6 	65°1 62°6 64°0	63.8 62.4 63.7	57.0 64.2 63.0 64.5	56.5 63.2 61.6 63.5	55°9 62°6 60°4 61°1	55.5 62.6 61.4 60.8	55°3 62°2 60°6 61°8	$\begin{bmatrix} -55.4 \\ 62.0 \\ 60.9 \\ 61.8 \end{bmatrix}$	63°87 66°22 65°95 67°18
70.9 69.3 68.8	71.6 68.5 66.6	68.5 66.8 67.2	66.6 66.6	65.7 65.8 66.6	66.0 65.2 66.0	65.7 65.2 — 66.4	65°1 64°8 — 65°6	64.8 62.8 64.8	63.4 65.6 — 64.6	62.8 65.2  64.2	$63.1 \\ 65.0 \\ \hline -64.2$	68.83 68.62 67.53
74.3 64.0 62.2 66.7 68.3	73°1 61°4 59°4 66°2 70°5	70·3 59·6 56·7 65·8 67·3	68'3 58'4 54'7 65'8 66'5	66.8 57.5 53.1 65.9 66.4	66.6 56.8 52.0 64.3 66.0	66.8 56.3 50.8 64.0 66.2	66°2 55°4 50°4 59°6 66°4	64.5 54.0 49.8 59.8 66.3	62.1 53.1 49.4 58.6 64.8	62.4 52.1 51.1 58.2 64.6	64.5 51.7 50.6 57.9 65.8	70°22 63°43 56°26 63°59 68°41
76°3 	76.3 	72·9 — 68·9 69·5 67·3	72.1 	72.5 — 67.3 69.8 65.6	72·3 — 67·9 69·3 64·6	68.5 68.1 69.2 65.2	66°3 66°6 68°7 65°3	67:5 66:7 67:6 65:0	66.5 67.0 68.7 66.1	65°9 66°8 67°6 66°5	66.0 66.4 67.7 67.3	71.68 72.59 71.36 69.58
64.0 65.6 63.6	61.7 62.8 63.0	59.8 60.0 62.5 — 50.7	59.0 57.5 63.0 — 48.6	56°3 56°1 63°6 — 46°5	54.6 55.4 64.0 — 45.2	53°1 54°5  64°8 44°9	51.2 54.5 — 67.1 44.6	50°5 53°9  67°4 44°0	49.6 53.0  65.7 43.9	47.8 52.6 — 59.0 42.2	$     \begin{array}{c}       47.8 \\       52.9 \\       \hline       56.5 \\       42.6     \end{array} $	60°33 59°59 63°67 49°87
51.8 58.1 53.7 62.8 62.6	50.9 56.1 55.3 61.8 61.0	52·3 53·7 61·4 59·0	50°3 51°4 61°0 58°6	49.8 51.0 61.8 57.1	47.5 50.6 61.0 55.9 53.6	46.9 50.6 60.0 54.9	47·3 51·4 58·0 52·4	45.9 51.4 57.2 53.0	45.9 50.2 55.0 49.8	45.4 48.8 54.5 48.0	44.6 48.2 54.2 47.8	52.03 53.88 60.67 57.64
59.4	55'4		56.6 —	55.0		53.6	53.5	52.4	50.6	50.0	50.0}	57.21
66.5		62.98	61.61	60.81	60.12	59.79	59.01	58.22	57.85	57.09	57.02	63.39
63.8 65.0 66.8 63.4 62.0	62.1 62.8 65.8 62.6 62.8	58.7 59.0 61.2 61.2 63.6	57 1 55 5 57 5 60 0 63 2	56.7 53.3 56.4 60.0 63.4	53.7 53.1 55.7 59.6 63.2	53 1 52 3 56 1 60 2 64 8	49.8 52.3 55.1 61.0 64.0	49.8 51.4 54.7 61.0 63.4	50°3 51°2 55°1 60°9 60°8	48.2 50.3 54.7 60.7 58.2	47.7 50.6 55.7 59.8 56.7	58°20 61°36 62°80 64°42
63.8 69.3 68.2 67.3 68.2 71.2	61.9 67.0 67.7 64.6 66.1 69.4	60°0 66°2 67°4 63°0 66°1 68°5	58.8 — 66.4 67.3 61.4 65.8 67.9	59°2 66°6 66°8 60°2 65°7 65°7	58.7 65.6 66.8 59.8 65.6 65.6	61:3 64:6 66:6 59:0 64:9 65:0	61.6 63.4 64.9 58.7 64.7 66.4	61.4 62.8 64.6 58.6 64.0 66.3	61.2 61.8 64.3 58.9 61.6 66.1	61.0 62.2 65.0 57.2 61.8 65.6	61.6 63.1 65.8 56.7 61.8 66.0	61.61 65.48 68.10 64.12 65.80 67.98
70·3 74·3 67·9 52·7 55·3	69.7 	68.1 	67.2 	66.2 65.8 59.9 48.2 51.1 55.1	66.2 65.2 59.5 47.3 50.9 53.7	65.6 64.8 57.0 46.8 51.8 54.0	64'8 63'8 55'5 45'9 50'6 52'7	64.4 64.1 53.8 46.3 50.0 52.5	63.4 63.6 55.0 47.3 48.6 51.4	63°2 64°1 55°6 47°3 49°2 50°2	63.6 62.4 53.7 43.0 50.0 49.4	69'06 69'28 64'84 51'94 51'63 56'55
58.2 60.0 61.6 62.1	56.7 59.0 — 58.4 58.0	55°9 55°2 — 55°5 55°1	55°3 54°1 — 54°7 53°9	53°5 — 53°3 52°6	52.4  52.1 52.8	49.8 50.9 52.5	49.8 51.0 52.1	49.0 50.9 51.3	49.0 50.7 51.3	48.8 48.7 49.8	$-\frac{1}{48.8}$	54.80 56.36 56.80
59.7 64.8 60.6 60.6	57.8 62.8 55.7 57.4	55.7 62.0 56.9 56.5	55°3 62°1 55°1 55°4	55°0 62°0 53°5 55°5	54.9 63.4 52.3 54.1	54'4 62'3 51'6 — 58'1	52.9 61.8 50.8 — 56.7	52°3 62°6 48°4 — 55°2	52.1 60.0 46.4 	52.2 58.6 47.0 — 54.9	50.6 54.5 47.7 — 54.9	57.64 63.00 54.66 57.50
62.6 55.2	61.2	59.0 50.0	58.6 48.2	57.8 47.3	56.0 47.2	54.2 46.9	53.6 45.9	52.7 44.7	49·2 47·1	48.6 47.3	47.8 48.8	59.74 51.30
63.6	6 61.75	60.02	58.89	58.11	57.53	57.25	56 <b>·5</b> 3	56.01	<b>5</b> 5.46	55.02	54.59	58.63

						WET T	HERMOM	ETER.					
Hours of Götti Tin	of Mean ingen	0	1	2	3	4	5	6	7	8	9	10	11
	of Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \end{pmatrix}$	49°8 48°9 56°8 53°7	50°8 54°1 61°9 53°7	54°4 59°0 63°1 53°5	55°9 61°7 63°1 54°2	58°4 63°5 67°1 54°7	59°5 64°0 69°1 55°2	59°8 63°6 69°1 55°2	60°2 63°4 66°9 55°7	59°·5 65°·4 69°·5 55°·7	59°2 66°0 68°5 56°3	59°6 66°5 66°9 56°3	60°2 65°4 61°2 56°8
	5 6 7 8 9 10 11	48.2 52.1 63.0 49.3 44.0 46.5	50°3 58°0 64°0 49°1 49°0 50°8	53°5 60°6 65°6 49°7 51°7 54°5	59°0 60°0 66°6 49°3 56°2 58°5	60°2 59°7 69°0 50°8 56°5 58°0		60.6 59.8 69.9 51.4 57.9 57.2	61.4 60.8 68.9 55.3 56.3	61.3 59.8 69.6 55.5 57.5 56.5	62.4 59.9 68.8 55.5 57.5 54.4	60°5 59°8 68°7 55°5 58°1 54°0	60°3 60°0 69°2 55°1 58°0 54°1
SEPTEMBER.	12 13 14 15 16 17 18	52.7 43.4 37.2 37.8 49.4 55.9	51.4 43.8 41.3 42.8 49.8 57.1	50.6 44.2 43.4 48.5 53.9 58.3	50°9 44°9 45°3 49°8 56°3 58°6	50.8 45.8 46.6 53.1 58.3 59.6	50°1 45°3 47°8 53°7 58°4 59°4	50°5 45°8 48°5 54°3 58°0 60°0	50.6 45.9 49.3 54.5 57.7 60.1	48.8 47.2 52.0 55.3 56.5 59.4	47.8 47.2 52.2 55.2 56.8 59.4	46.5 48.4 52.4 55.3 55.9 58.1	45.9 45.7 53.0 54.0 55.0 57.3
	19 20 21 22 23 24 25	53.5 50.5 44.2 49.6 52.7 47.1	54.0 52.6 47.5 52.3 52.5 47.5	54.7 54.0 50.6 56.9 52.5 48.5	54.7 55.1 51.6 59.0 52.5 50.7	54.9 55.5 56.3 59.7 52.9 52.6	55°1 56°3 56°3 61°6 52°7 53°9	55°3 57°3 56°0 61°5 53°7 56°0	55°5 56°2 54°9 62°2 53°9 55°2	55°1 56°3 54°5 62°8 53°7 54°6	55°1 54°9 53°9 61°8 53°9 54°1	54.4 53.7 55.5 62.2 54.0 53.7	55.7 53.1 55.3 62.3 54.1 53.9
	26 27 28 29 30	57°3 45°7 42°6 38°4	58°4 48°1 42°9 40°5	59°2 50°7 45°3 43°0	60°0 50°6 47°5 46°1	61.7 51.4 50.6 48.2	63°2 52°4 46°1 48°0	64.7 52.5 49.3 50.0	65°3 49°2 50°8 49°0	64.8 48.8 45.2 47.1	64.9 48.2 45.5 47.4	65°2 47°1 46°9 48°4	64.0 47.6 47.0 48.4
Hourly	y Means	48.86	50.93	53.07	54.24	56.00	56.30	56.84	56.79	56.63	56.42	56.29	55.87
	$\left(egin{array}{c}1\2\end{array} ight $	43°3 38°2	44°4 40°6	45.6 44.8	45°3 46°5	45°4 48°2	46.8 48.3	47·4 47·7	47·3 48·2	46.9 51.0	46°9 51°5	46.6 49.9	46°2 49°3
	3 4 5 6 7 8 9	40°3 56°6 55°8 54°2 54°9 39°5	43.7 57.6 55.9 53.9 54.7 43.0	50.9 58.1 56.0 53.9 54.9 45.3	55°2 59°3 56°1 53°7 55°2 47°8	56.0 58.6 55.8 54.2 56.2 49.6	56.9 59.5 55.8 53.7 56.7 49.1	57.1 61.6 56.1 54.0 57.1 49.1	56.1 61.3 55.8 54.1 55.9 51.6	55.7 61.3 55.7 54.7 55.7 53.4	54°3 61°9 55°7 54°7 55°7 52°8	55°1 60°0 55°8 55°2 56°0 53°3	54°3 58°8 56°2 55°0 55°1 53°1
OCTOBER.	10 11 12 13 14 15 16	36·3 39·3 36·9 33·7 28·7 41·4	36.8 40.6 37.5 33.9 29.2 42.2	37.8 42.2 38.9 33.9 31.6 43.9	38.6 43.5 38.6 35.7 33.3 44.8	39.4 44.7 39.5 36.7 34.3 46.0	40°2 44°7 39°9 36°1 38°5 46°7	40.6 43.4 39.9 36.1 38.4 47.5	41.0 42.9 39.5 35.2 38.6 49.6	42.1 42.6 39.5 36.0 39.3 50.3	42.8 42.5 38.8 35.6 39.1 50.5	42.4 42.7 38.8 34.3 37.8 49.9	42.1 43.0 36.6 32.3 37.5 49.1
OCT	17 18 19 20 21 22 23	38 · 8 41 · 0 28 · 9 32 · 8 37 · 2 35 · 0	40°1 40°7 30°9 33°6 37°3 34°4	44.6 43.5 36.0 36.0 37.2 36.8	48.2 46.1 41.3 38.6 37.0 40.8	52.0 44.7 44.4 39.7 37.5 42.6	53.8 44.9 45.5 41.3 37.6 43.6	56.7 45.1 45.0 41.1 37.2 46.5	57.5 44.5 45.8 40.4 37.8 46.4	57°3 45°4 44°7 40°3 38°4 45°8	56.9 45.4 44.4 40.4 39.2 46.3	56.4 43.7 43.1 40.4 39.4 46.0	55.4 42.7 40.1 40.2 38.7 44.3
	24 25 26 27 28 29 30 31	45°4 27°4 17°6 24°5 27°0 33°5	45.2 30.5 17.2 25.5 31.9 33.3	45.6 31.9 19.0 30.0 32.6 36.0	46'4 28'8 25'6 31'6 39'0 42'7	44.1 28.9 27.0 33.1 42.2 45.6	43.0 28.6 28.0 36.6 43.9 46.9	42.7 29.2 30.3 35.8 44.6 46.7	42.4 28.5 31.5 36.4 44.8 47.5	40.0 27.8 31.8 37.1 45.0 47.5	37.4 27.5 32.8 36.9 44.7 47.1	34.4 25.9 30.5 35.9 44.9 46.9	32.4 24.7 30.4 34.5 42.4 44.2
Hourly	Means	38.01	39.02	41.04	43.07	44.09	44.87	45.27	45.41	45.59	45.45	44.82	43.79

					WET	THERMO	METER.					
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
60.1	56·4	54.1	53.4	52.9	52.7	51.9	50.8	50°3	50.6	50°3	49.0	54.99
64.0	62.0	63.0	63.5	60.8	59.0	58.0	55.9	55.4	53.7	55.0	54.8	60.26
58.8	56.2	55.7	55.8	55.2	54.5	53.9	53.5	54'1	54.1	54.1	54.1	60.16
57.1	57.4	58.1	58.7	58.8	59.0				-		$\frac{-}{46\cdot 9}$	53 <b>·92</b>
_						48.4	47.5	47.3	46.9	46.9		
59.3	58.0	56.3	56.3	56.0	54.3	54.3	52.9	52.1	51.1	50.8	50.8 62.1	56.28 59.99
58.8	<b>5</b> 9 <b>.</b> 2	58.6	60.8	61.4	61.0	61.2	61.6	61.4	61.6	61.8 49.6	48.0	62.37
66.9	66.0	65.5	65.6	57.4	53.7	53.5	52.5	52.7	$\begin{array}{c} 52.5 \\ 43.3 \end{array}$	43.0	43.0	49.93
54.7	<b>5</b> 3 · 5	53.7	50.6	49.2	47.3	45°2 47°8	43°9 47°7	43.9 47.1	46.2	45.7	45.9	51.89
56.5	52.4	50.6	49.6 49.2	48.7 49.0	48.0 48.8	47.0						ŧ
54.2	50.4	49.2	i	49 0	40 0	54.5	54.2	53.7	53.7	53.9	$\frac{-}{54 \cdot 3} \}$	53.57
45.1	44.4	43.4	42.8	42.4	42.4	42.4	42.6	42.8	43.0	43.4	43.3	46.44
45 1	42.4	41.7	41.1	41.5	40.9	40.3	39.0	38.4	37.4	38.0	37.5	42.93
52.3	48.2	46.7	46.2	45.7	45'1	44.2	42.2	40'1	39.1	38.3	38.0	45.63
52.3	49.5	48.2	47.0	47.6	48.2	48.6	48.5	48.5	48.0	48.8	49.4	49.95
54.2	<b>54°</b> 1	54.0	54.7	53.3	53.3	53.1	58'1	57.1	56.7	56*4	56.3	55.30
56.6	58.2	58.2	57.5	57.4	57.7			50.7	53.7	53.2	$\frac{-}{53\cdot 5}\}$	57.09
					<u> </u>	53.5	53.5 51.8	53.7 51.8	51.0	52.5	51.2	53.28
54.5	51.8	51.9	51.6	51.2	50.6 46.7	50.6 45.7	43.8	43.0	43.9	44.0	43.8	50.30
50.6	48.8	47.5	47'1 48'6	46.7 50.1	48.1	47.2	45.7	45.3	44.9	45.1	45.3	50.40
52.3 60.0	50.9 58.9	49:4 58:8	57.8	56.4	55.7	57.4	55.2	55.0	54.2	<b>5</b> 3 • 4	52.7	57.82
53.9	53.7	53.7	53.4	53.2	52.3	52.1	52.0	51.3	49.2	47.7	47.1	52.45
53.2	53.3	53.3	52.7	52.2	51.3						$\frac{-}{57\cdot 1}$	53.64
	_	- 1	_			55.9	57.1	57.4	58.0	57.4	57.1	
62.6	60.9	60.6	56.2	54.8	51.9	49'1	47.8	47'1	45.8	45.7	45.3	57.37
46.6	46.2	44.7	43.6	43.8	42.5	41.4	41'1	41.0	42.0	42.2	$\begin{array}{c} 42.5 \\ 38.4 \end{array}$	46°25 44°48
45.7	45.2	44.9	43.4	43.0	43.6	43.6	42.0	39.9	40°3 46°9	37.8 46.9	44°3	45.89
47.8	44'3	43.7	42.8	44.0	44.9	46.9	47.3	47.1	40 9	40 3	11 0	10 03
54.75	53.18	52.2	51.92	51.58	50.2	50.03	49.56	49.13	48.76	48.55	48.27	52.79
			<u> </u>			j			2210	2010	00.1	40.71
44.6	41.8	41.1	38.4	39.5	39.3	38.2	37.0	37.6	38.8	38.2	38.1	42.71
45.8	44.4	43.6	45.4	45.3	43.0			42:0	43.4	42.5	$\left\{ \begin{array}{c} -1 \\ 42 \end{array} \right\}$	45.59
						45.4	45.4	43.6 52.8	53.2	53.6	55.4	53.43
54.2	54'6	54.7	54.3	53.2	53.1	53.6 56.6	53°5 56°6	56.4	56.4	56.5	55.7	58.50
57.9 56.4	57.7	57.7 56.4	57.6 56.1	56.8 56.2	56.6 55.6	55.3	54.9	54.9	54.7	54.2	54.6	55.69
55.4	56°3 55°7	55.9	55.2	55.0	54.2	54.4	54.8	54.5	54.3	53.7	55.1	54.28
54.0	53.9	51.2	48.4	47.1	46.8	46.0	45.3	44.0	43'1	41.6	41.3	51.28
51.5	51.0	51.3	51.8	50.2	49.9			_			$\frac{-}{37\cdot 3}$	46.97
-		_				40.3	39.2	38.8	38.8	38.9	37:35	39.33
41.6	<b>3</b> 9.5	40.4	39.3	38.6	37.1	36.9	36.7	37.6	37.6	39.1	39 <b>°</b> 5 37 <b>°</b> 3	39°33 41°62
43.1	42.9	42.2	42.1	41.9	42.1	41'4	39.5	38.8	38.0 33.4	$\frac{37.5}{34.2}$	34.3	35.97
35.3	35.3	33.9	32.9	32.1	31.3	30.9	32.3	$\frac{35.9}{26.0}$	27.5	$\frac{34}{27}$	28.5	31.54
30.9	30.4	29.4	28.8	28.2	28.0 41.0	26.4 41.0	25.9 40.9	40.8	41.0	41.0	40.2	37.72
36.6	39.0	38.8	38.5 49.7	40.0 49.7	49.9	-11 U		<del></del>				45.40
49.5	50.4	50.3	49 /	73 /	49 9	39.6	38.4	38.2	37.6	37.1	$\frac{-}{37\cdot 1}$	i
56.7	54.5	53.9	52.9	50.9	50.3	49.5	48.2	47.2	44.9	42.1	41.3	50.42
42.1	39.5	39.2	37.4	36.1	33.1	32.2	31.1	29.7	30.0	30.0	29.6	39.07
38.2	36.7	37.3	37.0	36.0	33.9	31.3	29.5	28.9	29.8	29.6	32.4	37.11
40.3	40.1	39.7	39.3	39.4	38.1	37.9	37.8	37.4	37.4	37.2	37.4	38.62
38.9	38.6	38.6	38.4	38.0	38.1	38.2	35.5	34'4	33.4	33.9	35.8	37:33
43.5	39.8	39.4	38.1	37.2	37.1	40:0	40:0	45.0	45.7	45.7	$\frac{-}{45\cdot 5}$	42.45
-						46.3	46.3	45.8 28.1	27.8	27.6	26.5	35.49
31.9	31.4	31.3	30.2	30.2	29.7	28.9 17.5	28.6 16.5	16.8	16.8	17.0	16.8	23.31
21.4	20.8	30.6	19.4 29.0	18.8 29.0	18.0 26.8	26.5	26.0	25.9	25.9	25.9	25.2	27.26
33.8	31.9 31.9	32.7	29.4	28.1	28.0	28.0	27.5	26.9	27.3	26.7	26.8	31.11
41.3	39.7	39.4	36.7	35.4	34.1	33.6	33.1	32.3	32.1	32.4	32.9	37.75
41.8	42.7	39.3	37.5	35.3	35.1						$\frac{-}{47.6}$	43.05
_		-		<del></del>		46.9	46.9	46'9	47.6	47.6	47.63	
42.95	42:39	41.86	40.93	40.34	39.63	39.35	38.75	38.37	38.34	38.13	38.26	41.65

						WET TH	ERMOME'	ΓER.					
Hours of Göttir Tim	Mean higen	0	1	2	3	4	5	6	7	8	9	10	11
	Mean }	18	19	20	21	22	23	0	1	2	3	4	. 5
	( 1 2 3 4 5 6 5	47.7 49.4 45.6 41.6 34.6 30.8	48°3 49°4 45°8 41°2 34°5 29°0	49°1 50°5 52°1 44°5 36°4 31°7	50°1 51°6 52°9 44°2 37°9 33°7	51.6 52.6 52.3 45.6 39.5 34.7	52.6 53.9 51.9 48.5 40.1 35.3	54.1 54.1 53.6 48.0 40.0 35.3	53°9 55°9 53°5 47°8 40°4 35°0	53°3 53°7 54°0 47°3 40°0 35°2	52°1 53°4 53°3 45°8 39°2 35°8	50°8 52°9 53°3 45°5 38°6 36°1	49°3 50°7 52°6 43°3 37°3 35°3
ER.	7 8 9 10 11 12 13	45.0 50.6 34.8 33.2 30.8 33.4	45.5 50.6 35.0 33.6 29.5 33.0	46.0 52.7 35.4 33.6 31.0 33.7	45.7 53.3 36.3 34.0 34.6 35.4	46.0 54.7 36.9 34.5 35.9 36.0	46.4 51.5 35.7 34.8 36.0 36.4	46.7 49.1 36.0 34.8 36.2 37.2	48.1 47.5 35.8 34.8 36.2 37.9	47.9 47.2 35.6 34.8 35.5 38.5	48.1 47.1 35.5 34.4 36.2 37.5	48.3 45.8 35.6 34.4 35.6 37.2	48.2 43.2 34.8 34.1 34.8 36.9
NOVEMBER.	14 15 16 17 18 19 20	37·1 28·0 43·2 42·2 31·6 19·2	37.2 27.4 43.1 42.0 31.4 19.2	37.4 30.4 43.6 42.0 29.4 20.4	38·1 35·6 44·5 42·2 28·4 23·0	38.7 37.7 46.1 42.7 27.9 25.8	38'9 39'3 47'3 42'8 26'9 26'9	38.7 42.0 47.4 42.9 27.2 27.4	37.9 43.1 47.9 42.8 26.6 28.1	37.2 44.6 47.6 43.2 26.9 28.6	36.9 45.2 48.1 44.0 26.9 28.4	36.7 44.0 47.6 45.4 26.1 28.0	37.0 43.2 47.4 46.0 25.8 27.2
	21 22 23 24 25 26 27	35°8 41°8 48°0 40°0 26°0 23°8	36°2 42°1 45°7 40°0 25°4 24°6	36.2 42.7 46.0 39.6 25.2 25.6	38.2 44.1 46.4 41.4 25.1 26.3	40.2 45.7 48.3 41.1 25.1 26.5	42.7 47.7 49.6 41.1 25.1 26.9	43.7 49.5 48.4 39.9 25.2 26.9	44°3 50°5 48°7 39°4 25°8 29°2	43°3 50°2 48°8 38°8 25°8 30°5	42.9 50.7 47.8 38.4 25.6 30.5	41.5 50.6 47.7 38.2 24.8 29.4	40.2 51.2 47.1 36.9 23.5 29.1
	28 29 30	10.0 18.4	9.8 18.2	10°3 20°6	10.4 22.2	11.4 23.1	$\begin{bmatrix} -13.4 \\ 23.7 \end{bmatrix}$	13.4 $24.2$	13.8 24.6	15°2 25°3	15.6 24.7	15.6 23.2	$\frac{13.9}{22.5}$
Hourl	y Means	35.48	35.30	36:39	37.52	38.48	39.05	39:30	39.60	39.56	39:39	38.96	38.13
	$\begin{pmatrix} 1\\2\\3\\4 \end{pmatrix}$	31.9 35.1 33.0 26.0	33.2 34.6 33.0 25.7	33.4 34.5 33.0 25.7	33.6 35.5 33.0 27.2	34·2 36·2 33·0 27·4	35°4 36°7 33°2 29°4	36.5 37.5 32.9 30.3	36°3 37°4 32°9 30°3	37.5 36.2 31.7 30.0	37°3 36°7 30°5 30°2	36.4 36.2 30.3 29.8	35.2 34.7 29.5 30.0
	5 6 7 8 9 10	26·3 31·7 35·1 36·0 47·2 33·8	26.7 31.7 34.7 36.0 46.1 34.2	27°0 31°2 35°8 35°6 46°2 34°7	28.6 33.2 37.2 36.0 46.3 35.2	30.5 34.7 39.6 36.5 47.3 35.8	29.6 36.0 41.3 37.5 46.9 35.7	31'3 36'5 42'2 38'3 46'9 33'6	31.7 36.7 42.8 38.8 46.7 34.1	33.2 37.3 42.3 39.7 46.9 34.5	32·4 37·2 42·8 41·9 43·7 34·4	32.4 37.1 42.6 42.5 42.5 34.1	30°4 34°6 42°4 43°3 41°0 32°1
DECEMBER.	12 13 14 15 16 17 18	36.8 31.5 32.8 12.9 16.0 14.0	36.7 31.6 29.4 12.9 16.6 14.3	35.8 31.9 27.8 13.3 17.1 15.4	35.9 32.5 28.6 13.3 17.7 19.0	35.9 32.8 28.1 14.6 18.2 22.5	36°0 33°0 29°4 15°3 19°8 24°8	36°3 33°0 30°9 16°5 22°1 26°9	36.0 33.0 29.2 17.2 24.6 29.4	35°2 32°9 29°3 18°2 25°8 30°3	34·1 33·0 29·5 18·6 26·2 30·3	34.0 33.0 28.2 19.6 26.4 31.1	33.6 32.9 27.4 20.0 25.3 32.0
Ö	19 20 21 22 23 24 25 a	13°3 11°1 20°8 17°7 20°4	13°3 10°2 20°6 17°8 20°0	12.7 9.8 20.6 19.6 19.9	12·4 10·4 21·4 19·4 21·4	13°1 13°2 22°4 19°6 21°6	13 · 4 16 · 4 23 · 5 21 · 8 20 · 0	13.8 17.1 23.2 23.1 19.9	14.4 17.7 23.3 23.5 20.4	14.8 18.2 23.5 24.1 20.3	14.1 19.4 23.7 24.3 20.3	13°1 20°5 23°8 23°6 20°1	11.1 20.8 22.5 23.3 19.8
	26 27 28 29 30 31	12°9 29°6 36°9 40°6 42°6	12.2 30.5 37.6 39.8 42.1	11:3 30:8 37:5 40:0 42:3	12·2 32·3 38·6 42·0 42·7	15:3 32:8 40:2 42:5 44:3	15.8 32.9 40.2 43.3 45.4	18'3 33'3 41'2 44'7 44'6	17.7 33.4 40.8 45.0 44.7	18.6 33.6 40.6 44.7 44.9	19°2 34°1 40°5 43°7 44°3	18'9 34'1 40'8 43'7 44'3	19.6 34.6 40.6 43.1 44.0
Hourl	y Means	27.92	27.75	27.80	28.68	29.70	30.49	31.19	31.46	31.70	31.63	31.20	30.95

^{*} Christmas Day.

					WET	THERMO	METER.					
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
46°9 49°6 53°4 40°9 35°7 32°5 — 48°2	47.8 48.8 51.8 39.5 34.6 30.2  48.1	49°0 49°8 51°9 39°4 33°6 29°1	49°9 51°8 52°5 36°2 33°6 29°4 ————————————————————————————————————	48°.8 50°.8 52°.3 37°.6 33°.8 29°.4	49°9 48°3 36°3 34°2 29°1 — 47°8	49° 2 49° 4 47° 6 35° 7 33° 8 — 43° 3 48° 8	50° 4 49° 2 47° 6 35° 5 33° 3 	49°1 49°3 45°0 34°4 33°0 — 43°7 48°8	49°0 48°9 44°2 33°6 32°3 — 44°1 50°3	49°4 47°2 42°5 34°0 31°9 — 44°4 50°3	49.5 46.8 41.2 35.1 31.4 	50.05 50.82 49.97 40.89 35.82 35.45 47.83
41.7 34.4 33.7 34.6 37.9	39.6 34.4 33.2 34.2 38.3	38.6 34.2 33.2 34.2 38.5	38.8 33.6 33.4 34.0 38.7	37.6 34.0 33.4 34.1 39.1	37 · 2 34 · 1 33 · 4 34 · 0 38 · 4	37 · 4 33 · 6 33 · 4 34 · 0 — 37 · 1	34.8 33.6 32.8 34.2 — 37.1	33.9 33.6 33.0 34.5 — 37.1	34.5 33.4 32.6 34.9 — 36.5	34.8 33.2 31.2 35.0 — 36.0	35.0 33.1 31.8 35.0 	43°22 34°69 33°59 34°37 36°86
 36.7 42.8 46.1 45.6 25.5 28.2	36.5 43.7 45.7 45.7 25.4 30.2	35.8 43.7 45.5 45.7 24.9 31.0	34.7 42.7 45.6 48.9 24.7 31.1	33.0 42.7 45.2 46.2 24.6 30.7	32 1 45 0 44 9 44 5 23 4 29 8	32·3 43·9 44·3 43·7 22·7 — 32·9	32·1 44·0 44·3 40·9 22·1 — 32·9	31.5 43.9 43.9 39.6 21.9 — 34.1	29'4 44'3 43'7 38'4 21'0  35'4	29.4 43.6 43.7 35.0 20.7 	29.0 42.9 42.8 34.2 19.4 	35.18 40.99 45.40 42.78 25.47 28.76
39.8 50.6 45.2 37.0 23.2 29.1	40°1 50°8 43°5 36°5 22°6 29°6	39.9 50.3 43.1 35.8 22.8 29.4	40.4 50.3 42.3 35.8 21.8 30.2	40.5 50.7 41.8 34.6 21.6 29.7	40.8 50.3 41.4 33.2 20.9 29.3	42°3 49°8 41°4 32°8 20°2	41.4 49.3 41.2 30.9 20.9	41.6 48.7 40.9 30.5 21.8	41.8 50.1 40.7 30.3 22.1	41.8 49.5 40.5 27.2 22.1	41.4 49.5 40.6 26.2 24.2	40°71 48°61 44°79 36°07 23°62 23°52
13.0 22.2	$\begin{bmatrix} \overline{12:3} \\ 23:7 \end{bmatrix}$	12·3 24·6	12.8 26.2	$\frac{-}{13.5}$ $28.2$	14.9 29.4	10°9 15°6 28°5	10°4 17°9 28°6	9°8 17°4 26°1	9°4 16°5 24°1	8°8 18°1 24°5	8.6 } 18.1 24.2	13.97 24.23
37.49	37:18	37:10	37:20	36.98	36.61	36:33	36.02	35.66	35*44	35.02	34.97	37.22
34.8 35.1 29.1 30.2 - 27.6	34.0 35.1 28.5 31.2  29.6	34°0 35°1 28°3 32°0 — 28°4	33.8 34.6 27.9 33.2 — 28.4	34.6 34.2 27.8 33.2 — 31.1	35.8 33.2 27.6 33.0	36.7 32.8 26.9 — 26.6 30.8	36.8 33.1 26.8 — 26.0 30.7	36.0 32.9 27.0 — 26.0 31.1	35.8 33.1 26.7  25.5 31.7	35.6 33.2 26.2 ————————————————————————————————	$   \begin{bmatrix}     35.2 \\     33.0 \\     26.1 \\     \hline     25.9 \\     31.7 $	35°18 34°86 29°79 28°73 30°18
32.7 41.9 43.4 39.7 29.1	31 · 9 41 · 1 44 · 1 38 · 7 27 · 5	31.5 41.1 44.1 38.3 26.9	31.9 41.2 45.0 38.1 27.4	32.9 41.0 44.5 37.5 26.9	31 · 7 42 · 0 47 · 4 36 · 7 28 · 4	32.8 42.0 46.6 36.5 — 39.6	32·4 39·9 47·0 36·2 — 39·1	$ \begin{array}{c} 32.8 \\ 38.2 \\ 45.2 \\ 35.7 \\ \\ 39.1 \end{array} $	32.6 37.9 44.8 34.3 — 39.1	34·4 37·2 46·2 33·6 — 38·9	$ \begin{array}{c} 34.3 \\ 36.2 \\ 46.6 \\ 33.8 \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\\\\\\\\\\\\\\\$	33.74 39.94 41.96 41.12 33.87
33·2 32·8 26·7 20·2 25·1 32·8	33.0 32.7 26.0 20.8 22.5 32.6	31 '9 32 '8 24 '1 19 '8 22 '5 33 '0	31.9 32.8 21.2 19.6 21.8 32.0	31.0 32.6 20.5 19.6 20.2 30.7	30.9 32.8 19.1 19.1 18.4 32.4	30.7 32.8 18.1 18.4 18.1	30.7 32.9 17.1 17.9 16.9	30.7 32.8 15.8 15.8 15.4	30.9 32.9 13.5 15.1 14.8	31.0 32.1 12.6 14.8 13.2	$     \begin{array}{c}       31.3 \\       33.2 \\       12.5 \\       15.8 \\       \hline       15.0 \\       \hline       15.8     \end{array} $	33.48 32.68 24.07 17.05 19.99 24.60
10.7 20.6 20.4 23.3 19.8	9.9 22.7 18.4 23.3 19.6	9'4 22'9 17'7 23'5 19'1	10.7 23.7 17.3 23.7 18.8	11.0 23.7 17.9 23.6 18.6	11.1 24.0 18.4 23.5 18.5	19.0 11.1 24.1 17.0 22.7	18.8 10.8 24.8 16.6 22.6	18:4 10:2 24:2 16:8 22:6	18 1 10 3 22 5 16 8 22 8 —	16.9 10.0 21.3 17.1 22.7	9'2 21'0 17'1 21'4	11.83 19.18 20.03 22.23
19.6 34.6 40.2 42.7 43.4	19°2 35°0 39°6 43°1 42°7	19.0 35.0 39.1 43.1 42.4	22°1 35°0 38°5 42°1 42°3	23°3 35°0 38°4 42°2 43°5		10.7 25.1 35.8 39.4 41.7 44.3	10.7 25.8 35.8 39.8 41.7 44.9	11:3 25:8 36:3 40:0 41:7 45:3	12:3 27:0 36:1 40:6 41:3 46:0	13.8 28.0 36.3 40.9 40.7 46.0	13·3 } 28·6 36·8 40·9 42·2 46·2	20°01 34°12 39°63 42°39 44°03
30:37	30.11	29.81	29.81	29.83	29.95	29.24	29.07	28.73	28.56	28.44	28.53	29.72

						WET TI	HERMOME	TER.					
	of Mean ingen	0	1	2	3	4	5	6	7	8	9	10	11
	of Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	_ 1	。 46 <b>·</b> 2	。 47·2	° 46°6	。 47°1	。 46 <b>·</b> 6	° 47.9	。 48`3	。 48 <b>·</b> 2	。 49 <b>·</b> 2	。 48°3	° 50°4	。 50°5
	2 3 4 5 6 7 8	32.6 33.7 24.2 12.0 13.5 30.4	32.5 34.1 25.6 11.2 14.8 31.0	32.9 32.1 26.5 10.4 14.6 30.8	34.0 28.0 27.4 10.7 15.5 30.7	34.5 28.6 27.8 10.7 15.8 31.0	35°2 28°1 29°3 12°1 17°0 31°6	35.5 26.0 31.7 12.9 18.8 31.8	36.0 25.1 33.4 13.9 19.6 33.1	36.2 25.5 33.6 13.5 19.8 33.0	36.5 25.1 35.6 14.0 19.9 30.7	35·4 24·0 33·6 14·0 19·7 30·3	35.0 21.6 29.6 13.3 19.7 29.2
ARY.	9 10 11 12 13 14 15	-10.5 9.6 11.7 31.5 36.7 40.0	-11.2 9.6 8.9 32.1 36.8 39.8	-10.9 14.9 8.2 32.8 37.3 41.1	$ \begin{array}{r}  -8.8 \\  16.6 \\  14.4 \\  33.1 \\  37.5 \\  41.1 \end{array} $	$ \begin{array}{r}  -6.2 \\  17.4 \\  19.1 \\  33.6 \\  37.5 \\  42.8 \end{array} $	$ \begin{array}{r} -2.5 \\ 19.4 \\ 21.4 \\ 34.2 \\ 37.9 \\ 43.7 \end{array} $	$ \begin{array}{r} -2.2 \\ 19.6 \\ 24.0 \\ 35.4 \\ 37.9 \\ 44.7 \end{array} $	- 1.8 21.0 25.9 35.7 38.3 44.5	0.8 21.8 25.5 35.8 38.4 44.9	0°9 22°3 26°0 36°3 38°4 47°1	0°6 21°6 23°7 36°2 38°4 45°4	- 1.9 21.2 21.2 36.3 38.5 41.8
JANUARY	16 17 18 19 20 21 22	29.5 27.0 5.6 27.5 35.9 15.1	29°3 25°3 5°6 28°0 35°8 15°4	24.6 19.7 6.5 28.2 35.8 16.5	24.0 22.0 9.6 30.7 37.2 17.6	22.7 20.6 13.5 33.2 39.6 19.2	21.6 19.6 14.3 33.5 39.8 21.7	22.0 20.0 16.9 34.2 38.5 23.5	23.5 19.2 17.5 35.9 37.3 24.6	22.9 18.9 19.3 36.7 35.4 25.6	23.7 18.3 20.3 38.2 33.8 27.4	23.7 17.0 20.9 36.7 29.7 26.8	23.5 16.6 21.4 35.4 29.6 26.4
	23 24 25 26 27 28 29	21'9 27'4 37'5 38'0 29'0 26'1	20.9 27.8 37.4 37.5 29.6 29.1	21'3 29'4 37'5 38'1 29'6 28'6	26.0 32.7 38.0 39.0 29.6 30.7	27.6 33.2 38.0 40.1 31.3 29.0	28.6 35.7 37.9 41.2 32.6 28.6	29.4 36.2 38.3 42.1 33.0 28.7	29°2 36°6 38°7 41°4 33°4 29°0	30.7 37.7 39.4 40.1 33.4 29.4	30.7 38.0 39.7 40.2 33.2 29.3	30.8 36.7 40.0 39.2 33.2 30.3	29.4 34.8 40.2 38.3 33.0 29.9
	$\begin{vmatrix} 30 \\ 31 \end{vmatrix}$	33.5	33.6	34.4	35.8	36.0	36.2	37.0	37.5	37.7	38.8	35.4	31.4
Hourly	y Means	25.29	25.68	25.67	26.92	27.82	28.73	29:39	29.87	30.50	30.49	29.76	28.69
	$\left( egin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{array} \right)$	24 1 21 1 29 0 32 3 27 2	24.6 21.5 27.6 32.8 26.8	25°1 21°8 27°7 33°2 26°4	25.8 27.4 32.1 35.4 26.0	26.4 31.9 33.0 37.5 26.4	26.6 33.2 34.4 37.8 26.9	26.4 33.0 37.1 37.6 26.9	25.6 33.0 37.5 37.8 25.8	26.0 33.2 37.7 37.0 26.5	26.0 33.4 37.5 37.3 26.4	26.0 33.2 36.5 37.4 25.7	25.6 33.0 34.6 37.0 25.2
Υ.	6 7 8 9 10 11 12	21.6 18.9 22.3 20.1 1.0 12.8	20.8 19.4 22.3 18.1 - 0.4 13.3	20.4 19.8 24.8 16.4 0.9 14.3	20°3 21°2 27°2 13°1 3°2 15°3	21.1 22.5 26.9 13.5 5.0 18.0	21.8 22.9 28.4 14.0 7.5 19.5	22.5 24.6 30.5 14.6 10.3 19.7	23.4 25.8 30.9 15.5 10.3 21.8	24.6 26.4 30.9 15.4 11.0 22.9	25.6 26.2 30.9 16.0 12.1 23.1	25.8 25.7 30.5 15.3 12.6 22.9	23.0 25.2 29.8 14.4 12.9 21.8
FEBRUARY	13 14 15 16 17 18 19	19.6 19.4 20.2 21.6 20.4 30.8	18.7 18.0 23.3 21.0 20.5 31.6	20.4 18.1 24.8 24.8 24.8 32.7	25.8 19.6 30.4 28.5 28.1 33.1	28.4 22.7 31.3 32.4 31.9 34.2	31°1 25°2 32°6 33°1 32°9 35°6	32.8 25.8 33.1 34.0 33.0 36.9	33.8 30.5 33.1 34.1 33.0 37.1	34.4 28.7 32.8 34.5 34.6 36.7	34.6 28.0 33.1 34.0 34.2 36.0	34.6 29.4 32.9 33.5 35.1 34.9	33.8 28.4 31.6 31.5 34.2 34.5
	20 21 22 23 24 25 26	34·4 31·1 30·5 20·0 10·7 13·0	34.2 31.3 29.6 21.0 10.2 12.9	34.2 32.5 32.3 22.0 11.5 19.0	35°4 33°8 33°7 21°8 14°9 25°2	35.9 35.3 32.6 23.0 16.9 27.9	36.5 36.7 31.5 24.0 18.1 27.6	38·1 37·7 29·6 24·1 19·4 27·9	38.7 38.3 34.2 25.4 20.2 28.6	39.8 37.1 31.1 26.8 22.7 30.5	39.2 36.8 31.1 27.0 21.0 30.8	39.0 36.3 30.5 28.0 20.9 30.5	38°1 35°7 29°4 26°2 20°2 30°3
	27 28	26.4	26.8	27.6	28.7	29.8	31.1	32.1	32.8	33.2	35.4	35.6	34.6
Hourl	ly Means	22.02	21.91	23.12	25.30	26.85	27.87	28.65	29.48	29.78	29.82	29.70	28.79

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Daily and Monthly Means.   41.16 34.80 23.46 24.33 12.08 21.91 20.43
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Means.  41.16 34.80 23.46 24.33 12.08 21.91
$ \begin{bmatrix} 38.7 & 37.0 & 35.8 & 34.3 & 32.3 & - & - & - & - & - & - & - & - & 32.4 \\ - & - & - & - & - & - & 31.4 & 31.7 & 31.3 & 32.1 & 32.1 & 32.4 \\ - & 35.0 & 35.1 & 35.1 & 34.8 & 35.0 & 35.4 & 35.4 & 35.3 & 35.0 & 34.0 & 34.7 & 34.2 \\ 19.8 & 19.2 & 19.2 & 18.9 & 18.4 & 18.0 & 18.5 & 18.6 & 18.8 & 19.8 & 20.9 & 21.0 \\ 26.2 & 25.4 & 25.6 & 21.1 & 19.6 & 18.1 & 17.1 & 16.1 & 16.9 & 14.6 & 12.3 & 12.5 \\ 12.5 & 11.3 & 11.5 & 11.6 & 11.1 & 11.4 & 11.3 & 11.5 & 11.7 & 12.2 & 12.1 & 13.0 \\ 22.5 & 23.7 & 23.5 & 25.1 & 25.8 & 26.6 & 27.1 & 28.0 & 27.8 & 28.4 & 29.2 & 29.5 \\ 29.0 & 29.1 & 28.2 & 26.6 & 24.4 & 23.5 & - & - & - & - & - & - \\ - & - & - & -$	41.16 34.80 23.46 24.33 12.08 21.91
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	34.80 23.46 24.33 12.08 21.91
	- 4.90 18.70 23.25 35.46 38.82 37.88 25.38 16.02 19.27 34.33 28.25 22.47
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	26.83 35.04 38.54 36.99 30.05 29.61 30.69
25.4   23.3   20.6   13.5   18.0   18.4   18.8   13.4   20.4   21.2   22.0   21.9	23.50
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	31 · 02 31 · 44 33 · 62 24 · 75 20 · 49 23 · 07 27 · 81 11 · 86 9 · 82 19 · 70
$ \begin{bmatrix} 31 \cdot 9 & 31 \cdot 5 & 29 \cdot 6 & 28 \cdot 4 & 28 \cdot 2 & 27 \cdot 0 & 25 \cdot 9 & 25 \cdot 3 & 24 \cdot 5 & 24 \cdot 8 & 22 \cdot 0 & 22 \cdot 0 \\ 26 \cdot 5 & 25 \cdot 9 & 25 \cdot 2 & 22 \cdot 8 & 22 \cdot 5 & 22 \cdot 0 & 21 \cdot 0 & 20 \cdot 4 & 19 \cdot 8 & 19 \cdot 8 & 19 \cdot 6 & 20 \cdot 8 \\ 28 \cdot 2 & 26 \cdot 7 & 25 \cdot 8 & 25 \cdot 8 & 25 \cdot 4 & 24 \cdot 6 & 24 \cdot 3 & 23 \cdot 8 & 24 \cdot 4 & 24 \cdot 0 & 22 \cdot 7 & 22 \cdot 2 \\ 30 \cdot 3 & 27 \cdot 8 & 27 \cdot 4 & 26 \cdot 2 & 25 \cdot 9 & 24 \cdot 7 & 23 \cdot 5 & 22 \cdot 5 & 21 \cdot 4 & 20 \cdot 6 & 19 \cdot 6 & 21 \cdot 4 \\ 30 \cdot 7 & 29 \cdot 7 & 29 \cdot 4 & 29 \cdot 2 & 30 \cdot 3 & 30 \cdot 3 & 30 \cdot 3 & 29 \cdot 4 & 29 \cdot 8 & 29 \cdot 6 & 29 \cdot 4 & 29 \cdot 1 \\ 34 \cdot 8 & 34 \cdot 8 & 35 \cdot 2 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 8 & - & - & - & - & - & - & - \\ 34 \cdot 8 & 34 \cdot 8 & 35 \cdot 2 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 8 & - & - & - & - & - & - & - \\ 34 \cdot 6 & 34 \cdot 8 & 34 \cdot 8 & 35 \cdot 2 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 8 & - & - & - & - & - & - \\ 34 \cdot 6 & 34 \cdot 8 & 34 \cdot 8 & 35 \cdot 2 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 8 & - & - & - & - & - & - \\ 34 \cdot 8 & 34 \cdot 8 & 35 \cdot 2 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35 \cdot 0 & 35$	27.88 23.34 27.38 27.26 30.01 34.85
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	34 '93 34 '14 28 '10 21 '22 16 '74 23 '97 29 '47
33·1         32·5         32·8         32·4         30·9         29·9         27·6         26·0         23·3         21·8         22·1         20·6           27·46         26·50         26·05         25·62         25·14         24·73         23·94         23·37         22·84         22·53         22·23         22·35	23 41

						WET TI	HERMOME	TER.					
Hours o Götti Tin	f Mean ngen ne.	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \end{pmatrix}$	10°2 8°5 19°0 17°9	7.8 9.4 19.1 17.5	9.7 11.9 18.2 18.8	10°7 13°8 19°0 20°0	12°3 16°0 19°6 22°5	14°6 15°6 21°7 22°3	17.0 17.9 23.1 23.0	18.6 19.8 23.7 22.3	18.8 20.8 25.4 22.8	18°8 20°2 25°3 21°7	18°1 19°8 24°4 20°4	17°1 17°9 22°2 18°9
	5 6 7 8 9 10 11	20.0 17.6 34.6 23.2 15.8 16.6	20.2 19.8 35.0 22.7 15.8 17.7	21.0 23.8 36.6 23.7 15.7 20.3	22.0 29.4 37.1 24.6 17.7 24.0	23.8 32.8 39.3 25.3 19.4 26.1	25°1 33°6 40°3 24°2 21°8 27°2	25:4 35:7 39:9 25:4 23:5 30:8	26.8 36.2 41.0 25.2 25.2 31.5	29.4 37.5 40.4 26.0 29.2 30.5	28.2 37.7 44.0 26.7 26.9 30.9	28.7 36.5 39.1 26.4 26.8 30.6	29 · 9 37 · 2 35 · 8 25 · 6 26 · 0 30 · 9
MARCH.	12 13 14 15 16 17 18	23°1 11°2 3°0 11°7 22°7 18°4	23°4 10°4 4°1 13°1 23°5 21°6	22·2 11·5 5·9 16·0 23·2 23·4	22·5 12·4 7·6 19·6 23·4 26·6	21.8 14.0 10.4 20.9 23.4 28.1	21.6 14.0 10.7 22.1 23.4 29.2	22'4 14'8 14'0 23'2 23'5 29'6	24.2 14.6 15.6 24.5 23.5 31.7	23.8 14.0 15.0 25.4 23.0 31.7	22.6 12.3 15.6 26.0 23.4 32.1	21.4 11.6 15.2 25.9 24.0 31.9	21.4 10.4 14.2 25.3 24.0 31.3
	19 20 21 22 23 24 25	25.2 38.7 29.4 31.9 26.7 34.7	26.8 38.5 31.1 31.9 29.8 35.5	31.0 38.2 32.5 31.9 32.6 37.7	32.6 40.2 33.6 32.6 33.9 38.1	33 · 2 42 · 2 33 · 8 34 · 4 34 · 9 36 · 7	33.4 42.9 34.0 34.7 36.2 37.2	33.4 43.3 34.8 37.3 37.1 37.5	34.0 44.7 34.8 38.1 37.8 37.5	34.9 44.2 34.6 36.7 35.6 39.0	35.7 44.0 34.8 37.3 36.3 40.9	36.2 42.5 34.9 36.7 36.9 40.8	36.5 41.6 33.8 36.7 36.2 41.0
	26 27 28 29 30 31	32.6 26.9 31.7 31.1 35.8	32.6 28.6 35.5 34.6 37.7	32.8 32.1 39.8 36.0 40.8	29 ° 9 33 ° 0 41 ° 9 37 ° 0 45 ° 4	30·7 36·0 43·6 37·7 47·9	31.9 38.3 44.0 37.9 50.6	35.6 39.8 46.1 38.6 52.5	36°2 39°0 47°4 38°2 53°1	36.7 40.8 51.5 39.2 55.3	36°3 40°9 48°3 40°2 59°4	35°0 40°3 49°2 41°0 58°2	34·2 40·8 50·1 41·0 56·7
Hourl	y Means	22.80	23.84	25.46	26.99	28.40	<b>2</b> 9·20	30.26	31.30	31.93	32.09	31.57	30.99
	$\left[\begin{array}{c}1\\2\end{array}\right]$	31.3	33.5	32.1	32.1	32.7	34.8	34.2	33.9	34.0	34.0	32.6	32.5
	3 4 5 6 7 8	31.7 41.4 32.5 27.4 32.5 27.6	36.7 42.0 32.1 31.4 34.8 32.1	38.7 42.0 32.3 33.9 36.7 37.4	39.6 43.5 33.0 38.3 38.9 40.2	41.0 43.9 33.8 38.9 41.4 40.8	41.6 43.9 35.2 40.2 41.4 42.0	41.2 44.7 40.1 41.8 40.4 42.9	41.8 44.8 38.8 41.8 38.9 43.1	41 · 9 47 · 3 38 · 7 41 · 8 39 · 4 45 · 6	42.3 46.1 38.2 42.3 40.0 45.8	43.7 44.6 36.9 42.8 39.2 45.2	43.5 43.9 37.7 42.0 39.2 45.2
APRIL.	9 10 11 12 13 14 15	36.7 42.3 31.4 34.2 36.5 37.2	42.1 42.0 37.0 35.0 37.9 39.6	46.6 43.5 39.1 35.6 38.1 42.3	52.4 42.0 43.3 35.2 40.1 44.0	50.9 42.4 44.5 37.0 39.8 45.4	55°1 42°6 45°4 37°0 39°8 45°9	54.3 43.4 45.6 38.3 41.3 46.6	55.0 42.8 46.8 39.1 44.4 46.6	53.6 44.3 47.2 38.3 42.7 46.4	53.0 43.5 46.2 38.1 42.8 45.6	53.7 42.0 46.0 37.7 42.5 45.6	51.7 42.3 44.9 37.3 40.6 43.9
AP	16 17 18 19 20 21 a	30.5 28.7 25.8 26.4	31.8 28.6 30.5 29.2	32·7 30·5 30·7 33·2	33.4 30.7 29.2 36.3	35°1 31°3 32°4 37°9	35.9 32.8 32.8 39.2	36'9 29'8 35'1 42'5	40°4 28°2 34°6 42°0	39.8 28.4 34.6 44.8	38.3 29.0 34.4 45.6	39·2 29·9 34·3 43·9	39.4 29.7 35.5 43.4
	$\begin{bmatrix} 21 & \\ 22 \\ 23 \end{bmatrix}$	38.6	38.9	40.1	40.6	40.4	40.7	43.0	44.1	44.3	42.7	43.3	45.7
	24 25 26 27 28 29 30	31.5 27.4 31.7 29.2 36.3 42.5	32 1 31 3 33 4 35 0 37 5 42 1	33.0 33.4 34.6 39.7 38.0 40.6	36.9 37.7 35.7 41.4 39.1 39.4	38.7 37.7 39.2 42.5 39.8 40.0	39'4 38'5 39'9 44'4 40'6 40'7	37.9 39.6 40.0 44.2 39.8 42.0	36.7 40.8 39.7 44.0 39.4 42.5	36.2 40.8 41.3 44.9 40.4 41.4	36·3 40·2 40·2 44·9 42·3 41·6	35.8 40.4 41.3 43.8 42.7 40.6	34.4 39.1 40.6 42.5 42.5 39.9
Hourly	Means	32.97	35.26	36.87	38.46	39.48	40.41	41.07	41.26	41.29	41.39	41.12	40.73

* Good Friday.

			<del></del>			WET	THERMO	METER.					
ľ	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
	6	7	8	9	10	11	12	13	14	15	16	17	Means.
	15.1	14.0	12.6	8·2	12.3	11.7	² ٠١	° 7	s ² ·1	<b>8</b> .6	9.0	<b>9°5</b>	12.03
	16.1	15.6	15.6	16.3	16.1	16.7	18.1	18.6	19.2	19.6	$\frac{19.7}{20.2}$	19.6 18.1	16.78 20.13
	20.8	19.8 17.2	17.9 17.7	17:5 17:7	16.9 17.9	16.6 16.9	17.5	17.5	19.6	20.0	20 2		
	_	1			_		19.7	20.6	21.6	19.6	19.9	$\frac{-}{21.6}$	19.85
	29.4	26.5	22.9	20.5	20.6	20.4	17.9	18.1	18.1	18.2	17.9 35.7	16.9 34.8	22.82 33.74
	36.5 35.2	36.0 34.8	35.8 34.4	36.2 34.2	36.5 34.4	36°3 34°0	36°0 33°4	36°1 31°6	$\frac{36\cdot3}{28\cdot2}$	35.8 27.4	26.4	26.0	35.13
ĺ	25.2	25.2	24.8	25.1	24.5	$\frac{34}{23} \cdot \frac{0}{3}$	23.0	$\frac{31}{22} \cdot 8$	19.4	19.4	17.7	17:3	23.61
-	24.8	23.2	21.6	20.4	20.1	20.3	20.0	18.8	18.1	16.9	16.5	17.3	20.90
	30.2	28.6	28.3	28.5	29.0	28'4	30.9	28.4	26.8	25.3	24.5	${23\cdot 3}\}$	27.05
	18.1	18.7	16.9	16.4	15.7	15.1	14.6	13.9	13.1	12.7	12.2	12.5	18.76
-	7.6	6.2	6.3	5.9	5.7	5.5	5.2	5.1	4.4	4.5	4.3	3.4	8 <b>·</b> 98
1	13.1 23.8	11.3 23.6	11.1 23.7	$\begin{array}{c} 10.7 \\ 23.5 \end{array}$	10.0	$\begin{array}{c} 9.4 \\ 23.7 \end{array}$	$\begin{array}{c} 9.4 \\ 23.5 \end{array}$	9°0 24°0	8.4 23.4	$\frac{8.0}{23.3}$	10.0 23.1	10.9 23.1	22.35
	23.5	23.6	20.8	20.6	24.0 19.4	18.1	18.4	16.7	16.5	17.4	17.9	18.4	21.29
	31.3	29.1	29.0	29.4	29.4	29.2	_	_				$\frac{-}{24\cdot 3}\}$	27.70
1	37.0	37.0	36.2	36.2	25.6	$\frac{}{35\cdot 2}$	$27.5 \\ 35.4$	24.8 35.8	$\begin{array}{c} 25.4 \\ 36.9 \end{array}$	$\begin{array}{c} 25.1 \\ 42.3 \end{array}$	24.6 42.3	42.1	35.22
	37.7	34.8	34.5	33.2	35.6 32.4	$\frac{35.2}{31.7}$	30.7	30.2	29.8	29.6	28.6	28.6	36.80
	33.4	32.6	32.4	31.2	31.3	31.7	31.2	31.6	31.7	31.7	31.9	31.8 26.4	32.72 31.90
	34·2 34·2	32.8	31.1 32.9	29.6	28.6	27.8	27.6	$\begin{array}{c} 27.2 \\ 34.9 \end{array}$	26.8 34.4	$\begin{array}{c} 26.8 \\ 34.5 \end{array}$	26.4 34.8	34.8	34'32
	40.6	32.6 40.4	40.6	33.8 40.4	33.8	$\frac{34\cdot2}{39\cdot8}$	34.8				_	30.5	37.07
1							33.8	32.8	32.1	31.3	30.7	30.2	31.75
	33.8	33.0	32.7	31.8	29'9	29.5	29.3	28.5 35.8	$\begin{array}{c} 27.1 \\ 37.3 \end{array}$	$\begin{bmatrix} 27.2 \\ 36.2 \end{bmatrix}$	$\frac{27.1}{35.2}$	26.6 32.6	36.82
	39.6 48.3	38.7 42.5	38.8 40.2	38.8 37.9	38.8 36.2	$\begin{array}{c} 37.9 \\ 35.0 \end{array}$	37.4 33.1	31.2	30.7	$\frac{30.7}{7}$	29.6	29.4	39.77
	39.8	38.3	38.1	38.1	38.3	37.9	37.5	37:3	36.9	36.2	35.9	35.1	37.59
-	23.9	51.1	49'1	48.6	46.0	39.4	36.0	35.6	34.3	33.8	32.9	32.8	45.29
-	29.68	28.40	27.63	27.09	26.79	26.13	25.54	24.79	24.49	24.25	24.52	23.98	27:44
	32.2	31.2	31.2	31.2	31.6	31.3	22:0	32.7	32.6	32.8	32.6	$\frac{1}{31\cdot 3}$	32.63
	42.7	42.3	42.5	42.1	41.4	42.1	$\begin{array}{c} 33.8 \\ 42.5 \end{array}$	$\frac{32}{42}$ .0	41.7	41.4	41.9	41.4	41.15
-	42.3	41.6	40.2	37.9	36.5	35.6	35.2	33.8	33.3	32.8	31.9	30.9	39 <b>·9</b> 9
1	36.7 40.2	36.5	34.2	32.6 $36.2$	$\frac{31.9}{34.9}$	30.5 34.6	$\frac{28.9}{33.6}$	$\frac{27.8}{32.8}$	$\begin{bmatrix} 27.0 \\ 32.8 \end{bmatrix}$	$\begin{array}{c} 27.2 \\ 32.8 \end{array}$	$egin{array}{c} 26.7 \ 32.7 \end{array}$	26.5 32.7	33°16 36°74
	39.8	38.5 $36.2$	37·3 34·6	33.0	33.9	33.3	31.6	31.3	31.2	28.5	27.9	26.6	35.45
	46.2	42.5	39.9	38.1	37.7	37.7	_			05:0	95.4	$\phantom{00000000000000000000000000000000000$	39.54
	51.1	50.1	49.3	$\frac{-}{45.2}$	45.0	43.5	38.4 44.1	37.7 45.0	36.7 45.0	35.6 45.2	35.4 44.0	42°3	48.12
-	42.5	43.3	49 3	45.0	47.0	46.4	41.8	38.3	36.0	33.4	34.6	30.7	41.48
-	44.1	43'1	42.7	43.1	43.9	43.3	42.7	42.5	42.1	40°2 36°1	37.5 36.1	36.7 $36.2$	$\begin{array}{c} 42.47 \\ 36.42 \end{array}$
	37.0 40.4	$\frac{36.7}{38.7}$	35.6 36.8	$35.8 \\ 36.2$	$\begin{array}{c} 35.7 \\ 38.3 \end{array}$	35.4 37.9	35.0	35.8	35.0	36 1 36 7	36.4	37.2	38.77
	42.2	40.6	39.1	$\frac{36\cdot 2}{38\cdot 7}$	38.7	38.1						$-29\cdot 8$	40.30
		_		_			36.5	35.6	33.8	32.8 32.6	31.7 31.3	29.8	35.50
	37.7 $28.2$	36°3 27°9	35.4 28.4	35.3 $29.5$	$\begin{array}{c} 35.1 \\ 29.2 \end{array}$	$\begin{array}{c} 35.0 \\ 27.2 \end{array}$	34.0 25.4	35.2 $23.8$	$\begin{bmatrix} 34.1 \\ 24.6 \end{bmatrix}$	23.2	23.2	23.5	28.00
	35.0	33.0	30.6	31.6	28.4	26.9	26.3	25.8	$25 \cdot 1$	25.1	25.2	24.6	30.31
	41.9	39.5	37.9	37.5	36.2	36.6	43.7	43.2	42.3	41.4	41.2	$\overline{39\cdot 1}$	39.38
1	45.6	41.6	38.3	36.2	35.5	32.8	30.3	31.5	32.8	33.3	33.1	$\frac{-}{32 \cdot 3}$	38.26
	37.5	36.7	34.9	32.9	30.8	$\frac{-}{29.5}$	28.2	28.2	28.2	25.8	25.6	25.3	33.01
	38.7	38.0	37.7	37.7	37.3	37.1	36.7	36.0	33.8	31.9	30.5 26.4	28.5 $26.7$	36°28 34°78
	37.6 41.6	35 <b>.</b> 2	36.5	35.4 $37.9$	35.0	$32 \cdot 1$ $35 \cdot 2$	30.3	27.8 $35.3$	27.4 35.0	$26.8 \\ 35.2$	35.6	36.0	39.13
	42.9	39 <b>·</b> 9 41 <b>·</b> 8	39.2 41.2	37 9 41 4 .	36°2 42°3	$\frac{35}{42}$ 3	42.6	42.2	42.5	42.3	42.1	42.0	41.01
	39.6	37.8	36.2	34.8	34.6	31.6	<u>-</u> 34·4	33.8	33.4	32.8	36.5	$\frac{-}{36\cdot 7}$	38.12
-	40.18	38.72	37.65	36.91	36.23	35.65	35.31	34.66	34.30	33.28	33.34	32.55	37.50
	10	00 12	01 00	00 01	55 50	00 00		00	-				

2 S

						WET T	HERMOMI	ETER.					
Hours o Götti Tir	f Mean }	0	1	2	3	4	5	6	7	8	9	10	11
Tor	f Mean onto me.	18	19	20	21	22	23	0	1	2	3	4	5
	$ \begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{bmatrix} $	38·3 41·2 44·0 44·1 52·5 51·7	40°2 42°1 49°5 45°3 57°5 57°5	41°4 44°1 50°9 48°1 58°2 59°9	44.3 47.8 52.0 50.9 61.8 61.0	44.9 49.9 53.6 50.7 63.0 61.4	45.6 49.0 54.1 51.1 63.8 64.2	45.9 49.7 53.9 49.8 63.6 64.4	44·4 50·2 52·4 48·8 64·0 64·9	43°5 50°4 52°1 48°6 61°4 66°8	45.2 49.4 54.8 48.8 62.8 64.7	46.5 48.9 53.7 47.6 62.9 62.4	46·3 49·6 52·3 48·4 59·4 62·9
	7 8 9 10 11 12 13	39°3 42°5 45°2 45°2 37°7 33°6	41.4 46.7 46.4 45.2 39.4 36.3	43.9 50.1 46.9 45.4 40.4 38.3	47.2 51.2 47.4 46.1 42.3 38.5	46.6 51.0 48.0 46.6 43.3 39.8	47.5 51.8 48.2 46.6 44.3 42.1	48.7 52.9 48.8 46.6 44.0 43.6	48.6 54.4 50.2 45.6 44.2 46.2	48.2 53.1 51.2 46.2 44.9 44.2	48 · 1 51 · 2 50 · 2 46 · 0 46 · 4 43 · 0	49'3 52'6 50'2 47'0 46'9 41'0	48.8 50.2 49.8 46.6 47.4 39.0
MAY.	14 15 16 17 18 19 20	37.0 49.0 42.0 49.9 54.6 58.6	41.8 50.9 49.7 55.7 55.8 58.6	45°1 51°6 51°2 56°7 59°9 62°6	46.4 52.1 52.6 58.4 61.9 67.1	47.8 54.4 53.6 59.7 63.6 66.6	50.0 55.7 55.5 59.0 66.1 66.9	49.2 56.2 55.8 60.6 65.7 70.6	49°3 55°6 56°7 60°8 65°3 67°4	47.6 54.7 58.0 62.7 66.5 68.4	45.6 54.0 57.8 62.0 63.9 66.3	45.6 55.7 57.4 62.0 63.1 64.7	46.5 55.2 55.6 62.5 65.3 66.0
	21 22 23 24 25 26 27	55°1 53°9 53°7 54°2 48°3 48°0	50.8 52.3 54.1 55.9 48.9 49.6	50°9 51°9 56°5 57°5 49°6 53°7	55.7 49.6 59.2 59.3 50.2 56.3	56.5 49.3 63.5 63.0 51.3 56.7	56.5 49.3 64.7 64.3 54.3 57.4	55.7 49.9 62.7 64.8 58.1 57.2	56.1 50.7 65.3 64.5 59.9 58.5	56.2 52.1 64.0 65.7 58.1 58.9	56°3 54°7 63°7 65°1 55°3 57°1	55.0 54.7 65.3 62.3 53.9 58.1	56.9 55.1 62.4 63.7 54.5 56.7
	28 29 30 31	57 ° 9 52 ° 9 38 ° 8	60°9 55°0 40°2	60°5 55°0 40°2	62°0 55°1 42°1	65.9 54.2 43.1	61.7 56.1 44.6	67.5 56.5 43.3	68°1 54°6 45°3	67 1 51 6 43 8	68.8 49.8 44.5	69°1 48°5 45°7	70°3 46°9 46°4
Hourly	Means	47.01	49.17	50.76	52.54	53.63	54.61	55.03	55.26	55.04	54.65	54.45	54.25
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	42.9 46.2 64.1	44.2 51.4 63.9	45°3 54°3 63°9	45.7 56.5 65.2	45.5 58.3 65.5	46°3 59°7 65°5	47.8 60.1 66.2	47.0 60.8 65.9	50'9 61'0 66'3	52.5 60.3 66.3	53.9 58.8 66.1	55.7 60.3 65.3
	4 5 6 7 8 9	54.0 46.4 43.2 48.0 52.9 58.0	55°8 48°2 44°6 51°2 56°8 59°4	59.7 48.4 45.7 54.2 61.9 58.8	60°1 49°4 47°1 55°9 61°9 61°3	60°3 48°4 48°7 59°3 62°1 64°4	61.7 49.1 50.1 60.1 63.0 63.3	61'9 50'0 52'0 59'3 63'5 63'5	57.7 50.4 52.2 59.3 63.5 64.4	56°9 49°4 53°1 59°6 63°9 64°6	61 · 3 49 · 9 53 · 5 60 · 7 64 · 6 64 · 4	62.4 49.1 52.3 62.5 65.7 62.0	58.0 47.4 52.2 59.5 64.9 64.4
JUNE.	11 12 13 14 15 16 17	43.6 41.1 42.4 59.3 68.4 64.9	43 · 2 40 · 6 42 · 4 63 · 7 69 · 3 69 · 0	42.8 43.2 46.4 68.6 71.1 70.9	43.1 42.9 50.3 70.1 72.4 71.5	43.9 45.1 50.9 72.4 73.4 73.3	43.4 46.0 54.8 70.7 75.6 74.3	44.8 46.8 53.4 72.1 72.4 74.7	45.4 47.2 53.5 71.7 74.1 72.3	45.7 46.4 56.2 71.1 74.0 71.3	46.9 47.3 57.3 70.9 74.1 73.3	46.4 47.2 59.0 68.9 72.3 71.3	45.6 46.6 58.1 68.5 72.5 72.7
	18 19 20 21 22 23 24	63.8 61.7 57.2 55.7 60.9 56.1	65°0 64°3 60°8 57°3 62°1 57°3	66.5 66.5 59.9 63.1 63.6 57.9	69.5 67.5 61.9 64.9 64.3 56.5	69.9 69.2 61.5 63.6 66.7 56.3	71.5 67.9 60.5 63.8 69.0 57.0	71.7 69.5 61.5 64.6 68.5 56.4	71.7 67.7 61.9 65.8 70.3 55.9	69°3 67°6 61°0 64°5 66°3 55°9	69°3 66°5 61°4 64°3 64°1 56°9	70.5 67.5 62.3 63.9 60.9 54.5	69.0 58.6 62.0 61.1 60.7 54.1
	25 26 27 28 29 30	60°3 58°2 68°9 56°5 56°9	64 ' 9 63 ' 0 68 ' 1 59 ' 8 58 ' 9	67.9 66.1 69.7 63.5 64.2	68.8 68.5 70.2 66.3 64.8	70°1 69°1 69°7 66°3 66°0	70.4 68.9 68.7 65.6 67.3	71.4 70.1 65.0 66.3 65.9	71.4 70.9 65.3 67.3 66.3	71.1 70.9 64.6 67.9 67.0	70.6 70.1 66.1 68.1 68.1	70'9 70'9 64'5 67'9 67'5	70·1 66·2 62·1 67·1 68·5
Hourly	y Means	55.06	57.12	59:39	60.64	61.23	62.08	62.58	62:30	62.17	62.65	62.58	61.50

					WET	THERMO	METER.					
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
45.2 48.4 51.0 49.6 57.6 58.4	42.6 46.0 48.4 50.2 54.9 60.1	41°3 43°4 46°7 51°1 58°8 60°1	39.7 41.4 45.0 50.9 59.0 58.4	39°4 40°2 43°2 51°2 54°2 57°4	38.8 38.7 42.2 51.0 54.4 55.8	38.6 43.6 43.4 50.1 53.6 45.0	37.5 44.1 41.8 49.4 53.4 	36.7 42.4 41.7 49.4 50.7	36.9 39.8 41.7 49.4 49.5 	36.6 37.8 39.8 49.0 48.0 	36.8 $39.6$ $38.8$ $47.2$ $47.2$ $ 36.8$	41.53 44.90 47.79 49.20 57.18 54.99
47.0 50.0 48.6 45.5 45.9 37.4	45.8 49.6 48.2 44.2 43.2 38.6	44.2 49.4 47.6 42.7 39.6 39.4	44.2 48.6 46.7 42.3 37.3 39.6	44.6 48.4 46.2 41.4 36.8 40.0	44.9 47.4 46.6 40.8 34.2 39.8	44'4 44'8 46'6 40'2 33'4	42.8 42.8 46.6 40.1 30.6	41°0 45°4 46°4 38°9 30°6	39°0 45°8 46°2 38°4 31°6	38.6 45.7 46.0 37.2 30.0	38.6 43.4 46.0 36.9 31.4 	44.70 48.71 47.68 43.40 39.41 38.40
45.9 53.6 52.7 62.2 65.1 65.6	46.6 52.0 51.2 58.9 60.9 65.6	44.6 49.6 50.5 55.4 55.9 62.4	45.2 48.6 49.4 53.4 56.8 56.7	45.6 46.1 47.9 52.6 58.3 57.7	45°8 44°4 47°1 51°1 58°2 59°6	38 · 4 46 · 2 42 · 8 47 · 8 50 · 2 57 · 5	35.4 46.9 40.4 47.0 49.4 57.2	33.0 47.0 38.2 46.4 49.0 57.1 	31 · 2 47 · 0 38 · 4 44 · 6 49 · 0 56 · 7 — 58 · 6	31 2 46.7 36.7 44.0 49.3 55.7 — 57.8	$ \begin{array}{c} 32 \ 0 \\ 47 \ 1 \\ 37 \ 4 \\ 43 \ 9 \\ 50 \ 2 \\ 56 \ 3 \\ - \\ 56 \ 9 \end{array} $	46.19 48.89 50.77 55.86 60.31 62.58
55°1 54°2 59°7 59°9 53°9 59°1	53.4 51.8 58.8 57.6 52.2 56.9	52°1 51°3 56°7 54°9 49°4 51°5	49.9 52.3 54.5 50.7 45.5 50.5	50°5 51°7 54°7 50°1 46°4 50°2	52.9 51.2 54.1 48.6 45.5 50.1	59°3 51°7 52°2 53°3 48°6 45°2	59°1 52°9 52°4 51°9 48°0 45°0	52.7 54.4 51.5 48.0 44.2	52'4 53'9 50'3 47'0 44'1	52.1 55.9 50.1 44.6 43.7 	50.97 $52.1$ $54.9$ $52.3$ $45.1$ $43.8$ $ 52.7$	53.73 52.49 57.63 55.98 50.05 54.55
70°6 45°6 46°0	67.0 44.5 45.8	63°0 43°6 46°0	59.6 43.3 45.0	57.8 44.0 42.4	54.7 43.8 42.2	54.9 52.3 41.4 42.1	53 · 9 51 · 9 39 · 8 40 · 4	53.9 51.3 40.0 38.8	53 ° 9 49 ° 7 39 ° 2 38 ° 4	38.6 37.6	47.4 38.8 38.3	60°56 47°45 42°54
53.10	51.67	50.04	48.69	48'11	47.55	46.95	45.80	45.34	44.74	44.09	44.14	50.27
52.5 59.9 64.2	51.5 59.5 60.9	46.8 58.5 60.9	43.6 55.9 59.8	44.4 58.0 58.7	44.8 59.8 56.9	43.4 59.4 — 57.9	43.5 59.1 — 57.9	42:3 57:2 — 57:7	42.6 58.3 — 57.3	40.7 59.9 — 52.9	$     \begin{array}{c}       41.0 \\       62.3 \\       \hline       49.6     \end{array} $	46.45 58.15 61.62
54'3 47'0 52'1 55'7 63'2 64'9	54.4 45.8 48.7 55.7 60.2 60.6	51.2 45.4 48.0 55.1 57.9 58.3	50.9 45.2 46.0 54.9 57.5 57.9	50°1 42°0 45°5 54°6 56°6 53°9	48.8 43.6 45.4 53.5 55.7 50.9	47.6 42.5 45.5 53.4 55.5	45.8 41.2 45.2 50.7 54.9	45°3 40°5 44°8 49°9 53°9	44.3 39.7 44.4 49.0 54.9	44.5 40.0 44.3 47.7 54.3	$ \begin{array}{c} 45.6 \\ 40.1 \\ 44.7 \\ 48.0 \\ 54.7 \\ \hline$	53.86 45.80 47.89 54.91 59.33 56.43
45.0 46.1 59.0 69.5 75.9 69.9	43.6 45.2 60.3 68.1 71.4 66.8	42.4 44.6 55.6 69.2 69.9 64.9	41 · 2 44 · 2 53 · 1 65 · 7 66 · 6 64 · 3	39.6 44.0 51.9 64.9 66.5 64.1	40.6 42.6 51.5 65.7 65.9 64.0	46.0 39.0 42.5 50.6 65.9 64.9	44.6 36.7 41.5 50.2 68.3 63.4	43.6 38.6 40.3 49.0 67.7 62.4	42.4 38.6 38.6 47.4 66.5 60.5	41.6 38.8 38.4 50.0 65.5 58.9	39.7 38.0 51.2 65.8 59.1	42.44 43.60 51.85 67.95 68.96
67.1 62.1 59.8 59.3 60.5	66°2 61°1 59°1 60°3 58°5	64.5 61.1 56.5 58.7 57.0	63.8 60.5 55.9 58.0 56.3	63°3 59°6 54°5 57°8 55°5	62.7 57.9 53.4 57.1 54.3	62.7 62.7 56.1 51.7 57.7 55.1	62.5 61.3 55.5 51.7 57.9 55.4	62.9 59.7 52.9 51.9 58.7 55.1	63.7 58.9 51.9 51.7 58.9 54.8	61:1 59:0 53:3 51:9 60:7 54:1	60.8 5 59.9 53.7 53.0 60.7 53.9	52.83 61.68 57.63 60.77 60.33
53°3 64°9 66°7 62°9 66°4 67°7	53°1 62°5 69°1 62°9 64°2 66°1	50°1 60°7 68°7 61°7 63°9 65°7	48.7 59.3 66.8 59.7 57.6 64.5	46.6 60.1 66.1 58.7 56.1 66.3	46.5 	58°1 60°2 63°9 55°9 54°1 63°8	57°3 59°9 66°5 54°4 53°0 62°7	55.7 58.9 66.1 54.2 51.2 61.7	55.9 55.9 65.9 54.1 49.8 59.3	55°9 55°9 66°5 53°3 51°7 55°9		54.70 64.39 67.15 62.13 60.78 63.82
60.38	3 59.07	57:59	56.07	55.36	54.78	54.47	53.89	53.16	52.21	52.18	52.44	57.96

ours of N Göttinge	Mean }	0	1	2	3	4	5	6	7	8	9	10	11
Time. ours of M Toront	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
Time	$\frac{1}{\left(\begin{array}{c c}1\\2\\3\end{array}\right)}$	76 100 89	81 100 86	82 100 90	86 91 83	93 96 87	89 91 82	79 92 73	74 95 70	87 96 66	98 95 73	95 94 83	96 94 73
	4   5   6   7   8   9   10	94 94 95 95 92 85	92 95 99 86 94 86	94 97 98 81 90 84	96 93 96 83 91 95	90 92 99 83 77 86	84 87 95 80 84 82	80 92 95 71 79 84	79 86 95 78 79 83	75 86 99 81 84 93	84 79 100 79 90 82	88 90 100 84 86 81	90 94 97 86 88 84
ANUARY.	11 12 13 14 15 16 17	87 93 78 93 86 76	83 90 84 95 84 78	86 83 90 93 83 70	82 90 93 89 84 73	96 88 86 80 80 75	66 75 87 71 76 69	75 68 79 76 80 71	68 64 78 76 78 60	72 69 73 70 78 65	76 71 75 71 76 63	73 72 76 80 75 68	75 78 78 78 78 79 60
JAN	18 19 20 21 22 23 24	72 85 89 87 85 81	58 88 91 52 87 81	56 83 90 68 90 82	81 91 93 100 85 77	61 91 92 80 82 74	79 87 88 88 84 67	66 91 88 96 83 83	66 87 94 85 70 85	73 87 94 64 82 87	75 92 94 69 76 74	78 93 90 68 83 77	81 87 83 67 86 88
Fel	25 26 27 28 29 30 31	98 85 87 91 700 73	98 87 90 87 98 72	97 90 90 86 99 74	99 84 89 90 99 78	94 80 86 80 91 79	95 80 83 80 97 85	99 83 76 80 98 66	96 81 79 79 97 66	97 78 73 86 94 76	97 78 75 92 95 77	97 86 88 90 98 57	93 86 83 90 95 63
Hourly 1	Means	88	86	86	89	85	83	82	80	81	82	83	83
	$\begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$	In. 121 213 149	In. 131 221 146	In. 135 223 153	In. •150 •203 •145	In. •163 •228 •156	In. •166 •206 •162	In. •144 •199 •150	In. •139 •205 •145	In. 158 202 141	In. 179 200 154	In. 178 194 171	In. 18 19 15
	4 5 6 7 8 9	146 138 192 181 144 139	143 160 199 168 145	144 166 197 161 136 144		165 172 209 162 119	156 166 205 160 128 140		165 171 207 153 126 152	156 171 210 161 126 159	·172 ·159 ·214 ·154 ·145 ·143	·176 ·167 ·207 ·162 ·146 ·135	·17 ·17 ·19 ·16 ·14 ·13
JANUARY.	11 12 13 14 15 16 17	·120 ·066 ·123 ·096 ·148 ·059	115 1065 129 128 149 1060	118 068 138 146 145 050	111 1076 146 159 149 1051	·120 ·090 ·143 ·160 ·145 ·055	·095 ·087 ·157 ·148 ·136 ·051	120 088 149 168 134 053	102 1085 154 180 125	106 1093 177 174 122	106 106 1095 154 181 112 051	· 098 · 092 · 155 · 186 · 109 · 051	· 09 · 09 · 14 · 18 · 11 · 04
Jensior	20 21 22 23 24	·047 ·061 ·109 ·037 ·054 ·092	·036 ·063 ·112 ·025 ·054 ·088	· 035 · 061 · 111 · 032 · 054 · 095	.056 .070 .114 .054 .065 .097	·048 ·081 ·111 ·052 ·073 ·108	·067 ·079 ·112 ·063 ·085 ·112	·061 ·090 ·112 ·079 ·091 ·144	·061 ·097 ·121 ·083 ·079 ·151	·067 ·104 ·126 ·068 ·095 ·162	·071 ·114 ·129 ·074 ·092 ·151	.075 .013 .128 .072 .101 .156	*07 *10 *11 *06 *10 *16
	25 26 27 28 29 30 31	·190 ·088 ·152 ·173 ·220 ·076	193 1082 160 168 1217 108	195 1083 163 170 210	 ·205 ·083 ·165 ·177 ·224 ·062	·220 ·084 ·165 ·165 ·226 ·063	173 1090 173 170 1228 1075		·214 ·101 ·171 ·171 ·240 ·065	·216 ·101 ·167 ·180 ·242 ·081	·216 ·103 ·166 ·189 ·240 ·071	·209 ·109 ·186 ·187 ·244 ·063	19 10 17 18 23 06

Note. —Wet Thermometer higher than the Dry Thermometer where the reading appears in italics.

	HUMIDITY OF THE AIR, AND TENSION OF THE ATMOSPHERIC VAPOUR.       12     13     14     15     16     17     18     19     20     21     22     23     Daily and Monthly Means.       6     7     8     9     10     11     12     13     14     15     16     17     Means.														
12	13	14	15	16	17	18	19	20	21	22	23				
6	7	8	9	10	11	12	13	14	15	16	17				
95 94	95 88	93 90	95 91	93 80	88 80	92 85	96 74	700	98 81	700 77	90 78	91 89			
78	67	66 —	70	84	74 —	97	88	90	92	94	$-\frac{1}{94}$ }	81			
97 90	92 84	90 94	95 92	94 95	93 95	90 94	94 92	86 94	93 96	93 95	94 97	90 92			
97	96	99	96	96	97	95	91	95	93	91	93	96			
97 94	88 97	$\frac{91}{92}$	95 90	98 80	98 87	91 87	95 94	90 95	89 90	$\frac{87}{95}$	90 94	87 89			
85	80	86	92 —	89	82 —	<del></del> 88	<del></del> 84	<del></del> 85	$\frac{-}{85}$	83	$\frac{-}{90}$ }	86			
76	75	82	83	73	88	91	91	90	90	92	86 87	82			
76 83	87 85	$\begin{array}{c} 79 \\ 92 \end{array}$	78 88	82 89	82 89	82 86	83 93	76 94	79 93	79 94	100	80 86			
72 77	66 80	68 81	84 80	82 75	83 73	87 76	89 79	83 79	80 85	$\frac{87}{83}$	· 90 · 99	81 80			
68	63	69	81	90	77			_			— n	70			
81	69	83	$\frac{-}{74}$	83	81	$\begin{array}{c} 78 \\ 92 \end{array}$	61 90	$\begin{array}{c} 70 \\ 83 \end{array}$	$\frac{63}{83}$	66 92	66 } 96	77			
89	86	81	68 95	79 94	79 99	88 100	91 700	91 100	88 700	$\begin{array}{c} 88 \\ 95 \end{array}$	87 86	87 91			
80 75	76 78	$\begin{array}{c} 77 \\ 82 \end{array}$	84	85	90	85	89	98	89	87	84	81			
89 87	88 86	83 85	$\frac{92}{85}$	85 91	88 81	94	89	95	91	90	81	86 0.5			
				_		97	95	94	$\frac{93}{81}$	89 81	99 } 81	$\frac{85}{93}$			
96 77	95 82	100 81	93 85	93 87	87 84	$\frac{93}{82}$	$\frac{92}{87}$	84 86	84	93	93	84			
85 88	81 93	$\begin{array}{c} 79 \\ 93 \end{array}$	93 91	93 99	$\begin{array}{c} 92 \\ 100 \end{array}$	$\frac{86}{95}$	94 700	$\frac{92}{99}$	91 400	91 400	90 100	$\frac{86}{91}$			
98	97	98	95	91	88	86	78	90	89	92	98	94			
63	84	78 —	66	81	74 —	93	91	91	88	83	77 }	76			
85	84	85	86	87	86	89	89	89	88	90	90	86			
In. 199	In. 192	In. 192	In. 195	fn. 193	·185	·191	In. 199	In. •206	In. •204	In. •212	1n . 199	In. 176			
194	171	·170 ·131	167 134	149 149	·149 ·133	·140	·121	123	·130	125	129	177			
.162		· <del>14</del> 0	·150	· <del>1</del> 47	·144	`180 `140	170 134	$^{:172}_{:119}$	$^{`164}_{`125}$	165 128	138 }	$^{\circ}152$			
173	144 168	.183	176	175	175			113		191	187	173			
196 178	194 158	.203				178	177	183	194						
160			197 159	195 163	.198	194	192	195	•190	176	178	198			
	·163	·155 ·152	159 145	.163 .129	198 163 137					176 140 156	178 143 155				
140		*155 *152 *145 —	159	163	198 163 137 143	194 149 137 —	$^{\cdot 192}_{\cdot 153}$	195 145	190 143 145 — 121	176 140 156 —	$\begin{array}{c} `178 \\ `143 \\ `155 \\ \hline 00000000000000000000000000000000000$	198 158 142 140			
·140 ·094	163 134 	155 152 145 —	159 145 157 — 094	163 129 155 —	198 163 137 143 —	194 149 137 — 133 082	192 153 147 — 125 080	195 145 148 — 125 078	190 143 145 — 121 1078	176 140 156 — 119 1073	178 143 155 	`198 `158 `142 `140 `096			
140  1094 1085 147	163 134 — 1092 1083 123	155 152 145 — 097 096 126	159 145 157 — 1094 098 143	163 129 155 — 076 102 140	198 163 137 143 — 085 104 139	194 149 137 — 133 082 110	192 153 147 ———————————————————————————————————	195 145 148 - 125 078 109 114	190 143 145 	176 140 156 	178 143 155 -126 168 136 106	198 158 142 140 096 095			
140 	163 134 	155 152 145 	159 145 157 — 1094 1098 143 185	163 129 155 - 1076 102 140 189	198 163 137 143 	194 149 137 — 133 082 110 122 186	192 153 147 — 125 080 112 107 186	195 145 148 — 125 109 114 165	190 143 145 — 121 1078 117 103	176 140 156  119 103 120 103	178 143 155 	198 158 142 140 096 095 135			
140  1094 1085 147	163 134 — 1092 1083 123	155 152 145 — 097 096 126	159 145 157 — 1094 098 143	163 129 155 	198 163 137 143 — 085 104 139	· 194 · 149 · 137 — · 133 · 082 · 110 · 122 · 186 · 081 —	192 153 147 	195 145 148 	190 143 145 	176 140 156 — 119 120 103 159 172 —	178 143 155 	198 158 142 140 096 095			
140 -094 1085 147 177 105 1046 -067	163 134 	155 152 145 	159 145 157 - 094 098 143 185 098 053 - 054	163 129 155 — 102 140 189	198 163 137 143 — 1085 104 139 183 1081 1044 1052	· 194 · 149 · 137 — · 133 · 082 · 110 · 122 · 186 · 081 — · 059 · 057	192 153 147 — 125 080 112 107 186 080 — 045 056	195 145 148 125 078 109 114 165 075 	190 143 145  121 078 117 103 157 079  043 055	176 140 156 119 073 120 103 159 072 045	178 143 155 - 126 068 136 106 154 078 - 044 065	198 158 142 140 096 095 135 166 110			
140 	163 134  1092 1083 123 163 108 1044  1054 110	155 152 145 	159 145 157 - 094 098 143 185 098 053 - 054 095	163 129 155  1076 102 140 189 1990 056  056 107	198 163 137 143 - 085 104 139 183 081 044 - 052 107	· 194 · 149 · 137 — · 133 · 082 · 110 · 122 · 186 · 081 — · 059 · 057 · 106	192 153 147 — 125 080 112 107 186 080 — 045 056 110	195 145 148 125 078 109 114 165 075 	190 143 145 — 121 1078 117 103 157 1079 — 043 1055 108	176 140 156 119 073 120 103 159 072 045 061 110	178 143 155 - 126 068 136 106 154 078 - 044 1065	198 158 142 140 096 095 135 166 110 050			
140 	163 134 1092 1083 123 163 108 1044 1054 110 1096 1070	155 152 145	159 145 157 1994 1998 143 185 1998 1053 1054 1995 1995	163 129 155 1076 102 140 189 1090 1056 107 1081	198 163 137 143 1085 104 139 183 081 044 052 107 078	· 194 · 149 · 137 — · 133 · 082 · 110 · 122 · 186 · 081 — · 059 · 057 · 106 · 070 · 062	192 153 147 — 125 080 112 107 186 080 — 045 056 110 063 072	195 145 148 - 125 078 109 114 165 075 - 049 054 110 056 065	190 143 145 121 078 117 103 157 079 043 055 108 050 057	176 140 156 119 073 120 103 159 072 045 061 110 047	178 143 155	198 158 142 140 096 095 135 166 110 050 058 093 095			
140 	163 134 1092 1083 123 163 108 1044 1054 110 1096 1070 1093	155 152 145	159 145 157 1094 1098 143 185 1098 1053 1054 1095 1095 1072 1089	163 129 155 1076 102 140 189 1056 107 081 1070 1081	198 163 137 143 1085 104 139 183 081 044 052 107 078 074 079	· 194 · 149 · 137 — · 133 · 082 · 110 · 122 · 186 · 081 — · 059 · 057 · 106 · 070	192 153 147 — 125 080 112 107 186 080 — 045 056 110 063	195 145 148 	190 143 145	176 140 156 119 073 120 103 159 072 045 061 110 047 052 086	178 143 155	198 158 142 140 096 095 135 166 110 050 058 093 095 062			
140 1094 1085 1147 1177 1105 1046 1067 1108 107 1068 1098 1160	163 134 1092 1083 123 163 108 1044 1054 110 1096 1070 1093 151	· 155 · 152 · 145 · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · ·	159 145 157 1094 1098 143 185 1098 1053 1054 1095 1072 1089 1154	163 129 155  1076 102 140 189 1090 1056 107 081 160 160	198 163 137 143 1085 104 139 183 1081 1044 1052 1107 1078 1074 1079 1157	· 194 · 149 · 137 — · 133 · 082 · 110 · 122 · 186 · 081 — · 059 · 057 · 106 · 070 · 062 · 081 — · 178	192 153 147 — 125 080 112 107 186 080 — 045 045 063 072 070 — 169	195 145 148 - 125 078 109 114 165 075 - 049 054 110 056 065 074 - 165	190 143 145 121 078 117 103 157 079 043 055 108 057 087 163	176 140 156 119 073 120 103 159 072 045 061 110 047 052 086 167	178 143 155	198 158 142 140 096 095 135 166 110 050 058 093 095 062 081			
140 1094 1085 1147 1177 1105 1046 108 1107 108 107 108 1098 160 185	163 134 1092 1083 123 163 108 1044 1054 110 1096 1070 1093 151 179	155 152 145	159 145 157 1094 1098 143 185 1098 1053 1054 1095 1072 1089 1154 1160	163 129 155  1076 102 140 189 1090 1056 107 081 160 159	198 163 137 143 1085 104 139 183 081 044 1079 157 143	· 194 · 149 · 137 — · 133 · 082 · 110 · 122 · 186 · 081 — · 059 · 057 · 106 · 070 · 062 · 081 — · 178 · 158 · 135	192 153 147 — 125 080 112 107 186 080 — 045 045 063 072 070 — 169 156	195 145 148 125 078 109 114 165 075 049 054 110 056 065 074	190 143 145 121 078 117 103 157 079 043 055 108 050 057 087	176 140 156 119 173 120 103 159 1759 1661 110 1647 1652 1667 167 167	178 143 155 126 126 136 106 154 078	198 158 142 140 096 095 135 166 110 050 058 093 095 062 081 145			
140 1094 1085 1147 1177 1105 1046 1067 108 107 1068 1098 160 185 1097 172	163 134 1092 1083 123 163 108 1044 1054 110 1096 1070 1093 151 179 115 162	155 152 145	159 145 157 - 094 098 143 185 098 053 - 054 095 095 072 089 154 - 160 126 180	163 129 155 — 076 102 140 189 090 056 — 056 107 081 160 — 159 134 178	198 163 137 143 — 1085 104 139 183 081 044 — 052 107 078 074 1079 157 — 143 137	· 194 · 149 · 137 — · 133 · 082 · 110 · 122 · 186 · 081 — · 059 · 057 · 106 · 070 · 062 · 081 — · 178 · 158 · 135 · 162	192 153 147 — 125 1080 112 107 186 1080 — 1045 1056 110 1063 1072 1070 — 169 156 138 166	195 145 148 - 125 078 109 114 165 075 - 049 054 110 056 065 074 - 165 124 139 164	190 143 145	176 140 156 119 173 120 103 159 175 1045 1061 110 1047 1052 1086 167 1097 147	178 143 155	198 158 142 140 096 095 135 166 110 050 058 093 095 062 081 145 174 113 168			
140	163 134 1092 1083 123 163 108 1044 1054 110 1096 1070 1093 151 179 115	155 152 145	159 145 157 1994 1998 143 185 1998 1053 1054 1995 1072 1089 154 1160 126 180 200 235	163 129 155  1076 102 140 189 1056 107 1081 1070 1081 160 159 134	198 163 137 143 — 1085 104 139 183 081 044 — 052 107 078 074 157 — 143 137 174 212 192	· 194 · 149 · 137 — · 133 · 082 · 110 · 122 · 186 · 081 — · 059 · 057 · 106 · 070 · 062 · 081 — · 178 · 158 · 135	192 153 147 — 125 1080 112 107 186 1080 — 1045 1056 110 1063 1072 1070 169 156 138	195 145 148 - 125 078 109 114 165 075 - 049 054 110 056 065 074 - 165 124 139	190 143 145 121 1078 117 103 157 1079 1043 1055 108 1057 1087 163 105 138	176 140 156 119 073 120 103 159 072 045 061 110 047 052 086 167 097 147 167 212 108	178 143 155 126 126 136 106 154 078	198 158 142 140 096 095 135 166 110 050 058 093 095 062 081 145			
140	163 134 1092 1083 123 163 108 1044 1054 110 1096 1070 1093 151 1179 115 162 198	155 152 145	159 145 157 1994 1998 143 185 1998 1053 1054 1995 1072 1089 1154 1160 1126 1180 1200	163 129 155 — 076 102 140 189 090 056 — 056 107 081 160 — 159 134 178 210	198 163 137 143 — 1085 104 139 183 081 044 — 052 107 078 074 1079 157 — 143 137 174 212	· 194 · 149 · 137 — · 133 · 082 · 110 · 122 · 186 · 081 — · 059 · 057 · 106 · 070 · 062 · 081 — · 178 · 158 · 135 · 162 · 203	192 153 147 — 125 080 112 107 186 080 — 045 056 110 063 072 070 — 169 156 138 166 219	195 145 148 - 125 078 109 114 165 075 - 049 054 110 056 065 074 - 165 124 139 164 209	190 143 145	176 140 156 119 073 120 103 159 072 045 061 110 047 052 086 167 097 147 167 212	178 143 155	198 158 142 140 096 095 135 166 110 050 058 093 095 062 081 145 174 113 168 192			

12	13	14	15	16	17	18	19	20	21	22	23	Daily an
6	7	8	9	10	11	12	13	14	15	16	17	Monthly Means.
84	87	89	91	87	88	90	97	95	98	98	99	87
66	64	67	74	72	86	80	95	76	91	80	79	80
73	76 50	73	70	59	60	57	62	61	62	66	69	68
64 78	59 78	71 78	80 82	$\begin{array}{c} 74 \\ 83 \end{array}$	73 94	$\begin{array}{c c} 78 \\ 92 \end{array}$	80 97	82 91	$\begin{array}{c c} 85 \\ 91 \end{array}$	89 95	87 94	$\frac{69}{82}$
77	$\frac{70}{70}$	64	70	$\frac{33}{72}$	69		-				<u>}</u> ]	83
						88	89	91	94	95	96 }	
64 80	$\begin{array}{c} 71 \\ 79 \end{array}$	76 87	88 94	83 95	89 94	87 94	87 89	87 91	89 89	84 91	78 94	$\begin{array}{c} 72 \\ 86 \end{array}$
89	82	86	81	86	81	80	83	85	84	68	67	86
90	93	93	94	88	85	88	93	85	81	84	86	88
80 87	80 83	80 78	82 80	88 76	93 88	92	100	87	100	100	92	83
-		10		- 10	- 00	96	91	94	$\frac{-}{94}$	89	$\frac{-}{88}$	87
94	94	91	91	91	92	88	91	89	91	91	94	89
89	90	86	86	90	84	86	92	81	96	95 85	85 89	89 85
83 77	$\frac{95}{86}$	94 97	94 93	100 100	100 98	96 97	$\begin{array}{c} 95 \\ 98 \end{array}$	88 93	84 97	96	93	82
92	96	93	96	93	93	99	91	89	92	99	87	94
89	87	86	82	80	75						$\frac{-}{93}$ }	84
85	$\frac{-}{82}$	 81	84	81	77	91 53	$\begin{array}{c} 92 \\ 75 \end{array}$	83 77	92 82	400 83	100	80
79	79	83	86	85	82	87	79	90	84	59	68	83
76	64	76	72	78	79	60		-				80
70 94	68 100	61 90	94	86	97	94	89	$\frac{}{92}$	94	— 85	$\frac{-}{78}$	71 88
71	73	71	70	<b>74</b>	77	<del></del>	<del></del>				<u> </u>	79
_						92	76	80	80	80	66 }	13
80	81	81	84	84	85	85	88	86	89	87	86	83
In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
139	145	148	.160	157	157	154	164	164	.169	.171	165	139
153	148	146	155	149	166	148	.170	134	153	133	130	166
150	158	158	152	142	147	138	142	138	134	141	141	.138 .133
131 161	·119 ·157	129 156	148 161	130 164	128 163	132 157	·126 ·151	129 140	130	133 138	122	150
169	136	104	.091	.082	.073	_			_		}}	•139
			•050	.054	-057	103	104	106	108 050	109 049	108 3	.053
050 110	$\begin{array}{c} \cdot 052 \\ \cdot 113 \end{array}$	.054 .128	·059 ·128	.054 .134	.057 .139	.052 .136	$\overset{\boldsymbol{.}052}{\cdot 126}$	.052 .115	112	109	113	.100
089	.080	.078	.072	.075	.070	.063	.066	.067	.047	.035	.030	.081
095	.097	095	.096	.090	.094 .128	.108	*110	106	105	111 085	.115 .086	.096 .124
136 154	`140 `148	144 129	$^{\cdot 142}_{\cdot 132}$	146 127	136	102	<b>.</b> 096	·077	·085			
-						.098	.100	.106	.109	106	$\frac{-104}{104}$	129
120	120	115	110	109	106	1094	.101	100	·103 ·071	·105 ·060	·107 ·049	`112 `113
125 086	·121 ·081	·113 ·071	110 071	113 074	·100 ·073	.102 .066	·101 ·061	*084 *059	.053	.023	.055	.080
121	136	134	131	140	138	136	135	124	129	127 ,	124	.113
136	136	120	135	135	135	.139	.130	127	133	.131	127	•136
123	.120	112	105	.092	·084		$\cdot \frac{-}{092}$	.086	.086	.090	$-\overline{079}$	.113
095	.088	.082	.080	.080	.071	.020	.068	.069	.069	.067	*079	.086
070	.060	.059	.056	.051	.045	050	.052	.052	.044	.029	.035	.068
064 048	·049 ·032	·052 ·031	.043	.048	.047	.028		_	_	_		043
075	.076	.070	.071	.066	.072	.071	.068	.071	.072	.065	•062	.069
073 —	·074	·070	.068	.070	.070	.090		.072	.072	.072	$\cdot _{057}^{-}\}$	.076

lours of Göttir Tio	f Mean	0	1	2	3	4	5	6	7	8	9	10	11
************	f Mean	18	19	20	21	22	23	0	1	2	3	4	5
	2 3 4 5 6 7	72 79 82 78 90 76	88 79 70 79 95 85	92 64 79 73 88 94	98 75 81 72 81 96	94 65 78 64 78 89	70 70 68 58 77 92	83 68 79 70 71 91	64 72 71 73 79 95	86 77 77 69 78 98	78 78 79 52 77 97	68 72 76 72 78 94	70 78 70 66 83 95
ie Air.	8 9 10 11 12 13 14	75 86 90 83 93 98	73 98 94 84 95 96	70 73 87 82 95 96	68 71 77 97 88	67 68 71 74 99 82	71 72 72 69 98 90	74 68 75 75 99 80	75 63 71 81 97 80	72 67 69 94 97 84	78 64 69 94 100 81	81 59 60 95 97 72	82 58 67 93 100 90
Humidity of the	19 20 21	78 75 83 83 94 71	77 77 83 74 95 66	67 83 80 60 89 68	87 70 70 57 56 61	70 67 67 45 81 73	72 69 50 52 84 61	68 73 64 50 73 56	70 67 65 52 64 56	78 64 66 57 67 59	86 63 61 60 71 57	83 65 68 61 67 46	88 72 72 63 75 50
	22 23 24 25 26 27 28	80 95 94 96 93	78 94 93 89 91 88	73 92 93 91 89 85	69 89 97 84 88 82	67 89 93 84 81 70	64 91 95 75 79	76 91 96 81 80 73	61 92 96 68 80 73	70 92 98 65 73 74	67 87 97 74 78 80	67 91 98 81 84 80	68 92 97 83 87 76
	29 30 31	90 95	81 82	79 70	54 70	58 68	55 67	$\begin{array}{c} -\\ 55\\ 73 \end{array}$	66 74	69 70	66 74	75 81	70 93
Hourly	y Means	85	85	81	78	75	73	75	73	76	76	76	78
	$\begin{pmatrix} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{pmatrix}$	In. '061 '057 '073 '143 '140 '056	In.	In. '093 '059 '113 '140 '144 '095	In. '015 '097 '150 '149 '144 '127	In. 122 100 154 146 129 135	In. '096 '116 '142 '140 '127 '146	In. 1110 1113 173 158 123 149	In. '091 '121 '163 '167 '132 '050	In. 123 129 175 167 131	In. 112 131 175 144 127 166	In. 100 121 168 174 129 160	In. 1099 12 16 18 13 16
vapour.	8 9 10 11 12 13 14	·146 ·136 ·131 ·161 ·218 ·203	141 135 130 179 226 204	140 151 157 186 220 219	·144 ·164 ·190 ·237 ·205	·151 ·161 ·173 ·197 ·246 ·197	155 172 170 191 252 214	·163 ·162 ·177 ·202 ·262 ·192	165 152 172 1227 2261 193	·152 ·163 ·166 ·239 ·268 ·192	167 159 169 229 278 187	171 146 147 230 289 161	·17 ·13 ·16 ·22 ·27 ·17
MARCH	3/ 16 H	128 108 103 168 142 133	127 110 115 162 159 125	·112 ·119 ·119 ·137 ·193 ·129	138 108 123 156 156 116	·113 ·107 ·140 ·130 ·205 ·140	120 112 117 161 229 120	·111 ·126 ·146 ·159 ·210 ·115	117 125 154 180 193	137 130 159 176 217	152 133 148 180 220 129	155 134 163 155 196 108	16 14 16 15 20
	22 23 24 25 26 27 28 29	160 222 220 195 194 180	163 ·222 ·220 ·186 ·200 ·176	·165 ·225 ·222 ·199 ·204 ·182	·165 ·222 ·231 ·219 ·206 ·183	·169 ·222 ·230 ·226 ·222 ·168	·168 ·218 ·240 ·216 ·212 ·184	·177 ·218 ·242 ·231 ·220 ·179	169 1220 1246 1201 1214 176	·185 ·224 ·247 ·207 ·211 ·180	171 1224 1246 1208 1202 182	173 ·218 ·238 ·198 ·210 ·179	·17 ·22 ·23 ·19 ·19 ·16
	30 31	.159 .049	158 154	158 146	112 136	·129 ·163	126 177	·152 ·183	164 185	·167 ·179	·157 ·189	·170 ·201	·16

		н	MIDITY	OF THE A	AIR, AND	TENSION	OF THE	ATMOSPH	ERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
67 64 67 59 83 94	80 83 72 48 83 94	77 93 75 62 85 91	78 97 72 68 94 95	80 97 72 56 82 97	85 97 79 59 87 95	86 93 87 66 88	96 99 87 79 99	87 74 87 81 96	83 73 78 85 100	79 81 77 97 96	$ \begin{array}{c} 80 \\ 82 \\ 73 \\ 98 \\ 95 \\ \hline 74 \end{array} $	81 80 77 70 86 87
85 66 70 93 99 87	83 74 73 95 97 86	85 80 74 95 99 82	80 73 83 94 100 78	80 85 84 99 100 79	82 82 83 100 100 79	67 81 88 87 98 100 —	68 79 91 88 100 97 —	71 82 86 88 100 97 —	69 89 86 100 97 	70 100 94 89 98 96 —	92 89 97 98 ——————————————————————————————	76 77 79 90 98
72 89 76 69 74 56	74 84 74 66 71 68	80 81 73 70 63 76	87 87 73 74 90 86	85 84 69 86 84 79	86 88 67 83 69 76	78 91 69 93 71 —	80 88 73 95 71 —	83 78 70 95 69 —	85 61 80 99 65 —	$   \begin{array}{r}     34 \\     86 \\     71 \\     76 \\     97 \\     70 \\     \hline     79   \end{array} $	86 87 78 96 76 78	79 76 71 72 75
62 92 97 88 88 88	78 84 97 92 94 87	67 87 97 89 87 79	85 93 83 90 87 79	88 86 83 92 87 81	89 88 81 90 91 86	90 88 82 91 91	88 94 88 93 88 ——————————————————————————————	89 92 89 97 88 —	86 93 90 94 90 — 84	95 95 91 97 90 —	94 94 94 93 88 	77 91 92 87 86 82
71 63	78 70	80 72	$\frac{-}{85}$	85 78	$\begin{array}{c c} - \\ \hline 91 \\ 73 \end{array}$	91 100 76	87 89	93 90	93 75	93 75	96 75	78 76
77	80	81	84	84	84	85	87	85	85	88	87	81
In. '083 '099 '160 '150 '113 '157	In. '076 '106 '167 '117 '093 '157	In. '072 '097 '168 '133 '085 '156	In. '065 '096 '157 '112 '087 '162	In.	In. '061 '094 '161 '098 '074 '156	In. '060 '110 '155 '097 '065 '138	In. '064 '115 '170 '121 '073 '142	In. '060 '090 '163 '126 '068 '145	In. '061 '080 '152 '139 '069	In. '055 '080 '156 '153 '068 '137	In.	In. '079 '099 '151 '140 '106
169 140 160 227 251 167	147 127 154 230 236 152	139 126 150 218 221 144	1144 1118 1160 2224 220 1137	150 127 162 242 218 136	156 122 163 246 218 136	158 126 157 240 220	158 132 156 243 208	160 127 153 247 201	162 133 151 248 201	171 133 158 228 197	128 159 224 208 - 138	156 141 158 220 235
126 161 154 164 185	120 133 143 148 174 134	124 122 136 147 167 134	124 125 140 147 165 132	117 115 136 151 193 118	115 115 128 139 158 116	161 111 110 130 148 152	160 115 105 146 159 150	124 115 1094 138 159 145	150 114 1074 160 154 133	159 114 086 156 152 139	118 1099 160 154 145	125 116 141 156 176
·156 ·224 ·232 ·203 ·204	184 214 230 202 210	-155 •227 •233 •195 •200	195 239 198 194 196	·204 ·225 ·194 ·196 ·191	·210 ·220 ·189 ·194 ·200	147 214 214 186 195	151 212 219 192 197 186	143 214 211 192 202 183	154 209 215 188 198 178	155 220 220 189 201 178	·153 } ·219 ·217 ·193 ·196 ·176	131 185 221 218 202 200
171 - 157 160	174  160 149	160  158 148	160  131 140	163  141 140	168  146 136	147 181 126	154 158 133	148 165 132	143 165 120	157 159 123	·155 ·159 ·123	168 154 147
165	159	154	153	153	151	152	155	150	149	152	151	159

Vol. III.

			нимі	DITY OF	THE AIR,	AND TE	NSION OF	THE AT	MOSPHER	IC VAPO	JR.		
ours of Göttir Tim	f Mean }	0	1	2	3	4	5	6	7	8	9	10	11
	f Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$ \begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix} $	81 81 74 72	98 73 69 64	70 64 49 72	56 59 50 69	60 59 55 63	53 66 56 67	58 57 60 64	64 54 52 66	61 51 42 61	53 49 38 53	49 52 34 54	59 52 41 48
	5 6 7 8 9	81 85 63 88	82 82 56 75	79 71 62 54	79 70 53 63	75 63 53 68	72 66 53 50	71 65 47 50	69 66 40 46	74 76 35 45	73 68 36 49	76 75 41 53	86 80 35 58
Alf.	10 a 11 12	95	96	95	97	86	77	61	51	47	54	62	59
APRIL.	13 14 15 16 17 18	90 95 78 90 83 55	88 85 78 83 73 64	86 66 78 53 73 81	82 70 69 72 62 82	63 67 79 62 67 87	69 60 78 62 59 79	67 62 68 65 60 85	62 66 63 54 60 74	54 70 85 53 57 78	45 50 58 59 57 69	50 57 33 67 57 69	53 80 56 65 52 66
H	19 20 21 22 23 24 25	89 69 88 86 83 68	80 66 84 89 85 67	81 58 83 99 85 69	71 53 84 94 82 67	67 55 82 86 80 67	62 51 78 80 84 67	62 46 76 75 80 62	57 50 77 75 89 54	50 28 79 70 87 57	50 35 77 72 93 55	50 74 75 66 96 54	53 60 80 75 96 56
	26 27 28 29 30	56 56 88 94	50 42 90 94	38 46 91 88	43 43 88 88	44 44 85 93	44 40 86 91	46 42 85 88	47 45 88 85	51 51 91 91	49 47 93 86	47 50 94 89	47 41 96 91
Hourly	Means	80	77	72	70	68	66	64	62	62	59	61	63
	$\begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix}$	In. '131 '134 '130 '146	In. 165 140 143	In. 144 146 121 176	In. 154 140 127 183	In. 149 140 145	In. 137 166 153	In. 151 148 171	In. 164 139 145	In. 162 132 131 200	In. '140 '130 '112 '183	In. '133 '131 '104 '189	In. *150 *130 *115
	5 6 7 8 9	214 243 123 119	211 249 113 144	·209 ·243 ·132 ·120	·222 ·264 ·114 ·165	·250 ·266 ·121 ·182	·262 ·282 ·131 ·146	-261 *267 *113 *154	266 277 102 151	·273 ·302 ·091 ·153	266 284 094	·279 ·326 ·110 ·148	·297 ·316 ·091 ·141
abom	11 12	•224	·225	.224	.339	329	325	·266	204	·160	162	·175	·152
APRIL.	18	134 146 133 136 160 243	134 168 132 161 191 250	132 153 132 124 216 304	134 181 123 180 228 331	116 185 158 172 257 301	134 174 164 172 241 295	138 170 156 182 249 300	153 182 149 162 256 316	122 189 218 164 239 314	106 130 146 180 249 312	118 162 140 172 254 308	117 204 148 158 233 307
<b>₹</b>	19 20 21 22 23 24 25	155 200 240 297 302	·192 ·264 ·243 ·328 ·320 ·190		·223 ·295 ·250 ·302 ·314 ·172	·241 ·325 ·249 ·307 ·318 ·172	·252 ·337 ·242 ·303 ·341 ·181	· 272 · 334 · 254 · 303 · 336 · 165	·279 ·351 ·276 ·314 ·395 ·156	· 269 · 269 · 283 · 302 · 361 · 177	270 291 375 308 398 162	· 264 · 393 · 281 · 278 · 416 · 155	· 258 · 332 · 267 · 328 · 425 · 162
	26 27 28 29 30	152 176 273	174 170 275 329	150 185 277 326	 196 174 291	·205 ·175 ·296 ·318	·203 ·174 ·295 ·348	 ·208 ·182 ·305 ·364	204 198 299 379	·219 ·232 ·302 ·412	·215 ·236 ·308 ·360	·224 ·254 ·305 ·378	·222 ·221 ·324 ·374
Jours.	Means	189	•202	205	•217	•222	•226	226	•229	•227	•223	•228	•225

^{*} Good Friday.

	HUMIDITY OF THE AIR, AND TENSION OF THE ATMOSPHERIC VAPOUR.           12         13         14         15         16         17         18         19         20         21         22         23         Daily and														
12	13	14	15	16	17	18	19	20	21	22	23	Daily and			
6	7	8	9	10	11	12	13	14	15	16	17	Means.			
67	69	74	67	76	70	70	71	80	85	89	76	69			
57	66	77	87	81	70	70	77	73	76	78	77	67			
56	59 55	59	73	70 66	70	70	67	69	78	87	85	61			
57	99	50	62	66	76	95	94	90	91	84	$\frac{-}{82}$ }	69			
81	84	83	89	88	95	87	89	89	90	89	87	82			
88	88	86	89	77	$\frac{36}{72}$	73	<b>6</b> 8	71	69	62	69	74			
36	49	52	63	57	55	78	78	83	86	85	89	58			
60	62	73	61	67	71						— J	66			
			_	_	=	72	82	81	84	92	90 }	00			
59	61	64	64	69	70	85		96	90	87	$\frac{-}{92}$ }	75			
70	75	70	$\frac{-}{82}$	80	80	77	86 83	85	89	89	90	74			
90	95	98	99	96	94	88	62	68	76	76	70	77			
68	78	86	87	92	92	93		$9\overset{\circ}{2}$	95	95	95	78			
68	76	73	75	75	81	75	79		78	81	89	71			
54	68	72	82	84	90	90	93	85	93	79	63	71			
94	57	70	74	84	78						<del>-</del> }	<b>78</b>			
<del></del>			-			87	87	$\begin{array}{c} 92 \\ 73 \end{array}$	86 70	88 67	93 } 68	64			
79	56 80	59 86	60 91	66 94	74 94	66 93	$\begin{array}{c} 55 \\ 94 \end{array}$	95	90	91	89	$\frac{04}{72}$			
82	86	87	89	93	93	90	91	86	88	94	86	85			
69	67	72	68	65	63	53	55	57	72	$7\overline{2}$	84	74			
97	99	95	96	98	95	92	95	95	96	85	76	90			
56	60	66	68	56	56						<del>-</del> }	61			
						64	60	57	57	63	61 }				
51	59	60	66	61	67	65	64	75 07	73	80 90	76	57 61			
40 95	41 95	58 91	$\begin{array}{c} 62 \\ 94 \end{array}$	67 93	86 94	90 92	94 95	95 95	91 94	90 94	93 94	$\frac{61}{92}$			
88	90	93	96	95	94	95	95	96	93	91	98	92			
6)	71	74	78	78	<del></del>	80	80	82	84	83	83	73			
	11	/1	10	10	1.5		1	02	01		00				
In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.			
160	131	129	112	121	115	114	.114	121	123	126	116	136			
.130	127	129	142	133	115	.118	127	121	126	127	122	.133			
156	122	118	132	136	143	146	.133	128	.131	156	153	135			
174	•162	147	.169	175	189			1000			$-\frac{1}{125}$	•193			
•280		.074	$\frac{1}{276}$	278	•282	·303 ·261	·295 ·263	·283 ·260	$^{:286}_{:252}$	155 244	233	.258			
330	$\begin{array}{c} 277 \\ 321 \end{array}$	$\begin{array}{c} 274 \\ 309 \end{array}$	·288	278	202	201	180	171	150	134	139	251			
.095	.110	108	119	.101	.099	124	119	120	122	121	120	112			
139	136	160	132	136	145					_					
						194	113	209	.213	225	$\cdot \frac{1}{214}$	158			
139	140	142	138	143	143					-	$-\frac{136}{136}$	184			
146	• 1 4 =	-11"	196	191	126	126 123	127	135	133 139	128 139	136 )	130			
219	$\overset{\boldsymbol{\cdot}}{}\overset{145}{}$	.115 .209	$^{\cdot 126}_{\cdot 212}$	$^{:121}_{:200}$	126	123	130 128	$^{129}_{122}$	139	139	140	130			
162	112	152	139	140	137	138	120	136	134	134	130	146			
164	185	177	187	180	195	180	189	_	182	171	170	171			
237	260	·248	241	.231	.238	228	•222	•225	236	243	.250	235			
312	226	`249	259	·248	.208						$-\frac{1}{148}$	251			
					•020	159	162	162	151	147	148 \$	į.			
·253 ·359	243	251	·249	247	·230	·213 ·334	198 333	219	·207 ·268	·205 ·248	·209 ·240	·235 ·312			
258	$\overset{\boldsymbol{\cdot}}{3}\overset{4}{3}$	$\begin{array}{c} 336 \\ 243 \end{array}$	$\overset{\boldsymbol{\cdot}}{2}\overset{\boldsymbol{\cdot}}{3}\overset{\boldsymbol{\cdot}}{4}0$	·348 ·262	·346 ·268	277	283	338 266	268	304	240	267			
293	278	243	$\overset{231}{273}$	$\cdot \frac{202}{272}$	•270	234	$\cdot ^{263}_{232}$	237	265	260	310	289			
408	320	294	298	320	329	320	*339	339	*335	294	223	*336			
162	169	181	.183	165	165			_			$\cdot \frac{-}{145}$	166			
						156	154	143	144	151	145 }				
225	207	179	186	172	182	178	174	182	174	176	167	191			
$^{:201}_{:323}$	194	211	·214	221	252	263	286	·309 ·300	309 304	304	*300 *309	·227 ·301			
362	$\begin{array}{c} \cdot 323 \\ \cdot 349 \end{array}$	306 343	·305 ·344	*300 *348	·299 ·340	·292 ·342	303 341	351	342	*304 *350	*358	*349			
	019		-213		l						194	214			
.227					•209	•209	206	209	.205	•199					

urs of Mean		1	2	3	4	5	e l	77	o	9	10	11
Göttingen							6	7	8			
Toronto	18	19	20	21	22	23	0	l	2	3	4	5 
$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	86 80	85 79	84 73	85 68	77 76	75 71	80 75	82 82	75 80	76 83	85 83	94 79
4	83	72	78	67	63	55	54	52	54	55	54	84
$\begin{vmatrix} 5 \\ 6 \end{vmatrix}$	87 80	72 63	66 55	76 56	77 60	75 60	70 57	$\frac{65}{58}$	74 49	70 51	72 49	80 50
$\begin{vmatrix} 7 \\ 8 \end{vmatrix}$	52 89	46 85	$\begin{array}{c} 43 \\ 82 \end{array}$	$\begin{array}{c c} 45 \\ 75 \end{array}$	56 68	60 67	65 67	67 78	73 69	70 67	76 71	76 76
9	96	95	94	95	93	96	95	96	96	96	97	94
	66	52 50	52	60	60	60	56	46	49	55 50	45	44
$\begin{vmatrix} 12\\13 \end{vmatrix}$	11	59 88	52 90	55 84	$\begin{array}{c} 48 \\ 83 \end{array}$	47 80	$\begin{array}{c} 66 \\ 72 \end{array}$	64 67	61 59	58 59	63 56	54 56
14 15 نيا	- 11	93 94	90 92	83 90	79 87	$\begin{array}{c} 74 \\ 82 \end{array}$	73 78	74 88	67 89	69 92	64 84	62 86
A 16	74	89	85	81	78	66	81	79	77	77	75	74
WAX 16 17 18 19 20	11	84	71	$\frac{-}{65}$	61	50	50	$\frac{-}{35}$	$\frac{-}{42}$	44	41	38
19 20	11	65 63	59 54	46 50	53 42	$\frac{62}{36}$	$\frac{62}{35}$	$\begin{array}{c} 63 \\ 32 \end{array}$	58 40	$\frac{59}{31}$	64 30	65 <b>3</b> 0
21	61	56	65	67	66	66	71	66	68	59	63	61
$\begin{vmatrix} 22\\23 \end{vmatrix}$		69 89	70 89	64 96	64 90	60 87	53 89	56 47	$\frac{49}{73}$	47 71	47 74	67 72
24 25		87	90	88	<del></del> 89	<del></del> 87	88	 88	86	90	92	92
26	96	92	86	85	83	. 82	81	81	83	80 56	80 53	81 57
27 28	92	80 83	73 80	6 <b>7</b> 86	66 85	63 80	61 84	57 80	54 79	77	80	76
30		80 94	68 93	$\begin{array}{c} 69 \\ 92 \end{array}$	74 89	71 87	73 87	72 84	69 84	$\begin{array}{c c} 72 \\ 78 \end{array}$	71 76	77 - 76
(31	- 00	77	74	70	70						67	69
ourly Mean	ns oo	77	14	73	72	69	70	68	68	67	1 07	09
		In. :348 :325	In. :347 :331	In. •350 •335	In. •340 •390	In. :336 :388	In. •348 •366	In. •356 •395	In. •338 •392	In. •329 •392	In. •347 •392	In. •37. •37.
	223	285	-363	•339	•350	.331	.329	•308	*322	$\cdot \overline{327}$	•345	•37
		:276 :272	$^{:213}_{:245}$	$^{\circ}_{246}$	$^{\circ}332$ $^{\circ}241$	:312 :236	·330 ·217	*356 *224	.415 .199	$\overset{\boldsymbol{\cdot}}{}\overset{417}{}$	·410 ·216	· 39 · 22
7	180	183	.180	192	•232	•265	.301	*314	.316	*312	341 345	*34 *35
	404	404	·371 ·413	`374 `404	·354 ·400	·364 ·402	·361 ·404	·393 ·419	·372 ·419	*338 *419	*430	12
$\begin{vmatrix} & & & 10 \\ & & & 11 \end{vmatrix}$	135	112	112	133	.163	·148	148	124	.142	168	•144	•14
		188	. 187 . 290	114 346	·204 ·388	$^{\circ}_{412}^{218}$	·321 ·407	·308 ·390	.316 .386	·302 ·389	·327 ·382	·31
N 14	₹ 398	*438	457	485	*485	<b>.</b> 436	<b>.</b> 438	•453	437	*401	•446	•40 •43
MAY. 16	249	343 305	*328 *353	*343 *391	·358 ·390	*348 *391	*366 *419	·447 ·421	·412 ·405	·454 ·397	·462 ·408	•37
팅     18	353 ∦	343	284	274	256	•221	.219	145	168	175	162	14
20   19 20		176 215	172 214	151 229	$^{`180}_{`224}$	$^{\cdot 228}_{\cdot 212}$	·224 ·209	·236 ·194	$\begin{array}{c} \cdot 237 \\ \cdot 250 \end{array}$	·251 ·193	·274 ·189	·26
21	167	·162 ·222	$^{195}_{238}$	204	•209	·211	•229	·221 ·249	·237 ·230	·220 ·208	·226 ·210	$^{:21}_{:26}$
22 23	329	366	397	·261 ·442	·274 ·477	·283 ·460	·238 ·540	·519	.230	·470	.472	•45
24   25	495	•529	•584	· <del>6</del> 11	620	•594	653	•662	.676	647	618	63
26 27	556	.562 .610	.614 .592	.638 .551	$\begin{array}{c} \mathbf{`618} \\ \mathbf{`535} \end{array}$	.614 .541	$\begin{array}{c} \cdot 652 \\ \cdot 522 \end{array}$	.709 .493	·674 ·482	.644 .484	.613 .485	·61
28	454	473	485	•529	.592	*535	•579	•607	.572	$\cdot 522$	.518 .482	·50 ·44
29	`462	·419 ·450	.435 .486	$^{\cdot 476}_{\cdot 518}$	$\begin{array}{c} \cdot 536 \\ \cdot 625 \end{array}$	·487 ·643	·524 ·659	.514 .655	.504 .630	· 500 · 605	*585	•58
\\31		-	-							_		
(0,	_	·	[ <del></del>					l			378	.36

		н	JMIDITY (	OF THE A	IR, AND	TENSION	OF THE	ATMOSPH	ERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
91 83	91 85	94 90	90 90	93 90	93 89	96	94	94	94	91	86	87
_	—					76	83	86	87	82	$\begin{bmatrix} -83 \end{bmatrix}$	81
52	61	72	75	73	79	83	80	83	83	84	87	70
81	80 62	86 60	90	89	88	91	83	85 69	$\frac{85}{68}$	$\frac{84}{73}$	85 66	80 61
52 80	82	85	59 87	70 86	68 84	68 83	70 83	89	91	93	91	$\frac{31}{73}$
79	82	84	83	88	90	91	90	$\frac{63}{92}$	93	94	96	82
94	96	94	94	96	96						— 7	87
_		_				54	58	58	65	65	63 }	
45	54	60	67	68	61	63	67	67	64	$\frac{62}{88}$	70 87	58 70
71 57	68 65	$\begin{array}{c c}82\\73\end{array}$	87 75	80 68	81 77	82 85	86 89	88 94	90 97	95	96	70 77
71	69	77	77	72	76	78	83	87	95	96	96	79
66	73	76	79	82	84	89	88	86	88	89	84	85
77	78	85	85	90	91						- }	82
-	40	-				78 50	79	91	$\frac{92}{74}$	89 76	86 } 78	58
39 69	42 49	50 62	55 83	57 87	59 88	59 81	72 77	72 70	74 71	$\frac{76}{72}$	70	$\frac{66}{67}$
37	45	54	62	56	68	60	61	73	70	84	80	53
63	69	74	82	83	86	86	87	87	85	85	83	72
66	69	58	57	59	56	77	78	90	88	94	95	67
74	74	82	85	85	85		0.5	96	97	99	$\frac{-}{92}$ }	84
88	90	$\frac{}{92}$	97	98	98	92 98	95 95	96 95	97 95	95	95	92
80	87	96	90	93	94	95	95	94	95	95	96	88
66	58	71	84	84	91	95	91	92	91	90	91	74
75	65	65	78	90	83	81	88	93	91	88	91	82
76	79	81	77	77	76	77	86	88	91	94	94	78
76	78	80	89	86 —	89 —	92	92	93	91	92	92	87
70	71	76	80	81	82	81	83	85	86	87	86	76
In. 367	In.	In. 366	In. •367	In. •391	In. •362	In. •361	In. •354	In. •354	In. 355	In. :350	In. •332	In. 353
401		326	302	•291	304	301	004		-	_	- )	ŀ
_						•222	•228	•223	•220	209	208	*320
302		*296	274	257	•252	255	.229	225	217	216	217	289
397		359	338	336	337	349	308	311	'311	·303 ·190	*344 *167	:340 :219
·214 ·349		199 334	194 312	$^{\circ}_{294}$	$^{\circ}195$	$^{\circ}_{283}^{195}$	$^{\circ}207 \\ ^{\circ}288$	$^{\circ}_{298}$	:181 :313	*306	318	$\frac{213}{286}$
377		365	363	•390	393	397	394	•392	394	.383	397	·372
437		454	457	'462	•464			<u> </u>	l —		— 1	•342
	.					149	146	134	139	133	.131 }	152
146		153	175	$^{\circ}_{225}$	156 210	$^{\circ}_{209}$	172 195	·172 ·199	·169 ·209	163 226	191 233	241
396		257 355	·251 ·340	374	428	427	·460	450	·439	403	.396	378
386	379	404	·404	.380	*384	.467	•477	·491	•433	*432	*364	•428
303	304	297	$\cdot 283$	286	.287	.276	267	263	•262	•260	250	.333
*384	363	.339	.309	.308	'312	.345	1945	.200	.395	.375	$\left  \frac{-}{359} \right\}$	*364
141	132	144	150	146	148	*345 *147	345 161	·389 ·152	158	155	160	189
264	179	203	204	204	205	197	195	184	186	.191	180	•207
206	211	•222	217	206	218	187	187	197	183	179	181	205
220	200	195	194	194	193	.188	187	180	169	168	167	198
264		224	216	217	216	•272	256	287	285	.302	.309	250
426	401	408	403	.400	·400 —	•334	•336	$\cdot {327}$	.367	•422	$-\frac{1}{424}$	*420
651	•636	•583	.562	•550	•532	.211	•488	489	•506	.468	•506	•575
557	.559	•540	'495	·490	.493	.478	•491	'484	.200	'491	:502	566
549	490	465	459	'460	420	426	'400	389	394	384	398	.485
555		'418	'414 '409	437	405	391	390	369	*331 *450	*341 *470	347 474	·469 ·457
3446 586		·429 ·480	·402 ·513	.403 .508	·403 ·508	418	*455	443	·459			1
	- 312		_		<del></del>	•423	·408	•402	415	•409	$\left\{ -\frac{1}{437} \right\}$	*521
371	351	.339	.331	.330	*327	.310	.309	.308	*307	*305	307	*345

An 4	Marris II		помі	DITT OF	IRE AIR,	AND TE	WEION OF	THE AT	MOSPHER	IC VAPO	UR.		
Götting Time	e. ]	0	1	2	3	4	5	6	7	8	9	10	11
Toror Time		18	19	20	21	22	23	0 .	1	2	3	4	5
	1 2 3 4 5 6 7	94 93 94 96 81 82	87 92 86 92 81 77	83 93 78 93 90 78	86 89 76 93 92 66	97 92 90 88 91 67	92 92 82 91 90 62	85 87 73 83 88 58	85 87 74 80 82 60	87 84 62 84 81 60	84 82 71 86 86 69	78 75 74 82 87 59	80 77 71 91 87 41
ile Alli.	8 9 10 11 12 13	87 70 81 76 61 79	61 69 75 74 57 74	70 63 70 73 53 75	64 74 56 71 53 70	60 62 66 70 62 73	61 54 73 76 64 75	62 58 73 80 64 70	64 61 72 82 63 66	61 59 64 81 62 71	60 62 67 75 59 73	61 63 65 80 59 88	64 54 69 87 56 65
JUNE.	14 15 16 17 18 19 20	90 77 83 91 94 78	83 73 77 94 93 79	71 67 71 88 91 77	68 64 72 85 94 78	74 65 69 84 88 79	73 65 66 79 87 77	77 72 70 81 78 75	73 71 71 80 64 68	72 70 70 93 59 68	63 69 68 87 48 71	70 75 73 90 43 67	50 72 73 84 49 68
	21 22 23 24 25 26 27	75 62 61 49 66 86	71 60 69 45 66 84	71 58 55 49 67 81	63 52 49 46 65 76	56 48 44 36 58 71	44 43 38 37 57 70	50 34 31 35 57 66	40 42 34 36 56 71	35 42 30 53 54 67	40 40 46 54 49 69	45 40 26 54 67 72	47 35 35 57 60 71
	28 29 30	94 84	94 77	$\phantom{00000000000000000000000000000000000$	$\phantom{00000000000000000000000000000000000$	$\frac{-}{82}$	78 67	77 65	70 64	74 67	76 59	69 59	69 58
ourly	Means	80	77	74	72	71	69	67	66	66	66	66	64
	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \end{pmatrix}$	In. '474 '538 '415 '492 '355 '240 '285	In. '514 '523 '438 '539 '348 '266 '264	In. '518 '553 '436 '532 '371 '287 '350	In. '509 '592 '474 '535 '381 '277 '349	In. '523 '574 '505 '535 '377 '287	In.	In. • 590 • 484 • 430 • 546 • 375 • 272 —	In. '597 '529 '430 '562 '377 '265	In. '602 '521 '415 '522 '381 '283	In. '579 '509 '485 '450 '452 '279	In. '600 '469 '494 '442 '413 '277	In. :620:480:522:490:413:-203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:203:
v apour.	9 10 11 12 13 14	· 257 · 323 · 359 · 238 · 380	*301 *354 *414 *236 *404	344 ·416 ·436 ·238 ·409	349 '466 '353 '481 '264 '427	*346 *418 *418 *497 *331 *442	378 369 512 496 319 442	381 378 548 480 315 418	*393 *395 *547 *451 *315 *393	*376 *408 *520 *463 *318 *433	*375 *433 *562 *475 *310 *424	. 403 . 438 . 543 . 496 . 321 . 379	37 52 54 31 35
JUNE.	15 16 17 18 19 20 21	·464 ·393 ·367 ·494 ·617 ·389	·473 ·409 ·419 ·525 ·636 ·392	*455 *408 *454 *520 *618 *388	515 426 512 603 645 397	·608 ·449 ·513 ·677 ·657 ·408	590 427 511 650 730 388	·614 ·484 ·570 ·693 ·709 ·377	.606 .485 .590 .737 .617 .360	*600 *482 *590 *716 *571 *359	*520 *481 *606 *625 *475 *353	*585 *516 *621 *785 *425 *335	·45 ·51 ·58 ·73 ·48 ·33
	22 23 24 25 26 27	*310 *293 *316 *305 *387 *485	306 326 409 307 393	335 333 343 372 435	· 324 · 336 · 337 · 396 · 446 · 504	328 354 342 347 477 489		302 ·279 ·293 ·366 ·482 ·521	·270 ·341 ·320 ·405 ·476 ·524	· 235 · 354 · 287 · 551 · 504 · 466	·266 ·332 ·415 ·534 ·486 ·469	288 336 254 529 575 507	· 29 · 28 · 33 · 53 · 53 · 49
	28 29 30	·570 ·575	.563 .589	 •582 •599	 *585 *615	.631 .645	·623 ·614	·624 ·602	609 595	-626 629	 •649 •557	-623 565	·61 ·57
lovely.	Means	397	•419	•433	•452	•468	•469	•467	469	•470	•465	·470	•46

		н	MIDITY	OF THE A	IR, AND	TENSION	OF THE	ATMOSPH	ERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
85 78 70 91 88 47	89 82 76 92 88 57	91 62 81 96 79 77	87 73 87 96 86 80	90 84 94 99 75 86	93 88 93 97 74 89	91 91 93 94 71	92 91 93 84 72	92 94 93 87 80	95 91 94 85 82	91 93 94 82 83	94 92 96 79 82	89 86 83 89 83
72 64 69 73 61 67	77 75 72 77 69 73	85 71 76 88 69 75	84 83 85 89 73 83	80 84 80 88 71 86	77 78 82 89 74 81	84 73 82 84 60 72 	84 76 83 91 53 67 	72 82 83 82 57 68 —	75 81 88 82 62 79 —	87 79 82 81 64 82 —	90 } 79 90 79 66 85	72 71 75 75 66
49 79 78 85 58 71	52 77 80 90 75 72	55 82 78 89 78 69	63 86 88 89 87 77	64 86 91 90 83 79	67 83 91 96 81 81	68 83 91 97 85 — 84	76 81 89 97 87 —	74 88 91 96 89 — 84	77 88 90 95 86 <del></del>	84 88 89 97 79 —	84 88 94 96 81 	70 77 80 90 77 76
64 40 40 71 66 68	67 45 55 50 67 74	74 41 53 53 71 77	71 43 48 56 74 84	79 44 54 55 78 86	84 40 63 54 76 89	85 54 48 54 83 — 91	78 57 49 55 77 —	69 58 48 56 75 —	64 66 47 55 81 —	63 66 47 55 85 —	60 61 47 74 89 — 95	62 49 47 52 69 80
68 64	78 63	83 78	85 73	87 73	86 75	85 82	79 85	85 86	88 87	92 90	90 87	82 73
68	72	74	78	79	80	80	79	80	81	81	82	74
In. '570 '437 '490 '490 '419 '224	In.  *546 *398 *451 *501 *395 *242 *389 *409 *465 *433 *324 *376 *405 *447 *543 *751 *521 *330	In. '534 '349 '441 '465 '326 '254 '339 '420 '410 '291 '372 '392 '435 '499 '609 '532 '319	In. '499 '368 '473 '465 '289 '240 '300 '423 '381 '279 '367 '417 '430 '476 '600 '537 '325	In. '515 '368 '483 '485 '268 '235	In. '516 '353 '473 '476 '257 '230 -258 '281 '387 '372 '280 '328 -398 '387 '453 '591 '489 '320	In.  ·498 ·349 ·464 ·460 ·241 —  ·316 ·242 ·282 ·381 ·258 ·278 — ·409 ·395 ·387 ·468 ·575 ·467 — -294	In. ·483 ·338 ·464 ·415 ·238 — ·310 ·237 ·268 ·380 ·216 ·312 — ·429 ·360 ·456 ·553 ·447 — ·304	In. '477 '356 '464 '400 '239 '248 '240 '268 '354 '224 '324 '420 '419 '361 '438 '529 '443 '294	In. ·491 ·328 ·450 ·385 ·235 ·251 ·229 ·270 ·360 ·228 ·346 ·424 ·429 ·323 ·452 ·535 ·425 ·273	In. '463 '320 '450 '368 '230 '253 '224 '255 '337 '231 '343 '422 '433 '317 '456 '549 '399 '273	In.  '490 '324 '470 '353 '223  -245 } '245  '340 '229 '350  -41 } '390 '321 '475 '545 '394 -280 }	321 344 431 391 302 400 476 424 505 623 536
357 330 353 592 511 473  585 619	*361 *330 *440 *410 *506 *470 	· 362 • 267 • 353 • 393 • 508 • 473 — • 574 • 600	*351 *261 *308 *393 *515 *498 — *547 *549	*366 *254 *320 *355 *512 *495  *529 *524	*360 *217 *343 *344 *503 *506 — *530 *525	· 330 · 287 · 288 · 334 · 512 — · 540 · 532 · 524	· 320 · 292 · 292 · 332 · 480 — · 541 · 526 · 509	· 290 · 293 · 277 · 330 · 453 · — · 539 · 533 · 503	*269 *307 *272 *330 *468 — *528 *512 *489	*266 *304 *264 *330 *461 — *546 *518 *512	$egin{array}{c} \cdot 256 \\ \cdot 293 \\ \cdot 272 \\ \cdot 414 \\ \cdot 440 \\ \hline - \\ \cdot 565 \\ \cdot 523 \\ \cdot 542 \\ \end{array}$	*309 *306 *323 *399 *481 *510 *575 *567
*465	•446	*416	•408	*398	*391	*389	*382	*374	·37 <b>0</b>	*366	373	*426

			HUMI	DITY OF	THE AIR,	AND TE	NSION OF	THE AT	MOSPHER	IC VAPOU	JR.	-	
lours of l Götting Time	gen }	0	1	2	3	4	5	6	7	8	9	10	11
ours of Toron	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\left( egin{array}{c c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{array} \right)$	81 82 93 82	74 76 83 80	75 71 74 80	68 72 67 76	71 70 65 75	66 59 54 71	72 69 57 72	74 64 54 73	71 69 62 66	71 73 54 71	74 65 54 65	85 67 58 67
	6 7 8 9 10	85 84 67 87 81 88	83 75 76 75 74 87	67 63 92 64 73 87	74 62 90 68 71 81	88 47 88 68 57 66	58 42 78 83 51 68	57 38 74 80 56 57	39 56 70 90 78 57	38 61 64 80 67 72	39 30 63 80 63 81	39 33 63 69 57 81	40 29 67 66 50 75
Humidity of the Air. JULY.	112 13 14 15 16 17 18	91 87 89 86 87 89	94 94 76 87 73 80	81 92 73 82 66 76	76 64 69 90 59 72	63 67 63 61 58 69	56 61 62 63 60 67	54 56 60 57 55 63	74 59 63 51 57 57	59 61 75 46 50 58	61 65 69 50 52 55	71 55 79 46 50 55	61 58 64 47 57 56
Humi	19 20 21 22 23 24 25	80 91 91 91 93 78	81 85 89 84 90 73	81 80 89 71 94 69	77 66 81 59 94 58	70 67 82 61 92 53	68 63 78 69 91 49	64 61 70 65 95 45	60 61 65 64 91 48	65 60 67 52 87 59	61 63 68 54 79 60	60 61 70 49 88 58	62 64 73 50 84 61
	26 27 28 29 30 31	89 82 95 94 83	83 83 87 92 79	77 77 77 81 87 77	73 70 80 85 70	70 67 76 79 60	68 65 77 76 57	55 68 72 81 56	51 69 71 82 48	48 70 77 63 48	49 67 71 59 46	49 54 68 64 47	46 72 65 62 56
lourly	Means	86	82	78	73	69	65	63	64	63	61	60	61
	$\left( egin{array}{c c} 1 \\ 2 \\ 3 \\ 4 \end{array} \right)$	In. *559 *495 *501 *390	In. '582 '491 '518 '511	In. '636 '476 '524 '589	In. '595 '486 '510 '585	I n. '630 '503 '500 '626	In. '604 '464 '427 '639	In. '673 '591 '472 '668	In639 -567 -442 -631	In. '639 '582 '510 '625	In. '603 '601 '446 '603	In. '620 '561 '427 '610	In. •639 •564 •472 •580
	5 6 7 8 9 10 11	·488 ·433 ·367 ·486 ·726 ·621	544 ·433 ·431 ·528 ·748 ·751	·470 ·388 ·503 ·567 ·849 ·775	.592 .402 .536 .652 .848 .781	*543 *430 *580 *625 *775 *773	*528 *327 *545 *665 *738 *776	· 535 · 306 · 574 · 562 · 880 · 695	*386 *450 *590 *583 *708 *697	·395 ·485 ·589 ·626 ·833 ·730	-390 ·269 ·607 ·653 ·872 ·693	·389 ·294 ·629 ·654 ·809 ·716	•403 •256 •603 •655 •583 •753
Tension of the Vapour.	18	·422 ·332 ·317 ·352 ·305 ·391	·472 ·410 ·315 ·438 ·355 ·456	·457 ·442 ·321 ·438 ·410 ·485	*504 *333 *332 *517 *385 *496	·446 ·364 ·295 ·369 ·411 ·495	·423 ·341 ·310 ·360 ·438 ·510	*442 *336 *323 *350 *405 *487		·495 ·366 ·416 ·319 ·395 ·477	*551 *378 *365 *334 *369 *453	·642 ·312 ·470 ·319 ·351 ·465	*508 *307 *380 *333 *382 *467
Tens	19 20 21 22 23 24 25	.504 .553 .539 .473 .598 .459	567 587 552 529 576 486	.560 .608 .564 .489 .564 .513	.599 .559 .580 .482 .578 .490	.600 .580 .572 .570 .570 .470	*558 *558 *567 *600 *573 *458	556 569 585 611 585 430	545 544 564 610 555 464	· 597 · 527 · 544 · 524 · 574 · 596	579 537 583 512 588 576	568 504 559 521 606 562	•556 •498 •567 •492 •590 •577
	26 27 28 29 30 31	·508 ·458 ·662 ·730 ·501	.558 .513 .712 .781 .490	·571 ·544 ·673 ·809 ·497	*561 *553 *727 *818 *490	· 557 · 577 · 729 · 792 · 469	.523 .559 .758 .756 .446	·441 ·557 ·783 ·787 ·476	·409 ·569 ·734 ·674 ·418	· 399 · 595 · 719 · 722 · 429	*415 *585 *740 *68 <b>5</b> *417	.416 .559 .736 .667 .436	*382 *618 *684 *658 *509
Hourly	Means	*488	•531	*545	.555	•550	•536	•544	•530	· <b>5</b> .45	•533	•533	•519

		н	MIDITY	OF THE A	IR, AND	TENSION	OF THE	ATMOSPH	ERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
84 71	86 76	92 84	93 91	94 89	85 93	95 93	90 93	88 92	87 92	88 96	86 95	81 79
87	75 85	83 82	87 82	86 82	84 76	86	85	81	79	79	81	74
$\frac{1}{36}$	43	50	<del>-</del> 59	$\frac{62}{64}$	$\frac{70}{70}$	96 76	92 79	91 81	90 84	88 87	86 } 97	79 64
29 73	35 74	52 69	55 80	55 71	60 73	$\begin{array}{c} 72 \\ 79 \end{array}$	58 85	61 80	61 91	72 93	79 92	55 77
69 63	78 64	79 80	90 85	90 91	89 89	90 94	89 93	94 84	89 87	92 89	76 90	81 74
83	87	87	85	85 —	87	90	88	$\frac{-}{93}$	98	$\frac{3}{87}$	$\frac{1}{96}$ }	82
74 60	82 65	88 69	89 76	88 73	92 75	92 78	75 85	85 87	88 87	87 89	90 85	78 73
66 56	65 59	81 70	87 82	83 79	82 79	82 86	78 84	83 85	85 85	86 84	88 90	75 71
59 65	66	71 87	75 87	73 89	76 88	75 —	77	78	84	86	89	68
$\frac{3}{72}$	$\frac{1}{81}$	83	<del></del>	$\frac{-}{91}$	$\frac{-}{92}$	69 92	74 94	76 91	79 91	87 93	82 } 96	73 79
65 73	80 78	75 87	81 90	84 92	86 86	89 88	89 91	92 92	95 92	94 96	94 94	77 83
57 80	71 87	79 84	81 86	86 80	86 84	84 88	84 89	87 88	82 90	87 91	87 85	73 88
61	63	63	59	60	60	87	92	92	93	91	$-\frac{1}{92}$ }	68
54 74	59 84	75 92	79 94	77 94	76 94	79 95	79 95	85 96	82 93	82 98	$\begin{array}{c} 78 \\ 94 \end{array}$	$\begin{array}{c} 69 \\ 81 \end{array}$
79 65	86 67	86 70	93 71	91 72	98 69	96 81	96 83	97 82	96 79	97 82	97 83	85 76
63	65	69	75	68	67	65	67	77	79	82	84	66
66	72	77	81	81	81	85	85	86	87	88	88	75 In.
In. :598 :590	In. :597 :557	In. :588 :510	In. • 573 • 474	In. •552 •445	In. •522 •430	In. *535 *444	In. 570 464	In. •550 •463	In. • 529 • 446	In. •517 •449	In. •498 •446	. 585 . 504
516 603	·516 ·597	'435 '566	'413 '518	386	*368 *485	364	359	*357	*346	*346	351	•438
333	338	.362	386	382	*393	.568 .395	.545 .397	·542 ·399	·524 ·372	·504 ·394	·475 }	$^{\circ}563$ $^{\circ}426$
245 626	·270 ·653	302 317 545	*323 *492	315 460	·290 ·459	*315 *473	·298 ·492	·305 ·478	$\frac{308}{455}$	*332 *449	·373 ·439	:340 :524
678	·692 ·567	·641 ·623	.636 .600	647 646	·674 ·618	·683 ·649	.649 .595	·670 ·562	·618 ·572	·639 ·573	633	630 689
697	663	.709	.677	· <b>6</b> 97	·687	·489	.466	•443	•426	372	$-\frac{1}{422}$	·646
538 302	·524 ·303	·478 ·291	·468 ·295	·465 ·265	·462 ·279	*423 *283	·287 ·287	·293 ·289	$^{\circ 275}_{\circ 270}$	$^{\circ}_{267}$ $^{\circ}_{275}$	·279 ·273	*448 *320
384 363	*355 *325	*384 *313	·395 ·312	350 287	·340 ·276	:340 :285	$^{\circ}_{280}^{\circ}$	$^{\circ}331$ $^{\circ}275$	·318 ·270	·304 ·267	:307 :265	$^{:}347 \\ ^{:}332$
376 475	·389 ·499	357 457	321 422	·325 ·416	·329 ·395	323	313	309	*314	·312	•327	•359
585	•583	541	  484	·468	 -470	·426 ·470	·429 ·493	·420 ·475	·433 ·452	·482 ·430	$\left. \begin{array}{c} -1 \\ -452 \\ -462 \end{array} \right\}$	*456 *530
·490 ·555	•530 •532	516 482	521 479	517 458	*512 *422	*540 *425	501 432	*483 *409	·492 ·395	·497 ·423	.489 .433	.530 .509
523	·562 ·592	548 572	*539 *559	*543 *496	*534 *480	'510 '486	529 491	*548 *486	*518 *493	•550 •496	.552 .465	.536 .548
584	•559	483	*424 —	.393	394	·499	513	•495	•464	- - 459	$\frac{1}{456}$	•492
·427 ·615	·386 ·620	·393 ·607	·377 ·564	*354 *535	·346 ·506	363 547	.373 .549	·397 ·582	·390 ·577	·410 ·593	·418 ·586	`432 `565
701 618	·727 ·607	723 560	.746 .538	·743 ·505	.737 .469	·724 ·537	712 539	·697 ·518	·685 ·487	·686 ·497	·662 ·501	.717 .636
521	478	·437	*424	365	*357	.339	371	.390	392	*408	'415	*436
•523	•519	·498	'480	*464	•453	·461	<b>.</b> 454	<b>.</b> 451	*438	•442	•443	`501

Vol. III.

			HUMI	DITY OF	THE AIR,	AND TE	NSION OF	THE AT	MOSPHER	IU VAPOI	. N.	<u> </u>	
ours of M Göttinge Time.	en }	0	1	2	3	4	5	6	7	8	9	10	11
ours of M Toronte Time.	Mean )	18	19	20	21	22	23	0	1	2	3	4	5
	(1	79	67	55	49	49	56	58	61	56	55	53	52
	$\begin{vmatrix} 2 \\ 3 \end{vmatrix}$	89	87	81	$\frac{-}{75}$	$\frac{-}{71}$	70	67	68	59	52	46	51 63
	4	74	71	75 76	$\frac{66}{78}$	$\begin{array}{c} 72 \\ 71 \end{array}$	62 69	60 68	61 64	60 63	60	61 60	60
	$\begin{vmatrix} 5 \\ 6 \end{vmatrix}$	91 84	$\begin{array}{c} 79 \\ 73 \end{array}$	64	59	67	63	61	58	60	56	60	53
	7	74	71	70	70	83	64	61	60	64 76	59 74	57 80	$\begin{array}{c} 62 \\ 84 \end{array}$
	8 9	82	78 —	71	87	87	88	83	78	-	_		
	10	87	86	82	75	67	69	64 66	59 63	$\begin{array}{c} 58 \\ 64 \end{array}$	56 61	56 61	53 61
	11 12	70 96	60 90	56 83	62 76	60 77	$\begin{array}{c} 62 \\ 72 \end{array}$	64	61	59	58	59	54
	13	89	90	85	80	76	75	63	62	89	78	75 61	75 65
T.	14 15	75 88	$\begin{array}{c c} 74 \\ 82 \end{array}$	63 80	53 77	$\begin{array}{c c} 67 \\ 72 \end{array}$	67 71	68 64	67 60	60 65	64 57	57	62
AUGUST	16						_	_	-		51	50	50
AUGUST.	$\begin{vmatrix} 17 \\ 18 \end{vmatrix}$	88 80	85 73	77 66	75 67	67 70	83 71	60 69	60 68	58 69	70	68	65
<b>A</b>	19	91	$\frac{76}{72}$	69	59	59	57	60	61	60	66	71	75 91
<b>i</b>	20	92	94	95	95	96 82	94 80	93 83	82 82	88 83	82 77	92 71	71
	$\begin{vmatrix} 21 \\ 22 \end{vmatrix}$	$\begin{array}{c} 93 \\ 87 \end{array}$	95 86	89 85	87 82	89	78	81	85	79	80	83	81
	$\begin{vmatrix} 23 \\ 24 \end{vmatrix}$	$\frac{-}{60}$	<del></del> 56	<del></del> 58	60	60	66	69	${71}$	63	64	60	64
	25	83	80	78	74	72	72	75	72	66	67	68	69
	26	92	97	84	77	73 79	73 80	71 76	65 77	$\begin{array}{c} 62 \\ 75 \end{array}$	59 71	53 70	59 70
	$\begin{vmatrix} 27 \\ 28 \end{vmatrix}$	91 90	88 89	$\frac{82}{79}$	81 79	82	81	81	81	74	79	80	89
	29 30	96	92	88	85	79	78	80	89	88	89	86	87
	31	90	88	87	85	78	79	74	71	65	65	67	93
ourly N	Ieans	85	81	76	74	73	72	70	69	68	66	66	68
	$\begin{pmatrix} 1 \end{pmatrix}$	In. •441	In. •433	. In. · 396	In. 387	In. •407	In. •470	In. •507	In. 531	In. •495	In. •496	In. •468	In. •45
	$\begin{vmatrix} 2 \\ 3 \end{vmatrix}$	•449	•537	.588	.601	.603	.625	628	688	.613	•534	485	•49
	4	•455	· <b>5</b> 08	.608	•599	.675	.656	678	697	693	699	.713 .709	·73 ·70
	$\begin{vmatrix} 5 \\ 6 \end{vmatrix}$	·638 ·478	$^{\circ}631 \\ ^{\circ}482$	$^{\circ}_{495}$	$\begin{array}{c} .773 \\ .552 \end{array}$	.756 .701	.769 .676	$\begin{array}{c} .764 \\ .559 \end{array}$	·774 ·637	$^{\circ}768 \\ ^{\circ}624$	.738 .598	597	• 56
	7	$\cdot 457$	·489	$^{\circ}528$	.595	.748	.636	·632	·642	·676	613	·569 ·641	·60 ·62
	8 9	.518	•512 —	•502	555	• 5 <b>5</b> 0	•593	·654	·627	·618	·603		
	10	:556	•554	•557	•542	•539	•579	:530	512	524	. 531	513 474	· 45 · 47
.   	11 12	·306 ·416	·311 ·494	·339 ·560	.413 .600	.432 .683	·445 ·647	·507 ·600	·488 ·603	$^{:}495 \\ ^{:}594$	·490 ·605	584	•52
od l	13	<b>.</b> 613	·670	<b>.</b> 689	*688	743	747	·691	.711	.703	703	.717	·73 ·58
ST.	14 15	.442 .445	$\frac{.467}{.516}$	·479 ·569	.454 .634	.603 .660	:610 :665	$^{\circ}620$ $^{\circ}622$	·584 ·593	$\begin{array}{c} \cdot 546 \\ \cdot 662 \end{array}$	·589 ·616	.596 .616	.63
AUGUST	16										.390	381	•36
AUGUST.	17 18	$\frac{464}{288}$	$^{\cdot 484}_{\cdot 291}$	$^{:}488$ $^{:}286$	· 506 · 331	·495 ·386	·466 ·406	$^{•453}_{•393}$	.434 .395	$\overset{\boldsymbol{\cdot}}{}447\\ \overset{\boldsymbol{\cdot}}{}401$	390 427	410	•39
A	19	.380	.391	$^{:}387$	*346	*348	*367	376	*388	.412	416	•435	·44 ·61
	20	492	*510	$\cdot 521$	*530	`548	·557	·568 ·637	·537 ·621	·578 ·637	· 539 · 631	·614 ·564	• 55
	$\begin{vmatrix} 21 \\ 22 \end{vmatrix}$	$^{\cdot 426}_{\cdot 512}$	$\begin{array}{c} 526 \\ 517 \end{array}$	•590 •515	.637 .518	$^{\circ}_{562}^{612}$	:607 :538	624	.616	625	600	• 592	• 54:
-	$\begin{vmatrix} 23 \\ 24 \end{vmatrix}$	$\cdot \frac{-}{273}$	$\frac{-}{286}$	$\cdot _{323}^{-}$	· <del>3</del> 78	$-{398}$	434	$\frac{-}{449}$	•460	· <del>4</del> 26	•442	417	45
	25	<b>.</b> 364	•423	·486	.208	•511	• 526	*526	·520 ·543	`511 `514	$\begin{array}{c} \cdot 534 \\ \cdot 459 \end{array}$	$^{\circ}524 \\ ^{\circ}435$	·514
	$\begin{vmatrix} 26 \\ 27 \end{vmatrix}$	.409 .459	$\begin{array}{c} :562 \\ :537 \end{array}$	$\frac{.587}{.572}$	$^{:}576 \\ ^{:}634$	• 552 • 655	·552 ·668	· 590 · 644	626	.618	•579	562	• 543
	28	<b>.</b> 495	$\cdot 525$	• 520	• 539	646	·649	.690	705	670	.680	.649 .566	· 663
	29 30	·506	·570	652	·683	·665	698	·703	705	.551 	·566  ·663	.670	•69
	\31	548	*555 	675	695	·679	.715	.711	.708	656			.55
	Ieans	455	•492	$\cdot 523$	•549	*583	.589	•591	•590	•579	•567	. 558	000

		H	UMIDITY	OF THE	AIR, AND	TENSION	OF THE	ATMOSP	HERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
57	63	66	63	64	69	91	89	$\frac{-}{93}$	93	${91}$	$\left\{\begin{array}{c} -\\ 92 \end{array}\right\}$	68
48 71	63 74	61 83	68 81	75 85	78 90	77 89	64 88	80 87	80 90	82 93	81 93	70 75
55	54	59	65	62	64	75	75	64	73	79	80	6 <b>9</b>
57 67	41 70	60 75	70 80	74 83	78 72	76 80	68 78	66 79	69 80	77 83	73 78	65 72
90	88	93	93	93	92		_				- 1	85
49	52	<del></del>	57	60	$\frac{}{67}$	89 62	92 64	96 68	86 68	86 68	85 } 71	65
69	76	88	91	91	93	91	92	93	96	93	90	75
62 81	67 57	65 66	68 69	$\begin{array}{c c} 72 \\ 67 \end{array}$	74 67	80 71	74 75	80 70	84 67	86 70	90 69	$\begin{array}{c} 73 \\ 74 \end{array}$
64	74	80	85	84	83	84	87	87	87	87	86	74
72	77	77	76	86	86	95	96	88	89	88	$\left\{\begin{array}{c} -87 \end{array}\right\}$	77
51	64	67	72	73	76	76	86	84	81	80	81	$\frac{71}{20}$
71 79	81 83	91 84	85 89	87 89	90 89	90 89	90 89	89 70	88 94	89 91	86 90	78 77
91	93	95	97	96	97	96	96	96	94	95	96	93
83 85	86 88	91 91	90 90	90 <b>9</b> 2	94 93	92	95	95 —	95	89	89	87
69	81					74	83	82	76	66	60 }	82 74
75	85	91 87	88 90	88	88 91	88 88	89 97	81 94	$\begin{array}{c c} 81 \\ 92 \end{array}$	85 96	85 95	81
60 79	83 80	87 81	81 83	84 80	85 81	86 77	84 75	83 76	88 88	87 89	89 90	78 80
84	90	91	93	93	93	94	95	96	96	96	94	87
85	91	92	96	95	96	$\frac{-}{92}$	90	90	90	92	$\frac{-}{92}$ }	89
77	81	80	85	83	85	91	93	94	90	91	92	83
70	75	79	81	82	84	84	85	84	85	86	85	75
In. 467	In. •443	In. •407	In, 390	.In. :392	In. •404	ln.	In.	In.	In.	ſn.	In.	In.
436	•497	· <del>4</del> 70	· <del>47</del> 3	· <del>4</del> 18	•424	·444 ·407	·420 ·372	·422	·412 ·398	·420 ·395	·410 } ·400	·438 ·497
'741	.676	.703	·648	·648	·616	.602	·602	$\begin{array}{c} \cdot 405 \\ \cdot 570 \end{array}$	•560	•585	*568	.635
.648 .583	.616 .397	·629 ·462	$^{\circ}650$ $^{\circ}452$	$\begin{array}{c} 626 \\ 437 \end{array}$	'631 '443	.606 .440	·535 ·417	'472	·467 ·413	·464 ·449	.466 .496	647
.603	548	•530	.517	526	•462	.200	.504	$^{:}411$ $^{:}508$	.507	•508	·426 ·499	.512 .559
.616	•593	·614	·615	.619 —	.603	•555	.572	•558	$\cdot \frac{-}{522}$	•528	$\{-\frac{1}{524}\}$	.580
*392	•347	•326	345	.329	351	*313	.301	.301	•295	281	285	•428
.509 .551	·491 ·544	.473 .505	$^{\circ}457 \\ ^{\circ}508$	$\overset{\boldsymbol{\cdot}}{3}\overset{4}{12}$	.457 .514	.421 .541	·405 ·533	$391 \\ 535$	·399 ·562	$^{\circ}397 \\ ^{\circ}568$	·369 ·563	·433 ·556
`725	.200	.521	·531	•466	<b>.</b> 468	•476	<b>.</b> 460	431	•397	•397	*386	•590
575 644	570 636	$\begin{array}{c} \cdot 548 \\ \cdot 620 \end{array}$	.496 .603	.480 .644	·464 ·629	·455 —	·464	·450	·439 —	·442	*430	516
_						·494	'483	•474	475	.474	.446}	.577
·356 ·396	386 375	$\begin{array}{c} 365 \\ 384 \end{array}$	$365 \\ 344$	$^{\circ}_{348}$	·361 ·347	$\begin{array}{c} 358 \\ 340 \end{array}$	$\begin{array}{c} 328 \\ 343 \end{array}$	·310 ·331	$\frac{.304}{.319}$	$^{\circ}_{322}^{300}$	$^{298}_{322}$	·394 ·356
•464	*466	·467	•489	481	•493	·489	·492	•497	•501	<b>.</b> 490	·483	·438
.603 .589	*565 *577	.547 .574	$\overset{\boldsymbol{\cdot}}{5}\overset{45}{63}$	$^{:}523$ $^{:}578$	·524 ·560	*515 *556	$\begin{array}{c} •495 \\ •543 \end{array}$	$\begin{array}{c} 484 \\ 528 \end{array}$	$\begin{array}{c} \cdot 454 \\ \cdot 528 \end{array}$	`449 `512	$\begin{array}{c} \cdot 442 \\ \cdot 525 \end{array}$	· 532 · 570
547	530	528	•519	509	.201			!			,	502
•443	-411			$\frac{-}{362}$	•360	$^{:}405$ $^{:}353$	$\frac{398}{340}$	·388 ·316	·364 ·316	$\begin{array}{c} :314 \\ :322 \end{array}$	·280 }	378
·516 ·427	530	.516	•504	•503	•499	·486 ·443	<b>.</b> 493	472	•453	•446	421	.491
550	.473 .495	·468 ·486	.432 .458	$\begin{array}{c} \cdot 438 \\ \cdot 446 \end{array}$	·441 ·445	·449	$\overset{\boldsymbol{\cdot}}{} \overset{\boldsymbol{4}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} \overset{\boldsymbol{1}}{}} \overset{\boldsymbol{1}}{} $	·408 ·431	$\begin{array}{c} 425 \\ 474 \end{array}$	$\begin{array}{c} \cdot 412 \\ \cdot 472 \end{array}$	·420 ·479	·476 ·530
.620 .593	:609 :557	·595 ·547	.568 .540	<b>•5</b> 53	· 557 · 540	535	519	.506	•490	.488	471	581
641	624	-595	 -596	·519 ·575	·532	· 547 · 525	·491 ·527	·479 ·527	·479 ·495	·495 ·544	$\left.\begin{array}{c} - \\ -543 \\ -545 \end{array}\right\}$	· 574 · 612
*548	.518	.211	·499		*486	471	457	•446	*440	•441	*436	.515
1 010	010	911	100	130	400	111	101	170	440	411	190	919

			HUMI	DITY OF	THE AIR,	AND TE	NSION OF	THE AT	MOSPHER	IC VAPO	UR.		
ours of l Götting Time	Mean }	0	1	2	3	4	5	6	7	8	9	10	11
ours of Toron Time		18	19	20	21	22	23	0	1	2	3	4	5
	$ \begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{pmatrix} $	93 94 95 94 98	92 93 94 93 95	82 92 87 86 94	79 86 92 88 89	78 81 89 89 84	57 79 88 89 88	52 81 89 87 88	58 74 94 87 84	62 74 97 81 85	60 75 97 83 88	62 76 94 84 86	73 81 97 85 89
Alfr.	6 7 8 9 10 11 12	96 84 59 59 90	97 81 56 62 90 93	92 78 59 65 81 87	85 73 58 52 80 81	85 71 60 51 80	83 70 58 47 80 77	82 68 50 44 78 86	75 70 55 47 75 84	72 79 51 53 72 86	71 62 49 54 77 78	72 57 47 56 83 78	72 59 50 60 83 81
SEPTEMBER.	13 14 15 16 17 18 19	97 72 85 88 86 91	97 65 81 83 84 88	93 59 69 83 83 88	87 57 63 84 76 76	80 52 66 81 68 77	76 43 65 75 69 76	78 47 65 80 71 73	77 39 62 79 71 67	78 35 62 77 73 71	82 35 63 86 75 72	88 38 65 88 73 69	85 42 66 91 79 71
-	20 21 22 23 24 25 26	63 88 92 93 91 91	78 89 95 92 90 89	78 80 94 87 89 85	76 79 84 94 95 86	67 81 82 95 94 83	63 79 78 95 94 79	62 75 79 94 94 71	62 76 73 94 92 73	58 73 73 90 94 75	59 72 73 85 95 77	55 73 75 85 93 69	54 76 80 85 93 77
	27 28 29 30	89 87 88	88 82 86	86 83 79	79 81 76	$\frac{-72}{78}$	$\begin{array}{c} - \\ 82 \\ 74 \\ 72 \end{array}$	$\begin{array}{c} - \\ 75 \\ 66 \\ 72 \end{array}$	74 71 75	75 67 75	71 68 76	71 78 79	72 85 82
Hourly 1	Means	87	86	82	79	77	74	73	73	73	72	73	76
ur.	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\$	In.  -558 -575 -656 -606 -700587 -435 -225 -317 -538	In626 -647 -685 -647 -729684 -449 -233 -334 -582	In624 -698 -669 -657 -772766 -463 -260 -351 -568	In. '715 '735 '680 '681 '801 '799 '467 '270 '299 '615 '768	In. '749 '752 '706 '703 '809 '835 '485 '293 '302 '626 '773	In.	In. • 588 • 815 • 717 • 762 • 768 — • 889 • 485 • 261 • 275 • 648 • 718	In. '643 '781 '724 '763 '765 '820 '488 '306 '295 '687	In. '668 '763 '728 '760 '760 '790 '548 '297 '339 '691	In. '639 '747 '746 '755 '788 '768 '421 '292 '353 '672 '590	In. '645 '743 '713 '749 '772 '752 '386 '285 '372 '677	In. :665 :741 :730 :745 :744 - :737 :378 :300 :397 :700 :633
Tension of the Vapour. SEPTEMBER.	19	·636 ·598 ·307 ·253 ·361 ·392 ·292	713 	·763 -727 ·263 ·327 ·380 ·403 ·431	708 733 256 353 395 425 440	7754 ·252 ·380 ·416 ·423 ·518	786 ·217 ·390 ·414 ·444 ·543	781 ·251 ·389 ·456 ·447 ·559	799 216 377 445 451 512	·827 ·209 ·382 ·421 ·467 ·541	*801 *214 *372 *434 *476 *530	·787 ·237 ·374 ·420 ·478 ·522	· 808 · 251 · 380 · 415 · 488 · 514
-	20 21 22 23 24 25 26 27	·234 ·215 ·278 ·464 ·320 ·254	· 296 · 250 · 381 · 522 · 325 · 276	· 293 · 307 · 475 · 512 · 326 · 294	· 297 · 369 · 492 · 546 · 345 · 339	·277 ·391 ·518 ·555 ·375 ·358	· 277 · 410 · 543 · 560 · 395 · 352	· 289 · 412 · 583 · 575 · 401 · 349	· 304 · 422 · 562 · 565 · 403 · 373	·294 ·424 ·572 ·476 ·420 ·375	· 299 · 422 · 567 · 457 · 427 · 388	286 :434 :561 :461 :398 :369	· 267 · 432 · 553 · 447 · 367 · 380
	28 29 30	·210 ·387 ·410	·231 ·395 ·435	·253 ·419 ·424	261 451 462	·268 ·465 ·445	·345 ·467 ·484	·325 ·434 ·497	·323 ·458 ·506	:350 :437 :489	`351 `424 `494	·346 ·449 ·483	·336 ·475 ·455
Jourly	Means	416	453	478	•500	.516	•523	•526	•520	•524	.516	•512	•513

		HU	MIDITY (	OF THE A	IR, AND	TENSION	OF THE	ATMOSPE	IERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
80 85 97 89 82	83 81 97 91 79	81 93 95 92 86	85 92 96 92 93	89 85 92 93	81 85 95 95 94	89 89 96 96	93 91 95 97	94 89 96 97 —	91 90 97 96 —	92 91 96 96 97	93 92 93 97 — 96 }	79 85 94 91
78 60 48 61 85 86	83 70 51 71 89 91	69 72 54 78 91 90	89 70 60 — 93 88 —	85 56 59 89 94 94 —	82 55 69 92 94 95 —	94 78 52 71 92 94 — 94 80	96 72 48 70 92 96 — 95 75	96 76 47 70 97 92 	55 78 54 67 91 97 	97 83 52 68 89 97 — 95 73	90 54 62 90 97 — 96 73	81 64 58 66 87 89
78 47 66 89 81 81	85 66 65 86 86 79	85 60 76 87 91 78	84 61 81 88 93 79	63 81 89 55 81	76 64 77 89 89 87	72 83 87 93 —	69 80 86 90 —	71 83 87 92 — 89	76 85 87 90 — 88	77 86 86 91 — 83	$   \begin{array}{c}     83 \\     87 \\     88 \\     89 \\     \hline         \\         \hline         \\         $	58 73 85 81 80
81 82 84 87 91 82	85 89 89 86 89	87 90 92 87 90 85	86 91 89 91 85 85	81 90 93 91 86 85	81 92 95 93 88 89	84 93 95 91 88	87 91 94 90 85 —	87 90 96 90 84 —	88 90 95 91 88 —	88 92 96 90 84 —	93 95 95 91 89 — 93	75 84 87 90 90
80 84 85	80 82 94	80 68 90	87 76 79	79 88 77	75 82 73	91 78 87 70	77 96 75	75 87 85	75 87 86	83 87 84	87 86 83	79 80 80
79	82	82	85	82	84	86	85	86	86	87	87	81
In688 -742 -730 -723 -668	In. :659 :721 :714 :708 :608	In. '660 '737 '660 '701 '604	Iu. '659 '718 '646 '701	In. '633 '668 '647 '695 '568	In. :648 :664 :657 :697 :570	In. •627 •674 •662 •712	In. •621 •672 •682 •726	In. '597 '649 '687 '726	In.	In.	In. 577 640 606 692	In. '635 '706 '688 '713
725 365 277 394 678 606	722 368 285 437 613	·617 ·374 ·304 ·451 ·633 ·538	·674 ·349 ·330 ·624 ·493		 ·597 ·247 ·372 ·453 ·592 ·522	·608 ·525 ·228 ·379 ·445 ·576	'601 '446 '212 '327 '457 '618	*591 *446 *203 *372 *489 *593	· 570 · 440 · 214 · 354 · 494 · 631	*593 *450 *207 *342 *506 *613	*582 }  *452  *212  *310  *422  *631	.667 .364 .322 .388 .627
755 252 384 409 456	·775 ·289 ·382 ·398 ·406 ·473		·717 ·257 ·407 ·407 ·397 ·437	 ·668 ·255 ·383 ·407 ·304 ·423		· 575 · 575 · 278 · 338 · 396 · 366	*576 *511 *262 *322 *395 *354	583 454 267 335 399 337 	*583 *344 *258 *341 *399 *304 —	.578 .343 .250 .342 .392 .301  .353	319 261 358 407 287 	*662 *255 *359 *406 *398 *459
347 '430 '536 '447 '345	318 378 378 558 430 333 366	·299 ·357 ·556 ·413 ·342 ·370	·292 ·331 ·540 ·406 ·322 ·336	·271 ·320 ·544 ·389 ·322 ·325	·261 ·308 ·515 ·378 ·333 ·296	*509 *262 *303 *527 *366 *322	*510 *253 *297 *540 *354 *315	.462 .245 .290 .534 .346 .313	*388 *240 *278 *491 *341 *288	· 242 · 276 · 479 · 328 · 268 —	·239 ·282 ·472 ·324 ·260	· 278 · 347 · 516 · 444 · 344 · 318
365 455 503	366  347 407 506	370 -335 -349 -495	329 371 470	308 367 429	-302 -398 -380	·264 ·307 ·407 ·345	*255 *308 *418 *349	·255 ·306 ·400 ·357	*229 *306 *404 *335	226 335 400 314	·218 } ·365 ·403 ·332	*313 *418 *433
.208	•492	•481	•472	`450	•445	•445	·438	.432	'418	'414	•406	°475

			нимп	OITY OF T	THE AIR,	AND TEN	SION OF	THE AT	MOSPHERI	C VAPOU	R.		
Gött	of Mean tingen ime.	О	1	2	3	4	5	6	7	8	9	10	11
Tor	of Mean ronto	18	19	20	21	22	<b>2</b> 3	0	1	2	3	4	5
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	77 89 88	77 90 86	76 91 81	74 89 78	72 86 77	71 83 80	72 79 80	73 79 79	77 70 75	$   \begin{array}{c c}     74 \\     66 \\     73   \end{array} $	72 68 71	76 69 73
	4 5 6 7 8 9	95 61 91 95 97 87	95 88 94 91 97 74	96 89 91 92 96 68	88 89 84 89 93 71	85 87 78 92 80 75	83 85 76 90 81 77	76 87 76 90 88 86	76 81 75 94 84 84	75 82 77 92 76 80	71 77 79 93 80 79	59 74 80 92 79 84	69 75 82 92 83 90
ity of the Air.	11 12 13 14 15 16 17 18	84 89 95 93 87 89	80 89 95 86 88 92	77 88 96 88 84 83	76 89 82 72 82 89	72 90 88 65 89 90	72 89 81 64 86 89	72 85 72 60 88 89	72 87 67 56 86 87	73 89 63 58 88 78	70 95 64 55 94 79	77 95 67 62 91 73	81 96 82 67 95 72
Humidity	19 20 21 22 23 24	96 91 87 87 92 92	94 97 87 87 86 94	79 85 85 88 88 82 89	66 89 78 93 85 85	54 83 73 86 81 83	62 79 71 80 97 65	59 77 68 80 95 62	61 80 68 67 93 62	59 82 70 72 84 57	58 79 76 78 86 57	62 80 78 81 75 56	69 75 80 91 70 46
	25 26 27 28 29 30 31 Nov. 1	89 93 85 86 78 70	95 88 88 84 78 84	91 85 82 84 78 72	90 83 78 81 76 76	91 79 73 75 67 76	89 78 72 74 60 80	79 67 63 71 57 80	76 50 68 61 58 84	75 68 63 57 61 90	78 72 66 58 63 92	80 73 68 56 60 80	80 74 81 67 64 91
	lv Means	88	88	85	82	80	78	76	74	74	75	74	77
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	In. '302 '283 '213	In. *281 *281 *221	In. •283 •281 •266	In. •272 •281 •297	In. •270 •285 •301	In. •276 •291 •322	In. 285 283 327	In. '290 '296 '328	In. '311 '266 '326	In. :307 :261 :310	In.	In. •289 •283 •272
	4 5 6 7 8 9	280 188 332 486 438 195	· 290 · 238 · 366 · 471 · 449 · 178	-336 ·301 ·459 ·506 ·452 ·174	 -354 -394 -484 -498 -577 -188	397 419 483 527 563 208	·422 ·435 ·488 ·532 ·562 ·233	·420 ·458 ·510 ·479 ·573 ·256	·420 ·457 ·520 ·469 ·549 ·260	·412 ·459 ·497 ·451 ·369 ·259	· 407 · 446 · 525 · 447 · 357 · 264	365 3414 519 440 332 270	· 385 · 412 · 496 · 430 · 333 · 273
Tension of the Vapour.	11 12 13 14 15 16 17 18	308 306 197 203 278	333 301 192 193 293 202	·347 ·298 ·230 ·219 ·296 ·161	371 306 232 206 301	367 303 290 200 353 184	·379 ·290 ·282 ·200 ·359 ·185	387 278 263 195 384 189	387 282 249 186 412	· 394 · 287 · 238 · 195 · 410 · 168	388 297 247 196 425 171	·410 ·287 ·249 ·214 ·408 ·157	·413 ·264 ·258 ·203 ·421 ·151
Tension	O 18 19 20 21 22 23 24 25	175 241 164 196 124 176	166 264 167 195 126	·180 ·246 ·171 ·199 ·123 ·205	182 261 182 210 138 219	173 ·248 ·183 ·195 ·162 ·232	·204 ·250 ·186 ·183 ·208 ·196	196 256 187 176 212 192	188 267 193 152 227 192	·182 ·249 ·187 ·161 ·213 ·167	184 224 191 159 215 169	194 228 192 155 207 161	197 209 193 163 190
	25 26 27 28 29 30 31 Nov.1	169 340 140 181 158 124	199 1309 145 180 156 153	·217 ·290 ·148 ·188 ·160 ·134	· 236 · 272 · 144 · 212 · 164 · 139	·262 ·258 ·146 ·215 ·152 ·144	· 295 · 273 · 146 · 228 · 144 · 157	295 · 230 · 135 · 196 · 138 · 160	303 193 156 190 141 175	·298 ·235 ·156 ·185 ·147 ·193	· 296 · 225 · 163 · 185 · 149 · 203	·295 ·220 ·163 ·172 ·141 ·191	·283 ·213 ·166 ·190 ·139 ·215
1.	11UV.1	236	•242	254		<u>-</u>	· ₂₈₆	•284	•284	•275	-274	268	-266

			н	MIDITY	OF THE A	AR, AND	TENSION	OF THE	ATMOSPH	ERIC VA	POUR.		
	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
	6	7	8	9	10	11	12	13	14	15	16	17	Means.
	80 71	79 82	80 79	80 87	80 93	80 88	84 91	85 88	93 91	92 91	88 91	89 90	79 83
	83	79	88	78	81	83	<u>-</u> 94	93	93	90	92	$\frac{-}{93}$ }	83
	83 77	82 76	71 87	75 94	83 93	79 92	85 91	93 86	93 90	95 89	93 90	88 91	83 85
Ì	87 91	87 92	86 93	88 94	89 95	74 95	94 95	$\frac{94}{97}$	92 96	94 97	94 97	95 96	86 93
	81 92	81 98	81	75 93	83 92	87 95	84	89	90	88	91	73	85
	$\frac{92}{78}$	87	90	91	$\frac{32}{94}$	96	94 96	84 96	85 91	85 87	91 88	87 } 90	85 83
	97	91 92	i	80 87	83 90	84 93	86 91	85 85	88 83	88 87	87 88	87 95	89 84
	89 78	77	78	73 85	74 79	75 84	74 86	82 85	83 80	90 84	84 81	88 87	74 86
	90 80	86 82	87 80	79	86	81	$\frac{30}{87}$	92	$\frac{00}{90}$	$\frac{01}{93}$	$\frac{01}{90}$	$\frac{3}{87}$ }	85
	<del>74</del>	75 85	75 85	$\frac{-}{76}$ 87	78 87	74 93	82 93	86 87	90 87	92 89	88 94	91 91	$\frac{75}{86}$
	77 81	79 79	85 87	84 89	$\begin{bmatrix} 77 \\ 73 \\ 94 \end{bmatrix}$	79 95	81 92	81 94	81 96	83 95	82 93	84 90	79 86
	78 72	75 73	73 75	81 79	87 85	90 90	89	78	92	93	94	96	85
	69	$\frac{73}{79}$		$\frac{73}{77}$	$\frac{33}{84}$	$\frac{30}{85}$	95 81	96 88	94 88	94 87	94 90	88 } 90	78 84
	79 75	75 91	80 87	78 95	76 95	79 96	88 95	92 87	83 72	77 92	78 89	81 85	78 82
	88 73	74	73 70	79 72	$\begin{array}{c} 75 \\ 72 \end{array}$	73 73	70 74	$\begin{array}{c} 72 \\ 79 \end{array}$	75 76	74 75	77 72	74 70	73 $69$
	64 93	69 93	96	94	96	97 —	$\frac{71}{87}$	90	<del></del>	$\frac{10}{89}$	88	$\frac{1}{92}$ }	87
	81	82	83	83	85	86	87	88	87	89	88	88	82
	In. *295 *267	In. •291 •253	In. •278 •242	In. •265 •230	In. •259 •231	In. •262 •230	In. '266 '234	In. •261 •220	In. •276 •220	In. •272 •210	In. •275 •210	·277 ·216	In. •280 •256
	258	•248	·261	·234	235	·230	•284	-050	_			1	.269
ļ	353	.010			.00=			`258	•249	237	•239	·246 }	
- 1	417	313 374	`301 `400	303 375	$\overset{\boldsymbol{\cdot}}{348}$	·256 ·385	268	255	:249 :244 :354	237 *237 *333	·239 ·234 ·346	·246 } ·236 ·322	$^{:}_{378}$
- 1	'417 '488 '421	$374 \\ 535$	.400 .534	·375 ·539	348 348 535 441	*256 *385 *481 *444	.268 .386 .520 .445		244 354 456 442	`237 `333 `480 `449	•234	.236	·322 ·378 ·487 ·458
	.488 .421 .306	· 374 · 535 · 424 · 296	`400 `534 `424 `292	`375 `539 `442 `250	*348 *535	·385 ·481	*268 *386 *520 *445 *215	255 378 479 439 227	244 354 456 442 224	·237 ·333 ·480 ·449 ·213	*234 *346 *480 *443 *212	·236 ·322 ·482 ·440 ·171 — }	· 322 · 378 · 487 · 458 · 350
	`488 `421 `306 `228	374 535 424 296 220	·400 ·534 ·424 ·292 ·209	`375 `539 `442	348 535 441 226 210	385 481 444 224 205  361	*268 *386 *520 *445 *215 — *337 *358	255 378 479 439 227 — 313	244 354 456 442 224  313 350	237 333 480 449 213 — 318 327	*234 *346 *480 *443 *212 — *325 *331	$egin{array}{c} \cdot 236 \\ \cdot 322 \\ \cdot 482 \\ \cdot 440 \\ \cdot 171 \\$	*322 *378 *487 *458 *350 *247
	·488 ·421 ·306 ·228 — ·409 ·273	374 535 424 296 220 — 437 252	·400 ·534 ·424 ·292 ·209 — ·379 ·248	·375 ·539 ·442 ·250 ·210 — ·359 ·226	348 535 441 226 210	*385 *481 *444 *224 *205 — *361 *225 *258	268 386 520 445 215 337 358 223 256	· 255 · 378 · 479 · 439 · 227 · 313	244 354 456 442 224  313 350 211 228	237 333 480 449 213 — 318 327 210 233	*234 *346 *480 *443 *212  *325 *331 *204 *213	· 236 · 322 · 482 · 440 · 171 	*322 *378 *487 *458 *350 *247 *369 *259 *242
	· 488 · 421 · 306 · 228 · 409 · 273 · 236 · 204	374 535 424 296 220  437 252 239 198	'400 '534 '424 '292 '209 — '379 '248 '250 '197	*375 *539 *442 *250 *210 — *359	348 535 441 226 210  359	**385 **481 **444 **224 **205 **— **361 **225 **225 **205 **248	· 268 · 386 · 520 · 445 · 215 — · 337 · 358 · 223	· 255 · 378 · 479 · 439 · 227 — · 313 · 357 · 218	244 354 456 442 224 — 313 350 211	*237 *333 *480 *449 *213 — *318 *327 *210	*234 *346 *480 *443 *212 — *325 *331 *204	· 236 · 322 · 482 · 440 · 171 · } · 335 · 200	*322 *378 *487 *458 *350 *247 *369 *259
	·488 ·421 ·306 ·228 — ·409 ·273 ·236	374 535 424 296 220  437 252 239	· 400 · 534 · 424 · 292 · 209 — · 379 · 248 · 250 · 197 · 350 · 150 —	375 539 442 250 210  359 226 248 188	*348 *535 *441 *226 *210  *359 *232 *254 *193 *242 *144	**385 **481 **444 **224 **205 **— **361 **225 **225 **205 **248 **142 **—	· 268 · 386 · 520 · 445 · 215 — · 337 · 358 · 223 · 225 · 205 · 251 — · 185	255 378 479 439 227  313 357 218 243 226 224  190	244 354 456 442 224 313 350 2211 228 228 199 	· 237 · 333 · 480 · 449 · 213 — · 318 · 327 · 210 · 233 · 264 · 199 — · 190	*234 *346 *346 *480 *443 *212 *325 *331 *204 *213 *265 *187 *181	· 236 · 322 · 482 · 440 · 171 — } · 291 · 335 · 200 · 215 · 283 · 185 — } · 174	*322 *378 *487 *458 *350 *247 *369 *259 *242 *211 *312 *172
	· 488 · 421 · 306 · 228 · 409 · 273 · 236 · 204 · 394 · 166 ·	· 374 · 535 · 424 · 296 · 220 — · 437 · 252 · 239 · 198 · 367 · 162 — · 200	· 400 · 534 · 424 · 292 · 209 — · 379 · 248 · 250 · 197 · 350 · 150 — · 200 · 198	**375	*348 *535 *441 *226 *210  *359 *232 *254 *193 *242 *144  *201 *180	**385 **481 **444 **224 **205 **— **361 **225 **225 **225 **248 **142 **— **202 **180	268 386 520 445 215 337 358 223 256 205 251 185 232	255 378 479 439 227 313 357 218 243 226 224 190 232 167	244 354 456 442 224 313 350 211 228 228 199 182 238 161	· 237 · 333 · 480 · 449 · 213 — · 318 · 327 · 210 · 233 · 264 · 199 — · 190 · 239 · 162	*234 *346 *346 *480 *443 *212 *325 *331 *204 *213 *265 *187 *181 *236 *162	· 236 · 322 · 482 · 440 · 171 —   · 291 · 335 · 200 · 215 · 283 · 174 · 238 · 168	*322 *378 *487 *458 *350 *247 *369 *259 *242 *211 *312 *172 *202 *212
	· 488 · 421 · 306 · 228 · 409 · 273 · 236 · 204 · 394 · 166	**374 **535 **424 **296 **220 **	· 400 · 534 · 424 · 292 · 209 — · 379 · 248 · 250 · 197 · 350 · 150 — · 200	375 539 442 250 210 359 226 248 188 304 141 200	*348 *535 *441 *226 *210  *359 *232 *254 *193 *242 *144  *201 *180 *167 *131	**385 **481 **444 **224 **205 **— **361 **225 **225 **225 **248 **142 **— **202 **180 **171 **120	268 386 520 445 215 — 337 358 223 256 205 251 — 185 232 169 174 114	255 378 479 439 227 313 357 218 243 226 224 190 232 167 174 115	244 -354 -456 -442 -224 -313 -350 -211 -228 -228 -199182 -238 -161 -176 -112	· 237 · 333 · 480 · 449 · 213 — · 318 · 327 · 210 · 233 · 264 · 199 — · 190 · 239 · 162 · 183 · 110	*234 *346 *346 *480 *443 *212 **212 **325 *331 *204 *213 *265 *187 *** **181 **236 **162 **188 **115	· 236 · 322 · 482 · 440 · 171 —   · 291 · 335 · 200 · 215 · 283 · 185 —   · 174 · 238 · 168 · 191 · 118	*322 *378 *487 *458 *350 *247 *369 *259 *242 *211 *312 *172 *202 *212 *181 *151
	· 488 · 421 · 306 · 228 · 409 · 273 · 236 · 204 · 394 · 166 · 205 · 206 · 191	**374 **535 **424 **296 **220 **— **437 **252 **239 **198 **367 **162 **— **200 **204	· 400 · 534 · 424 · 292 · 209 —— · 379 · 248 · 250 · 197 · 350 · 150 —— · 200 · 198 · 173	· 375 · 539 · 442 · 250 · 210 — · 359 · 226 · 248 · 188 · 304 · 141 — · 200 · 188 · 177	*348 *535 *441 *226 *210  *359 *232 *254 *193 *242 *144  *201 *180 *167	**385 **481 **444 **224 **205 **— **361 **225 **225 **225 **248 **142 **— **202 **180 **171 **120 **193 **159	· 268 · 386 · 520 · 445 · 215 — · 337 · 358 · 223 · 256 · 205 · 251 — · 185 · 232 · 169 · 174 · 114 · 193 —	· 255 · 378 · 479 · 439 · 227 — · 313 · 357 · 218 · 243 · 226 · 224 — · 190 · 232 · 167 · 174 · 115 · 169 —	244 354 456 442 224 313 350 211 228 228 199 182 238 161 176 112 195	· 237 · 333 · 480 · 449 · 213 — · 318 · 327 · 210 · 233 · 264 · 199 — · 190 · 239 · 162 · 183 · 110 · 193 —	234 346 480 443 212 - 325 331 204 213 265 187 - 181 236 162 188 115 190 -	· 236 · 322 · 482 · 440 · 171   · 291 · 335 · 200 · 215 · 283 · 185   · 174 · 238 · 168 · 191 · 118 · 180 	*322 *378 *487 *458 *350 *247 *369 *259 *242 *211 *312 *172 *202 *212 *181 *151 *183
	· 488 · 421 · 306 · 228 · 409 · 273 · 236 · 204 · 394 · 166 · 205 · 206 · 191 · 137 · 191 · 169 · 313	374 535 424 296 220 — 437 252 239 198 367 162 — 200 204 180 134 192	· 400 · 534 · 424 · 292 · 209 · 379 · 248 · 250 · 197 · 350 · 150 · — · 200 · 198 · 173 · 141 · 174 · 166 · — · 301	· 375 · 539 · 442 · 250 · 210 · 359 · 226 · 248 · 188 · 304 · 141 · 200 · 188 · 177 · 138 · 188 · 188 · 156 · 303	*348 *535 *441 *226 *210  *359 *232 *254 *193 *242 *144  *180 *167 *131 *199 *159  *323	**385 **481 **444 **224 **205 **361 **225 **225 **248 **142 *** **202 **180 **171 **120 **193 **159 *** **326	· 268 · 386 · 520 · 445 · 215 — · 337 · 358 · 223 · 256 · 205 · 251 — · 185 · 232 · 169 · 174 · 114 · 193 — · 182 · 322	255 378 479 439 227 313 357 218 243 226 224 190 232 167 174 115 169 178 331	· 244 · 354 · 456 · 442 · 224 - 313 · 350 · 211 · 228 · 228 · 199 - 182 · 238 · 161 · 176 · 112 · 195 - 183 · 331	· 237 · 333 · 480 · 449 · 213 — — — — — — — — — — — — — — — — — — —	*234 *346 *346 *480 *443 *212 *325 *331 *204 *213 *265 *187 *181 *236 *162 *188 *115 *190 *777 *337	· 236 · 322 · 482 · 440 · 171   } · 291 · 335 · 200 · 215 · 283 · 185   } · 174 · 238 · 168 · 191 · 118 · 180   } · 341	*322 *378 *487 *458 *350 *247 *369 *259 *242 *211 *312 *172 *202 *212 *181 *151 *183 *178 *292
	· 488 · 421 · 306 · 228 · 409 · 273 · 236 · 204 · 394 · 166 · 205 · 206 · 191 · 137 · 191 · 169 · —	· 374 · 535 · 424 · 296 · 220 · 437 · 252 · 239 · 198 · 367 · 162 · 200 · 204 · 180 · 134 · 192 · 169 · —	· 400 · 534 · 424 · 292 · 209 · 379 · 248 · 250 · 197 · 350 · 150 · 198 · 173 · 141 · 174 · 166 · 301 · 206 · 138	375 -539 -442 -250 -210359 -226 -248 -188 -304 -141200 -188 -177 -138 -188 -156303 -189 -156	*348 *535 *441 *226 *210  *359 *232 *254 *193 *242 *144  *201 *180 *167 *131 *199 *159  *323 *184 *167	**385 **481 **444 **224 **205 **361 **225 **225 **248 **142 **** **1202 **180 **171 **120 **193 **159 **** **326 **183 **169	· 268 · 386 · 520 · 445 · 215 · 337 · 358 · 223 · 256 · 205 · 251 · 185 · 232 · 169 · 174 · 114 · 193 · 182 · 322 · 190 · 150	255 378 479 439 227 313 357 218 243 226 224 190 232 167 174 115 169 178 331 191	244 354 456 442 224 313 350 211 228 228 199 318 161 176 112 195 31 166 150	· 237 · 333 · 480 · 449 · 213 — · 318 · 327 · 210 · 233 · 264 · 199 — · 190 · 239 · 162 · 183 · 110 · 193 — · 183 · 321 · 155 · 175	*234 *346 *346 *480 *443 *212 ** *325 *331 *204 *213 *265 *187 ** *181 *236 *162 *188 *115 *190 ** *177 *337 *158 *166	· 236 · 322 · 482 · 440 · 171 — } · 291 · 335 · 200 · 215 · 283 · 185 — } · 174 · 118 · 180 — } · 165 · 341 · 144 · 165	*322 *378 *487 *458 *350 *247 *369 *259 *242 *211 *312 *172 *202 *212 *181 *151 *183 *178 *292 *218 *154
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	· 488 · 421 · 306 · 228 — — — — — — — — — — — — — — — — — — —	**374 **535 **424 **296 **220 **437 **252 **239 **198 **367 **162 **200 **204 **180 **134 **192 **169 **201 **145 **180	· 400 · 534 · 424 · 292 · 209 · 379 · 248 · 250 · 197 · 350 · 150 · — · 200 · 198 · 173 · 141 · 174 · 166 · — · 301 · 206 · 138 · 174	375 -539 -442 -250 -210359 -248 -188 -304 -141200 -188 -177 -138 -188 -156303 -189 -156 -185	*348 *535 *441 *226 *210  *359 *232 *254 *193 *242 *144  *201 *180 *167 *131 *199 *159  *323 *184 *167 *172	**385 **481 **444 **224 **205 **— **361 **225 **225 **225 **248 **142 **— **202 **180 **171 **120 **193 **159 **— **326 **183 **169 **163	· 268 · 386 · 520 · 445 · 215 · 337 · 358 · 223 · 256 · 205 · 251 · 185 · 232 · 169 · 174 · 114 · 193 · 182 · 322 · 190 · 150 · 152	255 378 479 439 227 313 357 218 243 226 224 190 232 167 174 115 169 — 178 331 191 157	244 354 456 442 224 313 350 211 228 228 199 182 238 161 176 112 195 183 331 166 150 156	· 237 · 333 · 480 · 449 · 213 — · 318 · 327 · 210 · 233 · 264 · 199 — · 190 · 239 · 162 · 183 · 110 · 193 — · 183 · 321 · 155 · 175 · 154	*234 *346 *346 *480 *443 *212 **212 **325 *331 *204 *213 *265 *187 *** **181 **236 *162 *188 *115 *190 *** **177 **337 **158 **166 **157	· 236 · 322 · 482 · 440 · 171 — } · 291 · 335 · 200 · 215 · 283 · 185 — } · 174 · 188 · 191 · 118 · 180 — } · 165 · 341 · 165 · 153	*322 *378 *487 *458 *350 *247 *369 *259 *242 *211 *312 *172 *202 *212 *181 *151 *183 *178 *292 *218 *154 *179

				HUMI	DITY OF	THE AIR	, AND TE	NSION OF	THE AT	MOSPHER	IC VAPO	UR.		
G	rs of l ötting Time	Mean gen	0	1	2	3	4	5	6	7	8	9	10	11
1	rs of 1 Poron Time	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
		( 2   3   4   5   6   7   8	94 95 91 92 95 86	92 93 90 89 91 81	95 94 92 82 64 82	92 91 82 81 88	93 89 71 76 88 80	97 80 67 70 79 82	93 79 62 69 74 78	93 77 60 72 66 77	93 79 57 70 68 73	95 76 54 69 68 76	94 82 57 75 57	96 89 - 65 84 72 62
of the Air.	MBER,	9 10 11 12 13 14 15	96 93 90 82 86 90	96 95 92 79 84 89	96 93 93 82 84 91	96 94 93 82 85 89	96 88 92 82 84 84	94 85 90 79 87 84	93 80 91 77 89 80	92 81 93 78 87 85	92 82 93 77 84 77 —	94 90 90 80 84 70 —	91 85 90 79 84 72 —	93 84 86 84 87 75 —
Humidity o	NOVEMBER	16 17 18 19 20 21 22 23	93 92 93 92 81 79 —	91 91 94 88 77 80 —	95 89 95 85 77 77 —	93 89 92 90 76 77 —	$93 \\ 83 \\ 84 \\ 91 \\ 68 \\ 71 \\ \hline 74$	90 87 74 89 73 70 —	89 85 74 89 66 73 —	85 78 63 90 68 73 —	$   \begin{array}{r}     80 \\     82 \\     67 \\     92 \\     71 \\     \hline     74 \\     \hline     58 \\   \end{array} $	85 66 90 74 80 —	86 74 89 74 75 —	90 76 90 77 86 —
		24 25 26 27 28 29	91 84 75 76 93	89 84 72 82 93	90 87 74 85 82	88 90 76 88 84	82 80 79 74 85	74 78 76 71 82	79 86 85 75 72	68 73 85 80 68	79 76 85 81 67	71 75 70 79 68	69 80 71 75 76	76 87 75 75 76
_		(30	80	86	84	83	76	77	76	78	81	79	76	79
Ноц	urly I	Means	88	87	86	86	83	80	79	77	78	77	77	81
Tension of the Vapour.	NOVEMBER.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20	In.  '317 '300 '240 '201 '161 '201 '338 '328 '331 '245 '263 '258 '255 '227 '263 '241 '178 '178 '135 '177 '081 '103 '204 '121	In.  '308 '298 '240 '198 '164 '203 '337 '333 '340 '236 '260 '249 '259 '234 '257 '230 '169 '173 '138 '165 '103 '079 '102 '202 '121	In.  '311 '305 '272 '204 '136 '217 '347 '336 '343 '245 '260 '246 '268 '248 '283 '219 '169 '170 '138 '171 '198 '085 '108 '189 '118	In.  331 315 286 226 213 236 351 350 346 253 263 248 272 261 315 224 168 175 140 177 101 096 119 191	In.  343 323 252 246 252 244  382 349 347 260 263 242  288 265 324 229 164 166  141 189 089 107 106 196	In.  368 313 249 243 258 265 374 354 346 256 272 238 297 270 302 232 181 172 147 187 090 115 105 201	In.  356 312 239 243 254 273 385 348 345 253 272 292 232 173 184 130 198 076 130 119 187 123	In.  '354 '300 '230 '253 '237 '261 '381 '352 '351 '263 '270 '250 '280 '270 '248 '231 '181 '187 '123 '189 '085 '134 '135 '187 '126	In.  362 307 223 240 243 259 376 352 349 261 265 232 277 272 250 233 196 199 — 128 197 091 138 144 187 — 133	In.  '375 '294 '214 '240 '245 '265	In.  375 317 212 243 199 244  371 334 258 267 214  272 278 247 223 190 200  144 160 095 103 146 188  120	In.  379 307 215 236 222 215 363 324 329 269 272 315 270 290 244 211 185 200 158 156 103 102 118
11-		30	$\frac{\cdot_{121}}{\cdot_{218}}$	121	118	123	120	123	123	126	133	125	230	·233
HOU	uriy I	Means	218	·216	•223	•231	*235	•238	271	200	201	200	200	

		н	UMIDITY	OF THE A	AIR, AND	TENSION	OF THE	ATMOSPI	IERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
96 89 71 93 70 59	97 89 78 97 75 61	97 89 78 88 77 63	96 88 80 92 85 63	96 88 80 88 89 61	95 81 82 92 88 61	95 88 84 91 89	96 93 86 89 90	90 91 89 91 81	90 89 88 87 82	93 92 87 99 86	95 92 89 87 85	94 87 77 84 79
90 85 89 83 87 75	93 84 86 80 85 74 93	92 85 85 81 85 80 92	92 85 80 79 87 76 —	90 84 80 81 86 77 	91 82 81 81 86 79	92 91 88 83 82 86 — 90 91	88 92 89 82 80 87 	94 91 88 82 80 86 90	97 92 88 83 80 88 — 91 91	97 94 91 83 80 87 — 93 89	94	93 87 87 80 86 83
92 83 91 77 80 	92 82 91 83 84 	92 83 88 86 79 74 78	92 85 93 89 81 	91 88 85 92 79 —————————————————————————————————	89   89   87   93   80   —   92   80	92 90 87 93 — 71 93 89	89 93 87 86  69 86 82	90 96 87 89 	90 93 87 87 71 90 79	91 90 88 82 — 79 90 80	93 92 84 81 —————————————————————————————————	89 84 89 80 77 78
91 78 66 74 —	94 76 72 79 — 82	$   \begin{array}{c}                                     $	$   \begin{array}{c}     75 \\     73 \\     83 \\     86 \\     \hline     95   \end{array} $	75 74 92 82 — 88	75 75 95 89	$   \begin{array}{r}                                     $	74 80 95 	69 85 95 	82 78 95  81 86	81 72 96 — 80 88	$ \begin{array}{c c} 81 \\ 76 \\ 93 \\ \hline 74 \\ 87 \end{array} $	81 77 83 78
82	83	83	84	84	85	87	86	86	87	88	87	83
In.  377 307 212 215 203 211  357 326 329 264 272 221  276 284 251 210 181 210 159	In.  '373 '302 '218 '201 '199 '215 '359 '324 '316 '257 '268 '228 '278 '289 '239 '210 '191 '224 '154	Iu.  '376 '304 '211 '185 '183 '230	In.  -364 -301 -204 -193 -191 -231355 -329 -273 -250 -270 -245263 -296 -242 -211 -193 -238164	In.  '350 '301 '202 '172 '195 '214  -347 '328 '264 '254 '263 '247 -299 '246 '194 '191 '235 -157	In.  343 263 205 170 197 214  345 322 262 247 256 250 258 297 240 183 186 228 195	In.  1328 243 208 156 199 316 345 341 265 249 254 255 254 298 246 188 178 127	In.  1335 1246 1205 159 190 190 190 1340 1340 1247 1258 1247 1258 1247 1258 173 188 173 193	1n279 -228 -207 -161 -188329 -335 -331 -264 -247 -254252 -244 -281 -255 -188 -188 -195	In.    244     234     204     152     184     338     323     264     247     257     241     233     249     188     189     125     190	In.	In.  280 242 199 159 194	In.  1337 1287 1293 1203 1204 1257 1355 1366 1311 1253 1268 1245 1265 1275 1258 1212 183 182 159
160 105 105 136 172	143 106 106 152 177 	143 1091 100 167 167 	145 1080 102 169 180  109	138 1080 103 179 164 —	138 1078 1111 192 167 	152 1080 1111 197 	135 1078 120 196 — 119 1080	121 1075 125 195 — 122 1085	119 1093 1112 1195 — 134 1076	115 1094 103 207  131 1080	124 088 103 204 	157 1095 107 153 170
•226	*225	•225	•224	219	•218	•216	•212	•211	•209	•210	•209	•224

Vol. III.

			немі	DITY OF	THE AIR,	, AND TE	NSION OF	THE AT	MOSPHER	IC VAPO	U R.		
lours o Göttii Tir	f Mean and ngen ne.	0	1	2	3	4	5	6	7	8	9	10	11
Hours o Tord Tin	of Mean onto ne.	18	19	20	21	22	23	0	1	2	3	4	5
	$\begin{pmatrix} 1\\2\\3\\4\\5\\c$	86 91 71 85 78	93 94 71 86 88	71 95 65 86 88	84 95 57 84 81	84 97 69 93 86	84 96 70 72 81	80 96 75 72 78	79 95 80 73 75	80 92 59 80 75	84 92 65 76 79	83 90 70 76 87	82 91 72 68 88
JF.	6 7 8 9 10 11 12	78 87 80 87 82 86	75 85 78 87 78 94	82 83 79 80 81 85	80 87 76 90 78 88	80 80 81 95 75 85	81 77 80 95 72 84	81 72 81 95 74 81	81 74 79 93 76 76	83 73 75 95 76 77	84 74 76 96 80 77	84 74 76 95 77 81	89 81 74 86 81 84
numidity of the Air.	19	91 /00 80 85 80 82	93 400 81 87 79 80	80 700 70 85 77 89	80 95 78 89 78 84	74 85 74 86 72 77	76 81 74 90 69 73	71 62 72 85 71 69	65 60 74 84 69 74	66 65 79 82 64 89	78 54 74 82 76 79	72 60 85 81 80 69	74 67 82 79 76 75
H	20 21 22 23 24 25 ^a	83 82 100 79	81 87 100 89	75 81 100 83	76 69 700 84	75 69 93 78	67 71 83 78	63 63 79 78	60 66 77 79	55 66 74 77	56 71 71 77	62 73 70 77	79 84 97 81
	26 27 28 29 30 31	96 	92 73 86 95 95	86 	88 	82 71 74 95 93	76  73 75 95 90	75 70 83 94 90	78 	$ \begin{array}{c c} 81 \\ \hline 71 \\ 75 \\ 82 \\ 88 \end{array} $	$ \begin{array}{c c} 74 \\ \hline 72 \\ 76 \\ 82 \\ 83 \end{array} $	$ \begin{array}{c c} 81 \\ \hline 71 \\ 76 \\ 88 \\ 88 \end{array} $	79 74 77 91 93
lourly	Means	85	87	83	83	82	79	77	77	76	76	78	81
	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{pmatrix}$	In. '076 '179 '140 '121 '131	In. '079 '191 '139 '122 '143	In. '066 '198 '125 '128 '143	In.	In. '097 '216 '136 '165 '156	In. '108 '223 '139 '136 '157	In. '110 '229 '150 '140 '155	In. 1116 244 152 143 154	In. '121 '257 '114 '157 '151	In. '128 '245 '121 '155 '158	In. 128 239 124 155	In. 132 255 128 136 168
ur.	6 7 8 9 10 11 12	158 196 149 159 116	154 192 144 159 105 095	165 176 142 148 106 085	176 188 135 153 104 086	178 178 144 158 108 108	186 171 143 161 110	·189 ·155 ·149 ·164 ·114 ·083	192 164 147 166 121	196 163 142 173 121 085	198 164 143 177 130 088	·201 ·157 ·143 ·168 ·126 ·094	
DECEMBER.	1 10	· 087 · 068 · 067 · 104 · 066 · 135	· 090 · 066 · 069 · 109 · 065 · 133	·079 ·073 ·063 ·108 ·061 ·143	·077 ·077 ·082 ·122 ·074 ·135	· 073 · 087 · 091 · 125 · 078 · 128	·079 ·091 ·108 ·130 ·087 ·128	·079 ·079 ·110 ·129 ·100 ·126	·079 ·085 ·114 ·124 ·108 ·142	· 085 · 096 · 121 · 122 · 110 · 159	°095 °082 °111 °126 °126 °148	·084 ·085 ·121 ·122 ·128 ·126	· 085 · 081 · 106 · 105 · 123 · 133
. Te	20 21 22 23 24 25 ^a	·101 ·101 ·066 ·120	.093 .101 .057 .139	.079 .091 .058 .132	· 084 · 082 · 072 · 140	.088 .085 .085 .137	.086 .089 .086 .152	· 088 · 083 · 089 · 154	-088 -089 -094 -154	.086 .095 .097 .154	.086 .102 .094 .155	·091 ·102 ·092 ·154	· 094 · 103 · 091 · 167
	$\begin{vmatrix} 25 \\ 26 \\ 27 \end{vmatrix}$	.093	.089	.083	· 094	105	112	·123	131	142	138	·142	.120
	28 29 30 31	·160 ·083 ·207 ·188	148 1093 209 187	150 1092 208 202	152 1097 212 206	·148 ·107 ·214 ·215	·144 ·115 ·226 ·213	· 124 · 127 · 219 · 213	·132 ·124 ·221 ·215	·125 ·116 ·198 ·219	·124 ·121 ·193 ·207	·123 ·121 ·198 ·210	·124 ·125 ·197 ·215
		122	122	119	125	130	133	134	137	139	139	138	•140

		HU	MIDITY	OF THE A	IR, AND	TENSION	OF THE	ATMOSPH	ERIC VAI	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily an Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
85	77 93	83 93	79 89	78 87	80 83	$\frac{82}{75}$	87 67	$\frac{85}{82}$	92 84	90 80	90 73	83 88
$\frac{89}{75}$	79	$\frac{95}{74}$	77	80	00 74	$\frac{73}{78}$	78	78	80	80	78	73
66	68	80	89	90	89	89	89	91	90	87	78 84	82
84	74	75	78	79	80						— 7 l	81
						86	81	81	81	80	80 }	
89	89 79	$\frac{92}{78}$	91 78	95 80	94 78	$\frac{94}{76}$	89 78	93 79	$\frac{95}{78}$	$\frac{95}{82}$	$\frac{94}{82}$	87 79
80 78	86	85	83	78	83	70 79	81	84	84	85	84	$\frac{19}{79}$
86	94	90	87	89	87	88	91	89	89	87	86	90
78	80	83	80	80	81	90	91	87	87	91	85	81
82	79	86	82	85	82					<u> </u>	$-\frac{1}{91}$	85
$\frac{-}{75}$	81	$\frac{-}{92}$	$\frac{-}{92}$	$\frac{-}{85}$	99	91 100	89 97	93 99	$\frac{92}{100}$	95 99	100	85
88	93	96	96	98	96	95	96	97	86	86	87	85
88	84	80	86	88	89	89	89	87	86	87	87	82
86	91	81	92	91	74	81	86	73	68	70	66	82
76 71	75 71	$\begin{array}{c} 75 \\ 72 \end{array}$	67	68 76	59 76	64	70	70	75	77	85	73
/ L	71	12	77			$\frac{-}{74}$	80	$\frac{-}{75}$	$\overline{79}$	$\frac{-}{78}$	$\left[\begin{array}{c} -1\\ 82 \end{array}\right]$	77
91	89	89	88	88	81	81	70	75	73	67	87	75
85	89	83	82	89	89	91	100	100	86	98	100	81
93 81	89 78	$\frac{93}{79}$	89	88 82	96 81	94	88	92	92	93	84	89
			79 —			92	94	85	89	93	99 }	83
74	75 —	78 —	77	73	78 —	86	91	89	91	89	$\frac{1}{78}$	82
78	80	59	71	69	73	66	83	70	78	85	89	74
81	78	77	72	75	80	86	88	88 94	89 95	90 96	96 94	81 92
90 97	$\begin{array}{c} 93 \\ 95 \end{array}$	90 90	$\frac{94}{95}$	93 95	91 95	93 94	$\frac{92}{93}$	94 91	91	88 88	89	92
83	83	83	83	84	83	85	86	86	86	86	87	82
In.	In.	In.	ſn.	In.	In.	In.	In.	In.	In.	In.	In.	In.
136	131	146	145	143	150	152	164	.163	172	•170	171	129
263	279	278	248	245	287	256	185	211	190	174	152	227
130 132	133	$^{123}_{153}$	$^{:123}_{:162}$	·120 ·163	·106 ·161	108 1 <b>5</b> 9	·109 ·159	110 162	114 161	·115 ·150	110 141	· 124 · 147
152	`134 `129	.130	$^{102}_{135}$	133	135	159	199	102		1.50		
					_	156	152	152	152	155	$\{-\frac{1}{155}\}$	148
221	•221	•220	•226	.228	228	•229	217	215	218	212	214	203
158	156	154	151	153	147	145	148	·142 ·141	`137 `141	147 139	153 133	160 143
$^{146}_{154}$	$152 \\ 155$	150 141	$^{\cdot 146}_{\cdot 132}$	·135 ·133	`144 `133	137 134	137 138	133	.133	133	126	149
129	131	136	131	130	126	132	109	.099	.095	.095	.092	117
.098	095	<b>.</b> 097	.091	.082	.082				•00.7		$-\frac{1}{087}$	.088
081	.084	.089		.077	.074	$\begin{array}{c} 084 \\ 075 \end{array}$	.084 .078	.087 .079	.085 .083	.088 .070	.0873	.081
089	.084 .088	.083	084	.077	$074 \\ 072$	$075 \\ 072$	.078	.079	.071	.068	.070	.078
112	115	124	113	117	.110	.110	.110	.110	.110	.115	.109	105
094	.090	.086	102	.100	.077	.078	.082	.068	.066	.065	:061	100
123	117	113	116	·112	·102 ·125	.110	119	.119	·125	·126	140	106
125	122	·121	126	·125	125	.103	.108	.098	.099	.103	$\{-\frac{1}{101}\}$	125
.088	.082	.081	.081	.088	.086	.089	.084	.094	.099	.099	129	.090
'096	.097	102	105	114	.111	105	.097	.069	.078	076	<b>.</b> 069	.093
081	.090	.092	·098	·084	.080	.081	'082	.084	'084	.089	101	084
167	·165	·166	·164	·171	·172 —	·111	·112	102	105	105	$\cdot_{099}^{-}$ }	142
142	·146	154 —	152	·149	•166 —	$\frac{-}{220}$	· <del>2</del> 18	· <del>2</del> 13	$\frac{-}{211}$		$\left. \frac{-}{164} \right\}$	148
128	130	.090	102	.097	101	.099	107	085	.098	103	104	121
126	133	132	130	137	150	162	.166	166	179	186	202	133
$\frac{192}{223}$	197 217	$^{188}_{200}$	$\overset{\cdot 191}{\cdot 212}$	$^{186}_{207}$	183 206	$^{:186}_{:206}$	$^{:190}_{:203}$	·197 ·200	$\overset{\boldsymbol{\cdot}}{}\overset{\boldsymbol{188}}{}\overset{\boldsymbol{\cdot}}{}\overset{\boldsymbol{202}}{}$	·188 ·191	. 186 . 193	`199 `206
											128	
138	138	137	135	135	135	135	.132	.130	131	.129	* 100	133

			HUM	DITY OF	THE AIR	, AND TE	ENSION OI	THE AT	MOSPHEI	RIC VAPO	UR.		
Hours o Götti Ti	of Mean }	0	1	2	3	4	5	6	7	8	9	10	11
Hours of Tor-	of Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\left( egin{array}{c} 1 \\ 2 \\ 3 \end{array} \right)$	88 74	87 76	89 70	87 74	88 71	87 71	87 79	86 80	84 81	83 81	86 81	87 78
	4 5 6 7 8 9	78 67 73 80 75 89	74 62 75 87 83 82	78 50 75 87 77 89	74 59 74 90 87 79	71 51 90 90 81 78	61 55 74 89 74 75	73 55 55 78 75 67	78 46 55 78 74 69	84 68 55 76 75	87 63 59 71 81 69	91 74 63 73 80 71	91 61 65 76 80 72
idity of the Air.	. 11 12 . 13	88 68 66 81 92 82	90 83 66 87 93 71	99 76 69 91 93 64	89 72 71 91 95 61	74 69 67 89 95 63	70 69 60 92 95 61	70 66 68 92 95 80	65 61 64 82 93 95	58 63 66 81 93 69	61 62 68 83 92 59	65 72 65 88 95 59	69 85 73 88 95 56
Humidity	Y 18 19 20 21 22 23 24	70 77 83 78 77 64	71 95 87 79 75 65	72 76 83 69 83 63	72 78 80 69 75 61	69 55 67 64 77 54	60 56 56 59 65 55	60 54 60 80 67 60	65 60 59 80 65 43	57 61 58 80 63 46	53 65 63 77 49 44	53 62 57 76 73 47	60 72 65 83 77 56
	25 26 27 28 29 30 31	78 88 80 95 90 69	81 92 80 92 86 72	83 93 81 90 85 78	72 89 79 94 78 78	72 92 75 79 79 74	71 95 71 82 88 63	71 94 67 87 80 59	75 90 67 85 69 68	75 81 67 89 66 68	79 82 62 85 80 69	74 74 61 87 85 75	74 71 63 90 89 81
Hourly	y Means	79	80	79	78	74	71	72	71	70	70	73	75
	$egin{array}{c} 1 \\ 2 \\ 3 \end{array}$	In. • 191 • 156	In. 188 164	In. 190 147	In. •183 •155	In. •184 •153	In. 182 153	In. 183 175	In. 179 177	In. 169 176	In. 167 170	In. 167 168	In. :167 :160
	4 5 6 7 8 9	155 146 124 131 055 069	150 133 130 135 1057 1065	148 110 129 133 051 069	151 123 136 134 057 066	146 108 170 131 055 069	130 123 148 128 1053 1069	149 120 108 110 054 068	158 106 107 103 056 076	168 152 104 1099 1057 1069	174 132 110 098 063 075	183 154 119 096 060 075	187 126 117 1093 1059
Tension of the Vapour.	11 12 13 14 15 16	·037 ·056 ·091 ·168 ·201 ·174	. 046 . 070 . 093 . 182 . 203 . 147	'049 '066 '101 '193 '204 '124	·055 ·065 ·107 ·293 ·218 ·113	·055 ·066 ·115 ·192 ·222 ·117	·055 ·069 ·106 ·202 ·226 ·114	·056 ·067 ·122 ·211 ·231 ·157	·053 ·063 ·126 ·203 ·247 ·161	.050 .066 .133 .196 .245 .109	·055 ·064 ·136 ·199 ·231 ·079	·057 ·072 ·128 ·204 ·229 ·071	·060 ·079 ·137 ·199 ·235 ·059
Tension C	17 18 19 20 21 22 23 24	·121 ·059 ·052 ·069 ·051 ·080	131 066 054 068 049 084	134 055 054 057 053 088	136 1055 1059 1058 1051 1093	136 040 060 054 053 091	·125 ·043 ·059 ·049 ·051 ·100	·124 ·043 ·068 ·059 ·052 ·111	132 1046 1068 1059 1055 1081	116 047 068 056 056 087	103 1049 1075 1049 1043 1083		·111 ·049 ·073 ·048 ·071 ·095
	25 26 27 28 29 30 31	·079 ·127 ·067 ·054 ·107 ·085		. 087 . 173 . 068 . 054 . 114 . 083	·084 ·169 ·071 ·063 ·110 ·085	· 098 · 176 · 069 · 064 · 120 · 080	·099 ·188 ·066 ·080 ·141 ·064	101 187 1063 1094 139	·107 ·165 ·064 ·096 ·128 ·069	108 130 1064 106 126 1069		106 108 053 105 140	·102 ·103 ·058 ·102 ·140 ·071
	( 1					1	:						

	!		Н	UMIDITY	OF THE	AIR, AND	TENSION	OF THE	ATMOSPI	HERIC VA	POUR.		
!	12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
	6	7	8	9	10	11	12	13	14	15	16	17	Means.
	89 74	88 73	87 74	87 72	90 73	90 73	94	94	87	89	86	74	87
ĺ		_	_				95	93	84	83	86	80 }	78
į	$\frac{91}{64}$	92 68	92 65	96 69	94 69	87 62	80 72	73 75	77 81	73 85	81 78	74 73	81 66
	54	67	64	69	66	63	66	68	67	70	73	77	67
	68 80	67 78	69 78	72 77	55 85	67 85	73 75	81 79	85 78	75 77	75 77	81 77	77 79
	70	68	71	77	72	73			-			$\left \begin{array}{c} \frac{1}{72} \end{array}\right\}$	75
i	$\frac{-}{76}$	${71}$	81	80	$\frac{}{79}$	86	74	92 80	100 89	60 83	52 80	$\begin{bmatrix} 72 \ 83 \end{bmatrix}$	77
	92	79	81	79	79	82	93	82	72	83	74	73	75
	$\begin{array}{c} 76 \\ 92 \end{array}$	$\begin{array}{c} 72 \\ 95 \end{array}$	76 94	$\begin{array}{c c} 74 \\ 92 \end{array}$	78 94	78 90	72 86	78 93	79 90	79 90	76 88	76 94	72 85
1	95	95	95	95	94	90	88	88	87	90	84	86	$\frac{63}{92}$
	6 <b>6</b>	69	70	73	75	77	77	$\frac{-}{72}$	69	69	$\frac{}{71}$	$\left\{\begin{array}{c} \overline{72} \end{array}\right\}$	70
	$\overline{73}$	90	80	87	87	86	66	59	61	69	70	76	69
	75 69	75 69	77	73	74	76	76	79	83	83 84	76 77	79	$\frac{72}{70}$
i	95	95	78 85	80 76	80 81	84 81	80 83	82 83	78 85	81	79	78 79	73 79
	$\begin{array}{c} 78 \\ 63 \end{array}$	77	73	72	64	70	62	65	69	69	62	63	70
		74	76	79	83	78	95	84	84	80	$\frac{-}{79}$	$\begin{bmatrix} -75 \end{bmatrix}$	67
	78	78	79	77	85	82	85	87	92	86	89	89	80
!	74 66	73 76	77 81	69 85	66 83	73 85	$\begin{array}{c c} 72 \\ 85 \end{array}$	76 90	75 100	74 100 �	79 100	81 76	80 78
1	89	88	89	94	97	89	92	83	88	89	92	91	89
ļ	89 79	85 79	93 75	91 75	89 80	84 83	79	86	86	75	76	72	83
							73	61	63	79	86	87 }	74
	78	78	79	80	80	80	80	80	81	80	79	78	77
	·1n. ·166	In. •162	In. 162	In. 160	In. 168	In. •174	In. •191	In. 189	In 187	In. •191	In. 183	In. 156	In. 177
	155	153	151	147	148	148	ļ	<u> </u>				- 1	155
	$\cdot \overline{187}$	•202	•199	$\frac{-}{223}$	•226	•233	131 207	$^{126}_{184}$	143 181	·150 ·170	`164 `180	153 } 164	.177
	.134	141	137	142	142	129	141	142	153	145	131	123	133
!	.096 .073	·119 ·068	·112 ·067	.118 .068	·113 ·055	107	.110 .066	$^{:112}_{:071}$	112	117 068	·122 ·067	·127 ·069	:119 :091
1	.060	.058	.058	.056	.058	.028	.052	057	.058	.058	.059	.059	057
ı	·073	.070	074	.076	.072	·072	.049	055	.054	.028	$\cdot _{025}^{-}$	$-\frac{1}{033}$	·064
	064	$\cdot 058$	.065	065	.063	.068	<u> </u>	.062	.072	.070	*068	.068	.059
	.078 .139	.068 .134	.071 .137	.071 .138	073 143	.074 .150	.080 .146		*0 <b>8</b> 8 *165	.097 .169	.095 .160	.098 .1 <b>60</b>	.075 .133
;	202	203	*196	195	198	.193	173	182	185	188	. 191	205	.198
	·243 ·062	·244 ·061	$^{ullet}_{ullet}258 \\ ^{ullet}_{ullet}059$	252 060	249	·243 ·061	·230	*226	214	·208	.190	182	•226
	002						.095	092	•093	.101	106	$\cdot \overline{115}$	·100
				Í.			.001	1 .071	.000	· .070	.063	.066	112
:	·126	146	·130	135	127 1048	118	.091	.071 .052	.069	.070 .053			
:	.050 .076	146 049 074	·050 ·079	·048 ·078	.048 .078	.051 .077	·051 ·071	*052 *071	.053 .070	.053 .073	·049 ·069	.051 .069	.050 .068
•	.050 .076 .054	146 049 074 051	.050 .079 .048	.048 .078 .046	.048 .078 .050	.051 .077 .049	.051 .071 .050	*052 *071 *051	.053 .070 .053	.053 .073 .051	·049 ·069 ·051	.051 .069 .051	*050 *068 *053
	.050 .076	146 049 074	·050 ·079	·048 ·078	.048 .078	.051 .077	.051 .071 .050 .070	*052 *071	.053 .070	.053 .073 .051 .076	·049 ·069	.051 .069 .051 .077	*050 *068 *053 *063
1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.050 .076 .054 .070 .100	146 1049 1074 1051 1066 108	.050 .079 .048 .067 .105	.048 .078 .046 .069 .102	.048 .078 .050 .069 .101	*051 *077 *049 *076 *096	.051 .071 .050 .070 	*052 *071 *051 *073 — *084	.053 .070 .053 .077 	.053 .073 .051 .076 	·049 ·069 ·051 ·071 — ·080	·051 ·069 ·051 ·077 ·075 }	*050 *068 *053 *063 *091
1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.050 .076 .054 .070 .100 	146 1049 1074 1051 1066 108 	.050 .079 .048 .067 .105 	.048 .078 .046 .069 .102 	.048 .078 .050 .069 .101  .125	.051 .077 .049 .076 .096 	.051 .071 .050 .070 	*052 *071 *051 *073 — *084 *117	.053 .070 .053 .077 	.053 .073 .051 .076  .082 .133	· 049 · 069 · 051 · 071 — · 080 · 133	*051 *069 *051 *077 	*050 *068 *053 *063 *091 *109
1 2 2	.050 .076 .054 .070 .100 	146 049 074 051 066 108  108 097 052	· 050 · 079 · 048 · 067 · 105 — · 114 · 101 · 051	· 048 · 078 · 046 · 069 · 102 — · 114 · 085 · 053	*048 *078 *050 *069 *101 — *125 *080 *049	'051 '077 '049 '076 '096  '117 '089 '051	·051 ·071 ·050 ·070 — ·090 ·117 ·089 ·050	*052 *071 *051 *073 — *084 *117 *081 *052	·053 ·070 ·053 ·077 — ·085 ·137 ·074 ·055	.053 .073 .051 .076 	· 049 · 069 · 051 · 071 — · 080 · 133 · 072 · 054	·051 ·069 ·051 ·077 ·075 } ·126 ·071 ·043	*050 *068 *053 *063 *091 *109 *117 *057
	.050 .076 .054 .070 .100 	146 049 074 051 066 108  108 097 052 090	· 050 · 079 · 048 · 067 · 105 — · 114 · 101 · 051 · 092	048 078 046 069 102  114 085 053 095	048 078 050 069 101  125 080 049 093	.051 .077 .049 .076 .096 	.051 .071 .050 .070 	*052 *071 *051 *073 — *084 *117 *081 *052 *090	.053 .070 .053 .077 	· 053 · 073 · 051 · 076 — · 082 · 133 · 073 · 052 · 099	· 049 · 069 · 051 · 071 — · 080 · 133 · 072 · 054 · 103	`051 `069 `051 `077 	*050 *068 *053 *063 *091 *109 *117 *057 *089
	.050 .076 .054 .070 .100 	146 049 074 051 066 108  108 097 052	· 050 · 079 · 048 · 067 · 105 — · 114 · 101 · 051	· 048 · 078 · 046 · 069 · 102 — · 114 · 085 · 053	*048 *078 *050 *069 *101 — *125 *080 *049	'051 '077 '049 '076 '096  '117 '089 '051	·051 ·071 ·050 ·070 — ·090 ·117 ·089 ·050	*052 *071 *051 *073 — *084 *117 *081 *052	·053 ·070 ·053 ·077 — ·085 ·137 ·074 ·055	.053 .073 .051 .076 	· 049 · 069 · 051 · 071 — · 080 · 133 · 072 · 054	·051 ·069 ·051 ·077 ·075 } ·126 ·071 ·043	*050 *068 *053 *063 *091 *109 *117 *057

Gött	of Mean	0	1	2	3	4	5	6	7	8	9	10	11
Tor	of Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\left( egin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{array} \right)$	83 95 99 50 62 57	85 94 100 48 62 64	82 92 98 47 60 57	84 75 97 52 54 59	82 76 97 48 58 56	90 74 97 50 52 60	90 72 97 48 70 60	89 75 97 51 59 55	93 78 98 48 69 56	88 84 89 51 70 58	92 80 81 60 75 59	91 77 76 57 77 63
I the Air.	8 9 10 11	82 80 85 73 72 71	86 79 85 73 77 65	80 82 87 70 70 71	80 71 81 68 73 75	75 75 84 72 74 64	75 77 71 71 70 65	75 66 79 67 69 61	69 70 70 74 74 60	72 65 74 65 79 63	76 68 83 65 65 63	72 68 88 63 59 59	88 67 92 70 56 60
EEPDITADY	12 13 14 15 16 17 18 19 20 21	81 69 82 66 74 85	80 60 82 68 76 81	75 72 84 63 77 84	72 82 78 73 85 79	73 72 81 90 82 76	58 73 81 89 83 76	63 76 74 89 78 74	53 84 77 78 80 74	58 79 77 88 88 75	56 85 76 90 88 74	58 84 62 92 87 74	93 83 78 80 88 74
	22 23 24 25 26 27 28	64 79 25 57 50 89	67 21 17 53 53 89	69 29 28 53 62 91	68 33 43 60 65 91	74 36 51 59 65 95	69 39 54 55 66 94	71 51 65 56 72 96	66 51 75 55 71 91	71 45 72 65 74 96	71 46 70 64 71 95	74 53 72 67 70 95	72 68 74 70 64 95
Iourl	ly Means	72	69	70	71	71	70	72	71	73	73	73	76
Lension of the Vapour.	FEBRUARY.  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19	In. 109 148 225 040 047 048 — 133 130 126 071 061 067 — 135 071 097	In.  115 147 227 040 045 052 135 120 126 072 070 062 130 054 095 085	In. 114 1161 2222 038 043 049 130 121 128 067 063 067 116 075 100 083 118	In. 120 152 217 044 042 056 137 117 127 069 072 078 106 107 1106 127	In. 128 180 216 044 050 059 140 128 140 083 085 076 110 060 132 152	In. 153 177 215 050 050 068 151 139 128 084 089 084 085 062 141 162 137	In.  162 174 217 052 072 074	In.  166 185 220 063 066 079 144 129 145 091 102 083 1702 132 155 139	In.  170 197 184 061 082 084 148 117 153 078 119 090 070 103 134 167	In.  164 205 162 069 084 091 158 121 163 078 088 090 169 116 139 170	In.  169 190 131 074 091 093 — 148 121 159 074 069 085 — 069 111 113 169	In. 161 183 110 0666 093 094 160 118 150 076 064 086 097 191 1144 154
	20 21 22 23 24 25 26 27 28	· 125 · 061 · 046 · 013 · 061 · 034 · 133	·117 ·064 ·012 ·008 ·054 ·040 ·133 —	·118	·104 	· 096 · 075 · 025 · 047 · 073 · 096 · 147	·095 ·078 ·030 ·060 ·075 ·102 ·152	· 097 	· 095 	· 094 080 · 045 · 091 · 096 · 111 · 168	· 094 · 082 · 047 · 089 · 094 · 103 · 165 ·	· 092 · 085 · 056 · 089 · 096 · 100 · 172 · -	· 091 · 083 · 068 · 089 · 095 · 091 · 176

12				HU	JMIDITY (	OF THE A	AR, AND	TENSION	OF THE	ATMOSPH	ERIC VAI	POUR.		
91 94 88 82 83 86 89 92 90 90 90 95 95 88 89 79 80 79 80 79 82 91 95 94 94 90 90 90 95 95 88 85 77 86 66 61 68 68 59 65 65 65 62 60 56 46 61 64 57 88 85 75 62 60 67 64 59 58 63 63 62 65 64 64 64 57 88 85 75 65 65 65 65 65 65 65 65 65 65 65 65 65	:	12	13	14	15	16	17	18	19	20	21	22	23	Daily and
79		6	7	8	9	10	11	12	13	14	15	16	17	
Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sect		79 75 58 75	80 66 57 62	79 61 69 60	82 68 67 59	91 68 64 59	95 59 59 64	94 65 58 65	94 65 63 67	90 62 62 61	90 60 65 62	95 56 64 64	98 49 64 64.	85 78 57 64
64 58 55 57 55 54 56 52 69 70 72 72 75 65 65 77 77 78 86 86 84 84 80 81 78 78 77 77 78 77 77 78 85 86 84 84 77 77 81 81 76 75 77 77 78 85 86 84 84 77 77 81 81 76 75 77 77 78 87 77 78 85 86 84 84 77 77 81 81 76 75 75 77 74 87 80 77 74 87 80 89 88 89 89 99 90 86 91 91 91 91 87 87 87 85 85 85 74 74 78 71 68 67 — — — — — — — — — — — — — — — — — —		90 71 91 78 57	90 68 85 77 56 63	70 84 74 55 64	93 77 74 76 67	80 77 72 65 66	91 81 80 80 60 68	95 80 81 82 51	89 78 80 80 58	89 77 77 80 63	95 74 79 79 63	96 73 78 76 67	86 85 70 73 82	74 81 73 66
To		77 72 85 89	58 86 73 84 88 74	55 86 66 84 89 78	84 72 77 89	55 80 68 77 90	54 81 72 81 86 67	56 78 74 81 91	52 78 78 76 91	69 77 73 75 91	70 77 73 77 87	72 80 70 74 87	75 77 70 87 85	78 74 80 85
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Hours of Me Göttinger Time.	an } 0	1	2	3	4	5	6	7	8	9	10	11
Hours of Me Toronto Time.	an )	19	20	21	22	23	0	1	2	3	4	5
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Air.	$egin{array}{c c} 7 & \cdot & \overline{} \\ 8 & \cdot & \overline{} \\ 9 & \cdot & \overline{} \\ 65 & \cdot & \overline{} \\ 10 & \cdot & 89 \\ 11 & \cdot & 85 \\ 2 & 92 \\ 3 & \cdot & 75 \\ \hline \end{array}$	66 67 88 87 90 79	67 70 88 82 88 77	67 79 78 68 78 68	70 77 75 81 56 51	74 77 65 71 57 50	67 78 60 93 56 53	76 77 54 76 50 58	74 74 59 71 51 45	68 78 61 68 64 62	59 81 77 61 68 60	63 81 82 59 72 63
Humidity of t	4     69       5     82       7     80       8     81       9     73       78	71 82 81 78 70 80	76 78 76 78 57 82	74 73 85 75 62 79	70 68 67 62 62 62 86	69 64 62 49 56 74	61 61 62 55 58 72	61 73 67 60 61 72	63 67 51 61 64 74	77 79 56 63 59 74	65 84 57 52 59 83	70 79 54 63 61 85
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2	$     \begin{array}{c c}       8 & - \\       9 & 77 \\       0 & 73 \\       60 & 60     \end{array} $	$   \begin{array}{c c}     \hline     72 \\     69 \\     74   \end{array} $	56 68 63	57 65 52	64 65 52	61 58 48	44 57 51	55 56 54	49 61 60	$\begin{array}{c} -\overline{} \\ 56 \\ 70 \\ 48 \end{array}$	56 63 47	57 73 60
ourly Mea	111s 78	78	76	72	69	65	66	66	64	65	67	69
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1	$ \begin{array}{c cccc} 1 & .077 \\ 2 & .058 \\ 3 & .055 \end{array} $	.096 .072 .115 .080 .057 .057	105 1074 133 1082 1066 1063	111 1088 135 1075 1072 1064	124 1093 145 1087 1059	149 1093 132 1081 1062 1060	141 1094 125 107 1064 1068	160 1090 118 1091 1058 1075	132 1087 129 1089 1063 1069	123 1093 136 136 1085 1092	107 1097 165 1073 1085 1085	·110 ·098 ·168 ·069 ·085 ·086
MARCH.	5   '060 6   '060 7   '073 8   '131 9   '099 0   '146	.066 .060 .079 .131 .101 .152	· 073 · 065 · 084 · 143 · 096 · 155	·076 ·067 ·112 ·146 ·108 ·159		1087 1069 1112 1114 1118 1163	·072 ·076 ·120 ·129 ·129 ·168	·078 ·082 ·127 ·141 ·132 ·168	-084 -089 -103 -150 -136 -171	-088 -098 -113 -154 -128 -172	·079 ·102 ·112 ·142 ·129 ·183	-083 -095 -103 -165 -126 -186
2 2 2 2 2 2 2	2   '122 3   '164 4   '121 5   '134 6   '100 7   '080	129 167 125 139 116 069	137 170 129 166 111 061	146 172 143 166 121	152 178 134 160 119	152 180 148 178 135	156 199 138 179 141	140 185 117 139 139	145 168 127 132 167 097	149 150 118 133 140	153 147 135 135 173 090	-157 -143 -128 -173 -164 -081
$\begin{bmatrix} 2\\2\\3\\3 \end{bmatrix}$	$\begin{array}{c c} 9 & 138 \\ \hline 0 & 094 \end{array}$	141 1091 1071	125 101 065	·143 ·096 ·053	.174 :097 :060	170 1092 1059	·127 ·089 ·068	151 083 075	·125 ·091 ·085	153 099 073	·122 ·088 ·071	·116 ·100 ·085
	ns '097	100	106	110	114	115	·119	·119	.119	120	120	•121

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Section   Color	12	13	14	15	16	17	18	19	20	21	22	23	
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118 113 109 108 107 104 112 106 103 103 101 101 110	In. 100 102 166 118 119 123 113 101 129 1077 1079 1079 1081 1069 124 139 127 186 159 133 135 201 150 1043 130 106 089	In	In. 103 103 145 105 118 131 109 103 067 063 068 077 064 108 100 111 188 159 145 131 149 143 058 128 105 066	In	· 100 · 102 · 119 · 100 · 122 · 149 -	106 1074 104 1091 121 146 1081 125 1093 1057 1066 1074 1060 115 113 1146 158 142 125 174 103 1084 103 1097 1059	110 1097 105 1087 123 200 1081 122 1087 1062 1067 109 1068 1067 121 115 118 125 166 103 157 186 1056	107 1090 105 1081 127 196 1080 113 1090 1061 1067 1093 1068 1070 1121 114 117 1155 130 128 151 1097 132 1090 1094 1054	· 107 · 088 · 105 · 085 · 129 · 176 · 077 · 120 · 084 · 058 · 065 · 062 · 073 · 123 · 113 · 1141 · 117 · 115 · 126 · 136 · 138 · 102 ·	101 1090 115 1077 131 170 1076 104 1079 1059 1067 1077 1062 1066 124 119 143 118 156 123 142 120 1090 135 1090 1082 1055	.087 .093 .103 .081 .129 .157 .074 .112 .078 .060 .064 .067 .126 .117 .143 .117 .165 .127 .140 .102 .090 .091 .082 .055	\[ \begin{array}{c} \cdot 083 \\ \cdot 083 \\ \cdot 083 \\ \cdot 083 \\ \cdot 083 \\ \cdot 065 \\ \cdot 065 \\ \cdot 128 \\ \cdot 140 \\ \cdot 100 \\ \cdot 167 \\ \cdot 139 \\ \cdot 093 \\ \cdot 051 \\ \end{array} \} \]	. 099 . 096 . 129 . 101 . 116 . 149 . 105 . 101 . 115 . 073 . 067 . 073 . 073 . 111 . 127 . 125 . 156 . 150 . 151 . 132 . 154 . 127 . 091 . 126 . 093 . 064

		HUMI	DITY OF	THE AIR,	AND TE	NSION OF	THE AT	MOSPHER	C VAPOU	JR.		
Göttingen Time.	0	1	2	3	4	5	6	7	8	9	10	11
Hours of Mean Toronto Time.	18	19	20	21	22	23	0	1	2	3	4	5
$\begin{bmatrix} 1^a \\ 2 \end{bmatrix}$		_		_				_		Aprilla	_	_
$\begin{vmatrix} 3 \\ 4 \end{vmatrix}$						_	_	_			_	_
5 6				_	_	_	_	_	_		_	=
$\begin{bmatrix} & 7 \\ 8 \\ 9 \end{bmatrix}$		_			_	_	_	_	_	_	_	_
10				_	_			_	=	_	_	_
$\begin{bmatrix} \mathbf{A} \\ \mathbf{A} \end{bmatrix}$		_		_	_	_	_	_		_	_	_
APRIL. 12 14 15 15 14 15 15 15 15 15 15 15 15 15 15 15 15 15	_		_	_	_	_	_	_	_	_	_	_
API 16		_	_	_			_	_	_	_	_	_
Humidity of the Air.  APRIL.  15 19 11 12 12 12 12 12 12 12 12 12 12 12 12	_							_	_	_	_	_
$\begin{bmatrix} 20 \\ 21 \\ 22 \end{bmatrix}$	_			_			_	_	_	_	_	
$\begin{bmatrix} 23 \\ 24 \end{bmatrix}$	_						_	_	_		_	_
25 26			=	_		_	_	_	_	_	=	_
27 28		_	_	=	_	_	_	_		_	_	_
29	_		_	_	_	_	_	_	-	_	_	_
Hourly Means		—		_				_				
	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
$\begin{vmatrix} 2 \\ 3 \end{vmatrix}$		_	_			_	_	_	_	_	_	_
$\begin{bmatrix} 4 \\ 5 \\ 6 \end{bmatrix}$	_	_	_	_	=	_	_	_	_	=		_ _
7 8	_ _ _		_	_	_		_		_	_	_	
9	_	_	_	_	_			_	_		_	_
node 11 12		_	_	_	_	_	_	_	_	_	_	_
Tension of the Vapour.  APRIL.  10 11 12 12 13 14 15 16 11 10 11 11 11 11 11 11 11 11 11 11 11			-	_	_	_			=	_	_	-
APRIL. 12 12 12 12 12 12 12 12 12 12 12 12 12			_		_							
Tensi 18 19			_	_		_			_	_		=
$\begin{vmatrix} 20 \\ 21 \end{vmatrix}$	_	_		_	_	_	-			_	=	_
- 22 23	_	_	_	_	_	_	-	_	-	_	=	
$egin{array}{c} 24 \ 25 \ 26 \ \end{array}$		_	_	-		_	_		_	_		
27   28			_	_			_	_			_	-
29 30		_	_	=	_	-	_	_	_	_	_	
Hourly Means				_		_		_		_		-

^a No reliable observations for this month.

		н	J <b>MIDITY</b>	OF THE A	AIR, AND	TENSION	OF THE	ATMOSPI	HERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly Means.
6	7	8	9	10	11	12	13	14	15	16	17	Means.
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			HUMI	DITY OF	THE AIR,	AND TE	NSION OF	THE AT	MOSPHER	IC VAPO	JR.		
ours of Me Göttinger Time.	n }	0	1	2	3	4	5	6	7	8	9	10	11
ours of Me Toronto Time.	ean }	18	19	20	21	22	23	0	1	2	3	4	5
	1 2 3 4	   85	_ _ _ 81	— — 75	 - 70	<del>-</del> - 69		— — 57		  58			- - 64
	5 6 7 8	84 95 98 74	72 82 67 73	62 69 67 64	66 63 58 52	58 54 58 54	54 50 54 52	54 46 59 52	47 48 52 52	45 55 55 46	44 52 55 42	46 55 49 42	46 53 54
	9 10 11 12 13 14	77 97 96 89 73	68 97 93 78 64	66 96 82 71 72	$\begin{array}{c}$	61 76 81 60 56	67 76 76 67 63	67 65 77 57 65	69 69 72 57 65	70 69 71 58 66	70 74 86 59 68	75 80 82 59 57	79 85 85 58 63
NA	15 16 17 18	89  84 83	$\begin{array}{c} 69 \\ -74 \\ 74 \end{array}$	$\frac{67}{72}$ $68$	$\frac{64}{68}$	62  58 66	63 	59  57 54	$\frac{61}{56}$	57 — 50 59	53 — 46 57	56 	59 
	19 20 21 22	80 73 88 95	67 69 81 94	63 58 85 93	62 54 79 90	72 48 82 84	69 50 84 77	65 50 72 76	62 54 69 80	62 54 69 79	58 54 69 80	60 56 66 80	65 63 66 84
	23 24 25 26 27 28 29	96 97 74 94 79 83	96 94 74 86 83 83	94 89 68 78 84 82	97 89 64 74 79 80	97 85 60 73 72 79	97 83 63 72 68 78	94 76 72 74 68 81	92 77 67 74 63 88	94 73 64 57 63 83	92 81 63 66 67 85	84 87 63 65 68 85	88 88 64 67 74 85
	30 31	95	95	96	95	95	96	97	98	97	96	96	96
ourly Me	eans	87	80	76	72	69	69	66	66	65	66	66	69
	1 2	In. 	In. —	In. —	In. —	I.	<u>In</u> .	In.	In. —	In. —	In. —	In. —	In.
	3    4    5    6    7	· 199 · 184 · 237 · 255 · 246	·231 ·224 ·258 ·240 ·255	·248 ·232 ·262 ·268 ·248	·246 ·263 ·226 ·261 ·241	·272 ·261 ·249 ·271 ·243	·277 ·265 ·255 ·262 ·227	·247 ·266 ·264 ·291 ·230	·229 ·251 ·269 ·276 ·239	·222 ·238 ·291 ·307 ·252	·222 ·230 ·259 ·263 ·247	·228 ·242 ·259 ·244 ·248	·24 ·21 ·27 ·27
1 1	9 10 11 12 13 14 15	·259 ·375 ·397 ·370 ·291 ·292	· 271 · 375 · 403 · 367 · 306 · 304	·290 ·389 ·420 ·360 ·361 ·355	·290 ·422 ·438 ·353 ·313 ·372	·309 ·432 ·461 ·313 ·282 ·362	·337 ·442 ·465 ·292 ·305 ·396	· 335 · 391 · 485 · 297 · 300 · 385	348 398 455 322 291 393	·372 ·397 ·423 ·328 ·297 ·381	·373 ·423 ·458 ·342 ·323 ·371	·401 ·400 ·446 ·346 ·292 ·361	·39 ·41 ·45 ·34 ·34 ·36
M.	16 17 18 19 20 21 22	·258 ·265 ·285 ·248 ·292 ·433	·286 ·298 ·282 ·263 ·294 ·485	·349 ·329 ·301 ·258 ·308 ·457	·363 ·405 ·325 ·279 ·318 ·479	·335 ·390 ·433 ·263 ·322 ·505	·364 ·362 ·389 ·273 ·348 ·527	·326 ·374 ·373 ·270 ·351 ·513	335 '401 '383 '302 '378 '476	· 303 · 373 · 388 · 305 · 385 · 506	· 284 · 370 · 358 · 298 · 394 · 512	·279 ·374 ·369 ·300 ·343 ·480	· 26 · 389 · 309 · 32 · 459
	23 24 25 26 27 28 29	·417 ·354 ·180 ·283 ·323 ·388	-443 ·382 ·191 ·215 ·339 ·361	·446 ·416 ·198 ·322 ·367 ·369	·447 ·470 ·205 ·312 ·360 ·446	·458 ·459 ·205 ·333 ·421 ·409	·474 ·469 ·239 ·346 ·454 ·418	·472 ·424 ·276 ·342 ·516 ·399	501 '470 '265 '322 '485 '423	·529 ·456 ·262 ·302 ·489 ·452	·509 ·452 ·282 ·317 ·464 ·503	·504 ·424 ·298 ·319 ·444 ·441	· 500 · 449 · 29 · 350 · 47 · 52
	30 31	•320	,310	311	306	$\frac{103}{290}$	·288	•283	.281	$\frac{102}{279}$	$\frac{-}{277}$	. 279	•279
ourly Me		•298	308	*328	*340	345	353	350	354	356	*355	*347	•362

	. <del></del>	ни	MIDITY	OF THE A	IR, AND	TENSION	OF THE .	ATMOSPH	ERIC VAI	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and
6	7	8	9	10	11	12	13	14	15	16	17	Monthly Means.
_		<u> </u>		_	_			_			_	_
67	69	$\frac{}{73}$	$\frac{-}{73}$			$\frac{-}{82}$			$\frac{-}{75}$	<del></del> 87	<del>-</del> 87	$\frac{}{71}$
67 61	63	68	72	81 77	87 79	86	65 94	66 92	89	87	89	69
51 48	67 44	74 43	77 59	76 63	$\frac{83}{54}$	81 50	$\begin{array}{c c} 82 \\ 51 \end{array}$	89 49	89 58	88 70	87 61	69 57
56	59	55	56	57 —	58	<u></u> 94	<u>-</u> 94	$\frac{-}{82}$	 85	<del></del> 81	$\frac{-}{74}$ }	63
85 91	94 93	95 92	96 96	96 97	97 90	98 86	97 94	97 97	96 97	97 97	98 96	82 87
87	85	85	89	88	87	91	91	86	89	87	90	85
58 68	70 74	73 69	76 75	80 81	77 79	79 92	81 91	$\begin{array}{c} 78 \\ 92 \end{array}$	80 89	79 90	$\frac{82}{89}$	$\begin{array}{c} 71 \\ 73 \end{array}$
56	80	87	83	84	85	63	<del></del> 61	$\frac{-}{64}$	$\frac{-}{73}$	$\frac{-}{79}$	$\left\{\begin{array}{c} -83 \end{array}\right\}$	69
43 61	43 55	47 65	54 73	$\begin{array}{c} 62 \\ 75 \end{array}$	71 76	55 76	57 79	$\frac{62}{85}$	78 86	80 82	80 89	61 69
73 64	56 76	57 78	53	53 83	62 88	58 88	63 90	64 96	$\frac{65}{97}$	69 97	68 92	$\frac{64}{71}$
69	79	90	81 93	95	96	97	90 97	96 96	$\frac{97}{95}$	95	96 96	84
85	89	91 —	92	95	95 —	93	97	97	$\overline{97}$	97	$\left\{\begin{array}{c} \overline{97} \end{array}\right\}$	89
92 88	94 92	92 96	96 93	95 91	96 81	$\begin{array}{c c} 94 \\ 75 \end{array}$	96 77	$\frac{96}{75}$	97 78	$\frac{98}{73}$	$\begin{array}{c} 98 \\ 73 \end{array}$	$\frac{94}{84}$
69 65	$\begin{array}{c} 81 \\ 72 \end{array}$	82 81	88 85	89 89	93 89	95 90	96 87	96 95	96 96	96 95	$\begin{array}{c} 95 \\ 94 \end{array}$	78 80
74 83	73 81	81 84	70 86	$\begin{array}{c c} 72 \\ 81 \end{array}$	69 82	76	77	87	83	88	92	75
_						66	67	85	86	91	95	82
$\frac{98}{71}$	$\frac{98}{74}$	96	97 80	99 82	98 82	99 82	$\frac{98}{83}$	99 84	97 86	98	99	$\frac{97}{76}$
In.	In.	In.	In.	In,	In.	In.	In.	In.	In.	In.	In.	In.
-								_				
•234	-227	-228	•216	.216		· <del>1</del> 91	180	.177	.179	•176	·166	
.243	225	•234	•218	208	197	.208	206	.199	192	183	·187 ·198	•224
$^{\circ}_{242}^{220}$	·237 ·197	·238 ·190	·236 ·213	·233 ·220	·234 ·212	·223 ·208	$^{\circ 217}_{\circ 217}$	$^{\cdot 222}_{\cdot 217}$	·215 ·267	*208 *326	.309	·238 ·251
·270	270	·255 —	·255 —	·260 —	*256 —	.318	-312	305	•323	•288	$\left\{ -\frac{7}{247} \right\}$	263
379 421	·409 ·383	·395 ·373	·386 ·389	375 391	·408 ·384	·412 ·379	·403 ·388	*388 *392	*362 *385	·385 ·399	·395 ·418	:361 :398
·442 ·338	·450 ·350	·450 ·340	·462 ·311	·445 ·307	·442 ·295	·416 ·291	·428 ·290	$^{\cdot 403}_{\cdot 278}$	:387 :280	$^{\circ}_{275}^{349}$	·377 ·273	·432 ·319
.309	.331	.290	.287	287	•279	•279	261	256	•240	245	236	•292
337	397	*364	. 322	321	318	234	•233	235	234	235	·230 } ·237	*326
$^{:251}_{:373}$	·235 ·280	·251 ·297	·264 ·298	·273 ·299	·276 ·288	·235 ·286	·236 ·289	$^{\circ}_{302}^{226}$	·242 ·305	·238 ·290	•297	·280 ·330
·442 ·297	·326 ·318	·291 ·314	·258 ·297	·256 ·290	·269 ·284	·253 ·276	$^{\circ}258 \\ ^{\circ}276$	·252 ·270	·244 ·268	·245 ·265	·248 ·268	*318 *283
244 337	·337 ·451	·376 ·450	*320 *454	·315 ·441	·357 ·423	·357	387	·364	.366	·377	*396	*344
.495	_			_		·374 ·363	·361 ·338	·361 ·332	364 331	·363 ·316	·396 } ·327	·442 ·432
447	·470 ·459	453 454	·426 ·408	·416 ·409	·387 ·257	•224	'211	.193	.190	175	169	.368
·294 ·321	·270 ·311	·263 ·309	·260 ·299	·251 ·298	·242 ·283	·233 ·280	$^{\circ}230 \\ ^{\circ}258$	236 262	$^{234}_{259}$	·209 ·277	·212 ·288	·243 ·301
·477 ·443	·411 ·389	·419 ·382	.403 .383	·415 ·357	·385 ·363	·400	·402	·398	·397 —	·409 —	·410 — \	·419 ·382
288	•288	•286	•297	.305	•311	·243 ·318	·240 ·313	·288 316	·300 ·314	$^{\circ}_{322}$	$\begin{bmatrix} -331 \\ 318 \end{bmatrix}$	·299
.339	*334	*329	.319	.316	*306	•292	*289	286	•287	•286	•289	*324

ours of	f Mean i				· · · · · · · · · · · · · · · · · · ·			THE AT		1	<u> </u>	3.0	
Gottin Tin	ngen ne.	0	1	2	3	4	5	6	7	8	9	10	11
lours o Tord Ti		18	19	20	21	22	23	0	1	2	3	4	5
	$\left( \begin{array}{c c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{array} \right)$	97 87 96 90 85	97 85 91 89 79	100 82 89 83 75	96 76 88 79 73	96 72 86 74 67	91 72 83 66 63	87 69 83 52 60	85 82 84 66 75	85 81 84 61 76	91 81 83 61 73	86 79 82 65 52	92 77 84 65 54
Air.	7 8 9 10 11 12	80 81 97 92 95 84	78 76 96 91 92 75	69 75 91 91 88 83	69 74 87 96 90 80	66 75 85 96 83 72	63 79 85 94 83 77	62 81 84 94 91 70	60 78 81 94 85 67	58 77 80 95 88 67	60 78 79 96 94 67	66 79 74 96 95 67	61 82 75 96 77 67
JUNE.	18	91 85 74 89 77 96	89 82 72 72 72 72 95	79 79 65 71 72 96	90 75 64 79 70 97	84 75 62 75 70 97	79 74 64 75 65 95	78 74 64 75 67 96	89 73 65 77 77 90	83 73 64 66 67 82	74 67 66 64 65 84	69 64 63 54 68 78	68 63 65 52 82 78
A contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of	20 21 22 23 24 25 26	84 95 87 89 80 89	82 94 82 82 82 80 78	82 94 74 81 84 77	85 87 77 78 79 77	81 87 83 76 71 77	79 86 79 80 62 75	76 84 81 72 66 78	76 81 79 62 61 75	89 78 77 64 61 78	88 87 72 70 63 74	83 89 72 66 65 77	79 83 77 64 62 75
	27 28 29 30	82 72 72	78 71 71	67 67 67	59 66 63	59 63 64	61 60 64	63 56 65	70 58 69	46 57 67	43 76 69	46 74 69	59 77 70
lourly	Means	86	83	80	79	77	75	74	75	73	74	72	72
	$\begin{pmatrix} 1\\2\\3\\4\\5\\6\end{pmatrix}$	In.	In. '297 '336 '395 '391 '232	In. '332 '340 '399 '403 '359	In. '378 '334 '396 '370 '262	In. '415 '359 '398 '358 '273	In. '475 '369 '415 '354 '286	In.	In. • 444 • 445 • 450 • 331 • 370	In. '438 '407 '404 '298 '381	In. '402 '407 '410 '286 '394	In. '411 '399 '391 '274 '299	In. •432 •409 •371 •263 •306
pour.	6 7 8 9 10 11 12 13	·294 ·346 ·432 ·521 ·455 ·288	·332 ·326 ·462 ·522 ·489 ·293	·376 ·324 ·498 ·540 ·526 ·385	·411 ·337 ·542 ·553 ·568 ·402	· 394 · 379 · 543 · 540 · 504 · 376	·403 ·383 ·559 ·529 ·533 ·398	·412 ·382 ·573 ·541 ·505 ·382	·425 ·379 ·630 ·537 ·510 ·399	·419 ·406 ·649 ·572 ·462 ·404	·427 ·424 ·639 ·534 ·471 ·408	·401 ·408 ·632 ·538 ·459 ·427	· 355 · 390 · 579 · 519 · 349 · 421
Tension of the Vapour.	14 15 16 17 18 19	·399 ·206 ·232 ·296 ·301 ·416	·375 ·211 ·247 ·282 ·340 ·418	·300 ·214 ·246 ·327 ·340 ·450	·326 ·217 ·256 ·393 ·367 ·489	· 296 · 232 · 262 · 382 · 371 · 527	·277 ·241 ·275 ·387 ·388 ·517	·258 ·250 ·277 ·408 ·410 ·508	·259 ·275 ·275 ·275 ·409 ·472 ·498	·239 ·300 ·269 ·378 ·396 ·426	·248 ·313 ·290 ·389 ·378 ·451	·234 ·309 ·288 ·364 ·377 ·477	· 234 · 301 · 293 · 340 · 408 · 505
1	20 21 22 23 24 25 26 27	375 378 400 409 409 509		·461 ·377 ·439 ·512 ·479 ·605	·491 ·435 ·507 ·537 ·504 ·644	·488 ·470 ·528 ·570 ·483 ·655	·481 ·530 ·557 ·626 ·455 ·697	·492 ·538 ·561 ·548 ·495 ·677	·488 ·545 ·559 ·478 ·496 ·661	*442 *529 *543 *505 *497 *639	·490 ·486 ·541 ·568 ·535 ·648	.520 .460 .529 .536 .513	· 508 · 470 · 502 · 535 · 419 · 626
	28 29 30	·444 ·355 ·350	·437 ·371 ·398	*377 *366 *455	·376 ·393 ·464	·391 ·401 ·474	·397 ·414 •453	·452 ·404 ·495	·549 ·421 ·521	·375 ·450 ·516	360 506 502	·380 ·505 ·500	·426 ·516 ·485
lourl	y Means	·361	*380	•401	421	•426	*438	•441	·455	•436	•443	`433	$-\overline{\cdot_{422}}$

		HU	MIDITY (	OF THE A	AIR, AND	TENSION	OF THE	ATMOSPII	ERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
89 78 84 64 56	94 81 82 64 59	95 86 86 64 67	92 89 89 77 72	87 90 92 76 84	86 96 95 77 89	88 95 96 81	88 98 93 83	89 96 96 80	90 96 94 84	90 97 93 81	88 95 92 82	91 85 89 74 74
65 83 74 96 74 70	70 80 75 96 81 73	76 84 82 97 85 80	76 78 86 97 81 81	77 82 88 98 82 81	81 86 90 97 82 82	71 83 93 89 98 82 —	73 83 92 91 96 79 	91 84 96 93 97 80 	95 87 96 92 97 81 —	98 89 97 93 98 80 —	92 89 96 93 97 85 — }	73 83 86 96 85
73 65 70 53 87 78	74 67 70 70 93 87	76 73 70 75 96 87	71 77 85 82 97 93	72 80 91 86 96 94	71 84 89 84 96 95	72 78 88 87 96 —	72 77 87 89 96	71 78 88 85 96 —	71 83 88 86 96 —	76 82 90 76 96 —	$ \begin{array}{c c} 30 \\ 81 \\ 76 \\ 93 \\ 77 \\ 96 \\ \hline 93 \end{array} $	77 75 75 75 83 90
79 83 77 64 71 78	88 86 80 74 81 84	92 91 89 76 92 87	90 91 92 78 78 84	94 89 92 78 80 92	92 91 92 81 91 88	94 94 87 92 84 91 —	94 93 87 80 89 91 —	94 88 84 90 91 —	88 96 90 81 87 92 — 66	95 90 91 90 92 —	94 90 92 86 92 — }	87 88 83 78 78
62 53 70	64 59 77	55 60 73	57 58 80	55 66 79	59 66 71	61 64 73	62 71 76	62 65 82	65 72 83	86 72 81	74 72 75	62 66 72
73	77	81	82	84	85	85	85	86	87	88	87	80
In. '410 '398 '378 '262 '293	In. '416 '368 '360 '249 '303	In.	In. '377 '352 '371 '250 '282	In.	In. '344 '327 '366 '230 '270	In. '342 '316 '379 '224	In. '324 '306 '372 '221	In. '322 '289 '388 '192 '278	In. '316 '288 '386 '191	In. '336 '278 '377 '180 '265	In. '337 '282 '373 '178	In. '378 '352 '387 '276 '292
331 380 580 515 312 425	327 370 592 495 303 390	*339 *376 *569 *503 *316 *357	*335 *364 *519 *479 *295 *354	327 386 537 471 296 350	349 387 565 468 301 340	343 '400 '547 '496 '298 — '359	343 398 518 506 289 — 359	334 '421 '511 '496 '288 — '356	347 390 505 496 288  354	*354 *386 *488 *458 *264  *358	360 384 484 440 271 	*364 *380 *548 *511 *390
241 302 302 326 410 497	237 285 303 375 425 406	223 277 303 316 444 381	196 267 273 299 461 368	189 262 278 280 454 351	184 265 270 270 270 462 349	186 255 259 263 461	183 251 256 257 430	182 256 251 238 431	182 251 249 238 433	187 248 236 235 429	196 229 250 256 429	*243 *259 *268 *321 *409
490 467 506 519 477 581	·477 ·442 ·475 ·515 ·463 ·568	·426 ·421 ·463 ·501 ·481 ·570	·406 ·407 ·453 ·400 ·412 ·576	·413 ·402 ·439 ·376 ·412 ·568	·406 ·394 ·440 ·375 ·463 ·520	377 397 381 397 368 478	359 369 381 346 365 494	*357 *451 *377 *333 *360 *486	342 334 378 318 355 493	*347 *331 *326 *339 *393 *481	*349 ( *359 *346 *344 *369 *455	·438 ·431 ·456 ·467 ·473
.426 .383 .466	·410 ·386 ·449	·338 ·344 ·384	344 311 374	*318 *335 *352	336 327 321	.613 .333 .298 .313	*539 *326 *306 *298 *	*380 *317 *293 *300	*383 *323 *310 *294	·370 ·373 ·305 ·287	·414 } ·340 ·312 ·284	*567 *381 *376 *406
'411	*400	*384	·366	361	.359	*359	*348	`342	335	332	*333	*391

ours of Mean )	0	1	2	3	4	5	6	7	8	9	10	11
Ours of Mean Toronto	18	19	20	21	22	23	0	1	2	3	4	5
$\begin{array}{c c} \text{Time.} &  &  &  &  \\ \hline & & & & \\ \hline & & & & \\ \hline & & & & \\ \hline & & & &$	63 84 83	65 74 76	62 63 77	61 63 68	69 64 64	65 66 61	66 63 53	64 61 56	57 61 58	53 60 57	53 59 59	56 61 67
4 5 6 7 8 9 10	90 76 88 89 88 79	76 86 83 87 81 85	68 87 81 77 78 79	70 82 71 77 75 76	64 79 70 68 72 76	$ \begin{array}{c c} \hline 63 \\ 77 \\ 74 \\ 71 \\ 71 \\ 76 \\ \end{array} $	65 72 69 72 68 70	61 70 69 72 68 66	60 85 67 76 71 60	62 83 68 74 69 60	55 86 65 72 69 59	79 77 74 74 67 64
11   12   13   14   15   16   17   18   19   20	89 72 73 91 88 90	82 74 64 87 80 86	81 73 58 80 75 80	82 74 50 72 69 76	81 63 47 72 67 69	79 60 49 69 64 68	75 60 47 69 59 67	85 58 52 68 61 65	81 62 54 65 74 68	74 63 51 64 60 89	65 60 57 70 66 89	72 63 57 72 70 87
19 20 21 22 23 24 25	92 90 98 92 87 92	84 84 97 74 84 89	84 78 94 75 80 87	82 81 92 64 76 83	77 81 86 58 75 84	70 82 79 55 73 87	69 81 75 55 71 89	69 89 79 58 66 90	71 86 75 48 67 84	70 81 76 50 65 85	66 86 71 50 66 82	66 82 76 50 69 80
26 26 27 28 29 30 31 Aug. 1	91 78 85 88 95 95	92 72 77 84 91 90	86 66 64 79 88 79	76 64 64 75 89 79	81 66 73 72 79 76	76 64 66 70 81 76	75 66 63 69 78 71	78 69 67 69 90 76	56 64 62 74 92 72	56 64 61 81 87 71	54 62 62 74 83 65	48 67 58 76 82 63
ourly Means	86	82	77	74	72	70	68	69	69	68	67	69
$\begin{pmatrix} 1\\2\\3 \end{pmatrix}$	In. •290 •383 •337	In. *340 *427 *499	In. '373 '449 '614	In. *431 *555 *598	In. *540 *546 *613	In. •510 •544 •605	In. • 540 • 555 • 561	In. 537 576 588	In. :511 :570 :608	In. •454 •574 •590	In. •452 •579 •613	In. •474 •588 •657
4 5 6 7 8 9 10	·489 ·493 ·532 ·585 ·575 ·546	*495 *564 *546 *640 *625 *597	·519 ·562 ·562 ·681 ·676 ·598	·642 ·571 ·620 ·742 ·696 ·618	·633 ·382 ·631 ·669 ·683 ·634	·614 ·614 ·693 ·725 ·738 ·664	·646 ·620 ·683 ·725 ·693 ·626	·632 ·665 ·683 ·726 ·698 ·642	·628 ·762 ·689 ·700 ·695 ·630	·647 ·734 ·700 ·687 ·677 ·606	*519 *820 *668 *664 *629 *594	· 568 · 652 · 720 · 687 · 600 · 580
H 11 12 13 14 15 16 17 18 19 20 20 21	·607 ·554 ·340 ·383 ·535 ·638	682 636 343 420 579 641	.708 .645 .352 .457 .611 .659	·730 ·719 ·347 ·486 ·622 ·707	748 ·676 ·342 ·525 ·657 ·741	·774 ·657 ·384 ·545 ·657 ·745	734 662 377 584 636 772	·832 ·643 ·428 ·598 ·670 ·729	*841 *611 *419 *580 *667 *776	786 576 386 585 641 749	710 548 413 591 657 792	*701 *514 *411 *509 *639 *805
19 20 21 22 23 24 25	·693 ·665 ·671 ·649 ·352 ·443	762 718 733 566 417 496	*829 *712 *702 *569 *482 *557	*814 *750 *724 *501 *526 *569	·836 ·788 ·762 ·484 ·525 ·548	*843 *745 *774 *473 *529 *566	· 856 · 785 · 743 · 502 · 522 · 570	*802 *719 *765 *544 *492 *661	756 796 781 462 477 567	*812 *818 *735 *473 *510 *597	· 791 · 758 · 713 · 469 · 544 · 568	·776 ·732 ·707 ·469 ·546 ·538
26 27	·421 ·287 ·309 ·411	*407 *303 *347 *455	375 314 353 469	*331 *342 *376 *483	*345 *354 *439 *487	·335 ·359 ·394 ·503 ·471	*332 *381 *363 *502 *469	384 389 411 492 491	303 357 375 375 511 526	302 357 368 577 529	*303 *371 *379 *509 *515	·271 ·399 ·349 ·505
28 29 30 31 Aug. 1	·414 ·354	.452 .460	.454 .470	.456 .495	·498 ·509	.210	•523	·490	478	472	·469	•409

		н	UMIDITY	OF THE	AIR, AND	TENSION	OF THE	ATMOSPI	HERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
54 69	63 72	75 76	72 77	71 76	67 80	63 86	66 86	66 91	72 91	81 89	83 90	65 73
68	73	86	83	83	81	81	82	82	88	89	$-\frac{1}{92}$ }	74
80	81	$\frac{-}{92}$	89	89	76	77	82	75	77	75	75	74 85
84 71	85 77	87 88	92 90	94 92	9 <del>1</del> 89	93 90	$\begin{array}{c} 94 \\ 91 \end{array}$	94 93	91 94	88 93	87 93	81
72	84	85	84	78	83	81 77	81 79	81 83	84 85	84 84	84 82	79 76
71 69	75 70	$\begin{array}{c} 78 \\ 73 \end{array}$	75 74	78 74	77 75						- 7	7 <b>7</b>
_	$\frac{-}{74}$	<del></del> 85	90	89	89	96 87	94 88	96 92	96 92	$\frac{94}{84}$	96 } 72	82
74 64	64	67	72	75	78	79	78	74	73	74	74	69
67 81	76 85	80 87	84 88	80 88	80 89	86 89	87 94	86 92	88 90	$\frac{92}{92}$	92 92	69 81
70	80	81	87	89	90	89	92	92	92	94	93	78
93	95	94	96	96	97	92	89	$\frac{-}{92}$	96	96	$\left\{\begin{array}{c} \overline{97} \end{array}\right\}$	86
66	66	72	75	81	86	89	92	92 96	92 97	$\frac{92}{97}$	92 97	79 90
92 77	94 80	98 83	97 8 <b>5</b>	97 90	97 94	97 90	98 94	96 96	97	89	94	86
51	58	64	80	77	79 92	90 92	90 92	$\frac{91}{92}$	91 91	94 94	95 94	70 81
66 81	74 83	88 87	91 87	89 87	88 88	_	-				— 1 II	87
		$\frac{-}{76}$	$\frac{-}{75}$	84	84	97 84	93 82	$\frac{92}{80}$	90 83	87 88	84 } 69	75
55 69	<b>5</b> 9 77	86	90	91	90	91	91	92	94	100	93	78
55 75	69 74	$\begin{array}{c} 77 \\ 73 \end{array}$	84 86	86 94	90 95	90 96	$\frac{92}{92}$	92 90	93 95	95 95	96 96	$\begin{array}{c} 76 \\ 82 \end{array}$
85	91	94	95	95	93	93	96	100	97	95	95	90
78	75 —	82	92	93	94	86	86	87	90	92	94 }	82
72	76	82	85	86	86	87	88	88	90	90	89	79
In. '444	In. •443	In. •425	In. 376	In. •349	In. 334	In. 319	In. 319	In. *333	In. •341	In. 351	In. 338	In. •409
617	•528	·488	*456	·434 ·421	*335 *409	'418	'410	'410	*405	377	382	·484
634	·401	•552 —	·460			415	•409	•400	.408	:407	.415 }	·509
.584 .643	.580 .622	.611 .562	.588 .553	·573 ·540	.518 .535	·529 ·545	·520 ·519	·494 ·501	·499 ·509	·487 ·489	·483 ·493	·562 ·581
647	638	.602	•573	•564	*551	• 567	•549	•511	.508	•524	•524	.604 .634
657 618	.707 .614	$^{\circ}_{582}^{642}$	· 595 · 570	561 563	576 541	.568 .549	·553 ·546	*554 *575	·533 ·577	·521 ·563	·527 ·561	619
· <b>599</b>	557	.577	.570	.570	561				.582	•575	$\left\{ -\frac{1}{574} \right\}$	•596
746	713	.682	649	•609	•607	·620 ·606	.600 .597	·582 ·593	*528	.512	•523	·676
487	440	.421	<b>.</b> 416	408	*405 *343	338 · 338	:386 :337	$^{:356}_{:329}$	$^{:342}_{:327}$	*330 *355	325 348	$\begin{array}{c} :507 \\ :374 \end{array}$
.464 .589	$^{:}442 \\ ^{:}589$	.409 .585	389 588	·356 ·593	•559	•556	•485	•482	•463	•460	'456	<b>·5</b> 28
•593	<b>.</b> 669	603	.600	603	.597 .757	• 599	.611	.610	·578 —	·579 —	•601	617
*851 —	·863	·769	.751 —	-		:658	599	636	·620	·610	·615 }	.718 .713
.747 .705	.644 .703	.610 .692	·592 ·697	.602 .697	·628 ·687	642	.616 .673	·618 ·647	·622 ·671	·621 ·648	·612 ·649	.714
*661	<b>.</b> 628	.608	573	587	.579	• 579	•594	• 590	617	.606 .319	.635 .321	.669 .446
.440 .525	`428 `494	.417 .441	.443 .421	·393 ·408	·375 ·400	·377 ·401	$352 \\ 401$	$^{\circ}346 \\ ^{\circ}392$	·333 ·378	319	383	·456
527	522	573	.233	544	• 553	•588	•629	.633	$\cdot \frac{-}{593}$	•460	$\cdot \frac{1}{415}$	$\cdot 552$
280	· <del>2</del> 81	317	$\cdot \frac{-}{292}$	287	•269	267	<b>·26</b> 3	•253	•256	•248	.220	306
401	<b>.</b> 390	*358	*343	*336	·308 ·345	*303 *345	·307 ·359	$^{\circ}294 \\ ^{\circ}359$	·297 ·345	$\substack{ \cdot 298 \\ \cdot 332}$	:281 :326	·339 ·358
305 498	364 479	*359 *465	*344 *493	341 525	•513	•498	•455	•439	415	407	*403	•479
520	•506	.475	· 474 · 431	·447 ·410	·424 ·394	·413	.378	*394	*348	322	321	`450 `428
'447	·378 —	'434 —		-		•377	372	.364	*346	*341	344	428
						1						

ours of Mear Göttingen	'} o	1	2	3	4	5	6	7	8	9	10	11
Time.  ours of Mean Toronto Time.	18	19	20	21	22	23	0	1	2	3	4	5
	8   87 4   84 5   84 6   87 7   79	89 78 77 77 79 77	74 68 78 77 66 70	78 69 75 80 66 66	72 65 68 77 67 71	70 63 68 69 67 70	68 65 66 71 68 68	70 63 64 71 68 69	69 61 63 65 61 70	65 58 64 61 69 67	73 64 60 66 64 77	69 64 60 66 71 76
10 11 12 13 14	96 97 1 98 2 97 3 96 4 97	96 97 97 94 93 97	97 97 92 97 67 92	94 90 96 88 65 87	93 86 94 84 82 84	89 82 98 80 83 85	86 79 91 78 73 83	84 80 88 82 73 81	83 78 88 79 74 86	82 77 92 79 78 82	81 81 88 75 79 84	80 82 84 74 81 81
AUGUST. 15 25 25 25 25 25 25 25 25 25 25 25 25 25	96 7 97 8 85 9 91 0 87 1 74	91 94 89 84 81 70	85 93 79 76 83 71	76 90 71 61 66 64	67 89 65 58 63 52	75 92 61 53 73 49	75 96 56 51 64 47	74 91 60 48 57 46	67 82 53 50 58 45	65 92 55 49 69 45	71 91 55 48 69 41	69 91 60 45 84 47
2: 2: 2: 2: 2: 2: 2: 2: 2:	83 83 4 88 5 79 6 94 7 91 8 93	78 86 82 92 88 87	72 81 78 89 78 82	69 82 75 83 78 84	70 73 74 83 69 78	74 67 75 85 65 67	75 69 67 80 61 68	77 66 65 79 60 61	78 62 64 75 69 62	84 59 60 75 76 62	77 59 61 71 74 67	77 61 64 77 74 70
30	96	92 91	88 85	83 71	$\frac{-}{76}$	75 67	69 67	70 64	70 63	72 68	$\frac{\overline{72}}{74}$	83 75
ourly Mea	ns 90	87	81	77	74	73	71	70	68	69	70	72
	1 612 2 449 3 549	In.  '439 '342 '472 '472 '490 '387	In447 -421 -551 -532 -494 -408565 -638 -650 -561 -622	In. '491 '484 '534 '585 '536 '425 '587 '643 '602	In498 -465 -500 -574 -618 -481592 -719 -642 -674 -669	In512 -455 -532 -536 -613 -544607 -716 -698 -668 -684	In.	In. •539 •462 •519 •559 •605 •540 — •663 •709 •698 •692	In. '502 '447 '548 '541 '568 '519	In. •512 •447 •558 •490 •615 •498 — •675 •594 •664	In.	In. 4800 521 527 507 508 5200 — 641 673 601 649
AUGUST.	44 '610 55 -634 7 '579 88 '376 281 358 1 '315	·663 	·689 ·683 ·745 ·390 ·326 ·437 ·359	·712 ·671 ·748 ·377 ·288 ·408 ·372	·762 ·625 ·763 ·365 ·302 ·426 ·331	·759 ·759 ·707 ·349 ·293 ·467 ·331	.770 .747 .741 .347 .286 .463 .335	·790 -745 ·670 ·377 ·278 ·413 ·341	·743 -709 ·669 ·346 ·289 ·421 ·353	.783 .—. .705 .682 .364 .305 .351 .358	·735 — ·650 ·656 ·329 ·292 ·478 ·330	·729 ·749 ·674 ·312 ·275 ·435 ·389
2: 2: 2: 2: 2: 2: 2: 2: 2:	332 4 348 5 322 6 377 7 397 8 381	382 395 377 438 399 358		·412 ·485 ·511 ·539 ·392 ·483	· 392 · 471 · 527 · 560 · 387 · 489	·433 ·468 ·528 ·644 ·373 ·439	·466 ·499 ·479 ·590 ·370 ·452	·498 ·468 ·462 ·635 ·374 ·411	*510 *449 *465 *607 *416 *429	.557 :428 :444 :622 :434 :413	·510 ·427 ·426 ·591 ·435 ·446	*50° *442 *432 *558 *45° *473
30	463	*543 *375	*546 *382	.580 .324	·569 ·348	·572 ·333	.541 .346	*557 *346	•544 •340	·523 ·381	·49 <b>0</b> ·394	·529

		HU	MIDITY (	OF THE A	IR, AND	TENSION	OF THE A	ATMOSPH	ERIC VAL	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8.	9	10	11	12	13	14	15	16	17	Means.
63 62 64 73 90 82	74 68 73 78 91 86	82 82 86 81 . 83 83	80 86 87 83 83 82	80 89 87 79 82 83	76 91 87 81 82 84	77 84 88 84 90 —	79 88 92 87 91 	81 91 91 91 95	85 92 92 92 98 —	90 93 93 93 97 —	94 91 93 94 96 —————————————————————————————————	77 76 78 78 80 81
85 89 83 81 93 79	85 90 90 88 95 81	90 89 92 91 96 89	90 93 96 94 94 93	92 94 95 94 92 93	94 96 96 96 93 97	95 98 97 96 93 94 —	95 98 96 93 92 —	95 98 97 97 93 95 —	96 96 96 95 95 	96 97 96 95 97 —	96 98 96 96 97 ——————————————————————————————	91 90 93 88 86 90
72 95 64 54 89 50	78 93 69 72 88 64	85 93 73 76 84 76	90 93 78 64 83 77	93 85 78 73 88 77	94 88 84 72 91 81	97 86 88 75 91 74	95 92 84 78 91 — 80	96 92 86 84 90 — 81	96 92 93 88 87 — 85	$   \begin{array}{r}     97 \\     83 \\     95 \\     85 \\     \hline     83 \\     \hline     \hline     87   \end{array} $	97 84 98 88 78 	83 91 74 68 79 65
76 67 67 79 75 75	88 80 77 83 81 85	91 78 84 84 91 87	91 79 87 84 92 93	94 85 89 77 93 95	93 86 92 85 95 94	93 82 92 91 90 —	93 85 87 94 90 — 95	88 81 89 96 92 — 95	90 82 91 91 93 —	94 81 91 90 94 —	$\left\{ \begin{array}{c} 95\\ 84\\ 91\\ 86\\ 92\\ \hline -7 \end{array} \right\}$	83 76 78 84 82 83
93 81	96 85	97 91	89 92	91 90	88 94	85 95	85 89	84 94	95 92	94 88	95 89	85 82
76	82	86	87	87	89	89	90	91	92	92	92	82
In478 -501 -541 -502 -520 -533 -659 -644 -608 -623 -721 -665 -744 -651 -314 -318 -453 -375 -479 -464 -423	In.  '485 '477 '549 '502 '538 '509	In.	In.  '415  '404  '437  '470  '523  '445  -607  '634  '521  '603  -646  '630  -7  '301  '277  '393  '364  -402  '364  '402	In.	In. '356 '381 '418 '456 '520 '448 '600 '626 '493 '604 '596 '617 '591 '472 '294 '312 '389 '351 '368 '365	In.  350 366 416 474 574 517 585 626 480 582 588 607 589 425 295 329 393 303 353 354 398	In.  313 363 3411 494 559 525 556 592 476 578 611 589 567 416 278 322 375 316 355	In.  '320  '357  '402  '504  '551	In.  '332  '356  '408  '505  '515   '517  '530  '578  '480  '524  '614   '561  '563  '408  '307  '317  '349   '315  '346  '339  '366	In.  '316  '346  '406  '505  '468   '515  '539  '597  '450  '528  '605   '556  '574  '400  '312  '317  '326   '317  '332  '318  '367	In. '318 '346 '420 '489 '441	In.
*546 *459 *459  *538 *392	'418 '518 '395 '433 — '519 '358	*506 *436 *420 — *483 *340	·402 ·508 ·408 ·417 — ·462 ·319	·402 ·491 ·389 ·421 — ·450 ·306	376 376 401 413 315	*526 *357  *463 *385 *308	369 525 347  441 376 287	*545 *322  *417 *359 *283	·486 ·301 — ·408 ·337 ·306	·463 ·309 — ·415 ·328 ·300	389 315 -417 }	·529 ·384 ·423 ·476 ·339
•523	•505	•484	•467	·456	*450	•448	*438	•433	•426	•420	*415	•484

ours of I Götting Time	Mean )	0	1	2	3	4	5	6	7	8	9	10	11
	Mean }	18	19	20	21	22	23	0	1	2	3	4	5
	$\left(\begin{array}{c}1\\2\\3\\4\end{array}\right)$	89 97 96 86	87 93 97 85	88 90 95 85	82 84 94 87	79 80 84 86	77 77 81 86	79 72 81 88	81 72 70 91	67 70 77 88	66 73 78 88	69 74 83 87	74 80 78 88
1.	5 6 7 8 9 10 11	93 96 89 94 89 97	91 91 89 92 95 92	84 84 87 90 76 91	82 75 86 79 77 83	84 72 81 71 72 82	86 72 78 65 70 76	86 76 78 63 71 74	89 80 74 72 64 74	77 83 80 73 67 71	75 82 81 74 69 62	74 83 82 74 73 63	75 85 92 77 74 67
SEPTEMBER.	12 13 14 15 16 17 18	89 88 93 97 93 92	85 86 88 95 89 94	84 82 79 85 85 93	77 82 68 78 80 93	$     \begin{array}{r}                                     $	72 78 62 74 78 92	73 76 60 75 78 92	74 77 57 76 77 92	69 64 71 78 76 94	$     \begin{array}{r}                                     $	73 72 69 76 73 84	77 62 72 76 73 85
1	20 21 22 23 24 25	91 94 95 98 89 87	91 93 95 97 90 89	91 86 88 89 90	89 82 74 87 89 86	87 76 83 83 90 85	90 79 82 78 89 84	90 73 81 79 86 82	91 67 75 83 87 77	91 67 72 78 87 85	91 64 70 74 90 87	87 67 75 77 90 89	92 71 81 81 92 90
	26 27 28 29 30	96 91 92 90	95 93 88 88	95 86 80 85	96 74 75 81	96 66 78 72	$     \begin{array}{r}             \hline             95 \\             62 \\             71 \\             68 \\     \end{array} $	$     \begin{array}{r}                                     $	94 80 79 66	84 64 76 69	$ \begin{array}{c c} \hline 81 \\ 63 \\ 91 \\ 72 \end{array} $	81 68 90 72	84 76 89 79
ourly	Means	92	91	87	82	80	78	77	78	76	76	77	80
	$\begin{pmatrix} 1\\2\\3\\4 \end{pmatrix}$	In. '334 '336 '442 '378	In. •342 •398 •534 •377	In. *392 *468 *552 *374	In. '400 '500 '550 '290	In. •435 •524 •605 •592	In. •445 •527 •644 •398	In.  *454  *305  *645  *402	In. '467 '499 '562 '416	In. '419 '532 '637 '412	In. '411 '554 '619 '420	In. •424 •568 •597 •417	In. •45 •56 •47 •42
mr.	5 6 7 8 9 10	· 321 · 376 · 538 · 337 · 267 · 308	343 453 556 330 334 351	371 '480 '581 '334 '329 '398	·449 ·449 ·597 ·307 ·393 ·446	·474 ·437 ·642 ·307 ·387 ·431	·488 ·436 ·642 ·295 ·381 ·430	·485 ·446 ·652 ·290 ·406 ·401	507 475 617 369 361 405	·476 ·466 ·651 ·376 ·389 ·384	·489 ·465 ·635 ·379 ·393 ·331	·455 ·464 ·636 ·378 ·414 ·330	· 55 · 47 · 67 · 37 · 41 · 34
SEPTEMBER.	12 13 14 15 (16 17 18	368 260 210 222 336 421	·344 ·260 ·239 ·265 ·334 ·444	· 325 · 257 · 245 · 309 · 378 · 464	321 265 242 311 401 469	·319 ·270 ·252 ·343 ·441 ·482	·303 ·261 ·255 ·352 ·431 ·481	·312 ·262 ·255 ·362 ·424 ·491	*314 *265 *258 *367 *418 *493	·472 ·253 ·323 ·385 ·394 ·483	· 277 · 251 · 325 · 377 · 399 · 478	· 262 · 284 · 324 · 378 · 379 · 440	· 26 · 23 · 33 · 36 · 36 · 42
	19 20 21 22 23 24 25	385 352 279 345 368 297	393 375 315 315 379 369	·402 ·383 ·342 ·433 ·369 ·320	·399 ·387 ·323 ·460 ·365 ·337	· 394 · 381 · 410 · 464 · 375 · 360	·405 ·399 ·405 ·484 ·368 ·376	·408 ·401 ·400 ·485 ·364 ·403	·415 ·369 ·372 ·508 ·384 ·349	·406 ·369 ·359 ·506 ·381 ·390		·389 ·337 ·379 ·495 ·389 ·384	·41 ·33 ·38 ·50 ·39 ·39
	26 27 28 29 30	-452 $-289$ $-258$ $-217$	 '470 '320 '255 '234	·482 ·338 ·264 ·251	·495 ·313 ·279 ·275	.528 :304 :322 :279	.555 :304 :259 :271	·576 ·299 ·289 ·301	-593 -310 -326 -277	·557 ·273 ·256 ·261	-555 •262 •287 •273	·558 ·261 ·302 ·283	· 54 · 28 · 30 · 29
I a u wlu	Means	334	*359	379	*385	414	407	•405	·411	·416	•409	•405	•40

		HU	MIDITY (	OF THE A	IR, AND	TENSION	OF THE	ATMOSPF	IERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
80 80 82 87	88 83 81 87	86 88 81 87	90 95 82 89	90 95 84 89	92 97 89 97	92 97 88 —	92 96 86	95 96 85 —	95 96 85 — 91	95 96 86 — 94	95 96 87 - 91 }	85 87 85 95
78 86 94 76 78 73	88 84 98 78 91 86	92 85 97 83 95 88	95 88 99 84 92 89	95 86 94 94 94 90	96 89 90 95 94 91	90 96 89 90 95 94	90 96 88 90 95 95	93 96 88 91 94 95	95 89 93 94 95	95 89 85 94 94	94 89 89 97 94	88 85 88 83 84
79 62 84 81 75 84	80 74 91 91 75 88	80 78 89 94 75 91	80 83 78 95 79	80 84 82 94 85 92	82 88 85 91 87 91	89 83 87 88 94 90	91 85 91 92 95 98 — 89	94 88 91 93 95 93 —	96 89 94 95 95 92 —	97 94 91 94 96 93 —	93 } 90 91 95 95 93	84 81 80 80 87 83 91
93 73 91 87 94 91	92 81 93 88 96 92	89 84 95 96 94 95	90 83 95 98 90 94	90 88 97 97 94 94	91 89 95 97 93 87	89 91 91 99 94 94 	90 93 96 91 95 —	91 92 94 94 91 95 —	91 94 94 89 92 —	90 93 96 89 88 —	92 94 96 89 88 ——————————————————————————————	91 82 88 88 91 90
89 79 85 79	92 83 86 88	91 85 90 88	77 90 89 82	78 92 90 84	75 97 88 80	77 94 88 85	87 94 89 81	89 95 94 81	93 91 90 88	91 91 94 91	91 90 90 88	88 82 86 80
82	87	88	88	90	90	91	92	92	92	92	92	85
In. '464 '533 '445 '430	In. '422 '504 '406 '431	In. '386 '535 '395 '447	In. •382 •553 •400 •461	In. '375 '509 '401 '464	In. '376 '483 '395 '482	In. 368 468 385	In. '351 '425 '375	In. '350 '421 '382	In.	In350 -418 -384308	In. '332 '413 '387 -303	In. *395 *476 *483 *394
·445 ·457 ·626 ·372 ·400 ·357	·447 ·457 ·614 ·360 ·372 ·335	·427 ·452 ·603 ·374 ·353 ·324	·433 ·492 ·612 ·334 ·336 ·327	·430 ·498 ·452 ·334 ·330 ·326	387 313 320 325	318 '405 '503 '384 '290 '318	*310 *385 *506 *369 *276 *319	309 376 502 375 275 311	360 510 374 269 303	*356 *513 *323 *266 *294	354 521 312 270 297	*426 *472 *536 *326 *351 *372
·262 ·226 ·365 ·351 ·359 ·417	·257 ·226 ·317 ·332 ·359 ·453	·247 ·227 ·297 ·323 ·359 ·457	·241 ·230 ·272 ·310 ·379 ·446	·236 ·234 ·273 ·316 ·372 ·445	·242 ·236 ·272 ·317 ·375 ·450	395 241 230 269 328 378	397 •246 •223 •253 •327 •470	395 254 218 237 327 440	398 258 214 231 322 431	'404 '270 '215 '222 '335 '432	·400 } ·262 ·210 ·223 ·338 ·429 ·387 }	·287 ·242 ·271 ·332 ·395 ·440
·403 ·312 ·369 ·478 ·397 ·383	364 309 353 461 398 385		357 293 330 464 382 380	 ·353 ·296 ·350 ·438 ·388 ·377	346 297 322 428 373 347	378 346 289 319 452 371	378 360 273 297 414 372	389 364 266 289 408 363	· 392 · 351 · 274 · 286 · 392 · 330	*387 *369 *274 *300 *379 *306	361 274 292 368 298	·382 ·329 ·340 ·446 ·374
·530 ·276 ·279 ·292	.505 .280 .274 .270	·492 ·269 ·279 ·263	*396 *244 *260 *245	·376 ·269 ·259 ·260	·329 ·265 ·260 ·262	·331 ·301 ·250 ·260 ·291	·453 ·308 ·248 ·247 ·290	·454 ·301 ·247 ·238 ·287	*467 *293 *250 *234 *296	·452 ·288 ·252 ·218 ·304	$\begin{bmatrix} -447 \\ -284 \\ -252 \\ -217 \\ -270 \end{bmatrix}$	·382 ·449 ·277 ·268 ·273
.393	*380	*376	.368	.360	.350	*341	*341	.338	`334	.331	*327	*374

an 2005 dayla dayna bara bara da Callina		HUM	IDITY OF	THE AIR	, AND TE	NSION OI	THE AT	моѕрнев	RIC VAPO	UR.		
Hours of Mean Göttingen Time.	} 0	1	2	3	4	5	6	7	8	9	10	11
Hours of Mean Toronto Time.	]   18	19	20	21	22	23	0	1	2	3	4	. 5
$\begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$	91	86 89	77 85	69 69	65 68	64 62	67 59	62 60	64 70	58 72	56 70	$\begin{array}{c} 62 \\ 78 \end{array}$
5 6 7 8 9	97 96 91 92 96 89	97 96 92 94 96 90	96 96 94 93 96 87	91 92 95 92 94 74	88 94 95 88 92 73	86 96 93 88 89 72	81 89 92 93 89 73	81 89 91 91 95 85	80 87 87 95 94 81	78 84 83 93 96 78	83 87 84 95 96 81	85 90 86 94 84 85
Humidity of the Air.  OCTOBER.	74 83 85 88 90 92	76 85 87 86 86 83	70 88 81 84 80 83	57 88 75 72 81 78	51 85 73 66 72 74	48 78 70 66 75 71	43 85 55 61 73 68	45 82 47 61 75 70	46 89 47 62 70 71	48 87 50 60 73 70	47 90 61 55 70 72	59 92 49 45 80 74
Humidit 18 20 21 22 22 24 24	97 93 90 84 93 97	84 97 91 79 93 94	94 94 84 81 93 96	89 83 76 77 92 94	87 68 79 68 89 75	85 58 73 73 87 70	80 49 67 73 86 81	77 51 64 73 87 83	77 47 45 73 87 77	78 51 42 73 90 80	78 47 42 73 87 80	81 52 44 75 85 87
25 26 27 28 29 30 31	93 82 49 91 84 84	91 100 47 84 93 94	92 100 47 78 82 96	87 74 67 70 84 92	73 73 64 48 85 88	62 75 63 65 76 77	62 71 70 59 77 76	60 77 65 64 71 75	62 71 65 66 71 81	60 70 73 68 73 80	58 63 64 64 78 84	57 67 72 65 83 84
Hourly Mean	88	88	86	81	76	74	72	72	72	72	72	74
	In. 264 216	In. •266 •236	In. •263 •269	In. •243 •257	In. •235 •273	In. •248 •259	In. •261 •247	In. 247 255	In. •249 •307	In. :236 :319	In. •229 •295	In. •239 •306
5 6 7 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	*243 *440 *418 *396 *415 *226	·277 ·458 ·422 ·399 ·411 ·260	358 '465 '429 '396 '414 '276	·408 ·477 ·430 ·391 ·414 ·279		·426 ·492 ·423 ·383 ·429 ·289	*417 *509 *422 *399 *434 *292	·400 ·507 ·418 ·395 ·422 ·347	393 501 407 410 423 364	369 504 400 407 428 349	392 '479 '405 '417 '430 '360	 ·383 ·465 ·413 ·413 ·392 ·368
Tension of the Vapour.  OCTOBER.	1177 1215 1199 1178 1149 246	185 230 205 177 148 242	182 248 208 176 157 257	166 260 197 169 167 257	159 269 201 167 161 261	160 256 198 165 197 264	150 255 169 155 191 265	156 245 153 150 198 292	167 1253 154 155 194 302	178 249 152 149 197 303	173 256 174 134 182 301	196 262 137 107 196 295
Jo uoisuaL 17 18 19 20 21 22 23 24	230 244 151 167 210 200	· 223 · 247 · 162 · 165 · 211 · 192	· 283 · 269 · 190 · 186 · 210 · 212	·314 ·278 ·221 ·200 ·208 ·243	358 237 255 194 209 221	379 218 254 216 206 229	·409 ·198 ·238 ·214 ·201 ·280	·415 ·199 ·239 ·207 ·208 ·283	*411 *194 *186 *205 *213 *265	·408 ·204 ·173 ·209 ·224 ·277	397 176 164 208 222 272	-391 -185 -150 -210 -212 -267
24 25 26 27 28 29 30 31	289 134 059 127 134 184	284 170 055 125 172 180	· 290 · 180 · 060 · 143 · 164 · 206	·292 ·132 ·108 ·142 ·213 ·259	·241 ·130 ·111 ·116 ·243 ·282	·208 ·131 ·114 ·165 ·244 ·276	· 205 · 130 · 136 · 150 · 253 · 272	· 201 · 133 · 135 · 162 · 244 · 280	186 122 136 170 246 293	163 120 154 173 246 285	141 105 130 159 258 290	127 105 139 153 241 262
Tourly Mean	_	•235	250	•259	•260	•263	•264	•265	•266	·264	•260	-254

		HU	MIDITY	OF THE A	AIR, AND	TENSION	OF THE	ATMOSPH	ERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
76 83	88 90	90 88	88 90	92 89	88 90	89	92	93	89	88	88	78
						99	97	95	96	97	$\frac{-}{97}$ }	83
90	91	93	91	95 00	95	94	94	96	96	96	96	90 93
$\begin{array}{ c c c }\hline 92\\ 87\end{array}$	92 88	95 95	96 96	96 95	97 94	96 92	96 92	95 95	9 <b>5</b> 95	94 94	92 94	95 92
88	88	96	96	96	92	90	91	92	90	87	96	$\frac{52}{92}$
80	80	74	73	72	78	85	85	83	89	93	94	88
90	88	81	84	81	81						$\frac{76}{76}$	82
64	$\frac{-}{70}$	$\frac{-}{79}$	84	85	94	84 93	84 91	85 94	82 91	$\frac{83}{93}$	84	70
93	94	92	94	97	93	89	86	87	87	83	88	88
59	66	72	78	80	86	88	86	89	88	89	89	73
58	75	80	84	92	92	88	84	83	89	87	92	75 70
77 74	81 82	83 85	85 84	85 84	86 87	86	88	73	75	75	78	79
		_	—		_	92	94	94	94	95	$\frac{-}{97}$	82
86	84	85	72	81	87	88	87	88	84	90	93	85
71	62	66	73	76	89	88	90	87	92	91	89	73 70
50 78	50 76	57 77	71 75	68 75	76 86	86 91	82 93	83 93	86 93	86 93	85 93	80
89	89	90	91	93	92	91	80	93	92	92	94	90
87	97	94	95	90	85						$\left.\begin{array}{c} - \\ 92 \end{array}\right\}$	88
	<del></del>		0.5	85		96 70	96	93	93	93	92 J 83	75
71 46	73 48	73 50	85 51	56	81 57	79 57	78 54	74 53	77 53	87 52	50	65
80	99	91	78	74	80	82	81	82	77	78	84	72
65	70	72	84	82	84	84	77	81	84	84	78	74
83	85	86	94	73	92	91	93	93	93	94	96	85
84	82	83 —	90 —	88	93	85	87	94	95	99	98 }	87
77	80	82	84	84	87	88	87	87	88	88	88	81
In. 251	In. •244	In. •240	In. •215	In. 201	In. •222	In. •217	In. •208	In. •214	In. •219	In. 213	In. •212	In. •235
275	•273	260	283	281	259						- )	•272
						297	294	273	273	263	261 }	
397 455	·400 ·451	.407 .459	*397 *458	389 442	·387 ·441	*394 *440	*392 *440	*385 *435	·394 ·435	·396 ·429	·422 ·418	`38 <b>5</b> `461
420	420	·435	·430	431	423	·413	•409	'413	·410	406	'408	·418
'420	·420	·428	•419	415	'401	*395	•405	*401	*395	382	•417	404
370	369	320	285	269	277	.282	.274	257	•259	250	*248	·35 <b>4</b>
357	*345	336	*349	327	318	.225	•218	$\cdot \frac{-}{213}$	•208	•212	188	•292
201	196	•218	•217	212	'210	.209	•204	215	. *211	.227	.218	191
265	265	255	257	258	255	242	•222	216	210	200	206	·244
148	158 143	$^{ullet}_{142}$	·159 ·145	160 147	160 147	159 134	166 128	173 127	·176 ·140	184 140	185 147	$\overset{\boldsymbol{\cdot}}{112} \\ \overset{\boldsymbol{\cdot}}{148}$
185	208	·209	211	224	233	233	236	211	215	215	217	197
.300	329	*332	*322	*324	*332						$\left\{ -\frac{1}{215} \right\}$	.273
1400						231	223	224	216	·212	·215 } ·247	*338
.422 .219	·385 ·182	.381 .185	*336 *183	.330 .180	`337 `174	·329 ·167	'310 '163	301 152	·268 ·158	·250 ·157	154	·197
148	139	156	177	166	164	160	105	132	152	152	166	177
215	<b>.</b> 210	.209	.202	204	209	·214	•216	'212	·212	210	212	204
221	·218	$^{\circ}_{231}^{219}$	218	218	'217	.216	179	.191	.181	185	201	.208
257	·239 —	231 —	•222	.207	198	305	•305	•294	$\cdot_{293}^{-}$	•293	$\left\{ -\frac{1}{289} \right\}$	•253
147	145	144	154	154	145	138	135	127	.130	.139	129	.180
.069	.067	.068	.066	.067	.067	.067	•061	.061	.061	.060	059	.099
145 146	179	161 152	137 148	133	128	129	125	127	121	122 132	·125 ·126	$\overset{\boldsymbol{\cdot}}{} \overset{124}{} \\ \overset{\boldsymbol{\cdot}}{} \overset{142}{}$
232	`153 `222	221	208	137 170	139 187	.139 .181	·127 ·179	131 174	*135 *173	176	120	207
238	243	214	209	190	196	293	•295	.308	.319	324	$\left\{ \frac{1}{323} \right\}$	•259
255	*254	*252	•246	240		239	233	230	•229	•228	230	247
Z.).3	20 <del>4</del>	202	240	240	.239	239	200	<b>⊿</b> 30	229	240	200	441

Götting Time	gen }	0	1	2	3	4	5	6	7	8	9	10	11
	Mean ]	18	19	20	21	22	23	0	1	2	3	4	5
	1 2 3 4 5 6 6	100 98 96 97 90 92	100 98 96 97 90 94	98 98 91 94 80 94	97 96 93 68 79 83	94 91 94 75 74 82	94 89 93 79 74 79	93 86 95 78 67 80	92 86 95 78 59 80	93 85 95 76 67 81	93 85 95 78 58 79	93 88 96 72 60 79	97 91 97 79 69 93
e Air. IR.	7 8 9 10 11 12 13	98 98 79 78 92 91	100 97 79 78 88 91	100 97 77 76 88 91	93 97 80 76 83 82	100 95 87 79 80 79	100 85 68 79 72 73	92 78 68 75 74 73	98 81 65 73 70 74	99 72 65 73 67 81	98 69 66 71 69 80	98 64 72 73 72 83	93 70 71 77 73 81
NOVEMBER	14 15 16 17 18 19 20	90 96 80 98 79 100		87 98 82 100 81 100	84 94 84 100 78 92	80 85 82 100 80 94	81 86 78 100 80 90	89 90 69 100 88 85	78 90 82 100 81 85	67 86 87 100 73 84	64 87 76 100 82 84	67 83 74 100 78 87	75 82 87 100 81 93
	21 22 23 24 25 26 27	100 98 100 97 98 91	100 98 100 97 99 91	100 100 100 100 100 94 89	98 100 100 96 92 88	94 100 100 90 92 98	91 100 100 90 91 90	88 96 89 87 92 93	83 96 91 93 94 84	82 96 93 95 94 90	82 96 97 94 90 94	86 94 100 94 87 96	89 92 100 93 89 90
	28 29 30	100 97	100 100	100 94	100 94	100 92	100 89	100 89	100 87	100 86	100 77	100 73	100 78
lourly I	Means	94	94	93	90	89	87	85	84	84	83	83	86
	$\left( \begin{array}{c c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{array} \right)$	In. '327 '348 '296 '256 '188 '163	In. '333 '348 '298 '252 '187 '154	In. '339 '358 '367 '281 '188 '172	In. '350 '367 '380 '233 '196 '172	In. '365 '372 '375 '258 '202 '178	In. '377 '386 '366 '299 '206 '179	In. '398 '385 '395 '291 '193 '179	In. '394 '410 '395 '288 '182 '179	In. '387 '379 '401 '279 '193 '181	In. '369 '372 '391 '269 '171 '181	In. '352 '371 '393 '253 '170 '184	In. • 341 • 349 • 383 • 250 • 176 • 197
apour. R.	7 8 9 10 11 12 13	·292 ·360 ·174 ·161 ·163 ·180	 ·300 ·359 ·176 ·165 ·152 ·176	·305 ·385 ·175 ·161 ·159 ·181	·292 ·396 ·187 ·165 ·179 ·183	·305 ·410 ·202 ·172 ·183 ·183	*311 *345 *163 *175 *172 *176	·312 ·303 ·166 ·169 ·177 ·183	·328 ·293 ·160 ·166 ·172 ·191	·329 ·267 ·158 ·166 ·161 ·205	*328 *262 *159 *161 *169 *195	·330 ·267 ·168 ·164 ·168 ·197	· 321 · 227 · 162 · 168 · 166 · 192
NOVEMBER.	14 15 16 17 18 19 20	·206 ·150 ·244 ·263 ·156 ·108	·202 ·150 ·241 ·264 ·154 ·108	·204 ·168 ·252 ·264 ·144 ·114	·208 ·199 ·265 ·266 ·133 ·119	·204 ·204 ·279 ·270 ·134 ·136	·208 ·220 ·282 ·272 ·130 ·139	·219 ·249 ·264 ·273 ·138 ·137	·196 ·260 ·299 ·272 ·128 ·142	174 269 303 276 121 143	· 167 · 277 · 286 · 284 · 132 · 141	·170 ·257 ·278 ·299 ·123 ·141	· 184 · 248 · 300 · 307 · 124 · 143
-	21 22 23 24 25 26 27	·209 ·259 ·330 ·240 ·141 ·122	·212 ·262 ·302 ·240 ·139 ·127	·212 ·269 ·307 ·242 ·133 ·130	·226 ·285 ·311 ·251 ·131 ·133	·239 ·302 ·334 ·240 ·131 ·143	·257 ·327 ·349 ·240 ·131 ·140	·263 ·343 ·317 ·226 ·132 ·142	· 262 · 354 · 325 · 230 · 137 · 149	·249 ·351 ·328 ·228 ·137 ·160	·246 ·358 ·323 ·223 ·132 ·163	·238 ·351 ·327 ·221 ·125 ·160	· 232 · 356 · 319 · 209 · 120 · 151
	28 29 30	·073 ·102	·073 ·104	·074 ·110	·075 ·118	-078 -119	·085 ·121	·085 ·123	·086 ·124	·091 ·126	·093 ·115	·093 ·103	·086
	Means	•212	·211	·219	•224	'231	•233	•233	.235	•233	•230	•227	•224

12	13	14	15	16	17	18	19	20	21	22	23	Daily an
6	7	8	9	10	11	12	13	14	15	16	17	Monthly Means.
							00	07	97	99	100	96
.00	96	98	98	96	97	96	96	97 97	97	98	97	93
93	95	95	95	95 97	97	96	96 88	91	94	97	98	94
97	96	96 56	97	$\frac{97}{72}$	89 61	89 65	82	88	88	90	90	81
83	84	76 78	79 85	72 79	64 81	86	89	93	93	93	93	79
76 96	79 <b>9</b> 1	98	97	97	96						- 1	90
90	<i>J</i> 1	50	<del></del>	<del>-</del>	_	96	97	95	95	96	1	I
93	98	93	96	96	96	96	97	97	96	97	97	97
66	83	79	62	61	56	64	67	71	74	76	73	76
71	75	77	68	76	86	79	88	82	80	79	78	76 78
76	74	78	80	80	80	80	80	84	85	79	89 86	80
75	77	80	85	86	85	85	83	79	79	82	86	
86	86	88	89	91	95				93	94	$\frac{-}{90}$ }	86
-		<del></del> 1				94	94	94	95	90	98	85
81	92	90	92	94	86	86	86	92 87	82	87	$\frac{36}{78}$	87
82	85	87	82	82	79	85	86 88	89 89	95	97	98	85
89	88	85	94	93	89	85 88	82	82	83	80	83	95
100	100	100	99	87 06	87 05	99	100	100	100	100	100	87
78	86	86 93	89 97	96 96	95 93		100				l }	94
91	95	90	97	90	90	98	98	100	100	100	100 }	!
94	98	96	94	92	94	100	96	94	94	97	97	93
95	94	94	94	93	96	100	100	100	100	100	100	97
95	94	98	99	96	94	95	97	98	98	98	98	97
94	93	98	98	95	94	99	94	94	97	87	90	94
93	100	100	100	100	100	100	100	100	100	94	91	95
90	95	95	92	92	94					<del></del>	$\frac{-}{100}$	94
						100	100	100	100	100		100
.00	100	100	100	100	100	100	100	100	100	100	97	89
84	85	82	86	87	94	81	85	100	100	100	100	
88	90	90	90	90	89	90	91	92	93	93	93	89
In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.
*318	.321	<b>.33</b> 8	*351	*333	*340	*338	*356	*338	337	346	349	350
338	•332	•344	•369	*356	*350	*341	*338	341	*356	317	312	359 347
395	*357	•370	*383	381	.314	.308	*305	282	277	265	*253 *191	•228
230	·218	•205	185	184	.160	159	185	185	177	183	168	180
176	172	164	173	168	173	176	177	178	174	172		
180	•158	<b>15</b> 9	•161	161	157			.071	•278	$\cdot \frac{-}{283}$	$-\frac{1}{286}$	.198
				•001		273	271	274	*353	*354	367	*324
321	328	328	*322	321	322	*333	335	*335 *155	•165	170	•168	•249
205	218	202	176	165 165	·153 ·179	.168 .166	·157 ·177	169	166	162	.160	168
161	·167	167 163	151 166	166	166	168	162	168	168	152	167	165
162 168	·157 ·167	103	176	179	176	176	176	$\cdot 172$	175	.180	185	172
207	211	218	·219	224	225						- 3	.200
						210	•211	•211	205	·203	205	
190	•204	196	191	.180	166	166	165	•200	157	153	159	186
244	258	260	•242	•242	.261	260	$\cdot 262$	•262	•266	260	*238	238
289	284	275	•293	<b>·2</b> 86	•278	<b>.</b> 265	•270	•267	274	277	268	276
301	302	*302	•339	286	<b>.</b> 269	•263	•226	•216	208	177	176	266
119	•127	124	127	132	125	124	122	121	.116	.116	.109	.158
146	<b>.</b> 163	165	171	166	<b>1</b> 58				•000	• 900	$-\frac{1}{211}$	155
			_			184	184	197	206	209	211)	•242
236	•243	237	241	239	244	267	*252	252	·252	$^{ullet}257 \\ ^{ullet}347$	·347	334
353	*354	*350	350	351	353	352	'346	349	·357	·247	248	291
290	<b>2</b> 69	272	275	255	250	252	252	•250 •164	·248 ·166	136	135	206
211	205	206	206	194	181	185	165	164	100	118	125	126
122	124	125	121	120	116	112	116	.121	144		7	
151	160	159	159	157	.156	· <del>0</del> 76	.075	.072	$\cdot \overline{072}$	.070	•069 }	129
084	.081	.081	.084	.085	.091	.093	103	100	.097	.103	.101	.087
111	117	118	131	142	157	.138	103	143	132	135	135	124
1			•222	217	·212	•214	•213	•212	•212	•207	•207	•220

			HUMI	DITY OF	THE AIR,	AND TE	NSION OF	THE AT	MOSPHER	IC VAPOU	JR.		
Iours of . Göttin Time	gen e.	0	1	2	3	4	5	6	7	8	9	10	11
Iour : of Toro Tim	nto //	18	19	20	21	22	23	0	1	2	3	4	5
	$\left[\begin{array}{c c}1\\2\\3\\4\\5\end{array}\right]$	100 100 94 100	99 100 94 100	75 100 95 100	68 100 94 97	69 94 94 96	66 91 91 97	68 90 89 100	68 89 92 100	74 79 94 97	62 86 86 92	79 91 91 89	75 97 90 92
	6 7 8 9 10	93 91 89 86 100 100	100 91 88 90 100	93 96 86 92 100 100	91 74 79 91 100 99	94 74 81 100 100 97	94 79 79 100 100	99 79 77 100 82 78	96 77 78 100 79 73	95 78 83 100 82 75	97 78 85 100 83 72	97 91 85 100 83 81	100 94 88 100 76 84
midity of the Air. DECEMBER.	12 13 14 15 (16 17 18	99 95 86 94 93 100	99 95 97 94 98 100	97 97 79 91 85 100	99 97 85 91 81 100	99 97 71 91 63 100	99 97 79 91 79 100	96 95 87 91 77 99	97 97 67 86 86 95	99 98 70 83 85 99	99 97 71 83 86 89	100 97 67 95 87 88	100 100 77 85 91 88
Humidity	19 20 21 22 23 24	93 100 95 98 88	93 100 96 100 93	90 98 98 96 93	100 100 100 100 100 88	100 98 98 98 93 94	98 98 98 98 98	94 98 90 93 77	91 92 93 93 85	95 92 87 100 79	75 90 87 99 79	84 90 87 88 83	100 90 78 87 86
	25a 26 27 28 29 30 31	98 93 97 90 100	100 95 96 93 100	100 95 93 92 100	100 93 92 92 99	93 86 88 93 95	80 86 81 92 99	92 90 83 95 95	92 99 87 90 97	92 95 86 93 99	92 95 87 95 99	92 95 87 95 99	97 99 88 99 99
lourly I	Means	95	97	94	93	91	90	89	88	89	87	89	91
	$\left(egin{array}{c c}1\\2\\3\\4\end{array} ight]$	In. *180 *205 *179 *143	In. 188 201 179	In. *159 *200 *181 *141	In. *151 *206 *179 *147	In. *156 *204 *179 *147	In. *167 *205 *178 *161	In. *155 *209 *173 *169	In. 168 207 177 169	In. 187 184 171 164	In. •164 •198 •155 •159	In. *185 *202 *159 *154	In. 172 197 154 158
	5 6 7 8 9 10	137 169 191 193 320	147 169 186 198 307	137 171 191 191 308 201	149 156 192 199 309 204	163 166 214 214 321 206	158 183 225 223 316 199	174 179 230 230 288 164	176 184 238 234 278 162	182 190 250 243 288 167	·180 ·191 ·250 ·263 ·255 ·161	180 208 246 269 243 172	·170 ·192 ·250 ·277 ·217 ·163
Tension of the Vapour. DECEMBER.	12 13 14 15 16 17 18	•217 •172 •170 •081 •091 •087	215 172 161 081 096	·206 ·177 ·132 ·079 ·088 ·091	·208 ·182 ·145 ·079 ·087 ·106	·208 ·182 ·124 ·084 ·073 ·124	·210 ·183 ·141 ·087 ·096 ·136	·208 ·181 ·159 ·090 ·103 ·147	· 208 · 183 · 125 · 089 · 122 · 158	·204 ·184 ·130 ·091 ·128 ·168	·195 ·183 ·133 ·093 ·131 ·157	196 183 120 107 133	192 187 127 100 131
Tensic	19 20 21 22 23 24 25 ^a	·081 ·077 ·113 ·100 ·104	*081 *074 *112 *102 *107	·078 ·071 ·114 ·108 ·107	·082 ·075 ·119 ·109 ·110	*084 *083 *122 *106 *116	·084 ·095 ·128 ·119 ·098	·083 ·098 ·120 ·121 ·093	· 084 · 096 · 122 · 124 · 102	·087 ·098 ·118 ·132 ·096	·071 ·102 ·119 ·133 ·096	·074 ·107 ·119 ·119 ·099	· 0777 · 108 · 105 · 117 · 101
	26 27 28 29 30	•183 •157 •215 •237		-078 166 214 233 267	-081 174 221 252 269	-088 -170 -230 -259 -280	-080 171 220 265 297	:099 :177 :230 :285 :285	·096 ·189 ·234 ·282 ·285	100 186 231 283	103 190 232 275 285	-102 •190 •234 •275 •285	·109 ·199 ·234 ·273 ·282
	$\sqrt{31}$	•269	200	201	200		1	ł.	i .				-

^a Christmas Day.

		HU	MIDITY	OF THE A	AIR, AND	TENSION	OF THE	ATMOSPH	ERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
77 97 92 92	82 97 94 95	82 95 94 95	82 94 91 95	98 94 90 94 —	97 96 92 94	100 99 93 — 100	100 95 89 — 100	100 94 96 — 91	100 93 100 — 90	99 94 99 —	100 95 100 ——————————————————————————————————	84 94 93 96
92 100 92 100 81 92	80 80 93 100 80 90	80 100 95 100 76 94	95 100 95 100 82 94	81 98 95 100 85 97	86 99 94 100 82 100	82 100 94 100 83	86 100 81 100 85	85 95 77 99 91 —	89 95 80 100 91	90 95 79 100 100	90 86 83 100 100 — }	91 90 86 98 88
99 99 79 83 93	99 98 89 90 76	99 99 82 89 70	99 99 78 90 95	99 99 98 87 88 89	99 99 95 87 92 90	100 99 99 98 92 95	99 99 95 100 98 100	99 99 95 100 91 98	99 97 95 91 98 98	99 95 84 93 95 69	100 } 95 94 98 92 98	98 97 85 90 87
98 98 88 88 88 87	89 100 92 83 88 90	86 	84 	98 98 98 89 88 98	100 96 92 90 100	98 100 96 89 95	98 100 100 89 92	98 100 98 92 83	98 98 91 92 82	100 98 89 94 86	93 } 98 92 94 82 — }	95 96 95 90 92
100 99 92 99 99	97 97 97 93 99	98 97 93 99	100 89 97 100 100	98 95 97 99 100	100 97 97 99 99	98 99 97 95 100 99	98 97 95 95 100 99	100 97 94 92 100 100	98 100 97 90 99 99	91 95 96 88 99 99	98 } 95 97 88 99 100	90 96 95 91 96 99
92	91	91	93	94	95	96	96	95	95	93	95	92
In. 171 201 153 159	In. 174 201 150 169	In. •172 •199 •149 •176	In. 172 192 145 183	In. 197 190 144 181	In. 205 184 144 180	In. *216 *185 *142 *146	In. '217 '182 '138 '143	In. 211 179 145 - 136	In. '209 '179 '147 '131	In.	In. '205 '181 '143	In. *183 *195 *159 *155
144 186 252 277 214	144 144 246 285 206 142	136 177 248 285 197	*151 *180 *249 *295 *204 *145	154 235 248 289 202 145	159 178 246 322 193 156	1153 1186 246 246 314 1193	116 116 1184 1216 1319 1193	157 180 197 294 196	167 178 199 293 187	169 193 192 308 192	*168 *181 *191 *314 *194	159 182 225 264 243
187 185 126 099 133	1186 1183 1133 1108 1103	1179 1179 1185 1117 103 103 1171	179 185 099 103 117 163	172 183 114 101 103 159	172 185 104 097 099	170 185 102 099	1235 170 181 109 101 109	170 180 194 198 1991	*235 *170 *181 *080 *090 *089	167 163 1079 1087 1075		187 190 181 121 093 103
.075 .105 .104 .118 .102		.070 .120 .082 .121 .097	·075 ·130 ·088 ·125 ·101		·077 ·128 ·099 ·121 ·105	106 1077 129 1091 121	105 1076 136 1089 119	103 1074 131 1093 110	102 1073 1117 1093 1110	.099 .072 .110 .095 .113	·090 ·069 ·111 ·095 ·105 —	*132 *077 *106 *105 *116 *096
·111 ·199 ·235 ·269 ·275	106 200 234 273 269			127 197 197 227 264 278	136 201 227 260 275	·075 ·137 ·206 ·234 ·260 ·285	•075 •139 •203 •236 •260 •292	•078 •139 •205 •233 •260 •297	*080 *149 *208 *237 *255 *305	*081 *149 *208 *236 *249 *305	·084 } ·153 ·213 ·236 ·264 ·308	116 190 229 263 283
	167	166	<del></del>	170	170	·169	·168	165	•164	•163	·165	167

Hours	of M	lean )	0	1	2	3	4	5	6	7	8	9	10	11
Gott T Hours	ime.	<u>. ]  </u>		1	1	1	1			1	<u> </u>	<u> </u>	<u> </u>	1
To	ront ime.	o }	18	19	20	21	22	23	0	1	$\frac{1}{1}$	3	4	5
	ſ	$\begin{pmatrix} 1 \\ 2 \end{pmatrix}$	100	99	100	100	100	100	99	100	99	97	93	93
		3	95	95	91	87	87	85	85 82	83	81 88	84 93	79 98	85
		4 5	91 98	99 99	99 97	77 99	85 99	92 100	99	78 87	90	88	87	100 84
		6	100	98	100	98	98	98	100 98	98 100	100 100	100 98	100 98	100
ĺ		$\begin{bmatrix} 7 \\ 8 \end{bmatrix}$	100 100	98 97	98 97	98 99	100 95	98 95	95 95	95	89	80	82	98 86
		9 10	97	96	100	100	100	100	100	100	100	100	100	$\frac{}{41}$
		11	100	100	98	95	94	95	95	91	91	97	98 85	100
Air		12 13	100 83	100 83	100 97	100 80	100 78	95 85	98 98	91 89	96 88	90 92	93	98 95
e le		14	100	100	100	100	100	100	100 100	100 100	100 100	100 98	100 87	100 84
Humidity of the Air.	3(	15 16	100	100	100	99	100	100		_	_	<b> </b>	-	_
dity	AN	17 18	81 69	81 100	86 64	90 89	89 84	73 82	73 82	83 76	69 82	70 71	82 76	85 86
ım	ا ت	19	100	100	100	100	100	95	92	92	92	88	87	100 85
=		$\begin{vmatrix} 20 \\ 21 \end{vmatrix}$	78 79	78 80	79 80	$\begin{array}{c} 74 \\ 72 \end{array}$	$\begin{array}{c} 74 \\ 72 \end{array}$	64 60	64 51	75 48	68 50	71 63	79 62	79
	- 1	$\begin{bmatrix} 22 \\ 23 \end{bmatrix}$	98	100	94	89	90	87	79	81	77	77	77	91
	- 1	24	100	100	100	92	80	80	83	82	81	81	87	86
		$\begin{bmatrix} 25 \\ 26 \end{bmatrix}$	$\frac{100}{95}$	98 97	100 96	93 98	74 98	82 99	87 100	86 100	82 100	84 100	86 100	90
		27	99	100	100	100	100	100	98	100	99	100	99 99	100
		$\frac{28}{29}$	81 96	80 96	80 79	$\begin{array}{c} 83 \\ 92 \end{array}$	78 76	81 75	80 73	80 74	80 75	$\begin{array}{c c} 82 \\ 72 \end{array}$	83	99 84
	- 1	$\begin{vmatrix} 30 \\ 31 \end{vmatrix}$	99	97	100	99	98	98	97	97	98	96	70	59
Hourl	ly M	leans	94	95	94	92	90	89	89	88	88	87	88	89
		- 11		1	31	1	1			ļ			!	'
Ī		1	In. •308	In. 318	In. 314	In. 319	In. 314	In. *328	In. •332	In. 332	In. •343	In. 329	In. 348	In. •351
		$\begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$	·308	In. •318	In.	In.	In.	In.	In.	·332 - 190	·343 ·187	*329  *193	*348  *179	*351  *184
		$\begin{bmatrix} 3 \\ 4 \end{bmatrix}$	·308  ·178 ·181	In. '318	In. 314 	In. '319 — '180 '131	In. 314 — 184 145	In. '328 - '186 '146	In. '332 — '187 '127	·332 ·190 ·117	343  187 128	*329  *193 *133	*348  *179 *130	*351 
		3 4 5 6	*308  *178 *181 *131 *080	In. 318 178 195 139 076	In. •314 •176	In. '319 '180 '131 '149 '075	In. 314 184 145 152 075	In. '328 '186 '146 '163 '079	In332	332  190 117 174 085	343  187 128 179 085	193 193 193 192 087	*348  *179 *130 *176 *087	*351 
		3   4   5   6   7	·308 	In. '318 '178 '195 '139 '076 '089	In. '314 '176 '180 '142 '075 '088	In. '319 '180 '131 '149 '075 '091	In. *314 *184 *145 *152 *075 *094	In328186 -146 -163 -079 -098	In. '332 '187 '127 '177 '084 '105	*332  *190 *117 *174 *085 *111	343 	*329  *193 *133 *192 *087 *111	*348 	*351 -184 *120 *149 *085
		3   4   5   6   7   8   9	*308 	In. 318 178 195 139 076 089 170	In314	In319 -180 -131 -149 -075 -091 -170	In314 -184 -145 -152 -075 -094 -167	In328186 -146 -163 -079 -098 -172	In332	*332 	343 ———————————————————————————————————	*329 	*348 	*351 
		3 4 5 6 7 8 9 10	*308 	In318178 -195 -139 -076 -089 -170027	In314 -176 -180 -142 -075 -088 -168029	In319 -180 -131 -149 -075 -091 -170 -032	In314 -184 -145 -152 -075 -094 -167 -036	In328186 -146 -163 -079 -098 -172044	In332	332 -190 117 174 085 111 182 -044	343 	*329 -193 *133 *192 *087 *111 *150 -049 *121	*348 	*351 
our.		3 4 5 6 7 8 9 10 11 12	*308 	In318 -178 -195 -139 -076 -089 -170 -027 -072 -070	In314 -176 -180 -142 -075 -088 -168 -029 -090 -068	In319 -180 -131 -149 -075 -091 -170 -032 -094 -089	In314 -184 -145 -152 -075 -094 -167 -036 -096 -107	In328186 -146 -163 -079 -098 -172 -044 -105 -116	In332 -187 -127 -177 -084 -105 -174 -044 -107 -130	332 -190 117 174 1085 111 182  109 135	343	*329 -193 *133 *192 *087 *111 *150  *049 *121 *134	*348 	*351 
/apour.		3 4 5 6 7 8 9 10 11 12 13	*308	In318 -178 -195 -139 -076 -089 -170 -027 -072	In314	In319 -180 -131 -149 -075 -091 -170 -032 -094	In. '314	In328186 -146 -163 -079 -098 -172 -044 -105	In332	332 -190 117 174 1085 111 182 -044 109 135 194 230	343	*329 -193 *133 *192 *087 *111 *150  *049 *121 *134 *203 *231	*348 	*351 
the Vapour.		3 4 5 6 7 8 9 10 11 12 13 14 15	*308 	In318 -178 -195 -139 -076 -089 -170 -027 -072 -070 -163	In314	In319 -180 -131 -149 -075 -091 -170 -032 -094 -089 -163	In. '314	In328	In332	332 -190 117 174 085 111 182 -044 109	343 	*329 -193 *133 *192 *087 *111 *150  *049 *121 *134 *203	*348 	*351 
of the Vapour.		3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	*308	In318 -178 -195 -139 -076 -089 -170 -027 -072 -070 -163 -217 -243 -143	In314	In319 -180 -131 -149 -075 -091 -170 -032 -094 -089 -162 -223 -253 -123	In314 -184 -145 -152 -075 -094 -167 -036 -096 -107 -166 -223 -272 -116	In. '328  '186 '146 '163 '079 '098 '172  '044 '105 '116 '179 '227 '281 '097	In332	*332 -190 *117 *174 *085 *111 *182 - *044 *109 *135 *194 *230 *230 *289 - *115	**343 	*329	*348 	*351 -184 *120 *148 *083 *110 *148 -020 *117 *116 *207 *232 *238 -116
sion of the Vapour.	JANUARY.	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	*308	In318 -178 -195 -139 -076 -089 -170 -027 -072 -070 -163 -217 -243	In314	In. '319 '180 '131 '149 '075 '091 '170 '032 '094 '089 '163 '223 '223 '253 123 '113 '072	In. '314 '184 '145 '152 '075 '094 '167 '036 '096 '107 '166 '223 '272 '116 '102 '085	In. '328 '186 '146 '163 '079 '098 '172 '044 '105 '116 '179 '227 '281 '097 '097 '085	In332	*332 -190 *117 *174 *085 *111 *182 - *044 *109 *135 *194 *230 *289 - *115 *089 *095	**343	*329	*348 	*351 -184 *120 *148 *085 *110 *148 -020 *117 *116 *207 *232 *232 *116 *087 *119
Fension of the Vapour.	JANUARY.	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	*308	In.  '318   '178  '195  '139  '076  '089  '170   '027  '072  '070  '163  '217  '243   '143  '139  '062  '132	In314	In. '319 '180 '131 '149 '075 '091 '170 '032 '094 '089 '163 '223 '253 '123 '113 '072 '143	In. '314 '184 '145 '152 '075 '094 '167 '036 '096 '107 '166 '223 '272 '116 '102 '085 '157	In. '328 '186 '146 '163 '079 '098 '172 '044 '105 '116 '179 '227 '281 '097 '085 '143	In332	**332	**343	*329	*348 	*351 
Tension of the Vapour.	JANUARY.	3 4 5 6 7 8 9 10 11 12 13 14 15 16 117 118 119 220 21 22	*308	In.  '318  -178  '195  '139  '076  '089  '170  -27  '072  '070  '163  '217  '243  -143  '139  '062	In314	In. '319 '180 '131 '149 '075 '091 '170 '032 '094 '089 '163 '223 '223 '253 123 '113 '072	In. '314 '184 '145 '152 '075 '094 '167 '036 '096 '107 '166 '223 '272 '116 '102 '085	In. '328 '186 '146 '163 '079 '098 '172 '044 '105 '116 '179 '227 '281 '097 '097 '085	In332	*332 -190 *117 *174 *085 *111 *182 - *044 *109 *135 *194 *230 *289 - *115 *089 *095	**343	*329	*348	*351 -184 *120 *149 *085 *110 *148 -207 *116 *207 *232 *238 -116 *087 *119
Tension of the Vapour.	JANUARY.	3 4 5 6 7 8 9 10 11 11 12 13 14 15 16 17 18 19 20 21 22 23 24	*308	In.  '318   '178  '195  '139  '076  '089  '170   '027  '072  '070  '163  '217  '243   '143  '139  '062  '132  '183	In314	In319 -180 -131 -149 -075 -091 -170 -032 -094 -089 -163 -223 -253 -123 -113 -072 -143 -181 -093 -136	In314 -184 -145 -152 -075 -094 -167 -036 -096 -107 -166 -223 -272 -116 -102 -085 -157 -201 -100 -133	In328186 -146 -163 -079 -098 -172044 -105 -116 -179 -227 -281097 -085 -143 -181138	In332	*332 	**343	*329	*348	*351 -184 *120 *149 *085 *110 *148 -020 *117 *116 *207 *232 *238 -116 *087 *119 *184 *1142 *137 -150
Tension of the Vapour.	JANUARY.	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 22 24 25	*308	In318 -178 -178 -195 -139 -076 -089 -170 -027 -072 -070 -163 -217 -243 -139 -062 -132 -183 -092 -116 -151	In314	In319 -180 -131 -149 -075 -091 -170 -032 -094 -089 -163 -223 -253 -123 -113 -072 -143 -181 -093 -136 -177	In. '314	In328	In332	*332 	**343	*329	*348	*351 -184 *120 *149 *085 *110 *148 -020 *117 *116 *207 *232 *238 -116 *087 *119 *186 *142 *137 -150 *189 *247
Tension of the Vapour.	JANUARY.	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 23 24 22 5 26 27	*308	In. '318 '178 '195 '139 '076 '089 '170 '027 '072 '070 '163 '217 '243 '143 '139 '062 '132 '183 '092 '116 '218 '223	In314	In. '319 '180 '131 '149 '075 '091 '170 '032 '094 '089 '163 '223 '253 '123 '113 '072 '143 '181 '093 '136 '177 '224 '236	In. '314	In328	In332	**332	**343	*329	*348	*351 -184 *120 *148 *110 *148 -020 *117 *116 *207 *232 *238 -116 *087 *119 *186 *142 *137 -150 *189 *247 *230
Tension of the Vapour.	JANUARY.	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 22 24 22 5 26 27 28	*308	In. '318 '178 '195 '139 '076 '089 '170 '027 '072 '070 '163 '217 '243 '143 '139 '062 '132 '183 '092 '116 '218 '223 '144	In314	In319 -180 -131 -149 -075 -091 -170 -032 -094 -089 -163 -223 -253 -123 -113 -072 -143 -181 -093 -136 -177 -224 -236 -147	In. '314	In328	In332	**332	343 — 187 128 179 085 112 173 — 049 113 136 194 231 294 — 097 093 103 171 131 118 — 151 200 240 244 166	*329	*348 	*351 -184 *120 *148 *110 *148 -020 *117 *116 *207 *232 *238 -116 *087 *119 *186 *142 *137 -150 *189 *247
Tension of the Vapour.	JANUARY.	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 23 24 22 5 26 27	*308	In. '318 '178 '195 '139 '076 '089 '170 '027 '072 '070 '163 '217 '243 '143 '139 '062 '132 '183 '092 '116 '218 '223	In314	In. '319 '180 '131 '149 '075 '091 '170 '032 '094 '089 '163 '223 '253 '123 '113 '072 '143 '181 '093 '136 '177 '224 '236	In. '314	In328	In332	**332	**343	*329	*348	*353 

		ш	MIDITY	OF THE A	AIR, AND	TENSION	OF THE	ATMOSPI	ERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
100	84	83	88	83	77 —	93	<del>-</del> 89	95	95	95	$\frac{-}{94}$ }	94
85	80	81	79	79	79	75	79	85	87	88	81	84
95	92	97	98	95	94	100	92	92	93	100	100	93
76 98	85 94	91 100	72 98	95 100	98 99	98 100	88 100	89 100	95 100	98 98	98 98	$\frac{92}{99}$
95	100	98	99	99	100	99	99	95	96	96 97	95	98
90	92	96	97	87	98						11	94
				_		98	97	97	97	97	$\frac{-}{97}$ }	
100	100	97	58	94	100	100	100	100	100	100	100	96
100 98	97 89	94 88	95 88	98 88	98 89	98 89	100 89	100 91	100 87	100 88	100 87	$\begin{array}{c} 97 \\ 93 \end{array}$
95	95	95	95	96	97	97	98	98	98	98	100	9 <b>3</b>
100	100	100	100	100	100	100	100	100	100	100	100	100
99	83	83	87	93	88				-		$\frac{-}{89}$ }	94
-			-			99	100	95	91	87		
80	80 94	80 93	84 94	87 97	84 93	84 96	84 100	83 100	81 100	86 100	78 100	81 88
100	82	87	90	88	95 95	86	87	87	81	80	78	91
87	100	84	87	88	80	79	79	78	75	76	79	78
66	72	77	80	81	84	86	89	92	91	98	97	75
94	91	94	97	100	100				-		<del>-</del> }	91
92	94	99	99	100	100	93 100	93 100	$\begin{array}{c} 93 \\ 100 \end{array}$	96 100	93 100	98 } 100	93
92	92	99	99	99	99	98	95	93	93	87	90	91
93	100	100	100	100	100	100	100	100	100	100	100	99
100	100	100	99	97	98	99	93	95	82	91	90	97
100	99	100	95	75	78	88	91	94	95	92	100	88
79	79	82	84	85	85	100	100	100	100	100	100 }	86
60	77	$\frac{-}{78}$	80	93	93	100 85	92	76	76	73	74	86
91	90	91	90	92	93	94	94	93	93	93	93	91
In. 267	In. •212	In. 197	In. •194	In. 177	In. 156	In.	In.	In.	In.	In.	In.	In.
						·168	166	170	175	175	176}	•257
184	179	181	174	177	•179	173	178	184	180	186	174	181
108	103	106	106	101	.099	105	100	101	107	·116 ·080	116	125
121 081	·125 ·074	132 079	*093 *078	107 077	·102 ·077	.098 .078	.087 .079	.080	.086 .081	•079	.081 .083	.130 .080
121	130	128	137	141	146	148	153	148	152	159	160	122
150	154	151	144	123	128			_			- 1	127
-				•000		040	036	.034	.033	031	1029	
116	*035	·034 ·112	.021 .115	*032 *118	.034 .117	*034 *115	`034 `117	*038 *115	·044 ·113	·049 ·089	.050 .072	.037 .105
115	114 130	112	113	1137	139	138	117	113	1156	161	164	103
205	207	205	207	*208	•209	211	213	211	213	215	214	•197
234	•238	241	•243	•247	•245	•243	253	245	•244	•247	*244	*235
217	185	•178	184	184	172			-167	1101	155	}}	•223
115	•116	117	128	•127	•127	170 130	172 130	167 141	161 142	133	134	123
.087	*084	.081	.083	.087	.085	.083	.076	.072	.066	*064	.063	.088
116	.108	115	122	•124	.131	126	113	123	122	124	127	104
187	•199	176	184	185	180	182	184	184	182	182	184	171
1114	112	113	107	107	·103	.097	<b>.</b> 096	.099	.093	.097	*096	132
138	117	120	120	124	121	•124	124	•124	126	121	$\{-\frac{1}{132}\}$	117
146	143	145	144	145	143	143	137	143	143	146	149	141
199	•19 <b>9</b>	•201	•204	•209	•205	207	*205	205	•209	207	*206	.193
245	250	237	237	232	234	223	216	·22 <b>2</b>	227	227	227	231
223	213	·200	204	204	199	196	187	189	165	·175 ·133	163 137	·217 ·155
190 136	*193 *134	·191 ·137	180 139	129 139	·124 ·139	132	132	.133	134			
						175	179	181	183	185	$  \cdot \frac{1}{187} \}$	•150
124	138	137	129	.136	.135	.119	127	.106	•106	102	105	.160
153	•150	148	•146	145	143	141	140	141	140	140	140	•151

				ним	IDITY OF	THE AIR	, AND TE	ENSION O	THE AT	MOSPHER	C VAPO	UR.		
Hours Göt T	of Me tingen	ean }	0	1	2	3	4	5	6	7	8	9	10	11
Hours To		ean }	18	19	20	21	22	23	0	1	2	3	4	5
Humidity of the Air.	BRUARY.	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	68 100 100 100 84 — 86 100 100 87 100 96 — 100 89 83 96	71 100 100 92 87 — 100 98 97 92 100 98 — 100 89 83 100	70 100 100 90 89 	68 87 100 88 88 — 83 92 77 96 100 95 — 81 77 86 83	63 83 75 85 85 78 91 79 93 87 80 74 77 74 86	66 77 68 85 85 78 86 70 94 87 73 — 72 77 71 77	76 78 81 83 85 73 92 71 91 95 75 63 68 76	79 72 72 93 79 — 78 88 76 91 76 70 — 64 74 68 75	$   \begin{array}{c}     74 \\     70 \\     70 \\     95 \\     80 \\     \hline     77 \\     81 \\     66 \\     80 \\     73 \\     71 \\     \hline     \hline     63 \\     66 \\     71 \\     79 \\   \end{array} $	68 72 73 99 84 — 86 84 69 92 69 75 — 65 67 75 81	70 75 78 99 80 — 88 87 65 90 66 83 — 69 77 78 83	86 90 85 98 89 65 98 80 89 72 72 84 89
Hum		17 18 19 20 21 22 23 24 25 26 27 28	97 100 — 79 100 91 72 95 100 — 81	96 99 75 97 98 76 94 100 84	92 89 98 ———————————————————————————————	65 83 ———————————————————————————————————	74 85 ———————————————————————————————————	70 87 61 91 66 64 88 67 100	64 82 	63 80 	70 79 ——————————————————————————————————	72 81 	78 82 	77 80 
Hourl	ly Me	eans	92	93	91	85	80	78	77	76	75	77	79	84
l'apour.	1	1 2 3 4 5 6 7 8 9 10 11 12	In. 102 116 167 183 134 109 107 123 103 050 081	In. 107 119 152 176 135 116 108 121 098 047 084	In.  109 120 153 176 135 102 108 129 095 048	In110 -137 -181 -191 -132100 -111 -126 -082 -055 -089	In. 107 162 156 202 131 098 117 127 081 054	In111 -155 -156 -205 -134102 -114 -124 -084 -059 -088	In. 121 159 193 201 134 - 101 128 138 084 071	In. 120 151 183 216 122 - 110 131 146 087 060 095	In	In111 -155 -185 -219 -130 -127 -129 -137 -089 -060 -104	In113 -158 -184 -220 -122131 -129 -130 -085 -061 -111	In. 127 174 181 216 130 - 095 130 127 088 071 112
Tension of the Yapour.	FEBRUA	13 14 15 16 17 18 19 20 21 22 23 24 25	·111 ·100 ·099 ·119 ·112 ·171 - ·171 ·174 ·160 ·089 ·073	106 1085 114 116 112 177 165 172 163 096 070 084	·114 ·094 ·123 ·129 ·127 ·183 ·165 ·178 ·178 ·100 ·073 ·105	124 1092 155 140 116 167  163 187 178 188 189 189 182 128	·129 ·104 ·147 ·167 ·151 ·178 ·162 ·199 ·149 ·098 ·091 ·131	·142 ·117 ·149 ·155 ·148 ·190 ·157 ·204 ·136 ·097 ·094 ·118	139 100 147 165 140 193 162 213 111 104 102 115	146 142 147 165 142 192 158 203 163 115 108	148 122 150 173 160 188 168 191 151 126 115 132	·153 ·119 ·157 ·171 ·160 ·186 — ·151 ·213 ·146 ·118 ·103 ·137	158 138 160 170 175 180 150 209 151 131 092 134	· 158 · 127 · 161 · 165 · 167 · 174 · 171 · 206 · 150 · 130 · 100 · 146
	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	26 27 28	·084 ·127	133	131	158	156	• 174	.181	175	176	<b>.</b> 198	.199	•174

12	T			HU	MIDITY	OF THE A	IR, AND	TENSION	OF THE	ATMOSPI	IERIC VA	POUR.		
Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sect	ŀ	12	13	14	15	16	17	18	19	20	21	22	23	Daily and
Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sect	ŀ	6	7	8	9	10	11	12	13	14	15	16	17	
96   100   100   100   100   90   91   95   84   84   86   100   89   88   93   94   95   84   84   86   100   89   88   87   78   91   84   89   87   78   91   95   95   95   95   95   95   95		95 99 97 92 — 76 92 78	97 89 98 95 — 80 92 72 100	99 95 99 97 — 82 92 82 100	82 95 100 93 — 87 90 87 100	100 95 100 95 — 94 87 79 100	100 95 100 93 — 97 100 75 98	100 97 88 — 83 100 100 77 96	100 97 85 — 84 100 100 81 100	100 98 83 — 86 100 100 89 100	100 100 87 	100 100 84 — 91 100 100 87 100	100 99 76 ——————————————————————————————————	91 90 96 88 88 93 79
The color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the color of the		93 96 	98 100 — 86 91 97 98 96 75 — 61 100 89 80 95	93 100 	88 100  84 89 100 100 100 71  60 100 89 91 100	93 100 — 85 87 100 100 100 73 — 79 100 97 77	94 100 — 99 78 100 100 100 89 — 82 100 98 75 100	90 	95 98 95 100 97 99 	84 100 95 100 100 98 	84 87 95 100 89 100 79 94 100 97 87	86 84 95 100 90 100 	100 } 89 78 100 100 99	89 83 82 88 91 87 83 72 96 84 79
No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.												100		
Th.	ŀ			92	91	92	94	93	93	94	93	93	93	87
·143 ·139 ·138 ·135 ·134 ·134 ·129 ·127 ·125 ·123 ·121 ·122 ·133		In. 130 178 176 213 128 101 128 146 085 077 110 150 124 149 157 158 167 155 202 142 127 105 155 162	In. 122 182 156 207 131 1099 128 134 083 081 101 162 135 144 151 162 169 142 197 138 098 103 141 168	In. 110 183 165 194 130 194 128 151 082 079 099 145 125 140 150 164 166 147 194 140 103 101 146 186	106 164 159 194 126 101 128 156 081 073 094 141 117 142 144 162 165 141 138 113 097 131 180	103 181 151 186 127 100 126 141 081 076 091 - 144 139 143 169 168 - 170 186 143 094 095 134 - 165	104 185 149 180 127 102 132 129 071 077 089 148 103 135 169 195 167 192 144 091 097 133 167	106 187 146 153 110 099 128 125 064 075 138 139 109 133 124 169 188 177 186 109 099 099 094 142	109 187 148 143 108 099 122 122 063 076 130 137 110 130 122 163 186 174 186 117 091 093 092 135	110 187 148 138 110 095 111 133 059 077 129 134 108 134 119 164 188 186 124 085 092 086 111	111 180 158 142 105 105 125 055 078 133 125 108 131 106 165 174 165 185 122 083 091 084 109	116 178 166 137 113 102 119 128 053 081 113 108 107 124 103 164 170 177 099 079 088 104 111	119 175 174 121 -18 103 120 117 051 078 -115 113 097 122 119 160 -190 168 170 101 069 085 -130 112	*113 *163 *165 *184 *125 *104 *121 *132 *078 *068 *103 *136 *112 *139 *142 *153 *179 *162 *192 *140 *101 *094 *119 *155

ours of Mean }	0	1	2	3	4	5	6	7	8	9	10	11
Time.	18	19	20	21	22	23	0	1	2	3	4	5
$ \begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix} $	100 100 100 94	100 100 100 97	100 100 100 100	100 94 100 97	98 100 100 88	91 81 100 88	83 94 100 84	82 87 97 80	72 100 94 89	98 98 87 97	75 97 89 95	88 100 74 94
5 6 7 8 9 10	91 100 83 95 90 100	100 97 75 97 93 100	91 96 79 98 93 90	84 84 78 98 91 74	82 85 73 96 81 70	88 78 70 81 97 68	82 76 64 85 70 78	80 70 71 79 68 88	84 74 76 76 74 70	65 70 76 76 62 68	71 63 86 79 72 70	74 77 94 81 64 79
MARCH. 12   13   14   15   16   17   18   19   19   19   19   19   19   19	87 94 100 100 83 80	86 89 100 100 82 84	73 80 100 91 73 58	79 86 93 90 85 62	84 77 91 84 85 64	66 82 79 74 80 65	74 88 87 73 75 63	87 85 100 74 74 73	83 87 70 72 65 79	94 76 73 72 67 90	81 91 70 77 68 93	84 100 68 68 70 94
21 22 23 24 25	100 86 90 83 84 86	100 92 90 81 77 86	100 93 83 74 71 76	99 94 76 78 72 71	84 88 72 71 65 79	88 73 71 61 77 82	82 66 77 76 82 85	96 72 77 75 85 82	99 65 77 76 77 81	100 65 75 76 79 74	97 60 80 75 81 74	99 66 79 76 88 76
26 27 28 29 30 31	94 96 97 80 96	94 91 94 75 93	96 90 86 75 86	96 65 75 69 82	96 67 73 74 77	61 63 70 74 73	62 64 71 76 73	59 64 68 80 78	61 65 65 71 82	65 73 48 68 87	66 69 48 69 90	68 72 53 72 95
lourly Means	92	92	87	84	82	77	77	79	77	77	77	80
$\left \begin{array}{c}1\\2\\3\\4\end{array}\right $	In. •074 •069 •107 •098	In. •067 •071 •108 •098	In. •072 •080 •104 •106	In. '076 '083 '107 '110	Iu. *080 *095 *111 *115	In. •084 •080 •120 •114	In. *087 *098 *126 *113	In. •092 •102 •128 •106	In. '084 '116 '134 '117	In. 105 112 128 118	In. '084 '110 '124 '110	In. :09 :10 :10 :10
5 6 7 8 9 10	•105 •101 •178 •123 •087 •097	113 110 171 122 1090 101	109 127 188 129 1089	·108 ·149 ·189 ·133 ·094 ·108	·115 ·168 ·199 ·135 ·094 ·113	128 164 202 116 119	·123 ·176 ·187 ·125 ·101 ·148	129 172 208 120 108 164	·149 ·187 ·213 ·120 ·134 ·137	117 181 245 123 108 134	128 161 217 125 120 138	13 18 20 12 10
MARCH. 12 13 14 15 16 17 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19	·116 ·073 ·055 ·080 ·110 ·089	117 1068 1057 1084 1114 107		106 1074 1062 103 116 106	·108 ·072 ·069 ·103 ·116 ·115		101 1052 1079 103 107 123	121 1080 1093 1117 106 148	118 1079 1070 1112 1094 1157	120 166 074 115 099 170	104 1074 1070 1121 1101 1172	· 10 · 07 · 06 · 10 · 10 · 16
21 22 23 24 25	·139 ·214 ·154 ·162 ·132 ·183	148 220 163 160 140 188	173 219 164 152 150 192	184 239 161 158 159	169 248 158 161 154 188	175 230 157 147 182 195	168 220 171 188 195 202	191 244 171 192 205 198	·201 ·226 ·169 ·184 ·176 ·208	·208 ·225 ·169 ·188 ·185 ·214	·209 ·202 ·177 ·181 ·192 ·213	·21 ·20 ·16 ·18 ·19 ·21
26 27 28 29 30 31	·178 ·144 ·176 ·153 ·204	178 149 198 167	181 170 224 178 232	-163 •141 •224 •174 •270	·167 ·165 ·237 ·189 ·290	·132 ·173 ·235 ·190 ·314	154 158 1257 200	152 180 263 201	159 196 303 194 393	-164 •212 •225 •198 •468	-158 -199 -233 -205 -455	·15 ·20 ·25 ·21 ·44

		н	MIDITY	OF THE A	IR, AND	TENSION	OF THE	ATMOSPH	ERIC VAI	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
84	82	93	100	100	100	100 100	100	100 100	100 100	100 100	100 100	94 98
100 76	$\frac{100}{84}$	100 85	100 88	100 91	100 91	100 85	100 88	91	90	89	95	91
97	97	100	100	98	100						— )	94
7.4	93	95	100	100	96	100 100	100 100	100 100	91 100	76 100	86 }	90
$\begin{array}{ c c }\hline 74\\ 72\\ \end{array}$	79	81	79	79	76	79	79	74	77	79	80	79
97	99	99	99	100	99	99	97	83	87	85	88	86
77 70	$\frac{90}{78}$	83 84	86 95	88 95	84 100	84 100	85 100	78 100	83 100	89 100	97	86 87
90	87	84	87	99	81		<u> </u>			l	— 7	83
-				-		100	77	80	78	79 94	87 } 93	87
75 96	$\frac{98}{93}$	$\frac{85}{93}$	88 100	$\begin{array}{c c} 95 \\ 100 \end{array}$	98 100	100 100	98 100	94	93 100	100	100	$\frac{87}{92}$
80	80	83	97	96	96	100	100	100	100	100	100	90
62	61	70	69	74	73	75 86	85 85	85 100	87 94	80 91	82 86	78 83
70 97	94 80	96 84	97 80	97 91	95 91		80	100	94	<u></u>	- 7	1
-				l —		93	99	100	100	100	100 }	84
99	99 71	99 75	100 78	100 88	100 86	100 90	100	98 91	93 90	90 89	90 89	96 80
$\begin{bmatrix} 72 \\ 85 \end{bmatrix}$	71 88	96	18 88	90	91	89	86	94	89	86	82	84
76	74	84	90	91	89	87	87	89	81	89	84	80
90 81	$\frac{85}{82}$	82 87	88 92	84 91	84 93	83	83	88	86	83	86	82
- 01		-	52	<u></u>		72	71	72	71	72	$\left\{\begin{array}{c} \overline{72} \end{array}\right\}$	80
75	80	88	86	88	88	100	87	89	88	89 92	91	82
78 57	$\begin{array}{c} 80 \\ 64 \end{array}$	84 70	84 77	85 80	78 83	89 91	96 96	86 94	98 90	92 96	90	80 77
78	82	86	87	89	92	93	94	96	98	99	96	82
99	99	100	100	89	89	88	88	86	88	83	84	88
82	85	88	90	92	91	92	92	91	91	90	91	86
In.	In.	In.	In. •068	In. 081	In. •080	In. •065	In. •051	In. •060	In. •069	In. •070	In. '07:2	In. •077
.080 .095	$075 \\ 093$	·079 ·093	.096	.095	.098	.103	105	•108	.111	.111	1111	097
.092	.099	.091	•091	•092	.090	.089	.091	104	104	104	.100	106
100	.097	.101	.101	.101	.099	•111	115	•120	104	•092	$\left\{ \frac{1}{109} \right\}$	.106
136	$\cdot \overline{137}$	•122	115	115	.111	.102	103	.103	104	.105	.099	117
175	186	184	185	186	181	183	183	·178 ·138	178 137	·180 ·131	178 132	.169 .187
201 117	·200 ·133	197 121	196 125	·200 ·122	·194 ·115	·189 ·113	175 113	.091	*096	•093	·098	107
107	109	107	.110	.109	.113	.113	.106	.103	.099	•096	.100	105
159	145	140	144	.160	137		•132	•128	.118	113	$  \cdot \cdot_{117}^{-} \}$	132
.084	105	.088	.088	.090	.090	.090	.085	.081	.079	.079	.077	.098
'064	*060	.090	.062	.062	·062	.062	.060	•058	.057	058	.056	.071
.071 .095	.067 .092	.068 .102	·074 ·101	.071 .108	.069 .106	.071 .107	·070 ·118	·069	·067 ·117	·073 ·110	.076 111	.069 .105
101	120	113	1113	107	.100	.094	.087	.096	.096	.092	.094	104
172	140	149	140	155	153	-144	-195	•140	138	135	$-\frac{1}{133}$	•138
.216	.216	•212	•213	207	•205	·144 ·208	135 209	·140 ·215	·258	$^{155}_{252}$	250	.202
185	163	165	164	.109	164	.160	164	•156	155	147	147	.191
172	171	179	164	164	169 142	165 139	162 137	·172 ·138	167 130	165 135	.160 .130	·166 ·158
166 18 <b>5</b>	`155 `168	·157 ·165	155 179	149 174	142	180	137	185	182	180	184	175
221	•223	•232	•237	•232	•235			148		140	140}	.193
162	•163	•171	164	154	152	158 163	150 144	138	142 138	138	138	157
210	206	.211	•211	213	•208	207	•204	•203	.210	195	186	.191
250	<b>.</b> 210	201	194	188	182	·176 ·214	·173 ·213	·164 ·213	·160 ·211	$^{\circ}_{208}$	:153 :200	$^{:210}_{:200}$
·212 ·407	·204 ·367	·208 ·343	·210 ·338	215 287	·214 ·225	196	192	·180	179	166	167	292
157	152	150	150	146	•143	140	135	134	134	.131	130	146

		HUMI	DITY OF	THE AIR,	, AND TE	NSION OF	THE AT	MOSPHER	IC VAPO	UR.		
dours of Mean Göttingen Tice.	0	1	2	3	4	5	6	7	8	9	10	11
Hours of Mean Toronto Time.	18	19	20	21	22	23	0	1	2	3	4	5
1 2 3 4 5 6	78 	90 	85 	85 <del></del>	82 	82 	79 	78 	78 	$     \begin{array}{c c}       74 \\       \hline       79 \\       94 \\       73 \\       62     \end{array} $	$   \begin{array}{r}     71 \\     \hline     70 \\     94 \\     65 \\     62   \end{array} $	72 69 96 66 49
10       11       12	73 80  86 68	69 78 — 77 56	60 56 	53 54 — 60 45	62 50 57 47	65 55 	64 54 	59 55 	$   \begin{array}{r}     62 \\     54 \\     \hline     47 \\     61 \\   \end{array} $	57 51 	$   \begin{array}{c c}     57 \\     51 \\     \hline     52 \\     62 \\   \end{array} $	59 50 
APRIL. 12 12 13 14 15 15 15 16 17 17 17 17 17 17 17 17 17 17 17 17 17	93 75 90 72 — 72	83 69 91 67 — 65	$     \begin{array}{r}       67 \\       68 \\       89 \\       75 \\       \hline       64     \end{array} $	66 65 86 61 —	$   \begin{array}{r}     63 \\     66 \\     75 \\     52 \\     \hline     57   \end{array} $	$ \begin{array}{c c} 64 \\ 72 \\ 72 \\ 47 \\ \hline 52 \end{array} $	68 84 69 45 — 49	58 73 74 44 — 66	57 82 79 43 —	57 82 79 38 —	60 82 80 • 41 ————————————————————————————————————	69 88 82 35 
AtpumpH 16 17 18 19 20 21 a 22	55 96 87 <del></del>	59 99 78 — 76	63 86 51 —	61 64 63 —	61 68 64 —	60 66 66 —	65 64 69 —	$ \begin{array}{c c} 64 \\ 70 \\ 60 \\ \hline 62 \end{array} $	92 60 71 —	$ \begin{array}{c c}     \hline             100 \\             70 \\             \hline             68 \\             \hline             72 \end{array} $	100 67 70 	98 67 67 — 65
23 24 25 26 27 28 29 30	61 87 86 96 79 99	61 76 70 71 38 83	61 72 66 76 72 74	71 73 61 71 74 74	72 64 64 70 68 68	71 63 66 65 63 65 —	55 60 62 63 64 60	50 63 60 87 53 56	50 65 54 52 47 48	48 74 55 46 52 44	50 70 59 47 64 38	79 58 51 68 42
lourly Means	82	75	70	67	65	64	65	64	64	65	64	65
Tension of the Vapour.  (1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	In. 151  166 238 184 128 152 133  198 214 168 165 202 181  139 108 138 133  200 129 137 164 158 185 267	In. 176	In. 165 -209 255 157 150 157 155 -229 188 186 163 213 228 -140 128 156 122 - 206 -136 154 154 207 188 211	In. 165	In. 165	In. 179 -228 271 136 180 201 187 -341 167 234 179 203 200 -138 135 142 185 -199 -196 175 191 229 191	In170 -220 -284 -202 -210 -192 -193313 -191 -245 -208 -208 -208 -208 -203155 -219157 -180 -186 -221 -187 -197	In. 167	In. 168 -224 318 198 202 181 214 - 279 238 205 238 195 - 182 145 244 - 234 - 137 196 180 204 159 168 -	In. 163 -234 300 190 203 174 210 -286 216 226 229 173 -181 161 160 245 -245 -133 208 172 189 183 160 -	In150 -232 -285 -168 -209 -169 -204 -294 -294 -292 -231 -199 -238 -180153 -234220 -134 -203 -190 -184 -213 -138138	In. 148 -227 -278 -176 -177 -175 -200 -241 -200 -166 -166 -224 -115 -206 -181 -182 -144

[•] Good Friday.

		HU	MIDITY (	OF THE A	IR, AND	TENSION	OF THE .	A'TMOSPH	ERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means,
78 73 94 63 47 64 50	83 73 94 84 55 66 	88 	88 	94 75 86 86 68 86 76	94 	90 69 88 88 70 79 93	85 73 90 87 78 78 —	88 73 94 89 73 79 84 61	92 78 96 93 73 77 91 63	93 75 96 90 74 78 — 86 77	96 } 80 100 89 83 84	84 76 93 79 67 69 68 62
55 64 72 95 93 35 61 81 70	53 73 68 91 87 45 74 84 73	55 70 72 88 86 50 71 87 78	63 69 66 88 86 55 71 92 74	73 81 67 90 86 57 70 94 73	72 84 87 93 87 59 ———————————————————————————————————	70 68 91 91 96 — 65 56 86 91	61 75 88 92 88 — 69 75 62 99	$   \begin{array}{c}     88 \\     87 \\     94 \\     71 \\     \hline     72 \\     68 \\     87 \\     100   \end{array} $	90 82 94 71 — 73 68 86 80	96 74 94 72 — 73 66 88 87	94 74 92 83 ———————————————————————————————————	67 72 83 82 57 65 80 79
62 	68 	75 	76 	74 57 64 74 86 79 90 65	74 	66 59 73 56 94 80 97 —	56 -62 77 77 94 82 97 -78	64 68 77 76 89 88 99 88	69 72 88 79 91 91 99 — 81	71 74 92 86 97 88 99 80		69 67 68 72 73 72 78 66
67	71	74	75	77	79	79	80	81	82	83	85	73
In. 158 -226 -259 -162 -157 -188 -231 -275 -210 -239 -198 -239 -144 -166 -166 -166 -163 -199 -227 -173	In. 159	In. 164	In164229 -211 -164 -163 -164 -189230 -241 -218 -194 -195 -162167 -157 -148 -190 -147159	In. 170 — 195 195 165 159 177 192 — 249 286 227 195 210 167 — 164 155 128 178 — 142 — 130	In. 168	In	In	In	In	in	In	In. 166 220 230 163 170 165 192 260 206 224 191 209 176 157 133 146 194 186
208 147 194 245 142 - 196	189 133 187 238 149	*181 *182 *174 *242 *150 —	189 181 185 240 146	185 186 185 253 151 —	143 171 179 259 146 —	160 162 181 265 - 174	180 146 183 265 — 166	*163 *140 *189 *207 *165	158 140 193 265 — 164	155 142 192 263 - 187	144 140 190 264 -184}	176 165 191 217 176
130	.193	100	100	100	102	101	111	117	710	117	717	100

Göttir	f Mean	0	1	2	3	4	5	6	7	8	9	10	11
Tim Iours of Toro	f Mean	18	19	20	21	22	23	0	1	2	3	4	5
Tim	ne. )				<u> </u>	<u> </u>	1 20				1 3	4	)
	$\left( \begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{array} \right)$	80 98 88 83 89 96	81 98 87 73 84 87	80 94 76 68 85 84	82 81 75 59 79 79	78 77 68 60 77 74	77 82 66 58 72 72	74 81 60 62 72 72	86 81 59 62 68 72	92 78 52 64 66 75	91 77 54 69 68 72	93 73 50 72 67 71	92 73 41 80 83 73
AII.	8 9 10 11 12 13 14	84 82 94 93 65 76	66 65 89 93 62 79	61 67 79 84 59 86	61 64 69 77 59 87	57 62 72 76 52 97	53 66 73 67 50 98	51 63 73 70 46 98	52 59 74 75 45 87	52 61 74 83 45 87	51 67 72 84 54 77	55 69 74 81 56 83	55 65 76 72 59 75
MAY.	15 16	76 99 97 94 90 100	65 90 84 86 87 100	54 80 82 82 81 99	55 74 80 70 78 93	55 79 75 69 75 84	58 83 72 61 74 87	61 86 69 62 73 85	59 77 67 56 75 92	61 74 70 56 74 95	67 77 66 52 73 93	68 79 63 54 91	90 89 62 59 93 98
	22 23 24 25 26 27 28	87 82 99 90 77 81	74 83 97 92 68 80	71 77 92 87 61 75	78 67 95 83 59 72	96 66 92 81 56 70	73 66 90 75 62 74	72 68 69 74 63 74	72 70 71 72 69 68	72 72 72 64 70 57 64	72 73 58 54 51 57	72 76 62 38 51 58	73 73 74 57 51 60
	29 30 31	92 93 63	87 77 63	89 58 58	89 57 55	83 50 51	87 51 52	89 50 37	81 41 44	79 47 36	80 49 37	91 50 39	77 50 40
Iourly	Means	87	81	77	<b>7</b> 3	72	70	69	68	67	66	68	70
	1 2 3 4 5 6 7 8	In. '202 '253 '266 '259 '367 '368 — '216	In. '219 '262 '327 '251 '432 '438 '204	In. '228 '277 '320 '272 '444 '472 '214	In.	In.	In.	In.	In.	In.	In.	In. ·302 ·292 ·291 ·275 ·478 ·479	In. •296 •298 •243 •300 •460 •495
vapour.	9 10 11 12 13 14	·241 ·289 ·287 ·175 ·161	251 251 293 287 181 185	292 280 272 182 210	298 265 265 269 198 214	233 ·290 ·279 ·273 ·190 ·239	231 309 283 255 196 262	248 317 292 261 182 276	*241 *324 *309 *258 *181 *286	*235 *314 *321 *280 *186 *265	231 305 305 280 221 238	*253 *326 *309 *287 *232 *228	·248 ·289 ·308 ·265 ·242 ·200
Tension of the MAY.	.   7 ~	185 •340 •259 •343 •398 •481	206 348 322 406 411 481	*210 *336 *338 *414 *463 *550	*224 *332 *349 *416 *491 *629	*237 *374 *353 *428 *513 *595	*269 *402 *372 *396 *559 *608	· 267 · 413 · 369 · 421 · 550 · 686	264 387 379 407 544 632	· 252 · 367 · 406 · 439 · 569 · 662	·244 ·365 ·393 ·413 ·514 ·613	·245 ·393 ·375 ·421 ·540 ·584	·297 ·408 ·351 ·446 ·592 ·616
	22 23 24 25 26 27 28	·400 ·372 ·403 ·395 ·292 ·298	*316 *353 *406 *421 *279 *313	·309 ·337 ·431 ·438 ·269 ·354	· 390 · 285 · 482 · 458 · 274 · 384	·438 ·280 ·552 ·518 ·279 ·386	·389 ·280 ·571 ·526 ·331 ·405	·377 ·291 ·480 ·534 ·387 ·401	*380 *305 *532 *523 *433 *407	· 382 · 327 · 485 · 540 · 370 · 401	*384 *364 *463 *472 *313 *354	*364 *371 *506 *363 *294 *373	·395 ·370 ·480 ·462 ·300 ·357
	29 30 31	.455 .380 .177	•493 •377 •188	*493 *328 *180	·519 ·328 ·188	-581 -296 -188	·508 ·322 ·201	·629 ·324 ·154	·621 ·269 ·186	·594 ·257 ·153	·631 ·244 ·162	·669 ·232 ·176	·657 ·216 ·186
	Means	.306	•320	•330	*347	*359	*366	*373	*372				•362

		н	MIDITY	OF THE A	AIR, AND	TENSION	OF THE .	<b>A</b> TMOSPII	ERIC VA	POUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
98 72 62 79 82 84	97 77 68 77 86 87	97 83 80 77 78 88	94 84 84 79 83 78	98 89 85 80 88 78	99 93 91 77 87 77	100 73 92 79 87 91	100 75 87 80 88 —	98 80 87 80 100 74	99 91 86 88 100 — 85	98 89 89 91 97 —	$   \begin{array}{c}     97 \\     89 \\     93 \\     96 \\     97 \\     \hline     79   \end{array} $	90 83 74 75 83 79
60 79 80 63 61 81	64 79 75 57 64 83	63 91 78 53 63 85	64 95 81 56 69 84	58 97 83 55 69 83	53 99 85 57 63 83	54 99 89 58 63	74 100 94 59 74	76 100 94 62 70	81 100 97 64 69	83 100 96 62 83 	$\left\{\begin{array}{c} 76\\ 76\\ 93\\ 96\\ 62\\ 79\\ \hline 78\end{array}\right\}$	63 80 82 69 62 82
88 88 64 64 93 95	96 93 71 70 100 98	93 97 76 73 96 98	96 78 85 77 93 100	100 83 89 78 97 100	97 79 91 90 98 100	71 97 83 89 91 100 	71 100 85 97 95 100 	70 100 93 96 95 100 —	78 100 94 96 95 100 	100 94 96 97 100 —	99 87 97 95 100 ——————————————————————————————————	80 85 80 76 89 95
77 74 72 54 49 65	81 70 76 60 57 73	90 68 79 62 67 75	79 69 82 64 53 86	79 64 86 66 64 86	89 64 86 61 70 82	96 80 83 72 73 —	92 85 94 72 74 —	91 91 96 83 79 —	92 89 96 92 74 —	83 97 97 80 76 	82 95 91 90 77 —————————————————————————————————	81 76 83 72 64 78
77 49 45	80 53 47	76 61 76	83 61 82	90 64 87	88 65 76	86 62 69	86 70 79	86 62 80	88 59 84	91 69 84	95 75 82	85 59 61
72	76	79	79	81	81	82	85	87	89	89	88	77
In. •294 •284 •290 •310 •418 •446	In.	In252 -252 -280 -326 -439 -482	In. '234 '235 '270 '327 '452 '433	In. '237 '232 '253 '331 '390 '417	In232 -225 -225 -253 -325 -390 -387	In.	In. '223 '244 '242 '310 '377	In. '213 '236 '240 '311 '364	In. '216 '231 '239 '325 '349	In212 -211 -229 -327 -326	In. '213 '227 '224 '315 '316	In.
243 316 302 234 234 196	·239 ·310 ·286 ·209 ·215 ·210	·222 ·332 ·286 ·189 ·185 ·219	·223 ·330 ·282 ·191 ·177 ·220	215 330 280 181 173 220	·207 ·321 ·289 ·180 ·147 ·219	·282 ·204 ·291 ·296 ·180 ·141	196 232 272 305 180 142	180 218 298 303 177 138	186 208 303 304 175 140	185 210 302 300 163 149	189 ) 200 268 300 162 154	·226 ·301 ·294 ·229 ·182 ·208
284 381 315 458 586 602	309 369 313 417 521 609	*281 *344 *316 *374 *428 *543	·292 ·299 ·320 ·354 ·457 ·450	301 280 312 346 472 466	·299 ·255 ·305 ·351 ·472 ·500	187 304 246 309 343 464	167 316 228 315 338 458	148 319 219 306 334 456	150 319 223 286 334 450	145 315 208 279 341 434	*317 *204 *279 *349 *443	· 273 · 322 · 330 · 387 · 491 · 548
380 360 436 389 287 408	364 319 431 371 291 395	364 308 406 338 282 326	314 322 381 293 210 335	*322 *301 *392 *291 *247 *332	372 •295 •384 •262 •250 •323	*489 *368 *345 *367 *287 *252	*488 *379 *359 *369 *280 *252	*483 *375 *398 *367 *300 *252	·477 ·373 ·389 ·351 ·306 ·242	*461 *351 *431 *351 *258 *242	·439 ·350 ·413 ·369 ·280 ·246	*368 *341 *433 *388 *286
-666 204 194	 -592 -203 -198	*504 *212 *265	·464 ·210 ·267	·450 ·222 ·247	323  398 223 230	•408 •358 •197 •246	•407 •353 •199 •218	·403 ·347 ·186 ·206	•400 •331 •174 •209	·305 ·317 ·187 ·202	·382 } ·314 ·198 ·205	*369 *498 *250 *201
352	*339	*324	*309	*305	•300	•296	<b>·2</b> 91	*288	•285	·276	·278	*328

			HUMI	IDITY OF	THE AIR	, AND TE	NSION O	F THE AT	MOSPHEI	RIC VAPO	UR.		
ours of Götting Time	Mean }	0	1	2	3	4	5	6	7	8	9	10	11
	vlean )	18	19	20	21	22	23	0	1	2	3	4	5
	$\left[egin{array}{c} 1 \ 2 \ 3 \ 4 \end{array} ight]$	73 83 89	56 77 92	51 74 92	47 74 90	42 71 88	36 67 87	37 62 85	29 60 83	48 58 78	54 58 77	57 63 81	57 64 83
	5 6 7 8 9 10	92 88 72 71 89 87	81 83 67 70 77 92	83 81 63 66 100 62	84 78 61 66 81 62	80 75 57 75 74 67	75 72 56 74 72 68	73 64 56 75 66 69	86 65 51 74 62 71	83 61 49 77 60 67	86 62 49 75 61 77	69 57 50 71 63 72	75 55 49 80 72 72
Humidity of the Air. JUNE.	18 19	66 61 81 90 79 89	57 45 79 81 72 83 —	48 46 80 83 66 77 ————————————————————————————————	45 38 76 82 62 76 ————————————————————————————————	38 36 71 75 58 72 ———————————————————————————————————	34 34 63 48 69 68 — 85	37 30 67 46 47 68 — 84	39 28 80 41 63 72 	39 23 70 36 58 78 —	44 26 59 34 56 66 — 85	42 27 66 31 62 75 — 82	40 27 69 31 60 71 
Ŧ (	20 21 22 23 24 25	95 90 91 99 83	93 89 86 100 <b>75</b>	83 92 79 100 65	77 89 81 99 57	79 76 85 96 45	86 76 80 94 42	89 71 78 84 36	82 69 73 80 31	80 65 75 54 30	78 62 72 63 32	77 59 72 49 26	87 61 78 65 25
	26 27 28 29 30	91 88 99 78 89	78 87 100 74 82	68 79 94 72 81	74 74 96 74 81	70 75 89 73 79	66 77 90 71 71	64 75 73 70 69	60 77 75 72 52	58 71 69 71 57	55 72 73 71 62	58 72 67 66 60	59 71 59 72 61
Hourly	Means	85	80	76	73	70	68	64	63	61	62	61	63
	$\begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix}$	In. •230 •280 •560	In. •205 •329 •560	In. •204 •359 •560	In. 197 390 581	In. *182 *411 *583	In. 174 1423 1581	In. •189 •418 •590	In. •156 •419 •580	In. •254 •417 •575	In. 287 409 571	In. :313 :398 :577	In. •338 •425 •565
	5 6 7 8 9 10	·396 ·291 ·230 ·276 ·373 ·445	397 304 234 311 401 481	·464 ·303 ·236 ·342 ·540 ·395	·472 ·305 ·244 ·361 ·497 ·435	·468 ·289 ·252 ·438 ·482 ·507	*479 *289 *266 *449 *492 *485	·478 ·283 ·287 ·437 ·485 ·488	·438 ·292 ·276 ·435 ·472 ·517	·419 ·266 ·278 ·449 ·473 ·511	·496 ·276 ·284 ·460 ·492 ·534	·473 ·256 ·272 ·481 ·518 ·476	·419 ·232 ·268 ·452 ·526 ·519
Tension of the Vapour. JUNE.	12 13	·222 ·192 ·237 ·474 ·621 ·571	201 155 235 235 531 624 647	178 176 1278 640 644 675	173 152 314 668 659 665	161 162 310 702 667 717	144 164 341 564 766 728	164 157 333 578 593 740	174 154 363 549 706 692	176 127 378 510 686 688	201 141 366 492 681 695	193 148 408 433 655 679	· 179 · 145 · 401 · 423 · 655 · 696
Tensı	19 20 21 22 23 24	•574 •526 •438 •416 •518 •407	·596 ·571 ·497 ·432 ·544 ·407	.592 .592 .489 .512 .572 .390	·664 ·598 ·517 ·551 ·584 ·346	·676 ·638 ·478 ·539 ·625 ·304	708 630 463 531 672 302	·711 ·674 ·464 ·541 ·636 ·269	*680 *615 *466 *550 *665 *243	·651 ·605 ·440 ·528 ·497 ·239	659 579 436 518 486 260	·676 ·597 ·443 ·509 ·384 ·203	· 648 · 456 · 443 · 476 · 434 · 197
	25 26 27 28 29 30	·494 ·453 ·682 ·401 ·433	·544 ·533 ·667 ·443 ·447	.580 .573 .689 .503 .540	.615 .608 .706 .564 .551	·633 ·626 ·677 ·559 ·571	•628 •626 •657 •538 •575	 •643 •649 •535 •551 •541	•629 •675 •544 •578 •489	·613 ·654 ·516 ·586 ·520	.589 .638 .554 .590 .563	.608 .657 .508 .570 .543	· 595 · 552 · 441 · 573 · 568
lourly 1	Means	·413	·434	•463	*478	•487	·488	·478	•475	•464	·471	•461	•447

		ни	MIDITY (	OF THE A	IR, AND	rension	OF THE A	ATMOSPII:	ERIC VAI	OUR.		
12	13	14	15	16	17	18	19	20	21	22	23	Daily and Monthly
6	7	8	9	10	11	12	13	14	15	16	17	Means.
60 66 84	59 74 84	71 81 90	75 79 94	79 84 95	84 82 97	90 80 —	88 90 — 82	88 92 <del>-</del> 83	85 93 <del></del> 83	83 93 — 90	$\begin{bmatrix} 88 \\ 93 \\ \hline -7 \\ 97 \end{bmatrix}$	64 76 87
85 56 50 79 76 74	82 59 44 82 72 59	77 62 53 88 59 67	78 64 55 88 58 75	90 65 54 90 57 77	89 90 56 93 56 73	$   \begin{array}{c}     81 \\     84 \\     90 \\     59 \\     94 \\     \hline     60 \\     \hline     75   \end{array} $	$   \begin{array}{r}     82 \\     96 \\     88 \\     66 \\     95 \\     \hline     61 \\     \hline     74   \end{array} $	90 86 77 95 59 —	94 89 69 97 82 <del>7</del> 9	96 96 73 97 82 —	$     \begin{array}{c c}                                    $	84 74 59 82 70
41 32 70 39 58 78	45 39 84 41 67 81	51 40 84 71 68 87	71 41 84 72 86 80	69 57 86 75 88 89	64 77 87 82 89 89	84 78 87 84 90 —	86 86 87 80 91 —	72 87 92 77 96 —	72 80 94 58 95 —	72 80 91 76 96 —	71 79 95 87 96 —	55 50 79 63 74 83
82 89 54 75 67 28	88 89 61 78 69 36	92 94 65 82 76 45	94 96 65 79 78 46	90 96 83 81 85 56	85 97 89 87 82 64	96 86 92 93 89 87 —	93 95 90 100 87 —	94 96 90 94 88 —	93 96 94 96 91 —	95 92 96 97 92 —	87 97 96 95 90 	88 89 78 83 82 57
64 78 66 79 71	71 80 70 82 74	79 94 73 95 79	81 98 77 97 72	85 97 77 95 88	87 96 79 93 86	94 98 89 97 94	96 100 87 97 98	95 100 90 96 96	96 100 93 95 88	96 100 96 96 88	97 98 91 86 86	77 86 8. 82 78
65	68	74	76	76	83	86	89	89	89	90	90	75
In. :303 :424 :547	In. •288 •437 •485	In. •266 •440 •500	In. •239 •392 •486	In. •255 •439 •476	In. •267 •463 •449	In. •264 •470	In. •260 •470 —	In. •249 •444 —	In. •247 •464 —	In. •227 •490 — •375	In. •236 •533 •344}	In. •243 •423 •511
385 232 270 393 509 533	·378 ·227 ·221 ·398 ·447 ·414	·328 ·229 ·235 ·403 ·373 ·402	·326 ·233 ·218 ·400 ·366 ·417	·338 ·207 ·214 ·398 ·348 ·362	·323 ·265 ·216 ·389 ·334 ·315	·429 ·297 ·254 ·225 ·390 ·341	*298 *238 *238 *355 *336	283 230 254 345 318 	*280 *227 *237 *338 *387 —	284 264 244 323 378 	*288 *288 *248 *325 *385 *385 *224	*384 *262 *248 *390 *428 *403
178 159 419 493 729 651	·176 ·171 ·476 ·477 ·652 ·594	·181 ·173 ·402 ·615 ·622 ·567	·210 ·170 ·365 ·547 ·602 ·540	196 207 355 535 604 557	-193 •233 •353 •572 •595 •552	·262 ·213 ·234 ·342 ·582 ·575 —	*248 *198 *237 *335 *623 *546 — *545	192 230 329 602 540 	192 192 205 312 517 507 —	193 203 340 552 478 - 522	199 198 361 585 482	187 179 348 553 620
.607 .521 .387 .457 .436 .206	· 598 · 502 · 396 · 463 · 409 · 237	*572 *513 *370 *446 *403 *234	·564 ·508 ·360 ·427 ·397 ·226	. 543 . 492 . 384 . 430 . 402 . 229	 • 523 • 465 • 379 • 430 • 377 • 247	*547 *525 *425 *363 *445 *400	'513 '422 '358 '470 '405	·488 ·385 ·361 ·473 ·403	·472 ·371 ·366 ·478 ·403	*478 *385 *371 *512 *395	*476 *400 *386 *508 *390 	*591 *520 *419 *485 *477
.502 .580 .474 .579 .585	·481 ·641 ·485 ·542 ·559	-471 ·665 ·472 ·568 ·566	·453 ·634 ·450 ·461 ·523	·477 ·615 ·436 ·429 ·600	·499 ·570 ·416 ·410 ·578	*443 *497 *573 *415 *405 *563	*442 *496 *632 *390 *389 *550	*423 *477 *623 *395 *362 *528	*431 *428 *621 *397 *344 *468	*428 *428 *632 *392 *368 *413	*466 *676 *379 *370 *341	*535 *613 *512 *487 *526
*445	•429	•424	·404	•405	•401	•403	·401	*391	*382	*381	·386	`434

				DI	RECTIC	N AND FOR	CE OF	THE WIND.					
Mean Gö		Oh.		1h.		2h.		3h.		4h.		5h.	
Tim	ne.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{bmatrix} 1\\2\\3 \end{bmatrix}$	E. — N.W.	lbs. 1.5 0.0 0.5	E. — N.W.	lbs. 1.5 0.0 0.2	E. W.N.W.	1°5 0°0 0°2	E. N.W. by W.	lbs. 1.5 0.0 0.2	S.W. by S.	1°5 0°5 0°0	E. S.W. by S. W. by S.	lbs. 1.5 2.0 0.2
	4 5 6 7 8 9	S.W. N. by E. E. — S.W.	0.5 0.5 0.0 0.0 0.0 0.5	S.W. N.E. E. W.S.W.	0.2 0.2 3.0 0.5 0.0 0.5	N.N.E. E. W.S.W. S.W. by W.	0.0 0.2 2.5 0.0 0.0 0.5	S.W. by S. E.N.E. E. by N. W.S.W. N.W. by N. S.W. by W.	0.2 0.2 2.0 0.5 0.5	S.W. N.E. E. W. by S. W.N.W. S.W. by W.	0°2 0°2 1°0 0°5 0°5	W. by S. N.E. E. W. by S. N.N.W. S.W. by W.	0.2 0.2 1.0 0.5 0.5 1.0
JANUARY.	11 12 13 14 15 16 17	S.W. N. by W. N.	0.0 0.0 1.0 0.0 0.2 0.2	S.W. S.S.W. N. by W. N. by W.	0.0 0.0 1.0 0.2 0.2 0.2	N.N.W. N.W. S.W. S.S.W. N. by W. N. by W.	0.2 0.2 1.0 0.2 0.2 0.2	N.N.W. N. S.W. S. by W. N.N.E. N.	0.5 0.2 1.0 0.2 0.2 0.2	N.N.W. W. S.W. by W. S. by W. N. by W. N. by W.	0.5 0.2 0.5 0.2 0.2 0.2	N.N.W. W.N.W. S.W. by W. S. by W. N. by W. N.W. by N.	0.2 0.2 0.2 0.2 1.0
JA	18 19 20 21 22 23 24	N. by W. N. by E. N.N.E. N.N.W.	0.5 0.5 1.0 0.0 0.0	N. by W. N. by E. N.E. N.N.W.	0.2 0.2 1.0 1.5 0.0 0.2	N. by W. N. by E. N.E. N.N.W. W. by S. S.W.	0.5 0.5 1.0 0.5 0.5 0.5	N.E. N.N.W.	0.5 0.0 1.0 0.0 0.0	N. N. E. N. N. W	0°2 0°0 1°0 2°5 0°0 0°2	N. by W.  N.N.E. N.N.W. S.W. S.W.	0.2 0.0 1.0 2.5 0.2 0.5
	25 26 27 28 29 30 31	E.S.E. E. N. by W.	0.0 0.0 0.0 0.0 0.2 0.2	S.W. E. by S. N. by W.	0.0 0.0 0.2 0.2 0.0 3.5	S.W. E.S.E. N. by W.	0.0 0.0 0.2 0.2 0.0 3.5	N. S.W. by W. E.S.E. N. by W.	0.0 0.2 0.5 0.2 0.0 3.5	S.W. by W. E.S.E. N. by W.	0.0 0.0 0.2 0.2 0.0 2.5	W. by S. E.S.E. N. by W.	0.0 0.0 0.5 0.2 0.0 2.0
(continue	ed)					·				1		ı	
Mean Gö		12h.		13h.		14h.		15h.	1	16h.		17h.	
Tim	ie.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	W. by N.	1.2 1.0 0.0	W. by N.	lbs. 1 ° 0 0 ° 5 0 ° 0	E. W.	1bs. 1°0 0°5 0°0	E. W.	lbs. 0.5 0.5 0.0	E. W.	1 bs. 0 5 1 5 0 0 0 —	E.S.E. W.	lbs. 0.5 1.0 0.0
	4 5 6 7 8 9	E.N.E. N.W. W.N.W.	0.0 1.0 0.5 1.0 0.0 1.5	E.N.E. S.W. W.N.W. W.N.W. S.W.	0.0 1.5 0.2 0.2 0.2 1.0	E.N E. S.W. W.N.W. W.N.W. W.S.W.	0.0 2.5 0.2 0.2 0.2 0.5	E.N.E. S.W. N.W. by W. S.W.	0.0 2.5 0.2 0.0 0.2 0.5	E.N.E. S.W. — S.W.	0°0 2°5 0°2 0°0 0°5	E.N.E. S.W.  S.W.	0.0 3.5 0.2 0.0 0.0 0.5
JANUARY.	11 12 13 14 15 16 17	N.W. by N.	0.5 0.0 0.0 0.2 0.5 2.0	N.W.	0.5 0.0 0.0 0.0 0.5 2.5	N.N.W. S.W. — N. by W. N.W. by N.	0.5 1.0 0.0 0.0 0.5 1.5	N.W. by N. S.W. S.S.W. N.	0.2 1.5 0.2 0.0 0.5 0.5	N.W. S.W. — N. by W.	0.5 0.0 0.0 0.0	N.W.  W.N.W. N. by W.	0.0 0.0 0.0 0.2 0.2
JA	18 19 20 21 22 23 24	N. by W. N.W. by N. S.W.	0.0 0.0 0.2 0.0 0.0 0.0	N.E. N. by N. S.W.	0'2 0'0 0'5 1'5 0'0 1'0	N.N.E. E. by N. N. N.W. by N. S.W.	0°2 0°2 3°0 1°5 0°0 1°0	N.N.E. E. by N. N. by W. N.W. by N. W.S.W. S.W.	0°2 1°5	N. by E. N.N.E. N. by W. N.W. by N. W.S.W. S.W.	0.2 0.2 3.0 0.5 0.2 0.5	N. by E.  N.N.W. N.W. by N. W.S.W. S.W.	0.2 0.0 2.5 0.5 0.2 0.5
	25 26 27 28 29 30 31	E. by N. N.E. by N.	0.0 0.0 0.0 0.2 0.0 0.2	N.E. by E. S.S.W. E. by N. N.N.E.	0.2 0.0 0.2 0.0 0.2	N.N.E. S.S.W. E. N.N.E.	0.5 0.2 0.0 0.2 0.0 0.2	S.W. E.S.E. N.W.	0.0 0.2 0.0 0.2 0.0	S.W. by W. E.S.E. N.N.W.	0.0 0.2 0.5 0.0	N.N.E. S.W. by W.	0.0 0.0 0.0 3.0 0.0

				DIRE	CTION	AND FORC	E OF T	HE WIND.				3	
6 ^h .		7 ^h .		8h.		9 ^h .	-	10h.		11 ^h .			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	<u></u>	lime.
E. S.W. by S. W. by S.	lbs. 1 · 5 2 · 5 0 · 2	E. S.W. W.	lbs. 1.5 1.0 0.2	E. S.W. W.N.W.	lbs. 1 · 5 0 · 5 0 · 2	E. S.W. W.N.W.	lbs. 1 · 5 0 · 5 0 · 2	E. S.W. W.	lbs. 2.5 0.5 0.2	S.W. by W.	1bs. 2.0 0.2 0.0	1 2 3 4	
W. N.E. E. W. by S. N.N.W. W.S.W.	0.2 0.2 1.0 0.5 0.5	W. N.E. by N. E. W. N.W. by W. W.S.W.	0°2 0°5 1°0 1°5	S.S.W. E.N.E. E. W. N.W. by W. S.W.	0.2 0.5 0.5 0.5 0.2 1.0	S. by W. N.E. by E. E. W. by N. W.S.W. S.W.	0.2 0.5 0.5 1.0 0.2 2.0	E.N.E. N.N.E. W. by N. W.S.W. S.W.	0.0 0.5 0.5 1.0 0.2 2.5	E.N.E. N. by E. W. by N.	0.0 1.0 0.2 1.0 0.0 2.5	5 6 7 8 9	
N.W. W. by N. W.S.W. S. by W. N.N.W.	0.2 0.5 0.5 0.2 0.2 2.5	N. W. W.S.W. S. by W. N.N.W. N.N.W.	0.2 0.5 0.5 0.2 0.2 2.5	N. by W. W. by S. S.W. N. by W. N.N.W.	0.2 0.5 0.5 0.5 0.2 2.0	N. W. W. S.W. N. by W. N.N.W.	0.2 0.5 0.2 0.2 0.2 0.5 1.5	N.W. by N. W. by N. W.S.W. S.W. N.	0.2 0.5 0.2 0.2 0.5 2.5	N.W. by N. W. by S.  N. N.N.W.	0.2 0.2 0.0 0.0 0.0 0.5 2.5	11 12 13 14 15 16 17 18	JANUARY.
N.E. by N. N.W. by N. S.S.W. S.W.	0'2 0'0 1'0 2'5 0'2 0'5	N.N.E. N.N.E. N.W. by N. S.S.W. S.W.	0.2 0.0 0.5 2.5 0.2 1.5	N. by E.  N. N.N.W. S.W. by S. S.W.	0.2 0.0 0.5 1.5 0.2 2.5	N. by E.  N. by W.  N.W.  S.S.W.  S.W.	0.2 0.0 0.5 2.0 0.2 1.5	N. by W. N.W. S.W. S.S.W.	0.0 0.0 0.2 1.0	N.E. N. by W. N.W. S.S.W.	0°2 0°0 1°0 3°5 0°0 1°0	19 20 21 22 23 24 25	J.
W. by S. E.S.E. N.	0.0 0.0 0.2 0.0 1.0	S. W. by S. E.N.E.	0.0 0.2 0.5 0.2 0.0 0.5	S. by W. W.S.W. E. N. by E.	0.0 0.2 0.2 0.0 0.5	S. by W. W.S.W. E. by N.	0.0 0.2 0.2 0.0 0.5	S.S.W. S.W. E. by N. N.N.E.	0.0 0.2 0.2 0.0 0.5	S.W. E. by N. N.E.	0.0 0.0 0.2 0.2 0.0 0.2	26 27 28 29 30 31	
18h.		19 ^h .		20 ^h •		21 ^h .		22 ^h .		23 ^h .		Mean	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		Fime.
E.S.E. W.	lbs. 0°2 1°0	W.N.W.	3.0 3.0	N.W.	lbs. 0°0 2°0	N.W.	lbs. 0.0 1.0	N.W.	1 o 1 o 1 o	N.W.	0.0 1.0	$\begin{bmatrix} 1\\2\\3 \end{bmatrix}$	
E.N.E. W.S.W.	0.0 0.0 4.0 0.2 0.0 0.0	N.N.E. E.N.E. W. by S.	0'0 0'2 4'0 0'2 0'0 0'0	N. by E. E.N.E. W.S.W.	0.0 0.2 4.0 0.2 0.0 0.0	N. by E. E.N.E. S.W.	0.0 0.2 3.5 0.2 0.0 0.0	N. by E. E.N.E. W. by S. N.W. S.W.by W.	0.0 0.2 3.5 0.2 0.2 0.5	S.W. N. by E. E.N.E. W. by S.  S.W. by W.	0°2 0°2 3°5 0°2 0°0 0°2	4 5 6 7 8 9	
N.W. by N. N.W. S.W. N. by W. N.	0.5 0.2 0.0 0.2 0.0 0.2	N.W. by N.	0.5 0.0 0.0 0.0 0.0 0.2 0.0	N.N.W. S.W. by S.  N. by E. N. by W.	0.5 0.0 1.5 0.0 0.2 0.2	N. by W. S. W. by S. N. W. N. by W.	0.5 0.0 1.5 0.2 0.2 0.2	N. by W. S.W. by S. W.N.W. N. by E.	0.2 0.0 0.2 0.2 0.0	S.W. W. by S. N. by W.	0.0 0.0 2.0 0.2 0.2 0.0	10 11 12 13 14 15 16 17	JANUARY.
N. by E. N. by E. N.N.W. S.W. by W.	0.5 0.2 0.2 2.0 0.0 0.2	N. N. N.E. N. by W.	0.2 0.2 0.2 0.0 0.0	N. N. N.N.E. N. ————————————————————————	1	N. by W. N. by E. N.N.E. N.N.W.	0.2 0.5 2.5 0.0 0.5	N. by W. N. by E. N.N.E. N. W.S.W.	0.2 0.5 1.5 0.0 0.5	N. by W. N. by E. N.N.E. N.N.W.	0.2 0.2 1.0 1.0 0.0 0.2	18 19 20 21 22 23 24	JA
S.W. by W.  N. by W.	0.0 0.0 0.2 0.0 0.0 0.0 2.5	S.W. by W. S. by E. N. by W.	0.0 0.0 0.5 0.5 0.0 3.0	N.E. S.W. by W. N.E. N. by W.	0.0 0.2 0.2 0.0 0.2 3.0	N.E. S.W. by W.	0.0 0.2 0.2 0.0 0.0 3.0	S.W. by W. E.S.E. E.N.E. N. by W.	0.0 0.0 0.5 0.5 0.5 3.0	E.S.E. E. by N. N. by W.	0.0 0.0 0.0 0.2 0.2 3.0	25 26 27 28 29 30 31	

	.		1	~ 1101101	1		OF THE WIN		1		1	
fean Göttingen Time.	O ^h .		1 ^h .	<del></del>	2 ^h .		3 ^h .		4 ^h .	<del></del>	5 ^h .	1
l	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction	Force.	Direction.	Force.	Direction.	For
EEBRUARKY.  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	W. W.S.W.  N.N.W. N.E.  E. S.W. by W.  N.N.W.  N.E.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	M. N.N.W.  N.N.W.  N.N.W.  E. by N.  E. by N.  E. S.W.  N.N.W.  N.N.W.	0.0 0.0 0.0 0.2 0.2 0.0 0.0 0.0	W. by S.  W. w. by S.  N.N.W. N.E.  E. S.W.  W. N.W.  N.E.  D.  E. S. W.  N.W.  N.E.  D.  N.W.	0.5 0.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0	W.S.W. S.W. W. N.W. by W. S. N.N.W. N.E.  E. by N. E.S.E. W. S.W. W. N.W. N.W. N.W. N.E.	0.2 0.2 0.2 0.2 0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0	S.W. S.W. by W. W.S.W. N.W.  S.S.W.  N.N.W.  E.N.E.  W. by S.  S.S.E.  E. by S. E.S.E.  W.S.W.  N.N.W.  N.N.W.  N.N.W.  N.N.W.  N.E. by E.	0.2 0.2 0.2 0.2 2.5 0.0 0.0 0.5 0.0 0.0 0.0 2.0 0.0 0.0 0.0 0.0	S.W. S.S.W. W.N.W. S. by W. N.N.W. N.E. N.E. W.N.W. E.S.E. N.W. by N. E. S.E. W.S.W. N. W.N.W. N.W. N.W. N.W. N.W.	0 0 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
(continued)		1	1	1					1			
Mean Göttingen Time.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	For
HEBRUARY.  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 17 17 17 17 17 17 17 17 17 17 17 17	S.S.W. W. by S. S.W. N.W. S. N.W. — N.E.	lbs	S.S.W. W. S.W. N.W. S. N.W.  E. N.  E. N.	lbs. — 0.2 0.5 1.0 0.2 3.0 — 0.0 0.0 0.0 3.0 —	S. by W. W. by S. S.W. W.N.W. S. by E. N.W.  E. N.  E. N.  E.N.E.	1bs. — 0'2 0'2 2'0 0'5 0'2 4'5 — 0'0 1'5 0'5 0'0 3'5 — 0'5		lbs. — 0'2 0'2 1'5 0'0 0'0 5'0 0'0 1'0 0'2 0'0 0'0 3'5 — 0'5	S. by W. W.N.W. S.W. W. N.W.  E.N.E.  E.N.E.  E.N.E.	lbs.	S. N.W. S.W. by W. W. by S.  N.W.  E.N.E.  E.N.E.  E.N.E.	lbss

				DIRE	CTION	AND FORCE	OF TH	HE WIND,					
6h.		7 ^h .		8h.		9h.		10h.		11h.			löttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	<u></u>	me.
	lbs.		lbs.		lbs.		lbs.		lbs.		lbs.	1 \	
s.s.w.	0.5	s.w.	0.5	s.s.w.	0.2	s.w.	0.0	s.s.w.	0.0	S.S.W. W. by S.	$\begin{bmatrix} 0.5 \\ 0.2 \end{bmatrix}$	$\begin{bmatrix} \hat{2} \\ 3 \end{bmatrix}$	
s.s.w.	0.2	S. by W.	0.2	<u>s.</u>	0.2	S. by W.	0.2	s.s.w.	3.0	S.S.W.	2.5	4	
W.N.W.	3.0	W.Ň.W. S.	2.2 0.2	W.N.W. S.	2.2 0.2	W.Ň.W. S.	$\begin{array}{c c} 1.5 \\ 0.2 \end{array}$	W.N.W. S.S.E.	$\begin{bmatrix} 1.2 \\ 0.5 \end{bmatrix}$	W.N.W. S.	$\begin{bmatrix} 2.0 \\ 0.5 \end{bmatrix}$	5 6	
S. by W.	0.2	S.S.W.	1.0	S.W. by S.	1.2	S.W.	0.2	s.w.	0.2	s.w.	0.5	7 8	
N.N.W. E.	1.0	N.N.W. E.	1.0	N.N.W. E.	1°0 0°2	N.N.W. E.	0.2 1.0	N.N.W. E.	0.5	N. E.	0°2 1°0	9 10	
N.E.	0.2	N.E.	0.2	N.E. by N.	0.2	N.E. by N. W.S.W.	0.2	N.N.E. W.S.W.	0.2 0.2	N.	0.0	11 12	
w. <u>N</u> .w.	0.0	W. W.N.W.	0.5	W.N.W. —	0.0	W.S.W.	0.5	W.	0.5		0.0	13 14	RY
E	0.5	E	0.5	— E.	0.0	N.E.	0.5	N.E.	0.5		_	15	FEBRUARY.
E.S.E.	0.0	E. by S.	0.0		0.0	E.	0.0	E.	0.0	N.E. N.E.	$\begin{array}{c c} 0.5 \\ 0.5 \end{array}$	16 17	'EB]
W.N.W. E.	0.5 3.2	W.N.W. E.	0°2 3°5	N. E.	0.2	N. E.N.E.	0.2	S. E.N.E.	0°2 4°5	— E.	$\begin{vmatrix} 0.0 \\ 4.5 \end{vmatrix}$	18 19	H
E. by S. S.W.	1.0	E.S.E. S.S.W.	3.0 3.0	E. by S. S.W.	0.5 3.0	s.w.	3.0 0.0	w.s.w.	0.0	s.w.	$\begin{vmatrix} 0.0 \\ 2.5 \end{vmatrix}$	20 21	
		<u> </u>	$\frac{3}{2\cdot5}$	s.w.	$\frac{3}{2.5}$	S.W.	2.2	w.s.w.	3.0	w.s.w.	$\frac{-}{2.5}$	22 23	
S.W. W. by S.	0.2	S.W. by S. W. by N.	1.2	W. by N.	1.0	W. by N.	1.2	W. by N.	1.5	W.N.W.	2.2	24 25	
W.N.W.	0.5	W.N.W.	$\begin{array}{c c} 0.5 \\ 0.5 \end{array}$	W. N.	$\begin{array}{c c} 0.5 \\ 0.5 \end{array}$	W. N.	0°2 0°2	N. N.	0.5	N.N.W.	0.5	26	
N.E.	0.0	N.E. by E.	0.0	S.W. E.N.E.	0°2 1°5	E.N.E.	1.0	S.W. E.N.E.	0.5	S.W. E.N.E.	0.5	27 28 29	
18h.		19 ^h .	<del> </del>	20h,		21h.		22h		23h.			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		lime.
						l	I		ł			] ]	inie.
1	lbs.		lbs.		lbs.		lbs.		lbs.		lbs.	J	
<u></u>	0.5		0.0		0.0		0.0		0.0		lbs. 0.0	1 2	
N.W.	0.2 0.2	 N.W. W.S.W.		 N.W. by W. W.S.W.		N.W. by W. W.S.W.	0.0	— W.N.W. W. by S.	0.0 1.2 1.0	— W.	lbs. — 0.0 1.0 0.0	$egin{bmatrix} 2 \\ 3 \\ 4 \end{bmatrix}$	
S.W. by W.	0.5 3.0 0.0	 N.W. W.S.W.	0.0 0.5 1.5 0.0	w.s.w. —	0.0 1.5 2.5 0.0	W.S.W.	0.0 0.2 1.2 0.0	W.N.W.	0.0		lbs	2 3 4 5 6	
S.W. by W.	0.5 3.0 0.0 0.0	W.S.W.	0.0 0.2 1.2 0.0 0.0	W.S.W. — — —	0.0 1.2 2.2 0.0 0.0	W.S.W. N.E. by E.	0.0 0.5 1.5 0.0 0.2	W.N.W. W. by S.	0.0 1.2 1.0 0.0	w. 	lbs.  0.0 1.0 0.0 0.0	2 3 4 5 6 7	
S.W. by W.	0.5 3.0 0.0 0.0 - 1.0 0.0	W.S.W. — W. —	0.0 0.2 1.2 0.0 0.0 0.0	W.S.W. — — — — W.	0.0 1.2 0.0 0.0 0.0 0.0	N.E. by E. N.N.W.	0.0 0.5 1.5 0.0 0.2 - 1.0 0.0	W.N.W. W. by S.  N.N.W.	0.0 1.2 1.0 0.0 0.0 0.0	W	lbs.  0.0 1.0 0.0 0.0 0.0 0.0 0.0 0.5 0.0	2 3 4 5 6 7 8 9	
N.W. S.W. by W. — — — — W. — — E.	0.2 0.5 3.0 0.0 0.0 	W.S.W.	0.0 0.5 1.5 0.0 0.0 0.0 0.0 0.5 0.0	W.S.W. — — —	0.0 1.5 2.5 0.0 0.0 	N.E. by E. N.N.W. N.E.	0.0 0.5 1.5 0.0 0.2 - 1.0 0.0 0.5 0.5	W.N.W. W. by S.  N.N.W. N.E. by E.	0.0 1.2 1.0 0.0 0.0 0.0 0.0 0.0	w. 	lbs.     0.0   1.0   0.0   0.0   0.5   0.0   1.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	2 3 4 5 6 7 8 9 10	
N.W. S.W. by W. — — — — — — — — — — — — — —	0.2 0.5 3.0 0.0 0.0 	W.S.W. — W. —	0.0 0.2 1.2 0.0 0.0 0.0 0.0 0.0	W.S.W. — — — — W.	0.0 1.5 2.5 0.0 0.0 1.0 0.0 0.5	N.E. by E. N.N.W.	0.0 0.5 1.5 0.0 0.2 - 1.0 0.0 0.5	W.N.W. W. by S.  N.N.W.	0.0 1.5 1.0 0.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0	W	lbs.     0.0   1.0   0.0   0.0   0.5   0.0   1.0   0.0   0.0   0.0   0.0   0.2	2 3 4 5 6 7 8 9 10 11 12 13	
N.W. S.W. by W. W. E.		W.S.W.  W. E. by N.		W.S.W.	0.0 1.5 2.5 0.0 0.0 	W.S.W. N.E. by E. N.N.W. N.E.  N.E.  N.E.		W.N.W. W. by S.  N.N.W. N.E. by E.  N.W. by W.	0.0 1.5 1.0 0.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.0	W N.N.W E.N.E N. by E	lbs.	2 3 4 5 6 7 8 9 10 11 12 13 14 15	
N.W. S.W. by W. W. E. 		W.S.W. — W. —		W.S.W.  W.  W.  N.E. by N.	0.0 1.5 2.5 0.0 0.0 0.0 0.5 0.0 0.0 0.0 0.0 0.0 0	W.S.W. N.E. by E. N.N.W. N.E.		W.N.W. W. by S.  N.N.W.  N.E. by E.	0.0 1.5 1.0 0.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.0	W	lbs.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	
N.W. S.W. by W. W. E.  N.E. N. by W.		W.S.W.  W. E. by N.  N.E. by N.		W.S.W.  W.  N.E. by N.  N.E. by N.  N.E. by N.	0.0 1.5 2.5 0.0 0.0 0.0 0.5 0.0 0.0 0.0 0.0 0.0 0	W.S.W.  N.E. by E.  N.N.W.  N.E.  N.E.  N.W.  N.E.  E. by S.		W.N.W. W. by S.  N.N.W. N.E. by E.  N.W. by W.	0.0 1.5 1.0 0.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.2 0.2 0.0 0.0 4.5	W	lbs.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	
N.W. S.W. by W. W. E. 		W.S.W.  W. E. by N.		W.S.W.	0.0 1.5 2.5 0.0 0.0 0.0 0.5 0.0 0.0 0.0 0.0 0.0 0	W.S.W.  N.E. by E.  N.N.W.  N.E.  N.E.  N.W.  N.W.  N.W.		W.N.W. W. by S.  N.N.W.  N.E. by E.  N.W. by W. N. by E.	0.0 1.5 1.0 0.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.2 0.2 0.0 0.0	W	lbs.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	
N.W. S.W. by W.  E.  N.E.  N. by W.  E. by S.		W.S.W.  W. E. by N.  N.E. by N.  E. by S.		W.S.W.  W.  W.  N.E. by N.  N.E. by N.  E. by S.  W.S.W.		W.S.W.  N.E. by E.  N.N.W.  N.E.  N.W.  N.W.  N. W.  N. W.  N. W.  W.S.W.		W.N.W. W. by S.  N.N.W. N.E. by E.  N.W. by W. N. by E.  E. by S. W.S.W.	0.0 1.5 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	W	lbs.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	
N.W. S.W. by W.  W. E.  N.E.  N. by W.  E. by S.		W.S.W.  W. E. by N.  N.E. by N.  E. by S.  S.W. by W.  W. by S.		W.S.W.  W.  W.  N.E. by N.  N.E. by N.  E. by S.  W.S.W.  — — — —		W.S.W.  N.E. by E.  N.N.W.  N.E.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.		W.N.W. W. by S.		W	lbs.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	
N.W. S.W. by W.  E.  N.E.  N. by W.  E. by S.		W.S.W.  W.  E. by N.  N.E. by N.  E. by S.  S.W. by W.  W. by S.		W.S.W.  W.  W.  N.E. by N.  N.E. by S.  W.S.W.  — — — — — — — — — — — — — — — — — —		W.S.W.  N.E. by E.  N.N.W.  N.E.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.		W.N.W. W. by S.		W	lbs.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 20 21 22 23 24 25 26	
N.W. S.W. by W.  E.  N.E.  N. by W.  E. by S.		W.S.W.  W. E. by N.  N.E. by N.  E. by S.  S.W. by W.  W. by S.		W.S.W.  W.  W.  N.E. by N.  N.E. by N.  E. by S.  W.S.W.  — — — —		W.S.W.  N.E. by E.  N.N.W.  N.E.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.		W.N.W. W. by S.  N.N.W.  N.E. by E.  N.W. by W.  N. by S.  E. by S.  W.S.W.		W	lbs.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	

				DII	RECTIO	N AND FOR	CE OF	THE WIND.					
Mean Gö		0h.		1h.		2h.		3h.	·	4h.		5h.	
Tim	e.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} & 1 & & \\ & 2 & & \\ & 3 & & \\ & 4 & & \\ & 5 & & \\ & 6 & & \\ & 7 & & \\ \end{pmatrix}$	N.E. by N.  W.	1bs. — 0.2 0.0 0.0 0.0 0.0 0.0	N.E. by N.  W	lbs	N.E. S.W. W.	1bs. — 0°2 0°0 0°2 0°2 0°0 0°0	N.E. by E. N.E. by N. S.W. by S. W. E.N.E.	1bs. — 0°5 0°2 0°5 0°2 1°0 0°0	N.E. by E. E. S.S.W. W. by N. E.	lbs. — 0.5 0.2 0.2 0.2 1.5 0.0	N.E. by E. E. S.S.W. W. by N. E. by N.	1bs. 0.5 0.2 0.5 0.2 1.0 0.0
H.	8 9 10 11 12 13 14 15	N. by W. E.N.E.	0.0 0.2 0.0 0.0 0.0	N. by W.	0.0 0.2 0.0 0.0 0.0	N.E. by E.  S.W. by S.	0.0 0.2 0.0 0.0 0.0 0.0	N.E. by N. E.N.E. ——————————————————————————————	0.5 0.5 0.0 0.0 0.0 0.0	S.S.W. E. E. E. W.S.W.	0.2 0.2 0.2 0.2 0.0 0.5	S.S.W. E. E. E. W.S.W.	0·2 0·2 0·2 0·2 0·0 0·5
MARCH	16 17 18 19 20 21 22	W.N.W. N.W. — — W.N.W.	1.0 0.2 0.0 0.0 0.0	W. by N. N.W. N.E. N.W. by W.	0.5 0.2 0.0 0.2 0.0 0.5	W. N.N.W. E.N.E. N.W. by W.	2.5 0.0 0.0 0.0 0.0 1.0	W. N.N.W. E. by N. N. W.N.W.	1.5 0.5 0.0 0.2 0.2 1.5	W. N.N.W. S.W. by W. E. by N. E. by S. W. by N.	1.0	W. N.N.W. S. E. by S. E.S.E. N.W.	0.5 0.5 0.2 0.2 0.2 1.5
	22 23 24 25 26 27 28 29	E. by N. E.N.E. S.S.E. S.W. by W.	0.2 0.0 1.0 0.0 0.2 0.2	E.N.E. E.N.E. S. S.W. by W	0.2 0.0 0.0 0.2	E.N.E. E.N.E. E.N.E.	0.5 0.2 1.0 0.0 0.5 0.0	E.N.E. E.N.E. E.N.E. S. by E. S.	0.2 0.5 0.5 0.5 0.5 0.5	E.N.E. E. by N. E.N.E. S.S.E. S.S.W.	0.2 0.5 0.5 0.5 0.5 0.5	E. by N. E.N.E. E.N.E. S.S.E. S.S.W. W.S.W.	0.2 1.0 0.2 0.5 0.5 0.5
	30 31		0.0	_	0.0	W.N.W. N.W. by W.	0.5	W.N.W. N.W.	0.2	W. N.N.W.	0.5	W.N.W. N.N.W.	0.2
(continue	(d)	<del></del>		1						1		1	
Mean Go Time	ttingen	12h.	1	13h.		14h.		15h.		16h.		17h.	
	[	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	1 2 3 4 5 6 7 8 9	E. by S.  S.W.  E. by S.	1bs. — 0.2 0.0 0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0	W.S.W.  E. by S.	1bs.  0.0 0.0 0.5 0.0 0.0 0.2 0.0 0.0	E. by S.	lbs.	N.W. — N.W. — N.W. by N.	1bs. — 0.0 0.0 0.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0	N.W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.W. N.E.	0.0 0.0 0.0 0.0 0.2 0.2 0.0 0.0
MARCH.	11 12 13 14 15	w.s.w.	0.0	W. by S.	0.0 1.0 0.0 0.0 0.0	W. by S.	0.0 1.0 0.0 0.0	E. W.S.W.	0.0 0.5 0.0 1.0	E. S.W.	$0.0 \\ 0.2 \\ 0.0$	E. S.W. by W.	0.0 0.2 0.0 0.5 -
MAJ	17 18 19 20 21 22	E. by N.  W.N.W.	0.0 0.2 0.0 0.5	E. by N. W. by S. W.N.W.	0.0 0.2 0.2 0.0 -	E.N.E. W.N.W.	0.0 0.2 0.0 0.2 0.0	N.E. W.N.W.	0.0 0.5 0.0 -	N.E. W.N.W.	0.0 0.2 0.0 0.2 0.0	N.E. by N. W. by N.	0.0 0.2 0.0 2.0 0.0 -
	23 24 25 26 27 28	E. by N.  W.S.W.	0.0 3.5 0.0 0.0 0.0 0.2	E. by N S.W. by S. S. W.S.W.	0.0 3.5 0.2 0.0 0.5	E. S.S.W. — W.S.W.	0.0 4.5 0.5 0.0 0.0 0.2	E.N.E. S. — W.S.W.	0.2	E. S.S.W. S.W. by W. W.S.W.		E.N.E. E. S.S.W. W.S.W. S.W. by W.	4.0 0.5 0.0 0.2 0.5
	29 30 31	w.	0.0	w.	0.0	W. N.N.E.	0.5 0.5		0.0 0.0	<u>-</u> -	$\frac{0.0}{0.0}$	— —	0.0 0.0

								THE WIND.				<del> </del>	
6 ^h .		7 ^h .		8 ^h .		9h.		10 ^h .		11 ^h .		Mean G	
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	J Ti	me.
	lbs.		lbs.		lbs.		lbs.		lbs.		lbs.	1,	
N.E. by E.	0.2	E. by N.	0.2	E.S.E.	0.2	E. by S.	0.2	E. by S.	0.2	E. by S.	0.0	2	
E. by S. S.W. by S.	$0.2 \\ 0.5$	S.S.W.	$0.2 \\ 0.2$	S.E. by S. S. by W.	$0.5 \\ 0.5$	S.S.E. S. by W.	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	S.S.E. S. by W.	$0.2 \\ 2.5$	s.w.	2.0	$\begin{array}{c c} 3 \\ 4 \end{array}$	
S.W.	0.2	S.S.W.	0.2	W.Ň.W.	$0.5 \\ 0.2$	S.W. by W.	0.5	Ŵ.	$0.0 \\ 0.0$	W.N.W.	0.5	4	
E. by N. S. by E.	$0.5 \\ 0.2$	E. by N. S.S.E.	$0.2 \\ 0.2$	E. E.S.E.	0.2	E.S.E.	0.2	E.S.E.	0.2	E.S.E.	0.0	6 7	
s.s.w.	0.2	S. by W.	0.2	S.S.W.	0.2	s.s.w.	$\frac{0.5}{0.2}$	S.S.W.	0.2	_	0.0	$\frac{8}{9}$	
Ε.	0.2	Ĕ.	0.2	Е.	0.5	E.	0.5	E.	0.5		0.0	10	
E. E.	$0.2 \\ 0.2$	E. by S.	$0.0 \\ 0.0$	E. by S.	$0.0 \\ 0.5$	E. by S.	$0.0 \\ 0.5$	E.N.E. E.	$0.5 \\ 0.2$	E.N.E.	$\begin{bmatrix} 0.0 \\ 0.5 \end{bmatrix}$	$\begin{array}{c} 11 \\ 12 \end{array}$	
	0.0		0.0		0.0	C	0.0		0.0		0.0	13	
W.S.W.	1.5	S.W.	1.2	S.W. by S.	1.0	S.W. by S.	1.0	W.S.W.	2.0	w.s.w.	0.2	14 15	MARCH.
W. N.W.	$0.5 \\ 0.5$	N.W. N.W. by W.	1.0 0.2	N.N.W. W.N.W.	1.0	N.N.W. N.W.	0.2	N.N.W. S.S.W.	1.0	N. by W.	0.0	16 17	AR
	0.0		0.0		0.0		0.0	5.5. W. E.	0.5	E.	0.5	18	×
E. S.E. by E.	$0.2 \\ 0.2$		0.0		0.0	_	0.0	S.W. by S.	$0.0 \\ 0.0$		0.0	19 <b>2</b> 0	
W. by N.	$\frac{1.2}{1}$	W. by N.	1.2	N.N.W.	1.2	N.W.	1.2	N.W.	1.2	W.N.W.	1.2	21	
$\overline{E}$ .	$\frac{-}{0.5}$	_	0.0	E.	0.5		0.0	_	0.0	_	0.0	22 23	
E.N.E.	0.0	E.N.E. S.	$0.2 \\ 0.2$	E. by N.	0.0	E.	$\frac{0.0}{1.0}$	E. by S.	0.0	E. by N.	$\begin{vmatrix} 0.0 \\ 3.0 \end{vmatrix}$	$\begin{array}{c} 24 \\ 25 \end{array}$	
S.E. by S.	0.2	S.E.	0.5	S.E. by E.	0.5	E. by S.	0.2	E. by S.	0.2	s.	0.5	26	
S.S.W. S.W.	$0.2 \\ 0.2$	S. by W.	0.0	S. by W. S.S.W.	$0.5 \\ 0.2$	S.S.W. S.W. by S.	0.2	s.w.	0.2	W. by S.	0.0	27 28	
			<del></del>									29	
S.W. S.S.E.	$0.2 \\ 0.2$	S. by W. S.S.E.	$0.5 \\ 0.2$	S.W. by S. S.S.E.	0°5 0°5	S.W. S.S.E.	0.2	S.W. S.S.E.	$0.5 \\ 0.2$	W.	0.0	30 31	)
		(				1				A SERVICE CONTRACTOR OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWNER OWN		1	
18h.		19 ^h .		20 ^h .		21h.		22 ^h .		23 ^h .		Mean G	öttinge
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Foce.	Direction.	Force.	J T	ime.
	lbs.		lbs.		lbs.		lbs.		lbs.		lbs.	1.	
	0.0	_	0.0		0.0		0.0		0.0	-	0.0	2	
S.W. by S.	$0.0 \\ 0.5$	_	0.0		0.0	w.s.w.	$0.0 \\ 0.2$	$\overline{\mathbf{w}}$ .	$\begin{array}{c c} 0.5 \\ 0.0 \end{array}$	$\overline{\mathbf{w}}$ .	0.0	$\begin{array}{c c} 3 \\ 4 \end{array}$	
W.N.W.	0.2		0.0		0.0	W. by N.	0.0	W. by N.	0.0		0.0	5 6	
_	0.0			_					_		_	7	
N. —	$0.0 \\ 1.0$		$0.0 \\ 0.0$	N. by E.	$0.0 \\ 0.2$	N. by W.	0.0	N.	0.0		0.0	8 9	
	0.0	N.E. by N.	0.2	N.E. by N.	$0.0 \\ 0.5$	N.E. by N.	0.5		0.0		0.0	10	
_	$0.0 \\ 0.0$		$0.0 \\ 0.0$		0.0		0.0		0.0	_	0.0	11 12	
	0.0	-	0.0		0.0	_	0.0	_	0.0	_	0.0	13 14	ن
w.n.w.	$0.5^{\circ}$	w.	1.0	w.	0.5	W. by S.	0.2	S.W. by W.	0.5	W. by S.	1.0	15	MARCH
N.N.W.	0.0	N.W.	$0.0 \\ 0.5$	N.W.	0.5 0.0	N.W.	0.0	N.W.	0.0	N.W.	0.0	16 17	₹¥
N.E. by N.	0.5	N.N.E.	0.5		0.0		0.0	<del></del>	0.0		0.0	18	A
N.W. by W.	$0.0 \\ 0.5$	W. by N.	$0.0 \\ 0.0$	w.	0.5	$\overline{\mathbf{w}}$ .	1.0 0.0	w.	$0.5 \\ 0.0$	w.n.w.	0.5	19 20	
N.E. by E.	$\frac{-0.5}{0.2}$	N.E.	0.2	E.N.E.	0.5	E.N.E.	1.0	E.N.E.	0.2	E. by N.	0.2	$\frac{21}{22}$	
E.N.E.	0.5	E. by N.	0.5	E.N.E.	0.5	N.E.	0.5	<u> </u>	0.0		0.0	23	
E. S.S.W.	$\frac{4.0}{0.2}$	S. by W.	$\frac{3.5}{0.2}$	E. S. by W.	$\begin{array}{c} 4.0 \\ 0.2 \end{array}$	E	$\frac{0.0}{3.0}$		$\frac{2.5}{0.0}$	E	2.0 0.0	$\begin{array}{c} 24 \\ 25 \end{array}$	
w.s.w.	$0.0 \\ 0.2$	s.w.	0.0 0.5	s.w.	0.0		0.0		0.0	S. S. W.	$\begin{array}{c c} 0.2 \\ 0.2 \end{array}$	26 27	
	<del>-</del>	-				_						28	
777													
W. by S.	$0.0 \\ 0.0$	W. by S.	0°2		0.0 0.0 0.0	_	0.0		0.0		0.0	$\begin{pmatrix} 29\\30\\31 \end{pmatrix}$	

	ſ	Oh.		1 ^h .		$2^{\mathrm{h}}.$		3 ^h .		4 ^h .		$5^{ m h}$ .	
Mean Go Tin	ottingen	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Ford
	$ \begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \end{pmatrix} $	N.N.E. N.N.E.	lbs. 0°0 0°2 0°2 0°0	N.E. N.E. by E. E.	lbs. 0°0 0°2 0°2 0°2	E. by N. E. by S. E.	lbs. 0°0 0°2 0°5 0°2	S.E. E. E. E.	lbs. 0°2 1°0 0°5 0°5	E.S.E. E. by N. E. E.	lbs. 0.5 1.0 0.2 0.5	S.E. E. by S. E. E.	1b 0 0 0
	5 6 7 8 9	N. by W. W. by S.	0.2 0.0 2.2 0.0	N. by W. W. by S.	0.0 0.0 3.0 0.0	N. by E. W. S.W.	0.2 0.0 3.0 0.2	N. W.S.W. S. by W.	0.5 0.0 3.0 0.5	E. W. by S. S.	0.2 0.0 2.2 0.0	<u>E.</u> W.S.W. S.	0 0 2 0
	10 11 12 13	N. by E.	0.5	N.	0.0	N. by W.	0.5	S.W. by S. 	0.2 0.2 0.2	S.W. by S. N.W. by N. S.S.W.	1.0	W.S.W. N. by W. S.S.W.	$\begin{bmatrix} 2 \\ -0 \\ 2 \end{bmatrix}$
APRIL.	14 15 16 17 18	N.N.W.	0.0 2.2 0.0 0.0 0.5	S.W. by W. N.N.W. — — W.N.W.	0.2 2.5 0.0 0.0 0.5	S.W. by S. N.N.W. — E. by S. W.S.W.	3.0 0.0 0.2 0.5	N.N.W. S. by E. E.S.E. S.S.E.	2·5 0·2 0·2 0·2	N. by W. S. by E. E.S.E. S.W. by S.	2.0 0.2 0.2 0.5	W.N.W. E.S.E. E.S.E. S.S.W.	0 0 0
	19 20 21 22 23 24 25	E. N.N.E. E.	0.0 0.0 0.2 0.2 0.0 0.5	E. by N.  E.S.E.	0.0 0.0 0.2 0.0 0.0 0.5	S.W. by S.  E.N.E.  N.E. by N.  E.	0.2 0.0 0.2 0.2 0.0 0.5	E.S.E. E.S.E.	0.5 0.0 0.2 0.2 0.0 0.5	S.W. by S. E. E. E.	0.5 0.5 0.5 0.5 0.0 0.5	S. S.S.W. E. E.N.E. —	
	26 27 28 29 30	N.E. by N. E. by N. E.N.E.	0.0 0.5 5.0 0.5	E.N.E. E.N.E. E.N.E.	0.0 0.2	N. by E. E. E.N.E. E. by S.	0.5 1.0 1.0 0.2	S.E. by S. E.N.E. E.N.E. E. by S.	0.5 1.0 1.0 0.5	S. by W. E.N.E. N.E. by E. E.N.E.	0'2 1'5 1'0 0'2	S. by E. E. by N. N.E. by E. E. by N.	
		11		1	1			•					
(continue	ed)			1									
(continue Mean Gi	ottingen	12h.	Force	13h.	Force	14 ^h .		15h.	Force.	16h.		17h.	Fo
Mean Gi	$ \begin{cases} \text{ottingen} \\ \text{ne.} \end{cases} $	Direction.  E.N.E.	Force.   lbs.   0°0   0°0   0°2	13 ^h .  Direction.  — — — E.N.E.	Ibs. 0.0 0.0 0.0 0.2		Force.   lbs.   0.0   0.0   0.0   1.5		Force.   lbs.   0.0   0.0   0.0   0.5		Force.    Ibs. 0.0 0.0 0.0 0.2 0.2 0.2	17h.	Fo
Mean Gi	Sttingen {	Direction.	0.0 0.0	Direction.	1bs. 0'0 0'0	14h. Direction.  E.N.E. E. by N. S.S.W. N.E.	lbs. 0°0 0°0 0°0	15h.  Direction.  E. by N. E. by N. S.W. N.E.	lbs. 0.0 0.0 0.0 0.5 0.5 2.0 0.0 0.2	Direction.  E. by N.	Force.    lbs.   0.0   0.2   0.2	17 ^h .  Direction.  E. by N.  E. N.E. W. by S.	Fo
Mean Go	Sttingen {	E.N.E.  E.N.E. S.W. W.   E. W.   N.W. by W. W.S.W.	lbs.   0°0   0°0   0°0   0°2	E.N.E. E.N.E. S.S.W. W. by N. W.	lbs. 0.0 0.0 0.0 0.2	14h.  Direction.  E.N.E.  E. by N. S.S.W.  N.E.  W.  W.S.W.	Ibs. 0°0 0°0 1°5 2°0 0°0	15h.  Direction.  E. by N. E. by N. S. W.	lbs. 0.0 0.0 0.0 0.5 0.5 2.0 0.0	16h.  Direction.  E. by N. E.N.E. E. by N. W.	Force.    lbs.   0.0   0.2   0.2	Direction.  E. by N.  E. N.E.	Fo   1   0   0   0   0   0   0   0   0   0
Mean Gi	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	E.N.E. S.W. W. I. E. N.E. W. W.S.W. S. by E. E. by N. N.W.	lbs.   0°0   0°0   0°0   0°2   0°5   1°5   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5	Direction.	lbs.   0.0   0.0   0.0   0.2	14h.  Direction.  E.N.E.  E. by N. S.S.W.  N.E.  W.  W.S.W.  E. by N.	Force.   lbs.   0.0   0.0   0.0   1.5   0.0   0.0   0.2	15h.  Direction.  E. by N. S. W. N.E. W.N.W.  S.W.  W.N.W.	lbs.   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	16h.  Direction.  E. by N. E.N.E. E. by N. W. N.E. N.E. S.W.	Force.    Ibs. 0'0 0'0 0'2 0'2	17h.   Direction.	Foo
Mean G	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	E.N.E. S.W. W. I. E. N.W. by W. W.S.W. S. by E. E. E. by N.	lbs.   0°0   0°0   0°0   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5	Direction.  E.N.E. E.N.E. S.S.W. W. by N.  W. W. S.S.E.	lbs.   0°0   0°0   0°0   0°2   1°5   0°0   1°5   0°0   1°0   0°2   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0	14h.  Direction.  E.N.E.  E. by N. S.S.W.  N.E.  W.  W.S.W.  E. by N.	Force.   lbs.   0.0   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.0   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	15h.  Direction.  E. by N.  S.W.  N.E.  W.N.W.  S.W.	lbs.   0.0   0.0   0.0   0.5     0.0   0.5     0.0   0.5     0.0   0.5   0.0   0.0   0.0   0.0   0.0   0.2     0.2     0.2     0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	16h.  Direction.  E. by N. E.N.E.  E. by N. W. N.E.  N.E.  S.W.	Force.    lbs.   0.0   0.0   0.2   0.2	17h.  Direction.  E. by N.  E.N.E. W. by S.  N.W. by N.  N.W.	Foo

				D	IRECTI	ON AND FO	RCE OF	THE WIND	),				
6 ^h .		7 ^h .		8 ^h .		9 ^h .		10 ^h .		11 ^h .			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	]	Time.
S. by E. E. by S. E. E.	lbs. 0.5 0.5 0.2 0.5	S.S.W. E. E. E.	lbs. 0'2 1'0 0'2 0'5	S. by W. E. E. E.	lbs. 0°2 0°5 0°2 0°2	S. by W. E. by S. E. N.E. by E.	lbs. 0°2 0°5 0°2 0°2	S. by E. E. E. E. by N.	lbs. 0°2 0°5 0°2 0°2	E.N.E.	1bs. 0°0 0°2 0°0 0°2	1 2 3 4 5	
E. by S. S. by E. W.S.W. S. by E.	0.2 3.0 0.2	E. by N. S.W. W.S.W. S.E.	0.2 0.2 0.2 0.2	E. S.W. by S. W. S.E. by S.	0.5 0.2 3.5 0.5	E. S.S.W. W. E.S.E.	0.2 0.2 0.2 0.2	E. by N. S. W. W. E. by S.	0.5 1.5 2.5 0.5	E. by N. S.W. W. E.	0°2 1°5 2°5 0°5	6 7 8 9	
W. by S.	4.0	3 W.	5.2	w.	5.2	W.	5.2	W. by S.	4.0	W.	3.0	11 12	
N.W. S.S.W. N.N.W. E. by S. E.S.E. S.W. by S.	2.0 1.0 1.0 0.5 0.2 0.5	N.N.W. S.S.W. N.N.W. E.S.E. E.S.E. S.S.W.	2.5 1.0 1.0 0.5 0.2 1.0	N.N.W. S.W. by W. W. E.S.E. E. by S. S.S.W.	3.0 0.5 1.0 0.5 0.2 1.5	N.W. W.S.W. W. by S. E. by S. E. by S. S. by W.	3.0 2.0 1.0 0.5 0.2 1.0	N.W. W.S.W. S. by W. E. E. by S. S. by W.	3.0 1.5 0.5 0.5 0.2 0.2	N.N.W. W.S.W. S. by W. E. E.	2.5 2.0 0.2 0.5 0.2 0.0	13 14 15 16 17 18	APRIL.
S. by E. S.W. by S. E. N.E. by E. E. by S.	0.5 1.0 0.5 1.0 0.0 0.0	S. S.W. by S. E. by S. E.N.E. — E.	0.5 0.5 0.2 1.0 0.0 0.2	S. W. E.S.E. E.N.E.	0.2 2.0 0.2 1.0 0.0 0.2	S.W. by S. N. by W. E. by S. E.N.E.  E.	0.5 3.0 0.2 1.0 0.0 0.2	S.W. N.N.W. E. by S. E.N.E. E.N.E.	1.0 2.5 0.2 0.0 0.0 0.2	S.W. N.N.W. E.N.E. E.N.E.	1.0 3.0 0.0 0.2 0.0 0.2	20 21 22 23 24 25 26	
S.S.E. E.N.E. N.E. by E. E. by S.	0.2 2.5 1.0 0.2	S. N.E. by E. E.N.E E. by N.	0.2 2.5 1.0 0.2	S.S.E. E.N.E. E.N.E. E. by N.	0.2 2.0 1.0 0.2	S.S.W. E. by N. E.N.E. E.	0.2 2.0 1.0 0.2	S.S.W. E. N.E. by E. E.	0.2	S.S.W. E.N.E. E.N.E. E.	0.2 3.5 0.5 0.2	27 28 29 30	
18h.		19 ^h .		20h.		21 ^h .	127	22h.		23h.		] Moon	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		Time.
E.N.E. W.S.W.  E. by N.  N.W.  N.W.  E.S.E.  E.N.E.  N.N.E.  E. N.E.	lbs.   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	N.N.E.  E.N.E. W.S.W.  E.  N.W.  N.W.  E.  N.W.  N. by E.  N.N.E. by E.  N.N.E. by E.	lbs.   0.0   0.2   0.0   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	N.N.E.  N.E.  N.E.  N.E.  N.E.  N.W. by W.  N. by E.  E.  N.N.E.  N.E.	lbs.   0.0   0.2   0.0   0.5   0.2   0.2   0.5   0.2   0.5   0.2   0.5   0.2   0.2   0.2   0.5   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2	N.E. by N. E.N.E.  W.S.W.  E. by S.  N.W. N.W.  W. by S. E.  N.W. by S. E.  N.W. by S. E.  N.W. by S.	lbs.   0.0   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0		lbs.   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	N.N.E.  N. W. by S.  N.W. N.W.  N.N.W.  E.  E. by N. N.N.E. N.E. by E.	lbs.   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	APRIL,

		<del></del>		D	IRECTI	ON AND FO	RCE OF	THE WIN	D.				
Mean G	Göttingen	O ^h .		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
	me.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1\\2\\3 \end{pmatrix}$	E.N.E.	lbs. 0°2 0°0	N.E.	1bs. 0 ' 2 0 ' 0	N.E. by E.	0°2 0°2	E.N.E. N.E.	lbs. 0.5 0.2	E. by N.	1bs. 0.0 -	E. by N. S. by E.	1 0 0 2
	3 4 5 6 7 8 9	E.N.E. E.N.E.	0.0 0.0 0.2 0.0 0.0 0.5	S.W. E. E.N.E. N.N.E. E.N.E.	0.2 0.0 1.0 0.2 0.2 1.0	E. by N. E.N.E. N.E. E.N.E.	0.0 0.0 1.5 0.2 0.2 1.5	E. by N. N.E. E. by N.	0.0 0.0 1.0 0.2 1.0 2.5	S.S.W. S.W. by S. E. E. by N. N.E. E.N.E.	0.2 0.5 1.5 0.5 1.5 2.5	S.S.W. S.W. by S. E. E. by N. E. E. by N.	0.2 0.5 0.5 1.0 2.5
MAY.	10 11 ·12 13 14 15 16	N.N.W. N.W. by N. E.N.E. N. by W.	2·5 0·2 0·2 0·0 2·5 0·0	N. by W. N.W.  N.W.  N.W.	2.5 0.2 0.0 0.0 1.0 0.0	N. by W. N.N.W.	2.5 0.2 0.0 0.0 1.0 0.0	N.N.W. N.W. S. — N. by W. E. by S.	1.5 0.5 0.2 0.0 0.5 0.2	N.W. N.W. S. E. by S. N.W. by W. E. by S.	1:5 0:2 0:2 0:2 1:0 0:2	N.W. S.S.E. S. by W. E. by S. N.W. S.E.	1.5 0.2 0.2 0.5 0.5 0.2
M	17 18 19 20 21 22 23	N.N.W. N N.W. W. by N. E. by . N.N.E.	1:0 0:2 0:2 0:5 0:0 0:2	N.N.W. N.N.W. W. by N. E. by N.	2:5 0:2 0:2 0:5 0:0	N.N.W. N. by W. W. by N. E.S.E.	2.5 0.2 0.5 0.5 0.0 0.2	N.W. N.N.W. W. by N. E. E. E.S.E.	3.0 0.5 1.0 0.5 0.2 0.2	N.N.W. N.N.W. W.N.W. S.E. E. by S.	2.5 0.5 2.5 0.2 0.2 0.0	N.N.W. S. by W. W. S.S.E. E.	3.5 0.5 2.5 0.5 0.2 0.0
	24 25 26 27 28 29 30 31	N.W.	0.0 0.0 0.0 0.0 0.0 0.0	W.N.W.	0.0 0.0 0.0 0.0 0.0	N.W. W.N.W.	0.5 0.0 0.0 0.0 0.0	w.s.w.	0.0 0.0 0.0 0.0 0.0	S.W. W. by S. S.E. by S.	0.2 0.0 0.5 0.2 0.0 0.0	S.W. S.W. W. by N. S.E. by E. E.S.E.	0.5 0.5 1.0 0.5 0.5 0.0
(contin	nued)	1			1		<u> </u>						
Mean G	äöttingen∫	12 ^h .		13հ.		14h.		15h.		16 ^h .		17 ^h •	
Tir	me.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1\\2\\2\end{pmatrix}$	<u>-</u> s.	1bs. 0°0 0°2	$\overline{s}$ .	lbs. 0°0 0°2		0.0 0.0		0.0 0.0	W. by N.	lbs. 0°0 0°2		0.0
	3 4 5 6 7 8 9	S.S.E.  E.N.E. E.N.E.	0.2 0.0 0.0 0.0 0.5 3.0	S.S.E.  E.N.E. E.N.E.	0.2 0.0 0.0 0.0 0.2 2.5	E.N.E.	0.0 0.0 0.0 0.0 0.0 0.2 1.5	E. by N. E.N.E.	0.0 0.0 0.0 0.0 0.0	E.N.E. N.E.	0.0 0.0 0.0 0.0 0.2 0.5	E.N.E. N.N.E.	0.0 0.0 0.0 0.0 0.2 0.2
MAY.	10 11 12 13 14 15 16	N.W. S.W. S.S.W. N.N.E. S.	1.0 0.0 3.0 0.5 0.2 0.2	W.N.W. S.W. S.W. N. S.	0.2 0.0 2.0 0.5 0.2 0.2	W.N.W. S.W. N. by E.	0.0 0.0 0.0 0.0 0.5 0.2 0.0	S.W. S.W. N.	0.0 0.0 0.2 0.5 0.2 0.0	s.w. s.w.	0.0 0.0 1.0 0.2 0.0 0.0	S.W. S.W.	0.0 0.0 0.2 0.0 0.0
	17 18 19 20 21 22 23	N.N.W. S.W. by W N.W. E. by S. N.W. by W	2.5 0.2 0.0 1.0	N.N.W. N.N.W. N. by W.	0.5 0.2 1.0 0.0 0.0 0.5	N. by W.	0.0 0.0 0.2 0.0 0.0 0.0	N. by W.  N.E.	0.0 0.2 0.0 0.2 0.0	N. by W.  N.E.	0.0 0.2 0.0 0.0 0.5 0.0	N. by W. N.W. E.N.E.	0.0 0.2 0.2 0.0 0.5 0.0
	24 25 26 27 28 29 30 31	W S. by E.	0.0 0.0 0.2 0.0 0.0 0.2	N.N.W.	0.0 0.0 0.0 0.2 0.0 0.0	E. by N.	0.0 0.0 0.0 0.0 0.0 0.2 0.0	s.w	0.0 0.0 0.0 0.0 0.0	s.w.	0.2 0.0 0.0 0.0 0.0 0.0	- - - - - - -	0.0 0.0 0.0 0.0 0.0 0.0

				DIRE	ECTION	AND FORC	E ОГ Т	HE WIND.					
6 ^h .		7 ^h .		8 ^h .		9 ^h .		10h.		11h.			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		lime.
E. by N. S. by W.	lbs. 1 ° 0 0 ° 2	E. by N. S. by W.	lbs. 0.5 0.2	E.N.E. S.S.W.	lbs. 0°5 0°2	E.N.E. S.S.W.	lbs. 0°2 0°2 —	s.s.w.	lbs. 0°0 0°2	<u>s.</u>	lbs. 0°0 0°2	1 2 3	
S.S.W. W. E. E. E.N.E. E.N.E.	0.2 0.2 0.5 0.2 1.0 2.5	S. by W. W. by S. E. E. E. by N. E.N.E.	0.2 0.5 0.5 0.5 1.5 3.5	S. by W. S.W. E. E. E. E.N.E.	0.2 0.2 0.5 0.5 2.5 3.5	S. by W. S.W. E. E. by N. E. E.N.E.	0.2 0.2 0.2 0.5 1.5 3.5	S. by W.  E. E. by N. E. by N. E. N.E.	0.2 0.0 0.2 0.2 1.5 3.5	S.S.E. E. by N. E.N.E. E.N.E.	0.5 0.0 0.5 0.0 1.0 4.0	4 5 6 7 8 9	
N.W. S. S.S.W. S.E. by E. N.W. S.S.E.	2.0 0.5 2.0 0.2 0.2 0.2	N.W. S. S.W. S.E. S.W. by S.	2.5 0.5 2.5 0.2 0.5 0.2	N.N.W. S. S.W. S. by W. S.W. by S.	2.0 0.2 3.0 1.5 0.5 0.2	N.W. S.E. S.W. S.W. by S. S.S.W.	0.5	N.N.W. S.E. S. W. S.W. by S. S.S.E. S.	2·5 0·2 3·0 1·5 0·2 0·2	N.N.W. S.W. S.S.W, N. by E. S.	2.0 0.0 3.5 1.0 0.2 0.2	10 11 12 13 14 15 16 17	MAY.
N.N.W. S. by W. W. by N. S. by E. E. W.S.W.	4.0 0.5 3.5 0.5 0.5 0.2	N.N.W. S. by W. N.W. by W. S.E. E. W.	5.0 0.5 3.5 0.5 0.5 1.5	N.N.W. S. by W. W.N.W. S.E. by S. E. W.N.W.	3.5 0.5 3.5 0.5 0.2 1.0	N.W. S.S.E. N.W. S.E. by S. E. by S. W.N.W.	3.0 0.5 4.0 0.5 0.2 2.0	N.W. S.S.E. N.W. E.S.E. E. W.N.W.	2.5 0.2 4.0 0.2 0.2 1.5	N.N.W. S. by W. N.N.W. E. by S. E. by N. N.W.by W.	2.5 1.0 3.5 0.2 0.2	18 19 20 21 22 23 24	
S.W. S.E. W. S.E. by S. S.E.	0.5 0.5 1.0 0.5 0.5 0.0	S.W. S.E. W.N.W. S.E. by S. S.E.	0·2 0·2 1·0 0·2 0·2 0·0	S.W. W.N.W. S.E. by S. E.	0.5 0.0 1.0 0.2 0.2 0.0	N.W.by W.	0.0	N.W. S.E. by S. E. by S.	0.0 0.0 0.5 0.2 0.2 0.0	W. by N. E. by S. S. by E.	0.0 0.0 0.2 0.0 0.2 0.2	25 26 27 28 29 30 31	
					!		1					11	
18h.		19 ^h .		20 ^h .	. '	21 ^h .		22 ^h .		23 ^h .		Mean	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		ime.
N.N.E. N.E. by E.	lbs.   0°0   0°0   0°0   0°0   0°2   0°2	S.E. by E.  N. by E.  N.E. by E.	1bs. 0°0  0°0 0°0 0°2 0°0 0°2 0°5		lbs. 0°0  0°0 0°0 0°0 0°0 0°0 1°5		lbs.   0°0   0°0   0°0   0°5		1bs. 0 0 0	N.N.E.  E.N.E.	lbs.   0.0     0.0   0.0   0.0   0.5	1 2 3 4 5 6 7 8	
N. by W. S.W. W.S.W.	0.0	N.N.W.	0.0 0.0	N. by W. W. E.N.E. S.W. by S.	1.5 0.2 0.2 0.5 0.0 0.0	N.N.W. W. by N. S.W. by S.	0.5 0.2 0.0 0.2 0.0 0.0	N.N.W. W. by N. S.W. by S. N.	0.5 0.2 0.0 0.2 2.0 0.0	N.N.W. N.N.W. N. N.W.	1.5 0.2 0.0 0.0 1.5 0.0	10 11 12 13 14 15 16	MAY.
N	0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.N.E.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	W.N.W.  E.N.E.  N.W. S.W.	0.0 0.0 0.2 0.0 0.0 0.2 	W.N.W. E.N.E. N.W.	0.0 0.0 0.2 0.0 0.0 0.2 	W.N.W.  N. by W.  W.	0.0 0.0 0.2 0.0 0.0 1.2 	N.N.W. W.N.W. E. by N. N.N.E.	0.5 0.0 0.2 0.0 0.0 0.0 0.0 0.0	17 18 19 20 21 22 23 24 25 26	A
	0.0 	E. by N.	0.0 0.0 0.5 - 0.0	N.N.E.	0°0 0°0 0°2 — 0°0	 N.N.E. 	0.0 0.0 0.5 - 0.0	N.N.E.	0.0 0.0 0.5 - 0.0		0.0 — 0.0 0.0 0.0	27 28 29 30 31	

				DI	RECTIO	N AND FOR	1011 01	THE WIND				1	
Mean G	öttin g en	Oh.		1h.		2h.		3 ^h .		4h.		5h.	
Tin	ne.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force
	$ \begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{bmatrix} $	  N. by W. N.W.	lbs. 0°0 0°0 0°0 0°0 0°2 0°5	E E. by S. N. by W. N.W.	lbs. 0'2 0'0 0'0 0'2 0'2 0'2 0'5	E S.S.W. E. by S. N.N.W. N.W.	lbs. 0°2 0°0 0°2 0°2 0°2 1°0	E by N. S.W. N.W.	lbs. 0°2 0°0 0°2 0°0 0°0 1°5	E.N.E. S.W. by S.   N.W. by N.	lbs. 0°5 0°0 0°2 0°0 0°0 0°5	E. by N.  S.S.W.  N.N.W. N.W. by W.	1bs. 0.6 0.6 0.2 0.6 0.2 1.6
	7 8 9 10 11 12 13	N.N.E. N. by W. N.E. E.N.E.	0.0 0.0 0.2 0.2 0.2 0.2	N.E. by N. N.E. E. by N.	0.0 0.0 0.0 0.2 0.5 0.5	S.S.W. N.E. by N. E.N.E. E.N.E.	0.0 0.0 0.2 0.2 1.0 0.5	S.S.W. E. by N. E.	0.0 0.0 0.2 0.5 1.0 0.2	E. E.S.E. S.S.W. E. E.	0.2 0.2 0.2 0.5 0.5 0.5	E. by S. S.E. S.S.W. E. by S. E. E.	0.5 0.5 0.5 0.5 0.5
JUNE.	14 15 16 17 18 19 20 21	N. by E.  N.W. by N.	0.0 0.2 0.0 0.0 0.0 0.0	N. by E.	0.0 0.2 0.0 0.0 0.0 0.0	E.N.E. — — N.N.W.	0.0 0.5 0.0 0.0 0.0 0.0	S.W. E.S.E. S.E. by S. ————————————————————————————————————	0.2 0.2 0.2 0.0 0.0 0.0	S.S.W. E.S.E. S. by E. S.S.E. — N. by W.	0.2 0.5 0.2 0.2 0.0 1.5	S.S.W. S.E. by E. S. by E. S.S.E. W.S.W. N. by W.	0.2 0.3 0.2 0.3 0.3 1.3
	22 23 24 25 26 27	N.W. N.N.W. N.N.W. —	1.0 0.5 0.2 0.0 0.0	N.W. N.N.W. — — W.N.W.	0.2 0.0 0.0 0.0 0.2	N.W. by N. N.N.W. N. by W. N.N.W.  E.S.E.	1.0 0.5 0.2 0.2 0.0 0.2	N.W. by N. N. by W. N.N.W. N.N.W. ———————————————————————	1.5 0.5 0.2 0.5 0.0 0.0	N. by W. N. N.N.W. N.N.W.	2·5 0·5 0·2 0·5 0·0 0·2	N. N.N.W. N.N.W. N.N.W. E.	2:8 1:0 0:2 0:6 0:0
	$\left[\begin{array}{c}28\\29\\30\end{array}\right]$	E. by N.	0.0	E.N.E. E.N.E.	0.5	E.N.E. E. by N.	0.5	E.N.E. E.	0.5 0.2	E. by S.	0.2	E. E.	0.9
(continu	ued)					1		1				1	
Mean Gö	ittingen [	12 ^h .		13 ^h .		14 ^h .		15 ^h		16 ^h .		17 ^h .	
Tim	ie.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Forc.
	$\begin{bmatrix} 1\\2\\3\\4\\5\\6\end{bmatrix}$	E. by S. S. by W. S.W. N. by E.	1bs. 0°2 1°5 0°2 0°2 0°0	E. by S. S.W. S.	lbs. 0°2 1°0 0°2 0°0 0°0	W. by N. S.E. by E.	lbs. 0°0 1°5 0°0 0°2	W. by N. S.W. by S.	lbs. 0°0 0°2 0°2	  	lbs. 0.0 0.0 0.0	  	0.0 0.0 0.0 0.0
	6	N.N.W.	0.5	N.N.W.	0.5	N.N.W.	0.0	N.N.W.	0.0		0.2	N.W. —	
	7 8 9 10 11 12 13	N.N.W	0.5 0.0 0.0 0.0 0.0 0.5 0.2	N.N.W.		N.N.W.	0.5 0.0 0.0 0.0 0.0 0.0 0.0	E.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.E	0 0 		0.0 0.0 0.0 0.0 0.0
JUNE.	7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	— — — — E.	0.0 0.0 0.0 0.0 0.0 0.5 0.2		0°2 0°0 0°0 0°0 0°2 0°0 0°5 0°0 0°0 1°0 1°0		0°2  0°0 0°0 0°0 0°0 0°0 0°0 0°0 0°0 0°0	E.  E.  N.N.W.  N.N.E.  N.N.E.  N.N.W.	0.0 0.0 0.0 0.0 0.0 0.2 0.0 0.0	N.E.  E. by N.  N.N.W.  W.N.W.  N.N.W.  N.N.W.  N.N.W.	0 0 0	N.E.  N. by W.  N.W. by N.  N.W. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
JUNE.	7 8 9 10 11 12 13 14 15 16 17 18 19 20	E. N.E. by E. N.N.W. W.N.W. N.W. by N.	0.0 0.0 0.0 0.0 0.0 0.5 0.2 0.5 0.0 0.0 0.2	E	0'2 0'0 0'0 0'0 0'0 0'2 0'0 0'0	N.N.W.	0°2	E	0.0 0.0 0.0 0.0 0.0 0.2 0.0 0.0	N.E.  E. by N.  N.N.W.  W.N.W.  N.N.W.	0 0 0	N.E.  N. by W.  N. W. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

				DIRE	ECTION	AND FORC	E OF T	HE WIND.					
6 ^h ·		7 ^h .		8 ^h .		9 ^h .		10 ^h .		11h.			Göttingen
Direction.	Force.	Dir. etion.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	J 1	'ime.
E. by N. S. by W. S.W. E. by N. N. by W. W. by N.	lbs. 1 ° 0 0 ° 5 1 5 0 ° 2 0 ° 2 0 ° 5	E. S.S.E. S.W. by W E. by S. N.	lbs. 1 ' 5 0 ' 5 1 ' 5 0 ' 2 0 ' 2 1 ' 0	E. S.S.W. S.W. bv W. E.S.E. N.W. by N.	lbs. 1 '0 1 '0 2 '5 0 '2 0 '0 1 '0	E. S. by W. S.S.W. E. by S. S.S.W. N.W. by N.	lbs. 1 '0 1 '0 3 '0 1 '0 0 '2 0 '5	E. S.S.W. S. by W. E. S.S.W. N.W. by N.	lbs. 0 ' 5 0 ' 5 0 ' 2 1 ' 0 0 ' 2 0 ' 5	E. by S. S. by W. S. S.S.W. S.S.W. N.W. by N.	lbs. 0°2 1°0 0°2 0°2 0°2 0°5	1 2 3 4 5 6 7	
S.E. S.E. S.S.W. E. E.	0.2 0.2 0.2 0.0 1.0 0.2	S.E. S.E. S.S.W. E. E.	0.2 0.2 0.2 0.0 1.0 0.5	S.E. by S. S.E. S.S.W. E. by N. E.	0·2 0·2 0·2 0·2 0·5 0·5	S.E. by S. S.E. by S. S. by W. E. by S. E. E.N.E.	0.2 0.2 0.2 0.2 0.5 0.5	S.E. by S. S.E. by S. S. E.S.E. E. by N. E. by N.	0·2 0·2 0·2 0·2 0·2 0·2	S.E. by S.  S. E. E.N.E.	0.2 0.0 0.2 0.0 0.5 0.5	8 9 10 11 12 13 14	
S.S.W. S.E. by S. S. by E. S.S.E. W by S. N.W. by N.	0.2 0.5 0.2 0.2 1.0 2.5	S.S.W. S.S.E. S. by E. W. by S. N.N.W.	0.2 0.2 0.0 1.0 2.5	S.S W. S.S E. S. by E. W. N.N.W.	0.2 0.2 0.0 0.0 1.5 1.5	S.S.W. S.E. S. by E. W.N.W. N.W. by N.	0°2 0°2 0°0 1°5 1°5	S.S.W. S.E. — N.W. N.N.W.	0.2 0.2 0.0 0.0 1.5 2.5	N.N.W. —————————————————————————————————	0°2 0°0 0°2 1°0 2°0	15 16 17 18 19 20 21	JUNE.
N. by E. N. by W. N.W. N.N.W. N.N.W. E.	2.5 2.5 0.2 0.5	N. N. by W. N. by W. N. W. N.W. N.W. by W.	2.5 2.0 0.2 0.5	N. N.N.W. N. by W. S. by W. N.W. by W. E.	2:0 1:0 0:5 0:2 0:2	N. by W. N.W. W.N.W. S. by W. W. E.N.E.	2:0 1:0 1:5 0:2 0:2 0:2	N.N.E. N.W. N.W. by N. S.W.	1.0 1.0 0.5 0.0 0.2 0.0	N.N.E. N.W. N.N.W. ——————————————————————————	0.2 1.0 1.0 0.0 0.0 0.2	22 23 24 25 26 27 28	
E. E.	0.2	E. E.	0.2	E. by N.	1.0 1.2	E. by N. E. by S.	0°5 1°5	E.S.E. E. by N.	0.5 1.0	E. by S. E.N.E.	0°2 0°5	29 30	
18h.		19 ^h .		20h.		21 ^h .		22 ^h .		23 ^h .		Mean (	Göttingen
	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	T	ime.
Direction.	lbs. 0.0 0.0	Direction.	Force.   Ibs.   O'0   O'0   O'2   O'5   O'2   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0	N.N.W. W.N.W. N. by E.  N.N.W. N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.  N.E. by N.	Force.	N.N.W. W.N.W. N. by E.  N.N.W. N.E. E. by N.  N.W.  N.W.  N.W.  N.W.  N.W.  N. by W.  N. by W.  N. by W.  N. hy W.  N. hy W.  N. hy W.	lbs. 0'0 0'0 0'0 0'2 0'2 0'2 0'0 0'0 0'0 0'0	N.N.W. W.N.W. N.N.W. N.N.W. N.N.W. N.N.W. N.N.W. N.N.W. N.N.W. N.N.W. N.N.W. N.N.W. N.N.W. N.N.W. N.N.W.	lbs. 0'0 0'0 0'0 0'2 0'5 0'0 0'0 0'2 0'5 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0	N. by W. W.N.W. W.N.W. N.E	lbs.   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	JUNE.

				DI	RECTIO	ON AND FOI	RCE OF	THE WIND					
Mean Gö		Oh.		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
Tim	ie.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Fore
	$ \begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix} $	N. by W.	1bs. 0.0 1.0 0.0	N.E. by E. N. E. by S.	lbs. 0.5 1.0 0.2 0.0	E.N.E. N. E.	lbs. 0.2 2.5 0.2 0.0	E. by N. N. by W. E. by S.	lbs. 0 ' 5 1 ' 5 0 ' 2 0 ' 0	E.S.E. N. by E. E. by S. E.S.E.	lbs. 0°5 1°0 0°2 0°2	E. N.E. by N. E.S.E. E.S.E.	0. 0. 0. lps'
	5 6 7 8 9 10 11 12	W.N.W. W. W.S.W.	0.5 0.0 0.0 0.0 0.0 0.0	N.W. W. W.S.W. S.W.	0.2 0.0 0.2 0.0 0.2 0.2	N.N.W. N. N.W. W.S.W. W.S.W. S.W. by W.	1.0 0.5 0.5 0.2 0.2 0.2	W.N.W. N. by W. W. S.W. by S. S.S.W. S.S.W.	1.0 0.2 0.2 0.2 0.2 0.2	S.S.W. N. S.W. by W. S.W. by S. W. by S. W.S.W.	0.5 0.2 0.2 0.2 0.2 1.5	S. by W. N.N.W. S.W. by S. W. S.S.W.	0.0000000000000000000000000000000000000
JULY.	13 14 15 ( 16 17 18	N.W. N.W. by W.	0.2 0.0 0.0 0.0	N.W. N.N.W. N.W.	0.2 0.0 0.0 0.0	N.W. by W. N. by W. N.W. by N. N.N.W.	0.2 0.2 0.5 0.0 0.0 0.0	W. by N. N.W. N. by W. N.	1.0 0.5 1.5 0.2 0.0 0.0	N.W. N.W. N.N.W. N.N.E. S. by E. S. by E.	1.5 0.5 2.0 0.2 0.2 0.2	N.W. N.W.by N. S.S.E. S.E. by S. S.	0.0000000000000000000000000000000000000
	19 20 21 22 23 24 25	E. by N.   N.N.W.	0.0 0.2 0.0 0.0 0.0 0.0		0.0 0.0 0.0 0.0 0.0 0.0	S.E E. by S. N.N.W.	0.0 0.2 0.0 0.0 0.0 0.2 0.2	E.S.E. S.E. ————————————————————————————	0.5 0.5 0.0 0.0 0.5 0.5 0.5	S.E. E. E.N.E. W.	0.0 0.2 0.0 0.2 0.0 0.2	S.E. by S. S.E. S.E. E. N.N.W.	0,00
	26 27 28 29 30 31	E.N.E. N.E. —	0.0 0.0 0.0 0.0 0.0	N.E. by E. N.E. S.S.W.	0°2 0°2 0°0 0°2 0°0	E. by S. E. by N. S.W. N.N.W.	0.5 0.2 0.0 0.5 0.2	E. by N. S. by W. S.S.W. N. by W.	0.2 0.2 0.5 0.5 0.5	E. E.S.E. S. S.S.W. N.N.W.	0.5 0.5 0.5 0.5 0.2	E. by S. E.S.E. S.S.W. S.W. by S. N.N.W.	0 0 0 0
(continu	ed)												
Iean Gör Tim		12h.		13h.		14 ^h .	73	15 ^h .		16 ^h .		17 ^h .	Lare
	$ \begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix} $	Direction.  — — — E.	lbs. 0.0 0.0 0.0 0.2	Direction.	lbs. 0.0 0.0 0.0 0.2	Direction.	lbs. 0°0 0°0 0°0 0°2	Direction	lbs. 0°0 0°0 0°0	Direction. — — — — — — — — — — — — — — — — — — —	lbs. 0°0 0°0 0°0	Direction. — — — — — — — — — — — — — — — — — — —	1bs. 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0
	5 6 7 8 9 10 11	N.W.byW. N.N.W. — N.W.byW. S.S.W.	1:0 1:0 0:0 0:0 5:5 0:2	N.N.W. N.N.W.	0.5 0.5 0.0 0.0 2.5 0.2	N.N.W.	0°2 0°0 0°0 0°5 0°5	S.W. W.	0.0 0.0 0.0 0.0 0.0	N.N.W.  W.S.W. W.N.W.	0.5 0.0 0.0 0.0 0.5 0.5	N.N.W	0. 0. 0. 0. 0.
JULY.	$\begin{array}{ c c c }\hline 12\\ 13\\ 14\\ 15\\ 16\\ 17\\ 18\\ \end{array}$	S.W. N.W. N.N.W. E. E.S.E.	0.2 1.5 0.5 0.0 0.2 0.2	N.W. by N. N.W. N.W. by N.	1.0 1.0 0.2 0.0 0.2 0.0	N.W. by W.	0.0 0.0 0.0 0.0 0.0 0.0	N.W. byN.	0.0 0.0 0.0 0.0 0.0 0.0	N.W. by N. N.E. by N.	0.2 0.0 0.0 0.2 0.2 0.2	 N.W. byW.  N.E. byN. 	0. 0. 0. 0.
	19 20 21 22 23 24 25	E. by N. S.S.E. N.N.W.	0.2 0.2 0.0 0.2 0.2 0.0	E. by N. E. by N. S.S.E. N.N.W.	0.5 0.5 0.0 0.5 0.5 0.0	E. by N.  N.W.	0.0 0.2 0.0 0.0 0.5 0.0	   N.W. W.N.W.	0.0 0.0 0.0 0.0 0.2 0.2	N.W. by N.	0.0		0. 0. 0. 0.
	26 27 28 29 30 31	S.W. by S. W.N.W. N.N.W.	0.0 0.0 0.5 1.0 0.2	S.W. by S. W.N.W. N. by W.	0.0 0.0 0.2 0.5 0.2	W.N.W.	0.0 0.0 0.0 0.0	N.W.	0.0 0.0 0.0 0.0		0.0 1.0 0.0 0.0 0.0	S. by W. N.W. N. by W.	0. 0. 0.

				DIRI	ECTION	AND FORCE	E OF T	HE WIND.					
6h.		7h.		8h.		9հ.		10h.		11h.		] Mean	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		Time.
E. by S. S.S.E. E.S.E. E.S.E.	lbs. 0°2 0°5 0°2 0°2	E.S.E. S.S.E. E.S.E.	lbs. 0 · 5 0 · 5 0 · 5 0 · 0	E. by S. S. by E. E.S.E. E. by S.	lbs. 0.5 0.5 0.5 0.2	E. by S. S. E.S.E. E. by S.	1bs. 0°2 0°2 0°2 0°2	S.E. by E. S. E.S.E. E.	lbs. 0°2 0°2 0°2 0°2	E.N.E. S. E.	lbs. 0°2 0°2 0°0 0°2	1 2 3 4 5	
S. by W. S.S.E. S.W. by S. N.N.W. S.W. W. by S.	$0.2 \\ 0.2 \\ 0.2$	N.W. by W. S. S.S.W. S.S.W. N.W. by W. W. by S.	1.0 1.0 0.2 1.5 0.5 3.0	N.N.W. S. by W. S.S.W. N.W. S. by E. W.S.W.	1:0 1:0 0:5 0:5 0:2 2:5	N.N.W. N.N.W. S. by W.	1.0 1.0 0.2 0.0 0.0 1.0	W.N.W. N.W. by N. S. by W. S.W. by S. S.W. by S.	1.5 1.5 0.2 0.2 0.0 0.5	W.N.W. N.W. W. by S. S.S.W.	1.0 1.0 0.0 0.0 4.0 0.2	6 7 8 9 10 11 12	
W.N.W. N.W. N.W. by N. S.S.W. E.S.E. S. by W.	1.5 0.5 1.5 0.2 0.2 0.2	W. by N. N.N.W. N.N.W. S.S.W. S.E. S.S.E.	1.5 0.5 2.0 0.2 0.2 0.2	W.N.W. N.N.W. N.N.W. S. by W. S.E. S.E.	1.5 0.5 1.5 0.2 0.2 0.2	W. by N. N.W. N. by E. S.S.W. S.E. E.	1.5 0.5 1.5 0.2 0.2 0.2	W. by S. N.W. N.W. E. by S. E. by S.	0.5 1.0 1.0 0.0 0.2 0.2	S.W. N.N.W. N.W. by N. E. S.E.	0°2 1°5 0°5 0°0 0°2 0°2	13 14 15 16 17 18	JULY.
S.E. by S. S.E. by E. S.E. N.E. N.W. by N.	0.5 0.2 0.2 0.0 0.5 0.5	S.E. E. by S. S.E. by S. N. by W. N.N.W.	0.5 0.2 0.2 0.0 1.5 0.5	S.E. E. S.E. N. W.N.W.	0.5 0.2 0.0 1.5 0.5	S.E. by S. E. S.E. N.N.W. W.N.W.	0.2 0.2 0.2 0.0 1.5 0.2	S.E. by S. E. S. by E. N.W. by N. S.S.W.	0°2 0°2 0°0 0°2 1°0 0°2	E.S.E. E. by N. S.S.E. N.N.W.	0°2 0°5 0°0 0°2 1°5 0°0	20 21 22 23 24 25 26	
E.S.E. E.S.E. S. by W. S.W. by S. N.N.W.	0.5 0.5 1.0 0.5 0.5	E.S.E. S.E. S. by W. S.W. N.N.W.	0.5 0.5 1.0 1.5 0.5	E.S.E. E.S.E. S. by W. W.S.W. N.N.W.	0.5 0.5 1.0 2.0 0.2	E.S.E. S.E. by S. S. by W. W.S.W. N. by E.	0.2 0.2 2.0 2.5 0.5	E. E.S.E. S.S.W. W. by S. N. by W.	0.2 0.2 1.0 1.5 0.2	E. E.S.E. S.W. by S. W. N.N.W.	0°2 0°5 1°0 0°2	27 28 29 30 31	
		1		1 201		21h.		22h.		23h.		1	
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		Göttingen Time.
——————————————————————————————————————	bs. 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by E.  N.W.	lbs. 0 · 5 0 · 0 0 · 2 	N. by W.  N.W.  W.N.W.	1bs. 0°5 0°0 0°2 0°2 0°0 0°0 0°0	N. by W.  N.W.	Ibs. 0 · 5 0 · 0 0 · 2 0 · 0 0 · 0 0 · 0 0 · 0 0 · 0 0 · 0	N. by W.  N.W.  W.N.W.  W. by N.	lbs.   0°5   0°0   0°2   0°0   0°2   0°0   0°0	N. by W.  W.N.W.  W. by N.	7bs. 0 ' 5 0 ' 0 0 ' 0 0 ' 0	1 2 3 4 5 6 7 8 9 10	
N.W. by N.  S. by W.		S.W. by W.  N.N.W	0°2  0°0 0°0 0°0 0°0 0°0 0°0 0°0 0°0 0°0	W.N.W.  N.N.W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	W.N.W.  N.N.W. N.W. by N.  E.N.E.  E.N.E.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	W.N.W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.W. N.W. by N.  E. by N.  N.N.W.  N.N.W.	0·2  0·5  0·0  0·2  0·0  0·0  0·0  0·0	10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	JULY.

				DI	RECTI(	ON AND FOR	CE OF	THE WIND.					
Mean Gö	ittingen	O ⁵ .		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
Tim	ie.	Direct on.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force
	/ l	N. by W.	1bs. 0°2	N. by W.	0.2	N. by E.	0.2	N. by E.	1bs. 0°5	N. by W.	1bs. 0'2	N.N.W.	0 5
	3	N.E. by N.	0·2 0 0	N.E. by N. S.S.W.	$\frac{0.5}{0.5}$	N.E. by N. S.W.	0.5 0.5	S.W. by S.	0.0	S.E by S. S. by W.	0.2	N.W. by S.	0.0
	5		0.0		$0.0 \\ 0.0 \\ 0.5$		0.0	N.N.W.	0.0	N.E.	0.0	S.S.E.	0.2
	6 7 8	N.N.W.	$\begin{array}{c c} 0.0 \\ 0.5 \\ 0.0 \end{array}$	_	0.0		0.0		$0.0 \\ 0.0 \\ 0.5$		0.0		0.0
	9	N.N.W.	$\frac{0.5}{0.2}$	N. by W.	$\frac{0.5}{0.5}$	N.N.W.	0.2	N. by W.	1.0		1.2	N.N.W.	0.2
	11 12		0.0		$\frac{0.0}{0.0}$	N.N.E. S.S.W.	$0.5 \\ 0.5$	E.N.E. S S.W.	$0.5 \\ 0.2$	E.N.E. S S.W.	$0.2 \\ 0.5$	S.S.W.	0.2
	13 14	s.w.	0.0	S.W.	$0.0 \\ 0.0$		0.0	N. by W.	$0.0 \\ 0.2$	S.W. N. by W.	$0.5 \\ 0.2$	S.W. S. by W.	0.5
JST.	15 16		0.0	<u> </u>	0.0		0.0	N.W. by N.	0.5	S.W. by S.	0.5	S. by W. $\frac{1}{N}$	0.5
AUGUST.	17 18	_	0.0	N. by W.	$0.0 \\ 0.5$	N. N.E.	0.5 0.2	N. E.N.E.	0.5	N. S.E.	0.5	S.E. by E. E.N.E.	$0.5 \\ 0.2 \\ 1.0$
¥	19 20	N.E.	0.0	E.S.E.	0.0	E.S.E.	0.0	E. by S.	0.0	E. by S.	0.0 0.0	S.E.	0.0
	21 22	_	0.0		0.0 0.0		0.0		0.0 0.0	S.E. by E.	0.0	N.E. by N.	0.5
	23 24	N.N.E.	$\begin{array}{c c} - \\ 0.0 \\ 0.5 \end{array}$	N.N.E.	$0.0 \\ 0.0$	N.E. N.E. by E.	$0.5 \\ 0.5$	E. by N. E. by S.	0.5 0.5	E. by N. E.	$0.2 \\ 0.2$	E. S.E. by E.	0.5
	25 26	N.N.E.	$\begin{array}{c} 0.0 \\ 0.0 \\ 0.5 \end{array}$		$0.0 \\ 0.0 \\ 0.5$		0.0	— —	$0.0 \\ 0.0 \\ 0.5$	E.S.E. S.E. by S.	$0.2 \\ 0.2 \\ 0.2$	E.S.E. S.E. by S.	0.5
	27 28 29		0.0		0.0	N.E. by N.	0.5	E.N.E. E.	$0.2 \\ 0.2$	E. by S.	$\begin{array}{c} 0.5 \\ 0.2 \\ 0.2 \end{array}$	E. by S. E. by S.	0.5
	30 31	s.w.	$\frac{0.5}{0.5}$	s.w.	0.5	_	0.0	s.w.	0.5	S.W. by S.	0.2	S.W. by S.	0.2
(continu	ued)	1		1		1				,		1	
Mean G	öttingen [	12h.		13 ^h .		14h.		15 ^h .		16 ^h .		17 ^h .	1
Tir	ne.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force
	( 1		0 0		0°0		0°0	N.N.W.	0°2	_	0.0		0.0
	$\begin{vmatrix} 2\\3 \end{vmatrix}$		١		0.0				0.0		0.0		0.0
		S.S.W.	0.2	s w			0.0	S.W.	0.0	S.W.	0.0	S.W.	0.2
	4 5	S.S.W. S.W. by S. W. by S.	$\begin{array}{ c c }\hline 0.5\\0.5\\\end{array}$	S.W. W.	$0.2 \\ 0.2$	S.W. W.	1.0 0.2	S.W.	0.0	s.w.	0.0	S.W.	0.0
	4 5 6 7	S.W. by S. W. by S. —	0.0 0.0 0.0	S.W. W. —	0.0 0.0 0.2 0.2	S.W. W. —	0.0 0.2 0.2	S.W. 	0.0 0.0 0.0	_ _ _	0.2		0.0
	4 5 6 7 8 9	S.W. by S. W. by S. ————————————————————————————————————	0.5 0.0 0.0 0.0	S.W. W. — — —	0.0 0.2 0.2	S.W. W.	1.0 0.5 0.0 0.0 0.0 	S.W. 	1.0 0.0 0.0 0.0 0.2 -		0.5 0.0 0.0 0.0 0.2 -	_	0.5 0.0 0.0 0.0 0.2 -
	4 5 6 7 8 9 10	S.W. by S.  W. by S.  N.N.W. E.S.E.	0.2 0.2 0.0 0.0 0.0 - 1.0 0.2	S.W. W. — —	0.0 0.0 0.0 0.2 0.2	S.W. W. — —	0.0 0.0 0.0 0.2 0.2	S.W.  E. by N.	1.0 0.0 0.0 0.0 0.2 	E. by N.	0.5 0.0 0.0 0.0 0.2 - 1.0 0.0 0.0	E.N.E. N.N.W.	0.5 0.0 0.0 0.2 0.2 0.0 0.0
ci	4 5 6 7 8 9 10 11 12 13	S.W. by S. W. by S. ————————————————————————————————————	0.2 0.0 0.0 0.0 - 1.0	S.W. W. ————————————————————————————————	0.5 0.0 0.0 0.0 0.0 0.5 0.0 0.5 0.2 0.0	S.W. W. ————————————————————————————————	1.0 0.5 0.0 0.0 0.0 0.5 0.0 0.5 0.0 0.0	S.W E. by N N.N.W	1.0 0.0 0.0 0.0 0.2 	E. by N. N.N.W.	0.5 0.0 0.0 0.0 0.2 	E.N.E.  N.N.W.	0.5 0.0 0.0 0.0 0.2 0.2 0.0 0.0 0.0
UST.	4 5 6 7 8 9 10 11 12 13 14 15	S.W. by S.  W. by S.  N.N.W. E.S.E. S.S.W.	0.2 0.0 0.0 0.0 0.0 - 1.0 0.2 1.5 0.0	S.W. W. ————————————————————————————————	0.5 0.5 0.0 0.0 0.0 0.0 0.5 0.2 0.0 0.5	S.W. W	1'0 0'5 0'0 0'0 0'0 	S.W E. by N. N.N.W S.E	1'0 0'0 0'0 0'0 0'2 	E. by N.  N.N.W.  S.E.	0.5 0.0 0.0 0.0 0.2  1.0 0.0 0.0 0.0 0.0 0.0	E.N.E.  N.N.W.  S.E.	0.5 0.0 0.0 0.0 0.2 0.0 0.0 0.0 0.0 0.0
AUGUST.	4 5 6 7 8 9 10 11 12 13 14	S.W. by S.  W. by S.  N.N.W. E.S.E. S.S.W.	0.2 0.0 0.0 0.0 0.0 0.2 1.5 0.0 0.5 0.5	S.W. W. ————————————————————————————————	0.5 0.0 0.0 0.0 0.0 0.5 0.0 0.5 0.0 0.5 0.0	S.W. W. ————————————————————————————————	1'0 0'5 0'0 0'0 0'0 0'5 0'0 0'5 0'5 0'0	S.W E. by N. N.N.W S.E N by W.	1'0 0'0 0'0 0'0 0'2 	E. by N.  N.N.W.  S.E.  N.N.W.	0.5 0.0 0.0 0.0 0.2 	E.N.E.  N.N.W.  S.E.  N. by W.	0.6 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
AUGUST.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	S.W. by S.  W. by S.  N.N.W. E.S.E. S.S.W.  S.S.W.	0.2 0.0 0.0 0.0 0.0 0.0 1.0 0.2 1.5 0.0 0.5 	S.W. W. ————————————————————————————————	0.5 0.0 0.0 0.0 0.0 0.5 0.2 0.0 0.5 0.5 0.0 0.0	S.W. W	1'0 0'5 0'0 0'0 0'0 0'5 0'0 0'5 0'0 0'5 0'0 0'0	S.W E. by N. N.N.W S.E N by W.	1'0 0'0 0'0 0'0 0'2 	E. by N.  N.N.W.  S.E.  N.N.W.	0.5 0.0 0.0 0.0 0.2 1.0 0.0 0.0 0.0 0.0 0.5  0.5 0.0 0.0	E.N.E.  N.N.W.  S.E.  N. by W.	0.5 0.0 0.0 0.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0
AUGUST.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	S.W. by S.  W. by S.  N.N.W. E.S.E. S.S.W.  N. by W.	0.2 0.0 0.0 0.0 0.0 0.2 1.5 0.0 0.5 0.0 0.0 0.0 0.0	S.W. W. ————————————————————————————————	0.5 0.0 0.0 0.0 0.0 0.5 0.2 0.0 0.5 0.0 0.0 0.0 0.0	S.W. W	1'0 0'5 0'0 0'0 0'0 0'5 0'0 0'5 0'0 0'0 0	S.W E. by N. N.N.W S.E N by W.	1'0 0'0 0'0 0'0 0'2 	E. by N.  N.N.W.  S.E.  N.N.W.	0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0	E.N.E.  N.N.W.  S.E.  N. by W.	0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
AUGUST.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	S.W. by S.  W. by S.  N.N.W. E.S.E. S.S.W.  N. by W.	0.2 0.2 0.0 0.0 0.0 0.0 0.2 1.5 0.0 0.5 0.5 0.0 0.0 0.0 0.0 0.0 0.0	S.W. W. ————————————————————————————————	0.5 0.0 0.0 0.0 0.0 0.5 0.2 0.0 0.5 0.0 0.0 0.0 0.0 0.0 0.0	S.W. W	1'0 0'5 0'0 0'0 0'0 0'5 0'0 0'5 0'0 0'5 0'0 0'0	S.W E. by N. N.N.W S.E N by W.	1'0 0'0 0'0 0'0 0'2 	E. by N.  N.N.W.  S.E.  N.N.W.	0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0	E.N.E.  N.N.W.  S.E.  N. by W.	0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0
AUGUST.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	S.W. by S.  W. by S.  N.N.W. E.S.E. S.S.W.  N. by W.	0.2 0.2 0.0 0.0 0.0 0.0 0.0 0.2 1.5 0.0 0.0 0.5 0.0 0.0 0.0 0.0 0.0 0.0 0	S.W. W	0.5 0.0 0.0 0.0 0.0 0.5 0.0 0.5 0.0 0.5 0.0 0.0	S.W. W	1'0 0'5 0'0 0'0 0'0 0'5 0'0 0'5 0'0 0'5 0'0 0'0	S.W.	1'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0	E. by N.  N.N.W.  S.E.  N.N.W.  E.N.E.  N.E.	0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0	E.N.E.  N.N.W.  S.E.  N. by W.  E.N.E.  C.  C.  C.  C.  C.  C.  C.  C.  C.	0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0
AUGUST.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	S.W. by S.  W. by S.  N.N.W. E.S.E. S.S.W.  N. by W.	0.2 0.2 0.0 0.0 0.0 0.0 0.2 1.5 0.0 0.5 0.5 0.0 0.0 0.0 0.0 0.0 0.0 0	S.W. W. ————————————————————————————————	0.5 0.0 0.0 0.0 0.0 0.5 0.0 0.5 0.0 0.5 0.0 0.0	S.W. W	1'0 0'5 0'0 0'0 0'0 0'5 0'0 0'5 0'0 0'5 0'0 0'0	S.W E. by N. N.N.W S.E N by W.	1'0 0'0 0'0 0'0 0'2 	E. by N.  N.N.W.  S.E.  N.N.W.	0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0	E.N.E.  N.N.W.  S.E.  N. by W.   E.N.E.	0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0

				DIRE	ECTION	AND FORCE	E OF T	HE WIND.					
6 ^h .		7 ^h .		8 ^h .		9h.		10 ^h .		11 ^h .			Göttingen ime.
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	J 1	
N. by W.	lbs. 0°2	S.S.E.	lbs. 0.2	S.	lbs. 0 2	S.	lbs. 0'2	s.	lbs. 0 2	S.	lbs. 0 · 2	$\left[\begin{array}{c}1\\2\end{array}\right)$	
S. by E. S.S.W. S.S.W. S. by E. E.	0.2 0.2 0.2 0.2 0.0 0.0	S. by E. S.S.W. S.S.W. S. by W.	0.5 0.5 0.5 0.5 0.0 0.0 0.5	S. S. W. S. S. W. S. by W. E.	1.0 0.2 0.2 0.2 0.0 0.0	S.S.W. S.S.W. S.S.W. S. by W. E. by S.	1.0 0.2 0.2 0.2 0.0 0.0	S.S.W. S.S.W. S.W. by S. S.S.W.	1.0 0.2 0.5 0.2 0.0 0.0	S.S.W. S.S.W. S.W. by S.	0.2 0.2 0.0 0.0 0.0	3 4 5 6 7 8 9	
N. by W. S.E. by E. S.S.W. S.S.W. S. by W.	0.5 0.2 0.5 0.2 0.2 0.2	N.W. S.E. by S. S.S.W. S.S.E. S. S.S.E.	0·2 0·2 0·5 0·2 0·5 0·2	N. by W. S.E. S. S. by E. S. S.S.E.	0.5 0.2 1.0 0.2 0.5 0.5	N.W. by N. S.E. S. by W. S. by E. S.	0.5 0.2 1.0 0.2 0.2 0.5	N.W. by N. E.S.E. S S.W. S. by E. S. S. by W.	1.0 0.2 1.0 0.2 0.2 0.5	N.N.W. E.S.E. S.S.W.	1°0 0°2 1°5 0°0 0°5 —	10 11 12 13 14 15 16	AUGUST.
N.N.W. S.S.E. E. S.E. S.E. by S.	0.5 0.2 1.0 0.0 0.2 0.2	N. by E. S.E. by S. E. S.E. S.E. by S.	$ \begin{array}{c c} \hline  & & \\  & 0.2 \\  & 0.2 \\  & 0.0 \\  & 0.2 \\  & 0.2 \end{array} $	N.E. by N. S.E. by S. E. by S. S.E. S.E. by S.	1.0 0.2 0.5 0.0 0.2 0.2	N by W. S.E. by S. E	1.5 0.2 0.5 0.0 0.0 0.2	N.N.W. S. by E. E. S.E. by S.	0.2 0.2 0.0 0.0 0.0	N.N.W. S. by E. E.N.E. S.E. by E.	1.0 0.2 0.2 0.0 0.2 0.0	17 18 19 20 21 22 23	AU
E. by S. E.S.E. S.S.E. E.S.E. E.S.E. E S.E.	0·2 0·2 0·2 0·2 0·2 0·2	E.S.E. E.S.E. S.S.E. E.S.E. E.S.E. S.E.	0·2 0·2 0·2 0·2 0·2 0·2	S.E. by E. E.S.E. S.E. E.S.E. E. by S. W.	0.2 0.2 0.2 0.2 0.2 0.2 1.0	S.E. by E. E.S.E. E.S.E. E.S.E. E.S.E. N.W.	0.2 0.5 0.2 0.2 0.2 1.0	E. by S. E. E.S.E. E.S.E. W.N.W.	0.5 0.5 0.5 0.0 0.5 0.5 0.5	E. by S.  N.N.E. E.N.E.	0.0 0.2 0.0 0.2 0.2	24 25 26 27 28 29 30	
s.s.w.	0.2	S.W. by S.	1.0	S.W. by S	1.0	S.W. by S.	1.0	S by W.	0.2	S.S.W.	0.2	31 /	
18h.		19".		20h.		21h.		22h.		23 ^h .		Mean	Güttingen
Direction.	1	Dir etion.	Force.	Dire tion.	Force.	Direction.	Force.	Direction.	Force.	Direction	Force.		l'ime.
	108.	· · · · · · · · · · · · · · · · · · ·	ıbs.		ıbs.		ıbs		lbs.		ibs.	1 \	
N.E. S.W.	0.2 0.0 0.5 0.0 0.0	N.E. by N.	0.5 0.0 0.0 0.0 0.0 0.0	N.E. by N.	0.0 0.0 0.0 0.0 0.0	   	0.0 0.0 0.0 0.0 0.0 0.0	N.N.E.	0.0 0.0 0.0 0.0 0.0	N.N.E.	0.0 0.0 0.0 0.0 0.0	2 3 4 5 6 7	
N. by E.  S.W.  N. by W.  N. by W.  N. by W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	S.W. S. by W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	S. by W.  S. by W.	0.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0	N. by E.  S.W.  N. by E.  N. by E.  N. by E.  N. by E.	0.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0	N. by E.  N.N.E N.E	0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by W.	0 2 0·0 0·0 0·0 0·0 0·0 0·0 0·0 0·0 0·0 0·	8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	AUGUST.

				DI	RECTIO	ON AND FOL	RCE OF	THE WIND					
Mean G	öttingen	Oh.		1h.		2 ^h .		3 ^h .		4h.		5 ^h .	
Tir	ne.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1\\2\\3\\4\\5\\ \end{pmatrix}$	  W. by S.	lbs. 0°0 0°0 0°0 0°0 0°2	  w.s.w.	lbs. 0.0 0.0 0.0 0.0 0.0 0.0 0.2	 W.s.w. s.w.	1bs. 0°0 0°0 0°0 0°2 0°2	S. by S. S.W. by W. S.W. by S.	lbs. 0°0 0°2 0°0 0°2 0°2	S. by W. S.W. S.S.W.	lbs. 0°0 0°2 0°0 0°2 0°5	W. S. by W. S.W. by S. S.W. S.S.W.	lbs. 0°2 0°2 0°2 0°3
Ć.	6 7 8 9 10 11 12	N.E. E. by S. S.E.	0.0 0.0 0.5 0.5 0.2 0.0	N.N.W. N.E. E. by S. S.E. by S.	0.0 0.2 0.5 0.2 0.2 0.0	— N. E.N.E. E. by S. S.E. by S.	0.0 0.2 0.5 0.5 0.2 0.0	S.S.E. N. by E. E. by N. E. by S. S.E. by S. S.W.	0.2 1.0 2.5 1.0 0.2 0.2	S. by E. N.E. E. by N. E.S.E. S.S.E. S.S.W.	0.2 0.5 2.5 1.0 0.2 0.2	S. by W. N.N.E. E. by N. E. by S. S.E. by S. S.S.W.	0.2 0.5 3.0 0.5 0.2 0.2
SEPTEMBER	13 14 15 16 17 18 19	N. N. W. N. by E.	0.0 0.2 0.0 0.5 0.0	N.N.W. N.N.W. N. by E.	0.0 0.5 0.0 0.2 0.2 0.0	W.S.W. N. by E. N.N.W. N. by E.	0°2 1°5 0°0 0°2 0°2 0°0	S.W. by S. N. by E. S.E. by E. N. by E. N.E. W. by N.	0.5 1.5 0.2 0.2 0.2 0.2	S.W. by S. N. S. N. by E. E. by N. S.S.W.	1.0 1.0 0.2 0.2 0.2 0.2	S.W. N. S. S.E. by S. E.S.E. S. by W.	1:0 1:5 0:2 0:2 0:2
	20 21 22 23 24 25 26	N.W. by N.	2.0 0.0 0.0 0.2 0.2 0.2	N.W. by N. N.N.E.	2·0 0·0 0·0 0·2 0·2 0·0	N. by W. S.S.W. N. N.N.E.	2.0 0.0 0.2 0.2 0.2 0.0	N.E. by N. S. by E. S.S.W. W.S.W. N.E.	2.5 0.2 0.2 0.2 0.2 0.2 0.0	N. S. by E. S. by W. W. by S. E.N.E. S.W. by W.	1'0 0'2 0'2 0'2 0'2 0'2	N. by E. S. by E. S. W. by S. E. W.	0.5 0.2 0.2 0.2 1.5 0.2
	27 28 29 30	S.W. by S.	0.0 0.5 0.2	S.W. by S. S.W. by S.	0.0 0.2 0.2	S.W. by S. S.W. by S.	0.0 0.5 0.5	S.W. by S. S.S.W.	0.0 0.2 0.5	S.S.W. S.W.	0.0 0.5 1.0	S.W. by S. S.S.W.	0.2 0.5 0.2
(contin	ued)	101		13 ^b .		14 ^h .		15h.		16h.		17h.	
	Höttingen   me.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1\\2\\3\\4\\5\end{pmatrix}$	S.W. S. by E. S.S.W. N.	lbs. 0°2 0°2 0°0 0°5 0°2	S.W. by W. S. by E.  N.N.W.	lbs. 0°2 0°2 0°0 0°0	S.W. by W. S. by E.	lbs. 0 · 2 0 · 2 0 · 0 0 · 0 0 · 0	W.S.W. S. by E.	lbs. 0'2 0'2 0'0 0'0	S.W. by S.	lbs. 0°0 0°2 0°0 0°0	W.N.W. S.W. by S. S.W.	lbs. 0 · 2 0 · 0 0 · 0
В.	6 7 8 9 10 11 12	S.W. N. E. E.	0.2 0.5 1.5 0.2 0.0 0.0	N. E.	0.0 0.2 1.0 0.0 0.0	N.W. N.N.E. E. —	0.5 0.2 1.0 0.0 0.0 0.0	N.W. by N. N.N.E. E. —	0.5 0.2 1.0 0.0 0.0 0.0	N.N.W. E.N.E. E.	0.0 0.0 0.0 0.0 0.0	N.N.W. N.E. by N. E. —	0.2 0.2 0.0 0.0 0.0
SEPTEMBER.	13 14 15 16 17 18 19	s.s.w. s.w.	0.2 0.0 0.2 0.0 0.0 0.2	S. by W.  S. w.	0.2 0.0 0.5 0.0 0.0 0.2	w.n.w. s.s.w.	0.2 0.0 0.5 0.0 0.0 0.0	N.W. by W. S.W.	0.0 0.2 0.0 0.0	N.W. by W.	0.0 0.0 0.0 0.0 0.0	N.W. N.N.W. — — —	0.0 0.0 0.0 0.0 0.0
	20 21 22 23 24 25 26	N. by E. N.N.W.	0.0 0.0 0.0 0.2 1.0 0.0	N. by E. N.N.W.	0.0 0.0 0.0 0.2 1.0 0.0	N. by E. N.W. by N.	0.0 0.0 0.0 0.2 1.0 0.0	N.N.E. N.W.	0'0 0'0 0'0 0'2 1'0 0'0	N.E. by N. N.W.	0.0 0.0 0.0 0.2 0.5 0.0	N.E. by N. N.W.	0.0 0.0 0.2 0.5 0.0
	$ \begin{array}{c c} 27 \\ 28 \\ 29 \\ 30 \end{array} $	S.S.W. S. by W. S.W.	0.2 0.2 1.0	S.S.W. S.S.W. S.W.	0.5 0.5 0.2	S.W. S.W.	0.2 0.2 0.2	S.W. by S. W.	0.0 0.2 0.2	S.S.W. W.X.W.	0.0 0.5 0.5	S.W. by W. S.S.W. W.N.W.	0.2 0.5 0.5

				DIRI	ECTION	AND FORC	E OF T	HE WIND.		·			
6h.		7 ^h •		8h.		9 ^h .		10h.		11h.			löttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	<u> </u>	ime.
W. by N. S.E. by S. S.W. by S. S.S.W. S.W.	lbs. 1 '0 0 '2 0 '2 0 '2 0 '5	S.W. by S. S.E. S.W. S.W. by S. S.W.	lbs. 0.5 0.2 0.5 0.2 0.5	S.W. S.E. S.W. by S. S.S.W. S.W.	lbs. 1'0 0'2 0'5 0'5	S.W. E.S.E. S.W. by S. S.S.W.	lbs. 1 '0 0 '2 0 '5 0 '2 0 '0	S.W. E.S.E. S.W. by S. S.S.W.	lbs. 1 ° 0 0 ° 2 0 ° 5 0 ° 2 0 ° 0	S.W. E.S.E. S.S.W.	1bs. 0°2 0°2 0°0 0°5 0°0	1 2 3 4 5 6	
S. by W. N.N.E. E. by N. E. S.E. by S.	0.5 0.5 0.5 1.0 0.5 0.0	S.S.W. N.E. E. by N. E. S.E. by S. E. by N.	1.0 0.2 1.0 1.0 0.2 0.5	S.W. by S. E. E. by N. E. S.	1.0 0.2 1.0 0.0 0.0 0.2	S.W. by S. N. by E. E. by N. E. S.	1:0 0:2 1:5 1:0 0:0 0:2	S.W. N.E. by N. E. E. —	1.0 0.5 2.0 1.0 0.0 0.0	S.W. N. by E. E.N.E. E. S.S.W.	0.5 0.5 1.5 0.2 0.2 0.0	6 7 8 9 10 11 12 13	.B.
S.W. by S. N.N.W. S. E. E.S.E. S. by W.	0.5 1.0 0.2 0.2 0.2 0.2	S.W. by S. N.N.W. S. E.S.E. S.E. S. by W.	0.5 1.0 0.2 0.2 0.5 0.5	S.S.W. N.W. S.S.E. E.N.E. E.S.E. S. by W.	1.0 1.5 0.2 0.2 0.5 0.5	S.W. by S. N.N.W. S.S.E. S.E. S.S.W.	1.0 1.0 0.2 0.0 0.2 0.5	N.W. by N. S.S.E.	0.0 1.0 0.2 0.0 0.0 0.0	S.W. N. S.S.E. — — S W.	0.5 0.2 0.0 0.0 0.0 0.5	14 15 16 17 18 19 20	SEPTEMBER.
N. S. by E. S. E. S. by W.	0.2 0.2 0.2 0.0 2.5 0.2	N.N.W. S. by E. S. N. by W. E. S. by W.	0°2 0°2 0°2 0°5 2°5 0°5	N. by E.  S. N. by W. E.N.E. S.	0.2 0.0 0.5 1.0 0.2	S. by W. N.E. by N. E.N.E. S.	0.5 0.5 0.5	N. by W.  N.N.E.  N.E. by N.  S.W.	0·2 0·0 0·0 0·5 0·5	N. by E. N. S.W. by W.	0.0 0.0 0.0 0.2 0.5	21 22 23 24 25 26 27	
S. W. S.S.W.	0.2 1.0 0.2	S. S. W. S. S. W.	0°5 0°5 0°5	S. S.W. by S. S.S.W.	0.5 1.0 0.5	S. W. by S. S.S.W.	0°2 0°5 1°5	S.S.W. S.W. by S. S.W. by S.	0.5 0.5 5.0	S.S.W. S.S.W. S.W.	0.5 0.5 5.0	28 29 30	
18 ^h .		19h.		20h.		21h.		22h.		23h.		Mean C	
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		ime.
S.W. by S.  N.N.W.  N.E. by N.  E. by N.  W. by N.  N.W.  N.E. by N.  N.W.  S.S.W.  N.W.	lbs.   0 0 0 0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0	S.S.E.     N.N.W.   N.N.E.   N.E.     N.N.W.     N. by E.     N.E. by E.   N.W.     S.W. by S.   N.W.	lbs.   0	N.N.W. N.N.W.  N.N.W.  N.N.W.  N. by E.  N.W.  N.E. by E.  N.W.  S.W. by S.	lbs.   0.0   0.0   0.0   0.5   0.0   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.0   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	S.W. by S.  S.W. by S.  N. by W.  N.N.E.  E.  N.N.W.  N. by E.  N.N.W.  S.W. by S.	lbs.   0.0   0.0   0.5   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	S.W	lbs.   0 0 0   0 0 0 0 0 0 0 0 0 0 0 0 0 0	W. by S.	lbs.   0.0   0.0   0.0   0.5   0.0   0.0   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   1.0   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	SEPTEMBER.

				DI	RECTIO	N AND FOR	CE OF	THE WIND					
Mean Gö	ottingen ]	Oh.		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
Time	e. ]	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1\\2\\3\\4 \end{pmatrix}$	N.N.W. N. by W.	lbs. 0'2 0'5 0'0	N.N.W. N. by W.	lbs. 1 0 0 5 0 0	N.W. N. by W.	lbs. 0.5 0.5 0.0	N.N.W. N. by W. N.E.	lbs. 0 2 0 2 0 2	N. by W. E.	1bs. 0°2 0°2 0°2	N. by W. N. by W. S.E. by S.	lbs. 0°2 0°2 0°2
	4 5 6 7 8 9	N.W.	0.0 0.0 0.0 0.0 0.0	N.W. by W.	0.5 0.0 0.0 0.0 0.0 0.0	N.W. by W.	0.5 0.0 0.0 0.0	S.S.W. S.S.W. N.N.E.	0.0 0.0 0.2 0.0 0.2 0.2	S.S.W. S.E. S. W.N.W. N.E.	0.2 0.2 0.5 0.0 0.2 0.2	S. by E. E.S.E. S. by E. S.E. by E. W.N.W. E.	0'2 0'2 0'5 0'2 0'2 0'2
OCTOBER.	11 12 13 14 15 16 17	S.E. by E.	0.0 0.0 0.0 0.0 0.2	S.E. N. by W.	0.2 0.0 0.0 0.0 0.5 0.2	S.E. N. by W.	0.2 0.0 0.0 0.0 0.5 0.2	S W.N.W. S.E. by E. N. by W.	0.5 0.0 0.0 0.2 0.2 0.2	S. N.E. by N. S. by W. N.W. by W. S.E. by E.	1.0 0.2 0.2 0.2 0.2 0.0	S. by W. N. by E. S. by W. N.W. by W.	0.5 0.2 0.2 0.2 0.0 0.0
)	18 19 20 21 22 23 24 25	s.s.e. s.s.w.	0.0 0.2 0.0 0.2 0.0 0.0	S. by E. S.S.W.	0.0 0.2 0.0 0.0	S. by W. S.S.W. W.S.W.	0.0 1.0 0.0 0.2 0.0 0.2	W. by S. S.W. W. W.S.W.	0.2 0.2 0.5 0.2 0.0 0.0	S.W. by S. S.W. by S. W.N.W. N. by W. S.E. S.S.W.	0.5 0.2 0.2 1.0 0.2 0.5	S.S.W. S.W. by S. S.W. N. by W. S. by E. W.N.W.	0.5 0.2 0.5 2.5 0.2 1.5
	26 27 28 29 30 31	S.S.W. W. by N. N. by W. N.N.E.	0.0 0.2 0.0 0.2 0.2 0.2	N.N.W. W. by N. N.E.	0.0 0.0 1.0	N.N.W. N.W. by W. W. by N. N.N.W. N.N.W.	0.0 0.5 1.0 0.2 0.2 1.0	W.N.W. N.N.W. W. by N. N. by W. N.E. by N.	0.0 0.5 1.0 0.5 0.2 1.5	W.N.W. N.W. W. N. by E. N.E. by N.	0.0 0.2 1.5 0.2 0.2 2.0	N.W. by W. N.W. W. N. by W. N.E. by N.	0.0 0.2 0.2 0.5 0.2 2.0
No (continue								<u></u>					
Mean Gö	ttingen	12 ^h .		13 ^h .		14 ^h .		15h.		16 ^h .		17 ^h .	
Time	•  ]	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	1 2 3	E.N.E. N.	lbs. 0'5 0'2 0'0	E.N.E. N.	lbs. 0.5 0.2 0.0	N.E. N.	1 to 0 : 2 0 : 0	N.E. by N. N. N.E.	lbs. 1 0 0 2 0 2	N.E. —	lbs. 1.5 0.0 0.0	N.E. by N.	1.5 0.0 0.0
	4 5 6 7 8 9	S.S.E. S.W. by S. E. by N. N.N.W.	0.0 0.2 0.5 0.2 2.5 0.0	S.S.E. S.W. E. by N. N.	0.0 0.2 0.5 0.2 2.5 0.0	S.W. E. by N. N. by E.	0.0 0.0 0.2 0.2 1.0 0.0	S.W. E. by N. N.N.E.	0.0 0.0 0.2 0.2 0.5 0.0	S.W. E. by N. N.N.E.	0.0 0.0 0.2 0.2 0.0 0.2	N.W. by N.	0.0 0.0 0.5 0.0 0.0 0.2
OCTOBER.	11 12 13 14 15 16 17	W.S.W. N.N.W.  W. by S. N.W.	1'0 4'0 0'0 0'2 0'2	S.W. by W. N.N.W.	0.0 0.0 0.0 0.0 3.2	N. by W. N.W. by N. N.W. N.W. W.N.W.	0.5 0.5 0.0	N. by W. W. by N. N.E. by N. W.N.W. N.W. by N.	0.0 0.2 1.2	N. by W. N.W. by W.  W.N.W.  W.N.W.  N.W. by N.	0.0 0.0 1.2 0.5	W. by N. W. by S. W.N.W. N.W. by N.	0.0 1.5 0.2 0.0 1.0
0	18 19 - 20 21 22 23 24	S.W. W. W. N.W. by W. S.W. W.N.W.	0.2 0.5 0.2 0.5 0.5 0.2 0.5	S.W. W. W. by S. — .W.N.W.	0'2 0'2 0'2 0'0 0'0 0'0	W.S.W. W. by N. W. by S. — N.W. by W.		W.S.W. W. by N. W.S.W. W.S.W. N.W. by W.		w.s.w. w.s.w. w.s.w.	0.2 0.0 0.2 0.0 0.2 0.0	s.w. w.s.w.	0.5 0.0 0.5 0.0 0.0 0.0
No	25 26 27 28 29 30 31	S. by W. N.W. N.N.W. N.N.E. by N. E.	0'2 1'0 0'0 0'2 0'2 0'2 5'0	S.S.W. N.W. — N.N.E. E. by N.	0'2 0'2 0'0 0'0 0'2 3'5	S.S.W. N.W. — N.E. by N. E. by N.	0.2 0.5 0.0 0.0 0.2 3.5	S.S.W. N. by W.  N.W. by N.  N.E.  N.E.	0.2 0.2 0.0 0.2 1.0 3.5	S. N.N.W. — N. by W. N.E. N.E.	0.2 0.5 0.0 0.2 0.5 3.5	S.S.W. N. by W N. by W. N.E. N.E.	0.2 0.0 0.0 0.2 0.0 4.0

				DIR	ECTION	AND FOR	E OF T	THE WIND.					
6 ^h .		7 ^h .		8 ^h .		9 ^h .		10 ^h .		11 ^h .		Mean G	öttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		ime.
N. by W. N. by W. S. by E.	lbs. 0°2 0°2 0°2	N. by W. N. by W. S.E. by S.	lbs. 0°2 0°2 0°2	E. by N. N.W. by N. S.E.	lbs. 0 · 2 0 · 2 0 · 2	E. by N. N.N.W. E.S.E.	lbs. 0°2 0°2 0°2 —	N.E. N.N.W. S.E. by E.	lbs. 0°2 0°2 0°2	E.N.E. N. by W.	1bs. 0'5 0'2 0'0	1 2 3 4	
S.S.W. E.S.E. S. E.N.E. W. by N. S.W.	0°2 0°3 0°5 0°5 0°2 0°2	S. E.S.E. S. E.N.E. W. by N.	0.5 0.2 0.5 0.5 0.2 0.2	S. E.S.E. S.S.W. N.E. by E. N.N.W. S.E.	0.5 0.2 0.5 0.5 2.5 0.2	S.W. S.E. S.S.W. N.E. by E. N.N.W. S.E.	0.2 0.5 0.5 0.2 3.0 0.2	S.E. by S. S.S.W. E.N.E. N.N.W. S.E. by E.	0.0 0.2 0.5 0.2 3.0 0.2	S.S.E. S.W. by S. E. N.N.W.	0.0 0.2 0.5 0.2 2.0 0.0	5 6 7 8 9 10	
S. by W. W. by N.  —	0.5 0.5 0.2 0.0 0.0	S. N. S. by E. N.W. by W. S.	0.5 1.0 0.2 0.2 0.5 0.0	S. N. S.S.E. N.W. by N. S. by E. N.W. by N.	0.5 2.5 0.2 0.5 0.5 0.2	S. N. by W. S.E. W. by S. S. N.W. by N.	0.5 3.5 0.2 0.2 0.2 0.2	S. by W. N. by W. E.S.E. W.S.W.  N.W.	0.5 4.5 0.2 0.2 0.0 0.2	S. by W. N. by W. E.S.E. W.S.W. N.W.	0.5 5.0 0.2 0.0 0.2 0.2	11 12 13 14 15 16 17	OCTOBER.
S.W. by S. W.S.W. N. by W. W.	1.0 0.2 1.5 2.5 0.0 2.5	W.S.W. S.S.W. W. by S. N. by W. S. W. by N.	1.0 0.5 1.0 2.5 0.2 2.5	W.S.W. W. by S. W.N.W. N. W.S.W. N.N.W.	1.0 2.0 1.0 2.5 0.5 2.5	S.W. W. by S. W.N.W. N.	0.5 1.5 0.5 2.5 0.0 2.0	S.W. W.S.W. W. by S. N.W. by W. S.W. by W. N.W. by N.	0°2 1°0 0°5 2°0 0°5 1°5	S.W. W. by N. N.W. by W. W.S.W. W.N.W.	0.2 0.5 0.0 1.5 0.5 1.0	19 20 21 22 23 24 25	0
E. by S. W. by S. N.W. by W. W.N.W. N. by E. N.E.	0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	E. by S. W.N.W. N.N.W. W. N. by E. N.E. by N.	0°2 0°2 0°2 0°5 0°2 2°5	E.S.E. N.W. by W. N.W. W. N. by E. N.E.	0.2 0.2 0.2 0.5 0.5 3.0	E. by S. N.W. by N. W. by N. N.W. by N. N. by E. N.E.	0.5	E. by S. N.N.W. N.N.W.	0.2 1.0 0.2 0.0 0.2 3.5	E.S.E. N.N.W. N.N.E. E. by N.	0°2 1°0 0°0 0°0 0°2 5°0	26 27 28 29 30 31	Joyr
												1 2 1	
18h.		19 ^h .		20 ^h .		21h.		22 ^h .	1	23 ^h .			öttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	<u> </u>	ime.
N.E. by N.  S.S.W.  S.E. by S.  W. by N.  W. by S.  W.S.W.  W.S.W.  N.N.E.  N.N.E.  N.N.E.	lbs.   0 · 5   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0	N. by E.  S.S.W. S.E.  S.S.E.  W. by N. N.E. by N. N.W.  W.S.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.	lbs. 0.5 0.0 —	N. by E.	lbs.   0 · 2   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0	N.N.E.  N.W. by W. S.S.W.  W. S.E. by S. N.W. by W.  S.S.W.  W.S.W.  N.W. by W.  L.  S. by W.  N.N.W.  E.N.E.  N.E.	lbs,   0 * 2   0 * 0   0   0   0   0   0   0   0   0	N. by E.  N.W.  N.W.  N.W.  S.E. by S.  N.W.  W.S.W.  S.W.  S.S.W.  N.N.W.  E.N.E.  N.E.	lbs.   0 · 2   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0	N.N.E.  N.W.  S.E. by S.  N.W.  S.S.W.  S.S.W.  W.S.W.  N.N.E.  N.E.	lbs.   0 · 2   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0   0 · 0	1 2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 1 N	OCTOBER.

		ii						1					
Mean Gö Tim		Oh.		1 ^h .		2h.		3h.		4 ^h .	1	5 ^h .	
	$\frac{1}{2}$	Direction.	lbs.	Direction. N.E.	lbs. 2.5	N.E.	lbs.	Direction. E.N.E.	lbs.	Direction. E.N.E.	lbs.	Direction. E.N.E.	bs.
	$\begin{bmatrix} 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{bmatrix}$	S.W. by S.  N. N. —	0.5 0.0 0.5 0.0 0.0	N.W. by S.	0.0 0.0 0.0 0.2 0.0	N.W. by S. N.W. by W. N. N. N.E. by N.	0.5	S.W. by S. N.W. N. by E. N.E. by N.	0.5 0.5 0.0 0.0 0.2	S.W. by W. N.N.W. N. by E. N.E. N.E. by N.	0.2 1.0 0.2 0.2 0.2	S.S.W. N.N.W. E.S.E. N.E. by E. E.N.E.	0 0 0 0
3ER.	8 9 10 11 12 13 14	E.N.E. N. by E. E. by N.	0.0 0.0 0.2 0.5 0.0 0.2	N.N.E. E. by S.	0.0 0.0 0.0 0.2 0.0 0.2	E.N.E. N. by E. E.	0.0 0.0 0.2 0.2 0.0 0.2	N.N.E. N. by E. E.N.E. E. by S.	0.0 0.0 0.2 0.5 0.2 0.2	N. by E. N. E. N.E. E. by N.	0.0 0.0 0.2 0.5 0.5	S.S.E.  N. by E. N. by E. E. by N. E.N.E.	0 0 0 0 0
NOVEMBER	15 16 17 18 19 20 21	W.N.W. S.W.	0.0 0.0 0.0 0.0 0.0	N. E. by S. — N.W. by W. S.W.	0.5 0.5 0.0 0.0 2.5 0.2	N. by E. E.S.E. N. by E. N.W. by W. S.W.	0.5	E. by S.  N. by E.  N.W.  S.W.	0.5 2.0 0.5	E.S.E. S.W. by W. N.N.W. N.N.W. S.W.	0'2 2'5 1'0	E.N.E. E.S.E. W. by S. N. W. by N. W.S.W.	0 0 1 0 1 1 1
	22 23 24 25 26 27 28	W. by N.  N.N.E.  W.N.W.  W.S.W.	0°2 0°0 0°5 1°0 2°0 0°0	W. by N.  N.N.E.  W.N.W. S.W.	0.5 0.0 0.5 1.5 1.0	W. by N. W. N.N.E. W. by N. S.W. S.W.	0.2 0.2 0.5 1.5 0.5 0.5	W.N.W.  N.N.E.  W.  S.W.  S.W. by W.	0.2 0.0 1.5 3.0 0.5 0.2	W. by N. W. N. W.N.W. W.S.W. S.W. by W.	0.2 0.2 2.5 3.0 0.2 0.2	W.S.W. W. N. W. S.W. S.W. by W.	0 0 2 4 0 0
	29	N by E	0:5	N 1- F	0:0	_	0:0	_	-		0:0	N b- E	0
(continu	30	N. by E.	0.2	N. by E.	0.5		0.0		0.0	- Ich	0.0	N. by E.	0
(continu	ucd)	12h.	0.2	13h.		14h.		15h.		16 ^b .		17 ^h .	
Mean G	30  ucd)  sittingen {	1	Force.    Ibs. 0.0 0.0 0.2 0.2 0.2 0.2 0.2 0.2		Force.    lbs.	N.W. by N. N.N.E. N.E. by N.	Force.   lbs. 0.0 0.0 0.2 0.2 0.2 0.2 0.2	15h.  Direction.  S.S.W. N. by W. N. by E. E.N.E.	Force.    lbs.   0.0   0.2   0.2   0.2   0.0   0.5	16 ^h .  Direction.  W. by N. N. by W. N. by E. E.N.E.	Force.   lbs.   0°0   0°2   0°2   0°2   0°0   0°5		For   1bs   0   0   0   0   0   0   0   0   0
Mean Ge	30  ucd)  ittingen {	Direction.  N.W. by N. E. N.E.	Force.	13h.  Direction.  N.W. by N. N.E. N.E.	Force.    lbs.	Direction.  N.W. by N. N.N.E. N.E. by N.  E.N.E. N.N.E. E.N.E.	Force.   lbs.   0.0   0.2   0.2   0.2   0.2	S.S.W. N. by W. N. by E.	Force.    lbs.   0 0 0 2 0 2 0 2 0 2 0 0 2 0 0 0 0 0 0	Direction.  W. by N. N. by W. N. by E.	Force.    lbs.	17h.  Direction.  N. by W. N. by E. N.N.E. E.N.E.  E.N.E.  E.N.E.  E.N.E.	For
Mean G	30    ucd)	12h.  Direction.  N.W. by N. E. N.E. E. N. E. N. by W. N. by W. E.N.E.  E. by N. W.N.W. N. by W. W. by S. S.S.W.	Force.	13h.  Direction.  N.W. by N. N.E. E. E.N.E. E.N.E. E.N.E.  E.N.E.  W.S.W. S.S.W.	Force.    lbs.   0.0   0.2   0.2   0.5	Direction.  N.W. by N. N.N.E. N.E. E. by N. E. N.E. E. N.E. E. N.E. E. N.E. E. N.E. E. N.E. E. N.E. E. S.S.W. S.S.W.	Force.   lbs.   0.0   0.0   0.2   0.2   0.2   0.0   1.0   0.5   0.5   0.0   0.2   0.0   0.2   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5	S.S.W. N. by W. N. by E. E.N.E. E.N.E. N. by W.	Force.    lbs.   0.0   0.2   0.2   0.0   0.5	Direction.  W. by N. N. by W. N. by E. E.N.E. E.N.E. N.E. by N. E.N.E. E. by S. E. N.W. S.W.	Force.   lbs.   0.0   0.2   0.2   0.0   0.5   1.0     0.2   0.0   0.5   0.0   0.5   0.0   0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5     0.5   0.5     0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5	17h.  Direction.  N. by W. N. by E. N.N.E. E.N.E. E.N.E. E.N.E. E.N.E. W. by S. E. W. by N.	For 00 00 00 00 00 00 00 00 00 00 00 00 00
Mean Ge	30    ucd)	12h.  Direction.  N.W. by N. E. N.E. E. L. N. by W. N. by W. E.N.E.  E. by N. W.N.W. N. by W. W. by S.	Force.   lbs.   0.0   0.0   0.2   0.2   0.2   0.2   0.5   0.5   0.5   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2   0.2	13h.  Direction.  N.W. by N. N.E. E. C. E.N.E. E.N.E. C. E.N.E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. N. by E. C. C. N. by E. C. C. C. C. C. C. C. C. C. C. C. C. C.	Force.    lbs.	Direction.  N.W. by N. N.N.E. E. by N.  E.N.E. N.N.E. E. N.E.  E.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.N.E.  N.D.  N.N.E.  N.D.  N.N.E.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D.  N.D	Force.   lbs.   0.0   0.2   0.2   0.2   0.5   0.5   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5	S.S.W. N. by W. N. by E. E.N.E. E.N.E. N. by W. E. by S. E.N.E.  T. by N.  N.W.	Force.    lbs.   0 0 0 2 0 2 0 0 2 0 0 0 5   1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Direction.  W. by N. N. by W. N. by E. E.N.E. E.N.E. N.E. by N. E.N.E. E. by S. E. N.W.	Force.   lbs.   0.0   0.2   0.2   0.0   0.5   1.0	17h.  Direction.  N. by W. N. by E. N.N.E. E.N.E.  E.N.E.  E.N.E.  E. by S. E.  N.W.	For

				DIRE	CTION	AND FORCE	E OF TI	HE WIND.					
6h.		7 ^h .		8h.		9 ^h .		10h.		11h.			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	J T	'ime.
N.E. by E. S.S.W. N.N.W. E.S.E. E.	lbs. 0°5 0°2 0°5 0°2 0°2 0°5	N.E. W. by N. N.W. by N. S. by E. E. E.	lbs. 0°2 0°2 0°2 0°2 0°2 0°5	N.E. W. N.W. E.S.E. N.E. by E. N.E.	lbs. 0°2 0°2 0°5 0°2 0°2 0°2	N.E. W.N.W. N.W. E. by N. N.E. E.N.E.	lbs. 0°2 0°2 0°5 0°2 0°2 0°2	N.E. S.S.W. N.W. E. by N. N.E. E. by N.	lbs. 0°2 0°2 0°5 0°2 0°2 0°2	N.E. N.W. by N. E. N.E. E.	lbs. 0 2 0 0 0 2 0 2 0 2 0 2 0 2 0 2	2 3 4 5 6 7 8	
S. by E. E.S.E. N. by E. N. by E. E. by N. E.N.E.	0.2 0.2 0.2 0.5 0.5	E. by N. N. by W. N. E.N.E. E.	0.0 0.2 0.2 0.2 0.5 1.5	E.N.E. N. N. E.N.E. E.	0.0 0.2 0.2 0.2 0.5 1.5	E.N.E. N. N. by W. E. by N. E.	0.0 0.2 0.2 0.2 0.2 1.5	E.N.E.  N. by W. E. E. by N.	0.0 0.2 0.2 1.5	E.N.E.  N. by W.  E. by N.	0.0 0.5 0.0 0.2 0.0 0.5	9 10 11 12 13 14	IBER.
E. by N. E.S.E. W.S.W. N. by W. N.W. by W. S.W.	0.5 0.5 2.0 0.2 3.0 0.5	E.S.E. W. by S. N. W.N.W. S.W.	0.0 0.2 0.5 0.2 2.5 0.5	E.S.E. W. by S. N. by W. W. by N. S.S.W.	0.0 0.5 1.0 2.0 1.0	E. by S. E. W.S.W. N. by W. W. by N. S. by W.	0.2 0.5 0.5 0.5 1.5 1.0	E. by S. E. by N. W.S.W. N.N.W. W.N.W. S.S.W.	0°2 0°5 0°5 1°5 1°5 2°0	E. by S. E. by N. W.S.W. N. by W. W. by S. S.S.W.	0°2 0°5 0°2 2°5 0°5 2°0	16 17 18 19 20 21	NOVEMBER.
W.N.W. W. N. W. S.W. W. by S.	0.5 0.2 3.5 6.0 0.2 0.5	N.W. by W. N. by W. N.N.W. W. W.S.W.	0.5 0.5 3.0 10.0 0.0 0.5	W. by S. N. by W. N.N.W. W. S.E. by S. W.S.W.	0.2 0.5 3.5 10.0 0.2 2.0	W. by S. N.N.W. N.N.W. W.S.W. S.E. by S. W.S.W.	0.2 0.5 4.0 8.0 0.5 1.5	S.W. N.N.W. N.W. W.S.W. S.E. by S. S.W.	0.2 0.5 3.5 5.0 0.5 0.2	S.W. by S. N. by W. N.N.W. W.S.W. S.E. by S. S.W. by W.	0.2 0.2 3.0 4.5 1.5 0.2	23 24 25 26 27 28 29	
N. by E.	0.5	N. by W.	1.5	N.N.W.	1.2	N.W. by W.		N.W.	1.0	N. by W.	1.0	30 -	)
18h.		19 ^h .		20h.		21h.		22h.		23h.			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	<u> </u>	ime.
N. by W. N. by E. E.N.E. E.N.E. N. E. by S. N.W. by W. E.S.E. E. N.W. W.N.W. S.W. N. by W. N.N.W. N. by W. N.N.W.	lbs. 0'0 0'0 0'2 0'2 0'0 1'0 0'0 2'5 0'2 0'0 0'2 0'5 0'2 0'0 3'5 0'0 0'2 1'5 3'5 0'0 1'5 0'0	N. by W.  E.N.E.  N.E. by N.  N. by W.  E. by S.  N.W. by W.  S.E. by E.  W.N.W.  W.S.W.  W.N.W.  S.S.W.  N. by E.  W. by N.  W.S.W.  N. by E.  W. S.W.  N. by E.  W. S.W.  N. by E.  W. S.W.  N. by E.  W. S.W.  N. by E.  W. S.W.  N. by E.	lbs. 0'0 0'0 0'2 0'0 0'5 0'0 1'0 0'5 0'5 0'2 0'0 3'5 0'2 0'5 0'5 1'5 3'5 0'0 1'5	N. by W.  N. by W.  N.W. E.N.E. N. E. by S.  E.S.E.  W.W. S.W. by W.  N.N.E. W. by N. W.S.W.  N.N.E.  N.W. S.W.	lbs.   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	N. by W.	lbs.   0.0   0.0   0.0   0.0   0.0   0.0   0.5   0.2   0.0   0.2   0.0   0.2   0.0   0.2   0.0   0.5   0.2   0.5   1.0   3.5   0.0   0.2   0.0   0.0   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	N. by W. N. by E.     E.N.E.     E.S.E.     E.S.E.     N.W.   S.W.   by W. N.N.E.   W. by N. W. by S.     N.W.     N.W.     N.W.     N.W.     N.W.       N.W.       N.W.       N.W.       N.W.       N.W.         N.W.	lbs.   0 0 0   0 0 0   0 0 0   0 0 0   0 0 0   0 0 0 0   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	S.W. by S.  N. by W.  N.  W.S.W. E.N.E. N.  E. by N.  W.N.W. S.W.  W.N.W. W. by N.  N.N.E. W.N.W. W.S.W.	1bs. 0 · 2 0 · 0 0 · 2 0 · 0 0 · 2 0 · 5 0 · 5 0 · 0 0 · 2 0 · 0 0 · 2 0 · 0 0 · 0 1 · 5 0 · 0 0 · 0 1 · 5 2 · 0 0 · 0 0 · 5 1 · 5 2 · 0 0 · 0 0 · 5 0 · 0	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	NOVEMBER.

				DI	RECTIO	ON AND FOR	RCE OF	THE WIND				· · · · · · · · · · · · · · · · · · ·	
Mean G		Oh.		1 ^h .		2 ^h .		3h.		4 ^h .		5h.	
Tim	ne.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} & 1 & & \\ & 2 & & \\ & 3 & & 4 & \\ & & 5 & & \\ & & 5 & & \\ \end{pmatrix}$	E. by N. W.S.W. S.W. by W.	1bs. 0'0 1'5 3'0 2'0 0'0	E.N.E. W.S.W. W.S.W.	lbs. 0°0 2°0 2°5 2°5 0°0	E.N.E. W.S.W. W.S.W.	1bs. 0°0 2°0 3°0 3°0 0°0	N.E. by N. E. W.S.W. W. by S.	lbs. 0°2 2°0 3°0 2°5 0°0	N.E. by N. E. S.W. W. by S.	1bs. 0°2 2°0 3°0 3°0 0°0	N.E. E. S.W. W. by S.	lbs. 0°2 1°0 3°0 3°0 0°0
	6 7 8 9 10 11 12	E. by S. W.N.W. N.N.W. W.S.W. N. by W.	0°5 0°2 0°2 2°5 0°2 0°0	E. by S.  N. W.S.W. N.N.W.	0.5 0.0 0.2 3.0 0.2 0.0	E. by S.  N.N.W. W.S.W. N. by W.	0.2 0.0 0.5 0.0	E.S.E.  N.N.W. W. by S.  N. by W.	0.2 0.0 0.0 0.0 0.0	E.S.E. N.N.W. N. by W. W. by S.	0.2 0.2 0.2 1.5 0.0 0.2	E.S.E. N.W. N.N.E. S.W. by W. N.N.W. N.N.W.	1.5 0.5
DECEMBER	13 14 15 16 17 18 19	N.N.W.  N.E. by N.  W.N.W.	0°2 0°0 0°0 1°0 0°0 0°2	N.E. by N. W.N.W.	0.5 0.0 0.0 1.0 0.0 0.2	N.N.W.  N. by E.  N.E. by N.  O.W. by W.	1.0 0.0 0.2 1.0 0.0 0.2	N.N.W.  N.E. by N. N.E. by N. N. by E. N.W. by W.	1.0 0.0 0.2 0.5 0.2 0.2	N.N.W. W. N.E. N.E. N.W. by N.	2.0 0.2 0.2 0.0 0.0 2.0	N.N.W. W. E.N.E. N.E. N. by E. N.W.	1:8 0:2 0:2 1:6
	20 21 22 23 24 25	N.N.W. N.E. — S.S.E.	0.5 0.5 0.0 0.2	N.N.W. N.E. S.S.E.	1.0 0.5 0.0 0.2	N.N.W. N.N.E. S. by E.	0.2 0.5 0.0 0.2	N.N.W. N. by W. S. by E.	1.5 0.5 0.0 0.2	N.N.W. N.N.E. S. by E.	2·0 0·5 0·0 0·2	N. W. N. S. by E.	1.8 0.6 0.6 0.2
	26 27 28 29 30 31	E. by S.	0.0 0.0 0.0 0.2 0.0	N.N.W. E. by S.	0.0 0.5 0.0 0.0 0.0	W.N.W.  N. by W.  — — — —	0.0 0.0 0.0 0.0	N. by W. N.E. S. S.E.	0.0 0.2 0.2 0.2 0.2	N. by W. E. by N. S.W.	0.0 0.2 0.2 0.0	N. by W. E. S.W.	0.6
(continu	ıed)	1		1		1		1		I		1	
Mean G		12h.		13h.		14h.	1	15h.		16h.		17 ^h .	1
Tin	lie.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force
	$\begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{pmatrix}$	E. — W. by S. N.W. N.N.E.	lbs. 0°5 0°0 2°5 0°5 0°2	E. W. by S. W. by N.	lbs. 2 · 5 0 · 0 2 · 5 0 · 2 0 · 0	E. by N. W. by S. W.	lbs. 2 * 5 0 * 0 2 * 5 0 * 2 0 * 0	E. by N.  W. by S.  W.S.W.	2.5 0.0 3.5 0.2 0.0	E. by N.  W. W.S.W. N.N.E.	3.5 0.0 2.0 0.2 0.2	E. by N. S.W. S.W. by W. W.S.W. N.N.E.	5.0 0.8 2.8 0.2 0.8
	6 7 8 9 10 11 12	S.E. — N. N.W. by N. N.W.	0.2 0.0 0.0 0.2 0.2 0.2	E. by S. N. by E. N. by W. N. W. by N. N. by W.	0.2 0.2 0.0 0.2 0.2 0.5	E. by S. N. by E.  N.N.W. N.W.by N. N.N.W.	0.2 0.2 0.0 0.2 0.2 0.2 1.0	N.N.E. N.N.W. N.W. N.W.	0°0 0°0 0°2 0°2 0°5 0°5	N.E. N.N.W. N.W. N. W.	0.0 0.0 0.2 0.2 0.2 0.5	E. by S.  N.E.  N.W. by N.  N.W.	0.5 0.5 0.5 0.5 0.5 0.5
DECEMBER.	13 14 15 16 17 18 19	N.W. by W.  N.E.  N.E.  N.E.	0.5 0.0 1.0 0.2 0.0 1.5	N.W. by W.  N.E. by E.  N.E.  W.N.W.	0.5 0.0 1.5 0.2 0.0 1.0	N.W. by W. E. by N. N.E. W.N.W.	0.5 0.0 2.0 0.2 0.0 1.5	E. by N. N.E. W.N.W.	0.0 0.0 1.5 0.2 0.0 1.0	N.E. N.N.E. W.N.W.	0.0 0.0 1.0 0.2 0.0 1.0	N.E. N.N.E. N.W. W.N.W.	0.0 0.2 0.2 1.0
	20 21 22 23 24 25 26		0.0 0.0 0.0 0.0	w.s.w.	0.0 0.0 0.0 0.2 -	w.s.w. s.s.w.	0.0 0.0 0.0 0.2 -	S.W. by W. S.W. by S.	0.0 0.0 0.0 0.2 0.2	s.w. S.s.w.	0.0 0.0 0.0 0.0	s.w. s.s.w.	0.5
	26 27 28 29 30 31	N.N.W. E. S.W.	0°2 1°5 0°2 0°0	N.W. E. S.W.		N.W. by W. E. S.W.		N.W. by W. E. N.E.	1.0 3.0 0.0 0.5	N.W. by W. E. —	0.5 0.0 0.0 0.0	N.W. E. N.E. by N.	0.5 2.8 0.0 0.2

				DIRE	CTION	AND FORCE	OF TH	E WIND.					
6 ^h .		7 ^h .		8h.		9 ^h .		10 ^h .		11 ^h .			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	]	Time.
N.E. E. S.W. W. W. by N.	lbs. 0°2 0°5 3°0 2°5 0°2	E. by S. S.W. by W. W. by N. W.	lbs. 0°2 0°0 3°0 2°0 0°2	E.N.E. E. by N. W. by S. W. W. by S.	1bs. 0°2 0°2 3°5 0°5 0°2	E.N.E. E.N.E. W.S.W. W. by S.	lbs. 0°2 0°2 2°5 0°2 0°0	E.N.E. W. by S. N.W. by W.	1bs. 0°2 0°0 2°0 0°2 0°0	E. W. by S. N.W.	1bs. 0°2 0°0 2°5 1°0 0°0	1 2 3 4 5 6	
E.S.E. N.N.W. N.N.W. S.W. by W. N.W. N.N.W.	0.2 0.2 0.2 0.5 1.5 0.5	E.S.E. N.N.W. N.N.W. W.S.W. N.W.	0.2 0.2 0.2 0.2 0.2 1.5 0.5	E. N.N.W. N.W. by N. W.S.W. N.W. by W. N.N.W.	0.2	E. N.N.W. — N.W. by W. N.N.W.	0.2 0.2 0.0 0.0 0.5 0.5	E.S.E.  N.W. by W. N.W.	0.5 0.0 0.0 0.0 0.5 1.0	S.S.E.  N. by E.  N.W. by N.  N.W.	0°2 0°0 0°0 0°2 0°2 0°5	7 8 9 10 11 12 13	
N.N.W. W.N.W. E. N.E. by E. N. by E. N.W. by N.	1:0 0:2 0:2 0:5 0:2 2:0	N.N.W. E. N.E. by E. N. N.W. by N.	1.5 0.0 0.5 0.5 0.2 2.0	N.W. W.S.W. E. by N. N.E. W. by N.	1.5 0.2 0.5 0.2 0.2 2.5	N.W. N.W. by N. E. by N. N.E. W. by N.	1.5 0.2 0.5 0.2 0.2 0.2 2.5	W.N.W. E.N.E. N.E. N.W.	1.0 0.0 1.0 0.2 0.0 2.0	N.W. byW. N.E. N.E. N.W. byW.	0.5 0.0 1.0 0.2 0.0 1.0	14 15 16 17 18 19 20	DECEMBE <b>R.</b>
N.W. N. by W. S.W. by W.	0°2 0°5 0°0 0°2	N.W. — S.W. by W.	0.5 0.0 0.0 0.5	N.W. byW S.W. byW.	0.5 0.0 0.0 0.5	N.W. = S.W. by W.	0.5 0.0 0.0 0.5	N.W. — S.W. by W.	0.5 0.0 0.0 0.5		0.0 0.0 0.0 0.0	21 22 23 24 25	
S.W. by S.  N.W. by N. E. by S. S.W. by W.	0.5 1.5 1.5 0.2 0.0	S.W. by S. N.N.W. E.S.E. W.S.W.	0.2 1.0 0.2 1.0 0.0	S.S.W. — N.W. by N. E. by S. W.S.W. N.E. by E.	0.5  1.0 0.5 1.0 0.2	S.S.W.  N.N.W. E. S.W. N.E. by N.	1.5 1.5 0.5 0.5 0.2	S.S.W.  N.N.W. E. by S. S.W. N.E. by E.	1.5 0.5 2.0 0.2 0.2	S.S.W.  N.N.W. E. by N. S.W.	2.5 0.2 1.5 0.2 0.0	26 27 28 29 30 31	
		1										1	
18h.		19 ^h .	77	20h.	L'oras	21h.	Force	22h.	Force.	Direction.	Force.		Göttingen Lime.
E. by N. W. by S. W.S.W. W.S.W.	lbs. 5.5 0.5 1.5 0.2	E. by N. W. by S. W.S.W. W. by S.	lbs. 5.0 1.0 2.0 0.2	E. by N. S.W. by W. W.S.W. W. by S.	lbs. 4.0 2.0 1.5 0.2	E. by N. S.W. W.S.W. W. by S.	lbs. 4.5 1.0 1.5 0.2	E. by N. W.S.W. W.S.W.	lbs. 4.0 2.5 1.5 0.0	E. W.S.W. W.S.W.	1bs, 2°5 2°0 2°0 0°0	1 2 3 4 5	
E.S.E.  N.E. N.W. by N. N.W.	1.5 0.0 0.0 0.2 0.2 0.2	E. by S.  N. by E.  N.E.  N.N.W.  N. by E.	1'0 0'0 0'2 0'2 0'5 0'2	E. by S.  N. by W.  N.E.  N.N.W.  N. by W.	0.5 0.0 0.2 0.2 0.2 0.2	E. by S.  N. by W.  N.E. by E.  N.N.W.  N. by W.	1.0 0.0 0.2 0.2 0.2 0.2	E. by S.  N. E.N.E. N.N.W.	1:0 0:0 0:2 0:2 0:0	E. by S. W.N.W. N. E. N. by W.	1:0 0:2 0:2 1:0 0:2 0:0	6 7 8 9 10 11 12	
N.E. N.N.E. N.W.	0.0 0.0 0.0 0.5 0.2 0.2	N.E. N.W.	0.0 0.0 0.0 0.0 1.5 0.0 0.2	  N.E.  N.W.	0.0 0.0 0.0 1.5 0.0 0.2	N.E. W.N.W.	0.0 0.0 0.0 0.0 1.5 0.0 0.2	N.E. W.N.W.	0.0 0.0 0.0 1.5 0.0 0.2	N.N.W. N.E. by N. W.N.W.		12 13 14 15 16 17 18 19	DECEMBER.
W.S.W.	- 0.2 0.0 0.0 0.0 - 1.0	W.S.W. N.E. by N. — — N.W.	0.5 0.5 0.0 0.0 0.0	W.S.W. N.E. by N. — — — N.W.	0·2 0·2 0·0 0·0 - 0·2	W. N. by E.  N.W.	0.5 0.5 0.0 0.0 0.0	W.N.W. N. by E. — —	0.0 0.0 0.0 0.0	W.N.W. E. by N.	0.0 0.0 0.0 0.0 0.0	20 21 22 23 24 25	[
N. E. N. by W.	0.0 0.2 1.5 0.0 0.2	 N.E. by N. E.  N.	0.0 0.2 2.5 0.0 0.2	— — E. N.	0.0 0.0 2.2 0.0 0.0	— — — E. N.	0.0 0.0 0.0 0.0 0.0	— — — E. — N.	0.0 0.0 1.5 0.0 0.2	E. by S.	0.0 0.0 1.0 0.0 0.0	26 27 28 29 30 31	

				DI	RECTIC	N AND FOR	CE OF	THE WIND.					
	ottingen	O ^h .		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
Tim	ie.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Fore
	$\begin{pmatrix} 1\\2\\3 \end{pmatrix}$	N. W.S.W.	lbs. 0°2 1°5	N. S.W.	1bs. 0'2 1'0	W. by S.	lbs. 0.0 2.0	N. by E. S.W. by S.	lbs. 0°2 1°5	N. by E. S.W. by W.	lbs. 0°2 2°0	N. by E. S.W. by W.	1bs. 0
	4 5 6 7 8	E. by N. W.S.W.  S.W. by W. W. by S.	2:0 4:5 0:0 0:0 3:5 0:5	E. by S. S.W.  S.W. by W. W. by S.	2.5 5.5 0.0 0.0 4.0 0.5	E. by S. S.W. by W.  S.W. by W. W. by S.	3.5 6.5 0.0 0.0 3.0 0.2	S.W. by W. N. by W. S.W. by W. W. by N.	0.0	W. by S.  N.N.W. S.W. by W.  W.	3.0 5.0 0.0 1.0 3.5 0.2	E. S.W. by W. N.W. N.W. by N. W.S.W. W.	0.
JANUARY.	10 11 12 13 14 15 16	S.W. by W.S. E. W.N.W.	0.0 0.5 0.2 0.0 1.5 0.5	S.W. by W. S. E. W.N.W.	0.0 0.2 0.2 0.0 2.0 2.0	W.S.W. S. E. N.W. by W.	0.0 0.2 0.2 0.0 2.5 2.5	W. by N. W.S.W. S. ————————————————————————————	0.2 1.0 0.2 0.0 1.5 2.0	W. by S. W.S.W. S.W. by S. E. by S. W.N.W.	1.5 0.2 0.0 0.5 2.0	S.W. by W. W.S.W. S.W. E.S.E. W. by S.	1 0 0 0 0 2
JAN	17 18 19 20 21 22 23	S. by W. W.N.W. W.S.W. W. by N. W.S.W. S.W. S.W.	0.5 1.5 0.5 0.2 1.0	S.S.W. N.W. W.S.W. W. by N. W. by S. S.W. by W.	0.2 1.5 0.5 0.5 2.0 1.0	S.W. by S. N.W. W.S.W. W. by N. W. by S. S.W. by W.	0.2 2.0 0.5 1.0 1.5 0.5	W. by N. W.S.W. W. by N. W. by S. W.S.W.	0.0 2.0 0.5 3.0 2.0 1.0	W. W.S.W. W. by N. W. by S. W.S.W.	0.0 3.0 0.2 3.0 1.5 2.0	W. by S. W.S.W. N.W. S.W. by W.	0 3 0 2 1 2
	24 25 26 27 28 29 30	E.N.E. N. by E.  N.N.W.	0.0 2.2 0.0 0.0 0.0 3.0	E. N. by W.  N.N.W.	0.0 2.0 0.5 0.0 0.0 0.0	E. by S. N. by W.  N.N.W.	0.0 2.0 0.2 0.0 0.0 2.5	N.E. E. by S. N.W. by N.	0.5 1.0 0.5 0.0 0.0 2.5	E. by S. N.N.W.	0.2 0.2 0.2 0.0 0.0 0.0 2.0	E.N.E. S. N.N.W.  N.E. N. by W.	0.000
(continu	öttingen	12 ^h .		13h.		14h.		15h.	1	16 ^h .		17h.	
		Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	For
	$\begin{pmatrix} 1\\2\\3 \end{pmatrix}$	E.N.E. S.W. by W.	•	E.N.E. W.S.W.	lbs. 1.5 0.2	E.N.E. W.S.W.	lbs. 2.0 0.2	E.N.E.	lbs. 2.0 0.0	E	2.0 0.0	E	0
	5 6 7 8 9	E. S.W. W.N.W. S.W. W.	2.5 2.0 0.0 2.5 1.0 0.5	E. S.W. W.N.W. S.W. W.S.W.	2.0 1.5 0.0 2.5 1.0 1.0	E. S.W. — W. by N. S.W. W.S.W.	1.0 2.0 0.0 2.5 2.0 1.5	E. W.S.W. N.E. W. by N. W.S.W. W.S.W.	0.5 1.5 0.2 2.5 1.5	S. W.S.W. N.N.E. W. by N. S.W. W.S.W.	1.0 1.5 0.2 2.5 1.0 1.0	S. W.S.W. N. by E. W. by N. W.S.W. W.S.W.	4 1 0 1 1
JANUARY.	10 11 12 13 14 15 16	W. by S. S.W. S.E. by S. W.N.W.	2:0 0:0 1:0 0:0 0:2 3:5	W. by S. S.W. S.W. by S. W.N.W.	1.5 0.0 0.2 0.0 0.2 3.5	S.W W.N.W.	2.0 0.0 0.2 0.0 0.0 3.0	W.S.W. S.W. by W  W. by N.	1.5 0.0 0.2 0.0 0.0 2.0	W.S.W. S.W. by W. W. by N.	1.0 0.0 0.2 0.0 0.0 2.5	W.S.W. S.W. by W. N.N.E. W. by N.	1 0 0 0 0 0
INI	17 18 19 20	W. by N. W. W.S.W. N. by W.	0.5 1.0 1.0 0.2	W. by N. W. W.S.W. W.S.W.	0.5 0.2 1.5 0.0 3.0	N.W. by W. W. W.S.W. W.S.W.		W. by N. S.W. by W. W.S.W. W. by S. W.S.W.	1.0 1.0 1.0 0.5 2.0 0.0	W. by N. S.W. by W. W.S.W. W.S.W. S.W	1.5 1.5 0.5 0.5 2.5 0.0	W. by N. S.W. by W. W.S.W. W.S.W. W.S.W.	0 1 0 1 2 0
37	$ \begin{array}{ c c c } \hline 21 \\ 22 \\ 23 \\ \end{array} $	S.W. by W	0.0		0.0	_							-

				DIR	ECTION	AND FOR	CE OF 1	THE WIND.					
6 ^h .		7 ^h .		8h.		9 ^h .		10 ^h .		11 ^h .			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	<u> </u>	Time.
N.N.E. S.W. by W.	lbs. 0°2 2°0	N.E. by N. S.W. by W.	lbs. 0°2 1°5	N.E. S.W. by W.	1 to 1 to 1 to 1 to 1 to 1 to 1 to 1 to	N.E. S.W.	1bs. 0°2 1°5	N.E. S.W. by S.	1bs. 0°2 1°5	E.N.E. S.W.	lbs. 1 '0 0 '2	1 2 3	
W.S.W. N. W. W.S.W. W.S.W.	2.5 3.5 0.2 2.5 6.5 0.2	W.S.W.  N.W. W.S.W. W.	2.5 3.5 0.0 2.5 4.5 0.2	S.W. N.W. S.W. by W. W.S.W.	3.0 0.0 3.2 3.0 1.0	E. S.W. — N.W. W.S.W. W. by N.	3.0 3.0 0.0 3.5 2.5 1.0	E. by S. S.W. N.W. S.W. by W. W. by N.	3.0 0.0 3.0 2.5 1.0	E. W.S.W. W.N.W. S.W. by W. W. by N.	2.5 2.5 0.0 2.5 2.0 0.5	4 5 6 7 8 9	
W.S.W. W. S.W. by S. E.S.E. N.W. by W.	2:5 2:5 0:2 0:0 0:2	W.S.W. W. S.W. S.W. by W. S.S.W. W.N.W.	2·0 2·0 0·2 0·2 0·2 3·5	W. W. S.W. by S. W.S.W. S. by W. S. by W. N.W.	1.5 1.5 0.2 0.2 0.2 0.2 3.5	W. W. S.W. by S. W.S.W. S. N.W.	1.0 0.5 0.2 0.2 0.2 4.5	W.S.W. W. by S. S.W. by S. W.S.W. E.S.E. W.N.W.	0.5 0.2 0.2 0.2 0.2 0.2 4.0	W.S.W. S.W. by S.  W.N.W.	1.5 0.0 1.5 0.0 0.0 3.0	11 12 13 14 15 16 17	JANUARY.
W. W.S.W. N.W. by N. W.S.W. W.N.W.	0.0 3.0 1.5 1.5 2.0	W.N.W. S.W. by W. N.N.E. W.S.W. W. by N.	0.0 2.5 1.5 1.0 1.5 3.0	W.S.W. W. by N. S.W. E. W. by S. W. by N.	0.5 2.5 1.0 1.5 1.0 2.0	W. by S. W. by N. S.W. E. W. by S. W. by N.	2:0 2:5 1:0 1:0 1:5	W. W. by N. W.S.W. N. by W. W.S.W. W.S.W. W. by N.	1.5 2.5 0.5 0.5 1.0 1.0	W. by S. W. by N. W.S.W. N. by W. S.W. S.W.	0.5 1.5 0.5 0.2 1.5 0.0	18 19 20 21 22 23 24	JA
E.N.E. S. N.N.W. N.E. N.W.	0.5 0.5 1.0 0.0 0.2 2.5	E. by S. N.W. by W. N. by W. E.N.E. N.E. by E. N.W. by N.	0.2 0.5 1.0 0.2 0.5 2.0	E. by N. N. W. by N. N. by W. E. by N. N.W. by N.	0.2 0.5 1.0 0.0 1.0 2.0	E. by S. N.N.W. N. by W.  N.E. by E. N.N.W.	0°2 0°5 0°0 2°0 2°0	E. by S. N.W. by N. N. by W.  N.E. N. by W.	0.5 0.5 0.0 1.5 0.5	E. by S. N.W. N. N.E. N.E.	0.5 0.2 0.0 1.0 0.5	25 26 27 28 29 30 31	
							· — —	<u> </u>	<u> </u>	1			
18h.								1		0.01		112	
Direction	Force	19h.	Force	20h.	Force	21 ^h .	F ce	22h.		23h.	1		Göttingen Time.
Direction. S.E.	Force.	19 ^h .  Direction.	Force.  lbs. 0°0	Direction.  W.	Force.  lbs. 1.5	Direction. W.S.W.	1 to s.	Direction.  W.S.W.	Force.  lbs. 1.5	23h. Direction. S.W.	Force.  lbs. 2 ° 0	1	
S.E. S.W. by S. W. by N. N. by E. W. by N. W. S.W.	lbs. 1'0  0'0 3'5 1'5 0'5 1'0 1'5		lbs.	Direction.	lbs.	Direction.	lbs.	Direction.	Force.	Direction.	Force.    lbs.   2 * 0	1 2 3 4 5 6 7 8	
S.E.  S.W. by S. W. by N. N. by E. W. by N.	lbs,   1 · 0   -	Direction.  N.E. by N. S.W. by S. W.N.W. N. W.	lbs. 0°0 	Direction.  W. E. S.W. by S. W. by N. N. by E. W.	lbs. 1'5	Direction.  W.S.W. E. S.W. by S. W. by S. N. by E. W. by S.	1 bs. 1 · 5 3 · 5 1 · 0 0 · 2 3 · 0 0 · 5 	Direction.  W.S.W. E. S.W. by S. W. by S. N. W.S.W.	Force.	S.W. E. by N. S.W. N. S.W.by W.	Force.    Ibs.   2.0	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	Time.
S.E S.W. by S. W. by N. N. by E. W. by N. W.S.W S.W S.W S.W S.W S.W S.W.	lbs,   1 · 0   0 · 0   3 · 5   1 · 5   0 · 0   1 · 5   0 · 0   0 · 2   0 · 0   0 · 5   1 · 0   0 · 5   0 · 5   1 · 0   3 · 0   3 · 0	Direction.  N.E. by N. S.W. by S. W.N.W. N. W. W.S.W.  W.S.W.  W.S.W.  W.S.W.  W.S.W.	1bs. 0'0	Direction.	lbs. 1 ' 5	Direction.  W.S.W. E. S.W. by S. W. by S. N. by E. W. by S. W. by S. W. by S. W. by S.	1 bs. 1 · 5 3 · 5 3 · 5 1 · 0 0 · 2 3 · 0 0 · 5 0 · 0 0 · 2 0 · 0 0 · 2 0 · 0 0 · 2	Direction.  W.S.W. E. S.W. by S. W. by S. W.S.W. W. by S.  E. S.W. by S.  S.W. by S.	Force.	S.W. E. by N. S.W. N. S.W.by W. W. by S.  S.W. by W. E. by S.	Force.   Ibs.   2.0	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	
S.E S.W. by S. W. by N. N. by E. W. S.W S.W S.W S.W S.W S.E W.N.W. S.W. by W. S.W. by W. S.W. W.S.W. W.S.W.	lbs,   1 · 0   0 · 0   3 · 5   1 · 5   0 · 5   1 · 0   0 · 0   0 · 5   0 · 5   0 · 5   1 · 0   1 · 0   1 · 0   0 · 5   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   1 · 0   0 · 5   0 · 5   1 · 0   0 · 5   0 · 5   1 · 0   0 · 5   0 · 5   1 · 0   0 · 5   0 · 5   1 · 0   0 · 5   0 · 5   1 · 0   0 · 5   0 · 5   0 · 5   1 · 0   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5   0 · 5	Direction.  N.E. by N. S.W. by S. W.N.W. W. W.S.W. W.S.W. W.S.W. W. by S. S.W. N. by W. E.S.E. W.N.W. W.S.W. W.S.W. W.S.W. W.S.W.	lbs. 0'0	Direction.  W. E. S.W. by S. W. by N. N. by E. W. W.S.W.  W.S.W.  N. by W. S.E. by E. N.W. by W. W.S.W. W.S.W. W.S.W. W.S.W. W.S.W.	lbs. 1 · 5 	Direction.  W.S.W. E. S.W. by S. W. by S. W. by S. W. by S. W. by S. W. S.W. S.W. S.W. S.W. S.E. N. by W. W.S.W. W.S.W. W.S.W.	1 bs. 1 · 5 3 · 5 1 · 0 0 · 2 3 · 0 0 · 5  0 · 0 1 · 0 0 · 2 0 · 0 0 · 2 0 · 5 0 · 2 2 · 5 0 · 5 0 · 2 1 · 5	Direction.  W.S.W. E. S.W. by S. N. W.S.W. W. by S.  S.W.by W. S.W. by W. S.W. by W. S.E. by S. N.W. by W. W.S.W. W. by N. W.S.W.	Force.	S.W. E. by N. S.W. by S. W. by S. S.W. by W. S.S.W. E. by S. W. by N. S. by E. W.N.W. W.S.W. W. by N.	Force.    Ibs.   2 * 0   -	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	Time.

\$			······	Dì	RECTIO	ON AND FOI	RCE OF	THE WIND					
Mean Göttii	$_{ m ngen}$	O _h .		1h.		2h.		3 ^h .		4 ^h .		5h.	
Time.	]	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	1 2 3 4 5 6 7	— W.N.W. N. by W. N.	lbs. 0.0 0.0 0.0 5.5 0.2 0.2	N.W. by W.	lbs. 0°0 0°0 0°0 4°5 0°0 0°0	E. by N. N.W. by W.	lbs. 0.0 0.0 0.2 6.0 0.0 0.0	E. by S. E.N.E. N.W. N. N. by W.	lbs. 0'0 0'2 0'2 4'0 0'5 0'2	E.S.E. E.N.E. N.W. N. by E. N.N.W.	lbs. 0'0 0'2 0'2 3'0 0'2 0'2 -	E.S.E. E. by N. N.W. N. by E. N. by W.	lbs. 0'0 0'2 0'2 3'0 0'2 0'2
FEBRUARY.	8 9 10 11 12 13 14	W. by S. N.W. — — W. by N.	0.5 0.5 0.0 0.0 0.2 0.0	S.W. N.W. by W.	0.2	S.W. N.W. by W. N.	0°2 0°2 0°0 0°2 0°0	S.W. W. N. by W. S.W. by S.	0.5 0.2 0.0 0.2 0.0 0.2	W.S.W. W. N.N.W. N. by W. S.W. by W.	l —	S.W. W.S.W. W. by N. S.W. by W.	0.2 0.0 0.2 0.0 0.2
FEBRI	15 16 17 18 19 20 21	N. by W. E.N.E. N.N.E. E.N.E.	0.2 0.0 0.2 0.0	N. by W. N.E. N.N.W.	0.5 1.0 0.2 0.0 0.0 1.0	N. by W. E. by S. N.N.W. E.N.E.	2.0 1.0 0.2 0.0 0.0 1.0	N.N.E. E. by N. N.N.E. E. by N.	1.5 1.0 0.0 0.2 0.2 0.5	N. E.N.E. S.W. E.S.E. N.N.E. E.N.E.	1:0 0:5 0:5 0:2 0:2 0:5	N.N.E. N.E. S.W. S.E. N.N.E. N.E. by E.	1 '0 0 '5 0 '5 0 '2 0 '5 -
	22 23 24 25 26 27 28	N.N.E. N. by W. N.E. N.N.E. E.	0.2 0.2 0.0 0.2 0.2 0.2 4.0	N. by W.  N.E.  N.N.E.  E.	0.0 0.2 0.0 0.2 0.2 4.5	N.E. N.E. N.N.E. E.	0°0 0°2 0°0 0°2 0°2 4°5	N.N.E. N. N.E. by E. N.N.E. E.	0·2 0·2 0·0 0·2 0·2 5·5	N.N.E. N. N.E. by E. E.S.E. E.	0.2 0.0 0.2 0.2 0.2 5.0	N. by W. N.E. by N. E. by S. E.	0.2 0.0 0.2 0.2 5.5
(continued)	CII		!	i		1						1 Ph	
Mean Göttin Time.	gen }	12h.	Forms	13h.	Force.	14h.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
FEBRUARY.	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	S.E. N.N.W. W.N.W.  W. by N. W. by S. N. by W.  W.  E.N.E.  E.N.E.  E.N.E.  E. by N. S.S.W.	lbs.   0 0 0 2 12 0 0 0 0 0 0 0 0 0 0 0 0 0 0	S.E. N.W. N.W. by W. N. by E.  N.W. by N.  W. by S. N. by W. W.N.W.  N.E.  W.N.W.  E.  N.E.  S.W.	lbs. 0.0 0.2 9.0	S.W. by S. S.E. N.W. N.W. by W. N. by E.  W. by S. N. by W. W.N.W.  N.N.E. N. by E. W.N.W.  E.N.E.  E.N.E.  E. S.W.	lbs. 0°2 0°2 10°0	S.W. by S.  N.W. N.W. by W. N. by W.  E. by S. E. N.N.W.  N. by W. W.N.W.  N. by E. N. E.N.E.  E.N.E.  E.N.E.  E.N.E.  S.W.  N.E.  N.E.  S.W.	lbs. 0°2 0°0 12°0	N.W.   N.W.   N.W.   N.W.   N.W.   N.W.   N.W.   N.M.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.   N.N.E.	lbs.   0.0   0.0   0.2   0.0   0.5   0.2   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.5   0.0   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5	S.  N.W. N.W. by W. N. by W.  E. by N.  W.S.W.  N.E. N.N.W. N. by E. E.N.E.  E.N.E.  N.N.E.  S.W.  E.S.W.	lbs. 0°2 0°0 8°0

6 ^h .		7 ^h .		8 ^h .		9 ^h .		10h.		11h.			Göttinge Vimo
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		'ime.
E. by S. E.S.E. E.N.E. W.N.W. N. by W.	lbs. 0'2 0'2 0'2 1'5 0'2 0'2	E. by S. E.N.E. N.W. N. by W. N. by W.	lbs. 0°0 0°2 0°2 2°0 0°2 0°2 0°2	S. by W. E.S.E. N.N.W. N.W. S.W. N. by W.	lbs. 0°2 0°2 0°5 2°5 0°2 0°2	S. by W. E.S.E. N.N.W. N.W.	lbs. 0°2 0°2 3°0 2°5 0°0 0°2	S.S.W. E.S.E. N.W. W. by N.	lbs. 0 ' 2 0 ' 2 4 ' 0 2 ' 0 0 ' 0 0 ' 2	S.S.W. S.E. N.N.W. W.N.W.	lbs. 0°2 0°2 5°5 1°5 0°0 0°0	1 2 3 4 5 6	
S.W. W.S.W. N. by W. W.	$\begin{array}{ c c }\hline -\\ 0.2\\ 0.2\\ \end{array}$	S.W. by S. W. by S. S.W. by W. W. by S. S.S.W. W.S.W.	0·2 0·2 0·2 0·5 0·2 0·2	S.W. W. by S. S.W. W. by S. S. by W. W.S.W.	0.2 0.2 0.2 1.0 0.2 1.0	S.W. W.S.W. S.W. W. by S. N. by W. W. by S.	0·2 0·2 0·2 1·0 0·2 0·5	S.W. W.S.W. S.W. by W. S.W. by W. N. by W. W. by S.	0.2 0.2 0.5 1.0 0.5 1.0	S.W. by W. W.S.W. N. by W. W. by S.	0.0 0.0 0.2 0.5 2.0 0.2	7 8 9 10 11 12 13 14	ARY.
M. N.E. W. by W. S. by W. N.N.E. E. by N.	1.5 0.2 0.5 0.2 0.2 1.0	N. E. by N. S. by W. S. by W. E. by N.	1.5 3.0 1.0 0.2 0.0 1.0	N. E. W.S.W. S.S.E. E. by N.	1.0 3.0 1.0 0.2 0.2 1.0	E.N.E. W. S.E. by S. E. by N.	0.5 2.0 1.0 0.2 0.0 0.5	N.N.E. E. by N. W. E. by S.  E. by N.	0.2 2.0 1.0 0.2 0.0 0.5	N.N.E. E.N.E. W. E. — E.N.E.	0.2 1.0 0.5 0.2 0.0 0.5	15 16 17 18 19 20 21	FEBRUARY.
N. E.S.E. E.N.E. E. by N. E.	0.0 0.0 0.2 0.2 0.5 5.5	N.N.E. E.S.E. E.N.E. E. by N. E.	0.2 0.0 0.2 0.2 1.5 5.0	N. — E. by S. E. by S. E. by N. E. —	0.2 0.0 0.2 0.2 1.0 3.5	N. — E. by S. E.S.E. E.N.E. —	0.2 0.0 0.2 0.2 1.5 3.0	N. by E. E. by S. E. by N. E. —	0°2 0°2 0°2 1°5 1°5	E. N.E. E. by N. E	0.2 0.0 0.2 0.0 2.5 1.5	22 23 24 25 26 27 28	
18h.		19 ^h .		20 ^h .		21 ^h .		22 ^h .		23 ^h .		Mean	
18 ^h .	Force.	19 ^h .	Force.	20 ^h .	Force.	21 ^h .	Force.	22 ^h .	Force.	23 ^h .  Direction.	Force.		Göttin į
Direction.  N.W. W. by W.	lbs. 0'0 0'0 5'0 0'2 0'2		Ibs. 0'0 0'2 7'0 0'2 0'2 - 0'0	E.S.E. W.N.W. N.W. by N. N. by W.	lbs. 0.0 0.2 5.0 0.5 0.2 0.0	Direction.  W.N.W. N.W. by N.	lts. 0.0 0.0 4.0 0.2 0.0 - 0.0	Direction.  W.N.W. N.W. by N.	lbs. 0'0 0'0 4'0 0'2 0'0 —	Direction.  W.N.W. N.N.W.	Ibs.   0.0   0.0   5.0   0.2   0.0     0.0	1 2 3 4 5 6 7	
Direction.  N.W. N. by W. N.  N.E. S.E.	lbs.   0.0   0.0   5.0   0.2   0.2   0.5   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	S.S.E. N.W. by W. N.W. N. by W.  N.N.E.	lbs.   0 0 0   2   7 0 0 0 2   0 0 2	E.S.E. W.N.W. N.W. by N.	lbs.   0.0   0.2   5.0   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	Direction.  W.N.W. N.W. by N.  N.N.W.  N.W. by W.	lbs.   0.0   0.0   4.0   0.2   0.0	Direction.  W.N.W. N.W. by N.  N.N.W.  W. by N.	lbs.   0.0   0.0   4.0   0.2   0.0   0.5   0.0   0.0   0.0   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	Direction.  W.N.W. N.N.W.  N.W. byW.  N.W. byW.	Ibs.   0.0   0.0   5.0   0.0   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.2   0.2	1 2 3 4 5 6 7 8 9 10 11 12 13 14	ime.
N.W. N. by W. N.E. S.E.	lbs.   0.0   0.0   5.0   0.2   0.2   0.5   0.2   0.0   0.0   0.0   0.0   0.0	S.S.E. N.W. by W. N.W. N. by W.  N.N.E.	1bs. 0'0 0'2 7'0 0'2 0'2 - 0'0 0'5 0'0 0'0 0'0 0'0	E.S.E. W.N.W. N.W. by N. N. by W.	lbs.   0.0   0.2   5.0   0.5   0.0   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	Direction.  W.N.W. N.W. by N.  N.N.W.	lts. 0.0 0.0 4.0 0.2 0.0 - 0.0 0.5 0.0 0.0 0.0 0.0 - 0.0	W.N.W. N.W. by N.  N.N.W.  W. by N.	lbs. 0.0 0.0 4.0 0.2 0.0 - 0.0 0.5 0.0 0.0 0.0 0.2	Direction.	Ibs.   0.0   0.0   5.0   0.2   0.0   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	1 2 3 4 5 6 7 8 9 10 11 12 13	

				DI	RECTIO	N AND FOR	RCE OF	THE WIND.	•				
Mean Göt Time		O ^h .		1 ^h .		2h.		3 ^h .		4 ^h .		5 ^h .	
Time	е.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$   \begin{pmatrix}     1 \\     2 \\     3 \\     4 \\     5 \\     6 \\     6   \end{pmatrix} $	W. — N.W. by N. E. —	0.2 0.0 0.2 0.2	W.N.W. S. by E. N.E. by N.	0.5 0.0 0.2 0.0 0.2 0.0	W.N.W. S. by E. N.W.by N. N.	1.0 0.0 0.2 0.2 0.0	N.W. by W. W.N.W. S.S.E. N.W. N. E.N.E.	1.5 0.2 0.2 0.2 0.2 0.2	N.W. W.N.W. S.E. by S. N.N.W. E. by N.	3.0 0.2 0.2 0.2 0.0 0.5	N.W. W.N.W. S.E. by S. N. by W.	2.5 0.5 0.2 0.2 0.0 0.0
	7 8 9 10 11 12 13	N.N.E. N.W. by N. N. by W. N. by W. N. by W.	0.0 0.2 0.2 0.2 0.2 0.2	N.E. N.W. by N. N. by W. N.	$0.0 \\ 0.2 \\ 0.2$	E. E. N.E. S.W. by W. N. by W. N.	$ \begin{array}{c c}  - & \\  0.2 \\  0.5 \\  0.2 \\  0.0 \\  0.2 \\  0.2 \end{array} $	E. by N. W.S.W. W. S. W. N. by W.	0.5 1.5 0.2 0.2 0.2 0.0	N.W. E. W.S.W. N.	0.5 2.5 0.2 0.2 0.2 0.0	W.N.W. E. S.W. by W. N. by E. N. by E.	0.5 1.5 0.5 0.2 0.2 0.0
MARCH.	14 15 16 17 18 19 20	W. by S. W. by N. W E.N.E.	0.2 0.5 0.5 0.0 0.0 0.0	S.W. by W. W.N.W. W. ———————————————————————————	0.5 0.2 0.2 0.0 0.0 0.0	S.W. by W. W.N.W. W. S.W. E.N.E.	1.5 0.5 0.5 0.2 0.0 0.2	W.S.W. N.W. by W. W. by S. — N. by E. E.	2.0 0.2 1.0 0.0 0.2 0.2	W.S.W. W.N.W. W. by S. W.S.W. N. by E.	1.5 0.2 1.0 0.2 0.2 0.2	W. by S. W. by N. S.S.W. S.W. S.S.E. E.	1.0 0.2 0.5 0.2 0.2 0.5
	21 22 23 24 25 26 27	N.E. W. W.N.W. N.N.W.	0.5 0.0 0.2 0.5 0.5 4.5	N.E. S.E. by S. W.N.W. W.N.W. N.N.W.	0.5 0.2 0.5 0.5 0.5 4.0	E. by N.  W.N.W. W.S.W. N.W. N.W. by N.	0.5 0.0 1.0 0.5 1.0 4.5	E. by N. E.S.E. W.N.W. W. N.W. by N. N.W. by N.	0.2 0.2 0.5 2.0 1.0 5.0	E. W.N.W. W. N. N.W. by N.	1	E. S. W. W. N. by W. N.W. by N.	0°2 0°3 0°5 2°0 1°5 6°0
	28 29 30 31	E. by N. E.N.E.	0.5 0.5 0.0	E.N.E. N.E. N.	0·2 0·5	N.E. E.N.E. N. by W.	$     \begin{array}{c c}                                    $	E. N.	0.0 1.0 1.2	E.S.E. E.N.E. N. by W.	0.5 0.5 0.5	E.S.E. E. N. by W.	0.2 0.2 0.2
(continu	ued)	Toh		Joh		7.15		15 ^h .		16 ^h .		17 ^h .	
Mean Göt Time		Direction.	Force.	13 ^h . Direction.	Force.	14 ^h . Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$ \begin{array}{c c}  & 1 \\  & 2 \\  & 3 \\  & 4 \\  & 5 \\  & 6 \end{array} $	W.N.W E. by N.	lbs. 2 * 5 0 * 0 0 * 0 0 * 0 0 * 0 1 * 5	W  E. by N.	lbs. 1 '0 0 '0 0 '0 0 '0 0 '0 1 '5	W. by N.  N.N.E.  E.	lbs. 0°5 0°0 0°0 0°2 0°0 2°0	W  E. by N.	lbs. 0.5 0.0 0.0 0.0 0.0 0.0 2.0	W.   E.	lbs. 0°5 0°0 0°0 0°0 0°0 2°0	W.N.W.  N. by W.  E. by N.	lbs. 0.5 0.0 0.2 0.0 0.0 1.0
	7 8 9 10 11 12 13	N. E. W. N.N.E. S.W. by S. W.N.W.	1.5 2.0 1.5 0.2 0.2 0.2	N. E. W.N.W. N.N.E. N.	0.5 2.5 0.5 0.2 0.2 0.2	N. E. N.W. by W. — N. by W. N.N.W.	0.0 0.2 0.2	N. by W. N. by W. N. by W.	0.2 2.5 2.0 0.5 0.2 0.0	N. E. by S. N. by W. N. by W. N. by W.	0.2 2.0 1.5 0.5 0.5	E.N.E. N. by W. N. by W. N.	0.0 0.2 1.0 0.0
MARCH.	14 15 16 17 18 19 20	W.S.W. N.W. by N. S.S.W. N.W. S.E. by E.	1.0 2.0 0.2 0.0	W. by S. W.N.W. S.W. by S. N.W. by W.	0.0	W. W.N.W. S.W. N.W. by W.	0.0	W. by S. W.N.W. W.S.W. N.N.W.	0.5 0.5 0.5 0.2 0.0 3.0	W. by N. W.S.W. N.N.W. E. by N.	0.0 0.2 0.2 0.2 0.2 3.0	W. W.S.W. W.N.W. E. by N. N.N.W.	0.0 0.2 0.2 0.2 0.2 2.5
	21 22 23 24 25 26 27	S.E. by S. W. S. by W. W.N.W. N.N.W.	0.2 0.2 0.5 0.5 3.0 2.5	S. W.N.W. N. by W. N.W.by W.	0.0 0.0 0.2 0.2 3.0 2.0	S. by E. S.S.W. W.N.W. N. N.W.by W.	0.2 0.0 0.2 0.2 3.0 3.0	S. by E. W. S.S.W. N. by W. W.N.W.	0.2 1.0 0.2 0.0 4.0 2.5	W. by N. S.S.W. N. by W. W.N.W.	0.0 1.0 0.2 0.0 4.0 0.5	W. by S. S.E. by S. N. by W. W.N.W.	0.0 1.0 0.2 0.0 4.0 0.5
	28 29 30 31	N. E.S.E. N.	1'0 1'0 0'2	N. by E. E.S.E. N.	0.5 1.5 0.2	N.N.E. E.S.E. N.	0.2 1.5 0.2	N.E. N.E.	0.5 1.5 0.0	N.E. N.E.	0.0 0.2 0.0	E.N.E. N.E. by N.	0.5 0.2 0.0

				DIRE	CTION	AND FORCE	E OF T	HE WIND.				_	
6h.		7 ^h .		8h.		9h.		10h.		11 ^h .	1		Göttingen Time.
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	]	Time.
W.N.W. W.S.W. S.S.E. N.W. by N. S. E.	lbs. 2 · 5 0 · 2 0 · 2 0 · 2 0 · 2 0 · 2 0 · 5	W. by N. W.S.W. S.E.  E. by N.	lbs. 2 '8 0 '2 0 '2 0 '0 0 '0 0 '0 0 '2	W. by N. W. by S. E. N.N.W.  E. by N.	lbs. 2 · 5 0 · 2 0 · 2 0 · 2 0 · 0 0 · 5	W. by N. S.W. E. by S. W.N.W. S. E.	lbs. 2 · 5 0 · 2 0 · 2 0 · 2 0 · 2 0 · 2 0 · 5	W.N.W. S.W. E. by S. N.W. S. by E. E. by N.	lbs. 2 · 5 0 · 2 0 · 2 0 · 2 0 · 2 1 · 5	W.N.W. S.W.  S.S.E. E. by N.	lbs. 2 · 5 0 · 2 0 · 0 0 · 0 0 · 2 1 · 5	1 2 3 4 5 6 7	
W.N.W. E. W.S.W. N. by E. N. by E. N.W. by N.	1.0 1.5 2.0 0.2 0.2 0.2	N. by W. E. by N. W.S.W. N.N.E. N.W. by N. N. by W.	1.0 2.0 2.0 0.2 0.2 0.5	N. by E. E. by N. W. N.N.E. N. by E. N. by W.	1.5 3.0 3.5 0.2 0.2 0.5	N. E. W. N.N.E. S.S.W. S.S.W.	0.5 1.5 3.5 0.2 0.2 0.5	N. E. by N. W. N.N.E. S.W. by S. S.W. by S.	0.5 1.0 3.5 0.2 0.2 0.5	N. E. W. N.N.E. S.W. by S. S.W.	1.0 2.0 3.0 0.2 0.2 0.2	8 9 10 11 12 13 14	. •
W.N.W. W. by S. S.S.W. S.S.W. S.S.E. E.	1.0 0.5 1.0 0.2 0.2 0.5	W. by S. N.W. S.S.W. S. by W. S. by E. E.	0.5 0.5 1.5 0.2 0.2 0.2	W.S.W. W. S.S.W. S. S.S.E. E.N.E.	1.5 0.5 1.0 0.2 0.2 0.2	W.S.W. W.N.W. S.S.W. S. by E. N.E. by N.	1:0 1:0 1:0 0:2 0:0 0:2	W.S.W. N.W. S.S.W. N.W. S.S.E. N.E. by N.		W.S.W. N.W. by N. S.S.W. N.W. by W. S.E. by E.	1.0. 0.5 1.0 2.5 0.2 0.0	15 16 17 18 19 20 21	MARCH
E. S.S.W. W. by N. W. by N. N.W. by N.	0.5 0.5 0.5 2.0 1.0 6.0	E. S.W. W.N.W. W. N.W. by N. S.S.W.	0.5 0.2 0.5 2.5 1.0 6.0	E. W. by S. W.S.W. W. N.W. by N. W.S.W.	0.5 1.0 0.5 1.0 1.0 4.5	E. W. by N. S.W. by W. W. by N. N.W. by N. N.N.W.	0.5 1.0 0.5 1.0 2.0 4.0	E. W.S.W. W. by N. N.N.W. N.W.	0.5 0.0 0.5 1.0 2.5 4.5	E. W. by N. S.W. by S. W.N.W. N. by W. N.W.	0°2 0°5 0°5 3°0 4°5	22 23 24 25 26 27 28	
N. by W. E. N. by W.	2.5 1.0 1.0	N. E. by S. N. by W.	2·5 2·0 1·0	N. E. by S. N. by W.	2.5 1.5 0.5	N. E. by N. N. by W.	2.2 1.5 1.5	E. by N. N.	2:5 1:5 0:5	N. E.N.E. N.	2.2 1.0 0.5	29 30 31 /	
18h.		19h.		20h.		21հ.		22 ^h .		23 ^h .			Göttingen Time.
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	<u> </u>	1 me.
W.N.W.  E. by S.  W. N. by W. N.E. by E.  N. by W.	lbs.   0 * 2	N.W.	0.2	W.N.W. W. by S. N.W. E. by N. W. N. by E. N.N.W. N. by W. N.	lbs. 1 ' 5 ' 0 ' 2 ' 0 ' 2 ' 0 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 1 ' 0 ' 0 ' 2 ' 1 ' 0 ' 0 ' 2 ' 0 ' 2 ' 1 ' 0 ' 0 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 2 ' 0 ' 0	W.N.W. W. by N. N.W.  W. W.  N. by E. N.N.W. N. by W. N.	1bs. 1 0 0 2 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	W.N.W.  N.N.W.  N. by E. N. by E. N.N.W. N. by W.	lbs.   1 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	N.W. by N.  N.N.E.  N.N.E.  N.W. by N.  N. by W.  N. by W.  N. by W.	lbs. 0'0 0'0 0'2 0'0 0'0 0'0 0'0 0'2 0'2 0'2 0'2 0'2	1 2 3 4 5 6 7 8 9 10 11 12 13	
W.N.W.  W.S.W. W.S.W. W.N.W. E. by N.  N.E.  W. S.E.  N. by W.	0.2 0.0 0.2 0.2 0.2 0.2 0.2 0.0 0.0 2.0 0.5 0.0	N.W. W. by S. W. W.N.W. E. by N. N.E. W. by S. E. by S. E. by S.	1.5 0.2 0.2 0.0 0.2 0.2 0.2 1.0 0.0 1.0 0.2 0.2 0.2	W. by N. W. by S. W. W.N.W. E. by N. N.E. S. by E. W.N.W. E. D. by W.	1.0 0.2 0.2 0.0 0.2 0.2 0.2 0.2 0.2 0.5 0.2 0.5 0.2 0.5	W. by S. W. N.N.W. E. by N. S. by E. Y. W. N.W. E. N.N.W. N. by W. T. D. W. W. W. W. W. W. W. W. W. W. W. W. W.	2·0 0·2 0·2 0·2 0·2 0·2 0·2 0·5 0·2 0·5 5·5	W. by S. W. N.N.W. E.N.E. S. by E. W.N.W. E. N.N.W. D. N.N.W. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. E. N. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. by W. b	0.5 0.2 0.0 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	W. by S. W. W. E.N.E. N.E. W. by N. N.N.E. N.N.W. N.W. by N.	0.5 0.2 0.2 0.0 0.0 0.2 - 1.0 0.5 0.5 0.5 4.5	14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	MARCH.
S.E. E.N.E. N.E. by N.	0.2 0.2 0.0	S.E. E.N.E. N.N.E.	0.5 0.2 0.2 0.0	E.S.E. N. by E.	0.0 0.2 0.0 0.2	E. by N.  N.  —	0.0 0.2 0.0	E.N.E. N.	0.0	N. by E.	0.0 0.5 0.0	29 30 31 /	

				DI	RECTIO	N AND FOR	CE OF	THE WIND	•				
Mean Gö	Sttingen [	Oh.		1h.		2h.		3h.		4 ^h .		5 ^h .	
Tim		Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	( 1		lbs.		0.0		0°0	E.S.E.	lbs. 0°2	S.E.	lbs. 0 2	S.S.E.	lbs. 0'2
	$\left[ egin{array}{c c} 1 \\ 2 \\ 3 \end{array}  ight]$	_	0.0	_	0.0	_	0.0	S.W. by S.	0.5	_	0.0	S. by W.	0.5
	4 5 6 7 8	E. by N. W.S.W. E.	0°0 1°0 0°2 0°2	E. by N. W. E.	0°0 0°5 0°5 0°2	N.E. E. W.N.W. E.	0.2 0.2 1.5 0.2	E.S.E. E. by S. N.W. by W. S.E.	0.5	E.S.E. E. by S. N.W. by W. — N.N.W.	0.5 0.5	E. by S. W.N.W. — S.S.W.	0°2 0°2 1°5 0°0 0°2
	9 10 11	N.N.W. W.S.W.	0.5	N.N.W. W.N.W.	0.2 0.2	N.N.W. N.W. by W. —	1.0 2.5	N.N.W. W.N.W.	3.0	W.N.W.	3.2	W.N.W.	3.2
APRIL.	12 13 14 15 16 17	E. — N.W. — W. by N.	0.5 0.0 0.0 0.5 0.0 1.0	E. S.W. by S. — W.N.W. N.W. by W. N.W.	0.2 0.2 0.0 0.5 0.2 1.0	W.N.W. S.W. by S. N.W. W. by N. N.W.	1.5 0.2 0.0 1.5 0.2 3.0	N.W. by W. S.W. by S. S.S.W. N.N.W. S. N.W. by W.	2.5 0.2 0.2 1.5 0.2 2.5	N.W. by W. S.W. by S. S.S.W. N. by W. S. by W. N.W.	3.0 0.2 0.5 0.5 0.5 2.0	N.W. S. by W. S. by W. N. by W. S. by W. W.N.W.	3.5 0.2 0.5 1.0 1.5 2.5
,	18 19 20 21 22 23 24	W.S.W.  S.E.  N.E. by N.  N.N.E.	0'2 0'0 0'0 0'2 0'2 0'2	W.S.W. — S.E. N.E. by N. N.	0.2 0.0 0.0 0.2 1.0 0.2	W.S.W. N.E. by E. N.E. by N. N.E. by N. N.E. by N.	0.2 0.0 0.2 0.2 1.0 0.2	W.S.W. W. by N. N. N. by E. E.S.E.	0.2 0.0 0.2 0.2 0.5 0.5	W.S.W. S.E. N.W. N. by E. N.N.E. S.E. by E.	0°2 0°2 1°0 0°2 0°5 0°5	S.W. S.E. by S. W. by S. N. N. by E. S.E.	0.2 0.2 1.0 0.2 0.5 0.5
	24 25 26 27 28 29 30	W W N.N.W.	0.5 0.0 0.0 0.0 0.0	N.W.  N.N.W.	0.0 2.0 0.0 0.0 0.0	N.N.W. W.N.W. — N.N.W.	0.0 3.0 0.5 0.0 0.5	N.N.W. S.E. by S. — N.W.	0.0 3.5 0.2 0.0 1.0	N.N.W. S.S.E. N. by W. N.W.	0.0 3.0 0.2 0.2 2.0	S.S.W. N.N.W. S.E. by E. E.N.E. N.W.	0.5 3.0 0.5 0.5 1.5
(continu	ued)		<u> </u>		!			1		!			
	öttingen	12h.		13h.		14h.		15h.		16h.		17h.	
Tin	ne.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1 \\ 0 \end{pmatrix}$	E.	1bs. 0°2	E.	lbs. 0 ' 2	E.S.E.	lbs. 1 ° 0	E.S.E.	lbs. 1.5	E. by S.	lbs. 1.5	E.S.E.	lbs. 1 '0
	$\begin{pmatrix} 1\\2\\3\\4 \end{pmatrix}$		0.0		0.0		0.0		0.0	_	0.0	<u>-</u>	0.0
	$ \begin{array}{ c c } 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \end{array} $	E. by N. W. N. by W. S.S.W.	0.2 4.5 0.0 3.5 1.5	E. W. N. by W. S.W. by S.	0.2 3.0 0.0 2.5 0.5	E. W. N.W. by N. S.W.	0.2	E. by N. W. S.S.E. N.N.W. S.W.	1:0 1:5 0:2 1:0 0:2 0:2	E. by N. W. by S. N. by W. S.W.	1.0 1.5 0.0 1.5 0.2 0.0	E. by N. W. by S.  N. by W. S.W.	1.5 1.0 0.0 1.5 0.2 0.0
APRIL.	10 11 12 13 14 15 16 17	N.N.W. N.N.W. S.W. by S. E. by N. N.N.W. S.E. by S. W.N.W.	1'0 2'5 0'5 0'2 1'0 0'2 2'0	N.W. by N.  N.W.  E. by N.  N. by W.  E.S.E.  W.N.W.	1'0 0'2 0'0 0'2 1'0 0'2 2'0	N.N.W.  N.W.  N. by E.  N. by W.  E.  N.W.	1'0 	N.W. ———————————————————————————————————	0.0 0.0 0.2 0.2 0.2 2.5	N. by W. N. by W. N. by W.	0.0 0.0 0.2 0.2 0.0 3.5	N.N.W. N. by W.	0.0 0.0 0.2 0.2 0.3
	17 18 19* - 20 21 22 23 24 25	S.S.W. W.S.W. N.E. by N. S.	0.5 0.5 0.5 0.5 0.5 0.6 0.7	W.S.W. N.E. by N.	0.0 0.0 0.2 0.0 0.0	S.W. W. by S. N.E. by N.	0.5 0.0 0.5 0.0 0.0 0.0	N. N.E. —	0.0 0.0 0.0 0.2 1.0 0.0 0.0	E. by S. N. N.N.E. —	0.0 0.2 0.2 1.0 0.0 0.0	E. by S. S.S.E. N. by E. E.	0.0 0.2 0.2 0.5 0.0
	25 26 27 28 29 30	S.S.W. N.N.W. E. N.W. by W.	0°2 2°5 0°2 0°0	N.N.W. E. N.W. by N.	0.0 1.0 0.5 0.0 1.0	N.N.W. E. —	0.0 0.2 1.2 0.0 0.0	N.N.W. E.N.E.	0.0 0.2 0.0 0.0	N.N.W. E.N.E. —	0.0 0.2 0.0 0.0 0.0	S.W. N.N.W. E.N.E.	0.0 0.0 0.0 0.0

The second second				DIR	ECTION	AND FORC	E OF T	HE WIND.					
6 ^h .		7 ^h .		8 ^h .		9 ^h .		10h.		11 ^h .		Mean	Göttingen ime.
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		
S.E. by E.	lbs. 0°2	E. by S.	lbs. 0 2	E.	lbs. 0°2	E. by S.	lbs. 0°2	E. by S.	lbs. 0°2	E.	lbs. 0°2	$egin{bmatrix} 1 \ 2 \end{bmatrix}$	
S. by W.	0.5	_	0.0		0.0	_	0.0		0.0	_	0.0	$\begin{vmatrix} 3\\4 \end{vmatrix}$	
E. by S. W. W. by S. S.S.W. N.W.	0°2 0°2 2°0 0°2 0°5 3°0	E. by S. E. by S. W.N.W. S.E. by S. S.S.W. N.W. by N.	0.2 0.2 1.5 0.2 0.5 3.0	E.S.E. E. by S. W. by N. S.S.W. N.N.W.	0.2 0.2 1.0 0.0 0.5 2.5	E. by S. E. by S. W. S. by W. N.N.W.	0.2 0.2 1.0 0.0 0.2 2.5	E. E.S.E. S.W. N. S. by W.	0.2 0.2 0.5 2.0 0.2 2.0	E. by N. W. W. by S. N. by W. S.S.W. N.W.	0°2 4°0 0°2 1°5 1°0 2°5	5 6 7 8 9 10	
N.W. by W. S. S. by W. N.N.W. S. N.W.b y W.	3.5 0.2 0.5 0.5 1.5 2.0	N.W. S. S.S.E. N.N.W. S. by E. N.W.by W.		W.N.W. S. by W. E.S.E. N. S. by W. N.W.	4.0 1.5 0.5 0.5 2.5 2.0	N.W. by W. S.S.W. E.S.E. N. S.S.W. W.N.W.	3.5 1.5 0.5 1.0 2.0 2.0	N.W. by N. S.S.W. E. by S. W.S.W. S.W. by S. W.N.W.	3.5 1.5 0.5 0.5 1.0 1.5	N.W. S.S.W. E.S.E. N.N.W. S.W. by S. W.N.W.	3.5 1.5 0.5 0.5 0.2 2.0	12 13 14 15 16 17 18	APRIL.
S.W. S.E. by S. W.S.W. N.N.E. N. by W. S.E. by S.	0.2 0.2 1.0 0.2 1.0 0.2	S.W.  W.S.W.  N.N.E.  N.  S.E.	0.5 0.0 1.0 0.2 0.2 0.5	S.W.  W.S.W.  N.N.E.  N.E.  S.E.	1'0 0'0 1'0 0'5 0'2 0'2	S.W. S.E. W.S.W. N.E. N.W. S.S.E.	0.5 0.2 1.0 0.5 0.2 0.2	S. by W. W.S.W. N.E. S. by E.	0.5 0.0 0.5 0.2 0.0	S.S.W. W.S.W. N.E. by N. S.	0.2 0.0 0.2 0.2 0.2 0.0	19 20 21 22 23 24 25	
S.S.W. N. by W. S.E. by E. E.N.E. N.W. by W.	0°2 3°0 0°2 0°2 1°5	S. N. by W. E. E. W. by N.	0.5 2.2 0.5 0.5 0.5 2.0	S. N. by W. E. by S. N.E. by N. N.W.	0.2 3.0 0.2 0.2 3.0	S. N.N.W. E. N.E. by N. N.W.	0.2 2.5 0.2 0.2 2.0	N. by E. N. by W. E.N.E. S.S.E. N.W.	0.2 2.5 0.2 0.2 2.0	N.N.W. E. by N. N.W. by N.	0.0 2.5 0.2 0.0 2.5	26 27 28 29 30	
18 ^h .		19 ^h .		20 ^h .		21 ^h .		22 ^h .		23 ^h .			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		l'ime.
_	lbs.		lbs.		lbs.		lbs.		lbs.		lbs.	1	
W.N.W.  N. by W. E. by N. W. by S. E.N.E. N. by W. S.W.	0·2	N. by W. E. by N. W. by S. E. by S. N.N.W.	0.0 1.0 1.0 0.5 0.2 1.5 0.0	N. by W. E. by N. W. by S. N.N.W.	0.0 	E. by N. W. by S. N.E. N.N.W.	0.0 	E. W. by S. N.E. by E. N.N.W. S.W.	0.0 0.0 1.5 0.5 0.2 0.2 0.2	E. by N. W.S.W. N.E. by E.	0.0 0.0 1.0 0.2 0.0 0.0 0.0	2 3 4 5 6 7 8 9	
N.W. by N. N.N.W. N. by W.	0.0 0.2 0.0 0.2 0.2 0.0	N.W. N. by W. N.W. N.N.W.	0.0 0.2 2.0 1.0 0.2 0.0	S.E. by E.  N. by W. N.W. N.N.W.	0.2 0.0 2.0 1.5 0.2 0.0	E. by S.  N.N.W.  N.W.	0.0 1.0 1.0 0.0 0.0	E. N.W. by N. N.W. N.N.W. W.N.W.	0.2 0.0 0.5 0.2 0.2 0.2	E. N.W. by N. N.W. W.	0.2 0.0 0.2 0.5 0.0 1.0	11 12 13 14 15 16 17	APRIL.
W. E. E.N.E. N. by E. E.N.E.	0.2 0.0 0.2 0.2 1.0 0.2	E.S.E. E.N.E. N.E. by N.	0.0 0.0 0.2 0.2 1.5 0.0	— E. by S. N. by E. N.E. by N.	0.0 0.0 0.2 0.2 1.0 0.0	W. by S.  N.E. E.S.E. N.E. by N.	0.2 0.0 0.5 0.2 0.5 0.0	W. by S. S. by W. N.E. by N. E.S.E. N.E. by N.	0.2 0.2 0.2 0.2 0.5 0.0	W.S.W.  — S.E.  N.E. by N.  N.N.E.	0.2 0.0 0.0 0.2 0.5 0.2	18 19 20 21 22 23 24	7
S.W. by S. S.W. by S. N.N.W. E.N.E.	0.2 0.2 0.2 0.2 0.0 0.0	N.W. N.N.W.	0.0 0.5 0.0 0.0 0.0	N. by W.	0.0 0.0 0.0 0.0 0.0	N. - N.N.W.	0.0 0.0 1.0 0.0	S.W. by S.  N.  N.  N.  N.  N.  N.  N.  N.  N.	0.2 0.2 0.0 0.0 1.5 0.0	S.W. N. — N.N.W.	0.2 0.2 0.0 0.0 0.5 0.0	25 26 27 28 29 30	

_		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		171	RECTIO	N AND FOR		THE WIND.		<del>,</del>			
	ottingen	O ^h .		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
Tim	ie.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Ford
	( 1	N.N.W.	lbs. 0°2	N. by W.	lbs. 0°2	N. by W.	lbs. 0°2	S.	lbs. 0°2	S.	lbs. 0°5	S.	lbs.
ļ	$\begin{bmatrix} 2 \\ 3 \end{bmatrix}$	W. by N.	$\frac{0.5}{100}$	$\overline{\text{w.s.w.}}$	0.2	w.s.w.	1:5	w.	3.0	w.	3.0	$\overline{\mathbf{w}}$ .	2.
ļ	4 5		$\begin{array}{c} 0.0 \\ 0.0 \end{array}$		$0.0 \\ 0.0$		$0.0 \\ 0.0$	S.W. by S.	0.0	S. by W. S.W. by S.	0.2	S. S.S.W.	0.
	6	_	0.0		0.0		0.0		0.0		0.0		0
	7 8	_	0.0		$0.0 \\ 0.0$	E.N.E.	0.0	W. E.N.E.	0.2	W. N.E. by E.	0°2 0°5	E. by S. N.E.	0
	9	_	0.0	_	0.0		0.0	E. by N.	1.0	E. by S.	0.2	<u> </u>	0
	11		0.0		0.0	S.E.	$0.0 \\ 0.2$	S.E. E.	0.5	E. E.	$\begin{array}{c} 0.3 \\ 0.3 \end{array}$	E. E.	0
,	12 13	S.E. by S. N.E. by E.	0.5	N.E. by E.	$\begin{array}{c} 0.0 \\ 0.2 \end{array}$	N.E. by E.	0.5	E.N.E.	0.5	E.	1.0	Ε.	1
	14 15	<b>—</b>	0.0		0.0	E. by N.	$0.0 \\ 0.5$	E. by N.	0.0	E.	0.0	E.S.E.	0
X.	16	_	ĺ —		_	_	-					_	_
MAY.	17 18	_	0.0	<del></del>	0.0		0.0	_	0.0	_	0.0	_	0
	19		0.0		0.0		0.0		0.0		0.0	E 1 C	0
	20 21	_	0.0		0.0		0.0	_	0.0	E. by N.	0.0	E. by S. E.	0
	22 23	S.S.W.	0.2	S.S.W.	0.2	S.S.W.	0.5	S.S.W.	0.5	S.S.W.	0.5	s.w.	0
	24		0.0		0.0	N.W.	0.5	N.W.	0.5	N.W.	0.5	— E.	0
	25 26	W. by N.	$\begin{array}{c} 0.5 \\ 0.0 \end{array}$	S.E. W. by N.	$\begin{array}{c c} 0.5 \\ 0.5 \end{array}$	S.E. W.N.W.	$0.2 \\ 0.5$	S.E. N.W. by W.	0°2 0°5	N.W. by W.	0.0	S. by W.	0
	27 28		0.0		0.0		0.0		0.0	E.S.E.	$0.0 \\ 0.0$	E.S.E.	0
	29	E. by N.	0.2	_	0.0		0.0	E.N.E.	0.5	E.N.E.	0.5	E.N.E.	0
	$\begin{array}{c} 30 \\ 31 \end{array}$	E. by N.	$\frac{-}{2.5}$	E.N.E.	${2\cdot 5}$	N.E. by E.	$\frac{-}{2.5}$	E.N.E.	3.0	E.N.E.	3.0	E.N.E.	$\frac{1}{2}$
(continu	ied)	!!											
	öttingen {	12 ^h .		13h.		14 ^h .		15 ^h .	1	16 ^h .	1	17 ^h .	
Tin	ne.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	For
	/ 1		0.0		O.O		0.0	E.	0.5	E.	0.5	E.N.E.	0
	2		I —	w.n.w.	1.0	w.N.W.		_	0.0		0.0		-
	3	W. by N.	1.2	1 11 . 4 7 . 1 7 .		1 11 . 41 . 11 .	0.5						
	3 4	W. by N. S. by W.	0.5	S. by W.	0.5	S. by W.	0.5		0.0		0.0	_	0
		S. by W.	0.0 0.2 0.5		0.5 0.5 0.5		0.0 0.0 0.0		0.0 0.0 0.0	_	0.0 0.0 0.0		0 0
	4 5 6 7	S. by W. S. E. by N.	0.5 0.0 0.2	S. by W. S. —	0.5 0.0 0.0	S. by W.	0.0 0.0 0.0		0.0	 N.N.W.	0.0	 N. by W.	0 0 0 0
	4 5 6 7 8 9	S. by W. S. E. by N. N.	0.2 0.5 0.0 0.2 1.5	S. by W. S N.	0.5 0.0 0.0 5.0	S. by W  N	0.2 0.0 0.0 2.5 —	N. by E.	0.0 0.0 0.0 1.2	N.N.W. N. by E.	0.0 0.0 0.0 0.2 1.5	 N. by W. N. by E.	0 0 0 0 1
	4 5 6 7 8 9 10	S. by W. S. E. by N. N. S. by E.	0.2 0.5 0.0 0.2 1.5 - 0.2 0.0	S. by W. S. — N.	0.2 0.0 0.0 2.0 - 0.2 0.0	S. by W N	0.5 0.0 0.0 0.0 2.5 - 0.0 0.0	N. by E.	0.0 0.0 0.0 0.0 0.0 0.0	N.N.W. N. by E.	0.0 0.0 0.0 0.2 1.5 - 0.0 0.0	N. by W. N. by E.	0 0 0 0 1 - 0 0
	4 5 6 7 8 9 10 11 12	S. by W. S. E. by N. N.	0.2 0.5 0.0 0.2 1.5 - 0.2 0.0 0.5	S. by W. S. N. S. by E.	0.2 0.0 0.0 2.0 - 0.2 0.0 0.0	S. by W.	0.2 0.0 0.0 0.0 2.5  0.0 0.0	N. by E.	0.0 0.0 0.0 0.0 1.2 	N.N.W. N. by E.	0.0 0.0 0.0 0.2 1.5 -	N. by W. N. by E.  — — — — — —	0 0 0 0 1 - 0 0 0 0
	4 5 6 7 8 9 10 11 12 13 14	S. by W. S. E. by N. N. S. by E. E. by N.	0.2 0.5 0.0 0.2 1.5 	S. by W. S. N. S. by E.	0.5 0.0 0.0 2.0 0.2 0.0 0.0 0.0 0.0	S. by W N	0.2 0.0 0.0 0.0 2.5 - 0.0 0.0 0.0 0.0	N. by E.	0.0 0.0 0.0 0.0 1.5 - 0.0 0.0 0.0 0.2 0.0	N.N.W. N. by E.  — — — — — — — — E.N.E.	0.0 0.0 0.0 0.2 1.5 - 0.0 0.0 0.0 0.2 0.0	N. by W. N. by E.	0 0 0 0 0 0 0 0
IX.	4 5 6 7 8 9 10 11 12 13 14 15	S. by W. S. E. by N. N. S. by E. E. by N.  E. s. by N.	0.2 0.5 0.0 0.2 1.5 	S. by W. S. N. S. by E.  E.S.E.	0.2 0.2 0.0 0.0 2.0 0.2 0.0 0.0 0.0 0.0	S. by W.  N.  S.E. by S.	0.2 0.0 0.0 0.0 2.5  0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by E.  E.N.E	0.0 0.0 0.0 0.0 1.5  0.0 0.0 0.2 0.0 0.0	N.N.W. N. by E.  E.N.E	0.0 0.0 0.0 0.2 1.5  0.0 0.0 0.2 0.0 0.0 0.0 0.0	N. by W. N. by E.    N.E.	000000000000000000000000000000000000000
MAY.	4 5 6 7 8 9 10 11 12 13 14 15 16 17	S. by W. S. E. by N. N. S. by E. E. by N.  E. S. E. E.	0°2 0°5 0°0 0°2 1°5 0°0 0°5 0°0 0°0 0°2 —	S. by W. S. N. S. by E. E.S.E.	0.2 0.0 0.0 0.0 2.0 0.0 0.0 0.0 0.0 0.0	S. by W.  N.  S.E. by S.  E.	0.2 0.0 0.0 0.0 2.5  0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by E.  E.N.E.	0.0 0.0 0.0 0.0 1.5 	N.N.W. N. by E.  — — — — — — — — — — — — — — — — — —	0.0 0.0 0.0 0.0 0.2 1.5  0.0 0.0 0.2 0.0 0.0 0.0	N. by W. N. by E.  N.E	
MAY.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	S. by W. S. E. by N. N. S. by E. E. by N.  E. S.E.  E. S.E.	0°2 0°5 0°0 0°2 1°5 0°0 0°5 0°0 0°0 0°2 0°2 0°0 0°0	S. by W. S. N. S. by E.  E.S.E.	0.2 0.0 0.0 0.0 2.0 0.0 0.0 0.0	S. by W.  N.  S.E. by S.	0.2 0.0 0.0 0.0 2.5  0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by E.  E.N.E	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.N.W. N. by E.  E.N.E	0.0 0.0 0.0 0.0 0.2 1.5  0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by W. N. by E.    N.E.	
MAY.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	S. by W. S. E. by N. S. by E. E. by N.  E. S.E.  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E  E	0°2 0°5 0°0 0°2 1°5 0°0 0°5 0°0 0°0 0°2 ———————————————————————————	S. by W. S. N. S. by E. E.S.E. E. W.N.W.	0.2 0.0 0.0 0.0 2.0 0.0 0.0 0.0 0.0 0.0	S. by W.    N.	0.2 0.0 0.0 0.0 2.5  0.0 0.0 0.0 0.0 0.2 0.0 0.0 0.0	E.N.E.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.N.W. N. by E.  E.N.E	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by W. N. by E.  N.E N.W. by N.	
MAY.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	S. by W. S. E. by N. S. by E. E. by N. E. S. E. by N.  E.S.E.	0.2 0.5 0.0 0.2 1.5 0.0 0.5 0.0 0.0 0.0 0.2 0.0 0.0 0.0 0.0	S. by W. S. N. S. by E. E.S.E. E. W.N.W. W. by N.	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0	S. by W.  N.  N.  S.E. by S.  E.  N.N.W.  W. by N.	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0	E.N.E.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.N.W. N. by E.  E.N.E.  N.W. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by W. N. by E.  N.E.  N.E.  N.W. by N.	
MAY.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	S. by W. S. E. by N. S. by E. E. by N.  E. S. E.  E.  E.  E.  E.	0.2 0.5 0.0 0.2 1.5 0.0 0.5 0.0 0.0 0.0 0.0 0.0 0	S. by W. S. N. S. by E. E.S.E. E. W.N.W. W. by N.	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0	S. by W.  N.  N.  S.E. by S.  E.  N.N.W.	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by E.  E.N.E.   N.W. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.W. by E.  E.N.E.  N.W. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by W. N. by E.  N.E N.W. by N	
MAY.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	S. by W. S. E. by N. S. by E. E. by N.  E. S.E.  E.  W.	0.2 0.5 0.0 0.2 1.5 	S. by W. S. N. S. by E. E.S.E. E. W.N.W. W. by N. W.	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0	S. by W.    N.	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by E.  E.N.E.   N.W. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.N.W. N. by E.  E.N.E N.W. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by W. N. by E.  N.E N.W. by N.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
MAY.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	S. by W. S. E. by N. S. by E. E. by N.  E.S.E.  E.  W. S.S.E. E.	0.2 0.5 0.0 0.2 1.5 0.0 0.5 0.0 0.0 0.0 0.0 0.0 0	S. by W. S. N. S. by E. E.S.E. E. W.N.W. W. by N. S.S.E. E.	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0	S. by W.    N.	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by E.  E.N.E.   N.W. by N.   W. by S.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.W. by E.  E.N.E.  N.W. by N.  N.W. by N.  N.W. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by W. N. by E.  N.E.  N.W. by N.  N.W. by N.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
MAY.	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	S. by W. S. E. by N. N. S. by E. E. by N.  E.S.E.  E.  W. S.S.E.	0.2 0.5 0.0 0.2 1.5 0.0 0.5 0.0 0.0 0.0 0.0 0.0 0	S. by W. S. N. S. by E. E.S.E. E. W.N.W. W. by N. S.S.E.	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0	S. by W.    N.	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by E.  E.N.E.  N.W. by N.  W. by S.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.W. by E.  E.N.E.  N.W. by N.  N.W. by N.  N.W. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by W. N. by E.  N.E N.W. by N	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

				DIRI	ECTION	AND FORC	E OF T	HE WIND.					
6 ^h .		7 ^h .		8 ^h .		9 ^h .		10h.		11h.			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		'ime.
s.	lbs. 0.5	S.E. by S.	lbs. 0°2	S. by E.	lbs. 0°2		0.0		lbs. 0.0		0.0	$\frac{1}{2}$	)
S. by E. S. by E. S.S.E. E. by S. N.E.	2.5 0.2 0.2 0.2 0.2 0.2	W.N.W. S. by E. S.S.E. E.S.E. E. by S. E.N.E.	0.5 0.5 0.5 0.5 0.5 0.5 0.5	W.N.W. S. by E. S.E. by S. E.S.E. E. by S. N.N.E.	2.5 0.2 0.2 0.2 0.5 0.5	W. by N. S. S.E. by S. E.S.E. E. N.E.	3.0 0.2 0.2 0.2 0.5 0.5	W.N.W. S. by W. S.E. by S. E. by S. E. by N. N.	2.5 0.2 0.2 0.2 0.5 0.5	W.N.W. S. by W. S. by E.  E. by N. N. by W.	2·5 0·2 0·5 0·0 0·2 2·0	3 4 5 6 7 8 9	
E. E. E. E. E. E. E. E. E. E. E. E. E.	0.2 0.2 0.2 1.0 0.5 0.2	E. by S. E.N.E. E. by S. E.S.E. E. by S.	0.2 0.2 0.2 0.5 0.5	E. by S. E. by S. E.N.E. E. by S. E.S.E. E. by S.	0.2 0.2 0.5 0.5 0.5 0.5	E. by S. E. by S. N.E. by E. E. by S. E.S.E. E.S.E.	0°2 0°2 0°5 0°2 0°2 0°2	E. by S. E. by S. E.N.E. ———————————————————————————————	0°2 0°2 1°0 0°0 0°0 0°2	E. by S. E. E.S.E.	0°2 0°0 1°0 0°0 0°0 0°2	10 11 12 13 14 15 16	MAY.
E. by N. E. by S. E.S.E. S. by W.	0.5 0.0 0.5 0.0 0.0 0.0	E. by S.  E.S.E.  F.  S.	0.2 0.0 0.0 0.2 0.2 0.2	E. by S.  E.S.E.  E. S.	0.2 0.2 0.0 0.2 0.2 0.2	E. E.S.E. E. S	0.2 0.2 0.0 0.0 0.2 0.2	E. by N. S. —	0°2 0°0 0°0 0°2 0°2	E  S. by W.	0.5 0.0 0.0 0.0 0.0 0.0	17 18 19 20 21 22 23	M
E. S. by E. E.S.E. by E.	0.0 0.2 0.5 0.2 0.0	E. S. by E. E. E.S.E. N.E. by E.	0.0 0.2 0.5 0.2 0.2 0.2	W.S.W. E. S. by E. E. E.S.E. N.E. by E.	0°2 0°3 0°3 0°2 0°3	W.S.W. S. by W. S. by E. E. by S. E.S.E.	0.2 0.5 0.5 0.2 0.0	S.S.E. S. by E. E. E.S.E. N. by W.	0.0 0.2 0.2 0.2 0.2 0.2	S.S.E. S.S.E. E. — N. by W.	0.0 0.2 0.2 0.0 0.5 	24 25 26 27 28 29 30	
E.N.E.	2.2	E.N.E.	2.2	E.N.E.	2.2	E.N.E.	2.2	E.N.E.	2.2	E.N.E.	2.2	31	J 
18h.		19 ^h .		20 ^h .		21 ^h .		22 ^h .		23 ^h .		Mean (	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	T	ime.
N. by S.    N. by W.   N. by N.   N. by N.   N. by N.   N. by N.   N. by N.   N. by N.   N. by N.	0.0 0.0 0.0 - 0.0	N.N.E.  N.E.  N.N.W.  S.S.E.  W.N.W.	lbs.	N.E. by N.  N.E.  N.E.  N.E.  W.N.W.  S. by W.  W.N.W.	lbs.	S.W. by S.  N.E.  N.N.E.  N.N.W.  S.S.W.  W.N.W.  N.E. by E.	lbs.	N.E. by E.  N.N.W.  S.S.W.  W.N.W.  N.E. by E.	lbs.	W. by S.  S.W.  N.E. by E.  S.S.W.  W.N.W.  N.E. by E.	1bs. — 0'2 0'0 0'0 0'0 0'0 0'0 1'5 — 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	MAY.

				DIR	ECTION	N AND FORC	E OF	THE WIND.					
Mean Göt	tingen {	Oh.		1 ^h .		2h.		3հ.		4 ^h .	_	5 ^h .	
Time	e. [	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Fore
	1 2 3 4 5	  N.W. W.	lbs. 0°0 0°0 0°0 0°2 0°2	   W.N.W.	lbs. 0'0 0'0 0'0 0'0 0'2	W.N.W.  N.W. N.W. by W.	lbs. 0°0 0°2 0°0 0°2 0°5	W.N.W. W. W. by N.	1bs. 0.0 0.2 0.0 1.5 0.5	S.S.E.  W.N.W. W. by N.	1bs. 0°2 0°0 0°0 0°5 0°5	S. by E. N.W. W. W. W. by N.	0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 0° 0
	6 7 8 9 10 11 12	S.S.W.		S.S.W. S.	0.0 0.0 0.0 0.2 0.2 0.0	S. by W. S.W. by S.	0.0 0.0 0.0 0.0 0.0 0.2 0.2	S.W. by S. S. by W. S.W. by S.	0.2 0.0 0.0 0.2 0.5 0.2	S.S.W.  S. S. S. S. S. S. S. S. S. S. S. S. S. S	0.2 0.0 0.0 0.2 0.5 0.2	S.S.E.  E. by N. S.S.W. S. S. by W.	0. 0. 0. 0. 0.
JUNE.	13 14 15 16 17 18	W. by N. N.W. —	0.0 1.0 0.2 0.0 0.0	W.N.W. W.N.W. N.W.	2.5 1.0 0.2 0.0 0.2 0.0	W.N.W. W.N.W. W.N.W.	2·5 1·5 0·2 0·0 0·2 0·0	W. N.W. W.N.W. E.	2.0 3.0 0.2 0.0 0.2 0.0	W. W.N.W. N.W. S.S.W. E. S.S.W.	2·5 2·0 0·2 0·2 0·2 0·2	W. by N. W.N.W. W.N.W. S.S.W. E. S.S.W.	2. 2. 0. 0. 0.
	20 21 22 23 24 25 26		0.0 0.0 0.0 0.0 0.0 0.0 0.0	E.N.E. — — — W. by N.	0.0 0.2 0.0 0.0 0.0 0.0	S.W. by W. E.S.E. N.W. — S.W. by S.	0.0 0.0 0.0	S.S.W.  N.W. by N. S.W. S.S.W. S.W. by S.	0.2 0.0 0.2 0.2 0.2 0.2	S.S.W. S.S.W. S.W. S.S.W. S.S.W.	0.2 0.0 0.2 0.2 0.2 0.2	S.W. by S. S.E. by E. S.S.W. S.W. S.S.E. S.S.E.	0. 0. 0. 0. 0.
	27 28 29 30	 	0.0 0.0 0.0	 N.	0.0 0.0 0.0	N.N.W.	0°2 0°0 0°2	N.W.	0.2 0.0 0.5	N.W. by N. E. by S.	0.2 0.0 0.5	N.W. by N. E.S.E.	0,
(continue	ed)							1		1		1	
Iean Gött Time		12 ^h .		13h.		14h.		15h.		16h.	1 75	17h.	77
	1 2 3 4 5 6 7 8	W. S. E. W. N.W. by N. E.S.E.	lbs.   0°2   0°2   1°0   0°5     0°2   0°0	W. S. W. by S. N.W. by N.	Ibs. 0°2 0°2 0°0 0°5 0°5 0°0	W. S. W. N.W. by N. E.N.E.	lbs.   0°2   0°0   0°2   0°0   0°2   0°0   0°2   0°2   0°0   0°2   0°2   0°2   0°2   0°2   0°3   0°4   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5   0°5	Direction.	lbs.   0°0   0°0   0°0   0°2     0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0	Direction.  N.N.W.	Ibs. 0'0 0'0 0'0 0'0 0'2 0'0 0'0	N.W.  N.E.	Ibs.   0
JUNE.	9 10 11 12 13 14 15	S.W. by S. S. by W. W. S. by E. W.N.W. N.W. by W.	1.5 0.2 2.0 0.2 - 3.0 0.5	S.W. by S. S. by W. W. S. by E. W.N.W. W. by N.	1.0 0.2 1.5 0.2 - 3.0 0.5	S. by W. W. S. by E. W. by N.	0.0 0.5 1.0 0.5 - 2.0 0.0	W. S. by E. W.N.W.	0.0 0.0 1.0 0.2 - 2.0 0.0	w. - w.n.w.	0.0 0.0 1.0 0.0 - 1.2 0.0	W.N.W.	0.0000000000000000000000000000000000000
JL	16 17 18 19 20 21 22 23 24	E. by N.  S.W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	E. by N.	0.0 0.0 0.2 0.0 0.0 0.0 0.0	E. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	    	0.0 0.0 0.0 0.0 - 0.0 0.0 0.0	——————————————————————————————————————	0.0 0.0 0.0 0.0 - 0.0 0.0 0.0	s	0.0000000000000000000000000000000000000
	25 26 27 28 29 30	S. by W. S.W.  N. by W. N.N.W.	0.2 0.5 - 0.2 0.5 0.0	S.W. 	0.0 0.5 0.5 0.0 0.0	N.N.W.	0.0 0.0 0.0 0.0 0.0	N. by W. N.N.W.	0.0 0.0 0.5 0.5 0.0	N. by W. N.N.W.	0.0 0.0 0.5 0.5 0.0	N. by W. N.N.W.	0 0 0

				DIR	ECTION	AND FORC	E OF T	THE WIND.					
6 ^h .		7 ^h .		8 ^h .		9 ^h .		10h.		11 ^h .			öttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Ti	me.
 S.S.E. W. E.S.E.	lbs. 0'0 0'0 0'2 1'5 0'2	S. E.S.E. W. S. by E.	lbs. 0°0 0°2 0°2 2°5 0°2	S. E.S.E. W. S.	lbs. 0°0 0°2 0°2 2°5 0°5	S.W. S. E.S.E. W.N.W. S.	lbs. 0°2 0°2 0°2 2°5 0°2	S.W. by W. S. E. by S. W.N.W. N.E. by N.	lbs. 0°2 0°2 0°2 2°5 0°5	W.S.W. S. E. W. N.W. by N.	lbs. 0°2 0°2 0°2 1°5 0°5	1 2 3 4 5 6	
S.S.E. S.E. S. by W. S.W. S. W.	0.2 0.0 0.2 0.2 1.0 0.2	S.S.E. S.E. S.S.W. S.W. by S. S.	0.2 0.0 0.2 0.5 0.5 0.5	S.S.E. S.E. S.S.W. W.S.W. S.	0.2 0.0 0.2 0.2 0.5 0.5	S. by W. S.S.W. S.S.E.	0.0 0.0 0.2 0.2 0.5 0.2	S.E. S.S.W. S. by W. S.S.W. S.S.E.	0.2 0.0 1.0 0.2 0.5 0.2	E.S.E. S.W. by S. S. by W. S.W. by W. S. by E.	0°2 0°0 1°0 0°2 1°0 0°2	6 7 8 9 10 11 12 13	
W.N.W. W.N.W. W.N.W. S.S.W. E. by S. S.W.	3.5 2.0 0.5 0.2 0.2 1.0	W.N.W. W. N.W. S. by W. E. N.N.W.	3.5 1.5 0.5 0.2 0.5 2.5	N.W.by W. W. by N. N.W. by N. S. by W. E. by N. N.N.W.	3.0 1.5 0.5 0.2 0.5 1.0	W.N.W. W.N.W. N.W. by W. S. by W. E. by N. N. by W.	3.5 1.5 0.5 0.2 0.5 0.2	W.N.W. W.N.W. N.W. S. by W. E. by N. N.N.W.	5.0 1.0 0.5 0.2 0.5 0.2	N.W. N.W. N.W. S. by W. E. by N. S.S.W.	4.2 1.0 0.2 0.2 0.2 0.2	14 15 16 17 18 19 20	JUNE.
S.W. S.S.W. S.W. S.S.E. S.S.W.	0.2 0.0 0.2 0.2 0.2 0.2 0.5	S.W. S. by W. S.W. S.S.E. S.S.W.	0.2 0.0 0.2 0.2 0.2 0.2 0.5	S.W. by W. S.W. by S. S.W. by S. S.S.E. S.S.W.	0.2 0.0 0.2 0.2 0.2 0.5	S.W. by W. S.E. S.W. by S. S.W. by S. S.E. by S. S.S.W.	0.5 0.5 0.5 0.5	S.W. by W. S.S.W. S.W. by S. S.W. by S. S.S.W.	0°2 0°2 0°2 0°2 0°0 0°5	S. by W. S.W. by S. E. S.W.	0°0 0°2 0°2 0°0 0°2 1°0	21 22 23 24 25 26 27	
N.W. by W. N. S.E.	0.5 0.5 0.5 0.5	W. by N. N.N.W. S.E.	0.5 0.5 0.5 0.5	N. by W. S.W. by W. S.E.	0.5 0.5 0.5 0.5	N. S.S.W. S.S.E.	0.2 0.5 0.5	N. S.S.W. S.S.E.	0.2 0.5 0.5	N. by W. S.S.W. S.S.E.	0.5 0.5 0.5	28 29 30	
18 ^h •		19 ^h •		20 ^h .		21 ^h .		22 ^h .		23 ^h .	<u> </u>	h	
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Mean G Ti	ottingen ime.
N.W.  N.W.  S. W.  N. by W.  N. by W.  N. by W.  N. by W.  N. by W.  N. by W.  N. by W.	lbs.   0°5   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0   0°0	N.W.  S. W.N.W.  W.  N. by W.  N.W. by W.  N. by W.  N. by W.  N. by W.  N. by W.  N. by W.	lbs. 0'2 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0	Direction.	Torce.   Torce.   Torce.   Torce.   Torce.   Torce.   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce   Torce	Direction.	Force.	Direction.	Box   O 2   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0   O 0	Direction.	Torce.   Ibs.   0.0   0.0   0.2   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	JUNE.

	٢					ON AND FOI	<del></del>					-1.	
Mean Gö Time		O ^h .		1 ^h .		2 ^h .		3 ^h .		4 ^h .	·	5 ^h .	T
	$\begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}$	Direction.	lbs. 0.0 0.0	N.N.E.	lbs. 0°2 0°0 0°0	N.N.E.	lbs. 0.2 0.0 0.0	Direction.  E.N.E.	lbs. 0.0 0.2 0.0	E. E.S.E.	lbs. 0°2 0°2 0°0	E.S.E. E.S.E.	lbs. 0° 0° 0° 0° 10° 10° 10° 10° 10° 10° 10°
	4 5 6 7 8 9		0.0 0.0 0.0 0.0 0.0 0.0		0.0 0.0 0.0 0.0 0.0 0.0		0.0 0.0 0.0 0.0 0.0 0.0	s.s.w. E.	0.0 0.0 0.2 0.0 0.2 0.0	S.S.E. S. by W. S. by E. E. by S.	0.2 0.0 0.2 0.2 0.2 0.0	S. by E. S. by E. S. by E. E.S.E.	0. 0. 0. 0.
JULY.	11 12 13 14 15 16 17 18	N.W. N. by W.	0.0 0.2 0.0 0.0 0.0	E. N.N.W. N. by W.	0·2 0·2 0·2 0·0 0·0	S.E. N.N.W. N. S.W. S.W.	0.2 0.2 0.2 0.0 0.2 0.5	S.E. N.N.W. — S. by W. S.W.	0.5 0.5 0.0 0.0 0.0 0.2 1.0	S.E. N.W. N. S.S.W. S.W. by S.	0.5 0.5 0.5 0.0 0.0 0.5 1.0	S. by E. N.N.W. S.E. by S. S. S. by W. S.S.W.	0. 0. 0. 0.
	18 19 20 21 22 23 24 25		0.0 0.0 0.0 0.0 0.0 0.0	N. by W.	0.0 0.0 0.0 0.0 0.0	S. N.N.W. S.E. by S.	0.0 0.0 0.2 0.2 0.0 0.2	S. by W. S.W. by S. S.S.W. N.N.W. S.W. S.E. by S.	0.2 0.2 0.2 0.5 0.2 0.2	S. by W. S.S.W. S.W. by S. N. S. by E. E.S.E.	0.2 0.2 0.2 0.5 0.5	S. S.S.W. S.S.W. N.N.W. S. by E. E.S.E.	0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0
	26 27 28 29 30 31	N. by E.	2.0 0.0 0.0 0.0 0.0	N. by E. E.S.E.	1.0 0.5 0.0 0.5 0.0 0.0	N. by E. S.S.E.	2.0 0.2 0.0 0.2 0.0 0.0	N. E. by S. E. by N. S.E. by S. S.W. E. by S.	2·0 0·5 0·2 0·2 0·2 0·2	N. E.S.E. S.E. S.S.E. S.S.W. S.S.E.	2.0 0.2 0.2 0.2 0.2 0.2	N.N.W. S.E. by S. S.E. S.S.E. S.S.E.	1 0 0 0 0
(continu	sed)									1			
Mean Gö Time		12h.	Terror	Direction.	Force.	14 ^h . Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Fore
	1 2 3 4 5	S. by E.	Ibs. 0.0 0.0 0.2 0.2	S. by E.	lbs. 0'0 0'0 0'2 - 0'2	S. by E.	lbs. 0°0 0°0 0°2 —	E. by S.	1bs. 0°0 0°2 0°0	E. by S	lbs. 0°2 0°2 0°0 —	E.N.E.	0. 0. 0. 1ps.
	6 7 8 9 10		0.0 0.0 0.0 0.0 0.0		0.0 0.0 0.0 0.0 0.0		0.0 0.0 0.0 0.0 0.0		0.0 0.0 0.0 0.0 0.0	  	0.0 0.0 0.0 0.0 0.0		0. 0. 0. 0.
JULY.	12 13 14 15 16 17	N.N.W. S. by W. S.S.W.	0.0 0.2 0.5 0.0	N.N.W. S. by W. S.S.W.	0.0 0.5 0.0 0.2 0.5 0.0	S. by W. S.S.W. S. by W.	0.0 0.0 0.0 0.2 0.2 0.2	N.N.W. — — —	0.0 0.5 0.0 0.0 0.0	N.N.W.	0.0 0.2 0.0 0.0 0.0	N.N.W. — — —	0. 0. 0. 0.
	18 19 20 21 22 23 24	S.S.W. E. N.W. E.N.E.	0°2 0°5 0°0 0°5 0°0	S.W. S.E. N.W. E.N.E.	0°2 0°2 0°0 0°2 0°0 0°2	S.W. S.E. N.W.	0.2 0.2 0.0 0.2 0.0 0.0	S. by E.  E.N.E.	0.0 0.2 0.0 0.0 0.0 0.0	S.W  E.N.E.	0.2 0.0 0.0 0.0 0.0 0.0	S.W.	0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0
	25 26 27 28 29 30 31	N. by E. S.S.E. S.E. by S. E. by S.	0.5 0.2 0.0 0.2 0.5	N. by E.  S.E. by S. E. by S.	0.5 0.0 0.0 0.5 0.5 0.5	  E.S.E.	0.0 1.0 0.0 0.0 0.0	s.s.w.	0.0 1.0 0.0 0.0 0.0	   	0.0 0.0 0.0 0.0 0.0		0 0 0 0 0 0

				DIRE	CTION	AND FORCE	OF TI	HE WIND.					
6 ^հ .		7 ^h .		8h.		9 ^h .		10h.		11h.			Göttinger
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		'ime.
E.S.E. E.S.E.	lbs. 0°2 0°2 0°0	E.S.E. E.S.E. S.S.E.	lbs. 0°2 0°2 0°2	E.S.E. E.S.E. S. by E.	lbs. 0°2 0°2 0°2	E.S.E. S. by E.	lbs, 0°2 0°0 0°2	E.S.E. S. by E.	1bs. 0°2 0°0 0°2	 S. by E.	lbs. 0°0 0°0 0°2	1 2 3	
S. by W. S. by W. S.E. by E. E.S.E. E. by N.	0.5 0.0 0.5 0.5 0.5 0.5 0.5	S. by W. S. by W. S.E. by E. S.E. by E.	0.0 0.0 0.2 0.2 0.2 0.2 0.0	S. by W.  E.S.E. E. by N.	0.2 0.0 0.0 0.2 0.2 0.2	S. by W.  E. E. by S. E. by N.	0.5 0.0 0.0 0.5 0.5 0.5	E. E. by S. E. by N.	1.0 0.0 0.0 0.2 0.2 0.2	N. by W.	0.0 0.0 0.0 0.0 0.0	4 5 6 7 8 9 10	
S. N.N.W. S.S.E. S. S. S.	0.2 0.5 0.2 0.2 0.2 0.2 1.5	S. N.N.W. S. S. S. S.	0.2 1.5 0.2 0.2 0.5 2.5	S. N. by W. S. by W. S.S.E. S. by W. S.S.W.	0.2 1.5 0.2 0.5 2.0 1.5	S. N. by W. S. by W. S. by W. S. W.	0.5 2.0 0.5 1.0 2.0 3.0	S. N. by W. S.S.W. S. by W. S.W. S.W.	0.2 1.5 0.5 0.5 1.5 0.2	N.N.W. S. S. S.S.W.	0.0 1.0 0.2 0.2 0.5 0.0	12 13 14 15 16 17	JULY.
S. S.S.W. S. by W. N.W. S. by E. E.S.E.	0.5 0.2 0.2 0.5 0.2 0.2	S. S.W. S. N.W. S. E.S.E.	1.0 0.2 0.5 1.5 0.2 0.2	S.S.W. S.S.W. S. N.W. S. by E. E. by S.	0.5 0.2 0.2 1.0 0.2 0.2	S.S.W. S.S.W. S.W. by S. N.W. S. by E. E. by S.	0°2 0°2 0°2 0°5 0°2 0°2	S.W. S.S.W. S.W. W.N.W. S. by E. E. by S.	0°2 0°3 0°5 0°5 0°2	S.S.W. N.E. N.N.W. E.N.E.	0.5 0.0 1.0 0.0 0.2	19 20 21 22 23 24 25	
N. S.S.E. E. by S. S.E. by S. S.E. by E.	1.5 0.2 0.2 0.2 0.2 0.2	N. S.S.E. E.S.E. E.S.E. S.E. W.	1.0 0.2 0.2 0.2 0.2	S.S.E. E. by N. E.S.E. S.E. S.W. by W.	0.5 0.2 0.2 0.2 0.2 0.2 0.2	N. S.S.E. E. by S. S.E. by S. S.E. by S.	1.0 0.2 0.2 0.0 0.2 0.2	N. by E. S.S.E. E. S.E. S.E. E.S.E. S.W.	1.5 0.2 0.2 0.2 0.2 0.2	N. by E. S.S.E. E. by S. S.E. by S. S.E. by S. W.	1'0 0'2 0'2 0'2 0'5 0'5	26 27 28 29 30 31	
								1 021		23h.		1	<del></del>
18h. Direction.	Force.	Direction.	Force.	20h. Direction.	Force.	Direction.	Force.	22h. Direction.	Force.	Direction.	Force.		Göttinger ime.
N.E. by E.	lbs.	N.E. by E.	lbs.	N.E. by E.	lbs.	N.E. by E.	lbs. 0.2 0.0	N.E. by E.	lbs. 0°2 0°0		lbs. 0.0 0.0	1 2	)
N.N.W.  S.W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	S.S.W. N.N.W.  S.W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.W.  N. by W.   W. by N.   W. by N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N. by W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.W. by W. N. by W.  S.  N.  N.  N.  N.  N.  N.	0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.W. N. by W.   N. by E.		3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	JULY.

	1			1117011	ON AND FOI	OLI OE	I		43.		<b>~</b> 1.	
Mean Göttingen Time.	011.	1	1 ^h .		2 ^h .	1 .	3h.		4 ^h .		5h.	1_
I I I	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Fore
$\left( egin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \end{array} \right)$	E. by S.  N.N.E.	0.0 0.0 0.0 0.0 0.2 0.0 0.2		0.0 0.0 0.0 0.0 0.0 0.0	N.N.E. N.N.E.	0.0 0.0 0.0 0.0 0.0 0.2 0.2	S.E. by S.  E. by S.  N.N.E.	0.0 0.2 0.0 0.2 0.2 0.2	S.S.E. S. by E. E. by S. E. E.	0.0 0.2 0.2 0.2 0.2 0.2	S.W. S.S.E. S. by E. E. by S. E.S.E. E.	0,000
8 9 10 11 12	E	0.0 0.0 0.0 0.0 0.0	E. — — —	0.0 0.0 0.0 0.0 0.0	E. by N.	0.0 0.0 0.0 0.0 0.0	E. by N.	0.0 0.0 0.0 0.0 0.0 0.0	E  S.S.E S.W. by S.	0.2 0.0 0.0 0.0 0.2 0.2	E. by S. E.S.E. S.S.E. S.W. by S.	0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0
TSDDOV 114 15 16 17 18 19 20 21	W. by N. N.W. by W.	0.0 0.0 0.0 0.0 0.0 0.2 0.2	W.N.W.  W. by N. W.N.W.	0.0 0.0 0.2 0.0 0.2 0.5	N.W. N.W. W. by N. W.N.W.	0.0 0.0 1.0 0.2 0.2 0.2	N.W. W.N.W. W.S.W. W.N.W.	0.0 0.0 1.0 0.5 0.2 0.2	W.S.W. W.N.W. N.W. by W. S.W. by W. W. by N.	0.2	S.S.W. W.N.W. N.W. by W S.W. by W. N.W.	$\begin{bmatrix} -0 \\ 0 \\ 1 \\ 1 \\ 0 \\ 2 \end{bmatrix}$
22 23 24 25 26 27 28	N.N.W. — — N.W.	0.5 0.0 0.0 0.0 0.0 0.2 0.0	W. by N.  N.W.	0.5 0.0 0.0 0.0 0.0 0.2	E. by S.  N.W.	0.5 0.0 0.0 0.0 0.0 0.0	E.S.E. E. N.W.	0.0 0.0 0.0 0.2 0.2 0.0	E.S.E. S.S.E. N.N.W.	0.5 0.0 0.0 0.5 0.0	E.S.E. E.S.E. S. by W. N.N.W.	
29 30 31		0.0	E.S.E.	0.0	S.S.E. N.W. by N.	0.5	S. by E. N.N.W.	0.2	S. by W. N.N.W.	0.2	S.S.W. N.N.W.	1 0
(continued) Mean Göttingen	12h.		13h.		14h.		15h.		16h.		17 ⁿ .	
Time.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	For
TSDDA 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	S. S.E.  N E. S.E. by S.  S.S.W. E. by S.  N.W. by W. W. by N.	lbs.	S. S. E.  N. by W.  S.E. by S.  S.S.W. E. by S.  N.W. by W. W. by N. W. by N.	lbs.	S.S.E.  N. by W.  S.E. by S.  E. by S.  N.W. by W.	lbs.	N. by W.	lbs.	E. N. by W.	lbs.	E.N.E. N	lbss

				DIRE	CTION .	AND FORCE	OF TI	IE WIND.					
6 ^h .		7 ^h .		8 ^h .		9 ^h .		10 ^h .		11 ^h .		Mean	Göttingen Time.
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	]	a nue.
S.W. by S. S.S.E. S. by E. E. S.S.E. S.E.	lbs.  0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2	S. S. S. S. S. S. S. S. S. S. S. S. S. S	lbs.   -   0.2   0.2   0.2   0.2   0.0   0.2	S. by E. S. by E. E.S.E. S.S.E. S.E.	1bs 0.2 0.2 0.2 0.2 0.2 0.2 0.2	S. by E. S. by E. E. S. E.	1bs. — 0.2 0.2 0.2 0.2 0.0 0.2	S. by E. S. by E. E. S.E.	1bs. 0.2 0.2 0.2 0.2 0.0 0.0 0.2	S. S. S. S. S. S. S. S. S. S. S. S. S. S	1bs. 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.	1 2 3 4 5 6 7	
E.S.E. S.E.	0.5 0.5 0.0 0.0 0.0 0.0	E. by N. E.S.E. S.S.E. E. by S.	0·2 0·2 0·0 0·2 0·2 0·0	E.S.E. E.S.E. E.S.E.	0.5 0.0 0.0 0.0	E. W.N.W.  E. by S. S. by E.	0.5 0.0 0.5 0.5	E. S.W. E. by S. S. by E.	0.2 0.0 0.2 0.0 0.5 0.5	E. S.E. by S. W.N.W. E. by S. S. by E.	0·2 0·2 0·0 0·2 0·2 0·2	8 9 10 11 12 13 14 15	ST.
S.S.W. S.S.W. N.W. by W. N.W. by W. S.W. W.N.W.	0.2 0.2 1.0 1.0 2.0 2.0	S.S.W. S.S.W. N.W. W.N.W. W. N.W. by N.	0.2 2.0 1.0 2.0 1.5	S.S.W. S.W. by W. N.W. W. by S. W. N.N.W.	0°2 0°2 2°0 1°5	S.S.W. S.W. by S. N.W. W.N.W. N.W. by W. N.N.W.	0°2 0°2 2°0 1°5 2°0 1°0	S. by W. S.W. by S. N.W. W.N.W. N.W. by W. W.N.W.	0°2 0°2 3°0 2°0 0°2 1°0	S.W. by S. N.W. by W. W. by N. N.W. W.N.W.	0.0 0.2 2.0 1.5 0.5 0.5	16 17 18 19 20 21	AUGUST.
E.S.E. E.S.E. S. by E. N.	0.0 0.0 0.2 0.5 0.5 0.0	S.E. by S.  E.S.E. S. by E. N.	0.2 0.0 0.2 0.2 0.5 0.0	S.E. by S. E.S.E. S.S.E. S.S.W.	0.2 0.0 0.5 0.2 0.5 0.0	S.E. by S. S. by E. E. by S. S.S.E. S.S.W.	0.2 0.2 0.5 0.2 0.5 0.0	S.E. by S. S. by E. E. by S. S. S.S.W.	0°2 0°2 0°5 0°5 0°0	S. S. W.	0.0 0.0 0.0 1.0 0.2 0.0	23 24 25 26 27 28 29	
S. by W. N.N.W.	1:0 0:2	S. by W. N.N.W.	1.0 0.5	S. by W. N.N.W.	0.5	S.S.W. S.E. by S.	1.0 0.5	S.W. by S. S.E. by S.	1.0 0.5	W.N.W. S.E. by S.	0.2	30 31	)
18 ^h .		19 ^h .		20 ^h .		21 ^h .		22 ^h .		23h.		Mean	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	]	l'ime.
N.E. by E.  N.E. by E.  N. W. by N.  N.W. by N.  N.N.E. E.N.E. W.S.W.	lbs.	N.E. N.E. N.N.E.  E.  N.W.  N.W.  N.N.W.   N.N.W.	lbs.	N.E. N.N.E.  E.  N.W.  N.W.  N.N.W.	1bs.	N.E. N.E. E.  N.W. by N.  W. by N.  N.N.W.	lbs.	N.E. N.N.E. E. by N.  H. W. by N.  N.N.W.  W. by N.  N.N.W.  W.N.W.	1bs.	E. by S.  N.N.E.  E. by N.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.  N.W.	lbs.	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	AUGUST.

		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		Di	RECTIO	ON AND FOR	RCE OF	THE WIND					
Mean G	ottingen	O ^h .		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
Tim	e. [	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1\\2\\3\\4 \end{pmatrix}$		1bs. 0.0 0.0	S. by E.	lbs. 0'0 0'0 0'2 0'0	 S. by E. N. by E.	lbs. 0°0 0°0 0°2 0°2	E. by S. — E.N.E.	lbs. 0°2 0°0 0°0 0°5	E.S.E. S.S.W. E. by N.	1bs. 0'2 0'0 0'2 0'5	S.S.E. S. by E. S.S.W. E.	lbs. 0°2 0°2 0°2 1°0
	5 6 7 8 9 10	E. N.W. by W.	0.0 0.0 0.2 0.0 0.0	E. by S. W.N.W.	0.0 0.0 0.5 0.5 0.0 0.0	E. by S. E. by S. W.N.W.	0.0 0.2 0.2 0.0 0.0	S.W. E. by N. S.E. W. S.	0.2 0.5 0.2 0.2 0.0 0.5	S.S.W. E. by N. S. N.N.W. S.S.E. E.	0.5 0.5 0.5 0.2 0.2 0.5	S. by W. E.N.E. S. N.W. S.S.E. E.	0.5 1.0 1.0 0.2 0.2 0.5
SEPTEMBER.	12 13 14 15 16 17 18	N.W. N.W. by N. — — N.E.	0.2 0.2 0.0 0.0 0.0 0.5	N.W. by N. N.W. E.N.E. N.E. by E.	0.5 0.2 0.0 0.2 0.0 0.5	N.W. N.W. by N. N.W. N.N.W. E. by N. N.E.	1:0 0:5 0:2 0:2 0:2 0:5	W.N.W. N.W. by N. N.N.W. E. by N. N.E. by E.	1.0 0.2 0.2 0.5 0.5	N.W. by W. N.W. by N. W.N.W. S. E.	1:5 1:5 0:2 0:5 0:5	N.W. N.W. by N. W.N.W. S.S.E. E.	2:0 2:0 0:2 0:2 0:5 0:2
	19 20 21 22 23 24 25	N.N.W. N. by E. N.E. by E. N.N.E.	0.0 0.2 0.2 0.0 0.5 0.5	N.W. by N. N. by E. E. N. by E.	0.0 0.2 0.2 0.0 0.5 0.5	N. by W. N. by E. S.S.W. E. N.E. by E.	0.0 0.2 0.2 0.2 0.5 0.2	E.N.E. N. by W. W. by N. S.S.W. E. by N. N.N.E.	0.2 0.2 0.2 0.2 0.5 0.5	N.E. N. by W. S.S.W. S. by W. E. by N. N.E. by N.	0.2 0.2 0.5 0.2 0.5 0.2	N. by E. N.W. by N. S. S.S.W. E. by N. N.E. by E.	0.2 0.2 0.5 0.2 0.5 0.5
	26 27 28 29 30	S.S.W. W. by S. W. W.N.W.	0.5 0.5 0.5 0.5	N. by E. W.S.W. W. by S. W.N.W.	0.5 0.5 0.5 0.5 0.5	N.E. W.S.W. W. W. by N.	0.2 0.2 0.2 0.5 0.2	N.E. W.N.W. W.S.W. W.	0.2 0.2 0.5 0.5	N.E. W.N.W. S.W. W.N.W.	0.2 0.5 0.5 0.5	S. by E. W. by N. W. W. by N.	0°2 0°5 0°5 0°5
(continu	ed)	1		1				1>		1 ach		17 ^h •	
Mean Gö Tim		12 ^h .		13h.	<del></del>	14h.		15h.	l	16 ^h .	Force.	Direction.	Force.
	$\left(\begin{array}{c}1\\2\\3\\4\end{array}\right)$	N. by W. E. by S.	lbs. 0.0 0.0 2.5 1.0	N.N.W. E. by N.	Ibs. 0'0 0'0 1'5 0'5	S. by E. N.N.W. E. by N.	lbs. 0°0 0°2 0°5 0°5	N.N.W. E. by N.	lbs. 0'0 0'0 0'5 0'5	N.N.W. E. by N.	lbs. 0.0 0.0 0.2 0.5	N.N.W. E. by N.	lbs. 0°0 0°0 0°2 0°2
	5 6 7 8 9 10	S.E. by E. E. by N. S.W. by W. S. by W.	0.5 1.0 0.5 0.0 0.0	E. by N. S.S.W. S. by W.	0.0 0.2 0.2 1.0 0.0 0.0	E.N.E. S.S.W. S.W. by S.	0.0 0.5 0.2 0.5 0.2 0.0	S.S.W. S.W. by S.	0.0 0.0 0.5 0.2 0.0 0.0	N.W. S.W. by S.	0.0 0.0 1.2 0.0 0.0	  N.N.W.	0.0 0.0 2.5 0.0 0.0
SEPTEMBER.	12 13 14 15 16 17 18 19	N.W. N.W. by N. — E.N.E. E.N.E.	1.5 0.2 0.0 0.0 0.2 0.2	N.W. N.W. by N. — W.N.W. E.	1.5 0.5 0.0 0.0 0.2 1.0	N.W. by N	1.5 0.2 0.0 0.0 0.2 0.5	N. by W. N.W. N.N.W.  E.N.E. E.N.E.	0.5 0.2 0.0 0.2 0.0	N. by W. N.W. N.N.W. — E.N.E. E.N.E.	0.2 0.2 0.0 0.2 0.2 0.2	N.W. by W. N.W. N.N.W. E. by N. E.N.E. E.N.E.	0.5 0.2 0.2 1.0 0.5
	20 21 22 23 24 25 26	N.E. N. S. by E. S.S.E. E. by N. E. by N.	0.5 0.5 0.5 0.2 0.2 0.2	E. by N. E. by N.	0.0 0.2 0.0 0.2 0.2	N. N. E. by N. E.N.E.	0·2 0·2 0·0 0·0 0·2 0·2 —	N.N.W. N. N.E. E. by N.	0.2 0.2 0.0 0.0 0.2 0.2	N.N.W. N. by W.  N.E. by N. E. by N.	0.2 0.2 0.0 0.0 0.2 0.2	N.N.W. N. by W.  N.E. by N. E. by S.	0.2 0.2 0.0 0.0 0.2 0.2
	27 28 29 30	w. w.	0.0 0.2 0.0	<u>w</u> .	0.0 0.2 0.0	W. by N. W. —	0.0 0.0 0.2	N.W. W. —	1.0 0.5 0.0 0.0	N.W. by W.	0.0 0.0 0.0	W.N.W.  N.W. by W. 	0.2 0.0 0.2

				DIR	ECTION	AND FORC	E OF T	HE WIND.					
6h.		7h.		8h.		9h.		10h.		11h.	1		öttingen
ction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	] 1	ime.
S.E. y <b>E.</b> .W.	lbs. 0°2 0°2 0°2 1°0	S. by E. S. by E. S.S.W. E.	lbs. 0°2 0°2 0°5 0°5	S. by E. S. by E. S.S.W. E. by N.	lbs. 0°2 0°2 0°2 0°5	S. by E. S. by E. S.W. by S. E. by N.	0.2	S. by E. S. by E. N.W. by W. E. by S.	lbs. 0°2 0°2 2°0 0°5	N.N.W. E. by S.	lbs. 0.0 0.0 2.0 1.0	1 2 3 4	
y W.   y N.   y E.   S. W.   S. E.	0·2 1·0 1·0 0·2 0·2 0·5	S. E.N.E. S. S.S.E. S.S.E. E.	0°2 1°0 1°0 0°5 0°2 0°5	S. N.E. by E. S. S. by E. S.E. by S. E.	0°2 1°0 0°5 0°5 0°2 0°5	S.E. by E. E.N.E. S. S. S.S.E. E.	0.2 2.0 0.5 0.5 0.2 0.5	S.E. by E. E.N.E. S. by W. S.E. by S. E.	0.2 1.0 0.2 0.2 0.0 0.5	S.E. by E. E.N.E. S. by W.	0.5 1.0 2.0 0.0 0.0 0.0	5 6 7 8 9 10	
by W. W. by S. S. by E.	1.5 1.5 0.5 0.2 0.5 0.2	W.N.W. N.W. S. by W. S. E. E. by N.	1.5 1.5 0.2 0.2 0.5 0.2	N.W. by W. W.N.W. S. by W. S. E. by N. N.E.	1.5 1.5 0.2 0.2 0.5 0.2	N.W. W.N.W. S. by W. S. by E. E.N.E. N.E. by E.	1:0 1:5 0:2 0:2 1:0 0:2	N.W. by W. N.W. S. by W. S. by E. E.N.E. E.N.E.	1.5 0.5 0.2 1.0 1.0	N.W. by N. E.N.E. E.N.E.	0.0 0.2 0.0	12 13 14 15 16 17 18	SEPTEMBER.
N.E. N. y W. by S. y N.	0.2 0.5 0.5 0.2 0.5 0.2	N.E. by N. N.N.W. S. by W. S.S.W. E.S.E. E. by S.	0.2 0.5 0.5 0.2 0.5 0.2	N.N.E. N.W. by W. S. by W. S. by W. E. by N.	0.2 0.5 0.5 0.2 0.5 0.2	N.E. by N. N.W. by W. S. by W. S. by W. E.S.E. E.	1.0 0.2 0.2 0.2	N.E. by N. N.N.W. S.S.W. S. by W. E. E.	0.2 0.5 0.5 0.2 0.2 0.2	N.E. N.N.W. S. by W. E. by N.	0.2 0.5 0.0 0.2 0.2 0.2	20 21 22 23 24 25 26	
S.E. W. by S. S.W.	0.2 0.5 0.5 1.0	N.E. by E. N.W. by W. S.W. by S. W.	0.5 0.5 1.0 0.5	S.S.W. N.W. by N. N.W. by N. S.W. by W.	0.5 1.0 1.0	S.W. N.W. by N. W. W.N.W.	0.5 1.0 1.0 0.5	S.W. by S. N.W. by W. N.W. by W. W.	0.5	W.N.W. W. W. by S.	0.0 1.0 0.5 0.5 0.5	26 27 28 29 30	
18h.		19h.		20h.		21h.		22h.		23".		Mean G	löttinge
ction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	T	ime.
T.W.	lbs. 0'0 0'0 0'2  0'0 0'0 0'0 1'5 0'0		lbs. 0.0 0.0 0.2  0.0 0.0 0.0 1.0 0.0		lbs. 0.0 0.0 0.2 0.0 0.2 0.0 0.2 0.5 0.0	N.N.E.	lbs. 0.0 0.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.5 0.0	N.N.E.	lbs.   0.0   0.0   0.0   0.0   0.5   0.0	N.N.E.  N.N.E.  E. by N. N.W. by W.	lbs. 0.0 0.0 0.2 0.0 0.2 0.2 0.2 0.2 0.0	1 2 3 4 5 6 7 8	
	0.0 	N.W. by N. N.W. E. by N. E.N.E.	0.0 0.0 0.5 0.2 0.0 0.2 0.0	N.W. by N. N.W. — E.N.E.	0.0 	N.W. by N.  N.  E.N.E.	0.0 0.0 0.0 0.5 0.0 0.2 0.0 0.0	N.W. by N. N. E.N.E.	0.0 	N.W. by N. N. E.N.E.	0.0 0.0 0.2 0.0 0.2 0.0	10 11 12 13 14 15 16 17	SEPTEMBER.
y N. J.W. J.W. D.	0.5 0.2 0.2 0.0 0.5 0.0	E. N.N.W. N. by W. E.	0.5 0.2 0.2 0.0 0.2 0.0	E. by N. N.W. by W. N.N.W. E. by N.	0.5 0.0 0.2	E. by N. N.W. by W. N. by W. E. by N. N.E. by N.	0.2 0.0 1.0 0.5	E. by N. N.N.W. N. N.E. by E. N.E. by N.	0.2 0.5 0.2 0.0 1.0 0.5	N.N.W. N. N.E. by E. N.N.E.	0.0 0.2 0.2 0.0 1.0 0.5	18 19 20 21 22 23 24 25	IS SI
E. V.W. - -	0.0 0.0 0.0 1.0	E.S.E. W. — S.W.	0.5 0.5 0.0 0.0 0.5	E.S.E. W.S.W.	0.2 0.0 0.0 0.5	E.S.E. W.S.W. W. W. by S.	0.2 0.5 0.0 1.0	E. by S. W.S.W. W.N.W. W.N.W.	0.5 0.2 0.0 0.2 0.5	E. by S. W. by S. W.N.W.	0.5 0.2 0.0 0.0 0.5	26 • 27 28 29 30	

				DI	RECTIO	N AND FOR	CE OF	THE WIND					
Mean G		Oh.		1h.		2h.		3h.		4h.		5h.	
Tin	ne.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1\\2\\ 0\end{pmatrix}$	W.N.W. N.N.W.	lbs. 0'1 0'1	W. by N.	0.0 0.0	w.n.w.	0.0 0.3	N.W. by W. N.N.E.	0.7 0.1	N.W. N.W. by W.	1 ° 0 0 ° 1	W.N.W.	0.0 0.0
	3 4 5 6 7 8 9	E.N.E. E.N.E.	0.0 0.0 0.2 0.1 0.0	E. by N. E. E.N.E.	0.0 0.0 0.2 0.1 0.0	E.N.E. E. E.N.E. W. by N.	0.0 0.0 0.3 0.2 0.1	S. S. E.N.E. E. W.	0°1 0°2 0°3 0°0 0°1	S.W. by S. S. by E. E.N.E. E. E.N.E. W. by S.	0°1 0°5 0°4 0°3 0°1 0°2	S. by E. S.W. by S. E. by N. E. N. W.S.W.	0.3 0.2 0.3 0.3 0.1 0.3
OCTOBER.	10 11 12 13 14 15 16	W.N.W.  W. by S. N.N.W.  S. by E.	0.2 0.0 0.5 0.1 0.0 0.4	W.N.W. W. by S. N.W. by N.	0·3 0·0 0·7 0·1 0·0 0·4	W.N.W. S.E. W. by S. N.W. S. by E.	0.2 0.1 0.6 0.1 0.0 0.5	N.W. by W. W. N.W. by N. S.	0.5 0.0 0.6 0.2 0.0 0.5	W.N.W.  W. by S.  N.W. by W.  S. by W.	0.8 0.0 1.0 0.3 0.0 0.7	N.N.W. S.S.E. N.W. by W. N.N.W. S. by E.	0.6 0.1 0.9 0.4 0.0 0.5
TOO	17 18 19 20 21 22 23	N. by E. N.E. by N.	0.0 0.0 0.0 0.1 0.2 0.0	N.E.  N. by E.  N. by E.	0.0 0.1 0.0 0.0 0.0	N. by E. N. by E.	0.0 0.1 0.0 0.0 0.0	N. by W.	0.0 0.1 0.0 0.0 0.0 0.0	W.S.W. S.W. E. by S. N. S.W. by W.	0.0 0.1 0.1 0.1 0.4 0.1	E. by S. S.W. by W. S. by W. E.S.E. N. by E. W.N.W.	0·1 0·2 0·4 0·1 0·2 0·2
	24 25 26 27 28 29 30 31	N.W. by N. W. by N. N. — — N.N.E.	0.2 0.1 0.1 0.0 0.0 0.1	N.W. W. — W.S.W. N.N.E.	0.5 0.1 0.0 0.0 0.1 0.1	N.W. by W. W.N.W. N. —	0.3 0.5 0.0 0.0 0.0	W.N.W. N.N.W. N.W.	0.0 0.0 0.0 0.0	W.N.W. N. N.W. by N. S.S.W. S.S.W.	0.8 0.2 0.3 0.1 0.1 0.0	W. by S. N. N. by W. S.W. by S. S.W. by S.	1.0 0.4 0.1 0.2 0.3 0.0
(continu	ıed)		<u></u>	l			1	1	1				
Mean G		12 ^h .		13 ^h .		14 ^h .		15 ^h .		16 ^h .		17 ^h .	
Tim	ie.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{bmatrix} 1 \\ 2 \\ 2 \end{bmatrix}$	_	0.0 0.0	<u>-</u>	0.0 0.0		0.0 0.0	N. by W.	0°0 0°1		0.0 0.0	N. by E. N.	1bs. 0°1 0°1
	3 4 5 6 7 8 9	E. by N. E. N.N.W.	0.0 0.0 0.6 0.4 0.5 0.0	E.S.E. E. E. by N. N.W. by N.	0°0 0°1 0°3 0°5 0°4 0°0	E. E. E. N.N.W.	0.0 0.1 0.2 0.1 0.8 0.0	E. by N. E. E. N. N.W.	0.0 0.2 0.2 0.8 0.3	E.N.E. E. E. by S. N. by W. N.W. by W.	0.0 0.3 0.2 0.4 0.6 0.1	E. by N. E. E. by N. N.N.W. N.W. by W.	
OCTOBER.	10 11 12 13 14 15 16	W.N.W. N.W. S.E. by E.	0.0 0.0 0.2 0.4 0.0 0.1	— W. by N. N.N.W. S.S.E. S.E.	0.0 0.0 0.2 0.7 0.1	N. by W. N. by W. W. by N. N. S. by W. S.E. by E.	0·1 0·2 0·2 0·2 0·1	W. N.W. by N. S.W. by S. S.E. by S.	0.1 0.1 0.1 0.0 0.0	S. S.S.W.	0.3 0.1 0.0 0.0 0.0 0.0	S.W. by W. W. S. by E. S.W. by S.	0.1 0.1 0.1 0.1 0.0 0.1
OCT	17 18 19 20 21 22 23	S.W. by S. W. by S. N.E. by E.	0.1 0.0 0.1 0.4 0.0 0.0	S. by W. W. by S. N.E. by E.	0.2 0.0 0.1 0.4 0.0 0.0	S.W. by S.  N.W. by W.  N.E. by E.  E.N.E.	0.0 0.1 0.0 0.1 0.0	N.E.	0.0 0.0 0.0 0.0	N.W. N. by W. N.E. by N.	0.0 0.0 0.1 0.8 0.0	W.N.W.  N. N.E. by N.	0.0 0.0 0.1 0.2 0.0
	24 25 26 27 28 29 30 31	W.N.W. N. S. by E. S.S.W.	0.5 0.6 0.0 0.3 0.1 0.0	W.N.W. N. S. S. S.W. by S.	0.1 0.0 0.3 0.0 0.1	W. by N. N. S. by W. W.N.W.	0.1 0.5 0.0 0.1 0.0 0.1	W. by N. N	0.0 0.0 0.0 0.0 0.1 0.1	W. N. — —	0.0 0.0 0.0 0.0 0.1	W. N. 	0.0 0.0 0.0 0.0 0.1

	-		· · · · · · · · · · · · · · · · · · ·	DIRI	ECTION	AND FORCE	E OF T	HE WIND.					
6h.		7 ^h .		8 ^h .		9 ^h .		10 ^h .		11h.			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	]	me.
N.W.	lbs. 0.7 0.0	N.W. by W. N.N.W.	0.1	N.W. N. by W.	lbs. 0.5 0.1	N.W. by W. W.N.W.	lbs. 0°3 0°1	N.W. S.	0°3 0°2	N.N.W.	0°0	$\begin{bmatrix} 1 & 2 \\ 3 & 3 \end{bmatrix}$	
S.S.E. S.W. by S. E. by N. E.N.E. N. W. by S.	0.1 0.2 0.5 0.2 0.1 0.1	E.S.E. S.S.W. E. E. by N.	0°1 0°4 0°4 0°2 0°0 0°2	E.S.E. S. E.N.E. E. by N. S.W. by S.	0.1 0.5 0.6 0.4 0.0 0.2	E. by S. S. by E. E. by N. E. S.W.	0°2 0°6 0°6 0°2 0°0 0°4	E. by S. S.S.E. E. by N. E. by N. S.S.W.	0°1 0°2 0°6 0°2 0°0 0°2	E. by S.  E. by N. E. N. by W. S.W. by S.	0°1 0°0 0°4 0°3 0°1 0°3	4 5 6 7 8 9	
N.W. S. W. N.W. S.S.W. S.E. by S.	0.8 0.4 0.8 0.1 0.1 0.6	W. by N. S.S.W. W. by N. N.W. by N. S. by W. S.E.	0°3 0°4 0°9 0°4 0°1 0°5	W.N.W. S.E. W.S.W. N.W. by N.	0.0	W. S.E. by E. W. by S. N.N.W. S. by E. S.E.	0.2 0.1 0.9 0.3 0.1 0.4	W.N.W. S.E. by E. W.N.W. N.N.W.	0°2 0°1 0°6 0°3 0°0 0°2	W. by S. E.S.E. W.N.W. N.W. S.E. by E.	0·1 0·1 0·5 0·3 0·0 0·2	11 12 13 14 15 16 17	OCTOBER.
S.S.E. W. by S. S.S.W. N.E. by E. N. S.S.W.	0.2 0.2 0.5 0.1 0.5 0.2	S.E. by S. W. S.S.W. E.N.E. N.E. S.S.W.	0.2 0.2 0.8 0.1 0.2 0.5	S. by W. W.S.W. W. by S. E.N.E. N. by E. S. by W.	0.6 0.3 0.5 0.2 0.2 0.4	S.S.W. W.S.W. W.S.W. N.E. by E. N. by E. S. by W.	0.4 0.3 0.5 0.4 0.1 0.2	S.S.W. W. by S. W. by S. E.N.E. S.S.W.	0°3 0°2 0°5 0°3 0°0 0°2	S.W. by S. W. by N. W. by S. E.N.E. N. by E. S.S.W.	0.2 0.3 0.2 0.3 0.1 0.1	18 19 20 21 22 23 24	00
N.W. by W. N. S.S.W. S. by W. S.W. by S.	1.0 0.3 0.0 0.5 0.4 0.1	W. N. S.S.W. S.S.W.	0.9 0.6 0.0 0.2 0.5 0.0	W. by N. N. S.S.W. S	1:2 1:0 0:2 0:3 0:5 0:0	W. by N. N.N.W. S.W. by S. S. S. by E.	1.0 0.7 0.1 0.3 0.1 0.0	W.N.W. N. by E. W. S. by E.	1·1 0·8 0·2 0·4 0·0 0·0	N.W. N. W. S. by E. S.	1.4 0.7 0.1 0.2 0.1 0.0	25 26 27 28 29 30 31	
18h.		19 ^h .		20h.		21 ^h .		22 ^h .		23 ^h .		Mean (	Höttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		ime.
	lbs.		lbs. 0.0		lbs.	N.	1bs. 0'1	N.	1bs. 0°2	N.	1bs. 0°1	1	
N. by E.	0'1 0'0 0'0 0'3 0'3 0'2 0'3	E. by N. E. by N. N.W. by N.	0.0 0.0 0.4 0.3 0.2 0.1	E. by N. E. by N. E. by N. N.W.	0.0 0.0 0.3 0.5 0.1	N.E. by E. E. by N. E. E.N.E.	0.1 0.0 0.3 0.5 0.0 0.0	E. by S. E. by N. E.N.E.	0.0 0.0 0.4 0.2 0.3 0.0	E. by N. E. by N. E. N.E.	0.0 0.0 0.5 0.3 0.2 0.0	2 3 4 5 6 7 8 9	
W. by N. S.W. by W. S. by E.	0'1 0'0 0'2 0'0 0'0 0'4	W.N.W. S.W. by W. S. by W.	0.4 0.0 0.2 0.0 0.0 0.4	w. w.s.w.	0.5 0.0 0.3 0.0 0.6 —	W. by N. W.S.W.  S.S.W.	0.3 0.0 0.4 0.0 0.0 0.9	W. by N.  W. by S.  N.N.W.  S.S.W.	0.3 0.0 0.4 0.1 0.0 0.6	W.N.W. W.S.W. N.W. by N. S.S.W.	0.4 0.0 0.2 0.2 0.0 0.7	10 11 12 13 14 15 16	OCTOBER.
W. by N.  N.E. by N.	0.0 0.0 0.0 0.0 0.1 0.0	W. by N.  N.E.	0.0 0.0 0.0 0.0 0.1	W. by N. N.N.W. N.E. by N.	0.0 0.1 0.4 0.0	W. by S.  N.E. by N.	0.0 0.0 0.0 0.0 0.0	W. by S.	0.0 0.0 0.0 0.0 0.0	E.N.E N.E	0°1 0°0 0°0 0°2 0°0	17 18 19 20 21 22 23	00
N.E. W. N.	0.0 0.0 0.0 0.0 0.1 0.1 0.1	N.E. W. by N. N. —————————————————————————————————	0.0 0.0 0.0 0.0 0.0 0.0	N. by E. W. by N. N. —————————————————————————————————	0·1 0·2 0·2 0·0 0·0 0·0	N.N.W. W. by N. N. W. by N.	0.5 0.5 0.1 0.0 0.0 	N.N.W. W. by N. N. — — —	0·1 0·1 0·2 0·0 0·0 0·0	N.N.W. — N. — N. — — — — — .	0·1 0·0 0·2 0·0 0·0 - 0·0	24 25 26 27 28 29 30 31	

_	ſ	0,4										i .	
Mean Gör Tim		Oh.	Force.	1 ^h . Direction.	Force.	2 ^h . Direction.	Force.	3 ^h . Direction.	Force.	Direction.	Force.	5 ^h .  Direction.	Force
	$\begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ \end{bmatrix}$		lbs. 0 ° 0 0 ° 0 0 ° 0 0 ° 2 0 ° 2 0 ° 2	  W.S.W.	lbs. 0°0 0°0 0°0 0°0 0°2 0°0	E. by N. W.S.W.	lbs. 0°0 0°2 0°0 0°0 0°2 0°0	S.W.  W. W. W. N. by W.	lbs. 0°2 0°0 0°0 0°2 0°2 0°2	W.N.W. W.S.W. N. by W.	lbs. 0.0 0.0 0.0 0.2 0.2 0.2	S.W. S.W. by S. N.W. by W.	lbs. 0°0 0°2 0°2
BER.	7 8 9 10 11 12 13 14	W. by S. W. by N. W.S.W. W.N.W.	0.0 0.0 0.5 0.2 0.2	N.E. S. by W. W. by S. W. by S. W.S.W. W.N.W.	0·2 0·2 0·5 0·2 0·2 0·2	E. by N. S.W. by W. W.S.W. W. by S. W.S.W.	0·2 0·2 0·5 0·2 0·2 0·2	N.E. by N. S.S.W. W.S.W. W. by S. W.S.W. N.W.	0·2 0·2 0·5 0·2 0·2 0·2	E.N.E. S.W. W.S.W. W. by S. W.S.W.	0.2 0.2 0.5 0.2 0.2 0.2 0.2	N.W. W.N.W. W. W.S.W.	0.6
NOVEMBER	15 16 17 18 19 20 21	W. — E. N.W. by W.	0.2 0.0 0.0 0.5 1.5 0.0	W.N.W. — E.N.E. N.N.W.	0.5 0.0 0.0 0.5 1.0 0.0	E.N.E. N.N.W. N. by E.	0.5 0.0 0.0 0.5 0.5 0.5	N.W. — E.N.E. N.W. N.E. by E.	0.5 0.0 0.0 0.2 1.5 0.2	N.W. S. E.N.E. N.W. N.N.E.	1.0 0.2 0.0 0.2 1.5 0.2	N.W. by W. S.S.E. E. by N. N.W. by N. E. by N.	1 · 6 0 · 2 0 · 0 1 · 6 0 · 2
	22 23 24 25 26 27 28	E.N.E. — N.W. by N. W. by S.	0.0 0.5 0.0 0.0 2.0 0.5	E. — N.N.W. S.W. by S.	0.0 0.5 0.0 0.0 2.0 0.2	E. by N.  N. by W. S.W.	0.0 0.5 0.0 0.0 1.0 0.2	E.N.E.  W.N.W. S.W. by W.	0.0 0.0 0.0 0.0	E.N.E. S. by W. W.N.W. W.S.W.	0.0 0.2 0.0 0.2 0.5 1.0	N. by W. E. by S. W. N.W. S.W. by W.	0.9
(continu	29 30	N.N.W. S.S.E.	0°2 0°5	N.N.W. E.S.E.	0.5	N.N.W. E.S.E.	0.5	N	0.0	N.W. by N. S.E. by E.	0.2	N.N.W. S.E. by E.	0.
Mean Göt Tim		12h.	Force	13h.	Force	14 ^h .	72	15h.		16h.	72	17h.	E
	$   \begin{pmatrix}     1 \\     2 \\     3 \\     4 \\     5 \\     6   \end{pmatrix} $	Direction.		Direction.  N.W. by W.	lbs. 0°0 0°0 0°0 0°0 1°0	Direction.	lbs. 0°0 0°0 0°0	Direction.	lbs. 0.0 0.0 0.0 0.0	Direction		N.W. by W.	lbs. 0'0 0'0 1'0
ABER.	7 8 9 10 11 12 13 14	W.S.W. W. W. S.W. by W. E.S.E.	0.0 0.0 0.2 0.2 0.2 1.0 0.5 —	E.N.E.  W. W. W. by S. E.S.E.	0.0 0.2 0.0 0.5 0.2 0.2 1.5	W. by S. W.S.W. E. by S.	0.5 0.0 0.0 0.0 0.2 0.2 0.2 2.5	W E. by S. W.S.W. W. by S. W. by S. E. by S	0.2 0.0 0.2 1.0 0.2 0.2 0.2 0.2 2.5	W.N.W.  E. W.S.W. W.S.W. W. by S. W. by S. E. by S.	0.0 0.2 1.0 0.2 0.2 0.2 0.2 0.2	E. W.S.W. W. by S. E. by S.	0.5
NOVEMBER.	8 9 10 11 12 13	W.S.W. W. W. S.W. by W.	0.0 0.2 0.2 0.2 1.0 0.5	E.N.E.  W. W. W. W. by S.	0.0 0.2 0.0 0.5 0.2 0.2 1.5	W. W. by S. W.S.W.	0.0 0.0 0.0 0.2 0.2 0.2 2.5	E. by S. W.S.W. W. by S. W. by S.	0.0 	E. W.S.W. W.S.W. W. by S. W. by S.	0.0 0.2 1.0 0.2 0.2 0.2 0.0 0.0 0.0 0.5 0.2 0.5 0.5	E. W.S.W. W.S.W. W. by S.	0 

				DIRI	ECTION	AND FORC	E OF T	HE WIND.					
6 ^h •		7 ^h .		8h.		9h.		10h.		11 ^a .		Mean	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		Time.
S.S.W. S.W. by S. S.S.W. W. by S. N. N.E. by N. N.W.	lbs. 0°2 0°0 0°2 0°2 1°0 0°2 - 0°2 1°5	S. by W.  S.S.W. S. N.W. by W.  E. by N. W.N.W.	Ibs.   0°2   0°0   0°2   1°5   0°0	S.S.W. S.E. by E. S.W. by W. S.S.W. N.W. N.W. W.W.	lbs.   0°2   0°2   0°2   1°0   0°2	S. by W.  S. by W.  N.W. by W.  W.S.W.	lbs.   0°2   0°0   0°0   0°0	S.S.W. S.W. S. W.N.W. N.E. by E. W. by S.	lbs. 0°2 0°0 0°2 0°2 2°0 0°2 ———————————————	N.W. by W. S.S.E.	lbs. 0'0 0'0 0'0 0'0 0'0 1'5 0'2 0'0 0'2	1 \ 2 \ 3 \ 4 \ 5 \ 6 \ 7 \ 8 \ 9	
W.N.W. W. by S. W.S.W. N. by W.	0°5 0°2 1°0 0°2 —	W.N.W. W.N.W. W. by S.	0.2 1.0 0.0	N.W. W. by N. W. by S. S.E. by S.	0°5 0°2 1°5 0°2	W.N.W. W. W.S.W. E.S.E.	0°2 0°2 1°5 0°2	W. W. W.S.W.	0.5 0.5 1.0 0.0	W. W. S.W. by W. S.E. by E.	0.5 0.2 1.5 0.2 —	10 11 12 13 14	MBER.
N.W. S.E. by S. W. E. by N. N.N.W. E. by S.	1.5 0.2 0.2 0.2 1.5 0.2	N.W. by N. S.E. by S. E.N.E. N.N.W. E. by N.		N.W. by N. S. E. N.N.W. E.S.E.	1'5 0'2 0'0 0'2 1'5 0'2	N.W. by N. S.S.W.  E. by N. N.N.W. S.E.	1.0 0.5 0.0 0.5 1.5 0.2	N.W. by N. S.W. — N.N.W. E.	1:5 1:0 0:0 0:0 1:5 0:2	N.W. by N. S.W. N.N.W. N. by W. E. by S.	1.0 1.0 0.0 0.2 1.5 0.2	15 16 17 18 19 20 21	NOVEMBER.
E. W. N.W. by W. W.S.W.	0.0 0.2 0.0 0.2 1.0 0.5	E.S.E. S.W. by W. W.N.W. W.S.W.	0.0 0.2 0.0 0.2 1.0 1.0	E.S.E S.W. W.N.W. W. by S.	0.2 0.0 0.0 0.5 1.0 1.5	S.E. by S. S.W. by W. N.W. by W. W.S.W.	0.5 0.0 0.5 0.5 1.0	S.S.E. S.W. by W. N.W. by W. S.W.	0.0 0.2 0.0 0.5 0.5 1.0	S. by W. W.S.W. N.W. S.W.	0.0 0.2 0.0 0.5 0.2 1.5	22 23 24 25 26 27 28	
N.N.W. E.	0.5 0.5	N. E.	0.5	S.E. by E.	0.2	S.S.E. E.S.E.	0.5	S. by E. S.E.	0.5	E.S.E.	0.0	29 30	
18h.		19h.		20h.	·	21h.		22h.		23h.			Göttingen l'ime.
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	\	
   N.W. by N.   N.W.   N.W.   E.S.E.   E.N.E.   W.S.W.   W.S.W.   W.S.W.	lbs. 0'0 0'0 0'2 1'0 0'2 0'2 1'0 0'2 0'2 0'2 0'2 0'2 0'2		0.2 0.0 2.0 0.2 0.2 0.2	N.W. by N.   E. by S.   W.S.W.   W. by S.   W. by S.   W. by S.   N.W.   N.W.   N.W.	0.2 0.0 1.5 0.2 0.2 0.2	N.W. by N. E. W.S.W. W. by S. W. by S. W. by S. W. by S.	0.2 0.0 1.0 0.2 0.2 0.2	N. by W. E. by N. W.S.W. W. by N. W.S.W. W.S.W.	lbs. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	W. by S. N.W. by N.  W. by S. W. by N. W. by N. W.S.W. W.S.W.	lbs. 0'0 0'0 0'0 0'2 0'2 0'0 0'5 0'2 0'2 0'2 0'2 0'2	1 2 3 4 5 6 7 8 9 10 11 12 13	
S.W. by W. W.S.W. N. by E.  E.N.E. S.E. by S. N.W. by W. N.N.W.	0.0 0.0 0.2 0.0 1.5 0.2  0.0 1.0 0.2	S.W. by W. E.S.E. W. by S.  E. by N. E. by S. N.N.W. N.W.	0.0 0.0 0.2 0.2 1.5 0.0 1.0 0.2 0.2 1.0 0.2 0.2 1.5		0.0 0.0 0.2 0.2 1.5 0.0 1.0 0.2 1.0 0.2 1.0 0.2 1.0	W.S.W. E. by N. W.N.W.  E. by N.  W.N.W.  W.N.W. N.W. N.W. N.W.	0.0 0.0 0.2 0.2 1.5 0.0 0.5 0.0 0.2 1.0 0.2 1.0 0.2 1.0 0.2	W.S.W. E. N.W. by W.  E.N.E. S.W. W.N.W. N.W. W.S.W.	0.0 0.0 0.2 0.5 1.5 0.0 0.5 0.2 0.2 1.0 0.5  0.5	E. N.N.W. E.N.E. N.N.W. W.S.W. N.W. by N.	0.0 0.0 0.0 0.5 1.5 0.0 0.2 0.0 0.0 2.0 0.5 -	14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	NOVEMBER
S. by W.	$0.2 \\ 0.0 \\ 1.2$	S.E. S. by W.	$\begin{bmatrix} 1 & 3 \\ 0.2 \\ 0.2 \end{bmatrix}$	S.E. S. by W.	0.2	S.E.	0.0	S.E. by S.	0.0	S.S.E. S.	$0.2 \\ 0.2 \\ 0.5$	$\left[\begin{array}{c} 29\\30 \end{array}\right]$	

				Di	RECTIO	ON AND FOI	RCE OF	THE WINI	).			,	
Mean G		Oh.		1h.		2h.	·	3 ^h .		4 ^h .		5h.	
Tin	ne.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$ \begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix} $	S. N. by W. N.W. by W.	1bs. 0°5 0°0 0°2 0°5	S.  W.N.W.	lbs. 0.5 0.0 0.0 0.2	S. by W. N. by W.	lbs. 0.5 0.0 0.2 0.0	S.S.W. N.W. N. by W. S. by W.	lbs. 0.5 0.2 0.2 0.2	S.S.W. N.N.W. N.N.W. E. by N.	lbs. 0°5 0°2 0°2 0°2	S.S.W. N.N.W. N.N.W. S.S.E.	lbs. 0°5 0°2 0°2 0°2
	5 6 7 8 9 10	S.S.W. E.S.E. E.N.E. S.W. by W.	0.0 0.5 0.2 0.2 0.2 0.0	S.S.W. S. S.W.	0.0 0.5 0.5 0.0 0.5 0.0	S. by E. S.W. E. by S.	0.0 0.0 0.2 0.0 0.2	S.W. by S. S. by W. N.E. by E. W.	0.0 0.2 0.2 0.2 0.0 0.0	S.W. S.S.W. S. by W. W.S.W.	0.2 0.2 0.0 0.0 0.0 0.2	W.S.W. S.W. by S. S. E. by N. W. by S.	0'2 0'2 0'2 0'0 0'0
DECEMBER.	12 13 14 15 16 17 18	N.N.E. N. N. by E. N.E.	0.0 0.2 0.2 1.0 0.2 0.0	W.N.W. N.E. by N. N. by W. N.	0.5 0.5 0.0 0.0	W.N.W. N.E. by N. N. by W. N.N.E.	0.2 0.2 1.0 0.5 0.0 0.0	N. by E. N. by E. N. N. N. N. N.	0.0 0.2 0.5 0.5 0.5 0.2	N.E. N.E. N.N.E. N.	0.0 0.2 0.5 0.5 1.5 0.2	N. by E. N.E. N.N.E. N. S.W. by W.	0'0 0'2 0'2 0'5 2'5 0'2
I	19 20 21 22 23 24 25 a	N.N.W.  W.S.W. S.W. by S. W. by N.	0.5 0.0 0.2 0.2 0.5	N. by W. N. W. by W. W.S.W. S.W. W. by S.	0.5 0.2 0.2 0.5 0.5	N. by W. N.W. by W. W.S.W. S.W. W.S.W.	0.5 0.2 0.2 0.5 0.5	N. by W.  S.W. W. by S.	0.2 0.2 0.2	N.N.W. — S.W. N.W.	0.2 0.0 0.0 0.0	N.N.W. S.W. N.W. by W.	<b> </b> —
	26 27 28 29 30 31	W. S.W. S.W.	0.2 1.5 0.0 0.2 0.0	W. S.W. by W. S.S.W. S.S.W. N.E.	0.2 1.5 0.2 0.2 0.2	W. S.W. S.S.W. S.S.W.	0.2 0.5 0.2 0.2 0.0	W. S.W. S.S.W. S.W. by S.	0.2 0.5 0.2 0.2 0.0	W. S.W. S.S.W. S.W. by S. E.	0.2 2.0 0.2 0.2 0.2	S.W. by S. S.S.W. S.W. by S. E. by N.	0.0 1.5 0.2 0.5 0.2
(continu	ſ	12h.		13 ^b .		14 ^h .		15h.		16 ^h .		17 ^h .	
Mean G Tin		Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$ \begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \end{pmatrix} $	N.W. S.S.W.	lbs. 0.0 0.0 1.0 1.0	N.W. S. by W.	lbs. 0°0 0°0 1°0 1°5	 N.N.W. S.	lbs. 0.0 0.0 0.5 1.5	E. N.W. by N. S.	lbs. 0°2 0°0 0°5 1°5	 N.W. S. by W.	lbs. 0'0 0'0 0'5 1'5	 N.W. S.W. by S.	lbs. 0'0 0'0 0'5 1'5
	5 6 . 7 . 8 . 9 . 10 . 11	S.W. by W. S.W. by W.	0.0 0.0 0.2 0.0 0.2	S. by E. S.W.	0.0 0.0 0.0 0.0 0.0 0.0	S.W. by W.	0.5 0.0 0.0 0.0 0.0 0.0	S.S.W. S. by E.	0.0 0.0 0.2 0.2 0.0 0.0	S. by W. S.W. by W.	0.0 0.0 0.0 0.0 0.0	S.W. by W. E.N.E.	0.5 0.0 0.0 0.2 0.0 0.2
DECEMBER.	$\left \begin{array}{c} 12\\ 13\\ 14\\ 15\\ 16\\ 17\\ 18\\ \end{array}\right $	N. by W. N.N.E. N. by E. N. by W. S.W.	0.2 0.2 0.2 0.0 0.2 0.0 0.2 1.5	N.N.W. N. by E. N. by W. S.W. by W.	0.2 0.2 0.2 0.0 0.2 1.0	N.N.W. N. N.N.E. N. S.W. by W.	0.2 0.2 0.2 0.0 0.5 1.5	N. by W. N. by E. N.N.E.  N. by E. S.W.	0°2 0°2 0°5 0°0 0°2 0°5	N. N. W. N.E. by N	0.5 0.5 1.0 0.0 0.0 0.0	N. by E. N. N.E. by N.  S.W. by W.	0°2 0°2 1°0 0°0 0°0 0°2
I	19 20 21 22 23 24 25 a	N. by W. S.W. N.W. S.W. by W. N.W.	0.5 2.0 1.5 0.5 0.2	N. S.W. N.W. S.W. by W. N.W.	0°2 1°5 1°5 0°5 0°2	S.W. N.W. S.W. by W. W.N.W.	0.0 2.0 1.0 0.5 0.2	S.W. by S. W. W.S.W. W. by N.	0.0 2.5 0.5 0.5 0.2	S.S.W. W. S.W. by W. W.N.W.	0.0 2.5 0.5 1.0 0.2	N. S.W. W. by N. W.S.W. W.N.W.	0.2 2.5 0.2 1.0 0.2
	26 27 28 29 30 31	s.s.w.	1.0 0.0 0.2 0.0 0.0	s.s.w.	1.0 0.0 0.2 0.0 0.0	s.s.w.	1:0 0:0 0:2 0:0 0:0	s.s.w.	1'0 0'0 0'2 0'0 0'0	s.s.w.	1'0 0'0 0'2 0'0 0'0	s.  	0.0 0.0 0.0 0.0

^a Christmas Day.

				DIRI	ECTION	AND FORC	E ОБ Т	THE WIND.				11 -	
6 ^h .		7 ^h .		8h.		9h.		10h.		11h.			Göttingen ime.
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	] 1	
S.S.W. N.W. by N. N. by W. S.	lbs. 0°5 0°2 0°5 0°2	S.S.W. N.N.W. N. by W. S. by E.	lbs. 0.5 0.2 1.0 0.2	S. N.W. by N. N.N.W. S.S.E.	1bs. 0.5 0.2 1.0 0.2	S. by W. N.N.W. N.N.W. S.	1bs. 0°2 0°2 1°0 0°2	S.W. N.N.W. S.S.W.	1bs. 0°2 0°0 1°0 0°5	N.W. S.S.W.	1bs. 0°0 0°0 1°0 0°5	1 2 3 4 5	
W.S.W. S.S.W. S.S.W. E. by N. S.W. by W.	0.2 0.2 0.5 0.2 0.2 1.0	W. by S. S.S.W. E.N.E. S.W. W. by N.	0.2 0.0 0.5 0.2 0.5 1.0	S. by W. S.W. by S. N.E. by E. S.W. W. by S.	0.2 0.0 0.5 0.2 0.2 0.5	S.W. by S. E. S.W. by W. W. by S.	0.0 0.0 1.0 0.2 0.2 0.5	E.S.E. S.W. E. by N. W.S.W. W. by S.	0.0 0.2 1.0 0.2 0.2 0.5	s.w.	0.0 0.0 0.5 0.0 0.2 0.0	+ 6 7 8 9 10 11	
N. by E. N. by E. N.E. N.E. S.W. by W.	0.0 0.2 0.2 0.2 1.5 0.2	N.E. by N. N. N. N.N.E. N. S.W. by S.	0.2 0.2 0.2 0.2 0.2 1.0 0.5	N. by E. N. N.N.E. N. S.W. by S.	0.0 0.2 0.2 0.5 0.5	N. by E. N. N. N. S.W. by S.	0.0 0.2 0.2 0.0 0.5	N.N.E. N. by E. N.N.E. S.W.	0.0 0.2 0.5 0.2 0.0 0.5	N.N.E. N. by E. S.W.	0.0 0.2 0.2 0.0 0.0 0.0	$\begin{array}{ c c c }\hline 12\\ 13\\ 14\\ 15\\ 16\\ 17\\ 18\\ 19\\ \end{array}$	DECEMBER.
S.W. by W. S.W. by S. N.W.	0.5 0.0 4.5 1.0	N.N.W. S.W. by W. N.W. S.W. N.W. by W.	1.0 0.5 0.2 2.0 0.5	N. S.W. by W. N.W. S.W. N.W.	1.0 1.5 0.2 2.0 0.2	N.N.W. S.W. by S. N.W. S.W. by W. N.W.	1:0 1:5 0:2 1:0 0:2	N.W. S.W. by S. N.W. W. by S. N.W.	0.5	N. by W. S.W. N.W. S.W. by W. N.W.	1.0 1.5 1.5 0.5 0.5	20 21 22 23 24 25 a 26	
W. S.W. S.W. by S. E. by S.	0'2 2'5 1'5 1'0 0'2	S.W. by W. S.W. S.S.W. S.W. by S.	0.5 2.0 0.5 0.5 0.0	S.W. by W. S.W. S.S.W. S.S.W.	0.5 0.5 0.0	S.S.W. S.W. S.S.W. S.W. by S.	0.5 1.0 0.2 0.2 0.0	S.S.W. S.W. S.S.W. S.W. by S.	1.0 1.0 0.2 0.5 0.2	S.W. S.S.W.	1:0 0:2 0:0 0:0 0:0	26 27 28 29 30 31	
18 ^b .		19 ^h .		20 ^h .		21 ^h .		22 ^h .		23h.		Mean	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	]	l'ime.
 N.N.W.	lbs. 0'0 0'0 0'5	 N.N.W.	0.0 0.0 0.5		lbs. 0.0 0.0 0.5	 N.W. by W.	lbs. 0.0 0.0 0.2	N. by W. N.W. by W.	1bs. 0°0 0°2 0°2	N. by W. N.W. by W.		$\begin{bmatrix} 1\\2\\3\\4 \end{bmatrix}$	
W.N.W. S. by W.	0.5 0.0 0.0 0.0 0.0	W.N.W. S. W. by N.	0.5 0.0 0.2 0.0 0.0	W.N.W. S. N.W. S.W.	0.2 0.5 0.0 0.2 0.2 0.0	N.W. by W. S. by W. — — —	0.0 0.0 0.0 0.0 0.0	N.W. by W. S. by W. S.W. S.W.	0.2 0.5 0.0 0.0 0.2 0.2	N.W. by N. S.S.W. N.N.E.	0.5 0.0 0.0 0.0 0.0	5 6 7 8 9 10	
N. by W. N.E. by N.	0.0 0.2 1.0 0.0 0.0	N. by E. N.W. by N. N. by E. N. by E.	0.0 0.2 0.2 0.5 0.2 0.0	N. by E. N. by W. N. by E. N. by W.	0.0 0.2 0.2 1.0 0.2 0.0	N. by E. N. by E. N. by E. N. by W.	0.0 0.2 0.2 1.0 0.5 0.0	N. by E.  N. by E.  N. by E.  N.N.E.	0.0 0.2 0.0 0.5 0.5 0.0	N.N.E.  N. by E.  N.E. by N.	0.0 0.2 0.0 0.5 0.2 0.0	12 13 14 15 16 17	DECEMBER.
S.W. by S. W. by N. W.S.W.	0.0 0.0 2.0 0.5 0.5	N.E. by N. S.W. by S. W.S.W. W.S.W.	0.0 0.2 1.5 0.2 0.2	N. by W. N.N.E. W.S.W. W.S.W. W. by N.	0.2 0.2 1.0 0.2 0.2	N. by W. N.N.E. W.S.W. W.S.W. W. by N.	0.2 0.2 0.2 0.2 0.2 1.5	N.N.W. N. by E. W.S.W. W.S.W. W. by N.	0.5 0.2 0.2 1.0	N.W. by N. W.S.W. W.S.W. W. by N.	0.0 0.5 0.5 1.0	19 20 21 22 23 24	DI
s.w.	0.0 0.0 0.0 0.0 0.0 -	S.W. S.W. by W.	0.0 2.0	s.w. s.s.w.	0.0	S.W. by W. S.S.W.	0.0 1.5 0.0 0.0 0.0 0.0	W. S.W. S.S.W.	0.2 1.5 0.0 0.0 0.0	W. S.W. S.S.W.	0.2 1.5 0.2 0.0 0.0 0.0	25 a 26 27 28 29 30 31	

		1				,		THE WIND.					
	öttingen [	O ^h .		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
Tin	ne.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Fore
	$\begin{pmatrix} 1 \\ 2 \end{pmatrix}$		0°0	S.E. by E.	1bs. 0.2	E.S.E.	1bs. 0.2	S.E. by E.	1bs. 0.2		0.0		1bs.
	2 3 4	S.W. by S. N.W.	0.2	S.W. W.N.W.	0.5	S.W. N.W.	1.0	S.W. by S. N.W.	1.5 0.5	S.W. by S. N.N.W.	1.0 1.5	S.W. by S. N.W.	0.
	5 6	N.W. by N.	0.2	N.W. by N.	0.2	S.E. N.W. by N.		E.S.E. N.W. by W.		S.E. by S. N.W. by W.	0.5	S.E. by S. N.W. by W.	
	8	S. by W.	0.2	S. by W.	0.2	S.W. by S.	0.2	N.N.E. S.W.	$\begin{array}{c c} 0.3 \\ 0.5 \end{array}$	N.E. by N. S.W.	$\begin{array}{c} 0.5 \\ 0.5 \end{array}$	N.E.	0.
	9 10 11	N. S.W.	0.5	N. S.W.	$\begin{array}{c} - \\ 0.2 \\ 0.2 \end{array}$	N. by E. S.S.W.	$0.2 \\ 2.5$	N. S. by W.	0.5 3.0	N. S.S.W.	0.2 $2.5$	N. S.S.W.	0.
	12 13	N.W. S.E. by S.	$0.5 \\ 0.5 \\ 0.5$	S.E. by S.	0.0	s.s.e.	0.0	S.S.E.	0.0	S.S.E.	0.0	S.S.E.	$\begin{bmatrix} 0 \\ 0 \end{bmatrix}$
RY.	14 15	E. by N.	0.0	_	0.0	_	0.0		0.0		$0.0 \\ 0.0$	S.E. by E. S. by E.	0.
JANUARY.	16 17 18	N.W. W. by S.	1.0	N.W. W. by N.	$\frac{2.0}{2.0}$	N.W. W. by N.	2.0 5.0	N.W. by W. W. by N.	$\frac{1.5}{2.5}$	N.W. by W. N.W. by N.	1.5 3.5	N.W. by W. N.W.	1.
JA	19 20	S.W. by S.	0.0	s.s.w.	$0.0 \\ 0.2$	S. by W.	$0.0 \\ 0.0$	S. by W.	$0.2 \\ 0.0$	S. by W.	$0.2 \\ 0.0$	S. by W.	0.
	21 22	S.W. N.N.W.	$\frac{1.5}{0.2}$	S.W. N.N.W.	$\frac{1.5}{0.2}$	S.W. by W. N.N.W.	0.5	W.S.W.	0.0	W.Ś.W.	0.0	W. E.S.E.	0.
	23 24 25	E.N.E.	0.0	N.E.	0.0	E. by N.	0.0	E. by N.	0.0	E.	0.5	E.	0.
	26 27	E. by N.	0.0	E. by N.	$0.0 \\ 0.0$	E. by N.	0.0	E. by N.	0.0	E. by N.	0.0	E. by N.	0.
	28 29	W. by S.	$0.0 \\ 1.0$	W.S.W. N.W.	0.5	W.S.W. N.W.by N.	$\begin{array}{c} 0.3 \\ 0.2 \end{array}$	S.W. N.W. by N.	0.2	S.W. N.W.	$0.2 \\ 0.2$	S.S.W. N.W. by N.	0.
	$\begin{array}{c} 30 \\ 31 \end{array}$	E.	2.0	E.N.E.	0.2	E.	0.2	E. by S.	0.5	E. by S.	0.5	E. by S.	0.
(continu	ucd)	1	<del> </del>	1		1 246				İ		1	
Mean G Tin	öttingen }	12h.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Fore
	<u> </u>	Direction. N.N.W.	lbs. 2.5	N.N.W.	1bs. 2.0	N.N.W.	lbs. 1 0	N.N.W.	lbs. 1 0	N.N.W.	lbs. 1.0	N.N.W.	lbs.
	$\begin{pmatrix} 2\\3 \end{pmatrix}$	s.s.w.	0.5	s.w.	1.0	S.W. by W.		S.W. by W.	0.2	S.W.by W.	0.2	w.s.w.	0.
	5	N. by W. W. by N.	$\frac{5.2}{5}$	W. by S.	0.5 4.0	N. W. by N.	3.0	N. by E. N.W. by N.		N. by E. N.W. by N.	$0.5 \\ 2.5$	N.N.E. N.W. by N.	1.
	6 7 8	S.S.E. N.W. by W.	$0.0 \\ 0.2 \\ 0.0$	S.S.E. <b>N.N.</b> W.	$0.0 \\ 0.5 \\ 0.0$	S.S.E. N.	0.0	S.E. by S. N.	$0.0 \\ 1.5 \\ 0.2$	S. by E. N. by W.	$0.0 \\ 1.5 \\ 0.5$	S. by E. N. by W.	$\begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$
	9		0.0		0.0		0.0		0.5		0.0	N.	0.
	11 12	W.S.W.	0.0	W.S.W. E.S.E.	0.2	W.S.W. E.S.E.	$0.5 \\ 0.2 \\ 0.0$	W.S.W. E.S.E.	$0.2 \\ 0.2 \\ 0.0$	W.S.W. E.S.E.	0.2 0.0	W.S.W. E.S.E.	0.
ARY.	13 14 15	E. by N. N.W. by W.	0.0 0.2 1.2	E. by N. N.W. by W.	$0.0 \\ 0.5 \\ 0.0$	W.N.W.	0.0	W.N.W.	0.0	w.n.w.	0.0	w.n.w.	0.
JANUARY.	16	s.s.w.	$\frac{-}{0.2}$ $\frac{1.5}{1.5}$	S.W. by W.	0°2 1°5	S.W.by W. N.W.	$\frac{-}{0.2}$ 1.5	S. by W N.W.	0.2	S.W. N.W.	0.2 1.0	s.s.w. N.W.	0.
J	18 19 20	W.N.W. S.S.E. S.S.W.	$0.5 \\ 0.5$	N.W. S. —	$\begin{array}{c} 0.0 \\ 1.0 \\ \end{array}$	s.	1.0	S. by E.	1.0	S. by E.	0.0	S. S.W. by S.	0.
	21 22	N.W. by N. E. by N.	2.0 0.5	N.W. by N. E.N.E.		N.W. by N. E.N E.		N.W. N.E. by E.	1.2 0.3	N.W. N.E. by E.	$\begin{array}{c} 1.2 \\ 0.2 \end{array}$	N.W. N.E. by N.	0.
	23 24		0.0	_	0.0		0.0		0.0		$\frac{0.0}{0.0}$	<u> </u>	0.
	25 26 27		0.0		0.0		0.0		0.0	S.W. by S.	$0.0 \\ 0.0 \\ 0.2$	S.W. by S.	0.
	28 29	W.N.W.	0.0 0.5	W.N.W.	0.0	S. W.N.W.	0.5	W. by N.	0.0	W. by N. W.N.W.	$\frac{2.0}{0.5}$	W.N.W.	2: 0:
	30												

				DIRI	ECTION	AND FORC	E OF T	HE WIND.					
6 ^h .		7 ^h .		8h.		9 ^h .		10 ^h .		11h.			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	<u> </u>	lime.
_	0°0	s.s.w.	1bs. 0.2	s.s.w.	lbs. 0°2	s.s.w.	1bs. 0.2	w.s.w.	1bs. 0.2	w.s.w.	lbs. 0'2	1 2	1
S.W. by S. N.W. S.S.E. N.N.W. N.E.	0.5 2.0 0.5 0.2 0.2 0.0	S.S.W. N.W. by N. S.S.W. N.E.	0.5 2.0 0.5 0.0 0.2 0.0	S.S.W. N.N.W. S.W. by W. N.E. S.W.	0°0 0°2 0°2	S.S.W. N. by W. W.S.W. N.E. N.W.	0.2 0.2 0.5	S.S.W. N. by W. W. by N. N.E. N.W.	0.2 1.0 2.0 0.0 0.2 0.2	S.W. N. W. by N.	1 1	3 4 5 6 7 8	
S.S.E. S.E. by E. S.	0·2 2·0 0·0 0·2 0·2 0·2	N.N.W. S.W. N.E. S.S.E. S. by W.	0.2 0.0 0.2 0.0 0.2	N. by W. S.W. E. by N. S.S.E.	0.0 0.0 0.0	N. by W. S.W. by W. S.E. S.S.E.	0·2 1·0 0·2 0·2 0·2 0·0	N. by W. W.S.W. S.S.E. W. by N.	1	W.S.W.	0.0 0.2 0.0 0.0 0.0	10 11 12 13 14 15	JANUARY.
N.W. by N. N.W. S. by W. N.W. S.E. by S.	0.5 4.0 0.0 0.5 2.0 0.2	W.N.W. N.W. by N. S.E. by S. S. by W. W. by N. S.E.	0.2 4.0 0.2 0.2 2.5 0.5	W.N.W. S.E. by S. S. by W. N.N.W. S.E.	0.0 3.0 0.2 0.2 2.5 0.2	N.W. by W. N.W. S.S.E. S. by W. N.W. S.E.		S.S.W. W.N.W. S.S.E. S. by W. N.W. S.E.	0.2 3.0 0.2 0.2 0.2 3.0 0.2	S. by W. W.N.W. S.E. by S. N.W. E.S.E.	0·2 3·0 0·2 0·0 3·0 0·2	17 18 19 20 21 22 23	JANU
E. E.N.E. E.N.E. S.S.W. N.W. by N.	0°2 0°0 0°2 0°0 0°5 0°5	E. E.N.E. S.W. S.S.W. N.W. by <b>W</b> .	0.5 0.0 0.2 0.2 0.2 0.5	E.N.E. S.W. S.S.W. N.W.	0.5 0.0 0.5 0.5 0.5	E.N.E. S.W. by S. S.S.W. N.W.	0.0 0.0 0.2 0.2 0.2 0.2	E.N.E. S.W. by S. S. by W. N.W. by W.	0.2 0.0 0.2 0.2 0.2	S. by W.	0.0 0.0 0.0 0.0 0.2 0.2	24 25 26 27 28 29 30	
E. by S.	0.5	E.	0.5	E.	0.5	E.	0.5	S.W. by W.	1.0	w.s.w.	1.2	31 /	) 
18 ^h •		19 ^h .		20h.		21h.		22h.		23h.		Mean	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.		Direction.	Force.	Direction.	Force.		l'ime.
S.W. by W. W.S.W. W.N.W.	1bs. 0 ' 2 0 ' 2 0 ' 0 1 ' 0 0 ' 0 1 ' 0	W.S.W. W. N.W.	1bs. 0.2 0.2 0.0 1.0 0.0 0.5	S.W. by W. W. N.W. S.S.W.	0°2 0°0 1°5 0°0 0°5	S.W N.W S.S.W.	1bs.	S.W. by S. — N.W. S. by W.	0.0 0.0 0.2 0.0	N.N.W. N.W. S.S.W.	lbs.	1 2 3 4 5 6 7 8	
N. by W. N. W.S.W.	0.5 0.5 0.5 0.0 0.0 0.0	N. by W. N. W.S.W.	0.2 0.5 0.0 0.0 0.0	N. by W. N.	0.5 0.2 0.0 0.0 0.0 0.0	N. N. —	0.5 0.0 0.0 0.0 0.0	N. W. by S. S.E. by S.	0'0 0'2 0'2 0'2 0'0 0'0	N. N. W. by S. S.E. by S.	0.2 0.2 0.2 0.2 0.0 0.0	9 10 11 12 13 14 15	ARY.
— S.S.W. N.W. S.S.W. S.W. by W. N.W. by N.		S. by W. N.N.E. S.S.W. S.W. by W. N.W.	0.0 0.2 0.5 0.5	S.W. N.N.E. S.S.W. S.W. N.W.	0.0 0.5 0.2 0.2 1.0 0.5	W.S.W. N.N.E. S.W. by S. S.W.	0.0 0.5 0.2 0.2 1.5 0.2	W. by S. N.N.E. S.W. by S. S.W.	0.0 0.2 0.2 0.2 1.5 0.2	W. by S. N.N.E. S.W. by S. S.W.	0°0 0°5 0°2 0°2 1°5 0°2	16 17 18 19 20 21 22	JANUARY
E.S.E.  S.W. by S. W. by N.	0°2 0°0 0°0 0°2 1°0	E.S.E.  S.W. W. by N.	0.5 0.0 0.0 0.0 0.5 1.0	E.S.E.  S.W. W.	0°2 0°0 0°0 0°2 1°0	E.S.E.  W.S.W. W.	0.5 0.0 0.0 0.0 1.0	E.S.E.  W.S.W. W.	0.2 0.0 0.0 0.0 1.5 1.0	E.S.E. E. by N. W.S.W. W. by N.	0.2 0.0 0.2 0.0 1.5 0.5	23 24 25 26 27 28	
E. W.S.W.	1.2 0.2	E. by S. W.S.W.	1.0 0.2	E. S.W. by W.	1.0 0.2	E. S.W.	0.2 1.0	E. by N. S.W.	1.0	E. S.W. by S.	1.2 1.0	29 30 31	

		1		DIF	RECTION	N AND FOR	CE OF !	THE WIND.				·	
Mean Gö		Oh.		1h.		2h.		3h.		4h.		5 ^h .	
Tim	ie.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force
	$ \begin{bmatrix} 1\\2\\3\\4\\5 \end{bmatrix} $	S.W. by S. — W. by N.	1 to 0 to 0 to 0 to 0 to 0 to 0 to 0 to	S.W. by W.  E. by N. W. by N.	1 to 0 to 0 to 0 to 0 to 0 to 0 to 5	S.W. — E. W. by N.	1bs. 0.5 0.0 0.0 0.2 0.5	W.S.W. E. W. by N.	1bs. 0.2 0.0 0.0 0.0 0.2 0.5	W.S.W. E. E. by S. W. by N.	lbs, 0°2 0°2 0°0 0°2 0°5	W. by S. E. E.S.E. E.S.E. W.N.W.	1 bs. 1 6 0 2 0 2 0 2 0 3 0 3 0 3 0 3 0 3 0 3 0 3
· .	6 7 8 9 10 11 12	N.W. by N. N.E. by E. W.N.W. N. by W. N. by E. N.E. by N.	2.0 0.2 0.2 2.0 0.5 0.5	N.W. N.E. by E. W.N.W. N. by W. N.N.E. N.N.E.	2.0 0.2 0.2 1.5 0.2 0.2	N.W. by N. N.E. by E. W.S.W. N. by W. N. by E. N. by E.	2·0 0·2 0·2 2·0 0·2 0·2	N.W. by N. N.E. by E. S.W. N.N.W. N.	2·0 0·2 0·5 2·5 0·5 0·2	N.W. E.N.E. S.W. N.N.W. N.	2·5 0·2 1·5 2·0 0·2 0·2	N.W. by N. E. by N. S.S.W. N. by W. N.	2· 0· 2· 0· 0· 0·
FEBRUARY.	13 14 15 16 17 18 19	N. by W.  S.E. by E. S.E. by E.	0.0 0.5 0.0 0.0 0.0 0.5 0.5	N. by W. N. by W. S.E. by E. E. by S.	0.0 0.2 0.2 0.0 0.2 0.2	N. by W E. by S.	0.0 0.2 0.0 0.0 0.0 0.0 0.2	N. by W.	0.0 0.2 0.0 0.0 0.0 0.0	N.E. N. by W. — — E. by S.	0.2 0.5 0.0 0.0 0.0 0.0	N. by W. N. by W.	0. 0. 0. 0. 0.
	20 21 22 23 24 25 26	W.N.W.  N.W. by W.  N.E. by E.  S.E. by E.	1.5 0.0 0.2 1.5 0.2 0.2	W. N.W. N.E. S.E. by E.	1.5 0.0 0.0 0.5 0.2 0.2	W.N.W. W. W.N.W. N.E. S.E. by E.	1.5 0.0 0.2 0.5 0.2 0.2	W. by N.  W.S.W. N.W. E. S.E. by E.	1:0 0:0 0:2 1:0 0:2 0:2	N.W. by W. S.S.E. W. N.W. E. by S. S.W. by S.	1.5 0.2 0.5 1.5 0.2 0.2	N.W. E.S.E. W. N.W. S.E. S.W.	0. 0. 1. 0.
	27 28 29	S. by E. N.W.	0.2	S.S.E. N.W. by W.	0.2	S.S.E. N. by W.	1.0	S. by E. N.N.W.	1.2 0.2	S. by E. N. by W.	2:0	S.S.E. N.W. by W.	0.
(continu	ſ	12հ.		13h.		14 ^h .		15h.		16 ^h .		17h.	
lean Gö Tim		Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Forc
FEBRUARY.	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	W.N.W. E.  W.N.W.  W.S.W. N.  E.N.E.  E.N.E.  E.N.E.  W. by N.  N.  W. by S.	lbs.   0.5   0.2   0.0   0.0   0.5   0.0   0.0   0.5   0.0   0.0   0.5   0.0   0.5   0.0   0.5   1.5   1.5   0.0   0.2   1.5   1.5   0.0   0.2   0.5   0.0   0.5   0.0   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5   0.5	W.N.W. E.  W.N.W.  W. by S. N. by E.  L.  E.N.E.  E.N.E.  W.N.W.  N.  W. by S.  W.S.W.	lbs.   0°2   0°0   0°0   0°5   0°0   0°5   0°0   0°0   0°5   1°5   1°5   0°0   0°2   1°5   1°5   0°0   0°2   1°5   1°5   0°0   0°2   1°5   1°5   0°0   0°2   1°5   1°5   0°0   0°2   1°5   1°5   0°0   0°2   1°5   1°5   0°0   0°2   1°5   1°5   0°0   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°2   0°3   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4   0°4	W.N.W. W.N.W.  N.W. by N. N. by E.  N. by W.  E. by N.  N.E. W.N.W. N.  N.W. by W.	1bs, 0'0 0'0 0'0 0'2 1'5 - 0'0 0'5 0'5 0'0 0'0 0'0 0'0 0'0 0'0 0'0	E.  W.N.W. W. by N.  N.W. N. by E. N.N.E.  N. by W.  E.  N. by W.  W.  W.  W.  W.  W.  W.  W.  W.  W.	lbs. 0.0 0.2 0.0 0.5 1.5 0.0 0.0	W.N.W. W.N.W. N. by E. N.W. by W. N. by E. N.N.E.  E. S.W. by S. W.N.W. N.N.W. N.W.	lbs.  0'0 0'0 0'0 0'2 1'0	E. by N.  W. W.N.W.  N. by E.  N.W. by W.  N. by E.  W.N.E.  E.  W.N.W.  N.N.W.  N.W. by W.	1bs. 0.0 0.0 0.0 1.0 0.0 0.0 0.0

				DIRE	CTION	AND FORCE	OF TH	IE WIND.					
6 ^h .		7 ^h .		8h.		9 ^h .		10 ^h .	***	11 ^h .		Mean	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		l'ime.
W E. by S. W.N.W.	lbs. 1.0 0.0 0.0 0.2 0.5	W.S.W. S.E. E. by S. W. by N.	lbs. 0.5 0.0 0.2 0.2 0.5	W. by S.  E. by S.  N.W.	lbs. 0.5 0.0 0.0 0.0 0.2 1.0	W. E. S.S.W. E. W. by N.	lbs. 0°2 0°2 0°2 0°2 1°0	W. — E. N.W.	lbs.  1 ° 0 0 ° 0 0 ° 0 0 ° 2 1 ° 0	W.N.W. E. E. W.N.W.	lbs. 0.5 0.2 0.0 0.2 1.5	1 2 3 4 5	
N.W. E. S.S.W. N. by W. N. by W.	3.0 0.2 2.0 1.5 0.2 0.2	N.W. E. by S. S.W. by S. N. N.W. by N.	2·5 0·5 2·0 1·5 0·2 0·0	N.N.W. E. by N. S.S.W. N. E.N.E.	2·0 0·2 2·5 1·5 0·2 0·0	N. E.S.E. S.S.W. N. N.E. by E. S.S.E.	1.0 0.2 3.0 1.5 0.2 0.2	N.N.W. S.W. by W. N. by E. N.N.E. S.S.E.	0.5 0.0 2.0 1.0 0.2 0.2	N. by W. W.S.W. N. by E. S.S.E.		6 7 8 9 10 11 12 13	RY.
N. by W. N.N.W. E.S.E.	0.2 0.5 0.0 0.2 0.0 0.2	N.E. N.N.W. S.E. by S. S.E. by E.	0·2 0·2 0·2 0·2 0·0 0·2	N.E. S.S.W. S.E. by S. S.E. by E.	0.2 0.2 0.2 0.0 0.0	N.E. by N. S.W. by S. S.E. by S. S.E. by E. E.S.E. E. by N.	0.5 0.2 0.2 0.2 0.2 0.5	N. by E. S.W. S.E. by E. E.N.E.	0.5 0.2 0.0 0.2 0.0 0.5	N. by W. S.W. — — — E.N.E.	0.2 0.2 0.0 0.0 0.0 0.0	13 14 15 16 17 18 19 20	FEBRUARY.
W.N.W. E.S.E. W. by N. N.W. S.E. S.W.	1.5 0.2 1.5 1.0 0.2 0.5	W.N.W. E. by S. W.S.W. N.W. S.E. by S. S.S.W.	1.0 0.2 3.0 1.5 0.2 0.5	W.N.W. E. by S. W. N.N.W. S. by E. S.S.W.	1.0 0.2 3.0 1.0 0.2 0.5	W. E. W. by N. N.N.W. S. by E. S.W. by W.	0.5 0.2 2.0 1.0 0.2 0.2	W. E.N.E. W. N.N.W. S.S.E. W. by N.	0.5 0.2 2.0 1.0 0.2 0.2	E. by N. W. by N. N.N.E. W. by S.	0.0 0.2 2.0 1.0 0.0 0.5	21 22 23 24 25 26 27	
S.S.E. N.W.	1.0	S.S.E. N.W. by N.	0°2 2°5	S.W. by W. N.W. by N.	0.5 2.2	W.S.W. N.N.W.	0.5	W.S.W. N.W. by N.	0.5 2.2	W. by N. N.N.W.	0.5	28 29	
18h.		19 ^h .		20h.		21 ^h .		22 ^h .		23h.			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		l'ime.
E. by N.  W.  N.W. by N.  N.E.  N.W.by W.  N.N.E.  W. by N.  N.N.E.  N.W. by W.  N.N.E.  N.W. by W.  N.N.E.	lbs.   0.0   0.2   0.0   0.2   1.0   0.0   0.0   0.0   0.0   0.0   0.0   0.5   0.0   0.5   0.0   0.0   0.5   0.0   0.0   0.5   0.0   0.0   0.5   0.0   0.0   0.5   0.0   0.0   0.5   0.0   0.5   0.0   0.0   0.5   0.0   0.5   0.0   0.0   0.5   0.0   0.0   0.5   0.0   0.5   0.0   0.0   0.5   0.0   0.0   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	E. by N.  W.  N.W. by N.  N. by E.  W. by N.  N. by E.  N. by E.  N. by E.  N. W. by W.  N. by E.  N. W. by W.  N. by E.  N. W. by W.	lbs.  0.0 0.2 0.0 0.2 1.5 0.5 0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	W	lbs.	N. E. by N. W. by S. N.W. by N. N.E. N. by E. N. by E. N. by E. N. by E. E.S.E. W.N.W. N. by W. N.E. S.E. by S. N.N.W. W.N.W.	0.0	N. by E. E. by N. — W. by S. — N. by W. N.E. E.S.E. N.W. by W. N. by E. N. by E. — — — — — — — — — — — — — — — — — —	lbs.  0'2 0'0 0'2 0'0 0'2 1'5 0'2 2'0 0'5 0'5 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0	N. by E.  W. by S.  N.N.W. N.E. by E. W.N.W. N. by E. N.N.E.  N. by W.  S.E. by E.  W.N.W.  N.W. by W.  S.E. by E.  W.N.W.  N.W. by W.  N.W. by W.  N.W. by W.  N.W. by E.	lbs. 0'2 0'0 0'5	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	FEBRUARY.

				DI	RECTIO	N AND FOR	CE OF	THE WIND				1	
Mean Gö		0h.		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
Time	e.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force
	1 2 3 4	N. by E. N.N.W. N.N.E. W. by S.	lbs. 0°2 0°2 0°2 1°0	N. by E. N.N.W. N. W.	lbs. 0°2 0°2 0°2 0°5	N.N.W. N. by E. N. W. by S.	1bs. 0°2 0°2 0°2 0°2	N.N.W. N.E. N. W.S.W.	lbs. 0°2 0°2 0°2 0°2	N.N.W. N.E. N. by W. S.W. by W.	1bs. 0°2 0°2 0°2 0°2	N. by W. N.E. S.W. by S.	1 lbs. 0 : 2 0 : 2 0 : 1 : 0
	5 6 7 8 9 10 11	W. by S. N. S. N. by W. N.	2.0 0.2 0.2 1.0 0.5 0.0	W. by S. S. N.W. N.	0.5 0.0 0.2 0.5 0.2 0.0	S.W. by S. N.N.W. N.	0.2 0.2 0.2 0.0	W. by S. S.W. by S. N. N.N.W.	1.0 0.0 0.2 0.5 0.2 0.0	W. by S. E.S.E. S.S.W. N. by W. N.N.W.	1.5 0.2 0.2 0.5 0.5 0.0	W.S.W. S.S.E. S.S.W. N. by W. N.N.W.	0. 0. 1. 0.
MARCH.	12 13 14 15 16 17 18	W.N.W. N.W. by W. N.W. by N. E.S.E. N.N.E.	1.5 0.2	W. by N. N.W. N.N.W. — E.	1:0 0:5 0:2 0:0 1:5 0:0	W.N.W. N.N.W. N. by W. ————————————————————————————————————	1.5 0.5 0.2 0.0 2.0 0.2	W.N.W. N.N.W. N. by W. S.W. by S. E. by N. E.	2.0 0.5 0.5 0.2 1.5 0.2	W.N.W. W. by N. N.W. by N. S.W. by S. E.N.E. E.	2:0 1:0 1:0 0:5 1:5 0:2	W.N.W. W. by N. N.W. by W. S.S.W. E.N.E. S.E. by E.	2: 1: 0: 1: 0:
	19 20 21 22 23 24 25	N.W. N.N.W. N. by E. N. by W. E. by N.	0'0 0'5 0'2 0'2 0'2 0'2	N.W. N. N. by E. N.N.E. E. by N.	0.0 0.5 0.2 0.2 0.2 0.2	N.N.W. N. N.N.E. N.N.E. E. by N.	0.0 0.5 0.2 0.2 0.2 0.2	E.N.E. N.N.W. N. by E. N. by E. N.E. by E. E. by N.	0.2 0.5 0.2 0.2 0.2 0.2	E.N.E. N.W. E. by S. N. by E. S.E. by E. E. by N.	0.5 1.0 0.2 0.2 0.2 0.2	E.N.E. N.W. by W. N.E. by N. N.N.E. S.E. E.	0. 0. 0. 0.
,	26 27 28 29 30 31	N.N.E.	0.5 0.0 0.0 0.2 0.0	N. by E. S.E. by E.	0.0 0.0 0.0 0.2 0.0	<u> </u>	0.0 0.0 0.0 0.2 0.0		0.0 0.0 0.0 0.0	E.S.E. S.S.W. E. by S.	0.0 0.2 0.2 0.5 0.0	N. by W. S. by W. N.E. by E. S.E. by S.	0 0 0 0
(continu	ued)	11		ı		1		I		1		1	
Mean G		12h.		13 ^h .	1	14 ^h .		15h.		16 ^h .	1	17 ^h .	
Tim	ie.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	For
	$\begin{pmatrix} 1\\2\\3\\4 \end{pmatrix}$	N.W. N.E. by N. N.W. by W. S.W. by W.		W.N.W. N.E. by N. N.W. by W. W.S.W.	1 bs. 1 0 0 5 2 5 1 5	N.W. N.E. W.N.W. W.S.W.	1.0 1.2 1.0	N.W. by W. N.E. by N. W.N.W. W.S.W.	1.0 1.5 0.5	W. N.E. W. by N. W.S.W.	1 bs. 0 2 0 5 1 0 1 0	W. N.N.E. W. W.S.W.	1 lbs 0 1 0 1
	5 6 7 8 9 10 11	W.N.W. S.W. N.W. by N. N.	0.2 0.2 0.2 0.2 0.2 0.0	S.W. by W. N. N.N.W.	0.0 0.0 0.2 0.2 0.2	S.W. N.N.E. N.N.W.	0.0 0.0 0.2 0.2 0.2 0.2	S.W. by S. N. by E. N.N.W.	0.0 0.0 0.2 0.2 0.2 0.0	S.W. S.W. N.E. N.W. by N.	0.0	S.W. N.E. N.W. by N.	0 0 0 0
MARCH.	12 13 14 15 16 17 18	W. by N. N.N.W. N. by W. S.	1.5 2.5 1.0 0.5 0.0	N. W. by W. N. by W. N. by W. S. by E.	1'0 2'0 1'0 0'5 0'0 0'0	W.N.W. N.N.W. N.N.W. S.S.E.	1.0 2.0 1.0 0.5 0.0 0.0	N.W. by W. N.N.W. N.N.W. S.S.E. N.E. by N.	1.5 0.5 0.2	N.W. N.N.W. N.N.W. E.S.E. N.E. by N.	1'0 1'0 0'2 0'2 0'2 0'0	N.W. N.N.W. N.W. by N. E.S.E.	0 0
	19 20 21 22 23 24 25	E. by N. N. S. E. E. by N.	0.5 0.5 0.0 0.2 0.2	E. by N. N. E.N.E.	0.5 0.5 0.0 0.0 0.0 0.0	E. by N.  N.  E. by N.	0.0	S.S.E. N. by W. N.W. by W. E. by S.	0'2 0'2 0'0 0'2 0'2 0'0	E.	0.0 0.0 0.0 0.0 0.0	w.s.w.	0 0 0 0 0
	26 27 28 29 30 31	W.N.W. E. by N. S.W. by S.	0.0 0.0 0.2 0.2 0.2	N. by E. E. S.W. by S.	0.0 0.0 0.2 0.2 0.2	N. by E. E. by S. S.S.W.	0.0 0.0 0.2 0.2 0.5	N. S.W.	0.0 0.0 0.0 0.0	N. by W.	0.0 0.0 0.2 0.0 1.2	N.W. by W.	0 0 0 3

				DIKE	CTION	AND FORCE	S OF T	1		T		1)	
6 ^h .		7 ^h .	1	8h.		9h.	<del></del>	10h.	1	11 ^h .			Göttinge ime.
Direction. N.W. by N. E.N.E. W.S.W. S.W.	Ibs. 0°2 0°2 0°2 1°5	W. E.N.E. S.W. by W. S.W.	Ibs. 0°2 0°2 0°2 1°5	W. E.S.E. W.S.W. S.W.	lbs. 1.0 0.5 0.2 1.5	W. E. by N. W. S.W.	lbs. 1'0 0'5 1'5 2'0	W. E. by N. W. S.W.	1bs. 1 0 0 5 1 0 2 0	N.W. E. by N. W.N.W. S.W.	lbs. 1 0 1 0 2 0 2 5	1 7 2 3 4	
W.S.W. S.E. by S. S.S.W. N. N.N.W. S. by W.	1.0 0.2 1.0 0.5 0.5	W. by S. S.E. S.W. N. by E. N.W. S. by E.	1.0 0.2 1.0 0.2 0.5 0.5	W. S. S.W. N.E. by N. N.W.by N. S. by E.	1.5 0.2 0.5 0.2 0.5 0.2	W.N.W. S.S.W. S.W. by W. N.E. by E. N.N.W. S.S.E.	1:0 0:2 1:0 0:2 0:5 0:5	N.W. by W. S.S.W. N.W. N. N. S.E. by E.	1.0 0.2 3.0 0.2 0.5 0.2	W.N.W. S.S.W. N.W. by N. N. S.E.	0.5 0.2 2.0 0.2 0.5 0.5	5 6 7 8 9 10 11 12	
W.N.W. W.N.W. N.N.W. S.S.W. E.N.E. S.E. by E.	2.0 1.0 1.5 0.5 1.5 0.2	W. by N. N.N.W. N.N.W. S. by W. E.S.E.	2.0 1.5 2.0 0.5 1.0 0.0	W. by N. N.W. N.N.W. S. by E. E. by S.	2.0 2.0 2.0 0.5 0.5	N.N.W. N.N.W. N.N.W. S. by E. E. by S. E. by S.	1.5 2.0 2.5 1.0 0.5 0.2	W.N.W. N. by E. N. by W. S.S.E. E. by S.	1.5 2.0 2.0 0.5 0.2 0.0	W.N.W. N.W. by N. N. by W. S.S.E. E.N.E.	2.0 2.5 1.5 0.5 0.2 0.0	13 14 15 16 17 18	MARCH.
E.N.E. (.W. by W. S.E. by E. S.S.W. S.E. by E. E. by N.	0.2 0.5 0.2 0.2 0.2 0.2 0.5	E.N.E. N.W. E.S.E. E. S.E. by E. E.N.E.	0.5 1.0 0.2 0.5 0.2 0.5	E.N.E. N.W. S.E. by S. S.S.E. S.E. E. by N.	1.0 1.5 0.2 0.5 0.2 0.5	E.N.E. W.N.W. S. by W. S.E. E.N.E.	1.5 1.5 0.0 0.2 0.2 0.5	E.N.E. N.W. S. S.E. E. by N.	2.0 1.0 0.0 0.2 0.2 0.2	E.N.E. N. by W. S. E.S.E. E. by N.	1.0 0.5 0.0 0.2 0.2 0.2	20 21 22 23 24 25 26	
S.W. S.E. by S. S.S.W. E. by N. S.W. by S.	0°2 0°2 0°2 0°2 0°2	N.N.W. E.S.E. S.S.W. E. by N. S.W.	0.2 0.2 0.2 0.2 0.2 1.5	S.S.E. S.E. by E. W. by S. E. by N. W.S.W.	0.2 0.2 0.5 0.2 1.5	S.S.E. E. S.W. by W. E. W.	0°2 0°2 0°2 0°2 1°0	S.E. by S. S.E. W. by N. E. W.	0°2 0°2 0°3 0°5 0°2	S.E. by E. W. by N. E. W.S.W.	0'2 0'0 0'2 0'5 0'2	27 28 29 30 31	
18h.		19 ^h .		20 ^h .		21 ^h .		22 ^h .		23h.		Mean (	Götting
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	<u> </u>	
N.E. W. W. W. by S.	lbs. 0.0 1.0 0.5 - 2.0	N.E. W. by S. S.W.	1bs. 0°0 0°2 0°2 — 1°5	N.E. W. by S. S.W. by W.	1bs. 0°0 0°2 0°2 — 1°0	N.E. by N. W.S.W. W.S.W.	1bs. 0.0 0.2 0.2 - 0.5	N.E. by N. W.S.W. W.S.W.	lbs. — 0.5 0.5 — 0.5	N.E. W.S.W. W. by S.	1bs. 0°0 0°2 0°5 — 1°5 0°0	1 \ 2 \ 3 \ 4 \ 5 \ 6	
 .W. by W. N.E. N.W. by N.	0.0 0.0 0.2 0.2 0.2	S.S.W. N.N.W. N.E.	0.0 0.2 1.0 0.5 0.0	S.S.W. N. by W. N. by E.	0.0 0.5 1.0 0.5 0.0	N.N.W. S.S.E. N. by W. N. by E.	0.2 0.2 1.0 0.5 0.0	S. by W. N. by W. N. by E.	0.0 0.2 1.0 0.5 0.0	S. N. by W. N. by W.	0.5 1.0 0.5 0.0	7 8 9 10 11	
W.N.W. N.W. N.N.W. I.W. by N. E. by S. N.N.E.	1.5 0.2 0.2	W.N.W. N.W. by W. N.N.W.  E. by S. N.N.E.	1.0 0.2 0.0 0.2 0.0 0.2	W.N.W. N.W. N.N.W. E. by S. N.N.E.	1'0 0'2 0'2 0'0 0'2 0'2	W.N.W. N.W. by W. N.N.W. E. by S. N.N.E.	0.5 0.0 0.5 0.5	W.N.W. N.W. by W. N.N.W. E. by S. N.N.E.	0.2 0.0 0.5 0.2	W. by N. N.W. by W. N.N.W.  E.S.E. N.N.E.	0.5 0.5 0.2 0.0 1.5 0.2	12 13 14 15 16 17	MARCH.
.W. by W.	0.0 0.2 0.0 0.0 0.0 0.0	W	0.0 0.2 0.0 0.0 0.0 0.0		0.0 0.0 0.0 0.0 0.0 0.0 0.0	W. — — — E.	0.0 0.2 0.0 0.0 0.0 0.0	W. by N. — — — E.	0.0 0.2	N.W. N.N.W. N. by E. N. by W. E. by N.	0.0 0.5 0.2 0.2 1.2 0.2	19 20 21 22 23 24	
N	0.5 0.0 0.0 0.0 0.0 2.0	N. — — — — — — — — — — — — — — — — — — —	0.2 0.0 0.0 0.0 0.0 1.0	N. — — — — — — W.N.W.	0.2 0.0 0.0 0.0 0.0 0.0	N. — — — — — — — W.N.W.	0.2 0.0 0.0 0.0 0.0	N	0.2 0.0 0.0 0.0 0.0	N	1.0 0.0 0.0 0.0 0.0	25 26 27 28 29 30 31	

				D	IRECTI	ON AND FO	RCE OF	THE WINI	).				
Mean Gö	ttingen	O ^h .		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
Time		Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1 \\ 2 \end{pmatrix}$	W.N.W.	lbs. 2°0	W.N.W.	lbs. 2 0	w.n.w.	lbs. 1.5	W.N.W.	lbs. 2.5	W.N.W.	lbs. 3 ° 0	W.N.W.	lbs. 3°0
	2 3 4 5 6 7 8	S.W. by S. — N. —	0.0 0.5 0.0 0.0 0.0 0.0	S.W. by S. N. N. N.	0.0 0.2 0.2 0.0 0.2 0.0	E. by S. S.S.W. N. by W.	0·2 0·2 0·2 0·0 0·2 0·0	E. by S. S.W. by S. N.W. N.N.E. S.W. by S.	0.2 0.2 0.2 0.0 0.2 0.2 0.2	E.S.E. S.W. N. S. N. S.W. by S.	0.2 0.5 0.2 0.2 0.2 0.2	E.S.E. S.W. N.E. by N. N. by W. S.W. by S.	0.2 0.2 1.2 0.0 0.2 0.2
šIL.	9 10 11 12 13 14 15	E. by N. W. by N. N.W. by N. N. by W.	0.0 0.2 0.0 1.5 0.5 0.5	E. W. N.W. by N. N. by W.	0°0 0°2 0°0 1°5 0°5	E. by N. W. N.N.W.	0.0 0.2 0.0 1.5 0.5 0.5	W. E. by S. S.S.W. W.S.W. N.W. by N.	0°2 0°2 0°2 1°5 0°5 0°2	S.W. by S. E. by S. S.S.W. W.S.W. N.	0.2 0.2 0.2 1.5 0.5	S.W. E. by S. S. W.S.W. N.E. by N. N.W. by N.	0.5 0.5 0.5 0.5 0.5
APRIL.	16 17 18 19 20 21 a 22	E. N. by E.  N.N.W.	0.0 2.2 0.0 - 1.0	N. E. N.N.E. — W.	0.5 2.5 0.5 0.0 	N.N.W. E. N.N.E. — N.W.	0.5 0.0 0.0 0.0	N. E. by N. N. by E.  N. N. N. W.	0.5 2.0 0.2 0.0 0.5	N.W. by W. E. by N. N. by E. S. N.W.	0.5 2.0 0.2 0.5 0.2	N. E.N.E. N.N.E. S.	0°2 1°3 0°2 0°2 -
	23 24 25 26 27 28 29 30	W.N.W.	0.0 0.0 0.0 0.0 -	W. by N.	1.0 0.0 0.0 0.0 0.0 2.0	W. by N. N.W. by N. W.N.W.	1:0 0:0 0:2 0:0 0:0 2:5	W.N.W. S. by W. N.W. — W.N.W.	1:0 0:2 0:2 0:0 0:0	W.N.W. S. by W. W. by S.  W.N.W.	1.0 0.5 0.2 0.0 0.0 3.0	W.N.W. S. by E. S. by E. S. by E. N.W. by W.	1.0 0.5 0.5 0.5 0.0 3.0
(continu	ued)		<u> </u>										
Mean Gö	ottingen	12h.		13 ^h •		14 ^h .		15 ^h .		16 ^h .		17 ^h .	
Tim		Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force
APRIL.	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 a 22 23 24 25 26 27 28 29 30	W.N.W.  N.N.W.  N. by W.  S.W.  S.W.  W.N.W.  N. by E.  S.W.  S.W.  W.N.W.  L. by E.  S.W.  S.W.  W.N.W.  L. by N.  S.S.E.  N.W.by W.	lbs.   0.5	N.W.  N.N.W.  N. by W.  S.W.  N.W. by N.  N.E.  S.W.  N.W. by W.  S.S.W.  S. S.E.  N.W. by W.	0°2 0°2 0°3	N.W.  N.N.W.  N. by W.  N. by W.  N.E.  S.W.  N. by W.  N.E.  S.W.  N.W. by W.  N.W. by W.	lbs.   O'2   O'0   O'5   O'0   O'1   O'1   O'2   O'2   O'2   O'2   O'2   O'2   O'2   O'2   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'5   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0   O'0	N. by W.  N. by W.  N. by W.  N.N.E.  N.W. by N.  N. by W.  N.E. by E.  N. by W.  S. by W.  S. by W.  S. by W.  N.W. by W.	0.5 0.0 0.5	N. by W.  N. by W.  N. by W.  N. by W.  N. by N.  N. by W.  E.N.E.  N. by W.  S.W. by W.  E. by N.  N.W.	lbs. 0'0  0'0 0'5 0'0 0'2 0'0 0'5 0'2 0'5 0'0 1'0 0'0 0'0 0'2 0'0 0'2 0'0 0'2 0'0 0'2	N. by W.  N. by W.  N. by W.  N. by W.  N. N.W.  S.E. by S.  N.W. by N.  N.N.W.  W. by N.  W. by N.  E. by N.  E. by N.	lbs.   O * O * O * O * O * O * O * O * O * O

^{*} Good Friday.

				DIRI	ECTION	AND FORC	E OF T	HE WIND.					
6 ^h .		7 ^h .		8 ^h .		9 ^h .		10 ^h .		11 ^h .			Göttingen Sime.
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		
W.N.W.	lbs. 2°0	W.N.W.	lbs. 2.0	W.N.W.	lbs. 1.5	W.N.W.	lbs. 1'0	N.W.	0.2	W.N.W.	lbs. 0.5	$\begin{vmatrix} 1 \\ 2 \end{vmatrix}$	)
E.S.E. S.W. S.S.W. S. S.S.W. S.S.W.	0.2 0.2 0.2 0.2 0.5 0.5	E. S.W. by W. S.S.W. S.S.W. S. by W. S.S.W.	0.2 0.2 0.2 0.5 0.5 0.5	E. by N. S.S.W. S.S.W. S. by W. S.S.W.	0.2 0.0 0.2 0.5 0.5 0.5	E.N.E. N.N W. S.S.W. S.S.W. S. by W.	0.2 0.2 0.2 0.2 0.5 0.5	N. by E. N.N.W. S.W. by S. S.S.W. S.S.W.	0.2 0.2 0.5 0.2 0.2 0.2	N.N.W. S. by W. N. by W. S.S.W. S.S.W.	0.0 0.2 0.5 0.5 0.2 0.2	3 4 5 6 7 8 9	
S.W. E. by S. S.S.E. W. by S. N.E. by N.	0.2 0.2 0.2 1.0 0.5 0.5	S.S.W. E. by S. S. W.N.W. S.S.E. N.W. by W.	0.2 0.5 0.2 2.0 0.2 0.2 0.5	S.S.W. E. by S. S. by E. W.N.W. S.S.W.	0.5 0.5 0.5 0.5 1.0	S.S.W. E by N. S.W. by S. W. by N. S.W. N. by W.	0·2 0·2 0·2 2·5 0·2 1·0	S.W. E S.W. by S. W. by N. S.W. by S. N.	1.0	S.W. by S. W. by N. S.S.W. N. by W.	0.2 0.0 0.2 1.5 0.2 1.5	10 11 12 13 14 15 16	APRIL.
N. by E. S. by E.	0.2 1.5 0.0 0.2	S. N.E. by N. S.W. by S. S.S.E.	0.2 2.5 0.2 0.2	S.S.E. N.E. S. by W. S.S.E.	0°2 2°0 0°2 0°2	S.S.E. N.E. S.W. by S. S.	0.2 1.5 0.2 1.5	S. N.E. by E. S.S.W. S.S.W.	0.2 0.5 0.2 2.5	N.E. by E. S.S.W. S.W. by S.	0.0 0.2 1.0	17 18 19 20 a 21	API
N.W. W.N.W. S.E. S. S. by E. N.W. by W.	0.2 1.0 0.2 1.0 0.2 0.0 2.5	S. by W.  W. S.E. by E. S. S.S.E. N.W.	0·2 	S. by W.  W. S.E. by E. S. by W. S.S.E. N.E. N.W.	0.5 	S.S.W.  W. E.S.E. S.S.E. S.E. by S.  N.W.	0.5 	S.S.W.  W.N.W. E.S.E. S.S.E. S.E. N.W.	0.5 	S W. by N E.S.E S.S.E W.N.W	0.2 	22 23 24 25 26 27 28 29 30	
					1		<u> </u>				1		
18 ^h .		19 ^h .		20h.		21 ^h .		22 ^h .		23h.			Göttingen 'ime.
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	<u> </u>	
E. by N. S. by E. N.N.W.  N. by W.  N. N. E.  N.N.E.  N.N.E.  N.N.E.  W.  W. by N.  W. by N.	Tbs.	E. by N. N.N.W. N. by W. N. by W. N.N.W. N. by W. N.N.W. N. by W. N.N.E. N. by W. N.N.E. N.N.E.	lbs.	E. by N.  N.N.W.  N. by W.  N.N.W.  N.W. by N.  N. by W.  E.  N.N.E.  W.N.W.  N.W. by N.  N.W. by N.  E. by N.	lbs.	E.N.E.  W.N.W.  W.N.W.  N. by E.  W.N.W.  W.N.W.  E. by N.	lbs.	E.N.E.	lbs.	S. by E.  N.  W. by N.  N.N.W.  N.N.W.  E.  N.N.W.  W.N.W.  E.  N.N.W.	lbs. — 0'0 0'2 0'0 0'2 0'0 0'0 0'0 0'0 0'0 1'5 0'2 0'5 — 0'0 2'5 0'5 0'0 — 1'0 — 1'5 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 20 21 22 23 24 25 26 27 28 29 30	APRIL.

				D	IRECTI	ON AND FO	RCE OF	THE WIND	).				
Mean Gö	ttingen	O ^h .		1 ^h .		2 ^h .		3 ^h .		4 ^h .		5 ^h .	
Time		Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$ \begin{pmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{pmatrix} $	E.N.E.	lbs. 0°2 0°0 0°0 0°0 0°0	E. by N.	lbs. 0'2 0'0 0'0 0'0 0'0 0'0	s.s.w.	lbs. 0.0 0.0 0.2 0.0 0.0 0.0	S.S.W. E.N.E. S.W. by S.	lbs. 0°0 0°0 0°2 0°2 0°2 0°0	N.E. S.S.W. E.N.E. S.S.W. S.S.W.	lbs. 0°0 0°2 0°2 0°2 0°2 0°2	E. by S. S.E. S.W. E. by N. S. by W. S. by W.	lbs. 0°2 0°2 0°2 0°2 0°5 0°2
	7 8 9 10 11 12 13	N. by E. N. by W.	0.0 0.0 0.0 0.2 0.5 0.0	N. by W. N. by W.	0.0 0.0 0.0 0.2 0.5 0.0	S.W. by W.  N. N. by E. S. by W.	0.0 0.2 0.0 0.2 0.5 0.5	S. by W. S.W. by S. N. by W. N. by W. N.N.W. E. by S.	0.2 0.2 0.2 1.5 0.5 0.2	S.S.W. S. by W. N. N. by E. N.W. by N. S.E.	0.2 0.2 0.2 1.5 0.5	S.S.W. S. N. N. by E. N.N.E. S.E. by S.	0.5 0.5 1.0
MAY.	14 15 16 17 18 19 20	N.  	0.0 0.0 0.0 0.0 0.0		0.0 0.0 0.0 0.0 0.0 0.0	w.s.w.	0.0 0.0 0.0 0.2 0.0 0.0	S.S.W. N.N.E. S. by W. S.S.W.	0.5 0.5 0.5 0.5 0.0 0.0	S.S.W. N.W. S. by E. S.S.W. S.E.	0°2 0°2 0°2 0°2 0°2	S. S.S.W. S. S.S.W. S.E. S.S.W.	0.2 0.2 0.2 0.2 0.2 0.2
	21 22 23 24 25 26 27	N. by E. E. — — —	0°2 0°2 0°0 0°0 0°0	N.N.E. E. by S. — —	0.0	N.N.E.  S.W. by S. N.W. by W.	0.2 0.0 0.0 0.2 0.2 0.2	E.S.E. S.W. N. by W.	0.0 0.5 0.5 0.5 0.0	S.S.E. S.E. by E. S.W. by W. N.W. by N.	0.2 0.5 0.0 0.2 0.2 0.0	S.S.E. E. S.W. by S. S.W. by S. W. by N. S.S.E.	0.2 0.2 0.2 0.2 0.2 0.2
	28 29 30 31	 N.N.W.	0.0 0.0 0.0	N.N.W.	0.0 0.0 1.2	N. by W.	0.0 0.5 1.0	N.N.W. N. by W.	0.0 0.2 1.2	N.N.W. N. by W.	0.0 1.0 1.2	N.N.W. N.	0.0 1.0 1.2
(continue	ed)				***			1 -1		16 ^h .		17 ^h .	
Mean Gör Time		12 ^h .	72	13h.	T2	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$   \begin{pmatrix}     1 \\     2 \\     3 \\     4 \\     5 \\     6 \\     7 \\     8 \\     9 \\     10 \\     11 \\     12 \\     13 \\   \end{pmatrix} $	E.N.E. S. by W. E. S.S.W. N. by W. N.W. by N. N.N.W.	Force.    lbs.   0 0   0 0 0   0 0 0   0 0 0   0 0 0 0   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	E.N.E. S.S.W. N. by W.  N.E. N. N. N.W. N. by W. N.N.W.	Force.   lbs.   0.0   0.0   0.0   0.2   1.0   0.2   -0.0   0.2   0.2   0.2   0.2   0.2   2.0	E.   N.W.   N. by E.   N. by E.   N. by W.   N. by W.   N. N. W.   N. N. W.   N. N. W.	lbs.   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	E. N. N. N. N. N. N. N. N. N. N. N. N. N.	lbs. 0 0 0 0 0 0 0 2 1 5 5 0 2 2 0 0 0 2 2 0	E.N.E. S. by E. N. by W. N. by W. N.N.W.	lbs. 0'0 0'0 0'0 0'2 1'0 0'2 	S. by E. E. by N. S.S.E. N. by W.  N.E.  N. by E. N.N.W.	lbs. 0'0 0'0 0'2 0'2 0'5 0'2 0'2 0'0 0'5 0'2 0'0 2'0
MAY.	13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	S. by W. S. E. S.W. N.E. N. by E.  S.W. by W.	0.0 0.0 0.0 1.0 0.0 0.0 1.0 1.0 0.2 0.5 0.0 0.2	S.S.W. S.S.W. E. S.W. by W. N. by E. N. by W.		S.W. by S.  E. S.W. by W. N. by W. N. by W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.5 1.0 0.2 0.2 0.0 0.2 0.0 0.5	N.E. by N.  E. by S. S.E. by E.  E. S.S.W. N. by W. N.N.W.  W.N.W.	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	N.E. by N.   N.N.E. E. N. by W. N.N.W  W.N.W.	0.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.2 1.5 0.0 0.5 0.0 0.0 0.0	N.N.E.  N.N.E.  N.N.E.  E.  N. by W.  N. by W.	

1				·	DIR	ECTION	AND FORC	E OF T	HE WIND.				·	
1.	6h.		7h.		8h.		9 ^h .		10h.		11h.			Göttingen
	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		lime.
•	E. by S. S.S.E. S.S.W. E. by N. S. S. by E.	lbs. 0°2 0°2 0°2 0°2 0°5 0°5	E. by S. S. S.S.W. N.E. by E. S. by E. S. by E.	lbs.   0 · 2   0 · 2   0 · 2   0 · 2   0 · 5   0 · 2	S. by E. S. E. by N. S. S.E. by S.	lbs. 0'0 0'2 0'2 0'2 1'5 0'2	S. S.S.E. E.N.E. S.S.W. S.S.E.	1bs. 0'0 0'2 0'2 0'2 1'0 0'2	S. S. E.N.E. S. by W. E. by S.	1bs. 0.0 0.2 0.2 0.2 1.0 0.2	S.E. by E. E. by N. S. E.	lbs. 0°0 0°0 0°2 0°2 2°5 0°2	1 2 3 4 5 6 7	
	S. by W. S. N. N. by E. N. by W. S. by W.	0·2 0·2 0·2 1·0 0·5	S. by W. S. N. by W. N.N.E. N. by W. W.	0·2 0·2 0·2 1·0 1·0	S.S.W. S. S.E. N. by W. N. N.W. by N.	0°2 0°2 0°2 1°0 1°0	S. by W. S. by W. S.E. N. by W. N. by W. N.W. by W.	0.2 2.0 0.2 1.0 1.0 2.0	S.W. by S. S. N.N.E. N. by W. N.W.	0.2 1.5 0.0 0.5 1.0 2.5	S.S.W. S.S.E. N. by W. N.N.W. N.N.W.	0·2 0·2 0·0 0·2 0·5 2·0	8 9 10 11 12 13 14	
	S.E. S.S.W. S.E. by S. S. by W. E.S.E. S.	0·2 0·2 0·2 0·2 0·2 0·2	E.S.E. S.W. by S. S.S.E. S.	0·2 0·2 0·2 0·2 0·2 0·0	E.S.E. S.S.W. S.S.E. S.S.E. N.W.	0.2 0.2 0.2 0.2 0.2 0.0	E.S.E. S.S.W. S. by E. S.S.E. S.S.W. S. by E.	0·2 0·2 0·2 0·2 0·2 0·2	S.E. S.S.E. S.S.E. N. by W.	0.2 0.0 0.5 0.2 0.0	E. S. by W. S. —	0.2 0.0 1.5 0.2 0.0 0.0	15 16 17 18 19 20 21	MAY.
	S. by E. E. W. S. by W. N.W. by N. S. by W.	0·2 0·2 0·5 0·2 0·2 0·2	S.S.E. N.E. by E. W.S.W. S.S.W. S. by E.	0°2 0°2 1°5 0°2 0°2 0°2	S. by E. E. by N. W. S.S.W. S. S. by E.	0°2 0°5 1°5 0°2 0°2 0°2	S. by E. E.N.E. W.S.W. W. N. E. by S.	0.2 0.5 1.0 0.2 0.2 0.2	E. by S. W. by N. W. N. S.E.	0.0 0.5 1.0 2.0 1.0 0.2	E. S.W. by S. N. by E. N. S. by E.	0.0 1.0 0.5 1.0 0.5 0.2	22 23 24 25 26 27 28	
-	S.W. N. N. by W.	0°2 0°5 1°5	S.W. W.N.W. N. by W.	0°2 1°5 2°5	S.W. by S. N.W. by W. N. by W.	0.5	S.W. by W. N.W. by W. N.	0.2	W.N.W. N.W. by W. N.	0.2 3.0 2.5	W. by N. N.W. by W. N.	0°2 3°0 1°5	29 30 31	
-	18h.		19 ^h .	THE RESERVE OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE	20h.		21h.		22h.		23 ^h .			löttingen
	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	J T	ime.
	N.N.W. E.N.E. E. by N. S.E.	lbs.   0°0   0°2   0°2   0°2   0°2	N.N.W. W.N.W.	lbs.   0 ° 0   0 ° 2   0 ° 0   0 ° 0	N. by E.	lbs. 0'0 0'0 0'2 0'0	N. by E.	lbs. 0°0 0°0 0°2 0°0	S.W.	lbs. 0°0 0°0 0°2 0°0	N.N.W.	lbs. 0°0 0°2 0°0 0°0	1 2 3 4	

		,		DI	RECTIO	N AND FOR	OE OF	1		!			
Mean Göt Time		O ^h .	1	1 ^h .	T	2h.		3 ^h .	P	Direction.	Force.	5 ^h . Direction.	Force,
	1 2 3	N.N.W.	lbs. 0°2 0°0 0°0	Direction.  N.N.W.	lbs. 0°2 0°0 0°0	W. by S.	lbs. 0°2 0°0 0°0	W.N.W.	lbs. 0°2 0°2 0°0	N.W. S. S.W. by S.	lbs. 1 '0 0 '2 0 '2	N.W. by N. S. S.W.	lbs. 1 '0 0 '2 0 '2
	3 4 5 6 7 8 9	W. N. by W. N.	0.0	N.W. by W. N.N.W. N.	0.0	N.N.W. N.N.W. N W.S.W.		S.W. by S. N.N.W. N.N.W. N. S.S.W. S.W. by S.	0.5 1.0 0.5 0.2 0.2 0.2	S. N.N.W. N.W. by N. S. S.S.W. S. by W.	0.5 1.5 0.5 0.2 0.2 0.2	S. N.N.W. E. by N. S. S.S.W. S.S.E.	0.2 1.5 0.5 0.2 0.2 0.2
JUNE.	11 12 13 14 15 16 17	N. by W. N. by W. W. by S.	0.2 0.2 0.0 0.0 0.0 0.2 0.0	N. by W.	0.5 1.0 0.0 0.0 0.5 0.0	N.N.W. N. W.N.W.	0.2 0.2 0.0 0.0 0.0 0.2 0.0	N.N.W. N.W. by N. — W. —	1.0 0.2 0.0 0.0 0.2 0.0	N. by W. N.N.W. W. by S. S.S.W.	1.0 1.0 0.0 0.0 0.5 0.2	N.N.W. N.N.W. S.S.W. S. by W. S. by W.	1.0 0.2 0.0 0.5 0.5
	18 19 20 21 22 23 24	E. by N. W. by S.	0.0 0.0 0.0 0.0 0.0 0.2 0.2	— — — — — w.	0.0 0.0 0.0 0.0 0.0 0.0	S.S.W. S.W. by S. E. W.	0.0 0.2 0.2 0.0 0.2 0.5	S. by W. S.S.W. S.S.E. S. W. by N.	0'0 0'2 0'2 0'2 0'2 1'0	S.S.E. S.S.E. N.W. S.S.E. S.S.W. W.N.W.	0.2 0.2 0.2 0.2 0.2 1.0	S.S.E. S. by E. W. S.E. by E. S.S.W. W.N.W.	0.5 0.5 0.5 0.5 0.5 1.0
	25 26 27 28 29 30	-	0.0 0.0 0.0 0.0 0.0	N.N.W.	0.0 0.0 0.0 0.2 0.0	E.N.E.	0.0 0.0 0.0 0.0 0.0	S. by E. S. by E.	0.0 0.5 0.0 0.5 0.0	S. S. E. S. by E.	0.5 0.5 0.0 0.5 0.5 0.5	S. by W. S.S.E. S.E. by S.	0.5 0.5 0.5 0.5 0.5
(continue	۱۱	12h.		13h.		14 ^h .		15 ^h .		16 ^h .		17 ^h .	
Mean Göt Time		Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.
	$\begin{pmatrix} 1\\2\\3 \end{pmatrix}$	S.W. by W.	0.5	S.W. by W.	lbs. 0°0 0°2 0°0		lbs. 0.0 0.0		lbs. 0°0 0°0		0.0 0.0 0.0		1bs. 0.0 0.0
	4 5 6 7 8 9	N.W. N. N. by W. E. by S.	0.5 1.5 0.5 0.2 0.0 0.0	N.W. by N. N. N. by W.	0.5 1.0 0.5 0.0 0.0 0.2	N.N.W. N. by W. N.N.W.	0.5 0.2 0.5 0.0 0.2 0.0	N.N.W. N.N.W. N.	0.2 0.0 0.5 0.0 0.2 0.0	N.N.W.  N. by W.  N. by W.	0.5 0.0 0.5 0.0 0.2	N.W. N. by W. N. by W.	0.2 0.0 0.5 0.0 0.2 0.0
JUNE.	11 12 13 14 15 16 17	N.N.W. N. W. by N. W. by N.	1.0 1.0 0.2 0.2 0.2	N.W. N. W. W.S.W.	1.0 1.0 0.0 0.5 0.2 0.0	N.W. N. S.W. by W.	0.2 0.5 0.0 0.5 0.0 0.0	N. by W. E.N.E.	0.0 0.2 0.0 0.0 0.0	E.N.E.  E.S. by W.	0.0 0.0 0.2 0.0 0.0 0.2	N.W. E.N.E.	0°2 0°2 0°0 0°0
	18 19 20 21 22 23 24	S. by W. W.N.W. E. by N. W.N.W. W.N.W.	0.0 0.2 0.5 0.2	N.W. W.N.W. E.N.E. N.W. by W W.N.W.	0.0 0.2 0.5 0.2 1.5 0.2	S.W. W.N.W. W. W.N.W.	0.0 0.2 0.2 0.0 1.0 0.2	N.W. by W.	0.0 0.0 0.0 0.0 1.0 0.0	E.S.E	0.0 0.0 0.0 0.0 0.5 0.0	W. by N. S.S.W. — — — W.	0.5 0.5 0.0 0.0 0.0
	25 26 27 28 29 30	S.W. by S. S.W.	0.5 0.5 0.0 0.0 0.0	S.W. by S. W.	0.5 0.5 0.0 0.0 0.0	W. by S.	0.0 0.2 0.0 0.0 0.0	— — — —	0.0 0.0 0.0 0.0 0.0 0.0	N. by W. E.N.E. S.W. by W.	0.0 0.0 0.2 0.2 0.2	— — — W.	0.0 0.0 0.0 0.0

				DIRE	ECTION	AND FORC	Е ОГ Т	HE WIND.				1	
6 ^h •		7h.		8h.		9հ.		10h.		11b.			Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	]	Time.
N. by W. S.S.W. S.W.	lbs. 1.0 0.2 0.2	N.N.W. S. by W. W.S.W.	lbs. 1 '0 1 '0 0 '2	N.W. S. by W. S.W.	lbs. 1.0 1.5 0.5	S. by W. S. by W. S.W.	lbs. 0°2 2°0 0°5	S. S.S.W. S.W.	lbs. 0°2 1°5 0°5	S.W. S.W. by S.	lbs. 0°0 1°0 0°2	$egin{bmatrix} 1 & 5 \\ 2 & 3 \\ 4 & 4 \end{bmatrix}$	
S.E. by S. N.N.W. N.W. S.S.W. S.S.W. S. by W.	0.2 1.5 0.2 0.2 0.2 0.2 0.2	S. N. W. N. W. S.S. W. S. by W. S. by W.	0.5 1.0 1.0 0.2 0.2 0.2	S.W. N.N.W. N.W. S.S.W. S. by W. S. by W.	0.5 1.0 1.0 0.2 0.2 0.2	S. N.N.W. N.N.W. S. S. by W. S.S.W.	0.5 0.5 1.0 0.2 0.2 0.2	S. by W. N. N.N.W.  S.S.W.	0.2 0.5 1.0 0.0 0.0 0.2	S. N. N	0°2 2°0 1°0 0°0 0°0 0°2	5 6 7 8 9 10	
N.W. by N. N.W. S.W. by S. N.W. by W. W. by N. S.S.E.	1.5 0.5 1.0 0.5 0.2	N.W. N.N.W. S.S W. W. by N. S.S.W. S.W.	2:0 2:0 0:2 1:0 0:5 0:2	N.W. N.W. W.N.W. S.S.W.	1.5 2.5 0.0 0.5 0.5	N.W. by N. N.N.W. S.S.E. W. S.W. by S.		N.W. by N. N.N.W. E.S.E. W. by N. S.W. by S. S.E. by E.	1.0 2.0 0.2 1.0 0.2 0.2	N.N.W. N. W.N.W.	1.0 0.0 0.0 0.0 0.0	12 13 14 15 16 17 18	JUNE.
S.W. W. by N. E. by S. S.S.W. W.N.W.	0.0 0.2 0.5 0.2 1.5 1.5	E. by N. W.N.W. E. S.S.W. W. by S.	0.0 0.2 0.5 0.2 1.5 1.5	E.S.E. E.S.E. W.N.W. E. W.S.W.	$0.5 \\ 0.5$	S.E. E.S.E. N.W. by W. E. W. by S. W.	$0.5 \\ 0.5$	S.S.E. S.E. by E. W.N.W. E. by S. W. by S. N.W. by W.	0.2 0.2 0.2 0.2 2.5 1.0	W. by N. W.N.W. E. by N. W. by N. W. by N. W. N.W.	0.0 2.5 0.2 0.2 3.0 0.5	19 20 21 22 23 24 25	
S. by W.  S. by S.	0.2 0.5 0.0 0.2 0.2	S.E. S.S.W. N.N.W. S. S.E.	0.5 0.5 0.5 0.2 0.2	S.E. by E. S. by W. N. S. E. by S.	0.2 0.5 0.2 0.2 0.2	S.E. S.S.W. N. S.S.E. S.E.	0.2 0.5 0.2 0.2 0.2	S.E. S.S.W. N.N.W. — S.E. by E.	0°2 1°0 0°2 0°0 0°5	S. by E. S.W. by W. N.N.W.  S.E. by E.	0.2 0.0 0.2 0.0 0.2	26 27 28 29 30	
18h.		19 ^h .	\	20 ⁱⁱ .		21h.		22h.		230.		Mean	Göttingen
Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.	Direction.	Force.		Time.
Direction.	Force.	Direction.	Ibs.   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		Force.	Direction.	Ibs.   0.0   0.0   0.0   0.5   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0	Direction.	Borce.	W. N. by W. N. by W. N. by W.	Box   Control   Force	1 2 3 4 5 6 7 8 9 10 11 12 13	

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	s		

## TORONTO, 1846 to 1848.

METEOROLOGICAL JOURNAL.

oronto		Ext	tent of Cl	oudy Sk	y.	Max.	Min.	D-:-
Mean Time.	Weather and Phenomena.	3	9	15	21	Therm.	Therm.	Rain,
р.	JANUARY.					0	0	In.
1		1.0	1.0	1.0	1.0	29.0	9.5	0.250
$egin{array}{c} 1 \ 2 \end{array}$	Clouded all day; cir., cirstrat., and haze; snow, sleet, and rain  Clouded all day; circum. and haze; rain and snow till 13h, when it ceased	1.0	1.0	1.0	1.0	38.7	28.7	0.45
$\frac{2}{3}$	Cloudy all day; cir-cum, and haze; occasional rain	0.9	1.0		<del>-</del>	38.5	28.5 $28.2$	_
4	To represent alouded, air source and haze: halo round the moon at 10", imperiect	<u></u>	$\frac{1.0}{1.0}$	$\frac{0.0}{0.2}$	0.9	$\frac{36.0}{36.2}$	$\frac{28 \ 2}{26.7}$	<u>-</u>
5	In general alouded with cir-cum, and haze, except from 13" to 15", when it was clear	0.8   0.8	1.0	1.0	1.0	36.2	23.0	0.18
6	Clouded all day : eir -cum, and haze : snow and rain mixed from 8" to 17"	1.0	1.0	1.0	1.0	34.5	27.7	0.43
7	Clouded all day; dense haze; slight rain till 12h; snow at 16h and 17h  Clouded all day; dense haze; slight rain till 12h; snow at 16h and 17h	1.0	1.0	1.0	0.5	36.4	33.2	0.18
8	Clouded all day; circum. and haze; slight snow occasionally; clouded at 21 ^h Partially clouded to 1 ^h ; circum., cirstrat., and haze	1.0	1.0	1.0	1.0	33.8	28.0	-
9 10	Cloudy; circum., cirstrat., and haze; occasional snow	1.0	1.0			30.4	26.1	-
11	Clouded all day; cir -cum cir-strat, and haze; some slight snow			1.0	1.0	31.6	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	_
$\overline{12}$	Current will obe sime own a six estrate remainder of the day clear	1.0	0.3	0.3	1.0			
13 {	Generally clouded; circum., cirstrat., and haze; clear intervals occasionally; imperiect	1.0	0.3	1.0	1.0	27.7	9.0	
14	Clouded till 4 ^h ; circum., cirstrat., and haze; remainder clear; slight snow from 19 ^h to 22 ^h	1.0 0.4	$\begin{array}{c} 0.8 \\ 0.0 \end{array}$	$\frac{1.0}{0.0}$	0.0	29.5 35.2	9.7	
15	Generally clouded; circum, cirstrat., and haze; halo round the moon at 11 ^h and 15 ^h ,	1.0	0.6	1.0	1.0	40.4	18.4	_
16 {	imperfect					31.7	11.5	
17	Generally clouded; circum., cirstrat., and haze	1.0	0.3	1.0	0.5	12.7	-1.5	_
18	Clear at 10 ^h and 11 ^h ; remainder of the day clouded; circum. and cirstrat.; clouded at 18 ^h & 19 ^h	0.1	0.0	1.0	1.0	20.9	0.9	_
19	Clouded at 13 ^h to 17 ^h ; circum., cirstrat., and haze; remainder clear  Clouded all day; circum., cirstrat., and haze	1.0	1.0	1.0	1.0	17.7	5.2	
$\begin{array}{c} 20 \\ 21 \end{array}$	Clouded all day; circum., cirstrat., and haze Clouded till 4 ^h ; circum. and haze; remainder clear; snow from 21 ^h to 23 ^h	1.0	0.0	0.0	0.0	25.2	9.5	-
$\frac{21}{22}$	Snow from 1h to 4h · afterwards clear	0.0	0.0	0.0	0.1	27.9	1.1	-
23	Clear till 14h: remainder clouded; cirstrat. and haze	0.0	0.0	1.0	0.7	$\begin{vmatrix} 20.1 \\ 23.2 \end{vmatrix}$	5.9	_
24	Clauder, sin street and haze; clouded from 18 ⁿ to 23 ⁿ	0 z		1.0	1.0	37.0	19.6	
25	Clouded from 12 ^h to 17 ^h ; cirstrat. and haze; remainder clear; rain from 16 ^h to 17 ^h Clouded till 13 ^h ; circum. and haze; misty; remainder clear; slight rain and snow occasionally	1.0	1.0	0.0	0.5	44.0	31.7	0.5
26	Generally clear till 6 ^h ; remainder overcast with dense haze	0.5	1.0	0.9	1.0	37.3	17.7	-
$\begin{array}{c} 27 \\ 28 \end{array}$	Generally Great into ; remainder overcook with	1.0	1.0	1.0	1.0	31.7	15.5	-
			1		1	1	1	10.0
	Clouded all day; circum, and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h	1.0	1.0	1.0	1.0	38.0	31.5	
29 30 31	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded at 9 ^h and 10 ^h , and from 18 ^h to 21 ^h ; clear from 22 ^h to 23 ^h		1		1	1	1	0.3
29 30	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h	1.0	1.0	1.0	1.0	38.0 37.7	31.5 33.2	0.3
29 30	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h	1.0	1.0	1.0	1.0	38.0 37.7 42.0	31.5 33.2 17.0	0.3
29 30 31	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded at 9 ^h and 10 ^h , and from 18 ^h to 21 ^h ; clear from 22 ^h to 23 ^h FEBRUARY.	1.0 1.0 0.2	0.0		1.0 0.6 —	38.0 37.7 42.0 20.9	31.5 33.2	0.3
29 30 31	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded at 9 ^h and 10 ^h , and from 18 ^h to 21 ^h ; clear from 22 ^h to 23 ^h FEBRUARY.	1.0	1.0	1.0	1.0	38.0 37.7 42.0	8.3 9.1 22.5	0.3
29 30 31 1 2 3	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded at 9 ^h and 10 ^h , and from 18 ^h to 21 ^h ; clear from 22 ^h to 23 ^h FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded all day; circum. and cirstrat.; lunar halo at 7 ^h and 8 ^h , diameter 30°, perfect	1'0 1'0 0'2 	1.0 1.0 1.0 1.0 1.0	1.0 1.0 - 1.0 0.4 0.0	1.0 0.6 - 1.0 0.3 0.4	20.9 22.2 32.5 41.9	8·3 9·1 22·5 28·7	0.8
29 30 31 1 2 3 4	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded at 9 ^h and 10 ^h , and from 18 ^h to 21 ^h ; clear from 22 ^h to 23 ^h FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7 ^h and 8 ^h , diameter 30°, perfect Clouded till 11 ^h ; cir., cirstrat., circum., and haze; clear	1.0 1.0 0.2 1.0 1.0 1.0	1.0 1.0 0.0	1.0 1.0 - 1.0 0.4 0.0 0.2	1.0 0.6 - 1.0 0.3 0.4 0.0	20.9 22.2 32.5 41.9 40.1	8·3 9·1 22·5 28·7 28·1	0.8
29 30 31 1 2 3 4 5	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded at 9 ^h and 10 ^h , and from 18 ^h to 21 ^h ; clear from 22 ^h to 23 ^h FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7 ^h and 8 ^h , diameter 30°, perfect Clouded till 11 ^h ; cir., cirstrat., circum., and haze; clear Clouded till 11 ^h ; cir., cirstrat.; clear	1'0 1'0 0'2 1'0 1'0 1'0 0'7	1.0 1.0 0.0	1.0 1.0 - 1.0 0.4 0.0 0.2 0.4	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1	20.9 22.2 32.5 41.9 40.1 40.0	8'3 9'1 22'5 28'7 28'1 23'0	0.8
29 30 31 1 2 3 4 5 6 7	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded at 9 ^h and 10 ^h , and from 18 ^h to 21 ^h ; clear from 22 ^h to 23 ^h FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7 ^h and 8 ^h , diameter 30 ^o , perfect Clouded till 11 ^h ; cir., cirstrat., circum., and haze; clear Clouded at 4 ^h , 9 ^h , and 10 ^h ; circum. and haze; clear	1.0 1.0 0.2 1.0 1.0 1.0	1.0 1.0 0.0	1.0 1.0 - 1.0 0.4 0.0 0.2 0.4 -	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1	20°9 22°2 32°5 41°9 40°1 40°0 39°2	8·3 9·1 22·5 28·7 28·1	0.8
29 30 31 1 2 3 4 5 6 7 8 }	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded at 9 ^h and 10 ^h , and from 18 ^h to 21 ^h ; clear from 22 ^h to 23 ^h FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7 ^h and 8 ^h , diameter 30°, perfect Clouded till 11 ^h ; cir., cirstrat., circum., and haze; clear Clouded till 11 ^h ; circum. and cumstrat.; clear Clouded at 4 ^h , 9 ^h , and 10 ^h ; circum. and haze; clear Clouded at 7 ^h , 12 ^h , and 17 ^h ; circum., cirstrat., and haze; clear	1'0 1'0 0'2 1'0 1'0 1'0 0'7	1.0 1.0 0.0	1.0 1.0 - 1.0 0.4 0.0 0.2 0.4	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1	20.9 22.2 32.5 41.9 40.1 40.0	8'3 9'1 22'5 28'7 28'1 23'0 23'6	0.8
29 30 31 1 2 3 4 5 6 7 8 9	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded at 9 ^h and 10 ^h , and from 18 ^h to 21 ^h ; clear from 22 ^h to 23 ^h FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7 ^h and 8 ^h , diameter 30°, perfect Clouded till 11 ^h ; cir., cirstrat., circum., and haze; clear Clouded till 11 ^h ; circum. and cumstrat.; clear Clouded at 4 ^h , 9 ^h , and 10 ^h ; circum. and haze; clear Clouded at 7 ^h , 12 ^h , and 17 ^h ; circum. cirstrat., and haze; clear Clouded till till till till till till till til	1'0 1'0 0'2 1'0 1'0 1'0 0'7 1'0 	1'0 1'0 0'0	1.0 1.0 1.0 - 1.0 0.4 0.0 0.2 0.4 - 1.0 0.0 1.0	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 - 1.2 1.0 1.0	20.9 22.2 32.5 41.9 40.0 39.2 40.0 20.9 16.5	8·3 9·1 22·5 28·7 28·1 23·6 11·0 10·3 4·2	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10	Clouded all day; circum. and haze; slight rain from 2 ^h to 5 ^h , and from 15 ^h to 20 ^h Clouded all day; circum. and haze; slight rain from 18 ^h to 20 ^h Clouded at 9 ^h and 10 ^h , and from 18 ^h to 21 ^h ; clear from 22 ^h to 23 ^h FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7 ^h and 8 ^h , diameter 30°, perfect Clouded till 11 ^h ; cir., cirstrat., circum., and haze; clear Clouded till 11 ^h ; circum. and cumstrat.; clear Clouded at 4 ^h , 9 ^h , and 10 ^h ; circum. and haze; clear Clouded at 7 ^h , 12 ^h , and 17 ^h ; circum., cirstrat., and haze; clear Clouded at 7 ^h , 12 ^h , and 17 ^h ; circum., cirstrat., and haze; clear Clouded: circum. and strat.; halo round the moon at 12 ^h , diameter 40°, perfect Clouded: circum. and haze; snowing slightly all day	1'0 1'0 0'2 1'0 1'0 1'0 0'7 1'0 0'0 1'0	1'0 1'0 0'0	1.0 1.0 1.0 - 1.0 0.4 0.0 0.2 0.4 - 1.0 0.0 1.0 0.0	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 1.2 1.0 0.2	20.9 22.2 32.5 41.9 40.0 39.2 40.0 20.9 16.5 28.0	8·3 9·1 22·5 28·7 28·1 23·6 11·0 10·3 4·2 4·6	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10 11	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h  FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded; circum. and strat.; halo round the moon at 12h, diameter 40°, perfect Clouded; circum. and haze; snowing slightly all day Clouded till 14h; circum. and haze; snowing from 18h to 23h Clouded till 14h; circum. and haze; snowing from 18h to 23h			1.0 1.0 1.0 0.4 0.0 0.2 0.4 - 1.0 0.0 1.0	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 - 1.2 1.0 0.2 1.0	20.9 22.2 32.5 41.9 40.0 20.9 16.5 28.0 23.7	8·3 9·1 22·5 28·7 28·1 23·6 11·0 10·3 4·2 4·6 -3·4	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h  FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded; circum. and strat.; halo round the moon at 12h, diameter 40°, perfect Clouded; circum. and haze; snowing slightly all day Clouded till 14h; circum. and haze; snowing from 18h to 23h  Clouded till 14h; circum. and haze; snowing from 18h to 23h	1'0 1'0 0'2 1'0 1'0 1'0 0'7 1'0 0'6 0'9		1.0 1.0 1.0 - 1.0 0.4 0.0 0.2 0.4 - 1.0 0.0 1.0 0.0 1.0	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 1.0 0.2 1.0 1.0	20.9 22.2 32.5 41.9 40.1 40.0 39.2 40.0 20.9 16.5 28.0 23.7 24.4	8·3 9·1 22·5 28·7 28·1 23·6 11·0 10·3 4·2 4·6 -3·4 -7·0	0.3
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h - FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded iil 11h; circum. and strat.; halo round the moon at 12h, diameter 40°, perfect Clouded; circum. and haze; snowing slightly all day Clouded till 14h; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum. and haze; halo round the moon at 16h and 17h, diameter 40°, perfect			1.0 1.0 1.0 0.4 0.0 0.2 0.4 - 1.0 0.0 1.0	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 - 1.2 1.0 0.2 1.0	20.9 22.2 32.5 41.9 40.0 20.9 16.5 28.0 23.7	8:3 9:1 22:5 28:7 28:1 23:0 23:6 11:0 10:3 4:2 4:6 -3:4 -7:0 12:8 15:5	0.3
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h  FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; circum. and cumstrat.; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; elear Clouded; circum. and haze; snowing slightly all day Clouded till 14h; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum. and haze; halo round the moon at 16h and 17h, diameter 40°, perfect Clouded; circum. and haze; halo round the moon at 16h and 17h, diameter 40°, perfect Clouded; circum. and haze; halo round the moon at 16h and 17h, diameter 40°, perfect Clouded; circum., cirstrat., and haze; snow commences at 4h and continues all night Overcast: circum., cirstrat., and haze; slight snow from 0h to 10h	1'0 1'0 0'2 1'0 1'0 1'0 1'0 1'0 1'0 0'6 0'9 1'0	1'0 1'0 0'0 1'0 1'0 1'0 0'7 1'0 0'0 1'0 1'0 1'0	1.0 1.0 1.0 0.4 0.0 0.2 0.4 1.0 0.0 1.0 0.8 1.0	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 - 1.0 1.0 1.0 1.0	20.9 22.2 32.5 41.9 40.0 39.2 40.0 20.9 16.5 28.0 23.7 24.4 35.2 34.4 25.3	8·3 9·1 22·5 28·7 28·1 23·0 23·6 11·0 10·3 4·2 4·6 -3·4 -7·0 12·8 15·5 13·2	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h  FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; cir., cirstrat.; circum., and haze; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum. and haze; clear Clouded till 14h; circum. and haze; snowing slightly all day Clouded; circum. and haze; snowing slightly all day Clouded; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum. and haze; halo round the moon at 16h and 17h, diameter 40°, perfect Clouded; circum. and haze; snow commences at 4h and continues all night Overcast; circum., cirstrat., and haze: snow commences at 4h and continues all night Overcast; circum., cirstrat., slight fall of snow from 2h to 12h	1'0 1'0 0'2 1'0 1'0 1'0 1'0 1'0 1'0 0'6 0'9 1'0 1'0	1'0 1'0 0'0 1'0 1'0 1'0 0'7 1'0 0'0 1'0 1'0 1'0	1.0 1.0 1.0 0.4 0.0 0.2 0.4 	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 - 1.0 1.0 0.2 1.0 1.0 1.0 0.8	20.9 22.2 32.5 41.9 40.0 39.2 40.0 20.9 16.5 28.0 23.7 24.4 25.3 27.7	8:3 9:1 22:5 28:7 28:1 23:0 23:6 11:0 10:3 4:2 4:6 -3:4 -7:0 12:8 15:5	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h  FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded; circum. and haze; snowing slightly all day Clouded; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum. and haze; halo round the moon at 12h, diameter 40°, perfect Clouded; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum., cirstrat., and haze; snow commences at 4h and continues all night Overcast; circum., cirstrat., and haze; slight snow from 0h to 10h Clouded; circum., cirstrat., and haze; slight snow from 2h to 12h Destially alcouded; circum.; cumstrat.; slight fall of snow from 2h to 12h Destially alcouded; circum.; cumstrat.; after part of day clear	1'0 1'0 0'2 1'0 1'0 1'0 1'0 1'0 1'0 0'6 0'9 1'0	1'0 1'0 0'0 1'0 1'0 1'0 0'7 1'0 0'0 1'0 1'0 1'0	1.0 1.0 1.0 0.4 0.0 0.2 0.4 1.0 0.0 1.0 0.8 1.0	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 - 1.0 1.0 1.0 1.0	20.9 22.2 32.5 41.9 40.0 39.2 40.0 20.9 16.5 28.0 23.7 24.4 35.2 34.4 25.3	8·3 9·1 22·5 28·7 28·1 23·0 23·6 11·0 10·3 4·2 4·6 -3·4 -7·0 12·8 15·5 13·2 18·9	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h  FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; circum. and cirstrat.; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded; circum. and haze; snowing slightly all day Clouded; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum., cirstrat., and haze; snow commences at 4h and continues all night  Overcast; circum., cirstrat., and haze; slight snow from 0h to 10h Clouded; circum., cirstrat., sight fall of snow from 2h to 12h Partially clouded; circum.; cumstrat.; slight fall of snow from 2h to 12h Partially clouded; circum.; cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30°	1'0 1'0 0'2 1'0 1'0 1'0 1'0 1'0 1'0 0'6 0'9 1'0 1'0 1'0	1'0 1'0 0'0 1'0 1'0 1'0 0'7 1'0 0'0 1'0 1'0 1'0 1'0 1'0	1.0 1.0 1.0 0.4 0.0 0.2 0.4 1.0 0.0 1.0 0.8 1.0 0.1 0.0 1.0 0.1	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 - 1.0 1.0 0.2 1.0 1.0 0.8 1.0	20.9 22.2 32.5 41.9 40.0 20.9 16.5 28.0 23.7 24.4 35.2 34.4 25.3 27.7 30.9 27.2 29.6	8:3 9:1 22:5 28:7 28:1 23:0 23:6 11:0 10:3 4:2 4:6 -3:4 -7:0 12:8 15:5 13:2 18:9 4:0 a 5:4 a 7:0	0.3
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h.  FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; circum. and cumstrat.; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded; circum. and haze; snowing slightly all day Clouded; circum. and haze; snowing slightly all day Clouded till 14h; circum. and haze; snowing from 18h to 23h Clear till 19h afterwards clouded; circum. and haze Clouded; circum., cirstrat., and haze: snow commences at 4h and continues all night Overcast; circum., cirstrat., and haze: snow commences at 4h and continues all night Overcast; circum., cirstrat., and haze: snow from 0h to 10h Clouded; circum; cumstrat.; slight fall of snow from 2h to 12h Partially clouded; circum.: cumstrat.; after part of day clear Clouded; circum., cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum., cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum., cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30°	1'0 1'0 0'2  1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'	1'0 1'0 0'0 1'0 1'0 1'0 0'7 1'0 0'0 1'0 1'0 1'0 1'0 1'0	1'0 1'0 - 1'0 0'4 0'0 0'2 0'4 - 1'0 0'0 1'0 0'8 - 1'0 0'1 0'0 1'0 0'0 1'0 0'0	1.0 0.6  1.0 0.3 0.4 0.0 1.0 1.0 1.0 1.0 1.0 0.8 1.0 0.4	20.9 22.2 32.5 41.9 40.0 20.9 16.5 28.0 23.7 24.4 35.2 34.4 25.3 27.7 30.9 27.2 29.6 29.8	8:3 9:1 22:5 28:7 28:1 23:0 23:6 11:0 10:3 4:2 4:6 -3:4 -7:0 12:8 15:5 13:2 18:9 4:0 22:7	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum, and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h.  FEBRUARY.  Clouded all day; circum., 'cirstrat., 'and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded iill 14h; circum. and strat.; halo round the moon at 12h, diameter 40°, perfect Clouded; circum. and haze; snowing slightly all day Clouded iill 14h; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze clouded; circum. and haze; halo round the moon at 16h and 17h, diameter 40°, perfect Clouded; circum., cirstrat., and haze; snow commences at 4h and continues all night Overcast; circum., cirstrat., and haze; slight snow from 0h to 10h Clouded; circum.; cirstrat., and haze; slight snow from 0h to 10h Clouded; circum; cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum, cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum., cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum., cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum., cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum., cirstrat., snowing most part of the day Clouded; circum. and haze; snowing most part of the day			1.0 1.0 1.0 0.4 0.0 0.2 0.4 1.0 0.0 1.0 0.0 1.0 0.1 0.0 1.0 0.1 0.0 0.1 0.0 0.1	1.0 0.6  1.0 0.3 0.4 0.0 0.1  1.0 0.2 1.0 1.0 0.8 1.0 0.4  1.0	20.9 22.2 32.5 41.9 40.0 20.9 16.5 28.0 23.7 24.4 35.2 34.4 25.3 27.7 29.6 29.8 33.9	8:3 9:1 22:5 28:7 28:1 23:0 23:6 11:0 10:3 4:2 4:6 -3:4 -7:0 12:8 15:5 13:2 18:9 4:0 22:7 13:3	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum, and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h  FEBRUARY.  Clouded all day; circum., 'cirstrat., 'and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded; circum. and haze; snowing slightly all day Clouded; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum., cirstrat., and haze; snow commences at 4h and continues all night Overcast; circum., cirstrat., and haze; slight snow from 0h to 10h Clouded; circum, cirstrat., and haze; slight snow from 0h to 10h Clouded; circum, cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum, cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum, cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum, cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum, cirstrat., circum., and haze; clouded from 20h to 23h  Overcast from 9h to 12h; overcast from 18h to 23h  Overcast from 0h to 3h; cirstrat., circum., and haze; clouded from 20h to 23h			1.0 1.0 0.4 0.0 0.2 0.4 1.0 0.0 1.0 0.0 1.0 0.1 0.0 1.0 0.0 1.0 0.0 0	1.0 0.6  1.0 0.3 0.4 0.0 0.1  1.0 0.2 1.0 1.0 0.2 1.0 0.4 1.0 0.4  1.0 0.4	20.9 22.2 32.5 41.9 40.0 20.9 16.5 28.0 23.7 24.4 35.2 34.4 25.3 27.7 29.6 29.8 33.9 26.9	8:3 9:1 22:5 28:7 28:1 23:0 23:6 11:0 10:3 4:2 4:6 -3:4 -7:0 12:8 15:5 13:2 18:9 4:0 22:7 13:3 13:1	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h -  FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; circum. and cumstrat.; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded; circum. and haze; snowing slightly all day Clouded; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum. and haze; halo round the moon at 16h and 17h, diameter 40°, perfect Clouded; circum., cirstrat., and haze; snow commences at 4h and continues all night Overcast; circum., cirstrat., and haze; slight snow from 0h to 10h Clouded; circum.; cirstrat., and haze; slight snow from 0h to 10h Clouded; circum, cirstrat.; slight fall of snow from 2h to 12h Partially clouded; circum.: cumstrat.; after part of day clear Clouded; circum., cirstrat., and haze; shalo round the sun at 21h and 23h, diameter 30° Clouded; circum., cirstrat., and haze; snow squalls  Clear from 9h to 12h; overcast from 18h to 23h  Clear from 0h to 3h; cirstrat., circum., and haze; clouded from 20h to 23h  Clouded at 12h; circum., cirstrat., circum., and haze; clouded from 20h to 23h  Clouded at 12h; circum., cirstrat., circum., and haze; clouded from 20h to 23h  Clouded at 12h; circum., cirstrat., circum., and haze; clouded from 20h to 23h	1'0 1'0 0'2  1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'	1'0 1'0 0'0 1'0 1'0 1'0 0'7 1'0 0'3 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0	1.0 1.0 0.4 0.0 0.2 0.4 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 0	1.0 0.6  1.0 0.3 0.4 0.0 0.1  1.0 0.2 1.0 1.0 0.8 1.0 0.4  1.0 0.4  1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	20.9 22.2 32.5 41.9 40.0 20.9 16.5 28.0 23.7 24.4 35.2 34.4 25.3 27.7 30.9 27.2 29.6 29.8 33.9 26.9 27.0	8:3 9:1 22:5 28:7 28:1 23:0 23:6 11:0 10:3 4:2 4:6 -3:4 -7:0 12:8 15:5 13:2 18:9 4:0 22:7 13:3	0.3
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 25	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h  FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded; circum. and haze; snowing slightly all day Clouded; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum. and haze; halo round the moon at 16h and 17h, diameter 40°, perfect Clouded; circum., cirstrat., and haze; snow commences at 4h and continues all night Overcast; circum., cirstrat., and haze; snow commences at 4h and continues all night Overcast; circum., cirstrat., and haze; snow commences at 2h and continues all night Clouded; circum., cirstrat., and haze; snow commences at 4h and continues all night Overcast; circum., cirstrat., and haze; snow from 0h to 10h Clouded; circum., cirstrat., and haze; snow from 2h to 12h Partially clouded; circum.; cumstrat.; after part of day clear Clouded; circum., cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum., cirstrat., circun., and haze; clouded from 20h to 23h  Overcast from 0h to 3h; cirstrat., circun., and haze; clouded from 20h to 23h  Clouded from 9h to 14h; circum., cirstrat., and haze; snowing slightly			1.0 1.0 0.4 0.0 0.2 0.4 1.0 0.0 1.0 0.0 1.0 0.1 0.0 1.0 0.0 1.0 0.0 0	1.0 0.6  1.0 0.3 0.4 0.0 0.1  1.0 0.2 1.0 1.0 0.2 1.0 0.4 1.0 0.4  1.0 0.4	20.9 22.2 32.5 41.9 40.0 20.9 16.5 28.0 23.7 24.4 35.2 34.4 25.3 27.7 29.6 29.8 33.9 26.9	8:3 9:1 22:5 28:7 28:1 23:0 23:6 11:0 10:3 4:2 4:6 -3:4 -7:0 12:8 15:5 13:2 18:9 4:0 a 5:4 a 7:0 22:7 13:3 13:1 10:1	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 23 24 25 26	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h  FEBRUARY.  Clouded all day; circum., cirstrat., and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear Clouded till 14h; circum. and haze; snowing slightly all day Clouded till 14h; circum. and haze; snowing from 18h to 23h Clear till 19h, afterwards clouded; circum. and haze Clouded; circum., cirstrat., and haze; snow commences at 4h and continues all night Clouded; circum., cirstrat., and haze; snow from 0h to 10h Clouded; circum., cirstrat., slight fall of snow from 0h to 12h Partially clouded; circum., cumstrat.; after part of day clear Clouded; circum., cirstrat., and haze; halo round the suon at 21h and 23h, diameter 30° Clouded; circum., cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum., cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30° Clouded; circum., cirstrat., circum., and haze; clouded from 20h to 23h Clouded trom 9h to 12h; overcast from 18h to 23h  Overcast from 0h to 3h; cirstrat., circum., and haze; snowing slightly Generally clear; light circum., cirstrat., and haze; snowing slightly Generally clear; light circum., cirstrat., and haze; snowing slightly Generally clear; light circum., cirstrat., and haze; snowing slightly	1'0 1'0 0'2 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0	1'0 1'0 0'0  1'0 1'0 1'0 0'7 1'0 0'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0	1.0 1.0 0.4 0.0 0.2 0.4 	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 1.0 1.0 0.2 1.0 1.0 0.8 1.0 0.4 - 1.0 0.4 - 1.0 0.8 1.0 0.0 0.1	20.9 22.2 32.5 41.9 40.0 39.2 40.0 23.7 24.4 35.2 34.4 25.3 27.7 30.9 27.2 29.6 29.8 33.9 26.7 21.2 17.8 10.9	8:3 9:1 22:5 28:7 28:1 23:0 23:6 11:0 10:3 4:2 4:3 4:4 -7:0 12:8 15:5 13:2 18:9 4:0 22:7 13:3 13:1 10:1 0:2 -11:7 -16:4	0.8
29 30 31 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	Clouded all day; circum. and haze; slight rain from 2h to 5h, and from 15h to 20h Clouded all day; circum. and haze; slight rain from 18h to 20h Clouded at 9h and 10h, and from 18h to 21h; clear from 22h to 23h  FEBRUARY.  Clouded all day; circum., 'cirstrat., 'and haze Clouded; circum. and cirstrat.; lunar halo at 7h and 8h, diameter 30°, perfect Clouded till 11h; cir., cirstrat., circum., and haze; clear Clouded till 11h; circum. and cumstrat.; clear Clouded till 11h; circum. and cumstrat.; clear Clouded at 4h, 9h, and 10h; circum. and haze; clear  Clouded at 7h, 12h, and 17h; circum., cirstrat., and haze; clear  Clouded till 14h; circum. and strat.; halo round the moon at 12h, diameter 40°, perfect - Clouded; circum. and haze; snowing from 18h to 23h  Clear till 19h, afterwards clouded; circum. and haze  Clouded; circum. and haze; halo round the moon at 16h and 17h, diameter 40°, perfect - Clouded; circum., cirstrat., and haze; snow commences at 4h and continues all night  Overcast; circum., cirstrat., and haze; slight snow from 0h to 10h  Clouded; circum., cirstrat., silght fall of snow from 2h to 12h  Partially clouded; circum.; cumstrat.; after part of day clear  Clouded; circum., cirstrat., and haze; halo round the sun at 21h and 23h, diameter 30°  Clouded; circum., cirstrat., and haze; snow from 2h to 12h  Overcast from 0h to 12h; overcast from 18h to 23h  Overcast from 0h to 3h; cirstrat., circum., and haze; snowing slightly  Generally clear: light circum., cirstrat., and haze; snowing slightly  Generally clear: light circum., cirstrat., and haze; snowing slightly	1'0 1'0 0'2  1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'	1'0 1'0 0'0 1'0 1'0 1'0 0'7 1'0 0'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0	1.0 1.0 0.4 0.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 0	1.0 0.6 - 1.0 0.3 0.4 0.0 0.1 1.0 1.0 1.0 0.8 1.0 0.4 1.0 0.4 - 1.0 0.0 0.4 1.0 0.8 1.0 0.0 0.1	20.9 22.2 32.5 41.9 40.0 20.9 16.5 28.0 23.7 24.4 25.3 27.7 30.9 27.2 29.6 29.6 29.6 29.7 21.2 17.8	8:3 9:1 22:5 28:7 28:1 23:0 23:6 11:0 10:3 4:2 4:6 -3:4 -7:0 12:8 15:5 13:2 18:9 4:0 22:7 13:3 13:1 10:1 0:2 -11:7	0.8

Toronto		Ex	ctent of C	Cloudy Sl	cy.	Max.	Min.	Rain.
Mean Time.	Weather and Phenomena.	3	9	15	21	Therm.	Therm.	rtam.
D.  2 3 4 5 6 7 8 9 10 11 { 12 13 14 15 16 17 18 19 { 20 21 22 23 24 25 26 27 28 29 30 31	MARCH.  Partially clouded till 7h; cir., cirstrat., and haze; afterwards clear  Clouded from 4h to 10h; cir., cirstrat., and haze; clear; halo round the moon, diameter 40h  Clouded from 21h to 23h; cumstrat., circum., and cirstrat.  Nearly clear till 8h, then clouded; circum., cirstrat., and haze  Clouded till 3h; circum., cirstrat., and haze; cleared up  Clouded; circum. and haze; snow from 0h to 3h  Clear till 5h; clouded; circum., cirstrat., and haze  Clear, except light cirstrat. round horizon  Clear till 6h; clouded; circum., cirstrat., and haze; halo round the moon from 9h to 15h, diameter 30h  Clouded; circum., cumstrat., cirstrat., and haze; slight rain at 2h, 3h, and from 12h to 17h  Clouded; circum. and haze; rain; mist rising from the ground  Clouded; circum. and haze; slight snow from 4h to 9h  Clouded till 3h; circum., cumstrat., and haze; clear  Clouded ill 3h; circum., cumstrat., and haze; faint streamers in N. at 9h  Clouded at 6h, 13h, 15h, and 17h; circum., cirstrat., and haze; halo round the sun at 1h, diameter 35h  Clouded; circum., cirstrat., and haze; halo round the sun, diameter 30h; rain from 7h to 9h  Clouded; circum., cirstrat., and haze; rain from 5h to 11h; solar halo, diameter 30h  Clouded; circum. and haze; rain  Clouded; circum. and haze; rain  Clouded; circum. and haze; rain  Clouded; circum. and haze; rain  Clouded; circum. and haze; rain  Clouded; circum. and haze; rain  Clouded; circum. and haze; rain  Clouded; circum. and haze; rain from 5h to 8h  Clouded; circum. and haze; rain from 5h to 8h  Clouded; circum. and haze; rain from 5h to 8h  Clouded; circum. and haze; snow from 18h to 23h  Clouded; circum.; cirstrat.; clear	0°2 0°5 0°4 0°1 1°0 0°0 0°0 0°0 1°0 1°0 1°0 1°0 1°0	0'0 0'7 0'0 1'0 0'0 1'0 0'0 1'0 1'0 1'0 0'0 1'0 0'0 1'0 1	0.0 0.0 0.0 0.3 1.0 0.3 1.0 0.2 1.0 1.0 1.0 0.0 0.0 1.0 1.0 1.0 1.0 1.0	0°1 0°8 0°2 1°0 1°0 0°7 1°0 1°0 1°0 1°0 1°0 1°0 1°0 1°0	20.7 27.4 30.4 38.9 31.0 31.2 46.2 38.1 40.8 40.7 44.1 45.4 40.0 38.9 35.2 36.4 40.7 49.6 48.1 38.4 40.7 41.7 41.7 41.7 41.7 41.7 41.9 39.6 40.4	0.00 8.3 9.3 14.6 26.9 8.8 10.8 22.7 28.8 33.0 34.2 28.4 22.8 20.4 20.8 27.7 24.1 24.2 34.1 37.3 35.2 35.3 31.7 28.2	In.
1 2 3 4 } 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	Clear all day - Clear all day - Clear all day - Clear till 7h; clouded; cirstrat. and haze; halo round the moon at 8h and 9h, diameter 35°; rain at intervals - Clouded; circum., cirstrat., and haze; lunar halo at 10h, diameter 35°, imperfect - Clouded all day; circum., cirstrat., and haze; rain till 8h - Mostly clear; a few circum. dispersed Generally clouded; circum., strat., and haze; lunar halo at 10h, diameter 45°, perfect; rain  Clouded all day; circum. and haze Clouded till 6h; cumstrat. and circum.; clear; solar halo, diameter 35° Clouded; circum. and cirstrat.; slight rain from 6h to 11h Clear all day Clouded from 3h to 13h; cirstrat. and haze; clear Clear till 14h; clouded; cirstrat. and haze; clear Clear and clouded alternately; circum. and cumstrat.; auroral light in N. at 12h - Clouded from 6h to 9h; cir. and haze; clear Clear to 1h; clouded; circum., cumstrat., and haze; rain from 5h to 10h - Clouded all day; circum., cirstrat., and haze; rain from 13h to 17h - Clouded all day; circum., cirstrat., and haze; slight rain till 6h Clouded till 11h; circum., cirstrat., and haze; guite clear - Clouded; cirstrat., circum., cirstrat., and haze; guite clear - Clouded; cirstrat., circum., cirstrat., and haze; rain from 10h to 16h - Clouded; cirstrat., circum., and haze; rain from 10h to 16h - Clouded; cirstrat., cirstrat., and haze; rain from 5h to 11h - Clouded; cirstrat., cirstrat., and haze; misty	0.0 0.0 0.0 0.0 0.0 1.0 1.0 0.0 1.0 1.0	0.0 0.0 0.0 0.0 1.0 0.0 0.0 1.0 0.0 1.0 0.0 1.0 1	0.0 0.0 0.0 0.0 1.0 1.0 0.4 0.3 0.0 0.4 1.0 	0.0 0.0 0.5 1.0 0.6 0.7 1.0 0.9 0.2 0.0 0.2 0.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	43.9 43.1 43.0 46.3 50.4 54.3 56.1 43.8 56.0 36.6 39.3 45.4 45.7 47.0 58.1 55.5 62.8 81.8 56.6 56.5 46.2 54.6 59.8 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0 61.0	26.7 25.7 29.5 30.5 31.7 41.1 33.4 24.2 36.1 35.9 31.2 24.4 26.9 29.4 24.3 33.0 5 40.2 29.2 41.8 42.2 43.7 50.0 40.7 41.0 36.5 40.7 41.0 40.7 41.0 40.7 40.7 40.7 40.7 40.7 40.7 40.7 40	0·19

Mass		Ez	ktent of C	loudy Sl	ty.	Max.	Min.	F :
Mean Time.	Weather and Phenomena.	3	9	15	21	Therm.		Rain.
D.	MAY.					0	0	In.
1	Clouded all day; circum., cirstrat., and haze; rain from 0h to 15h -	1.0	1.0	1.0	1.0	59.0	50.8	0.15
$\left\{\begin{array}{c}2\\3\end{array}\right\}$	Clouded; circum., cumstrat., and haze; auroral light at 12h	0.4	0.5	$\frac{-}{0.4}$	1.0	63.0	$\frac{51.0}{42.7}$	_
(	Clouded; cirstrat. and haze; solar halo; lunar halo at 9h, diameter 40°; auroral light }	0.4	0.4	0.0	1.0	64.0	39.8	
4 {	in N. from 9 ^h to 11 ^h	1.0	1.0	1.0	0.4	67.6	40.0	
$rac{5}{6}$	Clear	0.0	0.0	0.0	1.0	64.8	51.0	
7	Clouded; cir., circum., and haze till 10 ^h ; afterwards clear Clouded; circum., cirstrat., and haze; rain from 9 ^h to 17 ^h ; solar halo, diameter 35°,	1.0	0.7	0.3	1.0	57.5	41.3	_
8 {	perfect and very bright	1.0	1.0	1.0	1.0	57.8	47°8 a	0.12
9 7	Clouded; circum. and haze; rain	1.0	1.0			62.4	53.9 a	1.43
10 ∫ 11	Clouded; circum. and cirstrat.; clear; auroral light at 10 ^h	$\frac{-}{0.2}$	0.3	0.0	$\frac{1.0}{0.2}$	59.3	54.5 33.8	
$\frac{11}{12}$	Clear; clouded at 15 ^h , 16 ^h , and 17 ^h , with circum. and haze	0.1	0.5	1.0	1.0	48.5	40.0	
13	Clouded; circum. and haze; showers of rain	1.0	1.0	1.0	0.9	64.0	38.6	0.38
$\frac{14}{15}$	Clouded; circum. and cumstrat; rain	0.8	0.4	1.6	0.8	70.5	49.8	1.63
16 ₇	Clear; clouded; circum. and haze; rain	0.6	0.0			62.8	44.7	_
17 }	Clouded; after part clear	0.0	$\frac{0.0}{}$	$\frac{0.0}{1.0}$	0.4	64.0	43°0 52°0	
18 19	Clouded; after part clear	0.0	0.2	0.0	0.0	56.0	34.9	_
20	Clear	0.6	0.0	$0.0 \\ 0.0$	$0.0 \\ 0.4$	56.3	37.7 34.3	_
$\frac{21}{22}$	Clear	1.0	1.0	1.0	0.4	51.6	33.1	0.5
23	Clouded; circum., cumstrat., and haze; sheet lightning in S. and S.W.; auroral light in	1.0	0.5	<del></del>		58.6	44.2	0.10
24 }	N. from 12 ^h to 16 ^h	1.0	0.4	0.4	0.0	70.8	47.0 51.1	0.14
$\frac{25}{26}$	Clouded; circum.; sheet lightning from 9 ^h to 14 ^h in S.E. and S. and W.	0.6	0.4	$0.5^{\circ}$	0.6	74.3	57.0	_
27	Clouded; circum. and cumstrat. dispersed	0.2	0.5	0.3	0.1	77.0	56.8	
28 29	Clouded; circum, and cumstrat. dispersed	$\frac{1.0}{0.8}$	$\frac{1.0}{0.3}$	$\frac{0.2}{1.0}$	$\frac{1.0}{0.0}$	79.7	54.8	0.00
<i>29</i> 30 Ղ	Clouded; circum. and cumstrat.; auroral light in N. at 10 ^h , 13 ^h , and 14 ^h -	0.8	0.7			71.8	59.3	0.03
31 \$	Clouded; encum, and come-strat.; autoral right in iv. at 10; 15; and 14			0.0	1.0	74.8	1 54 0	
	1			., .	1 0	110	54.0	
					1 0		J	
	JUNE.						34 0	
1	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder	0.9	0.7	1.0	1.0	75.3	55.7	0.18
2	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0.5	0.0	1.0	1.0	75°3 74°5	55°7 60°1	0.18
	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain		- • 1	1.0	1.0	75.3	55.7	0°18 0°13 0°28 0°17
2 3 4 5	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0.3 0.3 1.0 1.0	0.0 1.0 1.0 0.2	1.0 0.0 1.0 0.3	1.0 1.0 1.0 1.0 0.4	75°3 74°5 69°5 72°6 71°0	55.7 60.1 48.9 59.7 53.9	0°18 0°17 0°28 0°17 0°20
2 3 4 5 6 }	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0.3 0.3 1.0	0.0 1.0	1.0 0.0 1.0	1.0 1.0 1.0	75.3 74.5 69.5 72.6	55.7 60.1 48.9 59.7	0.18 0.11 0.28 0.17
$\left\{ \begin{array}{c} 2\\ 3\\ 4\\ 5\\ 6\\ 7\\ 8 \end{array} \right\}$	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0.2 0.3 1.0 1.0 1.0 	0.0 1.0 1.0 0.2 0.0	1.0 0.0 1.0 0.3 	1.0 1.0 1.0 0.4 - 0.3 0.0	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5	0°18 0°11 0°28 0°17 0°20 —
$\left\{ \begin{array}{c} 2\\3\\4\\5\\6\\7\\8\\9 \end{array} \right\}$	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0.2 0.3 1.0 1.0 1.0 	0.0 1.0 1.0 0.2 0.0 	1.0 0.0 1.0 0.3 	1.0 1.0 1.0 0.4 - 0.3 0.0 0.0	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0 68.5	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 43.5	0°18 0°11 0°28 0°17 0°20 —
2 3 4 5 6 7 8 9 10 11	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0.2 0.3 1.0 1.0 1.0 	0.0 1.0 1.0 0.2 0.0	1.0 0.0 1.0 0.3 	1.0 1.0 1.0 0.4 - 0.3 0.0	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0 68.5 71.4 76.2	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 43.5 44.5 52.6	0°18 0°11 0°28 0°17 0°20 —
2 3 4 5 6 7 8 9 10 11 12	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0.2 0.3 1.0 1.0 1.0 0.2 0.0 0.0 1.0 0.0	0.0 1.0 0.5 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.3 0.1 0.0 0.0 1.0	1.0 1.0 1.0 1.0 0.4 	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0 68.5 71.4 76.2 71.1	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 44.5 52.6 49.0	0.18 0.13 0.23 0.17 0.20 ——————————————————————————————————
2 3 4 5 6 7 8 9 10 11 12 13	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 0°2 0°0 0°0 1°0	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 1.0 0.3 	1.0 1.0 1.0 1.0 0.4 	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0 68.5 71.4 76.2 71.1 64.0	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 44.5 52.6 49.0 51.8	0°18 0°11 0°28 0°11 0°20 —
2 3 4 5 6 7 8 9 10 11 12 13 14 15	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 1°0 0°2 0°0 1°0 0°0 1°0	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.4 	1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	1.0 1.0 1.0 0.4 - 0.3 0.0 0.0 0.0 0.9 - 0.8 0.6	75·3 74·5 69·5 72·6 71·0 61·3 59·7 64·0 68·5 71·1 64·0 67·4 72·8	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 43.5 44.5 52.6 49.0 51.8 53.5 56.3	0.18 0.11 0.28 0.17 0.20 
2 3 4 5 6 7 8 9 10 11 12 13 14 15	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 1°0 0°2 0°0 1°0 0°0 1°0 0°7 0°7	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.4 	1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0 0.0 0	1.0 1.0 1.0 0.4 - 0.3 0.0 0.0 0.9 - 0.8 0.6 0.6	75·3 74·5 69·5 72·6 71·0 61·3 59·7 64·0 68·5 71·1 64·0 67·4 72·8 78·7	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 43.5 44.5 52.6 49.0 51.8 53.5 56.3 56.9	0.18 0.11 0.23 0.17 0.20 ——————————————————————————————————
2 3 4 5 6 7 8 9 10 11 12 13 14 15	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 1°0 0°2 0°0 1°0 0°0 1°0	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.4 	1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	1.0 1.0 1.0 0.4 - 0.3 0.0 0.0 0.0 0.9 - 0.8 0.6	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0 68.5 71.4 76.2 71.1 64.0 67.4 72.8 78.7 70.8 77.6	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 44.5 52.6 49.0 51.8 53.5 56.3 56.9 49.7 58.9	0.18 0.11 0.28 0.17 0.20 
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 1°0 0°2 0°0 1°0 0°0 1°0 0°7 0°5 0°9 0°4	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.4 	1.0 0.0 0.0 1.0 0.0 0.0 0.0 1.0 0.0 0.0	1.0 1.0 1.0 1.0 0.4 - 0.3 0.0 0.0 0.0 0.9 - 0.8 0.6 0.0 0.8 1.0 0.8	75:3 74:5 69:5 72:6 71:0 61:3 59:7 64:0 68:5 71:4 76:2 71:1 64:0 67:4 72:8 78:7 70:8 77:6 78:0	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 44.5 52.6 49.0 51.8 53.6 56.3 49.7 58.9 62.2	0.18 0.11 0.28 0.17 0.20 
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 1°0 0°2 0°0 0°0 1°0 0°7 0°7 0°5 0°9	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.4 	1.0 0.0 0.0 1.0 0.0 0.0 0.0 1.0 0.0 1.0 0.0 1.0	1.0 1.0 1.0 0.4 - 0.3 0.0 0.0 0.0 0.0 0.8 0.6 0.8 1.0	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0 68.5 71.4 76.2 71.1 64.0 67.4 72.8 78.7 70.8 77.6	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 44.5 52.6 49.0 51.8 53.5 56.3 56.9 49.7 58.9	0.18 0.11 0.28 0.17 0.20 ——————————————————————————————————
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 1°0 0°2 0°0 1°0 0°0 1°0 0°5 0°5 0°9 0°4 1°0	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.4 	1.0 0.0 1.0 0.0 1.0 0.0 0.0 1.0 0.0 1.0 1	1.0 1.0 1.0 1.0 0.4 	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0 68.5 71.4 76.2 71.1 64.0 67.4 72.8 78.7 70.8 77.6 81.0 62.5 58.4	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 43.5 44.5 52.6 49.0 51.8 53.5 56.3 56.3 949.7 58.9 49.7 48.7	0.18 0.11 0.28 0.17 0.20 ——————————————————————————————————
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 1°0 0°2 0°0 1°0 0°0 1°0 0°5 0°5 0°9 0°4 1°0 	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.4 	1.0 0.0 1.0 0.3 0.1 0.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.5 0.5	1.0 1.0 1.0 1.0 0.4 	75·3 74·5 69·5 72·6 71·0 61·3 59·7 64·0 68·5 71·4 76·2 71·1 64·0 67·4 72·8 78·7 70·8 78·0 81·0 62·5 58·4 70·0	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 43.5 44.5 52.6 49.0 51.8 53.5 56.3 56.9 49.7 58.9 49.7 48.7 50.2	0.18 0.11 0.28 0.17 0.20 
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	Clouded; circum, cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 1°0 0°2 0°0 1°0 0°0 1°0 0°5 0°5 0°9 0°4 1°0	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.4 	1.0 0.0 1.0 0.0 1.0 0.0 0.0 1.0 0.0 1.0 1	1.0 1.0 1.0 1.0 0.4 	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0 68.5 71.4 76.2 71.1 64.0 67.4 72.8 78.7 70.8 77.6 81.0 62.5 58.4	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 43.5 44.5 52.6 49.0 51.8 53.5 56.3 56.3 949.7 58.9 49.7 48.7	0.18 0.11 0.28 0.17 0.20 ——————————————————————————————————
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 0°2 0°0 0°0 1°0 0°7 0°7 0°0 0°5 0°9 0°4 1°0 0°0 0°0 0°0 1°0	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.7 0.8 0.3 0.7 1.0 0.8 0.0 0.0 0.0	1.0 0.0 0.0 1.0 0.0 0.0 1.0 0.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0	1.0 1.0 1.0 1.0 0.4 	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0 68.5 71.4 76.2 71.1 64.0 67.4 72.8 77.6 78.0 81.0 81.0 75.5 80.2 84.2	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 44.5 52.6 49.0 51.8 53.5 56.3 56.9 49.7 58.9 62.2 58.9 49.7 50.2 57.0 63.0 63.0	0.18 0.11 0.28 0.17 0.20 
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 0°2 0°0 1°0 0°0 1°0 0°7 0°7 0°0 0°5 0°9 0°4 1°0 0°0 0°0 0°0 1°0 1°0 1°0	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.7 0.8 0.3 0.7 1.0 0.8 0.0 0.0 0.0	1.0 0.0 1.0 0.3 	1.0 1.0 1.0 0.4 	75·3 74·5 69·5 72·6 71·0 61·3 59·7 64·0 68·5 71·4 76·2 71·1 64·0 67·4 72·8 78·7 70·8 77·6 78·0 81·0 62·5 58·4 70·0 75·5 80·2 84·2 81·0	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 44.5 52.6 49.0 51.8 53.5 56.3 56.9 49.7 58.9 62.2 58.9 49.7 48.7 50.2 57.0 63.0 63.0 59.5	0.18 0.11 0.23 0.17 0.20 ——————————————————————————————————
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	Clouded; circum., cum., and cumstrat.; heavy showers; loud thunder Clouded; circum. and haze; rain	0°2 0°3 1°0 1°0 0°2 0°0 0°0 1°0 0°7 0°7 0°0 0°5 0°9 0°4 1°0 0°0 0°0 0°0 1°0	0.0 1.0 1.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.7 0.8 0.3 0.7 1.0 0.8 0.0 0.0 0.0	1.0 0.0 0.0 1.0 0.0 0.0 1.0 0.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0	1.0 1.0 1.0 1.0 0.4 	75.3 74.5 69.5 72.6 71.0 61.3 59.7 64.0 68.5 71.4 76.2 71.1 64.0 67.4 72.8 77.6 78.0 81.0 81.0 75.5 80.2 84.2	55.7 60.1 48.9 59.7 53.9 42.5 39.1 42.5 44.5 52.6 49.0 51.8 53.5 56.3 56.9 49.7 58.9 62.2 58.9 49.7 50.2 57.0 63.0 63.0	0.18 0.11 0.23 0.17 0.20 ——————————————————————————————————

^a Taken from the lowest reading of the Standard Thermometer.

Toronto Moor	W. d. 150	E	xtent of C	Cloudy Sk	y.	Max,	Min.	
Mean Time.	Weather and Phenomena.	3	9	15	21	Therm.		Rain.
D. 1	JULY. Clear till 18h; clouded; cumstrat. and circum	0.5	0.7	0.0	0.2	° 83.1	62.6	In. 0.01
$\frac{2}{3}$	Clear till 18 ^h ; clouded; circum. and cirstrat.  Clouded till 11 ^h ; circum., cirstrat., and haze; clear	0.0	0.0 1.0 0.5	0.0	$0.2 \\ 0.7$	79·2 77·0 75·8	63·4 57·0 54·2	_
$\left\{ egin{array}{c} 4 \\ 5 \\ 6 \\ 7 \end{array} \right\}$	Clouded till 3 ^h ; circum., cirstrat., and cir.; clear; sheet lightning in S. horizon at 14 ^h - {  Clouded; cir., cirstrat., and haze; solar halo, diameter 35°	0.8 	1.0	0.5 0.0 1.0	0.0 0.4 0.9	80°1 86°8 82°3	61.5 61.8 55.7	=
8 9	Clouded till 7 ^h ; circum., cirstrat., and haze; slight rain Clear till 18 ^h ; clouded; circum., cirstrat., and haze; distant thunder and rain - Clouded; circum.; cumstrat.; heavy squall of wind and rain and hail at 0 ^h and 4 ^h ; sheet }	0.7 0.7	0.0 0.5	0.0	0.0	78 <b>·2</b> 81·4	55°1 58°6	0.02
10 { 11 }	lightning and distant thunder	$\frac{0.8}{0.6}$	1.0	1.0	0.9	81.1 94.6	67.7 68.0	0.51
12 }	Clouded till 12h; circum., cirstrat., and haze; rain; distant thunder			0.0	0.5	87.6	63.8	
13 14 15 16 17 18	Clear till 18h; clouded; circum. and cirstrat.; heavy rain and sudden squall  Clear, except circum. and cumstrat.  Clear, except circum. and cumstrat.  Clouded till 1h; circum. and cumstrat.; clear  A few clouds round horizon; circum. and cumstrat.; clear	0:8 0:9 0:7 0:2 0:4 0:2	0.9 0.0 0.2 0.0 0.2	0.0 0.2 0.0 0.2 0.2	0.8 0.6 1.0 0.1 0.2	81.8 78.6 65.7 65.3 70.6 73.8	54°9 45°5 46°0 49°1 44°5 49°0	0.04
19 }	Clear to 14 ^h ; clouded; circum. and cirstrat.	;		1.0	0.5	75.7	51.2	
20 21 22 23 24	Clear; a few circum. and cirstrat. round horizon	0.2 0.9 0.7 1.0 1.0	0.0 0.4 0.8 1.0 0.0	$\begin{bmatrix} 0.0 \\ 1.0 \\ 0.8 \\ 0.3 \\ 0.3 \end{bmatrix}$	0.5 1.0 0.2 1.0 0.0	76.5 79.2 78.0 76.8 81.8	61 · 2 57 · 0 59 · 7 55 · 5 64 · 8	- - 0.94
$\left. egin{array}{c} 25 \\ 26 \end{array} \right\}$	Clear till 17 ^h ; clouded; circum. and cumstrat.	1.0	0.7	0.0	$\frac{-}{0.2}$	$\frac{72.4}{81.5}$	$\frac{61.2}{60.5}$	_
27 28 29 30 31	Clear till 13h; clouded; cirstrat. and haze	0.0 0.6 0.7 0.6 0.2	0.0 0.0 1.0 0.0	0.8 0.8 0.4 1.0 0.0	0.4 0.6 0.4 0.5 0.0	78 ° 4 76 ° 3 77 ° 0 85 ° 0 88 ° 4a	59°1 56°7 62°4 67°7	1·49 —
	AUGUST.							
$\left.\begin{array}{c}1\\2\end{array}\right\}$	Generally clear	$\frac{0.0}{0.1}$	$\frac{0.0}{0.0}$	$\frac{0.0}{0.0}$	$\frac{0.0}{0.3}$	78°2 ^b 77°4 78°4	59°2 53°5 56°5	_
4 5 6	Clouded from 13 ^L to 15 ^h ; afterwards clear	0.0 0.2 0.2 1.0	1.0 1.0 1.0 0.0	1.0 1.0 1.0	1.0 0.0 0.0	81.8 85.4 86.4 83.0	58.5 65.0 61.4 62.0	
$\left.\begin{array}{c}8\\9\\10\end{array}\right\}$	Clouded till 11 ^h ; circum., cirstrat., and haze; rain at intervals; vivid lightning; thunder { Clouded; circum. and haze till 4 ^h ; clear	$\frac{0.7}{0.2}$	0.0	0.0 0.0 —	0.0	82.6 74.5 71.6	65.8 67.0 62.5	0.06
11 12	Generally clear	0.0 0.0	0.0 0.0	0.7 1.0	0.2 0.2	78.6 73.7	$\begin{array}{c} 53.2 \\ 52.7 \end{array}$	
$\begin{array}{c c} 13 & \{\\ 14 & \end{array}$	light in N.; lunar halo at 15h	1.0 0.4	$\begin{bmatrix} 0.0 \\ 0.2 \end{bmatrix}$	$\begin{vmatrix} 0.0 \\ 0.6 \end{vmatrix}$	$0.0 \mid$ $0.3 \mid$	81.6	66°0	0.32
$\left\{\begin{array}{c}15\\16\end{array}\right\}$	Clear; sheet lightning; auroral light in N. at 13 ^h and 15 ^h {	0.0	0.0	0.0	0.0	79°6 82°6	57°8 67°6	0.22
17 18 19 20	Generally clear	0.4 0.2 1.0 1.0	0.8 0.0 1.0 0.0	0.0 0.3 1.0 0.4	0.6 1.0 1.0 0.5	68:3 72:8 65:7 69:0	59.5 49.5 49.6 61.8	0.39
21 22 \	Generally clouded; circum.; cirstrat.; a few clear spaces	0.7	$\begin{array}{c c} 0.8 \\ 0.8 \end{array}$	0.8	1.0	$69.0 \\ 74.4$	57·3 62·4	_
23	Clouded; circum., cirstrat., and haze; rain; cleared up	0.0 0.1 0.7 1.0 0.4	0.0 0.0 0.0 0.5 0.5	0.0 1.0 0.0 0.0 0.0	0.0 0.6 0.6 0.6	73.9 77.7 69.7 73.7 72.2 76.3	56.0 55.9 52.0 55.9 57.7 61.0	0.04
29	Clouded; cir., cirstrat., and haze; storm, lightning, thunder, and rain, from 0 ^h to 3 ^h	1.0	0.8	<u>0.0</u>	0.0	77·2 77·0	59.7 58.5	0.16
30 5								

^a Taken from the highest reading of the Standard Thermometer. ^b The Max. Therm. for this month are the highest readings of the Standard Thermometer.

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Toronto		Ex	tent of Cl	loudy Sk	у.	Max.	Min.	Rain.
Mean Time.	Weather and Phenomena.	3	9	15	21	Therm.	Therm.	Kain.
b.  1 2 3 4 5 6 7 8 9 10 11 2 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	SEPTEMBER.  Clouded till 17h; circum. and cirstrat.; clear  Clouded; circum. and haze  Clouded; circum., cumstrat., and haze; rain  Clouded; circum., cumstrat., and cum.; rain  Clouded; circum., and cumstrat.  Clouded; circum. and cum. squalls, lightning, thunder, and slight rain  Clouded; circum. and cirstrat. and circum.  Clouded; circum. and cirstrat.; clear  Clouded; circum. and cirstrat.; distant thunder; sheet lightning; auroral light in N. from 9h to 11h  Clouded; circum., cirstrat., and haze; lightning, thunder, and rain; auroral light in N. from 8h to 11h  Clouded till 12h; circum., cumstrat., and haze; lightning, thunder, and rain  Clear all day  Clouded; circum., cumstrat., and haze; auroral light in N. at 11h  Clouded gircum. and cumstrat.; clear  Clouded; circum. and cumstrat.; rain  Clouded; circum. and cumstrat.; rain  Clouded; circum. and cumstrat.; rain  Clouded; circum. and cumstrat.; rain greater part of day  Clouded; circum. and cumstrat.; rain greater part of day  Clouded; circum. and cirstrat.  Clouded; circum. and cirstrat.  Clouded; circum. and cirstrat.	0'1 1'0 0'9 1'0 0'1 0'8 0'1 0'2 1'0 0'1 0'8 0'0 0'8 1'0 0'3 0'6 0'2 0'0 0'0 1'0 0'8 0'1 0'7 0'0	0.0 1.0 0.3 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	0'8 1'0 0'8	0'0 1'0 0'8	81·2 84·3 82·2 74·8 78·2 79·6 65·5 68·4 79·6 82·2 66·0 63·6 67·4 72·6 70·7 61·0 64·8 72·8 65·8 57·0 61·3 55·2 67·9	60.5 65.0 66.8 70.0 66.0 66.0 66.0 51.2 57.7 58.5 66.1 60.3 64.0 54.7 44.1 52.0 56.2 46.8 51.2 38.3 43.6 59.2 49.0 42.9 73.7 37.3 51.2 54.9	In. — 0.62 0.95 — 0.04 — 0.28 — 0.05 — 0.10 — 0.25 1.80 0.07 0.14 — —
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	Clouded; circum. and haze; rain; and haze; rain from 7h to 12h  Clouded; circum. and haze; sheet lightning and rain from 7h to 12h  Clouded; circum. and haze; sheet lightning and rain from 7h to 12h  Clouded; circum. and haze; sheet lightning and rain from 7h to 12h  Clouded; circum. and haze; sheet lightning and rain from 7h to 12h  Clouded; circum., cirstrat., and haze; rain, thunder, and lightning  Clouded till 8h; cum-strat and circum.; rain; aurora from 11h to 15h  Generally clear; aurora from 14h to 16h  Clouded; circum., cirstrat., and haze; rain  Clouded; circum., cirstrat., and haze; rain  Clouded; circum., cirstrat., and haze; rain  Clouded; circum., cirstrat., and haze; rain  Clouded; circum., cirstrat., and haze; snow  Clouded; circum., cirstrat., and haze; are frem part of day  Clouded; circum., cirstrat., and haze; a few clear spaces  Clouded; circum., and haze; clear  Clouded; circum., and haze; clear  Clouded; circum., and haze; clear  Clouded; circum., and haze; clear  Clouded; circum. and haze; clear  Clouded; circum. and haze; clear  Clouded; circum. and haze; rain  Clouded; circum. and haze; clear  Clouded; circum. and haze; clear  Clouded; circum. and haze; rain  Clouded; circum. and haze; rain  Clouded; circum. and haze; clear	1.0 0.3 0.6 	1'0 0'1 1'0 0'0 0'7 1'0 1'0 0'0 0'0 1'0 1'0 0'2 	1.0 0.1 1.0 0.0 0.0 0.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 1	1'0 0'4 	69.5 54.2 54.6 55.6 55.5	50.0 45.0 37.5 41.7 40.3 39.5 49.2 56.8 36.1 35.0 46.3 46.9 36.1 38.4 32.7 23.1 30.6 41.3 30.0 36.9 20.7 27.2 31.8 47.1 28.4 28.3 33.7	0·07

Toronto	Weather and Phenomena.	E	tent of C	loudy Sk	y.	Max.	Min.	Rain.
Mean Time.	weather and r nenomena.	3	9	15	21	Therm.		Itam.
D.	NOVEMBER.					0	0	In.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	Clouded; circum. and cirstrat.; rain at intervals Clouded all day; circum. and cumstrat. Clear Clear all day Clear  Clouded; circum. and cirstrat.; raining most part of the day Clouded; circum., cirstrat., and haze; thick fog Clouded; circum., cirstrat., and haze; slight rain Clouded; circum., cirstrat., and haze; rain most part of the day Clouded; circum., cirstrat., and haze; rain most part of the day Clouded; circum., cirstrat., and haze; slight rain Clouded; circum., cirstrat., and haze; slight rain Clouded; circum., cirstrat., and haze; slight rain Clouded; circum., cirstrat., and haze; showers Clouded all day; circum., and cirstrat.; a few clear spaces Clouded all day; rain Clouded; circum. and cirstrat.; slight rain at 9h and 11h Clouded; circum., cirstrat., and haze; sleet and rain Clouded; circum., cirstrat., and haze; snow; lunar halo at 7h and 8h Clouded; circum., cirstrat., and haze; snow; lunar halo, diameter about 45° Clouded; circum. and haze; a few particles of snow Clouded; circum. and haze; a few particles of snow Clouded; cirstrat. and haze; imperfect halo round the moon at 5h Clouded; circum. and haze; imperfect halo round the moon at 5h Clouded; circum. and haze; imperfect halo round the moon at 5h	1'0 1'0 0'0 0'0 0'1 1'0 1'0 1'0 1'0 1'0	1'0 1'0 0'0 0'0 0'0 1'0 1'0 1'0 1'0 1'0	0'4 1'0 0'0 0'0 0'0 1'0 1'0 1'0 1'0 1'0 1'0	1'0 0'4 0'0 1'0 0'7	49.0 53.3 53.1 53.0 50.0 50.4 50.9 51.2 54.4 55.6 52.6 48.6 47.2 45.4 48.0 49.2 54.0 43.0 45.4 42.2 37.0 43.0 25.0 28.6 43.3 36.6	43:3 41:2 40:5 35:7 29:7 34:1 48:7 45:3 49:5 50:5 41:8 42:6 41:2 39:0 41:7 39:4 32:1 19:3 18:0 22:0 24:7	0.29
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 22 23 24 25 27 26 27 28 29 30 31	DECEMBER.  Clouded all day; circum. and haze; rain from 14h to 17h  In general clouded; circum., cirstrat., and haze; rain Generally clouded; circum. and cumstrat.; particles of snow Clouded; cir. cum. and cumstrat.  Clouded; circum., cir., and haze; lunar halo, diameter 40°, perfect  Clouded all day; cir., cirstrat., and haze; rain from 8h to 13h  Clouded; circum., cumstrat., and haze; rain from 8h to 13h  Clouded; circum., cumstrat., and haze; snow Clouded; circum., cumstrat., and haze; snow  Clouded; circum., cumstrat., and haze; snow  Clouded till 12h; cumstrat., and haze; at intervals nearly clear, then suddenly clouded  Clouded till 12h; cumstrat., circum., and haze; slight snow  Clear; strat. in horizon Clear greater part of day; clouded at 21h Clouded till 4h; circum., and haze; clear  Clouded; circum., cirstrat., and haze  Clouded till 14h; circum. and haze; clear  Clouded till 11h; circum. and haze; clear	1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 0'7 - 0'0 1'0 0'6 1'0 - 0'0 1'0 - 1'0 - 1'0 1'0 - 1'0 1'0 1'0 1'0 1'0 1'0 1'0	1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 0'0 0	1'0 1'0 0'1 1'0 0'8 1'0 0'8 1'0 0'1 - 0'0 0'2 0'7 0'0 1'0 - 0'3 1'0 - 0'7 - 1'0 1'0 1'0 1'0 1'0	1'0 1'0 0'1 1'0 1'0 1'0 1'0 1'0 0'6 1'0 0'1 0'0 1'0 0'1 1'0 1'0 1'0 1'0 1'0	28.8 32.8 49.2 33.7 34.0 33.6 39.9 37.4 31.8 29.2 21.6 20.0 23.0 26.9 27.8 27.4 30.2 32.8 29.6 27.5 25.8 23.6 35.6 35.6 35.4 35.4 35.4 35.4 39.9	13·3 24·7 33·1 25·0 29·1 23·5 34·6 30·9 28·1 16·0 11·2 7·9 21·3 12·5 25·0 23·7 18·9 13·4 30·9 12·4 30·8 14·9 29·7 31·0 31·1 31·1 31·1 31·1 31·1 31·1 31·1	0'49

Toronto		Ex	tent of C	loudy Sk	y.	Max.	Min.	D.
Mean Time.	Weather and Phenomena.	3	9	15	21	Therm.		Rain.
D.  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 }	JANUARY.  Clouded all day; circum. and haze; rain from 3h to 11h  Clouded; dense circum., cir., and haze; lunar halo, diameter 40°, bright and perfect  Clouded to 18h; circum., cirstrat., and haze; rain and sleet; remainder clear  Partly clouded; cir. and circum.; lunar halo, diameter 35°, perfect  Clouded do 8h; circum. and cum. strat.; snow; remainder partly clear  Clouded to 8h; circum. and cum. strat.; snow; remainder partly clear  Clouded; circum., cirstrat., and haze; clear  Clouded from 13h to 23h; circum., cirstrat., and haze; remainder of the day clear  Clouded circum., cirstrat., and haze; clear from 5h to 11h  Clouded all day; circum., cirstrat., and cirstrat.; rain  Clouded all day; cumstrat. and circum.; rain; sheet lightning in S.W.  Clouded; circum. and cumstrat.; snow; clear from 5h to 12h  Clouded; circum., cirstrat., and haze  Clear; cir.; lunar halo at 6h and 7h  Partly clouded; circum., cirstrat., and haze; showers of snow  Clouded; circum., cirstrat., and haze; halo and parhelia round the sun at 3h  Partly clouded; circum., cirstrat., and haze  Generally clouded; circum. and cirstrat.; snow at 16h and 17h  Clouded; circum., cirstrat., and haze  In general clouded; circum. and haze  Clouded all day; circum. and haze  Clouded all day; circum. and haze; rain  Nearly clear; circum. and haze  Clouded all day; circum. and haze; slight snow  Clouded all day; circum., cirstrat., and haze; lunar halo at 8h, diameter about 35°  Clouded all day; circum., cirstrat., and haze; lunar halo at 8h, diameter about 35°	1.0 1.0 0.9 1.0 1.0 0.9 1.0 1.0 0.1 1.0 0.3 0.5 0.6 1.0 0.3 0.5 0.6 1.0 0.1 1.0	1'0 1'0 0'2 1'0 0'1 0'2 1'0 0'0 0'0 1'0 0'0 1'0 0'0 1'0 0'4 - 1'0 0'0 0'3 1'0 0'9 -	1'0	1.0 	\$\\ \begin{array}{c} \ \ 40.1 \\ 36.0 \\ 36.7 \\ 35.6 \\ 41.8 \\ 37.6 \\ 33.6 \\ 28.8 \\ 11.4 \\ 20.1 \\ 16.2 \\ 14.9 \\ 23.9 \\ 35.4 \\ 35.4 \\ 28.2 \\ 34.5 \\ 11.8 \\ 21.3 \\ 14.2 \\ 22.0 \\ 32.6 \\ 27.8 \\ 28.0 \\ 33.8 \\ 16.0 \\ 22.3 \\ 32.4 \\ 22.0 \end{array}\$	34.7 31.9 32.1 24.3 32.9 28.9 24.4 7.5 9.1 12.4 31.7 33.9 3.1 10.8 9.2 6.2 10.0 3.1 11.9 21.2 15.9 24.6 12.7 2.9	In. 0'40
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 3 24 25 26 27 28 3	FEBRUARY.  Generally clouded; circum., cumstrat., and haze; rain at 11 ^h and 17 ^h Clouded from 3 ^h to 15 ^h ; circum. and haze; snow from 1 ^h to 15 ^h ; clear  Generally clear  Clouded from 2 ^h to 14 ^h ; circum. and cirstrat.; remainder of the day clear  Clear to 11 ^h ; remainder of the day clouded; circum. and haze  Mostly clouded; circum., cirstrat., and haze; snow from 10 ^h to 14 ^h Generally clouded; cumstrat. and circum.  Mostly clouded; cumstrat. and circum.; snow from 11 ^h to 15 ^h Generally clouded; cumstrat., circum., and haze; snow snow  Clouded all day; circum. and cumstrat.; snow from 12 ^h to 15 ^h Mostly clouded; circum. and cumstrat.; snow from 12 ^h to 15 ^h Clouded all day; circum. and haze; snow; hail; rain from 19 ^h to 23 ^h Clouded all day; circum. and haze; snow; hail; rain from 19 ^h to 23 ^h Clouded all day; circum., cirstrat., and haze  Clouded all day; circum., cirstrat., and haze  Clouded all day; cirstrat., circum., and haze; snow occasionally  Clouded all day; cirstrat., circum., and haze; snow occasionally  Clouded all day; cirstrat., circum., and haze; snow occasionally  Clouded all day; circum. and haze; snow from 13 ^h to 17 ^h Generally clouded; circum. and haze; snow from 13 ^h to 17 ^h Generally clouded; circum. and haze; snow from 13 ^h to 17 ^h Generally clouded; circum. and haze; snow from 13 ^h to 17 ^h Clouded all day; circum. and haze; snow from 13 ^h to 17 ^h Generally clouded; circum. and haze; snow from 13 ^h to 17 ^h Clouded all day; circum. and haze; snow from 13 ^h to 17 ^h Clouded all day; circum. and haze; snow from 13 ^h to 17 ^h Generally clouded; circum. and haze; snow from 13 ^h to 17 ^h Clouded all day; circum. and haze; snow from 13 ^h to 17 ^h Clouded all day; circum. and haze; snow from 13 ^h to 17 ^h Clouded all day; circum. and haze; snow from 13 ^h to 17 ^h Clouded all day; circum.	1.0 0.5 1.0 0.0 1.0 0.0 1.0 1.0 1.0 1.0 1.0 1.0	1'0 1'0 1'0 0'0 0'5 0'0	1.0 0.0 1.0 0.0 1.0 0.0 1.0 1.0	0.6 1.0 0.1 0.0 0.0 0.8 0.3 1.0 1.0 0.2 1.0 1.0 1.0 1.0 1.0 0.3 0.8 0.1 1.0 0.7	24·0 32·4 40·9 37·6 23·4 21·4 27·8 29·0 35·4 32·2 35·0 21·8 26·4 25·2 29·6 29·2 24·0 31·9 34·2 32·3 26·0 20·8 20·8 22·4 25·9 27·9 33·0	6:1 23:1 37:1 12:2 8:1 11:1 17:7 19:1 26:6 20:9 10:8 10:9 7:8 16:8 22:5 11:1 13:4 13:1 26:3 22:1 15:1 14:7 0:9 15:7 7:0 25:3 26:1	0.55

Toronto Mean	Weather and Phenomena.	E	xtent of (	Cloudy Sl	ку.	Max.	Min.	Rain
Time.	o eather and I nenomena.	3	9	15	21	Therm.		Nain.
D.	MARCH.					0	0	In.
1	Generally clouded; circum. and cumstrat.; light snow	1.0	1.0	1.0	0.5	28.3	19.3	-
$\frac{2}{3}$	Generally clouded; circum. and cumstrat Clouded till 8h; cir., cir., circum., and cumstrat.; remainder of the day clear	$0.8 \\ 0.4$	$\frac{0.0}{1.0}$	0.0	0.1	$\begin{vmatrix} 30.5 \\ 30.2 \end{vmatrix}$	18.5	
4	Clouded to 11 ^h ; circum., cirstrat., and haze; remainder of the day mostly clear	0.8	0.2	0.0	0.1	$\frac{30.2}{35.2}$	$\frac{20.3}{12.9}$	_
5	Clear to 4h; remainder of the day clouded; circum., cirstrat., and cumstrat.	0.1	1.0	1.0	1.0	32.2	10.5	_
$\left. egin{array}{c} 6 \\ 7 \end{array}  ight\} \left[$	Clouded till 7h; circum, cir., and haze; remainder of the day nearly clear; halos and	1.0	0.5			30.3	23.9	
8	parhelia round the sun at 4 p.m. of 6 th	0.0	0.0	0.0	0.8	$\begin{vmatrix} 35.7 \\ 38.3 \end{vmatrix}$	32'1 24'4	0.10
9	Clouded all day; circum., cumstrat., and haze	1.0	1.0	1.0	1.0	35.4	18.3	
10	Nearly clear to 20h; remainder of the day clouded; circum., cirstrat., and haze	0.0	0.0	0.5	1.0	25.3	20.8	
11 12	Clouded to 6 ^h ; cumstrat., circum., and haze; clear  Generally clear; clouded from 5 ^h to 14 ^h ; circum. and haze	$\frac{0.1}{1.0}$	0.0	0.0	0.1	36.3	14.7	
13		0.0	0.0	0.0	0.0	23.1	$\frac{5.6}{10.5}$	_
14	Clear to 12h; remainder overcast; circum. and haze			1.0	0.4	26.2	7.9	
15 16	Mostly clear; some circum, round horizon	0.4	0.0	$0.0 \\ 0.0$	0.4	30.3	7:2	
17	Clear to 2 ^h ; remainder clouded; cir., cirstrat., and haze; solar halo at 3 ^h , diameter 35°	0.4 + 0.4	0.8	0.9	$\frac{1.0}{0.0}$	24.1 $23.7$	$\frac{10.5}{12.5}$	
18	Clear all day	0.0	0.0	0.0	0.0	34.3	26.2	
19 {	Clear at 9h; remainder of the day clouded; circum. and haze; brilliant aurora at night;	0.7	0.0	1.0	1.0	42.3	24.1	
20	Clouded all day; circum., cirstrat., and haze; slight rain most of the day	1.0	1.0			36.2	25.1	0.22
$\begin{bmatrix} 21 \\ 99 \end{bmatrix}$	Clouded all day; circum. and haze; slight rain	1:0		1.0	1.0	39.2	18.9	0.00
$\begin{bmatrix} 22 \\ 23 \end{bmatrix}$	Generally clouded; circum, and haze; snow from 8 ^h to 11 ^h	$\frac{1.0}{1.0}$	1.0	$\frac{1.0}{1.0}$	0.1	$\frac{30.7}{32.9}$	23°2 31°4	0.50
24	Partly clouded; circum., cirstrat., and haze; lunar halo at 9h, diameter 40°	0.4	0.9	1.0	0.4	40.9	23.5	
25	Clouded all day; circum., cumstrat., and haze Generally clouded; circum., cumstrat., cir., and haze	1.0	1.0	1.0	1.0	37.9	30.0	
26 27		$\begin{vmatrix} 0.5 \\ 0.6 \end{vmatrix}$	0.0	0.2	0.6	43.6 36.6	30.1	
00 ()	Partly clouded and clear alternately; cir., circum., and haze		_	0.7	0.0	26.1	17.1	
29	Clear till 4 ^h ; remainder clouded; cir., circum., and haze Clouded to 20 ^h ; circum., cirstrat., and haze; heavy storm; thunder; lightning; snow from	0.1	1.0	1.0	1.0	35.4	30.0	
30 {	5h to 16h	1.0	1.0	1.0	0.1	43.9	23.0	
31	Clear all day; some cir. and strat.	0.0	0.0	0.0	0.3	27.9	14.2	
	APRIL.							
$\begin{bmatrix} 1 \\ 2 \end{bmatrix}$	Clouded all day; circum., cir., and haze; snow from 6h to 12h	1.0	1.0	1.0	1.0	26.6 32.5	$\frac{9.3}{29.0}$	
3 }	Clouded to 7 ^h and from 20 ^h to 23 ^h ; cir., circum., and haze; remainder of the day clear -	1.0	0.0			37.2	27.7	
42 )	Clouded all day; cir., cirstrat., and haze; rain at 16 ^h and 17 ^h	$\frac{1.0}{1}$	1.0	$\frac{1.0}{0.0}$	1.0	42°1 40°5	$\frac{28.1}{30.9}$	
6	Generally clouded; cir., circum., and haze; rain occasionally	0.7	0.7	1.0	1.0	41.4	35.0	0.07
7	Clear to 14 ^h ; remainder clouded; cirstrat., circum., and haze; brilliant aurora at night	0.0	0.0	0.9	1.0	49.7	39.7	
8 {	Clouded till 12h; cir., cirstrat., circum., and haze; solar halo at 2h, diameter 30°, perfect; rain from 8h to 10h; auroral light in N. at 11h; clear	1.0	1.0	0.0	0.0	55.1	33.7	
	Partially clouded; cirstrat. and circum.	0.6	0.3	1.0	0.2	59.5	33.7	
$\{10, 10, 10, 10, 10, 10, 10, 10, 10, 10, $	Clear at 9h; remainder clouded; circum., cumstrat., and haze	0.9	0.0		_	45.9	36.7	
11 J 12	Partially clouded; circum., cirstrat., and haze	$\frac{0.8}{1}$	0.3	$\begin{vmatrix} 1.0 \\ 0.2 \end{vmatrix}$	$\frac{0.0}{0.8}$	48.8 41.3	27.7 30.3	
13	Clear to 6h; remainder of the day clouded; cirstrat. and haze	0.0	0.8	1.0	1.0	48.3	26.2	
	Generally clouded; cirstrat. and haze; light rain from 9 ^h to 11 ^h Clouded to 7 ^h ; circum. and cumstrat.; remainder nearly clear	0.3	1.0	0.6	1.0	46.7	29.7	0.04
	Generally clouded; circum., cirstrat., and haze	$0.0 \\ 0.9$	0.1	0.0	$\begin{bmatrix} 0.1 \\ 0.7 \end{bmatrix}$	45.9 38.1	$\begin{bmatrix} 29.7 \\ 24.2 \end{bmatrix}$	
17	Clear from 6h to 14h; remainder of the day clouded; cir., circum, and haze	1.0	0.0			39.8	30.9	
18 )	Clouded and clear alternately; cirstrat. and haze; auroral light in N. from 13h to 16h		0.8	1.0	1.0	35.4	17.4	
20	Clouded all day; circum., cirstrat., and haze; rain; thunder occasionally -	0.1	1.0	$\begin{bmatrix} 1.0 \\ 0.0 \end{bmatrix}$	$\frac{1.0}{1.0}$	$\frac{31.0}{45.5}$	21.4   29.5	0.12
21	Generally clouded; circum., cirstrat., and haze; rain and thunder from 10h to 16h	1.0	0.4	1.0	1.0	45.8	40.7	0.76
	Clouded all day; cirstrat., cir., and circum.; rain nearly all day  Clouded to 3h; circum. and cumstrat.; remainder clear	0.4	$\begin{bmatrix} 0.0 \\ 1.0 \end{bmatrix}$	0.0	1.0	65.1	47.9	1.00
24	Clear to 11 ^h ; remainder clouded; circum., cirstrat., and cumstrat.	0.0	0.0	_	0.0	$\frac{51.9}{45.5}$	35.1 28.1	0.07
25	· · · · · · · · · · · · · · · · · · ·			0.8	1.0	45.1	27.9	
	Mostly clouded; cir., cirstrat., and haze  Nearly clear all day	0.1	$0.0 \\ 0.8$	$\begin{vmatrix} 0.0 \\ 0.8 \end{vmatrix}$	$0.4 \\ 0.5$	51.2	42.1	-
	Clouded all day; cirstrat., circum., and haze; sheet lightning and thunder to 7h; rain		ŀ	j	-	59.5	40.7	0:45
20 {	from 7 ^h to 9 ^h , and at 12 ^h Clouded; circum., cirstrat., and haze; rain at 3 ^h	1.0	1.0	1.0	1.0	44.1	23.4	0.45
	oroute, en-cum, en-suat, and naze; rain at 3"	1.0	0.7	1.0	0.7	42.7	34'1	0.33
30 {	Clear from 10 ^h to 15 ^h ; remainder clouded; circum., cir., and cumstrat.; solar halo at 21 ^h , 7	0.8	0.8	0.0	0.8	44.6	35.2	

Foronto Mean	Weather and Phenomena.	Ex	ttent of C	lloudy Sk	xy.	Max.	Min.	Rain.
Time.	Westers and Phenomena.	3	9	15	21	Therm.	Therm.	Kain.
D.	MAY.					0	0	In.
$\left\{ egin{array}{c} 1 \ 2 \end{array}  ight\}$	Generally clouded; circum. and cirstrat.; slight rain from 9h	1.0	1.0	0.8	$\frac{0.9}{-}$	47.7	26.7	0.02
3	Partly clear to 6 ^h ; remainder clear	0.6	0.1	0.0	0.0	40.1	34.5 35.5	0.04
4 5	Clouded to 3h; circum. and cumstrat.; remainder of the day clear	1.0	0.0	0.0	0.0	48.3	35.0	_
5	Clear all day	0.0	0.0	0.0	0.0	54.3	32.1	-
$\frac{6}{7}$	Clear all day  Clear to 2 ^h ; clouded; cir., cirstrat., and haze; auroral light in N. from 10 ^h to 13 ^h	$0.0 \\ 0.4$	0.6	$\frac{1.0}{0.0}$	$0.0 \\ 0.0$	60.6	$\begin{array}{c} 35.3 \\ 37.2 \end{array}$	
8 }	Clouded to 12 ^h ; circum., cir., and haze; clear	1.0	1.0			$\frac{62}{62} \cdot \frac{4}{1}$	$\frac{37}{48} \cdot \frac{2}{9}$	_
9 ∫				0.0	0.0	64.3	46.8	_
10	Clouded all day; cir. cum., and haze; rain from 9 ^h to 13 ^h Generally clouded; circum. and haze; slight rain	1.0	1.0	1.0	1.0	56.7	45.2	0.32
$\frac{11}{12}$	Clouded to 15 ^h ; cirstrat. and haze; drizzling rain	$0.0 \\ 0.0$	$\frac{1.0}{1.0}$	$\frac{0.4}{0.4}$	$\frac{0.7}{0.0}$	61.4	52°3 53°9	0.09
13	Clear all day	0.0	0.0	0.0	0.0	66.1	53.6	0.52
14	Partly clouded to 3h; cir. and haze; remainder hazy	0.3	0.0	0.0	0.0	64.1	47.7	
15	Clear all day •	0.0	0.0	0:0		61.5	41.7	
16 ∫ 17	Clear all day	$\frac{0.0}{-}$	0.0	$0.0 \\ 0.0$	$0.0 \\ 0.0$	64.5	$\begin{vmatrix} 42.2 \\ 43.2 \end{vmatrix}$	
18	Clear to 12 ^h ; overcast; cir. and haze	0.0	0.0	1.0	1.0	65.2	44.1	_
19	Partly clouded from 8h to 16h; cir., cir., strat., and haze; clear	0.0	0.6	0.7	0.0	69.5	48.2	_
$\frac{20}{21}$	Clear to 16 ^h ; clouded; cir. and haze	$\begin{vmatrix} 1.0 \\ 0.0 \end{vmatrix}$	$\frac{1.0}{0.0}$	$\frac{1.0}{0.0}$	$\frac{0.8}{1.0}$	$\begin{vmatrix} 65.7 \\ 62.7 \end{vmatrix}$	48.7	
$\frac{21}{22}$	Clouded all day; cir. and haze; rain from 12h to 23h	1.0	1.0	_		63.0	43.5	0.18
23 S	· (1)	-		1.0	1.0	68.5	51.2	0.23
24	Clouded to 7 ^h ; circum. and cirstrat.; partly clear  Clouded to 20 ^h ; circum., cirstrat., and haze; light rain; clear	1.0	0.4	0.5	0.2	60.8	51.5	
$\begin{array}{c} 25 \\ 26 \end{array}$	Clear all day	$\frac{0.1}{1.0}$	$\frac{0.0}{1.0}$	$\frac{0.0}{0.8}$	0.0	64.4	$\begin{vmatrix} 47.9 \\ 37.7 \end{vmatrix}$	0.25
$\frac{20}{27}$	Nearly clear all day	0.0	0.0	0.4	0.7	57.8	35.9	_
28	Clouded; cir., cirstrat., and circum.	0.4	0.8	1.0	1.0	59.2	42.3	
	0. 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1						55.5	0.11
29 }	Clouded all day; circum., cirstrat., and haze; thunder; lightning; constant rain from	1.0	1.0	1:0	1:0	72.1	1	
	13 ^h to 23 ^h Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h	1.0	1.0	1.0	1.0	65.4	47.9 43.6	0.02
29 30 31	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum.	1.0	1·0 0·2	0.0	0.6	65.4 58.9 48.2 62.0	47.9	0.05
29 30 31 1 2 3	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum.	1.0	1.0 0.2 1.0	0.0 0.0 1.0	0.6 1.0 0.6 1.0	65.4 58.9 48.2 62.0 62.6	43.6 43.6 43.8 49.4 45.1	0.09
29 30 31	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h -  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum	1.0	1·0 0·2	0.0	0.6	65.4 58.9 48.2 62.0 62.6 62.1	43.8 43.4 45.1 52.7	0.08
29 30 31 1 2 3 4 5 6 }	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h -  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum	1.0 0.1 1.0 0.2 0.1	1.0 0.2 1.0 0.0 0.0	0.0 0.0 1.0 0.0 0.0 1.0	0.0 0.0 0.6 1.0 0.6 1.0	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7	43.8 49.4 45.1 52.7 36.7 49.7	0.05
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum	1.0 0.1 1.0 0.2 0.1 —	1.0 0.2 1.0 0.0 0.0 -	1.0 0.0 1.0 0.0 1.0 0.0	0.0 1.0 0.0 1.0 0.0 1.0	48.2 62.0 62.6 62.1 62.4 63.7 64.4	43.8 49.4 45.1 52.7 36.7 49.7 41.5	0.05 0.60 0.14
29 30 31 1 2 3 4 5 6 7 8 {	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h -  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum	1'0 0'1 1'0 0'2 0'1 0'2 1'0	1.0 0.2 1.0 0.0 0.0	0.0 0.0 1.0 0.0 0.0 1.0	0.0 0.0 0.6 1.0 0.6 1.0	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7	43.8 49.4 45.1 52.7 36.7 49.7	0.08 0.60 0.55 0.14
29 30 31 1 2 3 4 5 6 7 8 {	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum	1'0 0'1 1'0 0'2 0'1 - 0'2 1'0 0'4	1.0 0.2 1.0 0.0 0.0 0.0 1.0 0.4	1.0 1.0 1.0 0.0 0.0 0.0 1.0	1.0 1.0 1.0 1.0	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8	43.8 43.4 45.1 52.7 49.7 41.5 53.1 53.9	0.052 0.14 0.052
29 30 31 1 2 3 4 5 6 7 8 {	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum	1'0 0'1 1'0 0'2 0'1 0'2 1'0 0'4 1'0	1.0 0.2 1.0 0.0 0.0 0.0 1.0 0.4 1.0	1.0 1.0 1.0 0.0 0.0 1.0 0.0	1.0 1.0 0.6 1.0 0.6 1.0 	48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2	43.8 43.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7	0.052 0.14 0.02 0.16
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum.  Generally clouded; slight rain occasionally  Nearly clear to 20 ^h ; clouded; circum.  Mostly clear	1'0 0'1 1'0 0'2 0'1 - 0'2 1'0 0'4	1.0 0.2 1.0 0.0 0.0 0.0 1.0 0.4	1.0 1.0 1.0 0.0 0.0 0.0 1.0	1.0 1.0 1.0 1.0	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8	43.8 43.4 45.1 52.7 49.7 41.5 53.1 53.9	0.052 0.14 0.052 0.14
29 30 31 1 2 3 4 5 6 7 8 { 9 10 11	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h. Clear to 20h; remainder clouded; circum.  Generally clouded; slight rain occasionally  Nearly clear to 20h; clouded; circum.  Mostly clear  Mostly clear to 3h; remainder clouded; circum., cirstrat., and haze  Clouded all day; cumstrat., circum., and haze; slight rain from 10h to 12h; sheet }  lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10h to 13h  Mostly clouded; circum., cirstrat., and haze; rain  Clouded to 17h; cumstrat., circum., and haze; remainder clear; constant rain from 6h to 11h  Mostly clear to 12h; clouded; circum. and haze; auroral light at 10h and 11h; rain from 19h to 23h	1.0 0.1 1.0 0.2 0.1 	1.0 0.2 1.0 0.0 0.0 0.0 1.0 0.4 1.0	0.0 1.0 1.0 0.0 1.0 1.0 1.0	1.0 1.0 0.6 1.0 0.6 1.0 	48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4	43.8 43.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0	0.05 0.60 0.14 0.02 0.16 0.21
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum.  Generally clouded; slight rain occasionally  Nearly clear to 20 ^h ; clouded; circum.  Mostly clear	1.0 0.1 1.0 0.2 0.1 	1.0 0.2 1.0 0.0 0.0 0.0 1.0 0.4 1.0 1.0 0.0	0.0 0.0 0.0 1.0 0.0 1.0 0.0	1.0 1.0 0.6 1.0 0.6 1.0 1.0 1.0 0.7 0.7	48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7	43.8 49.4 45.1 52.7 36.7 49.7 41.5 53.1 53.9 60.7 57.0 46.6	0.03 0.03 0.14 0.03 0.16 0.21 0.18
29 30 31 1 2 3 4 5 5 6 7 8 { 9 10 11 12 13 14 } 14 { 15	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h Clear to 20h; remainder clouded; circum.  Generally clouded; slight rain occasionally  Nearly clear to 20h; clouded; circum.  Mostly clear	1.0 0.1 1.0 0.2 0.1 	1'0 0'2 1'0 0'0 0'0 - 1'0 0'4 1'0 0'0	0.0 0.0 0.0 1.0 1.0 1.0 1.0 0.5 -	1.0 1.0 0.6 1.0 0.6 1.0 1.0 1.0 0.7 0.0 1.0	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7 66.6	43.8 49.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7	0.05 0.60 0.14 0.16 0.16 0.16
29 30 31 1 2 3 4 5 5 6 7 8 { 9 10 11 12 13 14 } 14 { 15 16	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h Clear to 20h; remainder clouded; circum.  Generally clouded; slight rain occasionally  Nearly clear to 20h; clouded; circum.  Mostly clear  Nearly clear to 3h; remainder clouded; circum., cirstrat., and haze  Clouded all day; cumstrat., circum., and haze; slight rain from 10h to 12h; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10h to 13h  Mostly clouded; circum., cirstrat., and haze; rain  Clouded to 17h; cumstrat., circum., and haze; remainder clear; constant rain from 6h to 11h  Mostly clear to 12h; clouded; circum. and haze; auroral light at 10h and 11h; rain from 19h to 23h  Clear from 9h to 12h; remainder clouded; circum. and cumstrat.; light rain at 1h and from 18h to 22h  Clouded and clear alternately; circum., cumstrat., and cirstrat.	1.0 0.1 1.0 0.2 0.1 	1'0 0'2 1'0 0'0 1'0 0'4 1'0 0'0 0'0 0'0 0'0 0'0 0'0	0.0 0.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 0	1.0 1.0 1.0 0.6 1.0 0.6 1.0 1.0 0.7 0.0 1.0 1.0 0.0 0.0	48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7 66.6 55.0 54.6 58.6	43.8 49.4 45.1 52.7 36.7 49.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7	0.03 0.03 0.14 0.03 0.16 0.21 0.18
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h Clear to 20h; remainder clouded; circum.  Generally clouded; slight rain occasionally  Nearly clear to 20h; clouded; circum.  Mostly clear	1.0 0.1 1.0 0.2 0.1 	1'0 0'2 1'0 0'0 0'0 1'0 0'0 0'0 0'0 0'0 0'0 0'0	0.0 0.0 0.0 1.0 0.0 1.0 1.0 0.5 	1.0 1.0 1.0 0.6 1.0 0.6 1.0 1.0 1.0 0.7 0.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0	48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7 66.6 55.0 54.6 56.8	43.8 43.8 49.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2	0.05 0.16 0.16 0.16 0.16 0.16 0.16 0.16
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h. Clear to 20h; remainder clouded; circum.  Generally clouded; slight rain occasionally Nearly clear to 20h; clouded; circum.  Mostly clear  Nearly clear to 3h; remainder clouded; circum., cirstrat., and haze Clouded all day; cumstrat., circum., and haze; slight rain from 10h to 12h; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10h to 13h  Mostly clear to 12h; clouded; circum., and haze; remainder clear; constant rain from 6h to 11h  Mostly clear to 12h; clouded; circum. and haze; auroral light at 10h and 11h; rain from 19h to 23h  Clear from 9h to 12h; remainder clouded; circum. and cumstrat.; light rain at 1h and from 18h to 22h  Clouded and clear alternately; circum., cumstrat., and cirstrat.  Nearly clear to 20h; remainder clouded; circum. and cumstrat.	1.0 0.1 1.0 0.2 0.1 	1'0 0'2 1'0 0'0 1'0 0'4 1'0 0'0 0'0 0'0 0'0 0'0 0'0	0.0 0.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 1.0 0.0 0	1.0 1.0 1.0 0.6 1.0 0.6 1.0 1.0 0.7 0.0 1.0 1.0 0.0 0.0	48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7 66.6 55.0 54.6 56.8 67.9	43.8 43.8 49.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2 42.7	0.052 0.14 
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h Clear to 20h; remainder clouded; circum.  Generally clouded; slight rain occasionally Nearly clear to 20h; clouded; circum.  Mostly clear  Nearly clear to 3h; remainder clouded; circum., cirstrat., and haze  Clouded all day; cumstrat., circum., and haze; slight rain from 10h to 12h; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10h to 13h  Mostly clouded; circum., cirstrat., and haze; rain  Clouded to 17h; cumstrat., circum., and haze; remainder clear; constant rain from 6h to 11h  Mostly clear to 12h; clouded; circum. and haze; auroral light at 10h and 11h; rain from 19h to 23h  Clear from 9h to 12h; remainder clouded; circum. and cumstrat.; light rain at 1h and from 18h to 22h  Clouded and clear alternately; circum., cumstrat., and cirstrat.  Nearly clear all day  Clear to 20h; remainder clouded; circum. and cumstrat.  Clouded all day; circum. and cumstrat.; rain from 4h to 9h  Clouded to 3h; cirstrat. and haze; remainder mostly clear; thunder; showers at 0h  Clouded to 3h; cirstrat. and haze; remainder mostly clear; thunder; showers at 0h	1'0 0'1 1'0 0'2 0'1 0'2 1'0 0'4 1'0 0'1 1'0 0'2 0'5 0'0 1'0 0'8	1'0 0'2 1'0 0'0 0'0 1'0 1'0 0'0 0'0 0'0 0'0 0'0	0.0 0.0 0.0 0.0 1.0 0.0 1.0 1.0 0.5 	1.0 1.0 1.0 0.6 1.0 0.0 1.0 1.0 0.7 0.0 1.0 0.0 0.0 0.0 0.8 1.0	48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7 66.6 55.0 54.6 56.8	43.8 43.8 49.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2	0.052 0.14 0.02 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h -  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h Clear to 20 ^h ; remainder clouded; circum.  Generally clouded; slight rain occasionally Nearly clear to 20 ^h ; clouded; circum.  Mostly clear  Clouded all day; cumstrat., circum., and haze; slight rain from 10 ^h to 12 ^h ; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10 ^h to 13 ^h Mostly clouded; circum., cirstrat., and haze; remainder clear; constant rain from 6 ^h to 11 ^h Mostly clear to 12 ^h ; clouded; circum., and haze; remainder clear; constant rain from 6 ^h to 11 ^h Mostly clear to 12 ^h ; remainder clouded; circum. and cumstrat.; light rain at 1 ^h and from 18 ^h to 23 ^h Clear from 9 ^h to 12 ^h ; remainder clouded; circum. and cumstrat.; light rain at 1 ^h and from 18 ^h to 22 ^h Clouded and clear alternately; circum., cumstrat., and cirstrat.  Nearly clear all day Clear to 20 ^h ; remainder clouded; circum. and cumstrat.  Clouded all day; circum. and cumstrat.; rain from 4 ^h to 9 ^h Clouded to 3 ^h ; cirstrat. and haze; remainder mostly clear; thunder; showers at 0 ^h Generally clouded; circum. and haze; rain at 1 ^h ; lightning	1.0 0.1 1.0 0.2 0.1 	1'0 0'2 1'0 0'0 0'0 1'0 0'0 0'0 0'0 0'0 0'0 0'0	0.0 0.0 0.0 0.0 1.0 0.0 1.0 1.0 0.5 1.0 0.8 0.0 0.0 1.0	1.0 1.0 1.0 0.6 1.0 0.0 1.0 1.0 0.7 0.0 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7 66.6 55.0 54.6 56.8 67.9 65.5	43.8 43.8 49.4 45.1 52.7 36.7 49.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2 42.7 56.0	0.052 0.14 0.16 0.16 0.16 0.18 0.16
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h Clear to 20h; remainder clouded; circum.  Generally clouded; slight rain occasionally Nearly clear to 20h; clouded; circum.  Mostly clear  Nearly clear to 3h; remainder clouded; circum., cirstrat., and haze  Clouded all day; cumstrat., circum., and haze; slight rain from 10h to 12h; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10h to 13h  Mostly clouded; circum., cirstrat., and haze; rain  Clouded to 17h; cumstrat., circum., and haze; remainder clear; constant rain from 6h to 11h  Mostly clear to 12h; clouded; circum. and haze; auroral light at 10h and 11h; rain from 19h to 23h  Clear from 9h to 12h; remainder clouded; circum. and cumstrat.; light rain at 1h and from 18h to 22h  Clouded and clear alternately; circum., cumstrat., and cirstrat.  Nearly clear all day  Clear to 20h; remainder clouded; circum. and cumstrat.  Clouded all day; circum. and cumstrat.; rain from 4h to 9h  Clouded to 3h; cirstrat. and haze; remainder mostly clear; thunder; showers at 0h  Clouded to 3h; cirstrat. and haze; remainder mostly clear; thunder; showers at 0h	1'0 0'1 1'0 0'2 0'1 0'2 1'0 0'4 1'0 0'1 1'0 0'2 0'5 0'0 1'0 0'8	1'0 0'2 1'0 0'0 0'0 1'0 1'0 0'0 0'0 0'0 0'0 0'0	0.0 0.0 0.0 0.0 1.0 0.0 1.0 1.0 0.5 	1.0 1.0 1.0 0.6 1.0 0.0 1.0 1.0 0.7 0.0 1.0 0.0 0.0 0.0 0.8 1.0	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7 66.6 55.0 54.6 56.8 67.9 65.5 67.1	43.8 43.8 49.4 45.1 52.7 36.7 49.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2 42.7 56.0 48.7	0.052 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h Clear to 20h; remainder clouded; circum.  Generally clouded; slight rain occasionally Nearly clear to 20h; clouded; circum.  Mostly clear  Nearly clear to 3h; remainder clouded; circum., cirstrat., and haze  Clouded all day; cumstrat., circum., and haze; slight rain from 10h to 12h; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10h to 13h  Mostly clouded; circum., cirstrat., and haze; remainder clear; constant rain from 6h to 11h  Mostly clouded to 12h; clouded; circum. and haze; remainder clear; constant rain from 6h to 11h  Mostly clear to 12h; clouded; circum. and haze; auroral light at 10h and 11h; rain from 19h to 23h  Clear from 9h to 12h; remainder clouded; circum. and cumstrat.; light rain at 1h and from 18h to 22h  Clouded and clear alternately; circum., cumstrat., and cirstrat.  Nearly clear all day  Clear to 20h; remainder clouded; circum. and cumstrat.  Clouded and; circum. and cumstrat.; rain from 4h to 9h  Clouded to 3h; cirstrat. and haze; remainder mostly clear; thunder; showers at 0h  Generally clouded; circum., cirstrat., and haze; remainder clear; thunder; showers occasionally  Generally clouded; circum., cirstrat., and haze; remainder clear; thunder; showers	1.0 0.1 1.0 0.2 0.1 	1'0 0'2 1'0 0'0 0'0 1'0 0'0 0'0 0'0 0'0 0'0 0'0	0.0 0.0 0.0 0.0 1.0 0.0 1.0 0.2 0.0 1.0 0.5 	1.0 1.0 1.0 0.6 1.0 0.6 1.0 1.0 1.0 0.7 0.0 1.0 0.0 0.8 1.0 0.2 1.0	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.6 55.0 54.6 56.8 67.9 65.5 67.1 60.2	43.8 49.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2 42.7 56.0 48.7 50.2	0.052 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h. Clear to 20h; remainder clouded; circum.  Generally clouded; slight rain occasionally Nearly clear to 20h; clouded; circum.  Mostly clear  Nearly clear to 3h; remainder clouded; circum., cirstrat., and haze Clouded all day; cumstrat., circum., and haze; slight rain from 10h to 12h; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10h to 13h  Mostly clouded; circum., cirstrat., and haze; remainder clear; constant rain from 6h to 11h  Mostly clear to 12h; clouded; circum. and haze; auroral light at 10h and 11h; rain from 19h to 23h  Clear from 9h to 12h; remainder clouded; circum. and cumstrat.; light rain at 1h and from 18h to 22h  Clouded and clear alternately; circum., cumstrat., and cirstrat.  Nearly clear all day  Clear to 20h; remainder clouded; circum. and cumstrat.  Clouded all day; circum. and cumstrat.; rain from 4h to 9h  Clouded to 3h; cirstrat. and haze; remainder mostly clear; thunder; showers at 0h  Generally clouded; circum., and haze; rain at 1h; lightning  Clouded to 11h; circum., cirstrat., and haze; remainder clear; thunder; showers occasionally  Generally clear  Clear to 12h; remainder clouded; circum.; cirstrat.	1.0 0.1 1.0 0.2 0.1 	1'0 0'2 1'0 0'0 0'0 1'0 1'0 0'4 1'0 1'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'7 0'1 0'0	0.0 0.0 0.0 0.0 1.0 0.0 1.0 1.0 0.5 1.0 0.8 0.0 0.0 1.0 0.2 0.2 0.2 0.0 0.0	1.0 1.0 1.0 0.6 1.0 0.6 1.0 1.0 1.0 0.7 0.0 1.0 0.0 0.8 1.0 0.2 1.0 0.1 0.2 1.0	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7 66.6 55.0 54.6 56.8 67.9 65.5 67.1 60.2 67.0 68.4 71.1	43.8 49.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2 42.7 56.0 48.7 50.2 49.0 50.1 50.7	0.05 0.60 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16
29 } 30 } 31	Clear to 20 ^h ; cir. and haze; constant rain to 16 ^h ; thunder and lightning at 13 ^h and 14 ^h .  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7 ^h . Clear to 20 ^h ; remainder clouded; circum.  Generally clouded; slight rain occasionally Nearly clear to 20 ^h ; clouded; circum.  Mostly clear  Nearly clear to 3 ^h ; remainder clouded; circum., cirstrat., and haze  Clouded all day; cumstrat., circum., and haze; slight rain from 10 ^h to 12 ^h ; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10 ^h to 13 ^h Mostly clouded; circum., cirstrat., and haze; rain  Clouded to 17 ^h ; cumstrat., circum., and haze; remainder clear; constant rain from 6 ^h to 11 ^h Mostly clear to 12 ^h ; clouded; circum. and haze; auroral light at 10 ^h and 11 ^h ; rain from 19 ^h to 23 ^h Clear from 9 ^h to 12 ^h ; remainder clouded; circum. and cumstrat.; light rain at 1 ^h and from 18 ^h to 22 ^h Clouded and clear alternately; circum., cumstrat., and cirstrat.  Nearly clear all day  Clear to 20 ^h ; remainder clouded; circum. and cumstrat.  Clouded to 3 ^h ; cirstrat. and haze; remainder mostly clear; thunder; showers at 0 ^h Generally clouded; circum. and haze; remainder clear; thunder; showers occasionally  Generally clear  Clear to 12 ^h ; remainder clouded; circum.; cirstrat.  Clouded to 16 ^h ; circum., cirstrat., and haze; thunder and lightning in S.E. at 10 ^h ; clear	1.0 0.1 1.0 0.2 0.1 	1'0  1'0  0'2 1'0 0'0  0'0  1'0 1'0 0'0 0'0 0'0 0'0 0	0.0 0.0 0.0 0.0 1.0 0.0 1.0 1.0 1.0 0.5 	1.0 1.0 1.0 0.6 1.0 0.6 1.0 1.0 1.0 0.7 0.0 1.0 0.0 0.8 1.0 0.2 1.0 0.1 0.2 1.0	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7 66.6 55.0 54.6 56.8 67.9 65.5 67.1 60.2 67.0 68.4 71.1 74.6	43.8 43.8 49.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2 42.7 56.0 48.7 50.2 49.0 50.1 50.7 52.7	0.05 0.60 0.60 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h. Clear to 20h; remainder clouded; circum.  Generally clouded; slight rain occasionally Nearly clear to 20h; clouded; circum.  Mostly clear  Nearly clear to 3h; remainder clouded; circum., cirstrat., and haze Clouded all day; cumstrat., circum., and haze; slight rain from 10h to 12h; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10h to 13h  Mostly clouded; circum., cirstrat., and haze; remainder clear; constant rain from 6h to 11h  Mostly clear to 12h; clouded; circum. and haze; auroral light at 10h and 11h; rain from 19h to 23h  Clear from 9h to 12h; remainder clouded; circum. and cumstrat.; light rain at 1h and from 18h to 22h  Clouded and clear alternately; circum., cumstrat., and cirstrat.  Nearly clear all day  Clear to 20h; remainder clouded; circum. and cumstrat.  Clouded all day; circum. and cumstrat.; rain from 4h to 9h  Clouded to 3h; cirstrat. and haze; remainder mostly clear; thunder; showers at 0h  Generally clouded; circum., and haze; rain at 1h; lightning  Clouded to 11h; circum., cirstrat., and haze; remainder clear; thunder; showers occasionally  Generally clear  Clear to 12h; remainder clouded; circum.; cirstrat.	1.0 0.1 1.0 0.2 0.1 	1'0 0'2 1'0 0'0 0'0 1'0 1'0 0'4 1'0 1'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'7 0'1 0'0	0.0 0.0 0.0 0.0 1.0 0.0 1.0 0.2 0.2 0.2 0.2 0.0 0.6 1.0	1.0 1.0 1.0 0.6 1.0 0.6 1.0 0.7 0.0 1.0 0.0 0.0 0.8 1.0 0.1 0.2 1.0 0.1 0.0 0.1 0.0 0.8	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.4 66.7 66.6 55.0 54.6 56.8 67.9 65.5 67.1 60.2 67.0 68.4 71.1 74.6 75.0	47.9 43.6 43.8 49.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2 42.7 56.0 48.7 50.2 49.0 50.1 50.7 58.9	0.05 0.60 0.10 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h.  Generally clouded; slight rain occasionally Nearly clear to 20h; clouded; circum.  Mostly clear  Nearly clear to 3h; remainder clouded; circum., cirstrat., and haze  Clouded all day; cumstrat., circum., and haze; slight rain from 10h to 12h; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10h to 13h  Mostly clouded; circum., cirstrat., and haze; remainder clear; constant rain from 6h to 11h  Mostly clouded; circum., circum., and haze; remainder clear; constant rain from 6h to 11h  Mostly clouded to 12h; clouded; circum. and haze; auroral light at 10h and 11h; rain from 10h to 23h  Clear from 9h to 12h; remainder clouded; circum. and cumstrat.; light rain at 1h and from 18h to 22h  Clouded and clear alternately; circum., cumstrat., and cirstrat.  Nearly clear all day  Clear to 20h; remainder clouded; circum. and cumstrat.  Clouded all day; circum. and cumstrat.; rain from 4h to 9h  Clouded to 20h; remainder clouded; circum. and cumstrat.  Clouded to 11h; circum., cirstrat., and haze; remainder clear; thunder; showers at 0h  Generally clouded; circum., cirstrat., and haze; remainder clear; thunder; showers occasionally  Generally clouded; circum., cirstrat., and haze; thunder and lightning in S.E. at 10h; clear-  Clear to 12h; remainder clouded; circum.; cirstrat.  Clouded to 16h; circum., cirstrat., and haze; thunder and lightning in S.E. at 10h; clear-  Generally clouded; circum., cum., and cirstrat.; thunder at 5h and 6h	1.0 0.1 1.0 0.2 0.1 1.0 0.2 1.0 0.4 1.0 0.1 1.0 0.2 0.5 0.0 1.0 0.8 0.7 0.8 0.9 0.9 0.8 0.7	1'0 0'2 1'0 0'0 0'0 1'0 1'0 0'0 0'0 0'0 0'0 0'0	0.0 0.0 0.0 0.0 1.0 0.0 1.0 0.2 0.0 1.0 0.2 0.0 0.0 1.0 0.0 1.0	1.0 1.0 1.0 0.6 1.0 0.6 1.0 0.7 0.0 1.0 0.0 0.0 0.0 0.8 1.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.0	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.7 66.6 55.0 54.6 56.8 67.9 65.5 67.1 60.2 67.0 68.4 71.1 74.6 75.0 77.8 76.4	43.8 43.8 49.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2 42.7 56.0 48.7 50.2 49.0 50.1 50.7 52.7	0.05 0.60 0.60 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16
29 } 30 } 31	Clouded all day; cir. and haze; constant rain to 16h; thunder and lightning at 13h and 14h.  JUNE.  Generally clouded; circum., cirstrat., and haze; rain; thunder; lightning; rainbow at 7h. Clear to 20h; remainder clouded; circum. Generally clouded; slight rain occasionally Nearly clear to 20h; clouded; circum.  Mostly clear  Nearly clear to 3h; remainder clouded; circum., cirstrat., and haze Clouded all day; cumstrat., circum., and haze; slight rain from 10h to 12h; sheet lightning in N.  Clouded; cir., cirstrat., and haze; foggy; lightning in N.N.E. from 10h to 13h  Mostly clouded; circum., cirstrat., and haze; remainder clear; constant rain from 6h to 11h  Mostly clouded; circum., cirstrat., and haze; remainder clear; constant rain from 6h to 11h  Mostly clear to 12h; clouded; circum. and haze; auroral light at 10h and 11h; rain from 11h to 23h  Clear from 9h to 12h; remainder clouded; circum. and cumstrat.; light rain at 1h and from 18h to 22h  Clouded and clear alternately; circum., cumstrat., and cirstrat.  Nearly clear all day Clear to 20h; remainder clouded; circum. and cumstrat.  Clouded all day; circum. and haze; remainder mostly clear; thunder; showers at 0h  Clouded to 3h; cirstrat. and haze; remainder mostly clear; thunder; showers at ceasionally Generally clouded; circum., cirstrat., and haze; remainder clear; thunder; showers  Clouded to 11h; circum., cirstrat., and haze; remainder clear; thunder; showers  Clouded to 12h; remainder clouded; circum.; cirstrat.  Clouded to 16h; circum., cirstrat., and haze; thunder and lightning in S.E. at 10h; clear-  Clear to 12h; remainder clouded; circum.; cirstrat.	1.0 0.1 1.0 0.2 0.1 1.0 0.2 1.0 0.4 1.0 0.1 1.0 0.2 0.5 0.0 1.0 0.8 	1'0 0'2 1'0 0'0 0'0 1'0 1'0 0'4 1'0 1'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0	0.0 0.0 0.0 0.0 1.0 0.0 1.0 0.2 0.2 0.2 0.0 0.6 1.0	1.0 1.0 1.0 0.6 1.0 0.6 1.0 0.0 1.0 0.0 0.0 0.0 0.8 1.0 0.1 0.2 1.0 0.1 0.0 0.1 0.0 1.0 0.0 0.8	65.4 58.9 48.2 62.0 62.6 62.1 62.4 63.7 64.4 70.5 61.8 75.2 64.6 55.0 54.6 56.8 67.9 65.5 67.1 60.2 67.0 68.4 71.1 74.6 75.0 77.8	47.9 43.6 43.8 49.4 45.1 52.7 36.7 41.5 53.1 53.9 60.7 57.0 46.6 46.7 47.7 40.1 43.7 40.2 42.7 56.0 48.7 50.2 49.0 50.1 50.7 50.7 50.7 50.9 60.7 50.9 60.7 50.9 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7 60.7	0.05 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10

Toronto Mean	Washington Diagrams	Ex	tent of C	Cloudy Sk	xy.	Max.	Min.	Rain.
Time.	Weather and Phenomena.	3	9	15	21	Therm.	Therm.	Kam.
D.	JULY.					0	0	In.
$\frac{1}{2}$	Clear all day	0.0	$\begin{vmatrix} 0.0 \\ 0.0 \end{vmatrix}$	0.0	$0.0 \\ 0.0$	$72.1 \\ 75.8$	49°5 53°5	_
$\left\{\begin{array}{c}3\\4\end{array}\right\}$	Mostly clear all day	0.5	0.1	0.0	0.3	78.8 81.3	54.2	
5 6	Mostly clouded all day; thunder; slight rain at 6 ^h	0.8	1.0	1.0	$\frac{1.0}{1.0}$	$\frac{79.2}{81.3}$	55.7 66.3	0.03
7 8	Generally clouded; cir. and haze Clouded at 8 ^h and 21 ^h ; cir. and haze; remainder clear	1.0	0.0	0.0	$\frac{1.0}{1.0}$	78°2 80°8	62°1	
9	Clouded all day; cir. and haze; auroral light in N. at 10h	$\frac{0.9}{1.0}$	1.0	1.0	1.0	80.5	65°2 67°5	_
11 }	Clouded to 11 ^h ; lightning at 11 ^h ; remainder generally clear; auroral light at 13 ^h { Generally clouded; cir. and haze	$\frac{-0.5}{0.2}$	$\frac{1.0}{1.0}$	0.0	0.8 1.0	$81.3 \\ 78.4$	67·1 64·4	_
13 14	Clouded to 8h; circum., cirstrat., and haze; clear	0.0	0.0	0.0	0.2	$82.7 \\ 83.1$	63.2	
15	Partly clear to 8h and from 14h to 18h; clouded; cir. and haze	0.2	1.0	0.0	1.0	73.7	50.9	_ [
16 17 }	Clear from 9 ^h to 14 ^h ; generally clouded; cir., circum., and haze Clouded to 14 ^h ; circum. and haze; clear; rain, thunder, and lightning during the day - {	$\begin{vmatrix} 1.0 \\ 0.8 \end{vmatrix}$	1.0	0.2	0.8	76.4 82.8	59.0 66.1	0.75
18 }	Clouded and clear alternately; cir., circum., and cum.; sheet lightning	0.2	0.0	$\begin{vmatrix} 0.5 \\ 0.5 \end{vmatrix}$	1.0	84°2 82°4	70°0 66°5	0.50
$\frac{20}{21}$	Clouded all day; circum. and cumstrat.; thunder, lightning, and showers during the day - Partially clouded; circum. and cumstrat.; constant lightning, and rain at 16 ^h	$\begin{bmatrix} 0.3 \\ 0.3 \end{bmatrix}$	0.0	$\begin{vmatrix} 1.0 \\ 0.7 \end{vmatrix}$	$\frac{0.3}{1.0}$	87.0 80.2	68.4	$\begin{bmatrix} 0.65 \\ 0.84 \end{bmatrix}$
$\frac{22}{23}$	Generally clear	0.1	$\begin{vmatrix} 0.1 \\ 0.0 \end{vmatrix}$	0.0	$\frac{0.5}{1.0}$	81.0 78.8	66.2	
$\left\{ egin{array}{c} 24 \ 25 \end{array}  ight\}$	Clouded all day; cir. and haze; rain, thunder, and lightning {	1.0	1.0	1.0	1.0	74·2 69·6	53.0 64.2	0.30
26 27	Generally clear	0.1	0.0	$0.0 \\ 0.0$	$0.1 \\ 0.2$	75.9 62.9	58.5 43.2	_
28 29	Clouded to 8h; circum., cirstrat., and haze; clear Generally clouded; circum., cirstrat., and haze; rain	0.8	0.0	0.0	0.0	64.6 65.4	44.0 47.2	0.25
30	Partly clouded to 12h; cumstrat., circum., and cum.; clear; light rain	$\frac{0.8}{0.3}$	$0.7 \\ 0.1$	0.0	0.1	70.4	55.7	0.09
Aug. 1	Clouded to 8 ^h ; cum., circum., and cumstrat.; rain; clear	<del></del>	— I	0.0	0.4	$\begin{vmatrix} 66.2 \\ 71.2 \end{vmatrix}$	44.0 51.1	0.03
	AUGUST.							
2	Generally clear	0.4	0.0	0.0	0.5	69.6	46.0	_
$\frac{3}{4}$	Generally clear Generally clear; aurora from 9 ^h to 14 ^h	0°1 0°7	$\begin{vmatrix} 0.0 \\ 0.0 \end{vmatrix}$	$\begin{array}{c} 0.3 \\ 0.0 \end{array}$	0.3	72.2 73.8	47.9 50.5	_
5 6	Clouded and clear alternately; cir., cirstrat., and haze Mostly clouded; cir., cirstrat., and haze; lightning, thunder, rain	$\frac{1.0}{0.1}$	$\begin{vmatrix} 0.8 \\ 0.6 \end{vmatrix}$	0.0	$\frac{1.0}{0.8}$	76.6 74.4	55.0	0.07
$\left\{\begin{array}{c}7\\8\end{array}\right\}$	Clouded; cir., cirstrat., and haze; solar halo at 2h, diameter 40°; rain	0.9	0.5	$\frac{1.0}{1.0}$	1.0	78.0 72.8	57.8 58.5	0.16
9 10	Clouded; circum., cumstrat., and haze; lightning at 9 ^h and 10 ^h Clouded all day; circum., cirstrat., and haze; slight rain	0.4	0.6	1.0	$0.7 \\ 1.0$	$62.4 \\ 74.3$	62.0	_
11 12	Clouded to 4h; circum. and haze; nearly clear; rain from 0h to 4h	1.0	0.0	0.1	$0.2 \\ 0.7$	77.4	65·2 63·0	0.06
13	Generally clouded; circum. and haze; thunder at 3 ^h	0.9	0.3	1.0	0.4	75.2	61.0	0.03
$\left\{\begin{array}{c}14\\15\end{array}\right\}$	Clear from 12 ^h to 18 ^h ; remainder clouded; lightning in S.W. from 12 ^h to 15 ^h {	0.6	$\frac{0.0}{0.8}$	0.0	0.8	76.9	64.5	_
16 17	Clouded at 4 ^h and 21 ^h ; circum. and cirstrat.; remainder clear; auroral light in N. at 13 ^h - Generally clouded; cumstrat. and circum.; lightning; thunder; rain at intervals -	0.7	1.0	1.0	$\frac{1.0}{0.2}$	$81.0 \\ 82.6$	63.0	0.79
18 19	Clear from 6 ^h to 11 ^h ; remainder clouded; circum. and cir Partly clouded; circum. dispersed; clear	$0.7 \ 0.5$	0.0	0.0	$\begin{array}{c} 0.7 \\ 0.2 \end{array}$	75.6 67.4	52.5 44.6	_
20 21	Partly clouded to 12 ^h ; circum. and cumstrat.; slight rain; clear	$0.9 \\ 0.2$	$\begin{bmatrix} 0.5 \\ 0.0 \end{bmatrix}$	0.0	0.1	66.0 72.6	50.0 52.5	0.17
$\left\{egin{array}{c} 22 \\ 23 \end{array} ight\}$	Nearly clear; auroral light in N. at 11 ^h	0.5	0.5	0.0	0.1	$73.6 \\ 72.4$	51.2 51.0	_
24 25	Partly clouded; cir. and haze	$\begin{array}{c c} 0.4 \\ 0.3 \end{array}$	0.5	$\begin{array}{c c} 0.5 \\ 0.4 \end{array}$	$\begin{array}{c} 0.9 \\ 0.0 \\ 0.0 \end{array}$	68.0 70.3	50.2	
26	Clear and partly clouded alternately Generally clouded; circum. and haze; rain	0.3	0.8	1.0	1.0	70.8	52.0	0.12
27 28	Clear all day; very light rain	0.1	0.0	0.0	0.0	74.5 65.7	55.8 46.0	0.03
29 } 30	Mostly clear from 6 ^h to 18 ^h ; remainder clouded; cum., circum., and haze; rain	1.0	0.1	0.0	$0.4 \\ 1.0$	68.7 68.0	51.5 51.0	0.31
31	Clear from 6 ^h to 10 ^h ; remainder clouded; circum. and haze	1.0	0.0	1.0	1.0	73.0	48.1	

Toronto	Weather and Phenomena.		xtent of (	Cloudy Sl	ky.	Max.	Min.	
Mean Time.	Weather and Phenomena.	3	9	15	21	Therm.		Rain.
D.	SEPTEMBER.					0	0	In.
1	Nearly clear all day	0.5	0.0	0.0	0.1	62.4	44.9	
2	Generally clear to 18h; clouded	0.1	0.0	0.0	1.0	66.1	49.3	0:01
3	Generally clouded; circum. and cirstrat.; slight rain at 6h	$0.0 \\ 0.9$	$0.8 \\ 0.8$	1.0	1.0	71.8	52.2	0.01
$\left\{\begin{array}{c}4\\5\end{array}\right\}$	Clouded to 12h; circum. and haze; lightning, thunder, and rain from 10h to 11h; hurricane		<del></del>	$\frac{0.0}{-}$	$\frac{0.0}{-}$	74.5	56.0 57.6	1.24
6 6	at Cornwall, Upper Canada, at 21h	0.4	0.0	0.0	0.3	69.9	47.3	
7	Generally clouded; circum. and cirstrat.; clear occasionally	0.8	0.9	1.0	1.0	67.4	51.0	
8 {	Mostly clear all day; circum., cirstrat., and cumstrat.; thunder, lightning, and rain	1.0	1.0	1.0	0.9	65.0	61.9	2.20
,	from 6 ^h to 17 ^h	0.9	0.0	0.0	0.0	74.5	49.7	0.12
9 10	Clear and fine to 20h; clouded	0.1	0.0	0.0	0.7	60.2	41.3	
11 }	Clear and the to 20°, clouded	0.1	0.0	_		63.7	45.7	
12	Nearly clear to 11h; remainder clouded; circum. and cumstrat.; slight rain {			1.0	1.0	62.8	47.6	0.09
13	Clouded all day; cumstrat. and cirstrat.; slight rain	1.0	1.0	1.0	1.0		52.9	0.01
14	Quite clear all day	$\frac{0.0}{0.0}$	$0.0 \\ 0.0$	$\begin{vmatrix} 0.0\\0.0\end{vmatrix}$	0.0	55°1 52°9	41.0 35.8	_
$\begin{array}{c} 15 \\ 16 \end{array}$	Quite clear Generally clear to 9 ^h ; remainder clouded; circum, and cirstrat.	0.0	0.4	1.0	0.6	57.6	35.0	
17	Generally clouded; circum. and cirstrat; rain from 8h to 17h	0.7	1.0	1.0	1.0	59.4	47.7	0.25
18 7		1.0	1.0			62.2	54.5	0.09
19 }	Clouded all day; circum. and cirstrat.; rain from 0h to 4h -			1.0	1.0	61.2	52.5	0.31
20	Clouded; circum. and cirstrat.; slight rain	$\frac{1.0}{0.2}$	0.0	0.0	0.7	57.7 56.8	54.6 51.2	_
$\begin{array}{c} 21 \\ 22 \end{array}$	Nearly clear to 20 ^h ; remainder clouded; cumstrat. and circum Clouded to 6 ^h ; circum. and cumstrat; clear	0.6	0.0	0.0	0.1	62.4	41.8	_
$\frac{22}{23}$	Nearly clouded; circum. and cirstrat; lunar halo at 9h, diameter 400, imperfect	0.7	1.0	1.0	1.0	59.8	45.2	
$\frac{23}{24}$	Clouded all day; circum. and haze; rain from 4h to 14h	1.0	1.0	1.0	1.0	67.0	54.3	0.09
25 $)$	Clouded all day; circum., cirstrat., and haze; heavy storm of thunder; lightning; rain {	1.0	1.0			55*6	48.7	0.01
26 }	from 12h to 15h			1.0	1.0	58.8	51.0	1.08
$27$ $\{$	Clouded to 7 ^h ; cir., cir., strat., and circum.; showers, thunder, and lightning from 5 ^h to 8 ^h ; clear	0.6	0.1	0.0	0.0	59.3	55.2	0.19
20 (	Clear from 12h to 17h; remainder clouded; circum, and cum,-strat.; lightning, thunder,	0.8	0.1	0.0	1.0	68.8	46.2	0.04
28 {	and rain at 0h	0 0	0.1	0.0	10	00 0	40 2	0 04
$29$ $\{$	Partly clouded to 15h; eircum. and cumstrat.; thunder; lightning; rain from 0h to 4h;	0.8	0.3	0.5	0.0	60.0	39.7	0.11
30	frost ; clear	1.0	1.0	1.0	0.6	<b>5</b> 5.0	37.3	0.11
	OCTOBER.					<u>!</u>		
1	Clouded to 5 ^h ; remainder clear	0.7	0.0	0.0	0.0	54.4	43.7	
$\hat{2}$ )	Clouded to 10 ^h ; circum.; remainder mostly clear	0.5	1.0			53.6	36.5	_
3 }				0.0	0.1	55.9	38.2	
4 {	Generally clouded; circum. and cirstrat.; lightning; thunder from 9h to 17h; showers at 17h	0.8	0.6	1.0	1.0	54.4	40.2	0.03
5	Mostly clouded; rain most of the day	0.6	1.0	1.0	1.0	60.2	52.5	0.76
$\ddot{6}$	Clouded; dense; circum. and haze; rain most of day	1.0	1.0	1.0	1.0	64.6	56.0	1.18
7	Clouded; circum. and cirstrat.; slight rain most of day	1.0	1.0	1.0	1.0	58'4	54.5	0.32
8	Clouded to 8h; circum, and haze; clear; aurora at 11h	1.0	$\frac{0.5}{1.0}$	0.0	0.3	56.4	55°1ª   40°2	0.01
9 } 10 }	Clouded to 9h; circum., cirstrat., and haze; slight rain; clear {			0.3	$\frac{0.0}{-}$	56.5	42.2	0 01
11	Clouded; circum. and haze; slight rain	0.6	0.3	1.0	1.0	57.2	38.0	0.01
12 {	Clouded to 10 ^h and partly to 23 ^h ; circum., cirstrat., and haze; rain to 10 ^h ; auroral light	1.0	1.0	0.3	0.8	50.6	36.9	0.26
	in N. from $15^{\rm h}$ to $18^{\rm h}$	0.4	0.0	0.7	0.3	47.5	37.8	
13 14	Clear from 6h to 13h; remainder clouded; circum. and cumstrat.; snow; aurora at 12h -	0.6	0.0	1.0	0.9	47.0	32.0	_
15	Clouded to 10 ^h ; circum, and haze; clear; auroral light at 14 ^h	1.0	0.2	0.0	0.0	40.4	26.7	
16 ₇	Clouded from 3h to 9h; circum. and haze; remainder partly clear; solar halo at 0h,	0.3	1.0	_		44'0	37.2	
17 }	diameter 25°; rain from 6h to 8h	<u> </u>	1:0	0.0	0.6	55.3	46.3	0:14
18 19	Partly clouded from 5° to 14°; circum, and haze; clear; slight rain  Clouded to 5°; circum, and cirstrat.; clear	$0.8 \\ 0.3$	0.0	0.0	0.0	60.0	36.4 41.0	0.14
20	Clear to 14 ^h ; clouded; cir., cirstrat., and haze	$0.0 \\ 0.3$	0.0	0.5	1.0	54.1	28.8	
21	Clouded all day; cir., cirstrat., and haze; rain from 10h to 17h	1.0	1.0	1.0	1.0	54.0	30.5	0.22
22	Clouded to 16 ^h ; circum. and haze; rain at 23 ^h ; remarkable appearance of aurora at 16 ^h -	1.0	1.0	0.4	0.0	44.5	37:3	
$\{23, 34, 34\}$	Generally clear to 12h; remainder clouded; dense; cir. and haze; constant rain {	0.1	0.3	1.0	0.9	40'4	33.3	0:07
$24 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	Clouded from 0 ^h to 8 ^h and from 16 ^h to 23 ^h ; circum. and cumstrat.	0.6	0.0	0.0	0.9	49.0	45.3	0.97
$\frac{25}{26}$	Clear from 4 ^h to 13 ^h ; clouded; slight rain	$0.3 \\ 0.3$	0.0	0.8	0.3	48.4	28.4	_
27	Clouded to 9h; circum. and cumstrat.; clear	1.0	1.0	0.0	0.0	31.8	20.4	_
28	Generally clear	0.0	0.1	0.0	0.3	35.5	24.7	-
29	Clear from 9 ^h to 15 ^h ; remainder clouded	$0.0 \\ 0.9$	0.0	0.0	1.0	40.8	$\begin{vmatrix} 27.3 \\ 32.2 \end{vmatrix}$	_
$\left\{\begin{array}{c} 30 \\ 31 \end{array}\right\}$	Clear from 9h to 11h; remainder clouded; cir., cirstrat., and haze; rain from 13h to 17h - {			1.0	1.0	50.9	$\frac{32.2}{32.0}$	0.39
UI J	· ·		1	1 - 0	1 - 0	1 30 0	1 52 0	000

² Taken from the lowest reading of the Standard Thermometer.

Toronto	Weather and Phenomena.	E	xtent of (	Cloudy Sl	ky.	Max.	Min.	Rain.
Mean Time.	weather and Thenomena.	3	9	15	21	Therm.	Therm.	
D.	NOVEMBER.					0	0	In.
$_{2}^{1}$	Generally clouded; cir. and cirstrat.; dense fog Generally clouded; circum. and cirstrat.; lightning; faint aurora	0.3	$\frac{1.0}{1.0}$	$\frac{0.5}{1.0}$	$\frac{1.0}{1.0}$	51.0 54.8	$\frac{47.7}{46.4}$	
3 {	Clouded to $5^h$ , and from $18^h$ to $23^h$ ; circum. and haze; lightning, thunder, and rain from $\{$ $0^h$ to $5^h$ ; remainder clear $         -$	1.0	0.0	0.0	0.6	57:9	42.2	0.09
4	Mostly clear to 20h; circum.; remainder clouded	0.1	0.0	0.1	0.8	54.4	40.3	
5 6 )	Clouded to 12 ^h , and from 16 ^h to 21 ^h ; remainder clear; auroral light in N. at 15 ^h and 16 ^h - Partly clear to 12 ^h ; remainder clouded; circum., cirstrat., and haze; lightning; thunder	0.8	$\frac{0.5}{0.5}$	0.0	0.9	$\frac{51.1}{45.9}$	34°3 29°2	
$\left\{ egin{array}{c} 6 \\ 7 \end{array}  ight\}$	at 16 ^h and 17 ^h Clouded all day; dense haze; rain	$\frac{1.0}{}$	<u>-</u>	1.0	1.0	38.0 43.7	27.8 39.7	$0.98 \\ 0.03$
8 9	Clear to 14h; remainder clouded; circum, and cumstrat.; aurora at 9h and 10h	0.1	0.0	1.0	1.0	51.4	17.7	0.08
10 11	Clouded all day; circum. and cumstrat	1.0	$\frac{1.0}{1.0}$	1.0	$\frac{0.1}{1.0}$	55°2   39°7	36.7 34.1	
12	Clouded to 18h; circum. and cirstrat.; remainder generally clear	1.0	0.0	1.0	0.3	37.2 39.4	30°5 33°1	0.71
$\begin{bmatrix} 13 \\ 14 \end{bmatrix}$	Clouded all day; cirstrat., circum., and haze; rain from 9h to 16h on the 13th {	-		1.0	1.0	40.4	34.7	
$\frac{15}{16}$	Generally clouded; circum, and cumstrat Nearly clouded all day; circum, cirstrat., and haze	$\frac{0.0}{1.0}$	1.0	0.4	$\frac{0.0}{1.0}$	41.0	$\frac{36.2}{27.2}$	_
17 18	Clouded all day; circum., cirstrat., and haze; rain from 9 ^h to 16 ^h Clouded all day; circum., cirstrat., and haze; mist; rain	1.0	1.0	0.9	$\frac{1.0}{1.0}$	47.7 52.0	$\frac{43.7}{42.7}$	$0.17 \\ 0.32$
19	Clouded to 10h; circum, and cumstrat.; nearly clear	1.0	0.8	0.1	0.1	49.6	58.5	- 0.02
$\begin{bmatrix} 20 \\ 21 \end{bmatrix}$	Mostly clouded all day; circum., cirstrat., and haze; lunar halo at 6h, diameter 45°, { perfect	0.8	1.0	1.0	1.0	$33.1 \mid 31.2 \mid$	18°3   27°7	
$\begin{array}{c} 22 \\ 23 \end{array}$	Nearly clear from 2 ^h to 13 ^h ; clouded; cirstrat. and haze; very slight rain Clouded all day; cirstrat., circum., and haze: rain	0.1	$0.2 \\ 1.0$	1.0	1.0	$\frac{42.1}{46.2}$	32°3 40°7	0.35
$\frac{20}{24}$	Generally clouded; circum., cirstrat., and haze; slight rain Clouded all day; circum., cumstrat., and cirstrat.; slight rain; snow; auroral light in N- }	1.0	1.0	1.0	0.2	52.0	46.1	0.25
$25 \ \left\{  ight $	at 6 ^h and 7 ^h	1.0	1.0	1.0	1.0	49.7	38.9	0.13
26 27	Partly clear from 5 ^h to 13 ^h ; clouded; circum. and cirstrat.; aurora at 8 ^h	0.8   0.8	0.0	1.0	1.0	42.0 26.2	$\frac{24.7}{19.7}$	_
$28 \hat{j}$	Clear from 11 ^h to 13 ^h ; clouded; cirstrat., circum., and haze; clear; some snow { Partly clear; circum., cirstrat., and haze	$\frac{0.5}{0.2}$		0.0	0.6	31.0	24.7	
29 30	Clear to 18 ^h ; remainder clouded; circum., cirstrat., and haze	0.0	0.4 0.0	$\begin{array}{c} 0.0 \\ 0.8 \end{array}$	$\frac{0.3}{1.0}$	24.6 18.3	$\frac{8.7}{11.5}$	
	DEGEMBER							
1	DECEMBER.  Clouded all day; circum., cirstrat., and haze; rain from 8 ^h to 17 ^h	1.0	1.0	1.0	1.0	29.9	22.7	0.25
$\frac{1}{2}$	Clouded all day; circum. and haze; slight rain from 20 ^h to 23 ^h Nearly clouded all day; circum. and haze	1.0	1.0	1.0	0.0	40°0 38°0	35.0 32.2	0.11
$\left. egin{array}{c} 4 \\ 5 \end{array}  ight\}$	Partially clouded; cirstrat., circum., and haze; snow	1.0	1.0			30.2	25.2	_
6	Clouded to 11 ^h ; circum. and cumstrat.; remainder nearly clear	0.8	1.0	$\begin{bmatrix} 0.0 \\ 0.8 \end{bmatrix}$	$0.2 \\ 0.2$	$\frac{33.5}{32.6}$	26°0 23°7	_
$\begin{bmatrix} 7 \\ 8 \end{bmatrix}$	Partly clear; cir. and cirstrat. occasionally	1.0	0.1	0.6	$\frac{0.5}{1.0}$	$\frac{33.0}{39.4}$	28°2 30°3	
9 10	Mostly clouded all day; cirstrat. and haze; rain to 8h	1.0	1.0	1.0	0.6	45.5	35.2	0.51
11 7	Clouded all day; circum., cir., and haze; rain from 14 ^h to 17 ^h Partly clear from 3 ^h to 11 ^h ; remainder clouded; circum. and haze; slight rain from §	0.1	$\begin{bmatrix} 1.0 \\ 0.5 \end{bmatrix}$	1.0	1.0	46.8 49.6	$\frac{33.0}{38.0}$	0.02
12 <i>f</i> 13	12 ^h to 17 ^h	1.0	1.0	1.0	1.0	36.8 45.0	26.7 33.0	$0.13 \\ 0.27$
14 15	Clouded to 18 ^h ; circum. and haze; slight rain from 1 ^h to 9 ^h ; clear Clear and fine to 18 ^h ; remainder clouded; circum. and cirstrat	0.1	0.0	0.0	$0.0 \\ 0.1$	$\begin{array}{c} 36.3 \\ 33.2 \end{array}$	29.5 29.5	0.11
16 17	Generally clouded; circum. and cirstrat.; aurora from 15h to 17h  Generally clear; auroral light at 11h	0.6	1.0	0.4	0.7	33.4	12.9	_
18	Clouded all day; circum. and haze; aurora at 17h; great magnetic disturbance	1.0	1.0 1.0	0.0	0.0	21 4 27 2	14.8	_
19 3 20	Generally clouded; circum. and cirstrat.; clear occasionally	0.5	1.0	1.0	$\frac{1.0}{0.7}$	33.6	$\frac{27.9}{12.1}$	_
$\begin{array}{c} 21 \\ 22 \end{array}$	Clouded all day; cir., cir., cum., and cumstrat.; snow from 9 ^h to 15 ^h Clouded all day; circum. and haze; snow to 1 ^h	1.0	$\frac{1.0}{1.0}$	1.0	1.0	15.9 24.6	$\frac{9.\overline{3}}{18.1}$	
23	Clouded; circum., cirstrat., and haze; snow to 4h	1.0	1.0	1.0	0.4	24.8	17.4	_
$\left.\begin{array}{c}24\\25\\96\end{array}\right\}$	Generally clouded; circum., cirstrat., and haze; snow	0.8	1.0	1.0	0.8	24.4 22.2	20.4	_
26 J 27	Clouded all day; circum., cirstrat., and haze; snow	1.0	1.0	1.0	1.0	18 <b>·</b> 4 19 <b>·</b> 0	$\frac{2.1}{0.3}$	_
28 29	Clouded all day; circum., cirstrat., and haze	1.0	1.0 0.4	1.0	1.0	28.8 36.4	$\frac{18.2}{32.9}$	-
30	Clouded all day; cirstrat. and haze	1.0	1.0	1.0	1.0	43.0	36.5	
31	Clouded all day; dense haze; drizzling rain	1.0	1.0	1.0	1.0	45.9	40.1	0.52

Coronto		Ez	ktent of C	Cloudy Sk	cy.	_ Max.	Min.	D. 1
Mean Time.	Weather and Phenomena.	3	9	15	21	Therm.		Rain.
D.	JANUARY.						0	In.
$\left. egin{array}{c} 1 \ 2 \end{array}  ight\}$	Clouded till 12 ^h ; circum. and haze; rain; remainder clear	1.0	1.0	0.0	0.1	45°2 51°1	$\begin{vmatrix} 42.2 \\ 29.7 \end{vmatrix}$	0.56
3 4 5 6 7 8	Clouded; circum, cirstrat., and haze	1.0 0.1 1.0 1.0	1.0 0.2 0.1 1.0 1.0	0.8 1.0 1.0 1.0	1.0 0.2 1.0 1.0	35.4 37.6 34.0 36.2 14.3 29.6	30.7 26.7 17.5 10.5 10.9 18.1	
9 } 10 11 12 13 14 15 }	Clouded till 12 ^h ; circum. and haze; some snow; remainder clear  Clear till 14 ^h ; remainder clouded; circum., cirstrat., and haze; slight snow  Clouded; circum. and haze; slight snow occasionally; auroral light at 17 ^h Clouded; circum. and cirstrat	0.2 1.0 0.9 1.0 1.0	0.0 1.0 1.0 1.0 1.0 0.2	0.0 1.0 1.0 1.0	1.0 1.0 1.0 1.0 0.0	33.4 13.8 1.0 22.4 32.4 36.5 40.2	13.0 11.4 -8.9 7.1 20.3 35.2 36.0	0.9
16 }   17   18   19   20   21   22 }	Clouded till 5 ^h ; circum., cirstrat., and haze; aurora from 1 ^h to 2 ^h {  Partially clear till 5 ^h ; remainder clouded; cir. and haze; halo round moon from 6 ^h to 9 ^h -  Generally clear; slight showers of snow  Clouded; circum., cumstrat., and cirstrat  Mostly clouded; cir. and haze; halo round moon from 11 ^h to 15 ^h , diameter 35°, perfect  Generally clouded; circum. and cumstrat.; clear spaces occasionally	0°1 0°4 0°5 0°7 0°9 1°0	1.0 0.3 1.0 0.6 0.7 1.0	1.0 1.0 1.0 0.0 1.0	1.0 1.0 0.3 0.3 0.8	47.0   32.5   30.9   29.8   28.8   41.4   45.0	27.7 23.2 19.9 5.7 17.6 24.7 13.6	
23 } 24 25 26 27 28 {	Clouded all day; circum., cirstrat, and haze; particles of snow {  Clear till 11 ^h ; remainder clouded; circum. and cirstrat	1.0 1.0 1.0	0.8 0.8 0.0	0.0 1.0 1.0 1.0 1.0	0.8 1.0 1.0 0.8	29 · 2   24 · 2   32 · 0   39 · 3   40 · 2   41 · 8	17.0 17.4 24.3 35.0 36.5 30.1	0.0
29 30 31	Clouded; circum., cumstrat., and haze; showers of snow; rain from 17 ^h to 22 ^h { Clouded till 4 ^h ; circum., cirstrat., and haze; remainder of day mostly clear	1.0	0.2	0.0	1.0	34.8 31.8 32.0	24.2 21.7 22.5	0.5
1 2 3 4 5 6 7 8 9 10	FEBRUARY.  Clear from 7 ^h to 12 ^h ; remainder clouded; cumstrat. and circum Clouded from 11 ^h to 17 ^h ; circum. and haze; remainder of day mostly clear Clouded from 14 ^h to 21 ^h ; cirstrat. and haze; remainder mostly clear	1.0 0.2 0.4 1.0 1.0 	0.0 0.5 0.1 1.0 1.0 	0.6 1.0 1.0 1.0 	0.0 0.5 1.0 1.0 	38.5 29.7 35.8 40.8 39.0 28.4 28.4 26.6 27.8 34.2 21.0	24.2 17.9 27.0 26.1 26.7 23.9 21.0 16.1 17.6 13.4 0.0	0.4
12 13 14 15 16 17 18	Mostly clear ; cirstrat. and haze	0.0 0.4 0.0 0.0 0.0 0.0	0.0 0.7 0.3 0.0 0.0 0.0		1.0 0.0 0.0 0.0 0.0	15.0 25.2 31.7 38.2 32.6 36.0 36.2	10.8 11.9 18.2 18.5 19.5 19.7	
	Mostly clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h {  Mostly clear till 8 ^h ; remainder clouded; cirstrat. and haze; aurora from 7 ^h to 10 ^h - Clouded all day; cirstrat. and haze; slight rain and snow from 2 ^h to 9 ^h ; aurora from 13 ^h to 14 ^h	1.0 0.0 1.0 0.5	1.0 1.0 	1.0	0.3 1.0 0.3	37:4 38:8 41:2 46:6 40:0	28.5 34.0 36.4 29.7 28.6	0.0
24 25 26 27 28 29	Mostly clouded; circum. and cumstrat., aurora from 8 ^h to 17 ^h Generally clear  Clear from 12 ^h to 15 ^h ; remainder clouded  Clouded; circum., cumstrat., and haze; snowing most of the day  Generally clouded; cumstrat., circum., and haze; showers of snow and drift	0.7 0.4 1.0 - 1.0 0.9	1.0 0.0 0.6 - 1.0 0.4	0.0 0.0 0.0 0.0	0.1	36.5 29.8 23.4 33.6 30.0 36.1	22:1 10:7 11:4 22:9 12:6 18:6	

Toronto		Ex	tent of C	loudy Sk	у.	Max.	Min.	
Mean Time.	Weather and Phenomena.	3	9	15	21	Therm.	Therm.	Rain.
							0	In.
D.	MARCH.		0.0	1.0	1.0	22.2	7:3	.111.
$\frac{1}{2}$	Partially clear and partially clouded; circum. and cumstrat.; auroral light in N. at 11 ^h - Clouded all day; circum., cirstrat., and haze; snowing most of the day	1.0	$\begin{array}{c} 1.0 \\ 0.0 \end{array}$	$\frac{1.0}{1.0}$	1.0	21.0	0.0	_
3	Clear from 7 ^h to 11 ^h , and at 21 ^h ; remainder clouded, with circum., cirstrat., and haze	1.0	0.0	1.0	0.0	20.8	14.4	]
4 7	Clouded all day; circum. and cirstrat.; showers of snow; squally	1.0	1.0	1.0	1.0	26°1	$\frac{19.0}{19.9}$	_
5 } 6	Clouded till 2 ^h , and at 13 ^h and 15 ^h ; cirstrat. and circum.; aurora at 12 ^h	0.4	0.5	1.0	1.0	$\frac{24.7}{22.7}$	14.4	
7	Clouded till 2h, and from 9h to 14h; cirstrat. and haze; remainder mostly clear	0.4	1.0	0.4	1.0	32.1	15.5	0.06
8 9	Mostly clouded; circum., cirstrat., and haze; slight rain; auroral light in N. at 9 ^h Nearly clear from 12 ^h to 15 ^h ; remainder clouded; circum. and cumstrat.	1.0	$\frac{0.4}{1.0}$	$\begin{bmatrix} 1.0 \\ 0.2 \end{bmatrix}$	1.0	$\frac{41.1}{47.1}$	$\begin{vmatrix} 35.7 \\ 22.5 \end{vmatrix}$	
10	Generally clear	0.1	0.0	0.0	0.0	28.8	15.9	
$\{11, 10, 10\}$	Clear till 12h; remainder mostly clouded; circum. and haze; shower of snow at 13h - {	0.0	0.1	$\frac{-}{0.7}$	$\frac{0.3}{}$	31.4 34.0	$\frac{16.1}{29.2}$	0.58
12 } 13	Mostly clear	0.2	0.0	0.5	0.7	39.6	$\frac{22.9}{2}$	_
14	Mostly clear; aurora from 11 ^h to 14 ^h	0.6	0.0	0.0	0.5	25.0	11.2	
15	Mostly clear till 15 ^h ; remainder clouded; cirstrat. and haze  Generally clouded; cirstrat. and haze; halo round moon at 8 ^h and 9 ^h , diameter 45°; \(\chi^{\chi}\)	0.0	0.0	0.5	1.0	15.8	3.4	_
16 {	aurora at 16 ^h and 17 ^h	0.8	1.0	0.3	1.0	17.6	8.0	
17	Clear Clouded till 11 ^h , and at 21 ^h ; circum. and cirstrat.; remainder of day generally clear;	$\frac{1.0}{0.1}$	$\begin{bmatrix} 1.0 \\ 0.0 \end{bmatrix}$	0.0	0.1	$\frac{28.5}{26.7}$	$\begin{vmatrix} 22.9 \\ 16.2 \end{vmatrix}$	_
$\left\{\begin{array}{c}18\\19\end{array}\right\}$	auroral light in N. at 16 ^h and 17 ^h	_		0.0	1.0	34.5	22.4	
20	Clouded; cumstrat., circum., and haze; rain from 0h to 8h	$\begin{array}{c c} 1.0 \\ 0.7 \end{array}$	0.0	0.0	$\frac{1.0}{0.6}$	33.9 43.3	23°3 33°8	0.72
$\begin{array}{c} 21 \\ 22 \end{array}$	Mostly clouded till 4 ^h , and at 21 ^h ; cumstrat. and cirstrat.; remainder clear - Clouded; circum. and cumstrat	1.0	1.0	1.0	1.0	49.0	28.6	
<b>2</b> 3	Mostly clouded till 1h; remainder clear	0.5	0.0	0.0	0.0	37.0	31.8	
24	Partially clouded; cirstrat. and cir.; aurora from 9h to 12h	0.4	0.4	0.4	1.0	39.0	33.7	_
$\left. \begin{array}{c} 25 \\ 26 \end{array} \right\}$	Clouded; circum. and haze; rain at 11 ^h	_	_	1.0	1.0	43.8	37.8	0.17
27	Clouded till 8h; cir. and cirstrat.; remainder mostly clear; faint auroral light at 16h	$0.6 \\ 0.2$	$\frac{1.0}{0.3}$	$0.4 \\ 0.4$	$\frac{0.0}{0.8}$	$\begin{vmatrix} 46.2 \\ 41.2 \end{vmatrix}$	$\frac{33.0}{26.7}$	
$\begin{array}{c} 28 \\ 29 \end{array}$	Generally clouded; cirstrat. and cir.; nearly clear at intervals  Clear	0.0	0.0	0.0	$\frac{0.3}{0.0}$	45.3	31.3	_
30 31	Mostly clouded; cirstrat. and haze Mostly clouded; circum. and haze; rain from 4 ^h to 11 ^h ; auroral light in N. from 12 ^h to 15 ^h	1.0	$\frac{1.0}{1.0}$	$\begin{bmatrix} 0.7 \\ 0.3 \end{bmatrix}$	1.0	58.6 45.0	30.3	0.97
	APRIL.							
1 )	Mostly clouded; cumstrat. and cum.; aurora at night; halo round the sun at 21 ^h , diameter {	1.0	1.0			61.6	33.0	
$\begin{bmatrix} 1 \\ 2 \end{bmatrix}$	45°, perfect			0.0	1.0	36.5	27.2	
$\frac{3}{4}$	Clouded; cir., cirstrat., and haze	1.0	1.0	0.0	0.0	$\begin{vmatrix} 41.0 \\ 47.7 \end{vmatrix}$	$\begin{vmatrix} 31.7 \\ 42.2 \end{vmatrix}$	0.58
5	Mostly clear; aurora from 10 ^h to 15 ^h	0.3	0.0	0.0	0.0	47.2	30.0	_
6	Clear all day; beautiful aurora from 9 ^h to 16 ^h	0.0	0.0	0.0	$0.0 \\ 0.0$	43.5	26.5	_
7 8 1	Clear -	0.1	0.0	_		46.5	22.7	
9 }	Mostly clear	$\frac{0.0}{-}$	0.3	0.3	0.4	53.5	32.3	-
10 11	Mostly clouded; circum. and haze	1.0	1.0	0.5	0.3	65.1	43.4	
12	Mostly clear till 4h; remainder clouded; circum. and haze; slight rain from 9h to 12h -	0.3	1.0	1.0	1.0	51.6	30.9	0.05
13 14	Clouded; circum., cumstrat., and haze; slight rain from 2 ^h to 7 ^h Clouded till 6 ^h ; circum. and cum.; remainder partially clear	0.8	0.1	0.8	0.0	54.0	36.4	0.03
15 Ղ	Nearly clear all day; aurora from 9 ^h to 11 ^h	0.1	0.0			47.8	33.2	-
16 S 17	Partially clear till 2 ^h ; remainder clouded; circum. and haze	$\frac{0.9}{-}$	1.0	$\frac{1.0}{0.0}$	0.6	$\begin{vmatrix} 56.4 \\ 62.2 \end{vmatrix}$	34.1	
18	Clouded till 10h; cirstrat. and haze; remainder clear; snow from 2h to 9h -	1.0	1.0	0.0	0.0	44.8	32.9	_
19 20 )	Mostly clear  Mostly clear till 15 ^h ; remainder mostly clouded; circum., cirstrat., and haze; aurora in (	$\begin{array}{ c c } 0.3 \\ 0.0 \end{array}$	0.0	0.0	0.2	$\begin{vmatrix} 36.6 \\ 38.8 \end{vmatrix}$	23.8	_
21 }	N. from $14^{h}$ to $16^{h}$			0.5	1.0	20.0	$\begin{vmatrix} 23 & 1 \\ 33 \cdot 2 \end{vmatrix}$	
22	Clear from 4h to 11h; remainder mostly clouded; circum., cirstrat., and haze; auroral light at 8h	0.2	0.0	<u> </u>	1:0	54.1	40.5	-
$\begin{bmatrix} 23 & 5 \\ 24 & \end{bmatrix}$	Clouded till 7h; cumstrat. and circum.; remainder clear; aurora at 10h -	0.9	$\frac{0.0}{-}$	$0.0 \\ 0.1$	$\frac{0.0}{1.0}$	$\begin{vmatrix} 51.6 \\ 48.2 \end{vmatrix}$	27.8	_
25	Mostly clear	0.5	0.6	0.2	0.3	43.6	25.7	_
$\frac{26}{27}$	Mostly clear Mostly clear till 15 ^h ; remainder clouded; cir. and haze	0.1	0.0	$\frac{0.9}{0.0}$	1.0	45.7	28.9	_
28	Clouded all day; cir. and haze; slight rain from 6 ^h to 15 ^h	1.0	1.0	1.0	1.0	53.8	36.1	0.17
$\{\begin{array}{c} 29 \\ 20 \end{array}\}$	Mostly clear till 20h; remainder clouded; cumstrat., circum., and haze	0.4	0.0	— —		49.3	41.5	_
30 }		_	_	0.0	1.0	20.0	28.2	-
·								-

Toronto			y.	Max.	Min.			
Mean Time.	Weather and Phenomena.	3	9	15	21		Therm.	Rain.
D.	MAY.					0	0	In.
1	Clouded till 8 ^h ; cir., cirstrat., and haze; remainder mostly clear; slight rain from 0 ^h to 7 ^h Mostly clouded till 8 ^h ; circum., cirstrat., and haze; remainder almost clear; auroral	1.0	0.0	0.7	0.8		53.4	0.11
2 {	light at 6 ^h	1.0	0.3	0.0	0.7	49.4	34.6	_
3	Partly clouded till 8 ^h ; cumstrat. and circum.; remainder clear - Clouded till 15 ^h ; cirstrat., circum., and haze; remainder clear; thunder, lightning, and	0.9	0.0	0.0	0.0	53.7	37.5	_
4 {	showers of rain from $6^h$ to $12^h$	1.0	1.0	0.1	0.0	64.5	40.1	
5 {	Mostly clouded from 3h to 10h; circum, and cumstrat.; thunder, lightning, and showers of rain from 5h to 9h	0.2	0.9	0.0	0.8	58.4	46.7	0.03
$\left\{ \begin{array}{c} 6 \\ 7 \end{array} \right\}$	Mostly clouded till 6h; cum. and circum.; distant thunder; remainder mostly clear; halo ground the sun at 20h, diameter 40°	0.8	0.0	${0.2}$	$\frac{1.0}{1.0}$	70.6	47.1	
8 {	round the sun at 20 ^h , diameter 40° } Generally clouded till 12 ^h ; cirstrat. and haze; remainder clear; auroral light in N. at }	0.2	0.8	0.0	0.5	71.8	47·7 36·7	0.09
	12 ^h and 13 ^h } Clouded; circum. and cum.; showers of rain, lightning, and thunder from 6 ^h to 10 ^h -	0.7	1.0	1.0	0.5	57.1	39.2	0.22
10	Generally clouded; cir., circum., and haze; rain from 12h to 17h	0.9	1.0	1.0	1.0	62.0	42.9	0.12
11 {	Generally clouded; cir. and haze; rain from 0 ^h to 5 ^h ; imperfect halo round the moon at 9 ^h ; halo round the sun at 19 ^h , diameter 45°	1.0	1.0	0.3	0.0	55.0	45.5	0.12
12	Generally clear till 15 ^h ; remainder clouded; circum. and haze	0.1	0.0	0.4	1.0	51.4	41.2	
$\left\{\begin{array}{c}13\\14\end{array}\right\}$	Clouded till 12h; circum. and haze; rain from 0h to 4h; remainder mostly clear {	1.0	1.0	0.0	0.6	54.0 47.8	39.0	0.44
15	Mostly clouded; cir., circum., and haze; rain occasionally from 3h to 12h	1.0	1.0	1.0	1.0	56.4	32.5	0.53
16 17	Clouded till 9 ^h ; circum., cirstrat., and haze; remainder clear Generally clear; aurora from 9 ^h to 14 ^h	$0.1 \\ 0.1$	$0.0 \\ 0.8$	0.0	$0.0 \\ 0.2$	57·2 59·4	46°1	
18	Clear till 15h; remainder clouded; circum. and haze	0.0	0.0	0.1	1.0	64.6	43.7	_
19 {	Generally clouded; circum. and haze; heavy storm of lightning, thunder, and rain between \ 3h and 5h	1.0	1.0	1.0	0.8	72.9	48.6	0.38
20 }	Generally clouded; circum, and cirstrat.; showers of rain occasionally	1.0	1.0	_		71.7	55.5	0.26
21 }	Generally clouded; circum., cirstrat., and haze	$\frac{0.8}{-}$	0.6	1.0	1.0	73.6	56.5	0.18
23 {	Generally clouded; cir., cirstrat., and haze; storm of lightning, thunder, and rain from	1.0	0.8	1.0	0.7	61.8	51.9	0.12
(	Generally clear till 20 ^h ; remainder clouded; circum. and cirstrat.; auroral light in N. at	0.0	0:0	0:0	1.0	50.0	50.5	
$egin{bmatrix} 24 & \{ \\ 25 &  \end{bmatrix}$	10 ^h and 12 ^h Generally clouded till 15 ^h ; cir. and haze; remainder clear; auroral light in N. at 12 ^h	0.8	$0.3 \\ 0.0$	0.0	0.0	73.8	53.2	_
26	Mostly clear; auroral light in N. from 12h to 15h	$\frac{0.8}{0.8}$	0.0	0.0	0.1	78.0	46.2	
$\left\{ egin{array}{c} 27 \\ 28 \end{array}  ight\}$	Generally clear till 21 ^h ; remainder clouded; cumstrat. and circum.; storm of lightning, thunder, and rain from 22 ^h to 23 ^h	0.4	0.0	0.1	$\frac{1.0}{1.0}$	66.8	46.7	0.11
29	Generally clear	0.8	0.0	0.0	0.0	70.1	52.5	
30 31	Clear till 8 ^h ; remainder mostly clouded; cirstrat. and circum.  Mostly clear; auroral light in N. from 9 ^h to 12 ^h	$0.1 \\ 0.0$	0.6	0.0	$0.6 \\ 0.3$	75.6 67.3	47.7 41.3	
	JUNE.							
1	Partly clouded till 15 ^h ; circum., cirstrat., and haze; remainder clear	1.0	0.2	0.3	0.0	57.0	37.5	
2 {	Clouded from 9 ^h to 12 ^h , and at 21 ^h ; cir. and haze; sheet lightning round S. horizon; remainder of day clear	0.0	1.0	0.1	1.0	63.8	41.7	
3 }	Clouded till 8h; circum. and haze; remainder clear	1.0	0.0			70.0	58.1	
4 }	Clear and clouded alternately; showers; storm of lightning, thunder, rain, and hail at 5 ^h 30'	0.9	$\frac{-}{0.2}$	0.0	$0.8 \\ 0.0$	71.0 65.8	54.8 47.7	0.76
5 6	Mostly clouded till 9h, with circum. and cirstrat.; remainder quite clear	0.3	1.0	0.0	0.1	67.6	44.9	-
7 8	Quite clear Mostly clear till 21h; remainder clouded; circum., cumstrat., and haze	0.0 0.4	$0.6 \\ 0.0$	0.0	$0.0 \\ 0.0$	56.4 63.5	$\frac{40.7}{47.9}$	_
9	Generally clouded; circum., cumstrat., and haze	0.5	1.0	1.0	0.6	68.3	47.7	-
$\left\{\begin{array}{c}10\\11\end{array}\right\}$	Mostly clouded till 3h; circum. and haze; remainder clear	0.7	0.0	0.0	0.0	74.0	57°5 50°2	
12	Mostly clear; light cirstrat. in horizon	0.4	0.1	0.0	0.0	63.8	40.9	- I
13 14	Mostly clear till 21 ^h ; light cirstrat. in horizon; remainder clouded; circum. and cirstrat. Mostly clouded till 9 ^h ; circum. and cirstrat.; remainder of day clear	$0.8 \\ 0.0$	0.7 1.0	0.0	$0.0 \\ 1.0$	56.6 62.7	37.4 39.7	
15	Quite clear Clear till 16 ^h ; remainder clouded; circum. and haze	0.0	0.0	0.0	0.0	65.6	49.7	
16 17 }	Clouded; circum. and haze; distant thunder at 3 ^h	$\frac{1.0}{0.0}$	1.0	0.0	1.0	92.0	59.0 59.8	
18 \$	Generally clouded; cir. and haze; sheet lightning in W. at 9h		1.0	0.8	1.0 0.2	$\frac{82.2}{76.0}$	61.0 61.0	
19 20	Generally clouded; circum. and cumstrat; some heavy thunder showers	0.2	1.0	0.0	1.0	77.6	58.2	0.38
21	Mostly clouded; circum. and cumstrat.; a few clear spaces  Mostly clouded; cumstrat. and cirstrat.; faint auroral light in N. from 10 ^h to 12 ^h , rain }	0.8	1.0	0.9	0.8	73.6	52.0	-
$22$ $\left\{\right.$	from 18 ^h to 21 ^h	0.4	1.0	1.0	1.0	71.2	51.5	0.13
23 24 \	Clouded till 8h; circum. and cumstrat.; remainder of day clear	0.7 0.1	0.0	0.0	0.0	71.2 77.4	58°2 54°5	_
25 \	Generally clear			0.1	0.8	73.6	44.7	- 1
26	Mostly clouded; circum., cirstrat., and haze until 11 ^h ; remainder mostly clear - Clouded; cum., cumstrat., and haze; thunder, lightning, and slight rain from 6 ^h to 12 ^h , and )	1.0	0.8	0.0	0.6	76.2	56.0	-
27 {	from 17 ^h to 22 ^h	1.0	1.0	1.0	1.0	82.0	55.7	0.54
28 29	Generally clouded; cirstrat. and circum.  Mostly clouded till 8 ^h ; circum. and cirstrat.; remainder of day quite clear	0.9	0.0	0.0	0.0	77.4 71.8	64.4 53.7	_
30 {	Partially clear till 9h; sheet lightning and some slight rain from 8h to 12h; remainder of ]	0.3	1.0	0.3	1.0	75.6	20.0	0.02
00 }	day clouded; circum. and cumstrat.	J 0						

Toronto	Weather and Phenomena.			lloudy Sk	y.	Mar	M:		
Mean Time.	Weather and Phenomena.	3	9	17ª	21	Max. Therm.	Min. Therm.	Rain.	
D.	JULY.					0	0	In.	
$rac{1}{2}$	Clear Generally clouded; cirstrat. and haze; some rain and occasional thunder	0.0	0.0	1.0	1.0	78°0   66°6	51°5 45°4	0.16	
$\frac{2}{3}$	Mostly clouded till 3h; circum. and cum.; remainder clear; aurora at 10h and 11h	$\frac{0.2}{-}$	0.5	0.0	0.0	64.6	54.9	0 10	
4	Clouded till 4h; cir., circum., and haze; remainder mostly clear; aurora from 10h to 12h -	0.8	0.0	0.0	0.6	70.7	49.1		
5 C	Clear	0.5	0.0	0.4	0.0	70.6	44.1	-	
$\frac{6}{7}$	Mostly clouded; circum, and cirstrat	$\begin{bmatrix} 0.8 \\ 0.8 \end{bmatrix}$	$0.2 \\ 1.0$	$\begin{array}{c c} 0.8\\ 0.8 \end{array}$	$\frac{0.8}{1.0}$	72.3	48.7	_	
$\left\{ egin{array}{c} \dot{8} \\ 9 \end{array}  ight\}$	Clouded; cirstrat., circum., and haze	1.0	1.0			66.5	57.0	-	
10 {	Generally clouded; circum., cumstrat., cirstrat.; showers of rain, with thunder and	0.9	0.5	1.0	1.0	64.9	55.9	0.28	
11	lightning	0.8	0.7	1.0	1.0	69.5	61.2	_	
12	Mostly clouded; circum. and cumstrat.; distant thunder; some slight rain	1.0	0.7	0.7	() • 1	75.1	61.5	_	
13 14	Nearly clear; some slight circum, and cirstrat, round horizon Mostly clouded till 4 ^h ; circum, and cirstrat.; showers; remainder clear	$0.3 \ 0.7$	$\begin{bmatrix} 0.0 \\ 0.1 \end{bmatrix}$	$0.0 \\ 0.1$	$\frac{0.0}{0.5}$	76.8	59.7	0.14	
15	$\epsilon$	0.6	0.5			82.2	$\begin{vmatrix} 61.2 \\ 57.4 \end{vmatrix}$	U 14	
16 }	Partially clouded; circum. and cum.	_		0.0	0.9	74.2	52.7	-	
17 {	Clouded till 11 ^h ; cirstrat., circum., and haze; showers; sheet lightning; lunar rainbow at \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	0.9	0.6	0.4	0.3	61.7	45.7	0.28	
18	Clear from 9 ^h to 11 ^h ; remainder partly clouded; circum. and cumstrat.	0.8	0.0	0.2	0.6	72.2	49.2	-	
19 20	Mostly clouded; cir., circum., and cirstrat.; remainder nearly clear  Mostly clouded; circum., cirstrat., and haze	0.7	$\frac{1.0}{0.0}$	$\frac{1.0}{0.3}$	$\frac{0.7}{1.0}$	$78.5 \\ 79.2$	57°5 57°1	_	
21	Clouded; circum. and cirstrat.; showers during the day; steady rain from 12 ^h to 17 ^h	1.0	0.91	1.0	1.0	81.2	63.3	0.53	
22 7	Mostly clouded till 17 ^h ; cirstrat. and haze; remainder clear; showers of rain from 8 ^h to 9 ^h	1.0	0.5			77:1	64.7	0.08	
23 5	Clouded; circum. and cirstrat.; slight rain during the night	$\frac{-0.8}{0.8}$	1.0	0.7	0.0	69.0	57:7	0.15	
$\begin{array}{c c}24\\25\end{array}$	Mostly clouded; circum. and haze	0.8   0.7	0.4	0.7	$\frac{0.0}{1.0}$	72.4	90.6	0.50	
26	Mostly clouded; cirstrat. and haze; sheet lightning at 10 ^h and 11 ^h	0.8	1.0	1.0	1.0	75.4	54.5	0.02	
27	Mostly clear	0.5	0.1	1.0	0.4	72.8	64.3		
28 29	Partially clouded, with circum, and cumstrat.	$\begin{bmatrix} 0.3 \\ 0.3 \end{bmatrix}$	0.4	1.0	0.6	$76.2 \\ 76.1$	51.7		
$\frac{29}{30}$	Partially clouded; cirstrat. and cireum			1.0	0.7	73.6	49.9		
31 {	Mostly clouded till 9h; circum. and cirstrat.; remainder clear; showers of rain; sheet lightning at night	0.6	0.9	0.0	0.1	72.8	65.6	0.18	
`	AUGUST.								
1	Mostly clear; some light cum. and circum. occasionally	0.2	0:0	)					
2				1.0	0.0	78.6	59.9	l	
		0.7	0.0	1.0	0.0	73.6 73.1	52·2 49·7	_	
3 5	Mostly clouded; cirstrat. and haze Clouded all day; cirstrat., and haze; halo round the sun, diameter about 25°, at 3h;	0.7	0.7	1.0	1.0	73.1	49.7	0:23	
3 {	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night	0.7	0.7 1.0	1.0	1.0	73.1	49°7 52°5	0 20	
3 {	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h	0.7 1.0 1.0	0.7 1.0 1.0	1.0 0.6	1.0	73·1 77·2 73·7	49.7 52.5 63.3	0.31	
5 7	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night	0.7	0.7 1.0	1.0	1.0	73.1	49°7 52°5	0 20	
$\left\{ egin{array}{c} 5 \\ 6 \\ 7 \end{array}  ight\}$	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general	0.7 1.0 1.0 0.8 - 0.0	0.7 1.0 1.0 0.6 	1.0 0.0 0.0 0.0	0.0 0.0 1.0 1.0	73·1 77·2 73·7 74·8 71·8 71·2	49.7 52.5 63.3 64.0 51.8 48.7	0.31	
$\left\{ egin{array}{c} 5 \\ 6 \\ 7 \\ 8 \end{array} \right\}$	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h	0.7 1.0 1.0 0.8 	0.7 1.0 1.0 0.6 - 0.0 0.1	1'0 1'0 0'6  0'1 0'0 0'7	0.0 0.0 0.0 1.0	73·1 77·2 73·7 74·8 71·8 71·2 75·7	49.7   52.5   63.3   64.0   51.8   48.7   48.9	0.31	
$\left\{ egin{array}{c} 5 \\ 6 \\ 7 \\ 8 \\ 9 \end{array} \right\}$	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; misty at 16h and 17h	0.7 1.0 1.0 0.8 - 0.0	0.7 1.0 1.0 0.6 	1.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 1.0	73·1 77·2 73·7 74·8 71·8 71·2 75·7 79·1	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0	0.31	
5 6 7 8 9 10	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; misty at 16h and 17h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between	0.7 1.0 1.0 0.8 - 0.0 0.0 0.4	0.7 1.0 1.0 0.6 - 0.0 0.1 0.0	1'0 1'0 0'6 	0.0 0.0 0.0 1.0	73·1 77·2 73·7 74·8 71·8 71·2 75·7	49.7   52.5   63.3   64.0   51.8   48.7   48.9	0.31	
5 6 7 8 9 10 11 { 12 }	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general	0·7 1·0 1·0 0·8 	0.7 1.0 1.0 0.6 	1'0 1'0 0'6 0'1 0'0 0'7 0'0 0'2 0'7	1'0 1'0 1'0	73·1 77·2 73·7 74·8 71·8 71·2 75·7 79·1 83·0 84·9 84·4	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3	0.31	
5 } 7 8 9 10 11 { 12 } 13 }	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.	0·7 1·0 1·0 0·8 - 0·0 0·0 0·4 0·2 0·9 0·2	0.7 1.0 1.0 0.6 - 0.0 0.1 0.0 0.1 0.8 0.7	1'0 1'0 0'6 - 0'1 0'0 0'7 0'0 0'2 0'7 - 0'5	1'0 1'0	73·1 77·2 73·7 74·8 71·8 71·2 75·7 79·1 83·0 84·9 84·4 81·2	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5	0.31	
5 } 8 9 10 11 { 12 } 13 }	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clear; some light circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.  Mostly clear; some light circum. circum. clightning in W. and N.W. at 9h	0·7 1·0 1·0 0·8 - 0·0 0·0 0·4 0·2 0·9 0·2 - 0·3	0.7 1.0 1.0 0.6 -0.0 0.1 0.0 0.1 0.8 0.7 0.1	1'0 1'0 0'6 - 0'1 0'0 0'7 0'0 0'2 0'7 - 0'5 0'4	1'0 1'0	73·1 77·2 73·7 74·8 71·8 71·9 75·7 79·1 83·0 84·9 84·4 81·2 80·0	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2	0.31	
5 } 7 8 9 10 11 { 12 } 13 }	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clear; some light circum. distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.; distant thunder in N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum. and cirstrat., and haze; some slight rain and distant thunder during the	0·7 1·0 1·0 0·8 - 0·0 0·0 0·4 0·2 0·9 0·2	0.7 1.0 1.0 0.6 - 0.0 0.1 0.0 0.1 0.8 0.7	1'0 1'0 0'6 - 0'1 0'0 0'7 0'0 0'2 0'7 - 0'5	1'0 1'0	73·1 77·2 73·7 74·8 71·8 71·2 75·7 79·1 83·0 84·9 84·4 81·2	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5	0.31	
5	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clear; some light circum. distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.; distant thunder in N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum., cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; cumstrat. and circum.	0·7 1·0 1·0 0·8 — 0·0 0·4 0·2 0·9 0·2 — 0·3 1·0 1·0	0.7 1.0 1.0 0.6 	1'0 1'0 0'6	1'0 1'0	73·1 77·2 73·7 74·8 71·9 71·9 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5	0.31	
5	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.  Mostly clear; some light cir. and circum.; lightning in W. and N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum., cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; cumstrat. and circum.; remainder clear	0·7 1·0 1·0 0·8 — 0·0 0·4 0·2 0·9 0·2 — 0·3 1·0 1·0 0·8	0.7 1.0 1.0 0.6 	1'0 1'0 0'6	1'0 1'0	73·1 77·2 73·7 74·8 71·8 71·2 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8 66·0	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5   59.8	0.31	
5 } 7 8 9 10 11 { 12 } 13 } 14 15 16 { 17	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; misty at 16h and 17h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.  Mostly clear; some light cir. and circum.; lightning in W. and N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum., cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; cumstrat. and circum.; remainder clear  Mostly clouded till 3h; cumstrat. and circum.; remainder clear	0·7 1·0 1·0 0·8 — 0·0 0·4 0·2 0·9 0·2 — 0·3 1·0 1·0	0.7 1.0 1.0 0.6 	1'0 1'0 0'6	1'0 1'0	73·1 77·2 73·7 74·8 71·9 71·9 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5	0.31 	
5	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; misty at 16h and 17h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.  Mostly clear; some light cir. and circum.; lightning in W. and N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum. and cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; cumstrat. and circum.; remainder clear  Generally clear till 9h; remainder clouded; cir. and haze  Clear; aurora from 9h to 11h	0·7 1·0 1·0 0·8 — 0·0 0·0 0·4 0·2 0·9 0·2 — 0·3 1·0 1·0 0·8 0·9	0.7 1.0 0.6 0.0 0.1 0.0 0.1 0.8 0.7 	1'0 1'0 0'6 - 0'1 0'0 0'7 0'0 0'2 0'7 - 0'5 0'4 1'0 1'0 0'0 - 1'0 0'0	1'0 1'0 0'0 0'0 0'0 0'0 0'7 0'5	73·1 77·2 73·7 74·8 71·2 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8 66·0 74·0 73·8 73·1	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5   59.8   56.2   51.9   55.5	0.31	
5 } 7 8 9 10 11 { 12 13 } 14 15 16 { 17 18 19 20 } 21 22	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.  Mostly clear; some light cir. and circum.; lightning in W. and N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum., cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; cumstrat. and circum.; remainder clear  Generally clear till 9h; remainder clouded; cir. and haze  Clear; aurora from 9h to 11h  Partially clouded; cirstrat. and haze	0·7 1·0 1·0 0·8 	0.7 1.0 0.6 0.0 0.1 0.0 0.1 0.8 0.7 0.1 1.0 0.1 0.0 0.1 0.0	1'0 1'0 0'6 - 0'1 0'0 0'7 0'0 0'2 0'7 - 0'5 0'4 1'0 1'0 0'0 - 1'0 0'0 0'8	1'0 1'0 0'0 0'0 0'0 0'0 0'7 0'5 0'3 1'0 1'0 0'5 0'0 1'0 0'1 0'3	73·1 77·2 73·7 74·8 71·9 71·9 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8 66·0 74·0 73·8 73·1 71·4	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5   59.8   56.2   51.9   53.6	0.31 	
5 } 7 8 9 10 11 { 12 13 } 14 15 16 { 17 18 19 20 21 22 23	Mostly clouded; cirstrat. and haze  Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.; lightning in W. and N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum. and cirstrat.  Clouded; circum., cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; circum., cirstrat. and circum.; remainder clear  Generally clouded till 3h; cumstrat. and circum.; remainder clear  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; circum. and cirstrat.; halo round the sun at 21h and 22h, diam. 40°, perfect	0·7 1·0 1·0 0·8 — 0·0 0·0 0·4 0·2 0·9 0·2 — 0·3 1·0 1·0 0·8 0·9	0.7 1.0 0.6 0.0 0.1 0.0 0.1 0.8 0.7 	1'0 1'0 0'6 - 0'1 0'0 0'7 0'0 0'2 0'7 - 0'5 0'4 1'0 1'0 0'0 - 1'0 0'0	1'0 1'0 0'0 0'0 0'0 0'0 0'7 0'5	73·1 77·2 73·7 74·8 71·9 71·9 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8 66·0 74·0 73·8 73·1 71·4 73·8	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5   59.8   56.2   51.9   53.6   59.1	0.31	
5 } 7 8 9 10 11 { 12 } 13 } 14 15   16 { 17 18 19 } 20 21 22 23 24 25	Mostly clouded; cirstrat. and haze Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.; lightning in W. and N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum. and cirstrat.  Clouded; circum., cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; circum., cirstrat. and circum.; remainder clear  Generally clear till 9h; remainder clouded; cir. and haze  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat. and haze	0·7 1·0 1·0 0·8 	0.7 1.0 0.6 	1'0 1'0 0'6 - 0'1 0'0 0'7 0'0 0'2 0'7 - 0'5 0'4 1'0 1'0 0'0 - 1'0 0'0 0'8 1'0	1'0 1'0	73·1 77·2 73·7 74·8 71·8 71·9 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8 66·0 74·0 73·8 73·1 71·4 73·8 75·8 74·4	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5   59.8   53.6   59.1   61.5   60.0	0.31	
5 } 7 8 9 10 11 { 12 } 13 } 14 15 16 { 17 18 19 } 21 22 23 24 25 26 }	Mostly clouded; cirstrat. and haze Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.  Mostly clear; some light cir. and circum.; lightning in W. and N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum., cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; circum., cirstrat. and circum.; remainder clear  Generally clouded till 3h; cumstrat. and circum.; remainder clear  Generally clear till 9h; remainder clouded; cir. and haze  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat. and circum. and cirstrat.; some rain during the night  Generally clouded; cirstrat. and haze  Mostly clouded; cirstrat. and haze  Mostly clouded; cirstrat. and haze  Mostly clouded; cirstrat. and haze  Mostly clouded; cirstrat. and haze	0·7 1·0 1·0 0·8 	0.7 1.0 0.6 0.0 0.1 0.0 0.1 0.8 0.7 0.1 1.0 1.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.1 0.0 0.0	1'0 1'0 0'6 - 0'1 0'0 0'7 0'0 0'2 0'7 - 0'5 0'4 1'0 1'0 0'0 - 1'0 0'8 1'0 1'0 0'0	1'0 1'0	73·1 77·2 73·7 74·8 71·8 71·8 71·9 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8 66·0 74·0 73·8 73·1 71·4 73·8 75·8 74·4 75·4	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5   59.8   53.6   59.1   61.5   60.0   58.5	0.31	
5 } 7 8 9 10 11 { 12 } 13 14 15 16 { 17 18 19 20 21 22 23 24 25 26 27 }	Mostly clouded; cirstrat. and haze Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.; distant thunder in N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum. and cirstrat.  Clouded; circum., cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; circum., cirstrat. and circum.; remainder clear  Generally clouded till 3h; cumstrat. and circum.; remainder clear  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; circum. and cirstrat.; halo round the sun at 2h and 22h, diam. 40°, perfect  Mostly clear; very bright perfect halo round the sun at 1h 30′ of the 27th, diameter about 40°; sky hazy; sun shining dimly	0·7 1·0 1·0 0·8 — 0·0 0·0 0·4 0·2 0·9 0·2 — 0·3 1·0 1·0 0·8 0·2 — 0·4 0·6 0·4 0·7 0·6 0·6 0·6 0·6 0·6 0·7 0·7 0·8 0·9 0·9 0·9 0·9 0·9 0·9 0·9 0·9	0.7 1.0 0.6 0.0 0.1 0.0 0.1 0.8 0.7 	1'0 1'0 0'6 - 0'1 0'0 0'7 0'0 0'2 0'7 - 0'5 0'4 1'0 1'0 0'0 - 1'0 0'8 1'0 0'0 - 1'0	1'0 1'0	73·1 77·2 73·7 74·8 71·2 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8 66·0 74·0 73·8 73·1 71·4 73·8 75·8 75·8 75·8 75·8 75·8	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5   59.8   56.2   51.9   55.5   53.6   59.1   61.5   60.0   58.5   57.4	0.31	
5 } 6 } 7 8 9 10 11 { 12 } 13 } 14 15 16 { 17 18 19 } 21 22 23 24 25 26 27 } 28 {	Mostly clouded; cirstrat. and haze Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.; lightning in W. and N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum., cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; circum, cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; circum., cirstrat., and circum.; remainder clear  Generally clouded till 3h; cumstrat. and circum.; remainder clear  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Clouded till 4h; cirstrat., circum., and haze; thunder in S.W. and N.W. at 2h and 3h; aurora from 10h to 11h	0·7 1·0 1·0 0·8	0·7 1·0 1·0 0·6 - 0·0 0·1 0·0 0·1 0·8 0·7 - 0·1 1·0 1·0 0·1 0·0 0·4 0·6 0·9 0·5 0·0 - 0·2	1'0 1'0 0'6	1'0 1'0 1'0 0'0 0'0 0'0 0'0 0'7 0'5 0'3 1'0 1'0 0'5 0'0 1'0 0'1 0'3 0'9 1'0 0'7 1'0 0'0	73·1 77·2 73·7 74·8 71·8 71·2 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8 66·0 74·0 73·8 73·1 71·4 73·8 75·8 75·7 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1 70·1	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5   59.8   56.2   51.9   55.5   53.6   59.6   59.6   60.0   58.5   57.4   66.9	0.31	
5 } 7 8 9 10 11 { 12 } 13 14 15 16 { 17 18 19 20 21 22 23 24 25 26 27 }	Mostly clouded; cirstrat. and haze Clouded all day; cir., cirstrat., and haze; halo round the sun, diameter about 25°, at 3h; showers during the night  Mostly clouded; circum., cirstrat., and haze; showers between 6h and 7h  Partially clear; circum. and haze general  Clear; mist at night  Mostly clear; aurora at night from 9h to 11h  Mostly clear; some light circum. occasionally  Mostly clouded; cirstrat. and circum.; distant thunder in N.W. at 4h; slight rain between 6h and 7h  Mostly clear; some cum. and circum.; distant thunder in N.W. at 9h  Clouded; circum. and cirstrat.  Clouded; circum. and cirstrat.  Clouded; circum., cirstrat., and haze; some slight rain and distant thunder during the day; rain at night  Clouded; circum., cirstrat. and circum.; remainder clear  Generally clouded till 3h; cumstrat. and circum.; remainder clear  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat. and haze  Generally clouded; cirstrat., cir., and cumstrat.; some rain during the night  Generally clouded; circum. and cirstrat.; halo round the sun at 2h and 22h, diam. 40°, perfect  Mostly clear; very bright perfect halo round the sun at 1h 30′ of the 27th, diameter about 40°; sky hazy; sun shining dimly	0·7 1·0 1·0 0·8 — 0·0 0·0 0·4 0·2 0·9 0·2 — 0·3 1·0 1·0 0·8 0·2 — 0·4 0·6 0·4 0·7 0·6 0·6 0·6 0·6 0·7 0·7 0·8 0·9 0·9 0·9 0·9 0·9 0·9 0·9 0·9	0.7 1.0 0.6 0.0 0.1 0.0 0.1 0.8 0.7 	1'0 1'0 0'6 - 0'1 0'0 0'7 0'0 0'2 0'7 - 0'5 0'4 1'0 1'0 0'0 - 1'0 0'8 1'0 0'0 - 1'0	1'0 1'0	73·1 77·2 73·7 74·8 71·2 75·7 79·1 83·0 84·9 84·4 81·2 80·0 87·0 78·6 77·8 66·0 74·0 73·8 73·1 71·4 73·8 75·8 75·8 75·8 75·8 75·8	49.7   52.5   63.3   64.0   51.8   48.7   48.9   53.0   58.8   61.1   63.3   63.5   63.2   68.0   68.2   62.5   59.8   56.2   51.9   55.5   53.6   59.1   61.5   60.0   58.5   57.4	0.31	

^a In the last column under the head of Clouded Sky the 17^h has been substituted for the 15^h, commencing with the new system of observation on 1st July, 1848.

Toronto Mean	Weather and Phenomena.	E2	tent of C	loudy Sk	у.	Max.	Min.	Da!
Time.	weather and Phenomena.	3	9	17	21	Therm.	Therm.	Rain.
D.	SEPTEMBER.					0	0	In.
1	Generally a few clear spaces till 17 ^h ; remainder clouded; circum, and cirstrat	0.9	0.9	0.7	1.0	76.7	62.6	
$\{2, \}$	Clear till 9h; remainder clouded; cum. and circum.	0.3	0.0			71.0	58.0	—
3 }	Mostly clear from 4 ^h to 11 ^h ; remainder clouded; circum. and haze; aurora at 10 ^h -			1.0	0.9	73.4	51.0	_
$rac{4}{5}$	Quite clear	0.3	0.0	$\frac{0.0}{0.8}$	$0.0 \\ 0.8$	77.4	59.2	-
6	Generally clear	$0.1 \\ 0.2$	0.0	0.0	0.0	$80.4 \\ 73.4$	58.5 48.2	_
$\overset{\circ}{7}$	Quite clear	0.0	0.0	0.0	0.1	68.0	40.1	_
8	Clouded from 0h to 4h, and at 21h; eireum. and eirstrat.; remainder clear	1.0	0.0	$0.3 \\ 0.3$	0.8	68.0	$\frac{10.7}{49.7}$	_
9 }	Clear at 4h and 15h; remainder mostly clouded; circum. and cirstrat.; lightning, thunder,	0.7	0.0			73.8	45.6	
10 }	and rain during the night			0.6	1.0	65.0	38.7	0.13
11 {	Clouded; circum. and cirstrat.; thunder, lightning, and showers of rain during the day	1.0	1.0	1.0	0.8	69.2	54.7	0.2
12	and night	0.6	0.1			1		0 -
12	Generally clear till 4 ^h ; remainder clouded; cir., cirstrat., and haze; commenced rain at	. 00	0 1	0.0	0.1	65.4	48.9	-
$13 \stackrel{\checkmark}{\downarrow}$	17 ^h ; halo round the sun at 4 ^h , diameter 40°, perfect; halo round the moon at 9 ^h , 10 ^h , and	0.0	1.0	1.0	1.0	59.6	37.2	l
į,	11h, diameter 40°, perfect		- "	1 0		1000	0, 2	_
14	Clouded all day; rain at intervals, accompanied by lightning and thunder	1.0	1.0	0.6	1.0	60.4	47.0	1.00
15	Clouded till 2 ^h ; circum. and cumstrat.; remainder clear; boards white with frost	0.4	0.0	0.0	0.0	58.3	50.2	_
$\left\{ \begin{array}{c} 16 \\ 17 \end{array} \right\}$	Mostly clear till 3h; remainder clouded; circum. and haze; rain	0.1	1.0			57.4	35.1	
18	Clouded all day	1.0	1:0	1.0	1.0	55.4	46.7	0.6
19	Clouded all day; circum. and cirstrat.; constant rain most of the day	1.0	1.0	$\frac{1.0}{1.0}$	0.0	60.7	52.4 50.7	0.5
20	Mostly clouded; circum. and cirstrat.; some rain; aurora at 9h	0.6	0.6	1.0	0.4		51.7	0.2
21	Partially clear; circum. general; some showers of rain; hoar frost	0.0	0.2	0.5	0.0	59.4	40.7	0.0
22	Generally clear	0.3	0.0	0.1	0.5	52.4	36.5	_
$23$ }	Mostly clear; some circum. detached	0.4	0.5	_		48.2	30.9	
24 }	1 -	-		0.9	0.9	60.8	46.8	
$\begin{array}{c} 25 \\ 26 \end{array}$	Partially clouded till 2 ^h ; cir-cum. and cumstrat.; remainder mostly clear  Mostly clear	0.2	0.0	0.1	0.4	55.8	42.3	-
$\frac{20}{27}$	Clouded; cirstrat., circum., and haze	$0.2 \\ 1.0$	0.1	0.0	0.1	59.8	30.5	
$\frac{2}{28}$	Clouded; cumstrat. and circum.; slight rain	1.0	1.0	0.6 1.0	1.0	47.9	28.1	0.20
29	Generally clouded; circum. and cirstrat.; aurora from 9h to 11h; rain	1.0	0.2	1.0	0.7	51.0	44.3	0.10
30	Mostly clouded; circum., cirstrat., and haze; aurora from 9h to 11h -	0.7	0.6			59.0	35.5	_
	0.0000							
1	OCTOBER.							
1			i l					
9	Generally overcast; circum. and cirstrat			1.0	1.0		39.2	
2	Clouded; cirstrat. and haze; slight rain from 0h to 9h	1.0	1.0	1.0	1.0	49.3	44.1	0.5
$\begin{array}{c} 2 \\ 3 \\ 4 \end{array}$	Ch 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.8	1.0	1.0	1.0	49.3	44.1	0.5
$\frac{2}{3}$	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze	0.8 1.0	1.0	1.0 1.0	1.0 1.0	49°3 51°8 57°8	44.1 47.7 51.5	0.5
$egin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{array}$	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze	0.8	1.0	1.0	1.0 1.0 1.0	49°3 51°8 57°8 58°5	44.1 47.7 51.5 46.7	0.5
2 3 4 5 6 7	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze	0.8 1.0 1.0	1.0 1.0 0.2	1.0 1.0 1.0	1.0 1.0	49°3 51°8 57°8	44.1 47.7 51.5	
2 3 4 5 6 7 8	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Close till the regionary alouded; cir. cum and cumstrat.	0.8 1.0 1.0 1.0	1.0 1.0 0.2 1.0 1.0	1.0 1.0 1.0 1.0 - 0.5	0.0 1.0 1.0 1.0 1.0	49.3 51.8 57.8 58.5 57.7 52.0 61.0	44.1 47.7 51.5 46.7 44.5 46.6 40.2	
2 3 4 5 6 7 8 9	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze	0.8 1.0 1.0 1.0 	1.0 1.0 0.2 1.0 1.0	1.0 1.0 1.0 1.0 1.0 - 0.5 0.8	1.0 1.0 1.0 1.0 0.0	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0	44.1 47.7 51.5 46.7 44.5 46.6 40.2 31.3	0.5
2 3 4 5 6 7 8 9	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze  Mostly clear	0.8 1.0 1.0 1.0 1.0 0.0 0.2	1'0 1'0 0'2 1'0 1'0 -	1.0 1.0 1.0 1.0 1.0 - 0.5 0.8 0.0	1.0 1.0 1.0 1.0 0.0 0.4 0.0	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0 57°4	44.1 47.7 51.5 46.7 44.5 46.6 40.2 31.3 49.5	
2 3 4 5 6 7 8 9	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze  Mostly clear	0.8 1.0 1.0 1.0 1.0 	1.0 0.2 1.0 1.0 0.0 0.0 0.0	1.0 1.0 1.0 1.0 1.0 - 0.5 0.8 0.0 0.4	1.0 1.0 1.0 0.0 0.4 0.0 0.4	49.3 51.8 57.8 58.5 57.7 52.0 61.0 50.0 57.4 54.6	44.1 47.7 51.5 46.7 44.5 46.6 40.2 31.3 49.5 24.5	0.5
2 3 4 5 6 7 8 9 10 11 12 13	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze  Mostly clear  Mostly clear  Partially clouded; circircum., and cirstrat.	0.8 1.0 1.0 1.0 1.0 0.0 0.2	1'0 1'0 0'2 1'0 1'0 -	1.0 1.0 1.0 1.0 1.0 - 0.5 0.8 0.0 0.4 1.0	1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 0.0	49.3 51.8 57.8 58.5 57.7 52.0 61.0 50.0 57.4 54.6 48.4	44.1 47.7 51.5 46.7 44.5 46.6 40.2 31.3 49.5 24.5 31.4	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze  Mostly clear  Mostly clear  Partially clouded; cir., circum., and cirstrat.  Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear	0.8 1.0 1.0 1.0 1.0 0.0 0.2 0.0 0.0	1.0 0.2 1.0 1.0 0.0 0.0 0.0 0.0	1.0 1.0 1.0 1.0 1.0 - 0.5 0.8 0.0 0.4	1.0 1.0 1.0 0.0 0.4 0.0 0.4	49.3 51.8 57.8 58.5 57.7 52.0 61.0 50.0 57.4 54.6	44.1 47.7 51.5 46.7 44.5 46.6 40.2 31.3 49.5 24.5	0.5
2 3 4 5 6 7 8 9 10 11 12 13	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze  Mostly clear  Mostly clear  Mostly clear  Partially clouded; cir., circum., and cirstrat.  Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear  Quite clear till 17 ^h ; remainder clouded; circum., cirstrat., and haze	0.8 1.0 1.0 1.0 1.0 0.0 0.2 0.0 0.0 0.8	1.0 1.0 0.2 1.0 1.0 0.0 0.0 0.0 0.0 0.4	1.0 1.0 1.0 1.0 1.0 - 0.5 0.8 0.0 0.4 1.0	1.0 1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0	49.3 51.8 57.8 58.5 57.7 52.0 61.0 50.0 57.4 54.6 48.4 59.0	44.1 47.7 51.5 46.7 44.5 46.6 40.2 31.3 49.5 24.5 31.4 39.5	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze  Mostly clear  Mostly clear  Partially clouded; cir., circum., and cirstrat.  Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear  Quite clear till 17 ^h ; remainder clouded; circum., cirstrat., and haze  Clouded all day; circum., cirstrat., and haze; slight rain from 6 ^h to 10 ^h , and some during }	0.8 1.0 1.0 1.0 1.0 0.0 0.2 0.0 0.8 0.6	1.0 1.0 0.2 1.0 1.0 0.0 0.0 0.0 0.0 0.4 0.0	1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'1 	1.0 1.0 1.0 1.0 1.0 0.0 0.4 1.0 - 1.0	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0 57°4 54°6 48°4 59°0 48°0 61°0	44.1 47.7 51.5 46.7 44.5 46.6 40.2 31.3 49.5 24.5 31.4 39.5 33.9 36.7	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 {	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze  Mostly clear  Mostly clear  Mostly clear  Partially clouded; cir., circum., and cirstrat.  Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear  Quite clear till 17 ^h ; remainder clouded; circum., cirstrat., and haze  Clouded all day; circum., cirstrat., and haze; slight rain from 6 ^h to 10 ^h , and some during the night	0.8 1.0 1.0 1.0 1.0 0.0 0.2 0.0 0.8 0.6 -	1.0 1.0 0.2 1.0 1.0 0.0 0.0 0.0 0.0 0.4 0.0 	1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'1 0'0 1'0	1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0 1.0	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0 57°4 54°6 48°4 59°0 61°0 58°6	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   31.4   39.5   33.9   36.7   46.5	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 {17	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze  Mostly clear  Mostly clear  Mostly clear  Partially clouded; cir., circum., and cirstrat.  Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear  Quite clear till 17 ^h ; remainder clouded; circum., cirstrat., and haze  Clouded all day; circum., cirstrat., and haze; slight rain from 6 ^h to 10 ^h , and some during the night  Clouded all day; cumstrat. and circum.	0.8 1.0 1.0 1.0 1.0 0.0 0.2 0.0 0.0 0.8 0.6 	1.0 1.0 0.2 1.0 1.0 0.0 0.0 0.0 0.0 0.4 0.0	1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'1 	1.0 1.0 1.0 1.0 1.0 0.0 0.4 1.0 - 1.0	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0 57°4 54°6 48°4 59°0 48°0 61°0	44.1 47.7 51.5 46.7 44.5 46.6 40.2 31.3 49.5 24.5 31.4 39.5 33.9 36.7	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 {	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat., and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze  Mostly clear  Mostly clear  Mostly clear  Partially clouded; cir., circum., and cirstrat.  Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear  Quite clear till 17 ^h ; remainder clouded; circum., cirstrat., and haze  Clouded all day; circum., cirstrat., and haze; slight rain from 6 ^h to 10 ^h , and some during the night  Clouded all day; cumstrat. and circum.  Clouded all day; cumstrat., cirstrat., circum., and haze; auroral light through the clouds	0.8 1.0 1.0 1.0 1.0 0.0 0.2 0.0 0.8 0.6 -	1.0 1.0 0.2 1.0 1.0 0.0 0.0 0.0 0.0 0.4 0.0 	1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'1 0'0 1'0	1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0 1.0	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0 57°4 54°6 48°4 59°0 61°0 58°6	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   31.4   39.5   33.9   36.7   46.5	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 {17	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night  Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze  Mostly clear  Mostly clear  Mostly clear  Partially clouded; cir., circum., and cirstrat.  Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear  Quite clear till 17 ^h ; remainder clouded; circum., cirstrat., and haze  Clouded all day; circum., cirstrat., and haze; slight rain from 6 ^h to 10 ^h , and some during the night  Clouded all day; cumstrat. and circum.  Clouded all day; cumstrat. and cirstrat., cirstrat., and haze; auroral light through the clouds and content of the cloudes and cirstrat., cirstrat., circum., and haze; auroral light through the clouds and content of the cloudes and cirstrat., cirstrat., circum., and haze; auroral light through the cloudes and content of the cloudes and circum.	0.8 1.0 1.0 1.0 0.0 0.2 0.0 0.8 0.6 	1.0 1.0 0.2 1.0 1.0 0.0 0.0 0.0 0.4 0.0 	1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'0 1'0 1'0 1'0	1.0 1.0 1.0 1.0 0.0 0.4 1.0 1.0 1.0 1.0	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0 57°4 54°6 48°4 59°0 48°0 61°0 58°6 61°8 39°4	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   31.4   39.9   36.7   46.5   36.7   30.2	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 { 17 18 { 19 20	Clouded; cirstrat. and haze; slight rain from 0h to 9h Mostly clouded; cirstrat. and haze  Clouded; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze  Densely clouded all day; circum., cirstrat., and haze  Mostly clouded; circum., cirstrat., and haze; rain from 5h to 8h Partially clouded; circum. and cumstrat.; aurora at night Clear till 4h; remainder clouded; circum., cumstrat., and haze  Mostly clear  Mostly clear  Mostly clear  Partially clouded; cir., circum., and cirstrat.  Clouded till 3h, with circum. and cirstrat.; remainder of day clear Quite clear till 17h; remainder clouded; circum., cirstrat., and haze  Clouded all day; circum., cirstrat., and haze; slight rain from 6h to 10h, and some during the night  Clouded all day; cumstrat. and circum.  Clouded all day; cumstrat., cirstrat., circum., and haze; auroral light through the clouds at night  Clouded all day; cirstrat. and haze  Clouded all day; cirstrat. and haze  Clouded all day; cirstrat. and haze	0.8 1.0 1.0 1.0 1.0 0.0 0.2 0.0 0.0 0.8 0.6 	1.0 1.0 0.2 1.0 1.0 0.0 0.0 0.0 0.4 0.0 	1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'1 - 0'0 1'0 1'0 1'0	1.0 1.0 1.0 1.0 0.0 0.4 1.0 	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0 57°4 54°6 48°4 59°0 48°0 61°0 58°6 61°8 39°4 36°6	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   33.9   36.7   46.5   36.7   30.2   34.8	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 { 17 18 { 19 20 21	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat., and haze Clouded; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze Densely clouded all day; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night Clear till 4 ^h ; remainder clouded; circum., cunstrat., and haze Mostly clear Mostly clear Mostly clear Partially clouded; cir., circum., and cirstrat. Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear Quite clear till 17 ^h ; remainder clouded; circum., cirstrat., and haze Clouded all day; circum., cirstrat., and haze; slight rain from 6 ^h to 10 ^h , and some during the night Clouded all day; cumstrat. and circum. Clouded all day; cumstrat. and haze at night Clouded all day; cirstrat., cirstrat., circum., and haze; auroral light through the clouds at night Clouded all day; cirstrat. and haze Clouded all day; cirstrat. and haze Clouded all day; cirstrat. and haze Mostly clouded; cirstrat., cirstrat., and haze Mostly clouded; cirstrat., cirstrat., and haze	0.8 1.0 1.0 1.0 0.0 0.2 0.0 0.8 0.6 	1.0 0.2 1.0 0.0 0.0 0.0 0.0 0.0 0.4 0.0 1.0 1.0	1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'1 - 0'0 1'0 1'0 1'0 1'0	1.0 1.0 1.0 1.0 0.4 0.0 0.4 1.0 1.0 1.0 1.0	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0 57°4 54°6 48°4 59°0 48°0 61°0 58°6 61°8 39°4	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   33.9   36.7   46.5   36.7   30.2   34.8   39.7	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 { 17 18 { 19 20 21 22	Clouded; cirstrat. and haze; slight rain from 0h to 9h Mostly clouded; cirstrat. and haze Clouded; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze Densely clouded all day; circum., cirstrat., and haze; rain from 5h to 8h Partially clouded; circum. and cumstrat.; aurora at night Clear till 4h; remainder clouded; circum., cumstrat., and haze Mostly clear Mostly clear Mostly clear Partially clouded; cir., circum., and cirstrat. Clouded till 3h, with circum. and cirstrat.; remainder of day clear Quite clear till 17h; remainder clouded; circum., cirstrat., and haze Clouded all day; circum., cirstrat., and haze; slight rain from 6h to 10h, and some during the night Clouded all day; cumstrat. and circum. Clouded all day; cumstrat. and circum. Clouded all day; cirstrat., circum., and haze; auroral light through the clouds at night Clouded all day; cirstrat. and haze Clouded all day; cirstrat. and haze Clouded all day; cirstrat., cirstrat., and haze Mostly clouded; cirstrat., circum., and haze Mostly clouded; circum., cirstrat., and cumstrat.	0.8 1.0 1.0 1.0 1.0 0.2 0.0 0.8 0.6 - 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	1.0 0.2 1.0 0.0 1.0 0.0 0.0 0.0 0.4 0.0 1.0 1.0 1.0 1.0	1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'1 0'0 1'0 1'0 1'0 1'0 1'0	1.0 1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0 1.0 1.0 1.0	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0 57°4 54°6 48°4 59°0 48°0 61°0 58°6 61°8 39°4 36°6 44°0	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   33.9   36.7   46.5   36.7   30.2   34.8	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 { 19 20 21 22 23	Clouded; cirstrat. and haze; slight rain from 0h to 9h Mostly clouded; cirstrat. and haze Clouded; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze Densely clouded all day; circum., cirstrat., and haze; rain from 5h to 8h Partially clouded; circum. and cumstrat.; aurora at night Clear till 4h; remainder clouded; circum., cumstrat., and haze Mostly clear Mostly clear Mostly clear Partially clouded; cir., circum., and cirstrat. Clouded till 3h, with circum. and cirstrat.; remainder of day clear Quite clear till 17h; remainder clouded; circum., cirstrat., and haze Clouded all day; circum., cirstrat., and haze; slight rain from 6h to 10h, and some during the night Clouded all day; cumstrat. and circum. Clouded all day; cumstrat. and haze Clouded all day; cirstrat., circum., and haze; auroral light through the clouds at night Clouded all day; cirstrat. and haze Clouded all day; cirstrat., cirstrat., and haze Mostly clouded; cirstrat., cirstrat., and cumstrat. Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; cir., circum., and haze; aurora at 9h	0.8 1.0 1.0 1.0 1.0 0.2 0.0 0.8 0.6 - 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	1.0 1.0 0.2 1.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0 1	1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'1 0'0 1'0 1'0 1'0 1'0 1'0 1'0	1.0 1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0 1.0 1.0 1.0 0.2 	49·3 51·8 57·8 58·5 57·7 52·0 61·0 50·0 57·4 48·0 61·0 58·6 61·8 39·4 36·6 44·0 46·5 47·5 45·0	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   33.9   36.7   46.5   36.7   30.2   34.8   39.7   36.2	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 { 17 18 { 19 20 21 22 23 24	Clouded; cirstrat. and haze; slight rain from 0h to 9h Mostly clouded; cirstrat. and haze Clouded; circum., cirstrat., and haze Mostly clouded all day; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze; rain from 5h to 8h Partially clouded; circum. and cumstrat.; aurora at night Clear till 4h; remainder clouded; circum., cumstrat., and haze Mostly clear Mostly clear Mostly clear Partially clouded; cir., circum., and cirstrat. Clouded till 3h, with circum. and cirstrat. Clouded till 3h, with circum. and cirstrat.; remainder of day clear Quite clear till 17h; remainder clouded; circum., cirstrat., and haze Clouded all day; circum., cirstrat., and haze; slight rain from 6h to 10h, and some during the night Clouded all day; cumstrat. and circum. Clouded all day; cumstrat., cirstrat., circum., and haze; auroral light through the clouds at night Clouded all day; cirstrat. and haze Mostly clouded; cirstrat., cirstrat., and haze Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum., and haze; aurora at 9h Mostly clouded; circum. and cumstrat; rain	0.8 1.0 1.0 1.0 1.0 0.2 0.0 0.8 0.6 1.0 1.0 1.0 1.0 1.0 0.8 0.8 0.9	1.0 0.2 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0 1.0	1'0 1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'1 0'0 1'0 1'0 1'0 1'0 0'3	1.0 1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0 1.0 1.0 0.2 	49°3 51°8 57°8 58°5 57°7 52°0 61°0 50°0 57°4 54°6 48°4 59°0 48°0 61°0 58°6 61°8 39°4 36°6 44°0 46°5 47°5 45°0 46°5	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   33.9   36.7   46.5   30.2   34.8   39.7   36.2   26.7   31.0   40.7	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 { 17 18 20 21 22 23 24 25	Clouded; cirstrat. and haze; slight rain from 0h to 9h Mostly clouded; cirstrat. and haze Clouded; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze Densely clouded all day; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze; rain from 5h to 8h Partially clouded; circum. and cumstrat.; aurora at night Clear till 4h; remainder clouded; circum., cunstrat., and haze Mostly clear Mostly clear Mostly clear Mostly clear Mostly clear Quite clear till 17h; remainder clouded; cirstrat. Clouded till 3h, with circum. and cirstrat. Clouded all day; circum., cirstrat., and haze; slight rain from 6h to 10h, and some during the night Clouded all day; circum., cirstrat., circum., and haze; auroral light through the clouds at night Clouded all day; cirstrat. and circum. Clouded all day; cirstrat., cirstrat., and haze Mostly clouded; cirstrat., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum., and haze; aurora at 9h Mostly clouded; circum. and cumstrat; rain Mostly clouded; cirstrat. and haze; aurora at 9h to 12h; rain from 15h to 17h	0.8 1.0 1.0 1.0 0.2 0.0 0.8 0.6 - 1.0 1.0 1.0 1.0 0.8 0.9 0.9	1.0 1.0 0.2 1.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0 1	1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'1 0'0 1'0 1'0 1'0 1'0 0'3 1'0	1.0 1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0 1.0 1.0 1.0 0.2 0.5 1.0 0.2 0.8	49·3 51·8 57·8 58·5 57·7 52·0 61·0 50·0 57·4 54·6 48·0 61·0 58·6 61·8 39·4 36·6 44·0 46·5 47·5 45·0 46·5 54·7	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   31.4   39.5   33.9   36.7   46.5   30.2   34.8   39.7   36.2   26.7   31.0   40.7   35.6	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat., and haze Clouded; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze Densely clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze Mostly clear Mostly clear Mostly clear Partially clouded; cir., circum., and cirstrat. Clouded till 3 ^h , with circum. and cirstrat. Clouded till 17 ^h ; remainder clouded; circum., cirstrat., and haze Clouded all day; circum., cirstrat., and haze; slight rain from 6 ^h to 10 ^h , and some during the night Clouded all day; cumstrat. and circum. Clouded all day; cumstrat., cirstrat., circum., and haze; auroral light through the clouds at night Clouded all day; cirstrat., cirstrat., circum., and haze Mostly clouded; cirstrat., cirstrat., and haze Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum., and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; circum. and cumstrat.	0.8 1.0 1.0 1.0 0.2 0.0 0.8 0.6 - 1.0 1.0 1.0 1.0 0.8 0.9 0.9 1.0	1.0 1.0 0.2 1.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0 1	1'0 1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'1 0'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0 1'0	1.0 1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0 1.0 1.0 1.0 0.2 0.5 1.0 0.2 0.8 0.0	49·3 51·8 57·8 58·5 57·7 52·0 61·0 50·0 57·4 54·6 48·0 61·0 58·6 61·8 39·4 36·6 44·0 46·5 47·5 45·0 46·5 54·7 51·0	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   31.4   39.5   33.9   36.7   46.5   30.2   34.8   39.7   36.2   26.7   31.0   40.7   35.6   37.9	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze Clouded; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze Densely clouded all day; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze Mostly clear Mostly clear Mostly clear Partially clouded; cir., circum., and cirstrat. Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear Quite clear till 17 ^h ; remainder clouded; circum., cirstrat., and haze Clouded all day; circum., cirstrat., and haze; slight rain from 6 ^h to 10 ^h , and some during the night Clouded all day; cumstrat. and circum. Clouded all day; cumstrat., circum., and haze; auroral light through the clouds at night Clouded all day; cirstrat., and haze Mostly clouded; cirstrat., cirstrat., and haze Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and at 21 ^h ; remainder clouded; circum. and cumstrat. Clear from 9 ^h to 11 ^h , and at 21 ^h ; remainder clouded; circum. and cumstrat. Clear till 17 ^h ; remainder clouded; cirstrat. and haze Clouded all day; cirstrat. and haze	0.8 1.0 1.0 1.0 0.2 0.0 0.8 0.6 - 1.0 1.0 1.0 1.0 0.8 0.9 0.9 1.0 0.9 0.0 0.0	1.0 1.0 0.2 1.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0 1	1'0 1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'1 0'0 1'0 1'0 1'0 0'3 1'0 0'3 1'0 0'0	1.0 1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0 1.0 1.0 1.0 0.2 0.5 1.0 0.2 0.8 0.0	49·3 51·8 57·8 58·5 57·7 52·0 61·0 50·0 57·4 54·6 48·4 59·0 48·0 61·0 58·6 61·8 39·4 36·6 44·0 46·5 47·5 54·7 51·0 47·0	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   31.4   39.5   33.9   36.7   36.7   30.2   34.8   39.7   36.2   26.7   31.0   40.7   35.6   37.9   34.8	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze Clouded; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze Densely clouded; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze Mostly clear Mostly clear Mostly clear Mostly clear Partially clouded; cir., circum., and cirstrat. Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear Quite clear till 17 ^h ; remainder clouded; circum., cirstrat., and haze Clouded all day; circum., cirstrat., and haze; slight rain from 6 ^h to 10 ^h , and some during the night Clouded all day; cumstrat. and circum. Clouded all day; cumstrat. and circum. Clouded all day; cirstrat., cirstrat., circum., and haze; auroral light through the clouds at night Clouded all day; cirstrat. and haze Mostly clouded; cirstrat., cirstrat., and cumstrat. Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum., and haze; aurora at 9 ^h Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat. Clear from 9 ^h to 11 ^h , and at 21 ^h ; remainder clouded; circum. and cumstrat.	0.8 1.0 1.0 1.0 0.2 0.0 0.8 0.6 - 1.0 1.0 1.0 1.0 0.8 0.9 0.9 1.0	1.0 1.0 0.2 1.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0 1	1'0 1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'0 1'0 1'0 1'0 1'0 1'0 0'3 1'0 1'0 0'0	1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0 1.0 1.0 0.2 0.5 1.0 0.2 0.8 0.0	49·3 51·8 57·8 58·5 57·7 52·0 61·0 50·0 57·4 54·6 48·0 48·0 61·0 58·6 61·8 39·4 36·6 44·0 46·5 47·5 45·0 47·0 51·2	44.1 47.7 51.5 46.7 44.5 46.6 40.2 31.3 49.5 24.5 31.4 39.5 36.7 30.2 34.8 39.7 36.2 26.7 31.0 40.7 35.6 37.9 34.8 38.2	0.5
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	Clouded; cirstrat. and haze; slight rain from 0 ^h to 9 ^h Mostly clouded; cirstrat. and haze Clouded; circum., cirstrat., and haze Mostly clouded; circum., cirstrat., and haze Densely clouded all day; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum., cirstrat., and haze; rain from 5 ^h to 8 ^h Partially clouded; circum. and cumstrat.; aurora at night Clear till 4 ^h ; remainder clouded; circum., cumstrat., and haze Mostly clear Mostly clear Mostly clear Partially clouded; cir., circum., and cirstrat. Clouded till 3 ^h , with circum. and cirstrat.; remainder of day clear Quite clear till 17 ^h ; remainder clouded; circum., cirstrat., and haze Clouded all day; circum., cirstrat., and haze; slight rain from 6 ^h to 10 ^h , and some during the night Clouded all day; cumstrat. and circum. Clouded all day; cumstrat., circum., and haze; auroral light through the clouds at night Clouded all day; cirstrat., and haze Mostly clouded; cirstrat., cirstrat., and haze Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum., cirstrat., and cumstrat. Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and cumstrat; rain Mostly clouded; circum. and at 21 ^h ; remainder clouded; circum. and cumstrat. Clear from 9 ^h to 11 ^h , and at 21 ^h ; remainder clouded; circum. and cumstrat. Clear till 17 ^h ; remainder clouded; cirstrat. and haze Clouded all day; cirstrat. and haze	0.8 1.0 1.0 1.0 0.2 0.0 0.8 0.6 - 1.0 1.0 1.0 1.0 0.8 0.9 0.9 1.0 0.9 0.0 0.0	1.0 1.0 0.2 1.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0 1	1'0 1'0 1'0 1'0 1'0 1'0 0'5 0'8 0'0 0'4 1'0 0'1 0'0 1'0 1'0 1'0 0'3 1'0 0'3 1'0 0'0	1.0 1.0 1.0 1.0 1.0 0.0 0.4 0.0 0.4 1.0 1.0 1.0 1.0 0.2 0.5 1.0 0.2 0.8 0.0	49·3 51·8 57·8 58·5 57·7 52·0 61·0 50·0 57·4 54·6 48·4 59·0 48·0 61·0 58·6 61·8 39·4 36·6 44·0 46·5 47·5 54·7 51·0 47·0	44.1   47.7   51.5   46.7   44.5   46.6   40.2   31.3   49.5   24.5   31.4   39.5   33.9   36.7   36.7   30.2   34.8   39.7   36.2   26.7   31.0   40.7   35.6   37.9   34.8	0.5

Toronto Mean	Woodbar and Dharaman	E:	xtent of (	Cloudy SI	cy.	Max.	Min.	Rain.
Time.	Weather and Phenomena.	3	9	17	21	Therm.	Therm.	Tuttii.
D.	NOVEMBER.					0	0	In.
1	Mostly clear; some cumstrat. and cirstrat. round horizon	0.4	0.1	0.4	0.1	46.6	37.8	
$\frac{2}{3}$	Nearly clear at 9h; remainder clouded; cumstrat., circum., and cirstrat.	1.0	0.4	1.0	1.0	44.3	31.9	
4	Clouded; circum., cirstrat., and haze	1.0	$\frac{1.0}{1.0}$	1.0	1.0	38.9 43.2	$\frac{31.6}{39.2}$	0.41
5	Mostly clouded; circum, cumstrat., and haze; rain till 17 ⁿ		_	1.0	1.0	49.0	$\frac{35.7}{35.7}$	
6	Mostly clouded; circum. and cumstrat	0.3	0.9	1.0	1.0	40.0	32.3	
7	Mostly clouded; cirstrat. and haze; some particles of snow	0.9	0.3	0.8	1.0	42.0	26.9	
8	Mostly clouded till 9h; cirstrat. and haze; remainder clear; some snow from 6h to 9h	1.0	1.0	0.1	0.0	35.7	24.8	
9	Mostly clouded; cirstrat, and haze	0.8	0.0	1.0	1.0	33.6	20.1	
10 11	Clouded all day; cirstrat. and haze; some faint auroral light at 11h	1.0	1.0	1.0	1.0	$\frac{28.0}{29.4}$	15.9	_
12	Clouded all day; circum, and cirstrat.; some slight snow Clouded all day; cirstrat, and haze	_		1.0	1.0	31.6	$\frac{25 \cdot 2}{25 \cdot 2}$	
13	Clouded all day; cirstrat, and haze; some very slight snow at 11 ^h	1.0	1.0	1.0	1.0	27.6	25.2	
14	Clouded all day: circum, and haze: slight rain at 10 ^h and 11 ^h	1.0	1.0	1.0	1.0	3415	31.9	0.03
15	Clear at 9h and 10h; remainder clouded; circum, and haze	0.8	1.0	0.0	1.0	40.6	33.5	
16	Clouded till 4h; remainder partly clear; circum, and haze; auroral light from 10h	1.0	0.4	0.5	0.7	39.2	35.4	
17 18	Mostly clouded; circum. and cirstrat.; very brilliant aurora at night	1.0	0.4	1.0	0.1	$\frac{43.2}{37.7}$	$\frac{28.7}{26.1}$	_
18	Mostly clouded; cir. cum. and cumstrat.; some slight appearance of aurora at night			1.0	1.0	33.4	26.2	
20	Clouded all day; some slight auroral light at night  Mostly clear	0.0	0.0	0.6	1.0	33.0	30.5	
21	Generally clear; aurora from 7 ^h to 11 ^h ; moderately bright -	0.1	0.0	0.0	0.5	38.8	21.7	_
22 {	Clouded from 2 ^h to 10 ^h , and at 21 ^h ; circum. and cirstrat.; remainder mostly clear; faint auroral light from 9 ^h to 11 ^h	1.0	0.9	0.0	1.0	41.1	27.7	-
23 {	Clear from 9 ^h to 11 ^h ; remainder clouded; cirstrat., circum., and haze; faint auroral light at 11 ^h	0.9	0.0	1.0	1.0	40.8	26.9	
24	Clouded all day; circum., cirstrat., and haze; constant light rain till 8h	1.0	1.0	1.0	1.0	43.0	29.8	0.89
25	Clouded all day; circum. and cumstrat.; rain and sleet till 4 ^h	1.0	1.0	-		44.6	32.7	0.22
26	Clouded all day; cir-cum. and cumstrat; aurora from 10h to 12h -	0.7	$\frac{-}{0.4}$	$\frac{1.0}{1.0}$	$\frac{1.0}{1.0}$	38°1 30°8	$\frac{28.7}{20.6}$	
27 28	Mostly clouded; cirstrat. and circum.; faint auroral light at night Mostly clouded; cumstrat. and cirstrat	0.5	0.9	1.0	1.0	$\frac{30.8}{32.4}$	$\frac{20.6}{29.7}$	_
	Clouded; cirstrat. and haze; rain from 2 ^h to 11 ^h ; heavy squall of wind at 16 ^h ; wind		l	1	Į.	}		
29 {	continuing high	1.0	1.0	1.0	1.0	41.0	35.7	0.45
30	Clouded all day; circum. and haze	1.0	1.0	1.0	1.0	41.4	29.5	
	DECEMBER.				ļ			
1	Clouded all day; circum, and cumstrat.; snow from 3h to 9h; turned to rain -	1.0	1.0	1.0	0.9	38.0	23.7	0.20
2	Mostly clouded; circum. and cumstrat.; rain	0.8	0.6	_			22.2	0.78
3	Clouded; circum., cumstrat, and haze	1:0	1:0	1.0		40.4	33.2	
4	Clouded; circum., cirstrat., and haze; slight snow at 17 ^h Clouded; circum., cirstrat., and haze; snow at intervals	$\begin{bmatrix} 1.0 \\ 1.0 \end{bmatrix}$	$\frac{1.0}{1.0}$	1.0	$\frac{1.0}{1.0}$	$\frac{38.0}{3}$	$\frac{28.9}{28.9}$	
5 6	Clouded; cirstrat. and haze; drizzling rain, freezing as it falls from 2 ^h	1.0	1.0	1.0	1.0	31.1	$\frac{26.9}{26.2}$	0.22
7	Clouded; circum. and haze; drizzling most of the day	1.0	1.0	1.0	0.8	29.0	$\frac{26.2}{26.2}$	0.39
8	Partly clear; circum. and cirstrat. general	0.0	1.0	0.3	1.0	35.0	30.7	
9	Clouded; cirstrat. and haze; sleet and rain from 9 ^h	1.0	1.0			48.8	27.7	0.25
10	Mostly clouded; some rain			1.0	1.0	34.4	31.8	0.32
11	Clouded; cumstrat	1.0	1.0	1.0	1.0	46.6	26.2	_
12 13	Mostly clouded; cirstrat., cumstrat., and haze	$\frac{0.0}{1.0}$	$0.3 \\ 1.0$	$0.4 \mid 0.2 \mid$	$\frac{0.7}{0.8}$	30.1	$\frac{23.5}{22.2}$	_
14	Clear from 2 ^h to 4 ^h ; remainder clouded; circum. and haze	0.0	1.0	0.8	0.1	34.2	$\frac{27.7}{27.7}$	
15	Clouded from 10 ^h to 21 ^h ; circum. and cirstrat.; remainder clear; slight snow at 19 ^h	0.0	0.0	1.0	1.0	42.0	32.2	_
16	Mostly clouded; circum. and cumstrat	0.8	0.9			35.6	27.5	
17	Clouded; cirstrat. and haze		- !	1.0	1.0	43.9	32.7	_
18	Clouded; circum. and cumstrat.; faint appearance of auroral light at 10 ^h and 11 ^h	1.0	0.9	1.0	1.0	38.0	31.7	
19 20	Clouded; dense; circum. and haze	$\frac{0.4}{1.0}$	$\frac{1.0}{1.0}$	$\frac{1.0}{1.0}$	$\frac{1.0}{1.0}$	$\frac{41.7}{48.6}$	$\frac{32.7}{21.9}$	
$\frac{20}{21}$	Clouded; dense; haze; snowing and drift	1.0	1.0	1.0	1.0	59.0	$\frac{19.3}{21.9}$	_
$\frac{21}{22}$	Mostly clouded; circum. and haze; snowing and drift till 3h	1.0	1.0	0.6	1.0	20.6	8.1	
23 {	Mostly clouded; circum. and cirstrat.; some slight snow from 19h, which turned to rain	0.9	1.0			12.8	1.1	
24	at $21\frac{1}{2}$ h			1.0	1.0	25.6	18.0	0.24
$\frac{24}{25}$	Clouded; circum. and haze; rain, which ceased at 2 ^h Clouded; circum. and cumstrat	1.0	1.0			33.0	23.6	
26 26	Mostly clouded; circum. and cumstrat.	1.0	0.6	1.0	1.0		$\frac{23.0}{21.0}$	_
27	Clouded till 11 ^h ; circum. and cirstrat; snow from 0 ^h to 10 ^h ; cleared up	1.0	1.0	0.0	0.0	24.3	15.2	
28	Clear till 3h; remainder clouded; circum. and cirstrat	0.0	1.0	0.6	1.0	33.1	15.7	
29	Mostly clouded; circum. and haze; clear at 17 ^h	0.8	0.4	0.0	0.4	30.6	27.5	
30	Clear from 2 ^h to 4 ^h ; remainder clouded; cirstrat. and cumstrat Mostly clouded; cirstrat. and cumstrat	0.0	1.0	<u></u>	0.6	34.2	11.4	
31	Mostly clouded; cirstrat. and cumstrat			0.7	0.6	31.7	15.7	

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